

Report On

Moosehorn Range Area Placer Exploration Project

Swamp Creek Definition Drill Program

EIP 88053

February - March 1989

Whitehorse Mining Division

N.T.S.: 115-N-2

63°05'N Latitude; 140°55'W Longitude

Owned by:

CLAYMORE RESOURCES LTD.
11003-84th Avenue
Edmonton, Alberta
T6G 0V6

120113

Optioned by:

CANADA TUNGSTEN MINING CORPORATION LIMITED
Executive Office
Box 12525, Oceanic Plaza
Ste. 1600-1066 West Hastings Street
Vancouver, B.C. V6E 3X1

S.C. Bartlett, M.Sc.
Senior Geologist

May 1989

120113

MAY 15 1989



RECEIVED
MINES

EIP88-053
Vol. 1 of 2

Summary

Rotary drilling was carried out at the Swamp Creek, Yukon placer gold mine during March and February 1989. A total of 653 meters (2,142 ft) of drilling was completed in 77 holes. Drilling delineated pay gravel along a 2.6 kilometer (1.6 miles) length of Swamp Creek. In conjunction with the drilling, 5,335 meters (17,500 ft) of magnetometer survey was conducted along 1.35 kilometers (0.84 miles) of Swamp Creek.

Global reserves outlined by rotary drilling and magnetometer survey are 1,585,000 cubic meters (2,073,000 yd³) containing 561 kilograms (18,050 oz.) of gold. The average grade of pay gravel is 0.35 grams per cubic meter (0.009 oz/yd³).

Pay gravel is overlain by 2,419,000 cubic meters (3,164,000 yd³) of overburden for an average strip ratio of 1.5.

The total cost of the program was \$189,615.00. This equates to \$291.00 per meter (\$89/ft) drilled or \$338.00 per kilogram (\$11/oz.) of gold indicated. Twenty-five percent of the cost, to a maximum of \$45,000.00, is eligible for reimbursement through the Yukon Government Exploration Incentives Program agreement EIP 88053.

Table of Contents

	Page
Summary	i
1.0 Introduction	1
1.1 Location and Access	1
1.2 Claim Status	3
1.3 Previous Work	3
1.4 Bibliography	5
2.0 Present Work/Budget	6
2.1 Definition Drilling	7
2.2 Magnetometer Survey	10
3.0 Pay Gravel Reserves	13
4.0 Conclusions	14
5.0 Recommendations	15
Appendix I	
Back Up To Financials	
Appendix II	
Table 1 Summary Of Drill Holes	
Table 2 Sample Logs	
Appendix III	
Magnetic Profiles	
Magnetic Anomaly Maps	
Appendix IV	
Table 3 Pay Gravel Intercepts	
Table 4 Pay Gravel Reserves	

List of Figures

Figure 1.	Swamp Creek Location Map - Yukon
Figure 2.	Claim Map
Figure 3.	Drill Hole Location
Figure 4.	Section 800S
Figure 5.	Section 850S
Figure 6.	Section 900S
Figure 7.	Section 950S
Figure 8.	Section 1000S
Figure 9.	Section 1050S
Figure 10.	Section 1150S
Figure 11.	Section 1250S
Figure 12.	Section 1350S
Figure 13.	Section 1500S
Figure 14.	Section 1650S
Figure 15.	Section 2100S
Figure 16.	Section 2400S
Figure 17.	Section 2700S
Figure 18.	Section 3000S
Figure 19.	Section 3300S
Figure 20 A	Swamp Creek Magnetometer Survey - Sheet 1
Figure 20 B	Swamp Creek Magnetometer Survey - Sheet 2
Figure 20 C	Swamp Creek Magnetometer Survey - Sheet 3
Figure 20 D	Swamp Creek Magnetometer Survey - Sheet 4

CANADA TUNGSTEN MINING CORPORATION LIMITED
MOOSEHORN RANGE AREA PLACER EXPLORATION PROJECT
SWAMP CREEK DEFINITION DRILL PROGRAM
SWAMP CREEK, YUKON

1.0 INTRODUCTION

A rotary drilling program was carried out at the Swamp Creek mine during February and March 1989. The purpose of the program was to delineate pay gravel reserves so as to extend the mine life and permit more effective short and long term planning. Reserves were defined using a combination of rotary drill holes and the results of a magnetometer survey. This report provides a summary of the field work carried out and costs required to complete the work. Global pay gravel reserves outlined by this program are tabulated and presented.

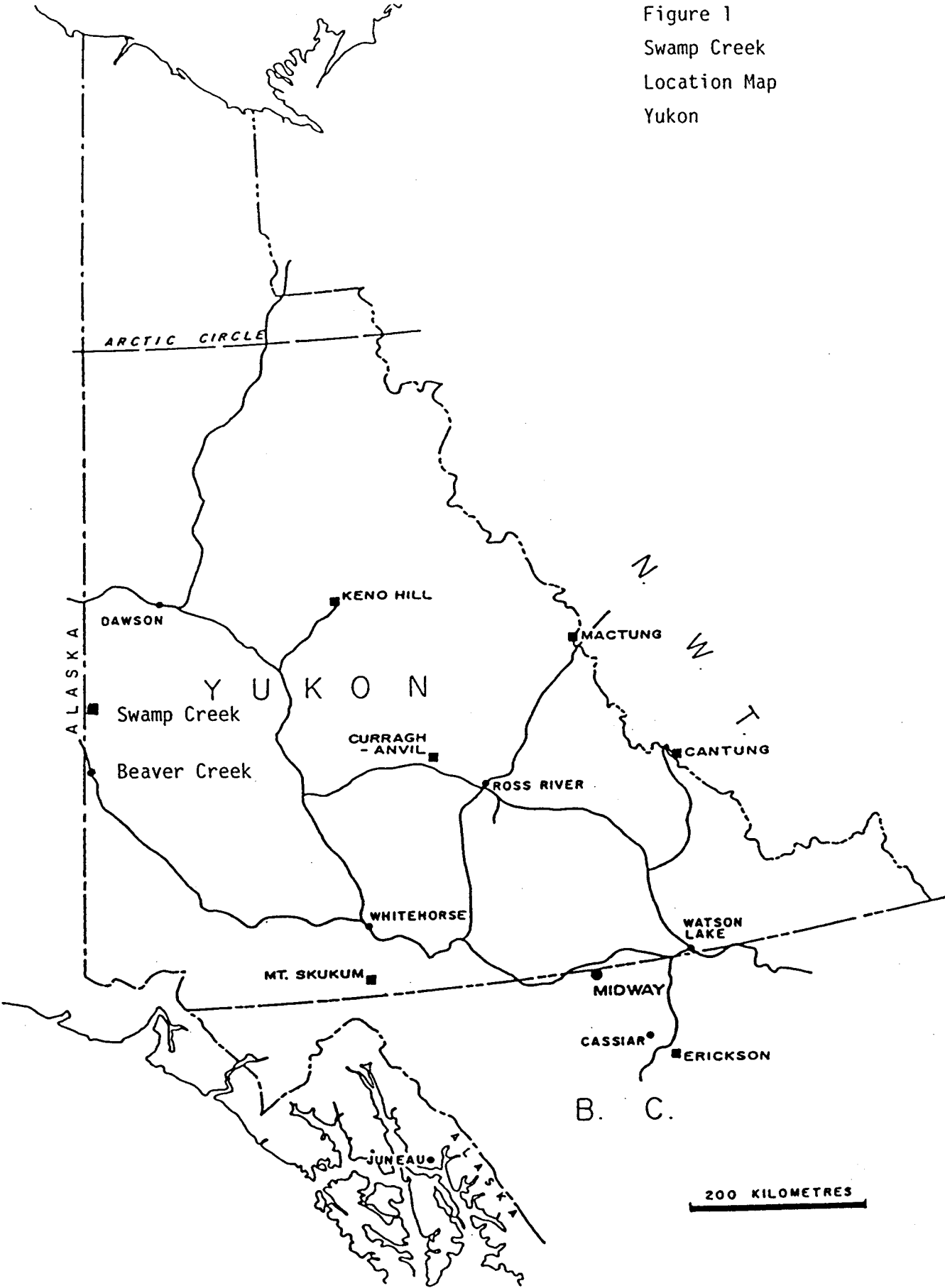
The project was funded by Canada Tungsten Mining Corporation Limited. Twenty-five per cent of the cost to a maximum of \$45,000 is eligible for reimbursement through the Yukon Government Exploration Incentives Program agreement EIP88053.

1.1 LOCATION AND ACCESS

The Swamp Creek mine is situated on the southwest slope of the Moosehorn Range on the Ladue River map sheet, N.T.S. 115-N-2. The property lies approximately 400 kilometers northwest of Whitehorse and 140 kilometers southwest of Dawson City.

During the operating season supplies must be air freighted from Whitehorse utilizing the 600 meter long Claymore airstrip. The airstrip is located six kilometers north of the camp. During the winter months heavy equipment and supplies are transported over a 70 kilometer winter road from Beaver Creek, Yukon.

Page 2
Figure 1
Swamp Creek
Location Map
Yukon



1.2 CLAIM STATUS

Claim status at the Swamp Creek mine is summarized below.

<u>Name</u>	<u>Grant No.</u>	<u>Anniversary</u>	<u>Type</u>	<u>No. Claims</u>	<u>Owner</u>
Deer 1	P3128	Mar 25, 1990	Creek	1	Claymore
Red 1	P3129	Mar 25, 1990	Creek	1	Claymore
Soya 1	P3132	Mar 25, 1990	Creek	1	Claymore
Deer 2-9	P3135-P3142	Apr 20, 1990	Creek	8	Claymore
Red 2-12	P3154-P3164	Apr 20, 1990	Creek	11	Claymore
Soya 2-9	P3170-P3177	Apr 20, 1990	Creek	8	Claymore
Beef 1-5	P3485-P3489	Apr 19, 1990	Creek	5	Claymore
Tracy 1	P27418	Jun 16, 1990	Creek	1	P. Thompson
Hoho 1-2	P3345-P3346	Jul 7, 1990	Creek	2	Claymore
M 1-13	P25800-P25812	Oct 3, 1990	Creek	13	Claymore

A claim map is presented in Figure 2.

1.3 PREVIOUS WORK

Lode gold was first discovered on the crest of the Moosehorn Range by Quintana Minerals Limited in 1970. In 1975 Claymore Resources Ltd. discovered placer gold in Discovery (Kenyon) Creek and also in Swamp and Great Bear Creeks. Exploration work was carried out on Kenyon Creek in 1975 and 1976 and test mining began in 1976. In 1977 the placer claims were optioned to Goldwin Consulting Ltd. and Goldwin managed production on Kenyon Creek from 1977 to 1986. During this time 623 kilograms of fine gold was produced from 239,000 cubic meters of pay gravel (2.6 g/m³). With reserves at Kenyon Creek depleted mining shifted to Swamp Creek. In 1987 104 kilograms of fine gold was recovered from 19,000 cubic meters (5.5 g/m³) of pay gravel. Canada Tungsten Mining Corporation Limited purchased Goldwin's option on the Moosehorn Range area placer claims in 1988 and produced 137 kilograms of fine gold from 42,000 cubic meters of gravel (3.3 g/m³).

At the end of 1988 no formally defined pay gravel reserves existed at Swamp Creek but encouraging "colours" were obtained from four small test pits downstream from the 1987 cut. These pits were essentially 10m x 10m test pits excavated to bedrock using a backhoe. The pits were channel sampled and the samples were concentrated in a short sluice box and the concentrate amalgamated. While these samples provided encouragement they provided almost no information about the volume of available gravel and grade continuity.

The lack of systematically defined ore reserves for mine planning dictated the need for a formal exploration program. In an attempt to assess the potential benefit of a drill program three Airtrac holes were drilled near the test pits. All three holes were abandoned due to unstable hole conditions in the overburden. In a second test overburden was stripped from an area measuring 215m x 25m and 21 Airtrac holes were drilled to bedrock. While the quality of the sample data was suspect the average grade of 19 holes was 2.1 g/m³. The Airtrac holes indicated that pay gravel volume and grade could be determined by a systematic drill program and subsequently the 1989 definition drilling program was designed and carried out.

1.4 BIBLIOGRAPHY

Debicki, R.L., 1983, Yukon Placer Mining Industry 1978 - 1982,
Indian and Northern Affairs Canada.

Morin, J.A., et al, 1977, North of 60 - Mineral Industry Report,
1976, Yukon Territory, Canada, Indian and Northern Affairs
Canada, Report EGS 1977-1.

Sinclair, W.D., 1976, North of 60 - Mineral Industry Report, 1975,
Yukon Territory, Canada, Indian and Northern Affairs Canada,
Report EGS 1976-15.

2.0 PRESENT WORK/BUDGET

The Swamp Creek definition drilling program was carried out during February and March 1989. Work conducted included 673 meters of rotary drilling and 5,335 meters of magnetometer survey. A total of 299 man days were required to complete the field work at a total cost of \$189,615. A summary of costs for the program is presented below. Supporting documentation is provided in Appendix I. The supporting documentation includes a list of all personnel engaged in the project and their respective employers.

Final Budget - May 5, 1989 Swamp Creek - Definition Drilling

Salaries	13,927
Temporary Personnel	24,745
Overhead & Fringes	3,867
Fuel	13,912
General Consumables	2,940
Camp Materials/Food	16,445
Maps & Reports	110
Tools & Equipment Rentals	15,351
Vehicles Rental	3,000
Aircraft Charters	1,612
Assaying	953
Survey Contractor	7,735
Exploration Drilling	60,418
Metallurgical Contractor	8,146
Geophysics Contractor	4,801
Telephone, Fax	722
Travel	4,317
Freight	1,364
Insurance	<u>5,250</u>
TOTAL	189,615

2.1 DEFINITION DRILLING

During the 1989 definition drilling program 77 rotary drill holes were completed for a total of 673 meters. Holes were drilled on 16 grid lines over a 2.6 kilometer length of Swamp Creek. Lines were spaced at 50 to 300 lines. Hole numbers such as 800-1, indicate line designation in meters on the Swamp Creek survey grid and site location on the line. A plan of drill holes is presented in Figure 3 and a summary of drill holes is provided on Table 1 in Appendix II.

All drilling was contracted to E. Caron Diamond Drilling Ltd. of Whitehorse, Yukon. Caron supplied a track-mounted, Schram T64H rotary drill rig and all drilling equipment. Drilling operated on two 12 hour shifts per day, 7 days per week. A drill crew consisted of a driller and a drill helper/sampler supplied by Caron, and a geologist representing Canada Tungsten.

The first holes completed were drilled using 15.2 centimeter tricone bits and reverse circulation (12.7cm) dual tube, centre sampling rods. In this system drill cuttings pass through the tricone bit and flush upwards to the collar, using 650 cfm air pressure. This method proved to be ineffective in the Swamp Creek environment due to mud packing, and the remainder of the drilling was carried out using conventional drill rods and casing.

The conventional system consisted of a 15.2 centimeter tricone bit with 7.9 centimeter rods. Casing (15.2cm I.D.) was advanced 0.6 to 2.0 meters ahead of the bit and the cased gravel core was drilled out. In this system 650 cfm air pressure was directed down the drill stem, through the tricone bit. Cuttings returned to the collar along the void between the casing and drill stem. Although this method provided better quality samples, the drilling was slow and production was approximately one-quarter of that anticipated using the reverse circulation method.

The original plan was to drill without casing using reverse circulation equipment. In overburden a plug was to be placed in the inner tube of the drill string at the bit. Cuttings would be directed upwards between the hole wall and the outside wall of the drill stem. This would prevent contamination of the inner tube and sampling system with sticky black mud. In gravel the plug was to be removed and gravel cuttings were to travel upwards through the inner tube of the drill stem. The success of this plan was contingent on establishing a stable hole wall in frozen ground.

Two seasons of previous mining and numerous test pits indicated that both overburden and gravel would be frozen. Drilling problems were encountered immediately with reverse circulation equipment as black mud (overburden) jammed between the hole wall and drill stem. This resulted in extreme contamination of gravel cuttings. It became apparent that overburden and gravel are variably frozen. Thawed sections of black mud were rapidly liquified when subjected to 70°C air compressed to 650 cfm, and drill vibration.

To prevent contamination of gravel cuttings modifications were made to the drill system and, conventional drill rods and casing were employed. Casing was driven ahead of the tricone bit using a casing hammer. The casing was advanced 0.6 to 2.0 meters and the resulting core was drilled out. This method provided a stable hole wall and usually prevented influxes of water. Casing was initially cut to 3.0 meter lengths then welded as each new length was required. This extra work further contributed to lower production and higher costs.

Under favourable ground conditions this method proved to be very effective in recovering uncontaminated gravel cuttings. Evidence of this quality lies in the low variance of sample volumes from dry holes. Where ground conditions would permit, sample quality was sacrificed to increase production. Here, casing was only driven into the top 0.6 meters of gravel. The hole wall was supported only by gravel. The potential for contamination under these conditions must be noted.

Another noteworthy problem encountered was the contamination of the casing by black mud. The black mud proved to be of extremely sticky consistency. In overburden mud would frequently jam the bit and jam between the inside wall of the casing and the drill stem. This problem was overcome by reducing the advance rate of the bit. Even at the reduced rate mud was found to line the inside of the casing. This material had two effects; first, it tended to rob particles (wood, pebbles and possibly gold) from material cut further down the hole and deplete samples and, second, would later rip off the casing wall and contaminate gravel cuttings also from further down the hole. This second effect made recognition of gravel and bedrock contacts very difficult.

SAMPLING

Sampling of drill cuttings was restricted, where possible, to the pay gravel and bedrock formations. A sample interval of 0.6 meters was chosen to accurately define gravel contacts and to maintain a manageable sized sample. For a 15.2 centimeter diameter hole the theoretical sample volume is 11.12 liters. Assuming an average specific gravity of 1.75 for gravel the expected weight of a sample of this size is 19.5 kilograms. Approximately 515 samples were collected during the program and, after compositing samples and discarding overburden and bedrock samples, 440 were washed and concentrated.

Gravel cuttings were directed to a cyclone and into 91cm x 53cm 0.13mm sample bags. The bags were labelled and tagged and transported to a clean-up area. In the clean-up shack samples were sorted, and logged for volume, weight, colour, texture and moisture content. One geological technician was employed to organize and log samples.

Samples were concentrated using a 24.1 centimeter HY-G Concentrator. The HY-G Concentrator utilized a 6.4mm wet, vibrating screen and riffled, fluid bed centrifuge. Sample volumes were reduced from an average of 11.0 liters to 2.5 liters, a ratio of concentration of 4.4. Screen reject was collected and logged for rocktype and texture. The HY-G unit required one operator and was capable of processing 20 to 35 samples per 10 hour shift, depending on clay content. The concentrator was supplied by HY-G Manufacturing of Vancouver, B.C.

Sample concentrates were amalgamated on site using 4.5 liter amalgam barrels. Gold particles were scrubbed prior to amalgamation by adding about 5 grams of NaOH powder to the HY-G concentrates. Mercury was added to the concentrates in the ratio of 1 cubic centimeter of mercury to 2.5 liters of concentrate. The amalgam barrel was rolled for one-half hour and the mercury amalgam was recovered using a 46 centimeter wet, tilting spiral wheel. The heavy mineral concentrate produced by the wheel was bagged and logged. The mercury amalgam product was dissolved in hot, dilute nitric acid, diluted in a ratio of one acid to two distilled water. On solution of the mercury free gold precipitated in the acid solution. The mercury pregnant, acid solution was decanted and free gold was dried and recovered. Gold was stored in vials and shipped to Bacon, Donaldson & Associates Ltd. of Vancouver for cupellation and weighing. Sample logs are presented in Table 2 in Appendix II.

2.2 MAGNETOMETER SURVEY

Pay gravels in the Moosehorn Range area are notably enriched in magnetite and at bedrock contain up to 25 kilograms per yard or more. It was decided to conduct a limited magnetometer survey to determine if the magnetic susceptibility of the pay gravel was distinct enough to be discerned from the background signature of the granitic bedrock.

On-Line Exploration Services Inc. of Anchorage, Alaska was engaged to carry out the test survey. On-Line has extensive experience in placer magnetics and uses the EDA OMNI-IV Tie-line magnetometer system. This system utilized two proton precession magnetometers; a field unit to record and store total field and gradient readings and, a continuous recording base station to measure and record diurnal drift. Base station readings were recorded every 10 seconds and field readings were corrected for drift automatically by interfacing the two magnetometers.

The survey covered 5,335 meters on 15 lines. Lines were variably spaced at 50, 75 and 150 meters, measurements were recorded at 5 meter intervals along the lines. The lines surveyed are listed below. Line numbers correspond to the Swamp Creek survey grid.

<u>LINE</u>	<u>LENGTH</u> <u>(m)</u>	<u>LINE</u>	<u>LENGTH</u> <u>(m)</u>
1200S	200	1725S	320
1250S	250	1800S	310
1300S	460	1950S	310
1350S	370	2100S	345
1425S	450	2250S	330
1500S	355	2400S	545
1575S	340	2550S	425
1650S	325		

Total field and gradient profiles were generated and interpretive plans were drawn. Both the profiles and interpretive maps are presented in Appendix III.

Generally, the survey proved very successful as the magnetic response of the pay gravel was readily distinguished. Pay gravels display a strong and highly irregular gradient signature that masks the underlying bedrock response. Where gravel is absent the total field strength of the basement rocks is predominant. Swamp Creek demonstrated a broad, strong magnetic gradient anomaly upstream, at Line 1200S and a weaker, more restricted anomaly 1,350 meters downstream, at Line 2550S. The west limit of the pay gravel is well defined by the sudden predominance of the total field signature of the bedrock. The eastern margin is not so well defined but may be indicated by the strong total field anomaly believed to represent a fault. The magnitude of the gradient anomaly appears to be influenced by the depth of overburden though no work has been done to define this relationship.

While Morin (1977), has described the geology of the Moosehorn Range area the detailed geology of the Swamp Creek area is largely unknown. Outcrop is sparse and exposure is limited to road cuts and placer workings. Several rock types are present in the area among which include granodiorite, dykes, hornblende and feldspar porphyries, and younger, crosscutting dacite dykes. All of these rock types occur at Swamp Creek and their varying influence on the total field and gradient data collected is problematic. Also, some bedrock structures had pronounced magnetic signatures and obliterated gradient responses locally. Interpretation of some of the data is difficult and more geological information is required to fully explain the survey results.

3.0 PAY GRAVEL RESERVES

A global estimate of pay gravel reserves and overburden was prepared using the 1989 drill data. Pay gravel volume was calculated using a simple sectional method in which the cross-sectional area of a drill section was multiplied by half the length to adjacent sections. The limits of pay gravel on each section was defined by either borehole data or by the magnetometer survey. To determine the overburden volume a slope of 65° was measured to surface from the limit of pay gravel. Volume was again estimated by measuring cross-sectional area and projecting the block length half the distance to adjacent sections.

Borehole grades were calculated for the total gravel interval intersected in the hole. Grades were projected only to bedrock and no contingency was allowed for bedrock dilution. Gold recovered from samples logged as bedrock was assumed to have fallen down the hole and was assigned to the lowest stratigraphic gravel sample. Sample grades were determined by dividing the gold recovered by the sample volume measured in the field. Grades were then adjusted 15 percent to express bank volumes. It was assumed that no positive bias was introduced in sampling and that sample material lost was of the same grade as the material recovered. Borehole grades are weighted averages of individual samples and include nil grades. No trimming functions or statistical transformations have been applied. A summary of gravel intercepts is presented in Table 3 of Appendix IV.

Section grades are weighted averages of bore hole composites. Again the data has not been subject to statistical transformations. The global pay gravel reserve tabulation is simply a sum of sectional volumes and a weighted average by volume of section grade.

Pay gravel reserves are 1,585,000 cubic meters containing 561 kilograms of fine gold. The average grade for the deposit is 0.35 grams per cubic meter. Pay gravels are overlain by 2,419,000 cubic meters of overburden for an average strip ratio of 1.5. Pay gravel and overburden volumes are summarized on Table 4 in Appendix IV.

4.0 CONCLUSIONS

Definition drilling on widely spaced lines at Swamp Creek indicates global pay gravel reserves of 1,585,000 cubic meters of pay gravel containing 561 kilograms of gold. Pay gravels are overlain by 2,419,000 cubic meters of partially frozen, black mud. The average strip ratio (waste:ore) for these reserves is 1.5.

Rotary drilling has provided reasonably precise data on the thickness of gravel and overburden in Swamp Creek. However, grade information obtained from the 1989 program is suspect. Two seasons of previous mining at Swamp Creek yielded 241 kilograms of gold from 61,000 cubic meters of pay gravel. The average grade of the material mined was 3.95 g/m³. The reserves outlined by the 1989 program are of considerably lower grade at 0.35 g/m³. Although based on a limited number of holes per section, the grade of pay gravel appears to decrease downstream. It is apparent that production grade control will become increasingly important as mining proceeds downstream.

In order to selectively mine pay gravel above a cutoff grade more sample data will be required. This data will likely be derived from closely-spaced grid drilling during the pre-season period and channel sampling cut walls in the post season. Channel sampling proved successful at the Dublin Gulch mine, operated by Canada Tungsten.

Borehole grades are highly variable and range from nil to 14.68 g/m³. It is believed that rotary drilling has significantly undervalued the upper portion of Swamp Creek. The grade of the pay gravel section drilled by Airtrac was 2.15 g/m³ compared with 1.69 g/m³ for rotary drill holes. If the two high grade holes drilled one meter apart on Line 900S are rejected then the grade of the same area is 0.85 g/m³. The relationship between expected and realized production grade will only be understood once a reconciliation of the 1989 production results is carried out.

The magnetometer survey proved to be successful in delineating the magnetite-bearing gravels in Swamp Creek. Valuable information about channel width was obtained at relatively low cost. More interpretive work is required to determine if more information, particularly overburden depth can be ascertained from magnetometer data.

5.0 RECOMMENDATIONS

To maintain suitable grade control, particularly on the west limit of the pay gravels, more drilling is required. Grid drilling using the Airtrac drill should be carried out on gravel prepared for the 1989 season. A grid spacing of 20 meters by 20 meters is recommended. The section to be mined in 1989 measures approximately 350 meters by 100 meters and would require approximately 100 holes. Samples should be collected in appropriate lengths so as to minimize interval contamination by bedrock.

The 1989 cut should be made in such a manner as to produce vertical final walls. The walls should be channel sampled by cutting vertical grooves measuring 15cm by 15cm by 150cm. Loose gravel from channels should measure approximately 40 liters. Channel samples should be collected at 15 meter intervals near the channel axis and 7.5 meter intervals at the margins. In addition to grade these samples should be examined for gold grain size and recoverability.

A test pitting program should be carried out on pay gravel reserves beneath shallow overburden. Test pitting would promote confidence in the volume and grade of pay gravels outlined by drilling. A suitable location for a test pit is near line 2400S where pay gravels are within two meters of surface near the creek.

A magnetometer survey should be carried out in Swamp Creek to fill-in holes left from the initial survey. Soya Creek, the camp creek, and the creek near Line 2400S should be surveyed. Effort should be made to calculate overburden depth from magnetometer data.

SCB:ms:1220A

May 8, 1989

APPENDIX II

TABLE 1 SUMMARY OF DRILL HOLES

TABLE 2 SAMPLE LOGS

TABLE 1

AII-1

FILE:SWBHSUM.WK1

MOOSEHORN RANGE EXPLORATION PROJECT
SWAMP CREEK MINE
SUMMARY OF 1989 DEFINITION DRILLING PROGRAM
FEBRUARY - MARCH 1989

BHID	START	FINISH	DEPTH (m)	OB THIK (m)	GRAV THIK (m)	BDRK (m)	CASING (m)	NOTES
800-1	FEB 21	FEB 21	9.1	3.7	1.8	3.7	0.0	REVERSE CIRCULATION
800-2	FEB 22	FEB 22	7.6	4.3	3.4	0.0	0.0	REVERSE CIRCULATION
800-2A	FEB 26	FEB 26	9.1	4.3	3.3	1.6	9.1	CONVENTIONAL / CASING
800-3	FEB 26	FEB 26	7.9	3.7	3.6	0.7	6.7	CONVENTIONAL / CASING
850-1	FEB 21	FEB 21	3.0	0.0	1.8	1.2	0.0	REVERSE CIRCULATION
850-2	FEB 21	FEB 21	3.0	0.0	1.2	1.8	0.0	REVERSE CIRCULATION
850-3	FEB 26	FEB 26	7.3	4.9	0.6	1.8	6.1	CONVENTIONAL / CASING
850-4	FEB 26	FEB 26	6.1	3.7	1.5	0.9	3.0	CONVENTIONAL / CASING
850-5	FEB 27	FEB 27	3.7	1.2	1.5	0.9	1.5	CONVENTIONAL / CASING
900-1	FEB 21	FEB 21	3.4	0.0	1.8	1.6	0.0	REVERSE CIRCULATION
900-2	FEB 21	FEB 21	3.4	0.0	1.8	1.6	0.0	REVERSE CIRCULATION
950-1	FEB 22	FEB 22	2.4	0.0	2.4	0.0	0.0	REVERSE CIRCULATION
950-2	FEB 22	FEB 22	2.4	0.0	2.4	0.0	0.0	REVERSE CIRCULATION
950-3	FEB 27	FEB 27	4.0	4.0	0.0	0.0	3.7	CONVENTIONAL / CASING
950-4	FEB 27	FEB 27	6.7	3.7	1.2	1.8	6.7	CONVENTIONAL / CASING
950-5	FEB 28	FEB 28	7.3	4.0	1.5	1.9	6.7	CONVENTIONAL / CASING
1000-1	FEB 22	FEB 22	4.3	0.0	4.3	0.0	0.0	REVERSE CIRCULATION
1000-2	FEB 22	FEB 22	3.7	0.0	3.7	0.0	0.0	REVERSE CIRCULATION
1000-3	FEB 22	FEB 22	3.7	0.0	3.7	0.0	0.0	REVERSE CIRCULATION
1000-4	FEB 28	FEB 28	10.4	6.7	2.4	1.3	6.7	CONVENTIONAL / CASING
1000-5	FEB 28	MAR 1	12.2	8.5	1.9	1.8	9.8	CONVENTIONAL / CASING
1000-6	MAR 1	MAR 1	7.3	5.5	0.6	1.2	6.7	CONVENTIONAL / CASING
1050-1	FEB 22	FEB 22	4.3	0.0	3.0	1.3	0.0	REVERSE CIRCULATION
1050-2	FEB 22	FEB 22	3.0	0.3	2.1	0.6	0.0	REVERSE CIRCULATION
1050-3	FEB 22	FEB 22	3.0	0.0	3.0	0.0	0.0	REVERSE CIRCULATION
1050-4	FEB 22	FEB 22	4.9	0.6	2.4	1.9	0.0	REVERSE CIRCULATION
1150-1	MAR 1	MAR 1	6.1	3.0	3.7	0.7	6.1	CONVENTIONAL / CASING
1150-2	MAR 1	MAR 1	5.5	1.8	2.5	1.2	3.7	CONVENTIONAL / CASING
1150-3	MAR 1	MAR 1	4.3	2.7	1.0	0.5	3.7	CONVENTIONAL / CASING
1150-4	MAR 1	MAR 1	9.8	7.3	1.2	1.2	9.8	CONVENTIONAL / CASING
1150-4A	FEB 22	FEB 22	6.1	6.1	0.0	0.0	0.0	REVERSE CIRCULATION WET MUD
1150-5	FEB 22	FEB 22	5.5	5.5	0.0	0.0	0.0	REVERSE CIRCULATION WET MUD
1250-1	MAR 2	MAR 2	4.3	3.7	0.3	0.3	3.7	CONVENTIONAL / CASING
1250-2	MAR 2	MAR 2	6.7	1.8	4.0	0.9	3.7	CONVENTIONAL / CASING
1250-3	MAR 2	MAR 2	7.3	3.0	3.1	1.2	3.7	CONVENTIONAL / CASING
1250-4	MAR 1	MAR 2	12.8	9.8	1.2	1.8	10.4	CONVENTIONAL / CASING
1250-6	FEB 22	FEB 22	6.1	3.0	3.0	0.0	0.0	REVERSE CIRCULATION
1250-7	FEB 22	FEB 22	7.3	7.3	0.0	0.0	0.0	REVERSE CIRCULATION WET MUD
1300-2	FEB 22	FEB 22	4.9	4.9	0.0	0.0	0.0	REVERSE CIRCULATION
1300-3	FEB 22	FEB 22	3.7	2.7	0.0	0.9	0.0	REVERSE CIRCULATION
1300-4	FEB 22	FEB 22	6.1	3.7	0.0	2.4	0.0	REVERSE CIRCULATION

SOYA-1	FEB 22	FEB 22	6.7	3.0	2.4	1.3	0.0	REVERSE CIRCULATION
SOYA-2	MAR 3	MAR 3	9.1	4.0	3.7	1.5	6.7	CONVENTIONAL / CASING
SOYA-3	MAR 3	MAR 3	10.4	5.8	2.1	2.5	6.1	CONVENTIONAL / CASING
SOYA-4	MAR 3	MAR 3	4.3	2.4	1.0	0.8	3.7	CONVENTIONAL / CASING
SOYA-5	MAR 3	MAR 3	10.4	5.5	3.7	1.2	3.7	CONVENTIONAL / CASING
1350-1	MAR 2	MAR 2	7.6	4.0	2.4	1.3	3.7	CONVENTIONAL / CASING
1350-3	MAR 2	MAR 2	7.3	1.8	4.0	1.5	3.7	CONVENTIONAL / CASING
1350-4	MAR 3	MAR 3	6.7	1.8	3.7	1.2	3.7	CONVENTIONAL / CASING
1350-5	MAR 3	MAR 3	11.0	4.9	5.5	0.6	6.7	CONVENTIONAL / CASING
1500-1	MAR 3	MAR 3	11.0	4.3	5.8	0.9	6.7	CONVENTIONAL / CASING
1500-2	MAR 5	MAR 6	12.8	4.9	5.5	2.4	6.7	CONVENTIONAL / CASING
1500-3	MAR 3	MAR 3	9.8	5.5	3.6	0.7	6.7	CONVENTIONAL / CASING
1650-1	MAR 5	MAR 5	11.6	4.3	6.1	1.2	6.7	CONVENTIONAL / CASING
1650-2	MAR 4	MAR 5	11.6	1.8	6.7	3.1	3.7	CONVENTIONAL / CASING
1650-3	MAR 4	MAR 4	9.8	6.7	1.8	1.2	9.8	CONVENTIONAL / CASING
1650-4	MAR 3	MAR 4	15.2	6.7	7.3	1.2	9.8	CONVENTIONAL / CASING
2100-1	MAR 6	MAR 7	7.9	4.3	2.7	1.0	6.7	CONVENTIONAL / CASING
2100-2	MAR 6	MAR 6	6.7	1.8	4.9	0.0	3.7	CONVENTIONAL / CASING
2100-3	MAR 6	MAR 6	8.5	7.3	1.2	0.0	8.5	CONVENTIONAL / CASING
2100-4	MAR 8	MAR 9	19.5	12.2	6.7	0.6	15.8	CONVENTIONAL / CASING
2400-2	MAR 7	MAR 7	10.7	8.2	2.4	0.0	9.8	CONVENTIONAL / CASING
2400-4	MAR 7	MAR 7	17.7	11.0	3.7	3.0	12.8	CONVENTIONAL / CASING
2400-5	MAR 7	MAR 7	11.0	2.4	4.9	3.6	6.7	CONVENTIONAL / CASING
2400-6	MAR 8	MAR 8	14.0	1.8	4.3	7.9	6.7	CONVENTIONAL / CASING
2400-7	MAR 8	MAR 8	11.6	9.1	1.2	1.2	9.8	CONVENTIONAL / CASING
2700-1	MAR 9	MAR 9	17.1	4.6	11.2	1.3	9.8	CONVENTIONAL / CASING
2700-2	MAR 10	MAR 10	14.0	5.2	6.4	2.4	9.8	CONVENTIONAL / CASING
2700-3	MAR 10	MAR 11	11.6	6.7	3.4	1.5	9.8	CONVENTIONAL / CASING
2700-4	MAR 12	MAR 12	18.9	16.5	2.4	0.0	15.8	CONVENTIONAL / CASING
2700-5	MAR 12	MAR 13	19.5	9.8	9.7	0.1	12.8	CONVENTIONAL / CASING
3000-1	MAR 11	MAR 11	8.5	5.8	0.9	1.8	6.7	CONVENTIONAL / CASING
3000-2	MAR 11	MAR 11	13.4	7.9	4.6	0.9	9.8	CONVENTIONAL / CASING
3000-3	MAR 11	MAR 11	14.9	7.0	6.7	1.2	9.8	CONVENTIONAL / CASING
3300-1	MAR 12	MAR 12	14.0	8.5	4.3	1.2	9.8	CONVENTIONAL / CASING
3300-2	MAR 12	MAR 12	19.2	12.5	5.5	1.2	12.8	CONVENTIONAL / CASING
3300-3	MAR 11	MAR 11	18.9	11.6	4.2	3.1	12.8	CONVENTIONAL / CASING
		TOTAL =	672.4	346.9	233.5	93.7	399.0	

FILE:SWBHGRAD.WK1

 MOOSEHORN RANGE PLACER EXPLORATION PROJECT
 SWAMP CREEK DEFINITION DRILLING PROGRAM
 FEBRUARY - MARCH 1989

BHID	FROM	TO	LENGTH (feet)	LENGTH (meters)	VOLUME (liters)	Au (mg)	GRADE (fop1cm)	GRADE (fgpbcm)	GRADE (fopbcy)	WEIGHT (kg)	NOTES
800-1						Z=738.78M					
	X=6988955.52N	Y=501914.62E									
800-1	0	12	12	3.7							OB
	12	18	6	1.8	18.0	0				30.0	GRAV
	18	30	12	3.7	7.0	5.806	0.83	0.95	0.023	7.5	DIOR
800-2						Z=742.94M					
	X=6988967.14N	Y=501890.83E									
800-2	0	14	14	4.3							OB
	14	22	8	2.4	4.0	1				7.0	GRAV 16-18 NO SAMPLE
	22	25	3	0.9							GRAV NO SAMPLE
800-2A						Z=742.72M					
	X=6988967.66N	Y=501889.35E									
800-2A	0	14	14	4.3							OB
	14	16	2	0.6	2.5	0				4.5	GRAV
	16	18	2	0.6	5.0	tr				8.0	GRAV
	18	20	2	0.6	14.0	3				27.0	GRAV
	20	22	2	0.6	7.0	tr				9.0	GRAV
	22	24	2	0.6	12.0	1				17.0	GRAV
	24	26	2	0.6	21.0	tr				26.0	GRAV/HBFP PPYY
	26	28	2	0.6	21.0	1				23.0	HBFP PPYY
	28	30	2	0.6	20.0	0				28.0	HBFP PPYY
800-3						Z=743.46M					
	X=6988970.48N	Y=501873.16E									
800-3	0	12	12	3.7							OB
	12	14	2	0.6	21.0	0.327	0.02	0.02	0.000	31.0	GRAV
	14	16	2	0.6	16.5	0				27.0	GRAV
	16	18	2	0.6	16.5	0				27.0	GRAV
	18	20	2	0.6	16.0	0				25.0	GRAV
	20	22	2	0.6	15.0	0				25.0	GRAV
	22	24	2	0.6	17.0	0				26.0	GRAV
	24	26	2	0.6	20.0	0				30.0	GRDI
850-1						Z=736.68M					
	X=6988916.97N	Y=501897.97E									
850-1	0	4	4	1.2	11.0	18.354	1.67	1.92	0.047	19.0	GRAV
	4	6	2	0.6	10.0	14.118	1.41	1.62	0.040	16.0	GRAV
	6	8	2	0.6	9.0	tr				15.0	GRDI
	8	10	2	0.6	6.0	0.5				11.0	GRDI
850-2						Z=736.67M					
	X=6988917.49N	Y=501897.06E									
850-2	0	6	6	1.8							GRAV NO SAMPLE
	6	8	2	0.6	6.0	35.219	5.87	6.75	0.166	11.0	GRAV/GRDI
	8	10	2	0.6	11.0	92.657	8.42	9.69	0.238	20.0	GRDI
850-3						Z=741.70M					
	X=6988923.35N	Y=501871.87E									
850-3	0	16	16	4.9							OB
	16	18	2	0.6	1.0	0				1.5	GRAV
	18	20	2	0.6	17.5	0				24.0	DIOR
	20	24	4	1.2	8.0	0				11.0	DIOR
850-4						Z=743.72M					
	X=6988928.64N	Y=501853.37E									
850-4	0	8	8	2.4							OB
	8	10	2	0.6	5.0	0				12.0	OB

	2	4	2	0.6	1.0	0				3.0 GRAV
	4	6	2	0.6	3.0	0.5				4.0 GRAV
	6	8	2	0.6	1.0	tr				4.0 GRAV
	8	10	2	0.6	5.0	1				8.0 GRAV
	10	12	2	0.6	11.0	4.572	0.42	0.48	0.012	23.0 GRAV
	12	14	2	0.6	7.0	1				12.0 GRAV
1000-2	X=6988773.22N			Y=501855.92E			Z=730.56M			
1000-2	0	12	12	3.7	27.0	22.820	0.85	0.97	0.024	48.0 GRAV/GRDI 8-12
1000-3	X=6988776.95N			Y=501833.69E			Z=730.57M			
1000-3	0	2	2	0.6	4.0	0				8.0 GRAV HAND PANNED
	2	6	4	1.2	6.0	0				12.5 GRAV
	6	8	2	0.6	7.0	17.135	2.45	2.82	0.069	15.5 GRAV
	8	10	2	0.6	11.5	6.212	0.54	0.62	0.015	21.0 GRAV
	10	12	2	0.6	3.5	1				7.5 GRAV
1000-4	X=6988789.36N			Y=501798.88E			Z=736.02M			
1000-4	0	20	20	6.1						OB
	20	22	2	0.6	9.5	0.5				19.0 OB
	22	24	2	0.6	7.5	0				11.5 GRAV
	24	26	2	0.6	13.5	0				20.0 GRAV
	26	28	2	0.6	12.0	0				18.5 GRAV
	28	30	2	0.6	12.0	0				19.0 GRAV
	30	32	2	0.6	12.0	0				18.5 GRDI
	32	34	2	0.6	13.0	tr				20.0 GRDI
1000-5	X=6988795.58N			Y=501784.67E			Z=739.20M			
1000-5	0	24	24	7.3						OB
	24	26	2	0.6	7.5	0.285	0.04	0.04	0.001	13.0 OB
	26	28	2	0.6	20.0	0				39.0 OB
	28	30	2	0.6	9.0	0				13.0 GRAV
	30	32	2	0.6	16.0	4.726	0.30	0.34	0.008	27.5 GRAV
	32	34	2	0.6	9.5	2				16.0 GRAV
	34	36	2	0.6	12.5	1				18.0 GRDI
	36	38	2	0.6	14.0	0				20.5 GRDI
	38	40	2	0.6	16.5	0				22.0 GRDI
1000-6	X=6988811.28N			Y=501759.57E			Z=743.18M			
1000-6	0	16	16	4.9						OB
	16	18	2	0.6	17.0	0				33.5 OB
	18	20	2	0.6	18.0	0				32.0 GRAV
	20	22	2	0.6	10.5	0				15.5 GRDI
	22	24	2	0.6						GRDI NOT PROCESSED
1050-1	X=6988737.82N			Y=501843.28E			Z=729.26M			
1050-1	0	2	2	0.6	3.0	tr				7.0 GRAV
	2	4	2	0.6	2.0	0				4.5 GRAV
	4	6	2	0.6	2.5	0				5.5 GRAV
	6	8	2	0.6	1.0	0				3.0 GRAV
	8	10	2	0.6	5.0	tr				10.0 GRDI?
	10	12	2	0.6	4.0	12.735	3.18	3.66	0.090	8.0 GRDI?
	12	14	2	0.6	6.0	6.213	1.04	1.19	0.029	12.5 GRDI?
1050-2	X=6988732.90N			Y=501818.79E			Z=728.62M			
1050-2	0	2	2	0.6	2.0	0				6.5 OB/GRAV

	2	4	2	0.6	4.0	tr					11.0	GRAV
	4	6	2	0.6	10.0	32.302	3.23	3.71	0.091		21.0	GRAV
	6	8	2	0.6	10.0	4.890	0.49	0.56	0.014		22.0	GRAV
	8	10	2	0.6	6.0	2					13.0	GRAV/GRDI
1050-3				X=6988738.43N	Y=501793.26E	Z=728.84M						
1050-3	0	10	10	3.0	35.0	4.509	0.13	0.15	0.004		55.0	GRAV
1050-4				X=6988748.69N	Y=501779.75E	Z=729.55M						
1050-4	0	2	2	0.6								OB
	2	10	8	2.4	19.5	tr					31.0	GRAV SAMPLES COMBINED V CALC
	10	16	6	1.8								GRDI? 8-10 NO SAMPLE
1150-1				X=6988654.10N	Y=501752.32E	Z=726.27M						
1150-1	0	5	5	1.5								OB
	5	8	3	0.9	13.0	0.5					25.0	OB
	8	12	4	1.2	17.0	tr					43.0	OB/GRAV 10-12
	12	16	4	1.2	35.0	44.274	1.26	1.45	0.036		49.0	GRAV
	16	20	4	1.2	43.0	63.009	1.47	1.69	0.041		53.0	GRAV
1150-2				X=6988645.09N	Y=501783.21E	Z=727.49M						
1150-2	0	6	6	1.8								OB
	6	8	2	0.6	10.0	0					18.5	GRAV
	8	10	2	0.6	8.0	0					14.0	GRAV
	10	12	2	0.6	10.5	11.515	1.10	1.26	0.031		23.0	GRAV
	12	14	2	0.6	6.5	7.550	1.16	1.34	0.033		16.0	GRAV
	14	16	2	0.6	9.0	0					14.5	GRDI
	16	18	2	0.6	17.0	0					24.5	GRDI
1150-3				X=6988638.80N	Y=501804.66E	Z=729.42M						
1150-3	0	8	8	2.4								OB
	8	10	2	0.6	9.5	0					18.5	OB/GRAV
	10	12	2	0.6	14.5	0					29.5	GRAV
	12	14	2	0.6	10.0	0					12.5	GRDI
1150-4				X=6988662.98N	Y=501716.34E	Z=729.93M						
1150-4	0	24	24	7.3								OB
	24	26	2	0.6	10.0	3					19.0	GRAV
	26	28	2	0.6	10.0	3					18.0	GRAV
	28	32	4	1.2	12.0	0					22.0	GRDI
1250-1				X=6988547.73N	Y=501753.54E	Z=724.80M						
1250-1	0	12	12	3.7								OB
	12	14	2	0.6								GRAV/GRDI
1250-2				X=6988551.06N	Y=501732.11E	Z=722.93M						
1250-2	0	6	6	1.8								OB
	6	8	2	0.6	13.5	0					19.5	GRAV
	8	10	2	0.6	17.5	10.184	0.58	0.67	0.016		25.5	GRAV
	10	12	2	0.6	16.5	7.066	0.43	0.49	0.012		24.0	GRAV
	12	14	2	0.6	11.0	0					19.5	GRAV
	14	16	2	0.6	8.5	tr					11.5	GRAV
	16	18	2	0.6	6.0	8.901	1.48	1.71	0.042		8.0	GRAV
	18	20	2	0.6	8.0	0.5					20.0	GRAV/GRDI
	20	22	2	0.6	8.0	12.708	1.59	1.83	0.045		14.5	GRDI

	32	34	2	0.6	4.0	0					6.0 GRDI
SOYA-4	X=6988418.06N			Y=501841.13E			Z=722.15M				
SOYA-4	0	8	8	2.4							OB
	8	10	2	0.6	15.0	tr					26.0 GRAV
	10	12	2	0.6	14.0	1.628	0.12	0.13	0.003		25.0 GRAV/GRDI
	12	14	2	0.6	2.0	0					3.5 GRDI
SOYA-5	X=6988397.35N			Y=501852.58E			Z=724.02M				
SOYA-5	0	18	18	5.5							OB
	18	20	2	0.6	12.0	tr					25.0 GRAV
	20	22	2	0.6	16.0	9.700	0.61	0.70	0.017		32.0 GRAV
	22	24	2	0.6	15.0	0.5					26.0 GRAV
	24	26	2	0.6	9.0	0.5					13.0 GRAV
	26	28	2	0.6	7.0	0					10.0 GRAV
	28	34	6	1.8	35.0	35.966	1.03	1.18	0.029		54.0 GRAV/GRDI 30-34 V CALC
1350-1	X=6988449.27N			Y=501728.69E			Z=720.30M				
1350-1	0	13	13	4.0							OB
	13	15	2	0.6	12.0	tr					26.0 GRAV
	15	17	2	0.6	7.0	tr					11.5 GRAV
	17	21	4	1.2	22.0	33.643	1.53	1.76	0.043		56.5 GRAV
	21	25	4	1.2	27.0	13.351	0.49	0.57	0.014		44.0 DIOR?
1350-3	X=6988459.02N			Y=501703.55E			Z=718.30M				
1350-3	0	6	6	1.8							OB
	6	8	2	0.6	9.0	tr					18.0 GRAV
	8	10	2	0.6	23.0	tr					47.0 GRAV
	10	12	2	0.6	20.0	13.105	0.66	0.75	0.019		34.0 GRAV
	12	14	2	0.6	14.0	13.601	0.97	1.12	0.027		23.0 GRAV
	14	16	2	0.6	9.0	0					13.5 GRAV
	16	18	2	0.6	12.0	0					17.5 GRAV
	18	20	2	0.6	15.0	0.5					19.0 GRAV/GRDI
	20	22	2	0.6	20.0	1					24.0 GRDI
	22	24	2	0.6	14.0	0					22.5 GRDI
1350-4	X=6988463.68N			Y=501671.31E			Z=718.97M				
1350-4	0	6	6	1.8							OB
	6	8	2	0.6	14.0	0					25.0 GRAV
	8	10	2	0.6	11.0	3.302	0.30	0.35	0.008		20.0 GRAV
	10	12	2	0.6	7.0	0					15.0 GRAV
	12	16	4	1.2	9.5	0					25.0 GRAV
	16	18	2	0.6	13.0	20.503	1.58	1.81	0.045		26.0 GRAV
	18	20	2	0.6	10.0	11.133	1.11	1.28	0.031		24.0 GRDI
	20	22	2	0.6							GRDI NOT PROCESSED
1350-5	X=6988475.52N			Y=501639.55E			Z=720.02M				
1350-5	0	16	16	4.9							OB
	16	18	2	0.6	12.0	tr					23.0 GRAV?
	18	20	2	0.6	11.0	0					25.0 GRAV?
	20	22	2	0.6	8.0	0					13.5 GRAV?
	22	24	2	0.6	4.5	0					6.0 GRAV
	24	26	2	0.6	3.5	tr					6.0 GRAV
	26	28	2	0.6	21.0	0					47.0 GRAV V CALC
	28	30	2	0.6	4.0	0					6.0 GRAV
	30	32	2	0.6	15.0	2					33.0 GRAV

	32	36	4	1.2	15.0	0.5					29.5 GRAV/GRDI 34-36
1500-1	X=6988308.64N			Y=501675.59E			Z=712.80M				
1500-1	0	14	14	4.3							DB
	14	16	2	0.6	13.0	2					24.0 GRAV
	16	18	2	0.6	9.0	0.5					14.0 GRAV
	18	20	2	0.6	9.0	1					11.0 GRAV
	20	22	2	0.6	12.0	3.207	0.27	0.31	0.008		20.0 GRAV
	22	24	2	0.6	15.0	4.420	0.29	0.34	0.008		25.0 GRAV
	24	26	2	0.6	9.0	14.001	1.56	1.79	0.044		14.0 GRAV
	26	28	2	0.6	3.0	0					7.0 GRAV
	28	30	2	0.6	10.0	tr					23.0 GRAV
	30	32	2	0.6	18.0	3					28.0 GRAV
	32	34	2	0.6	7.0	1					10.0 GRAV/FP PPYY?
	34	36	2	0.6	11.0	38.126	3.47	3.99	0.098		16.0 FP PPYY?
1500-2	X=6988300.79N			Y=501707.09E			Z=715.17M				
1500-2	0	16	16	4.9							DB
	16	18	2	0.6	14.0	1					20.0 GRAV
	18	20	2	0.6	13.0	tr					19.0 GRAV
	20	22	2	0.6	10.0	15.211	1.52	1.75	0.043		14.0 GRAV
	22	24	2	0.6	15.0	14.258	0.95	1.09	0.027		22.0 GRAV
	24	26	2	0.6	14.0	28.990	2.07	2.38	0.059		19.0 GRAV
	26	28	2	0.6	13.0	50.773	3.91	4.49	0.110		15.0 GRAV
	28	30	2	0.6	12.0	27.549	2.30	2.64	0.065		17.0 GRAV
	30	34	4	1.2	29.0	9.455	0.33	0.37	0.009		40.0 GRAV
	34	42	8	2.4	29.0	9.973	0.34	0.40	0.010		41.0 GRDI
1500-3	X=6988316.57N			Y=501647.07E			Z=713.53M				
1500-3	0	11	11	3.4							DB
	11	14	3	0.9	6.0	0					9.0 DB
	14	18	4	1.2	5.0	0					10.0 DB
	18	20	2	0.6	18.0	0.5					32.0 GRAV
	20	22	2	0.6	8.0	0					14.0 GRAV
	22	24	2	0.6	20.0	tr					32.0 GRAV
	24	26	2	0.6	7.0	1.881	0.27	0.31	0.008		11.0 GRAV
	26	28	2	0.6	10.0	0					15.0 GRAV
	28	30	2	0.6	9.0	0					18.0 GRAV
	30	32	2	0.6	4.0	1					7.0 GRDI
1650-1	X=6988149N			Y=501684E			Z=711M				
1650-1	0	14	14	4.3							DB
	14	16	2	0.6	8.0	0					14.0 GRAV
	16	18	2	0.6	6.0	0					12.0 GRAV
	18	20	2	0.6	8.0	0					14.0 GRAV
	20	22	2	0.6	5.0	0					8.0 GRAV
	22	24	2	0.6	13.0	tr					26.0 GRAV
	24	26	2	0.6	7.0	tr					12.0 GRAV
	26	28	2	0.6	8.0	0.5					14.0 GRAV
	28	30	2	0.6	10.0	tr					20.0 GRAV
	30	32	2	0.6	8.0	tr					12.0 GRAV
	32	34	2	0.6	22.0	13.798	0.63	0.72	0.018		37.0 GRAV
	34	36	2	0.6	8.0	0.5					12.0 FP PPYY
	36	38	2	0.6	6.0	tr					8.0 FP PPYY
1650-2	X=6988158.90N			Y=501654.03E			Z=708.82M				

1650-2	0	4	4	1.2								OB	
	4	8	4	1.2	15.0	0						24.0 OB/GRAV	
	8	10	2	0.6	15.5	0						25.0 GRAV	
	10	12	2	0.6	7.0	0						11.0 GRAV	
	12	18	6	1.8	21.0	4.374	0.21	0.24	0.006			34.0 GRAV	
	18	20	2	0.6	13.0	5.803	0.45	0.51	0.013			21.0 GRAV	
	20	22	2	0.6	16.0	4.502	0.28	0.32	0.008			26.0 GRAV	
	22	24	2	0.6	12.5	2.590	0.21	0.24	0.006			20.0 GRAV	
	24	26	2	0.6	8.0	0						13.0 GRAV	
	26	28	2	0.6	11.0	0						18.0 GRAV	
	28	30	2	0.6	7.5	3.560	0.47	0.55	0.013			12.0 GRAV	
	30	38	8	2.4	42.0	0						47.0 DIOR	
1650-3	X=6988172.25N			Y=501591.59E			Z=711.58M						
1650-3	0	22	22	6.7								OB	
	22	26	4	1.2	6.0	0						15.0 GRAV	
	26	28	2	0.6	4.0	tr						10.0 GRAV	
	28	30	2	0.6	8.0	0						21.0 GRDI	
	30	32	2	0.6	6.0	tr						16.0 GRDI	
1650-4	X=6988168.94N			Y=501619.14E			Z=709.43M						
1650-4	0	22	22	6.7								OB	
	22	24	2	0.6	8.0	0						15.0 GRAV	
	24	26	2	0.6	11.0	0						23.0 GRAV	
	26	30	4	1.2	12.0	0						24.0 GRAV	
	30	32	2	0.6	19.0	3.706	0.20	0.22	0.006			36.0 GRAV	
	32	34	2	0.6	21.0	tr						44.0 GRAV	
	34	36	2	0.6	6.0	0						14.0 GRAV	
	36	38	2	0.6	18.0	8.411	0.47	0.54	0.013			37.0 GRAV	
	38	40	2	0.6	17.0	15.762	0.93	1.07	0.026			32.0 GRAV	
	40	42	2	0.6	9.0	0.5						14.0 GRAV	
	42	44	2	0.6	17.0	49.893	2.93	3.38	0.083			22.0 GRAV	
	44	46	2	0.6	10.0	29.720	2.97	3.42	0.084			12.0 GRAV	
	46	48	2	0.6	7.0	tr						8.0 GRDI	
	48	50	2	0.6	10.0	5.321	0.53	0.61	0.015			13.0 GRDI	
2100-1	X=6987712N			Y=501574E			Z=696.55M						
2100-1	0	14	14	4.3								OB	
	14	16	2	0.6	9.0	0						13.0 GRAV	
	16	18	2	0.6	10.0	2.731	0.27	0.31	0.008			15.0 GRAV	
	18	20	2	0.6	10.0	1						16.0 GRAV	
	20	22	2	0.6	15.0	17.064	1.14	1.31	0.032			25.0 GRAV	
	22	24	2	0.6	12.0	10.330	0.86	0.99	0.024			18.0 GRAV/GRDI	
	24	26	2	0.6	10.0	tr						14.0 GRDI	
2100-2	X=6987721N			Y=501545E			Z=693.5M						
2100-2	0	6	6	1.8								OB	
	6	8	2	0.6	9.0	0						15.0 GRAV	
	8	10	2	0.6	9.0	tr						14.0 GRAV	
	10	12	2	0.6	9.0	0.5						18.0 GRAV	
	12	14	2	0.6	4.0	5.556	1.39	1.60	0.039			8.0 GRAV	
	14	16	2	0.6	11.0	0.5						19.0 GRAV	
	16	18	2	0.6	9.0	tr						16.0 GRAV	
	18	20	2	0.6	12.0	4.770	0.40	0.46	0.011			18.0 GRAV	
	20	22	2	0.6	4.0	0.5						6.0 GRAV	

2100-3	X=6987731N			Y=501511E		Z=696.55M				
2100-3	0	16	16	4.9						OB
	16	24	8	2.4	5.0	0				9.0 OB
	24	26	2	0.6	16.0	0				25.0 GRAV
	26	28	2	0.6	8.0	0				13.0 GRAV
2100-4	X=6987739N			Y=501482E		Z=699.57M				
2100-4	0	26	26	7.9						OB
	26	34	8	2.4	12.0	0				21.0 OB
	34	36	2	0.6	13.0	0				22.0 OB
	36	38	2	0.6	6.0	0				8.0 OB
	38	42	4	1.2	9.0	0				22.0 OB/GRAV 40-42
	42	44	2	0.6	25.0	0				40.0 GRAV
	44	46	2	0.6	11.0	0				17.0 GRAV
	46	48	2	0.6	17.0	0				26.0 GRAV
	48	50	2	0.6	18.0	1.653	0.09	0.11	0.003	24.0 GRAV
	50	52	2	0.6	11.0	3.844	0.35	0.40	0.010	16.0 GRAV
	52	54	2	0.6	6.0	1.991	0.33	0.38	0.009	10.0 GRAV
	54	56	2	0.6	6.0	1.829	0.30	0.35	0.009	11.0 GRAV
	56	58	2	0.6	5.0	tr				8.0 GRAV
	58	60	2	0.6	8.0	0				13.0 GRAV
	60	62	2	0.6	10.0	3.562	0.36	0.41	0.010	16.0 GRAV
	62	64	2	0.6	8.0	7.622	0.95	1.10	0.027	13.0 GRAV
2400-2	X=6987352N			Y=501659E		Z=693M				
2400-2	0	27	27	8.2						
	27	29	2	0.6	6.0	0				13.0 OB
	29	31	2	0.6	11.0	0				24.0 GRAV
	31	33	2	0.6	16.0	0				32.0 GRAV
	33	35	2	0.6	3.0	0				10.0 GRAV
2400-4	X=6987294N			Y=501699E		Z=693.61M				
2400-4	0	36	36	11.0						OB
	36	38	2	0.6	5.0	0				10.0 GRAV
	38	40	2	0.6	9.0	0				18.0 GRAV
	40	42	2	0.6	16.0	0				29.0 GRAV
	42	44	2	0.6	15.5	0				25.0 GRAV
	44	46	2	0.6	15.5	0				27.0 GRAV
	46	48	2	0.6	18.0	0				32.0 GRAV
	48	50	2	0.6	11.0	0				14.0 GRDI
	50	52	2	0.6	12.0	0				17.0 GRDI
	52	54	2	0.6	7.0	0				11.0 GRDI
	54	58	4	1.2	7.0	0				11.0 GRDI
2400-5	X=6987411N			Y=501536E		Z=686.16M				
2400-5	0	8	8	2.4						OB
	8	10	2	0.6	6.0	0				12.0 GRAV
	10	12	2	0.6	15.0	0				27.0 GRAV
	12	14	2	0.6	7.0	0				13.0 GRAV
	14	16	2	0.6	10.0	6.081	0.61	0.70	0.017	15.0 GRAV
	16	18	2	0.6	7.0	1.875	0.27	0.31	0.008	11.0 GRAV
	18	20	2	0.6	7.0	0				10.0 GRAV
	20	22	2	0.6	7.0	0				9.0 GRAV
	22	24	2	0.6	7.0	0				12.0 GRAV
	24	26	2	0.6	10.0	tr				18.0 GRAV
	26	28	2	0.6	7.0	0				10.0 GRDI?

	28	30	2	0.6	7.0	0					9.0 GRDI?
	30	32	2	0.6	3.0	0					4.0 GRDI? NOT PROCESSED
	32	34	2	0.6	5.0	0					8.0 GRDI? NOT PROCESSED
	34	35	2	0.6	5.0	0					8.0 GRDI? NOT PROCESSED
2400-6	X=6987419N			Y=501507E		Z=685.08M					
2400-6	0	6	6	1.8							OB
	6	8	2	0.6	3.0	0					5.0 GRAV
	8	10	2	0.6	11.0	0					19.0 GRAV
	10	12	2	0.6	20.0	4.721	0.24	0.27	0.007		32.0 GRAV
	12	14	2	0.6	12.0	0					19.0 GRAV
	14	15	2	0.6	7.0	0					14.0 GRAV
	16	18	2	0.6	7.0	3.945	0.56	0.65	0.016		15.0 GRAV
	18	20	2	0.6	7.0	0					15.0 GRAV
	20	22	2	0.6	13.0	0					22.0 DIOR?
	22	24	2	0.6	9.0	0					15.0 DIOR?
	24	26	2	0.6	5.0	0					8.0 DIOR?
	26	28	2	0.6							DIOR? NOT PROCESSED
	28	30	2	0.6	6.0	0.5					8 DIOR?
	30	32	2	0.6	9.0	5.017	0.56	0.64	0.016		11 DIOR?
	32	45	14	4.3							DIOR? NOT PROCESSED
2400-7	X=6987429N			Y=501474E		Z=687.88M					
2400-7	0	30	30	9.1							OB
	30	32	2	0.6	22.0	0					45.0 GRAV
	32	34	2	0.6	6.0	0					10.0 GRAV V CALC
	34	36	2	0.6	7.5	0					12.0 DIOR? V CALC
	36	38	2	0.6	7.5	0					12.0 DIOR? V CALC
2700-1	X=6987150N			Y=501357E		Z=680.22M					
2700-1	0	15	15	4.6							OB
	15	18	3	0.9	4.0	0					12.0 GRAV
	18	20	2	0.6	8.0	0.5					15.0 GRAV
	20	22	2	0.6	14.0	4.088	0.29	0.34	0.008		29.0 GRAV
	22	24	2	0.6	9.0	0					16.0 GRAV
	24	26	2	0.6	12.0	tr					23.0 GRAV
	26	28	2	0.6	11.0	tr					18.0 GRAV
	28	30	2	0.6	10.0	1					13.0 GRAV
	30	32	2	0.6	13.0	4.250	0.33	0.38	0.009		26.0 GRAV
	32	34	2	0.6	11.0	0					16.0 GRAV
	34	36	2	0.6	9.0	0					13.0 GRAV
	36	38	2	0.6	9.0	0					13.0 GRAV
	38	40	2	0.6	10.0	0					14.0 GRAV
	40	42	2	0.6	10.0	0.5					14.0 GRAV
	42	44	2	0.6	9.0	0					13.0 GRAV
	44	46	2	0.6	8.0	tr					12.0 GRAV
	46	48	2	0.6	6.0	tr					9.0 GRAV
	48	50	2	0.6	5.0	1					8.0 GRAV
	50	52	2	0.6	10.0	2.693	0.27	0.31	0.008		14.0 GRAV
	52	54	2	0.6	15.0	2.714	0.18	0.21	0.005		20.0 DIOR
	54	55	2	0.6	10.0	0					14.0 DIOR
2700-2	X=6987140N			Y=501389E		Z=679M					
2700-2	0	17	17	5.2							OB
	17	20	3	0.9	12.0	0					24.0 GRAV
	20	22	2	0.6	20.0	0					38.0 GRAV

	22	24	2	0.6	10.0	0					14.0	GRAV
	24	26	2	0.6	12.0	0					17.0	GRAV
	26	28	2	0.6	4.0	0.5					6.0	GRAV
	28	30	2	0.6	14.0	tr					19.0	GRAV
	30	32	2	0.6	7.0	0					15.0	GRAV
	32	38	6	1.8	10.0	0					17.0	GRAV
	38	40	2	0.6	14.0	0					22.0	GRDI
	40	46	6	1.8	38.0	0					50.0	GRDI
2700-3	X=6987130N			Y=501425E		Z=680.37M						
2700-3	0	22	22	6.7								OB
	22	24	2	0.6	10.0	0					12.0	GRAV
	24	26	2	0.6	16.0	0.5					22.0	GRAV
	26	28	2	0.6	16.0	0.5					24.0	GRAV
	28	30	2	0.6	13.0	1.481	0.11	0.13	0.003		19.0	GRAV
	30	32	2	0.6	5.0	1.314	0.26	0.30	0.007		6.0	GRAV
	32	34	2	0.6	7.0	0.5					10.0	GRAV/GRDI
	34	36	2	0.6	12.0	0					17.0	GRDI
	36	38	2	0.6	10.0	0					14.0	GRDI
2700-4	X=6987166N			Y=501299E		Z=681.59M						
2700-4	0	44	44	13.4								OB
	44	48	4	1.2	12.0	0					26.0	OB MUD+GRAV
	48	54	6	1.8	14.0	0					29.0	OB MUD+GRAV
	54	56	2	0.6	11.0	0					24.0	GRAV
	56	58	2	0.6	12.0	0					21.0	GRAV
	58	60	2	0.6	6.0	tr					9.0	GRAV
	60	62	2	0.6	7.0	0					10.0	GRAV
2700-5	X=6987158N			Y=501327E		Z=680.83M						
2700-5	0	16	16	4.9								OB
	16	26	10	3.0	20.0	0					33.0	OB
	26	28	2	0.6	20.0	0					35.0	OB
	28	32	4	1.2	20.0	0					36.0	OB
	32	36	4	1.2	18.0	0					28.0	GRAV
	36	40	4	1.2	11.0	0					32.0	GRAV
	40	42	2	0.6	16.0	0					32.0	GRAV
	42	44	2	0.6	16.0	0					28.0	GRAV
	44	46	2	0.6	11.0	0					14.0	GRAV
	46	48	2	0.6	13.0	0					22.0	GRAV
	48	50	2	0.6	11.0	0					20.0	GRAV
	50	52	2	0.6	12.0	0					21.0	GRAV
	52	54	2	0.6	12.0	0					21.0	GRAV
	54	56	2	0.6	8.0	0					14.0	GRAV
	56	58	2	0.6	16.0	0					26.0	GRAV
	58	60	2	0.6	16.0	0					25.0	GRAV
	60	62	2	0.6	17.0	4.572	0.27	0.31	0.008		21.0	GRAV
	62	64	2	0.6	13.0	2.748	0.21	0.24	0.006		23.0	GRAV
3000-1	X=6986869N			Y=501253E		Z=675M						
3000-1	0	19	19	5.8								OB
	19	22	3	0.9	14.0	27.304	1.95	2.24	0.055		32.0	GRAV
	22	28	6	1.8	29.0	1.086	0.04	0.04	0.001		51.0	GRDI
3000-2	X=6986877N			Y=501226E		Z=674.39M						
3000-2	0	26	26	7.9								OB

	26	30	4	1.2	19.0	0				33.0 GRAV
	30	32	2	0.6	15.0	0				22.0 GRAV
	32	34	2	0.6	13.0	0.5				19.0 GRAV
	34	36	2	0.6	11.0	0.5				17.0 GRAV
	36	38	2	0.6	11.0	tr				16.0 GRAV
	38	40	2	0.6	9.0	tr				12.0 GRAV
	40	44	4	1.2	23.0	3.751	0.16	0.19	0.005	35.0 GRAV/GRDI 41-44
3000-3	X=6986885N			Y=501197E		Z=673.32M				
3000-3	0	21	21	6.4						DB
	21	23	2	0.6	5.0	0				15.0 DB
	23	25	2	0.6	20.0	2.240	0.11	0.13	0.003	39.0 GRAV
	25	27	2	0.6	9.0	0				14.0 GRAV
	27	29	2	0.6	14.0	1				22.0 GRAV
	29	31	2	0.6	14.0	0				24.0 GRAV
	31	33	2	0.6	10.0	0				17.0 GRAV
	33	35	2	0.6	8.0	1.077	0.13	0.15	0.004	14.0 GRAV
	35	37	2	0.6	7.0	0				10.0 GRAV
	37	39	2	0.6	9.0	5.652	0.63	0.72	0.018	13.0 GRAV
	39	41	2	0.6	7.0	0				10.0 GRAV
	41	43	2	0.6	13.0	0.5				18.0 GRAV
	43	45	2	0.6	13.0	0.5				18.0 GRAV
	45	47	2	0.6	12.0	tr				15.0 GRDI
	47	49	2	0.6	11.0	tr				13.0 GRDI
3300-1	X=6986572N			Y=501204E		Z=666.22M				
3300-1	0	28	28	8.5						DB
	28	30	2	0.6	9.0	0				18.0 GRAV
	30	32	2	0.6	17.0	0				34.0 GRAV
	32	36	4	1.2	11.0	0				20.0 GRAV
	36	38	2	0.6	18.0	1				37.0 GRAV
	38	40	2	0.6	16.0	tr				27.0 GRAV
	40	42	2	0.6	14.0	0.5				23.0 GRAV
	42	44	2	0.6	9.0	2				13.0 GRDI?
	44	46	2	0.6	7.0	0				10.0 GRDI?
3300-2	X=6986582N			Y=501167E		Z=666.98M				
3300-2	0	37	37	11.3						DB
	37	41	4	1.2	20.0	0				41.0 DB
	41	43	2	0.6	19.0	1.078	0.06	0.07	0.002	42.0 GRAV
	43	45	2	0.6	11.0	0				18.0 GRAV
	45	47	2	0.6	8.0	0				14.0 GRAV
	47	49	2	0.6	6.0	0				10.0 GRAV
	49	51	2	0.6	7.0	0				14.0 GRAV
	51	53	2	0.6	12.0	0				18.0 GRAV
	53	57	4	1.2	10.0	0				16.0 GRAV
	57	59	2	0.6	6.0	0.5				11.0 GRAV
	59	61	2	0.6	8.0	tr				14.0 GRDI?
	61	63	2	0.6	7.0	0				13.0 GRDI?
3300-3	X=6986591N			Y=501138E		Z=666.83M				
3300-3	0	38	38	11.6						DB
	38	40	2	0.6	6.0	1.725	0.29	0.33	0.008	12.0 GRAV
	40	42	2	0.6	11.0	0.5				23.0 GRAV
	42	44	2	0.6	8.0	0				14.0 GRAV
	44	46	2	0.6	9.0	0				14.0 GRAV

46	48	2	0.6	5.0	0				10.0 GRAV
48	52	4	1.2	22.0	1.622	0.07	0.08	0.002	35.0 GRAV
52	54	2	0.6	6.0	0				10.0 GRAV
54	56	2	0.6	7.0	0				14.0 GRAV
56	58	2	0.6	4.0	0				7.0 GRAV
58	62	4	1.2	9.0	0				14.0 GRAV

OB = BLACK MUD AND SILT

GRAV = GRAVEL

V CALC = CALCULATED VOLUME

GRDI = GRANDIORITE

HBFP PPYY = HORNBLENDE - FELDSPAR PORPHYRY

DIOR = DIORITE

FP PPYY = FELDSPAR PORPHYRY

APPENDIX III

MAGNETIC PROFILES

MAGNETIC ANOMALY MAPS

SWAMP CREEK MAGNETICS PROJECT
FOR: CANADA TUNGSTEN
MARCH 26, 1989

BY: ON-LINE EXPLORATION SVS. INC.
11976 WILDERNESS DRIVE
ANCHORAGE, ALASKA 99516

PRINTER WIDTH= 80 CHAR.S
ENTER 40, 80 OR 130

PRINTER WIDTH= 80 CHAR.S

TOTAL FIELD FULL SCALE= 100 GAMMAS
ENTER NEW SCALE (0 IF N/A)

TOTAL FIELD FULL SCALE= 200 GAMMAS

GRADIENT FULL SCALE= 10 GAMMAS
ENTER NEW SCALE (0 IF N/A)

GRADIENT FULL SCALE= 20 GAMMAS

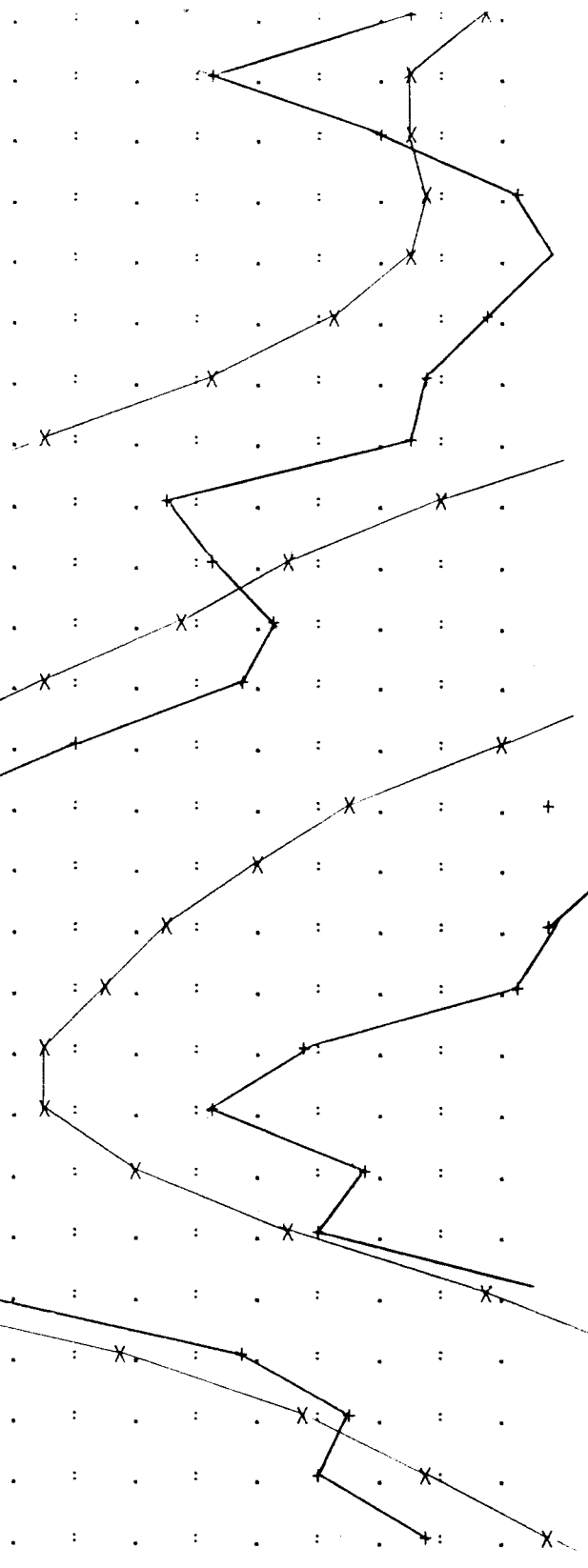
EDA OMNI-IV Tie-line MAG Ser #255007
TOTAL FIELD DATA (Base stn. corrected)
& GRADIENT
Date: 26 MAR 89
Operator: 5001
Reference field: 57450.0
Datum subtracted: 0.0
Records: 185
Bat: 15.6 Volt Lithium: 3.68 Volt
Last time update: 3/14 7:12:00
Start of print: 3/26 12:41:05

Base stn. Pos: 0+00 E Line: 0+00 N
Last time update: 3/14 7:12:00
Start of print: 3/26 12:40:54

Line: 13+00 S Date: 26 MAR 89 #1
POSITION FIELD ERR DRIFT TIME DS
2+85 W 57385.7 .06 -240 7 9:17:56 88 4 : : : : X

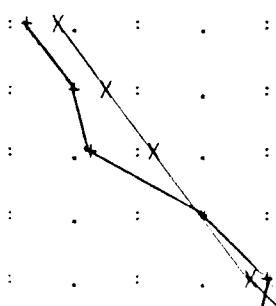
1200

0+55 E 57551.1 .05 -262.2 9:53:44 88	5.1
	-1.5
0+60 E 57551.1 .05 -262.6 9:53:58 88	4.0
	8.6
0+65 E 57554.1 .05 -263.0 9:54:13 88	
	10.8
0+70 E 57549.8 .05 -263.6 9:54:31 88	
	7.7
0+75 E 57523.6 .05 -263.9 9:54:47 88	
	5.4
0+80 E 57483.7 .05 -264.1 9:55:31 88	
	4.9
0+85 E 57429.5 .06 -263.3 9:56:00 88	
	-3.2
0+90 E 57359.0 .04 -263.6 9:56:20 88	
	-1.5
0+95 E 57312.1 .05 -264.6 9:56:53 88	
	0.7
1+00 E 57273.5 .04 -265.2 9:57:17 88	
	-0.4
1+05 E 57227.6 .05 -265.5 9:58:19 88	
	-6.2
1+10 E 57179.8 .06 -265.3 9:58:38 88	
	-10.3
1+15 E 57131.7 .07 -264.4 9:58:56 88	
	-9.4
1+20 E 57100.3 .06 -263.0 9:59:21 88	
	-10.3
1+25 E 57072.2 .06 -262.1 9:59:38 88	
	-11.6
1+30 E 57049.3 .06 -261.5 9:59:54 88	
	-18.6
1+35 E 57028.8 .06 -260.6 10:00:13 88	
	-21.5
1+40 E 57028.6 .06 -259.7 10:00:31 88	
	-16.4
1+45 E 57061.8 .06 -259.2 10:00:52 88	
	-18.1
1+50 E 57108.3 .06 -259.3 10:01:11 88	
	-9.3
1+55 E 57176.9 .06 -261.7 10:02:19 88	
	-0.4
1+60 E 57257.2 .05 -262.5 10:02:42 88	
	3.2
1+65 E 57316.4 .06 -263.0 10:03:00 88	
	2.2
1+70 E 57355.5 .05 -262.0 10:03:28 88	
	5.7
1+75 E 57394.0 .05 -262.3 10:03:58 88	



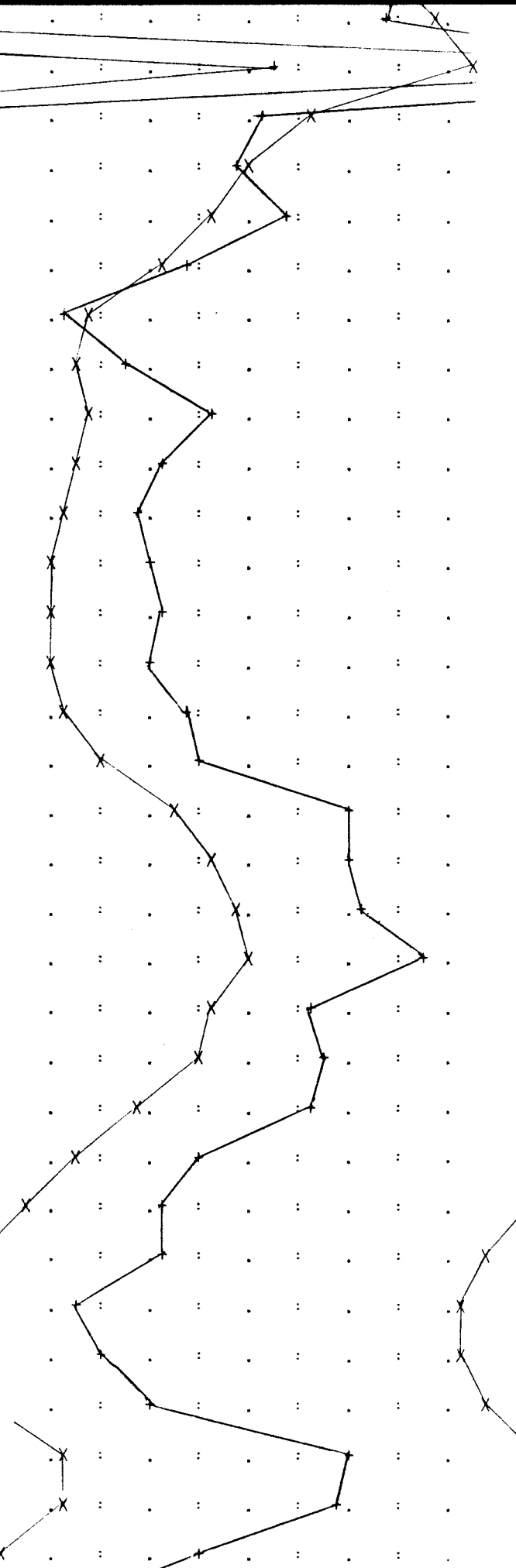
Line: 12+50 S Date: 26 MAR 89 #94

POSITION	FIELD	ERR	DRIFT	TIME	DS
2+00 W 57493.9 .05 -278.6 10:30:25 88		-1.4			
		0.2			
1+95 W 57510.3 .05 -278.1 10:31:51 88		0.6			
		4.1			
1+85 W 57540.2 .06 -277.4 10:32:28 88		6.1			
1+80 W 57556.5 .05 -276.9 10:33:00 88					



1250

1+75 W	57574.6	.05	-277.7	10:33:20	88
	5.6				
1+70 W	57588.1	.06	-278.1	10:33:37	88
	21.1				
1+65 W	57522.5	.06	-279.6	10:34:33	88
	0.3				
1+60 W	57502.1	.06	-280.5	10:35:08	88
	-0.5				
1+55 W	57487.0	.05	-281.3	10:35:45	88
	1.3				
1+50 W	57462.7	.06	-281.5	10:36:04	88
	-2.7				
1+45 W	57434.6	.05	-280.5	10:37:32	88
	-7.6				
1+40 W	57429.5	.05	-280.1	10:37:55	88
	-5.2				
1+35 W	57436.0	.05	-280.6	10:38:44	88
	-1.5				
1+30 W	57428.7	.05	-280.9	10:39:11	88
	-3.5				
1+25 W	57423.3	.05	-280.7	10:39:43	88
	-4.3				
1+20 W	57422.0	.05	-280.7	10:40:05	88
	-3.8				
1+15 W	57418.2	.06	-280.3	10:40:35	88
	-3.4				
1+10 W	57417.6	.05	-280.2	10:40:55	88
	-4.2				
1+05 W	57425.2	.05	-280.1	10:41:20	88
	-2.7				
1+00 W	57440.4	.05	-280.0	10:41:45	88
	-1.8				
0+95 W	57472.0	.05	-280.4	10:42:48	88
	4.0				
0+90 W	57482.7	.05	-280.8	10:43:14	88
	4.2				
0+85 W	57493.4	.06	-281.1	10:43:47	88
	4.6				
0+80 W	57498.5	.05	-281.1	10:44:08	88
	6.9				
0+75 W	57485.8	.05	-280.2	10:44:45	88
	2.6				
0+70 W	57479.2	.04	-279.5	10:45:10	88
	3.2				
0+65 W	57457.4	.05	-278.5	10:45:31	88
	2.3				
0+60 W	57429.0	.05	-279.1	10:45:51	88
	-2.0				
0+55 W	57409.2	.05	-279.9	10:46:12	88
	-3.5				
0+50 W	57396.9	.05	-280.9	10:46:33	88
	-3.3				
0+45 W	57385.8	.05	-286.5	10:47:26	88
	-6.8				
0+40 W	57383.5	.05	-287.4	10:47:47	88
	-6.2				
0+35 W	57396.2	.05	-287.9	10:48:04	88
	-4.2				
0+30 W	57424.7	.05	-287.9	10:48:21	88
	3.9				
0+25 W	57423.7	.06	-287.3	10:48:41	88
	3.5				
0+20 W	57401.1	.05	-286.3	10:48:58	88
	0				



1250

0+05 W	57409.1	.06	-281.0	10:49:44	88	.	:	.	:	.	:	.	:	.	:	.	:	.	:	.
	-1.6																			
0+00 E	57425.0	.05	-278.9	10:50:15	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	-1.7																			
0+05 E	57423.6	.05	-279.9	10:52:00	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	-6.0																			
0+10 E	57442.2	.05	-278.8	10:52:34	88	.	X	:	X	:	.	:	.	:	.	:	.	:	.	:
	-7.5																			
0+15 E	57485.6	.05	-278.0	10:52:58	88	.	.	:	.	:	X	:	.	:	.	:	.	:	.	:
	-0.5																			
0+20 E	57534.7	.04	-278.3	10:53:20	88	.	.	:	.	:	.	:	X	:	.	:	.	:	.	:
	4.9																			
0+25 E	57572.5	.05	-278.3	10:53:50	88	.	.	:	.	:	.	:	.	:	.	:	.	:	.	:
	7.5																			
0+30 E	57608.6	.05	-278.1	10:54:12	88	.	X	:	X	:	.	:	.	:	.	:	.	:	.	:
	11.8																			
0+35 E	57624.7	.04	-278.3	10:54:41	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	10.0																			
0+40 E	57616.7	.04	-278.6	10:55:04	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	4.6																			
0+45 E	57617.2	.05	-278.5	10:55:32	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	6.3																			
0+50 E	57601.6	.06	-278.8	10:56:02	88	.	X	:	.	:	.	:	.	:	.	:	.	:	.	:
	15.5																			

Line: 12+00 S Date: 26 MAR 89 #145

POSITION	FIELD	ERR	DRIFT	TIME	DS	.	:	.	:	.	:	.	:	.	:	.	:	.	:	.	
0+50 W	57484.8	.06	-276.0	11:07:51	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	2.6																				
0+45 W	57474.3	.05	-273.7	11:09:45	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	1.5																				
0+40 W	57456.4	.06	-273.2	11:10:08	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-1.9																				
0+35 W	57441.2	.06	-273.5	11:10:31	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-4.3																				
0+30 W	57443.2	.06	-273.3	11:11:11	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-1.0																				
0+25 W	57442.6	.05	-273.2	11:11:28	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-1.3																				
0+20 W	57442.4	.05	-273.1	11:11:45	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-0.2																				
0+15 W	57444.3	.05	-273.1	11:12:01	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-0.1																				
0+10 W	57441.5	.05	-273.1	11:12:17	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-0.2																				
0+05 W	57439.9	.05	-273.1	11:12:32	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-1.3																				
0+00 W	57445.7	.06	-271.4	11:18:32	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	1.1																				
0+05 W	57445.8	.05	-271.4	11:18:58	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	1.5																				
0+10 W	57441.9	.05	-271.1	11:19:29	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	1.6																				
0+05 W	57425.5	.05	-270.7	11:19:54	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-0.7																				
0+00 W	57406.6	.04	-270.5	11:20:10	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-4.6																				
0+25 W	57395.7	.05	-270.4	11:20:26	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-5.1																				X
0+70 W	57397.2	.05	-270.3	11:20:47	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-2.5																				X
0+05 W	57402.0	.05	-270.4	11:21:15	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:
	-1.9																				
0+00 W	57406.4	.05	-269.9	11:21:45	88	.	:	.	:	X	:	.	:	.	:	.	:	.	:	.	:

SWAMP CREEK MAGNETICS PROJECT
FOR: CANADA TUNGSTEN
MARCH 16, 1989

BY: ON-LINE EXPLORATION SVS. INC.
11976 WILDERNESS DRIVE
ANCHORAGE, ALASKA 99516

PRINTER WIDTH= 80 CHAR.S
ENTER 40, 80 OR 130

PRINTER WIDTH= 80 CHAR.S

TOTAL FIELD FULL SCALE= 100 GAMMAS
ENTER NEW SCALE (0 IF N/A)

TOTAL FIELD FULL SCALE= 200 GAMMAS

GRADIENT FULL SCALE= 10 GAMMAS
ENTER NEW SCALE (0 IF N/A)

GRADIENT FULL SCALE= 10 GAMMAS

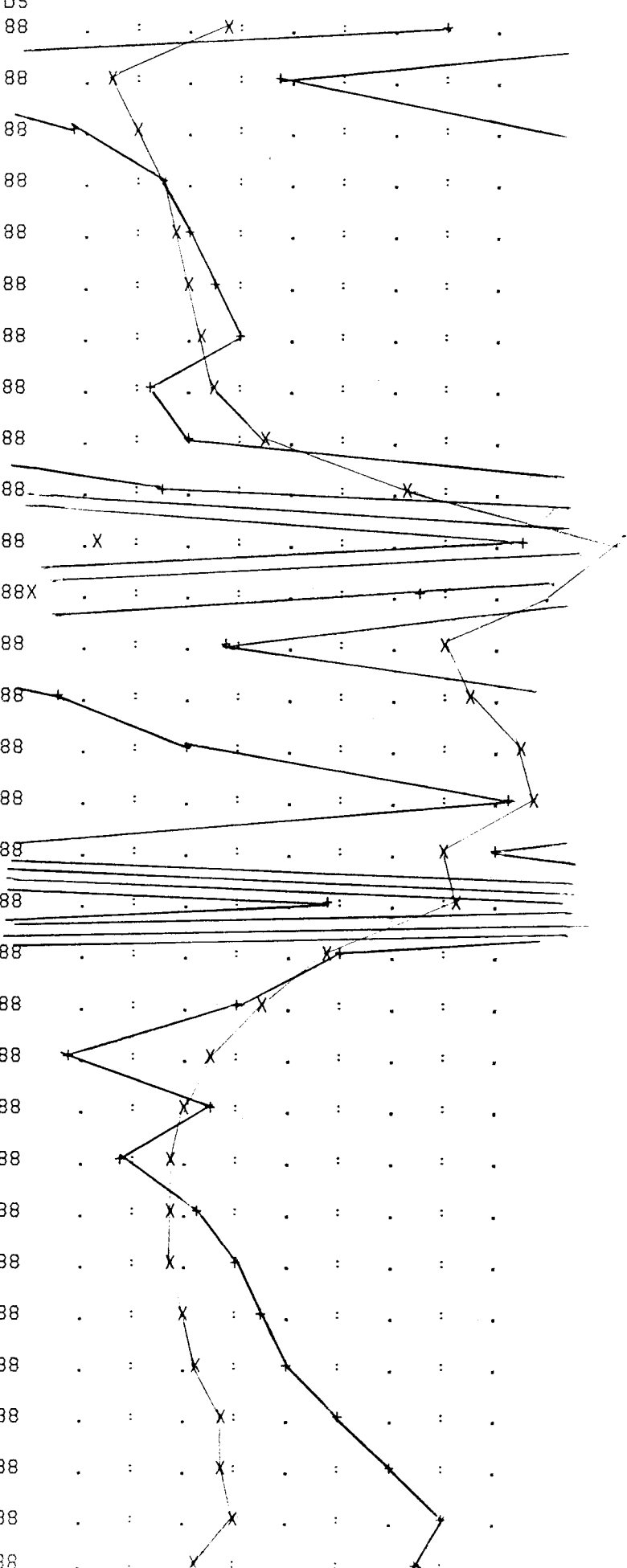
EDA OMNI-IV Tie-line MAG Ser #255007
TOTAL FIELD DATA (Base stn. corrected)
& GRADIENT
Date: 16 MAR 89
Operator: 5001
Reference field: 57450.0
Datum subtracted: 0.0
Records: 255
Bat: 15.6 Volt Lithium: 3.68 Volt
Last time update: 3/14 7:12:00
Start of print: 3/17 7:52:53

Base stn. Pos: 0+00 E Line: 0+00 N

Line: 16+50 S Date: 16 MAR 89 #1

POSITION FIELD ERR DRIFT TIME DS

0+90 W	57474.5	.06	-261.5	10:02:34	88
	12.9				
0+85 W	57427.7	.05	-248.8	10:05:10	88
	-10.2				
0+80 W	57438.0	.05	-249.8	10:05:31	88
	-4.2				
0+75 W	57448.6	.05	-249.9	10:05:49	88
	-2.6				
0+70 W	57453.0	.05	-250.0	10:06:11	88
	-1.9				
0+65 W	57459.5	.04	-250.6	10:06:34	88
	-1.6				
0+60 W	57464.9	.04	-252.8	10:06:54	88
	-1.1				
0+55 W	57472.3	.05	-253.4	10:07:11	88
	-2.7				
0+50 W	57491.0	.05	-253.1	10:07:30	88
	-2.0				
0+45 W	57543.8	.04	-252.6	10:07:52	88
	7.4				
0+40 W	57624.4	.04	-255.2	10:10:03	88
	34.4				
0+35 W	57598.0	.05	-252.2	10:11:14	88X
	12.4				
0+30 W	57558.8	.05	-246.7	10:11:42	88
	-1.2				
0+25 W	57569.8	.06	-245.7	10:12:01	88
	5.6				
0+20 W	57588.8	.04	-247.2	10:12:23	88
	7.9				
0+15 W	57596.4	.06	-250.9	10:12:41	88
	14.3				
0+10 W	57561.8	.05	-256.2	10:13:04	88
	4.0				
0+05 W	57566.8	.04	-250.4	10:13:36	88
	40.7				
0+00 E	57514.4	.05	-246.5	10:14:11	88
	1.1				
0+05 E	57491.0	.05	-250.2	10:15:35	88
	-0.9				
0+10 E	57467.7	.05	-256.2	10:15:57	88
	-4.3				
0+15 E	57460.9	.05	-257.5	10:16:16	88
	-1.4				
0+20 E	57454.0	.05	-258.0	10:16:33	88
	-3.2				
0+25 E	57454.4	.05	-260.9	10:16:55	88
	-1.8				
0+30 E	57456.5	.05	-262.2	10:17:26	88
	-1.0				
0+35 E	57462.2	.04	-261.1	10:17:52	88
	-0.6				
0+40 E	57465.6	.04	-259.2	10:18:21	88
	0.0				
0+45 E	57473.1	.04	-259.9	10:18:40	88
	1.0				
0+50 E	57476.8	.04	-262.5	10:19:05	88
	1.9				
0+55 E	57479.6	.04	-263.2	10:19:42	88
	3.0				
0+60 E	57463.2	.05	-269.4	10:20:08	88



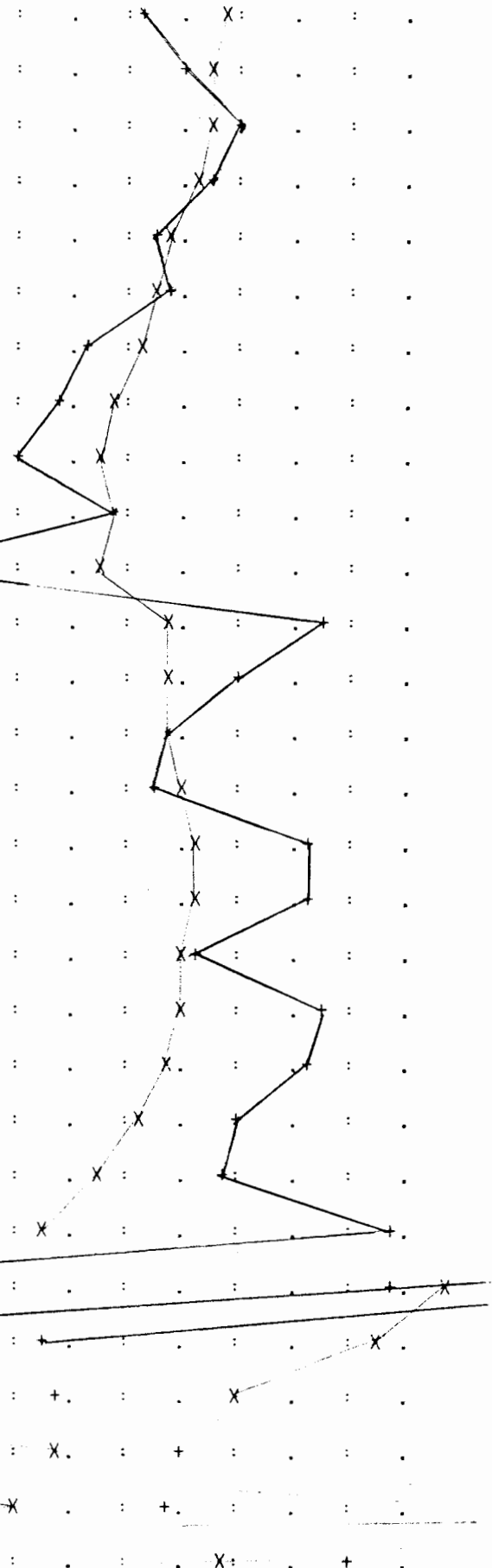
1650

2.5

0+65 E 57445.5 .04 -266.8 10:20:40 88
4.1

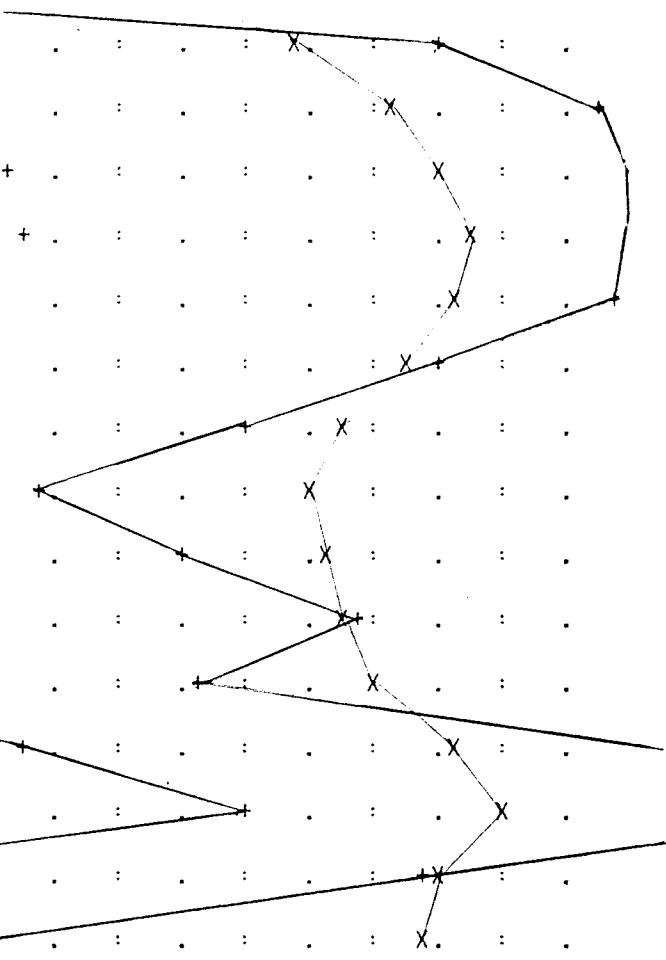
Line: 15+00 S Date: 16 MAR 89 #33

POSITION	FIELD	ERR	DRIFT	TIME	DS
1+20 W	57515.6	.04	-253.8	10:42:54 88	
	-0.7				
1+15 W	57510.6	.04	-253.2	10:43:58 88	
	-0.1				
1+10 W	57509.5	.05	-256.1	10:44:34 88	
	0.9				
1+05 W	57503.4	.04	-254.8	10:45:05 88	
	0.5				
1+00 W	57495.4	.04	-255.8	10:45:30 88	
	-0.4				
0+95 W	57490.1	.04	-248.3	10:48:11 88	
	-0.2				
0+90 W	57483.7	.04	-247.6	10:50:48 88	
	-1.8				
0+85 W	57473.3	.05	-241.9	10:54:18 88	
	-2.2				
0+80 W	57469.8	.04	-240.2	10:55:09 88	
	-3.1				
0+75 W	57472.5	.04	-239.2	10:55:27 88	
	-1.3				
0+70 W	57468.4	.04	-243.6	10:59:39 88	
	-4.9				
0+65 W	57493.2	.04	-249.4	11:02:24 88	
	2.6				
0+60 W	57497.4	.04	-248.6	11:02:49 88	
	1.0				
0+55 W	57495.9	.05	-250.0	11:03:16 88	
	-0.2				
0+50 W	57500.0	.04	-247.9	11:03:57 88	
	-0.5				
0+45 W	57507.2	.04	-238.7	11:09:10 88	
	2.2				
0+40 W	57505.2	.04	-238.9	11:09:28 88	
	2.3				
0+35 W	57498.4	.04	-239.4	11:09:45 88	
	0.2				
0+30 W	57497.9	.04	-240.0	11:10:04 88	
	2.6				
0+25 W	57493.7	.05	-240.1	11:10:23 88	
	2.3				
0+20 W	57484.0	.04	-239.9	11:10:40 88	
	0.9				
0+15 W	57469.0	.05	-238.8	11:11:08 88	
	0.7				
0+10 W	57452.2	.04	-233.0	11:12:56 88	
	3.7				
0+05 W	57396.9	.04	-238.0	11:14:16 88	
	-6.2				
0+00 E	57367.7	.04	-251.8	11:16:39 88	
	-12.5				
0+05 E	57318.7	.03	-252.5	11:19:03 88	
	-62.2				
0+10 E	57854.6	.05	-251.5	11:19:48 88	
	-220.0				
0+15 E	62838.4	33.	-249.9	11:21:39 27	
	5139.8				
0+20 E	57716.2	.15	-254.5	11:23:22 88	



1500

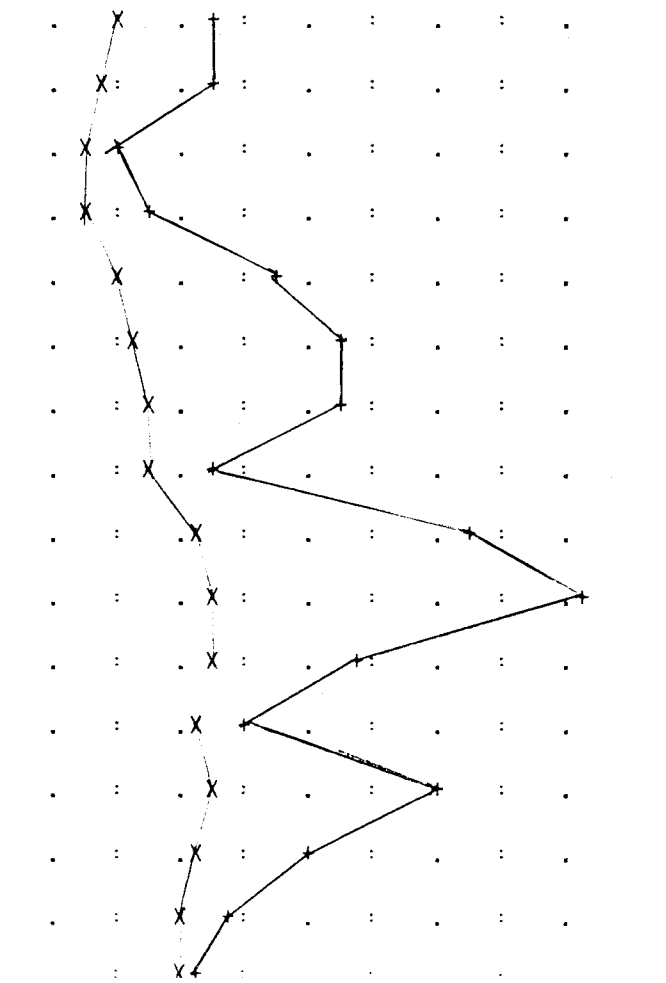
TIME	POSITION	FIELD	ERR	DRIFT	TIME	DS
0+35	E 57495.4	.04	-254.1	11:24:21	88	
	1.9					
0+40	E 57525.1	.04	-253.8	11:24:42	88	
	4.4					
0+45	E 57541.2	.04	-252.6	11:25:06	88	+
	5.3					
0+50	E 57549.5	.04	-239.0	11:27:57	88	+
	5.4					
0+55	E 57545.3	.04	-237.7	11:28:39	88	
	4.7					
0+60	E 57530.5	.04	-238.1	11:28:56	88	
	2.1					
0+65	E 57511.1	.04	-238.3	11:29:16	88	
	-1.0					
0+70	E 57498.7	.04	-238.1	11:29:36	88	
	-4.2					
0+75	E 57504.2	.03	-237.6	11:29:57	88	
	-2.0					
0+80	E 57512.0	.04	-238.0	11:30:12	88	
	0.8					
0+85	E 57518.4	.04	-238.9	11:30:30	88	
	-1.8					
0+90	E 57546.6	.03	-239.9	11:30:47	88	
	5.4					
0+95	E 57559.4	.04	-241.2	11:31:05	88	
	9.1					
1+00	E 57539.5	.05	-247.7	11:32:29	88	
	1.8					
1+05	E 57537.3	.04	-249.1	11:33:04	88	
	-5.0					



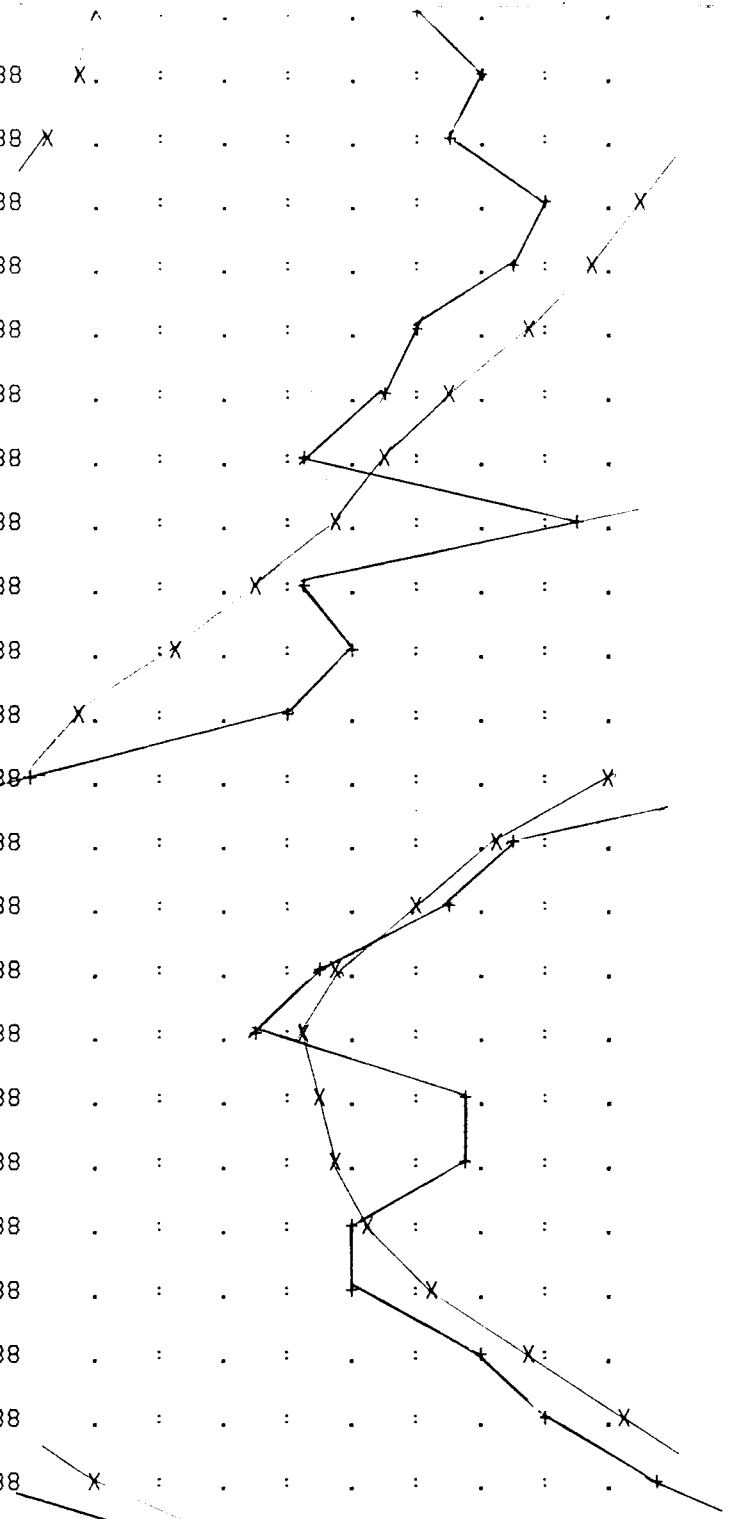
Line: 13+50 S Date: 16 MAR 89 #79

POSITION FIELD ERR DRIFT TIME DS

1+70	W 57442.1	.03	-206.2	13:01:13	88	
	-1.5					
1+65	W 57435.6	.04	-205.8	13:02:31	88	
	-1.5					
1+60	W 57427.8	.04	-205.6	13:04:24	88	
	-3.0					
1+55	W 57429.6	.03	-204.4	13:05:35	88	
	-2.5					
1+50	W 57439.1	.04	-203.5	13:06:00	88	
	-0.6					
1+45	W 57446.5	.04	-203.1	13:06:19	88	
	0.6					
1+40	W 57448.1	.04	-202.3	13:06:44	88	
	0.4					
1+35	W 57450.1	.03	-201.9	13:07:05	88	
	-1.4					
1+30	W 57462.5	.04	-202.5	13:07:26	88	
	2.5					
1+25	W 57472.1	.04	-202.7	13:07:47	88	
	4.2					
1+20	W 57467.6	.04	-204.3	13:08:18	88	
	0.8					
1+15	W 57465.9	.04	-205.0	13:08:57	88	
	-1.0					
1+10	W 57470.5	.04	-203.9	13:09:47	88	
	1.9					
1+05	W 57466.2	.04	-203.1	13:10:37	88	
	0.0					
1+00	W 57460.8	.03	-198.7	13:13:28	88	
	-1.2					
0+55	W 57450.5	.04	-199.6	13:14:39	88	

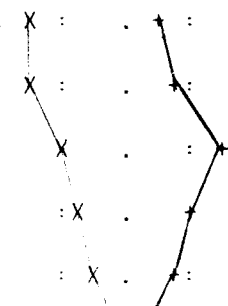


0715 E	57422.0	.03	-200.5	13:36:08	88	X	:	:	:	:	:	:	:	:	:	:	:	:	:	:
	1.0																			
0+80 E	57413.9	.04	-200.0	13:36:40	88	X	:	:	:	:	:	:	:	:	:	:	:	:	:	:
	2.0																			
0+85 E	57403.3	.04	-200.0	13:37:03	88	X	:	:	:	:	:	:	:	:	:	:	:	:	:	:
	1.4																			
1350 0+90 E	57392.1	.04	-200.0	13:37:18	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	3.1																			
0+95 E	57375.0	.03	-199.5	13:37:38	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	2.4																			
1+00 E	57353.6	.03	-196.0	13:38:52	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	1.0																			
1+05 E	57331.9	.03	-186.9	13:41:03	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	0.4																			
1+10 E	57311.5	.04	-184.8	13:41:20	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-0.8																			
1+15 E	57296.7	.04	-183.3	13:41:47	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	3.6																			
1+20 E	57269.4	.04	-182.8	13:42:09	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-0.8																			
1+25 E	57245.8	.03	-182.6	13:42:27	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	0.0																			
1+30 E	57212.8	.04	-183.0	13:42:48	88	X	:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-1.0																			
1+35 E	57179.4	.04	-184.2	13:43:08	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-4.9																			
1+40 E	57146.4	.04	-186.3	13:43:29	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-7.4																			
1+45 E	57118.3	.03	-188.9	13:43:59	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-8.4																			
1+50 E	57093.9	.04	-184.6	13:44:56	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-10.5																			
1+55 E	57083.4	.03	-183.7	13:46:11	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-11.5																			
1+60 E	57089.7	.04	-180.4	13:46:42	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-8.3																			
1+65 E	57096.1	.04	-179.0	13:47:06	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-8.2																			
1+70 E	57102.6	.03	-179.9	13:47:48	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-10.0																			
1+75 E	57124.1	.04	-183.6	13:48:28	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-9.9																			
1+80 E	57153.9	.04	-189.9	13:50:55	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-8.0																			
1+85 E	57186.0	.05	-189.8	13:51:16	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-7.0																			
1+90 E	57222.2	.03	-190.0	13:51:40	88	X	:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-5.3																			
1+95 E	57266.1	.04	-189.9	13:52:05	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	-2.4																			
2+00 E	57313.1	.04	-189.4	13:52:39	88		:	:	:	:	:	:	:	:	:	:	:	:	:	:
	1.5																			



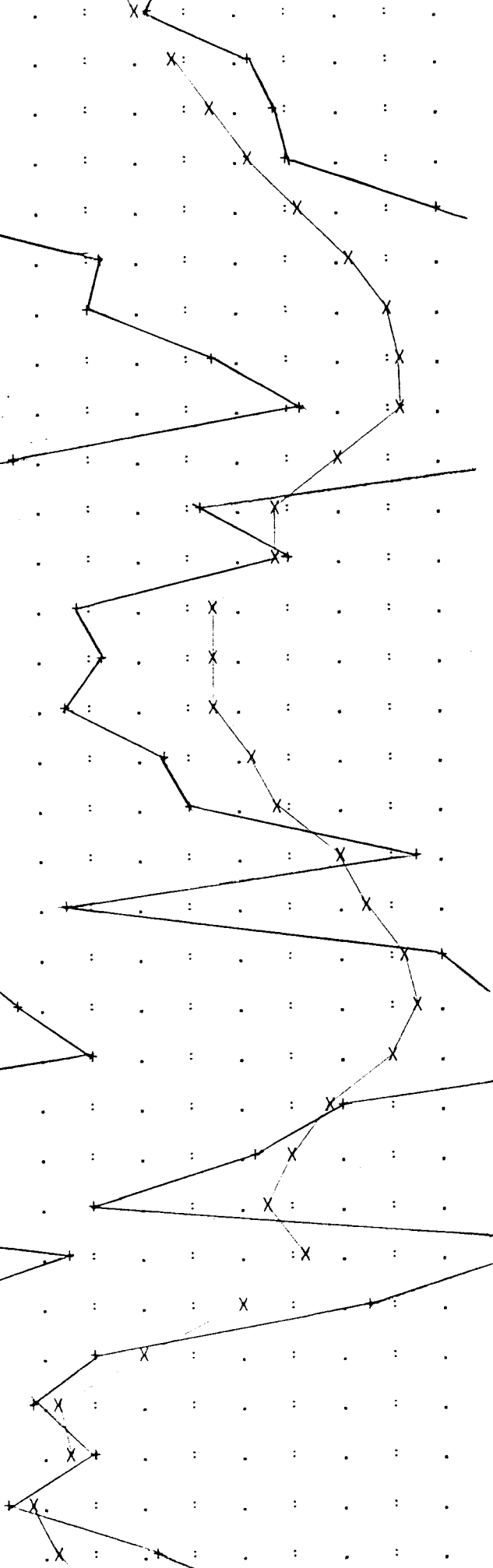
Line: 14+25 S Date: 16 MAR 89 #154

POSITION	FIELD	ERR	DRIFT	TIME	DS
1+70 W	57429.5	.04	-187.7	14:46:17	88
	-1.4				
1+65 W	57432.3	.04	-188.5	14:47:21	88
	-1.3				
1+60 W	57438.5	.04	-188.6	14:47:40	88
	-0.6				
1+55 W	57444.1	.04	-186.8	14:48:02	88
	-1.0				
1+50 W	57447.8	.04	-186.5	14:48:19	88
	-1.2				



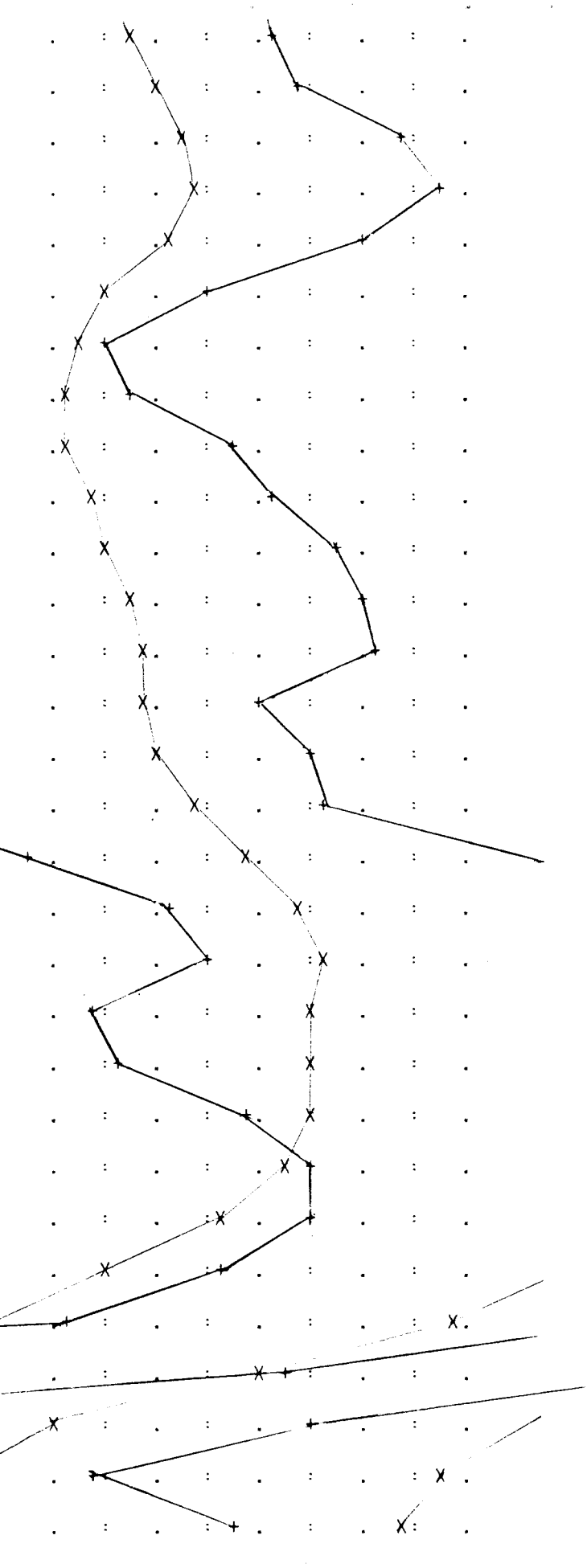
1425

1+45 W	57457.6	.04	-186.2	14:49:38	88
	-1.8				
1+40 W	57474.2	.03	-186.8	14:49:57	88
	0.2				
1+35 W	57488.6	.04	-187.9	14:50:18	88
	0.8				
1+30 W	57502.8	.04	-188.8	14:50:39	88
	1.1				
1+25 W	57524.6	.04	-189.4	14:50:58	88
	4.0				
1+20 W	57545.2	.04	-190.1	14:51:13	88
	7.3				
1+15 W	57558.2	.04	-190.9	14:51:28	88
	7.1				
1+10 W	57567.0	.03	-191.7	14:51:45	88
	9.6				
1+05 W	57566.1	.03	-192.5	14:52:02	88
	11.3				
1+00 W	57541.1	.03	-192.5	14:52:22	88
	5.6				
0+95 W	57516.7	.03	-193.6	14:53:35	88
	-0.8				
0+90 W	57512.9	.03	-194.2	14:53:55	88
	1.1				
0+85 W	57491.8	.04	-193.6	14:54:17	88
	-3.2				
0+80 W	57489.3	.04	-192.4	14:54:41	88
	-2.7				
0+75 W	57492.1	.04	-191.6	14:55:01	88
	-3.6				
0+70 W	57503.1	.03	-191.8	14:55:33	88
	-1.6				
0+65 W	57514.8	.03	-188.2	14:57:25	88
	-0.9				
0+60 W	57541.6	.03	-187.6	14:58:14	88
	3.5				
0+55 W	57549.1	.03	-186.6	14:58:33	88
	-3.4				
0+50 W	57567.1	.04	-187.6	14:58:54	88
	3.9				
0+45 W	57567.8	.04	-188.1	14:59:12	88
	5.6				
0+40 W	57558.9	.03	-188.4	14:59:30	88
	7.0				
0+35 W	57536.6	.03	-188.1	14:59:48	88
	2.0				
0+30 W	57519.6	.04	-188.0	15:00:08	88
	0.2				
0+25 W	57510.0	.04	-188.3	15:00:28	88
	-3.1				
0+20 W	57523.2	.04	-188.0	15:00:46	88
	6.6				
0+15 W	57498.9	.03	-192.8	15:08:21	88
	2.6				
0+10 W	57459.5	.04	-193.9	15:09:07	88
	-2.9				
0+05 W	57426.5	.04	-195.1	15:09:31	88
	-4.3				
0+00 E	57428.0	.04	-194.4	15:13:07	88
	-3.1				
0+05 E	57416.3	.04	-194.7	15:14:57	88
	-4.7				
0+10 E	57426.4	.04	-194.8	15:15:21	88



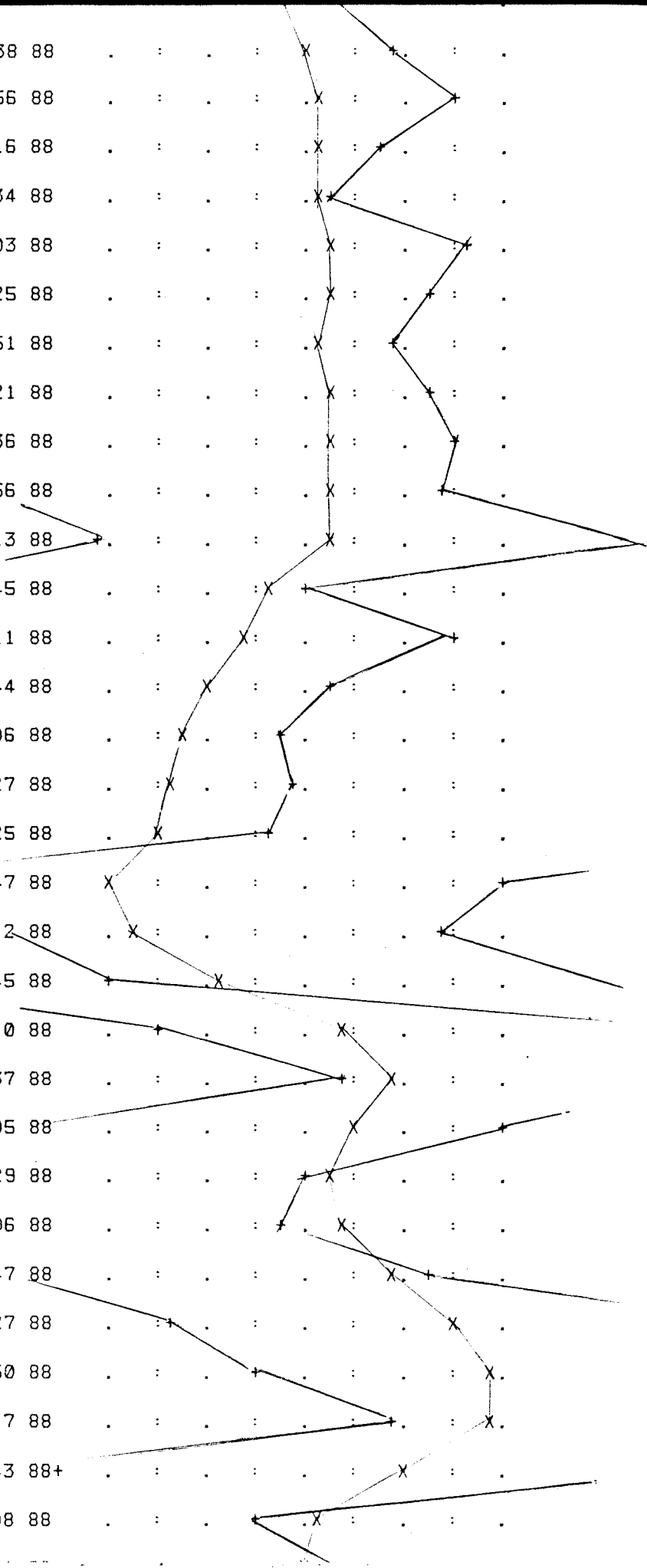
1425

Time	Lat	Long	Alt	DRIFT	TIME	DS
0+25 E	57451.0	.03	-190.3	15:16:54	88	
0+30 E	57459.5	.03	-190.4	15:17:13	88	
0+35 E	57471.0	.03	-190.9	15:17:30	88	
0+40 E	57473.3	.04	-190.3	15:17:53	88	
0+45 E	57462.6	.04	-189.0	15:18:25	88	
0+50 E	57442.4	.03	-189.1	15:18:54	88	
0+55 E	57427.7	.04	-195.6	15:21:01	88	
0+60 E	57423.3	.04	-196.5	15:21:20	88	
0+65 E	57426.9	.03	-197.4	15:21:36	88	
0+70 E	57432.6	.03	-198.6	15:21:55	88	
0+75 E	57441.6	.04	-198.5	15:22:12	88	
0+80 E	57449.1	.04	-197.7	15:22:29	88	
0+85 E	57453.3	.04	-195.2	15:22:54	88	
0+90 E	57453.4	.04	-194.4	15:23:13	88	
0+95 E	57461.1	.03	-194.6	15:23:47	88	
1+00 E	57475.6	.04	-194.8	15:25:21	88	
1+05 E	57497.2	.04	-197.7	15:27:51	88	
1+10 E	57515.8	.04	-197.5	15:28:11	88	
1+15 E	57522.7	.04	-197.9	15:28:32	88	
1+20 E	57520.2	.04	-197.5	15:28:51	88	
1+25 E	57520.4	.04	-197.2	15:29:19	88	
1+30 E	57520.8	.04	-197.1	15:29:45	88	
1+35 E	57510.0	.03	-196.6	15:30:24	88	
1+40 E	57484.2	.04	-196.0	15:30:56	88	
1+45 E	57438.9	.03	-196.0	15:31:38	88	
1+50 E	57376.1	.03	-196.4	15:32:58	88	
1+55 E	57297.7	.04	-198.8	15:35:30	88	
1+60 E	57222.1	.04	-199.5	15:35:52	88	
1+65 E	57172.4	.04	-198.7	15:36:19	88	
1+70 E	57156.3	.05	-196.5	15:36:59	88	



1575

0.5	0+80 W	57499.2	.03	-184.6	16:04:38	88
1.8						
0+75 W	57505.6	.04	-185.3	16:04:56	88	
3.0						
0+70 W	57505.5	.03	-185.2	16:05:16	88	
1.4						
0+65 W	57506.3	.04	-184.6	16:05:34	88	
0.5						
0+60 W	57511.6	.03	-183.3	16:06:03	88	
3.2						
0+55 W	57508.2	.03	-183.3	16:06:25	88	
2.4						
0+50 W	57504.3	.03	-183.4	16:06:51	88	
1.8						
0+45 W	57509.0	.04	-182.1	16:08:21	88	
2.5						
0+40 W	57511.9	.03	-182.1	16:08:36	88	
2.9						
0+35 W	57510.2	.03	-181.6	16:08:56	88	
2.8						
0+30 W	57507.6	.03	-180.9	16:09:13	88	
5.8						
0+25 W	57486.9	.03	-179.5	16:09:45	88	
0.1						
0+20 W	57475.6	.03	-178.8	16:10:11	88	
2.9						
0+15 W	57458.8	.04	-178.1	16:10:44	88	
0.4						
0+10 W	57449.7	.04	-177.5	16:11:06	88	
-0.4						
0+05 W	57445.9	.03	-176.4	16:11:27	88	
-0.2						
0+00 E	57438.9	.04	-174.7	16:12:25	88	
-0.7						
0+05 E	57419.3	.03	-167.1	16:15:47	88	
-6.1						
0+10 E	57429.9	.04	-166.0	16:16:12	88	
-7.2						
0+15 E	57465.3	.03	-165.0	16:16:45	88	
-4.0						
0+20 E	57515.3	.03	-164.2	16:17:10	88	
7.0						
0+25 E	57535.7	.04	-163.2	16:17:37	88	
10.8						
0+30 E	57520.1	.04	-162.6	16:18:05	88	
4.0						
0+35 E	57509.9	.03	-161.5	16:18:29	88	
-0.1						
0+40 E	57515.2	.03	-159.2	16:19:06	88	
-0.5						
0+45 E	57533.6	.03	-157.2	16:19:47	88	
2.6						
0+50 E	57560.1	.03	-153.9	16:20:27	88	
7.2						
0+55 E	57573.5	.04	-150.5	16:21:50	88	
9.0						
0+60 E	57573.4	.03	-150.6	16:22:17	88	
11.8						
0+65 E	57539.9	.04	-151.1	16:22:43	88+	
5.0						
0+70 E	57506.2	.04	-151.6	16:23:08	88	
-1.0						



SWAMP CREEK MAGNETICS PROJECT
FOR: CANADA TUNGSTEN
MARCH 17, 1989

BY: ON-LINE EXPLORATION SVS. INC.
11976 WILDERNESS DRIVE
ANCHORAGE, ALASKA 99516

PRINTER WIDTH= 80 CHAR.S
ENTER 40, 80 OR 130

PRINTER WIDTH= 80 CHAR.S

TOTAL FIELD FULL SCALE= 100 GAMMAS
ENTER NEW SCALE (0 IF N/A)

TOTAL FIELD FULL SCALE= 100 GAMMAS

GRADIENT FULL SCALE= 10 GAMMAS
ENTER NEW SCALE (0 IF N/A)

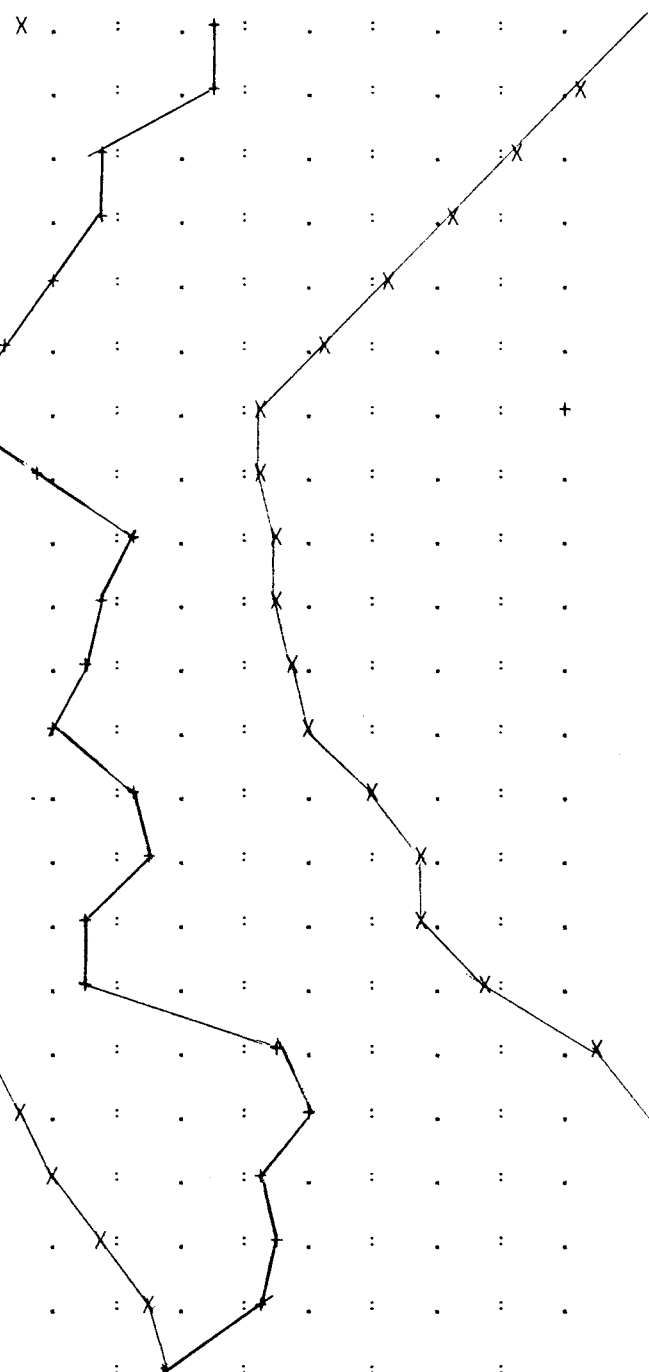
GRADIENT FULL SCALE= 10 GAMMAS

EDA OMNI-IV Tie-line MAG Ser #255007
TOTAL FIELD DATA (Base stn. corrected)
& GRADIENT
Date: 17 MAR 89
Operator: 5001
Reference field: 57450.0
Datum subtracted: 0.0
Records: 123
Bat: 16.0 Volt Lithium: 3.68 Volt
Last time update: 3/14 7:12:00
Start of print: 3/17 16:47:54

Base stn. Pos: 0+00 E Line: 0+00 N
Last time update: 3/14 7:12:00
Start of print: 3/17 16:47:42

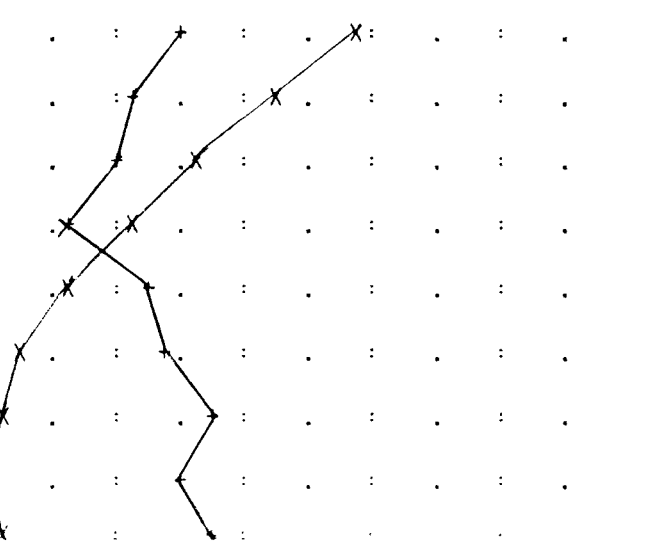
1425

POSITION	FIELD	ERR	DRIFT	TIME	DS
2+80 W	57404.9	.05	-203.5	14:02:31	88
	-1.4				
2+75 W	57392.6	.04	-203.1	14:03:28	88
	-1.5				
2+70 W	57382.8	.05	-201.9	14:04:48	88
	-3.2				
2+65 W	57372.8	.05	-201.9	14:05:35	88
	-3.2				
2+60 W	57362.1	.04	-201.7	14:06:00	88
	-3.9				
2+55 W	57353.4	.04	-200.9	14:06:25	88
	-4.8				
2+50 W	57341.7	.04	-200.7	14:07:19	88
	-6.0				
2+45 W	57342.4	.05	-200.4	14:07:39	88
	-4.2				
2+40 W	57344.4	.04	-199.6	14:07:56	88
	-2.8				
2+35 W	57344.2	.05	-199.7	14:08:20	88
	-3.3				
2+30 W	57346.5	.03	-199.6	14:08:42	88
	-3.4				
2+25 W	57349.5	.04	-199.4	14:09:08	88
	-4.1				
2+20 W	57358.9	.04	-200.5	14:09:26	88
	-2.7				
2+15 W	57366.3	.04	-200.2	14:09:47	88
	-2.5				
2+10 W	57368.4	.04	-199.5	14:10:02	88
	-3.6				
2+05 W	57378.1	.04	-199.5	14:10:22	88
	-3.4				
2+00 W	57393.8	.05	-200.0	14:10:54	88
	-0.6				
1+95 W	57403.8	.04	-199.4	14:11:30	88
	0.0				
1+90 W	57411.1	.05	-199.1	14:11:50	88
	-0.7				
1+85 W	57418.2	.03	-198.8	14:12:05	88
	-0.5				
1+80 W	57424.0	.04	-197.7	14:12:35	88
	-0.8				
1+75 W	57427.5	.04	-197.7	14:13:28	88
	-2.3				



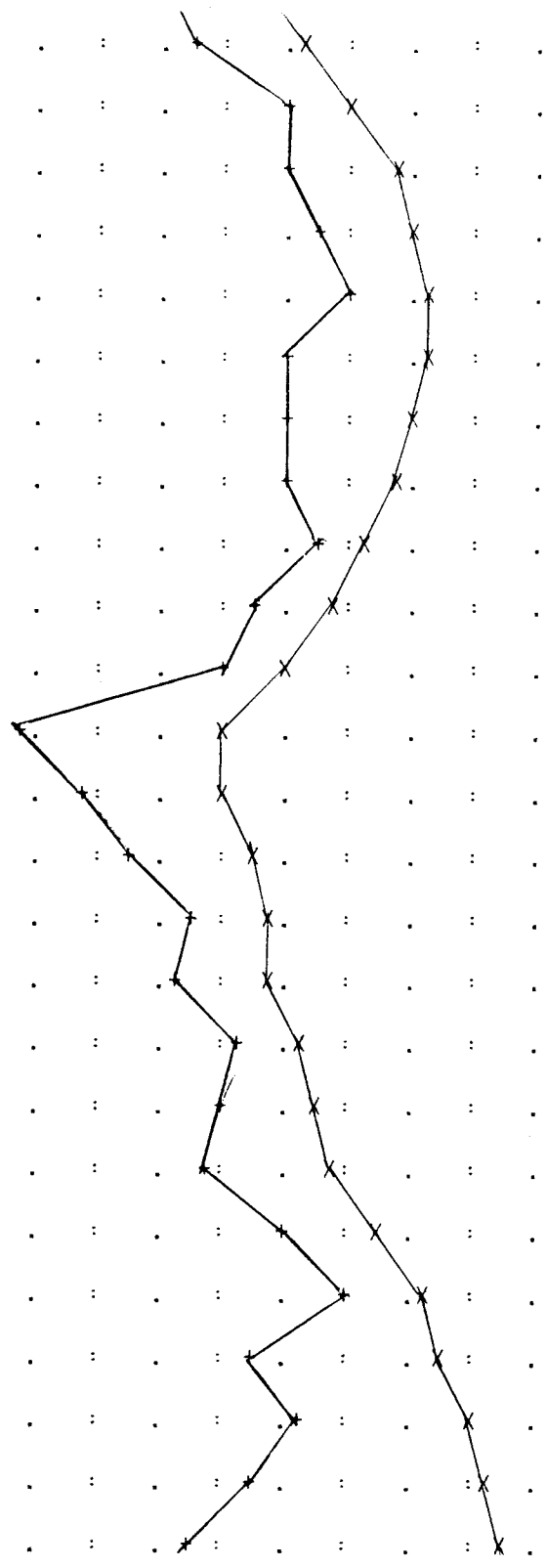
Line: 15+00 S Date: 17 MAR 89 #23

POSITION	FIELD	ERR	DRIFT	TIME	DS
2+70 W	57457.3	.05	-195.1	14:36:31	88
	-1.9				
2+65 W	57445.0	.05	-195.8	14:37:26	88
	-2.8				
2+60 W	57432.8	.04	-196.3	14:37:49	88
	-2.9				
2+55 W	57422.0	.03	-196.7	14:38:09	88
	-3.7				
2+50 W	57411.8	.04	-197.3	14:38:39	88
	-2.6				
2+45 W	57406.1	.05	-198.7	14:39:22	88
	-2.2				
2+40 W	57403.6	.05	-199.4	14:39:45	88
	-1.4				
2+35 W	57400.5	.04	-199.9	14:40:00	88
	-1.9				
2+30 W	57400.0	.04	-200.4	14:40:17	88



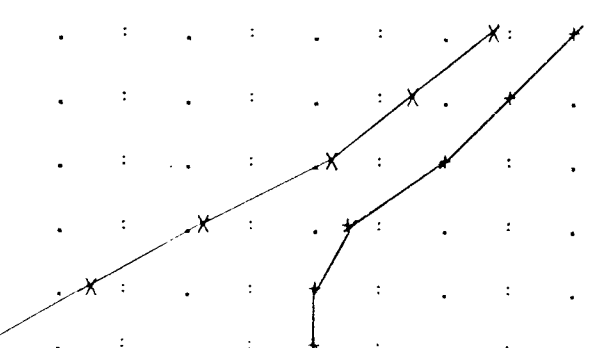
1575

2+10 W 57452.8 .04 -214.4 15:12:14 88
-1.4
2+05 W 57460.3 .03 -214.4 15:12:35 88
0.0
2+00 W 57467.8 .04 -214.8 15:12:55 88
0.0
1+95 W 57471.2 .04 -214.4 15:13:59 88
0.6
1+90 W 57472.2 .05 -214.4 15:14:14 88
0.9
1+85 W 57472.0 .04 -214.6 15:14:28 88
0.0
1+80 W 57470.1 .04 -214.6 15:14:44 88
0.0
1+75 W 57467.1 .04 -214.4 15:14:59 88
0.0
1+70 W 57463.6 .04 -213.9 15:15:15 88
0.5
1+65 W 57457.9 .05 -213.4 15:15:36 88
-0.5
1+60 W 57450.8 .04 -213.4 15:15:56 88
-0.9
1+55 W 57440.6 .04 -213.4 15:16:15 88
-4.2
1+50 W 57439.6 .05 -213.5 15:16:38 88
-3.2
1+45 W 57443.9 .04 -214.4 15:17:43 88
-2.6
1+40 W 57446.7 .04 -214.2 15:18:02 88
-1.6
1+35 W 57447.3 .04 -214.4 15:18:19 88
-1.8
1+30 W 57452.6 .04 -214.6 15:18:47 88
-0.8
1+25 W 57455.8 .04 -214.5 15:19:10 88
-0.9
1+20 W 57458.2 .04 -214.5 15:19:27 88
-1.3
1+15 W 57465.8 .04 -214.2 15:19:48 88
0.0
1+10 W 57472.6 .04 -214.0 15:20:06 88
1.1
1+05 W 57475.3 .04 -214.0 15:20:25 88
-0.5
1+00 W 57480.5 .04 -213.5 15:21:15 88
0.3
0+95 W 57483.4 .04 -213.1 15:21:46 88
-0.5
0+90 W 57485.2 .04 -213.1 15:22:15 88
-1.6



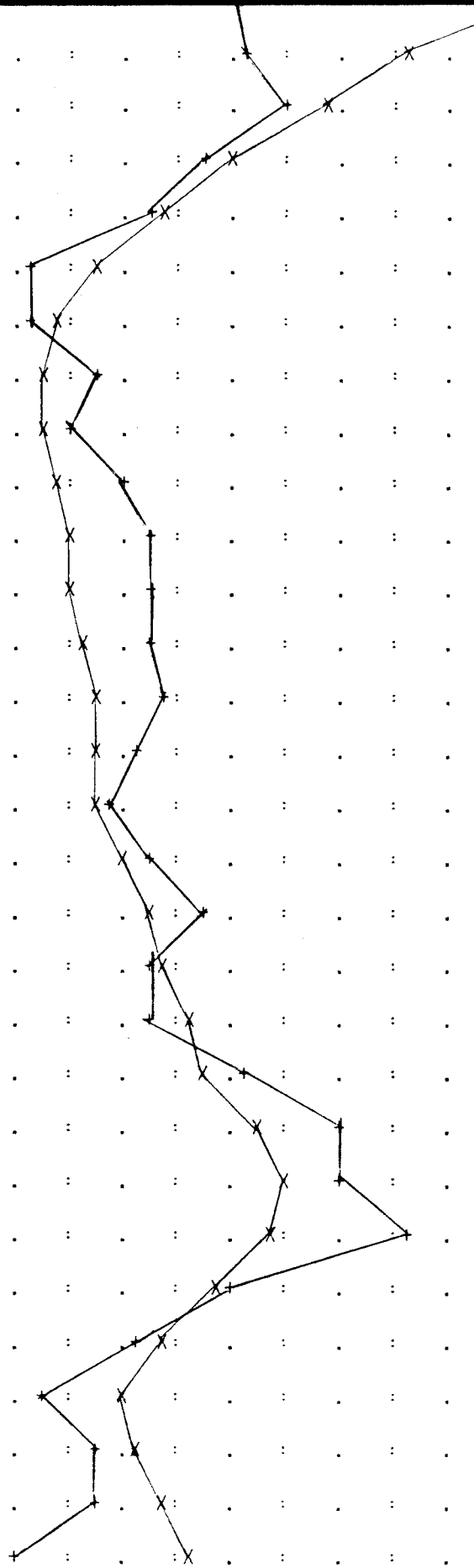
Line: 16+50 S Date: 17 MAR 89 #89

POSITION	FIELD	ERR	DRIFT	TIME	DS
2+65 W 57577.1 .04 -212.7 15:38:48 88					
4.0					
2+60 W 57564.2 .05 -212.4 15:39:36 88					
2.9					
2+55 W 57551.5 .05 -212.4 15:39:57 88					
1.9					
2+50 W 57532.7 .05 -212.5 15:40:16 88					
0.4					
2+45 W 57514.5 .04 -212.9 15:41:21 88					
-0.1					
2+40 W 57499.6 .04 -213.6 15:41:53 88X					



1650

		0.0							
2+35	W	57481.8	.04	-213.9	15:42:15	88			
		0.3							
2+30	W	57466.5	.05	-214.2	15:42:33	88			
		1.1							
2+25	W	57449.8	.04	-214.4	15:42:51	88			
		-0.5							
2+20	W	57436.4	.04	-214.6	15:43:11	88			
		-1.6							
2+15	W	57424.1	.04	-214.7	15:43:30	88			
		-3.8							
2+10	W	57416.7	.05	-214.2	15:44:04	88			
		-3.7							
2+05	W	57414.7	.04	-213.3	15:44:28	88			
		-2.5							
2+00	W	57415.5	.04	-212.9	15:44:50	88			
		-2.9							
1+95	W	57416.6	.04	-212.2	15:45:47	88			
		-2.1							
1+90	W	57418.8	.05	-212.6	15:46:07	88			
		-1.6							
1+85	W	57420.2	.04	-212.6	15:46:25	88			
		-1.6							
1+80	W	57423.3	.04	-213.0	15:46:43	88			
		-1.4							
1+75	W	57425.7	.05	-213.5	15:47:05	88			
		-1.3							
1+70	W	57425.6	.04	-213.9	15:47:29	88			
		-1.8							
1+65	W	57426.1	.04	-214.4	15:47:48	88			
		-2.3							
1+60	W	57430.4	.04	-214.8	15:48:05	88			
		-1.4							
1+55	W	57434.4	.04	-214.8	15:48:22	88			
		-0.6							
1+50	W	57436.6	.03	-215.0	15:48:51	88			
		-1.5							
1+45	W	57441.8	.04	-214.8	15:50:30	88			
		-1.4							
1+40	W	57446.2	.04	-215.2	15:50:49	88			
		0.2							
1+35	W	57455.2	.05	-216.3	15:51:16	88			
		1.9							
1+30	W	57459.0	.04	-217.2	15:51:36	88			
		2.0							
1+25	W	57458.2	.04	-218.2	15:52:01	88			
		3.3							
1+20	W	57447.0	.04	-218.4	15:52:18	88			
		-0.1							
1+15	W	57436.8	.05	-219.7	15:52:52	88			
		-1.8							
1+10	W	57430.8	.04	-220.1	15:53:17	88			
		-3.5							
1+05	W	57433.1	.04	-220.2	15:53:36	88			
		-2.4							
1+00	W	57438.1	.04	-219.3	15:55:25	88			
		-2.6							
0+95	W	57442.9	.04	-216.4	15:56:50	88			
		-4.0							



SWAMP CREEK MAGNETICS PROJECT
FOR: CANADA TUNGSTEN
MARCH 19, 1989

BY: ON-LINE EXPLORATION SVS. INC.
11976 WILDERNESS DRIVE
ANCHORAGE, ALASKA 99516

PRINTER WIDTH= 80 CHAR.S
ENTER 40, 80 OR 130

PRINTER WIDTH= 80 CHAR.S

TOTAL FIELD FULL SCALE= 100 GAMMAS
ENTER NEW SCALE (0 IF N/A)

TOTAL FIELD FULL SCALE= 100 GAMMAS

GRADIENT FULL SCALE= 10 GAMMAS
ENTER NEW SCALE (0 IF N/A)

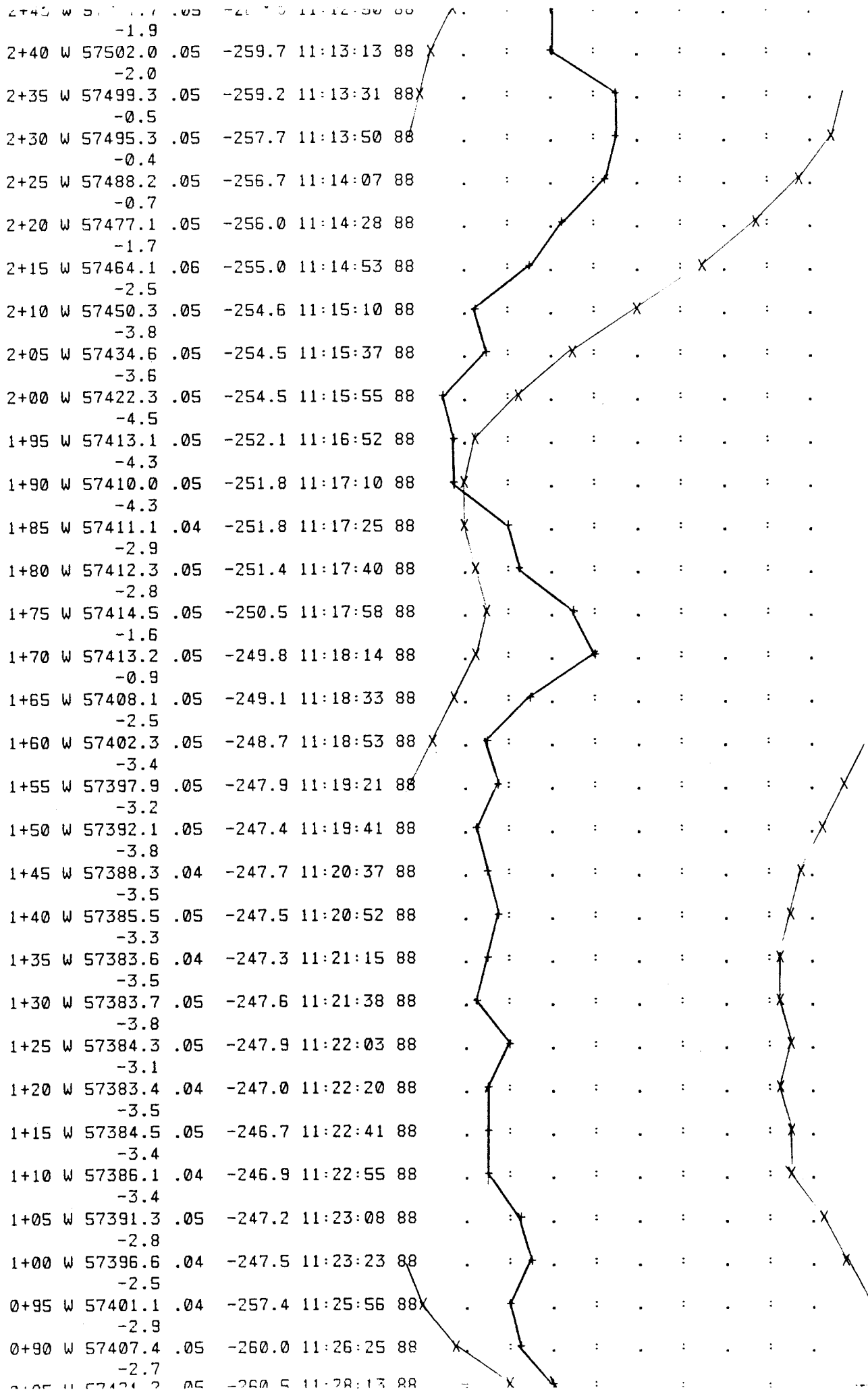
GRADIENT FULL SCALE= 10 GAMMAS

EDA OMNI-IV Tie-line MAG Ser #255007
TOTAL FIELD DATA (Base stn. corrected)
& GRADIENT
Date: 19 MAR 89
Operator: 5001
Reference field: 57450.0
Datum subtracted: 0.0
Records: 191
Bat: 15.7 Volt Lithium: 3.70 Volt
Last time update: 3/14 7:12:00
Start of print: 3/19 17:34:53

Base stn. Pos: 0+00 E Line: 0+00 N
Last time update: 3/14 7:12:00
Start of print: 3/19 17:34:48

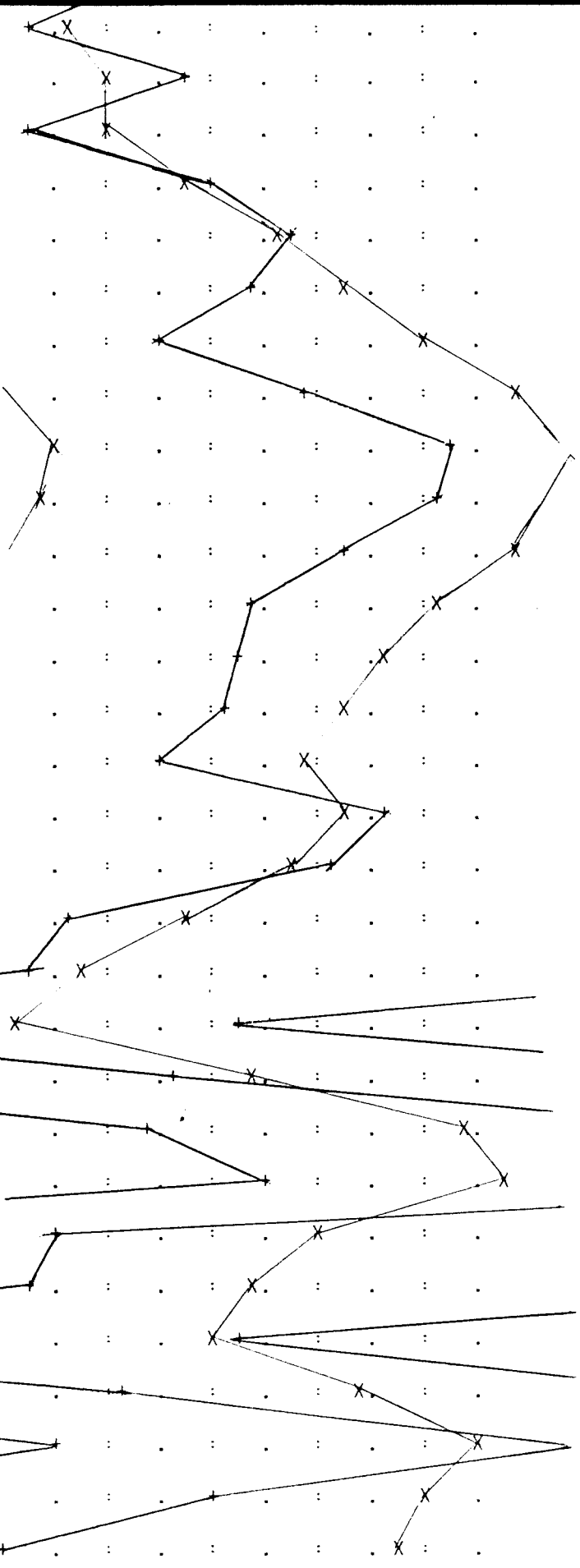
Line: 17+25 S Date: 19 MAR 89 #1
POSITION FIELD ERR DRIFT TIME DS

1725



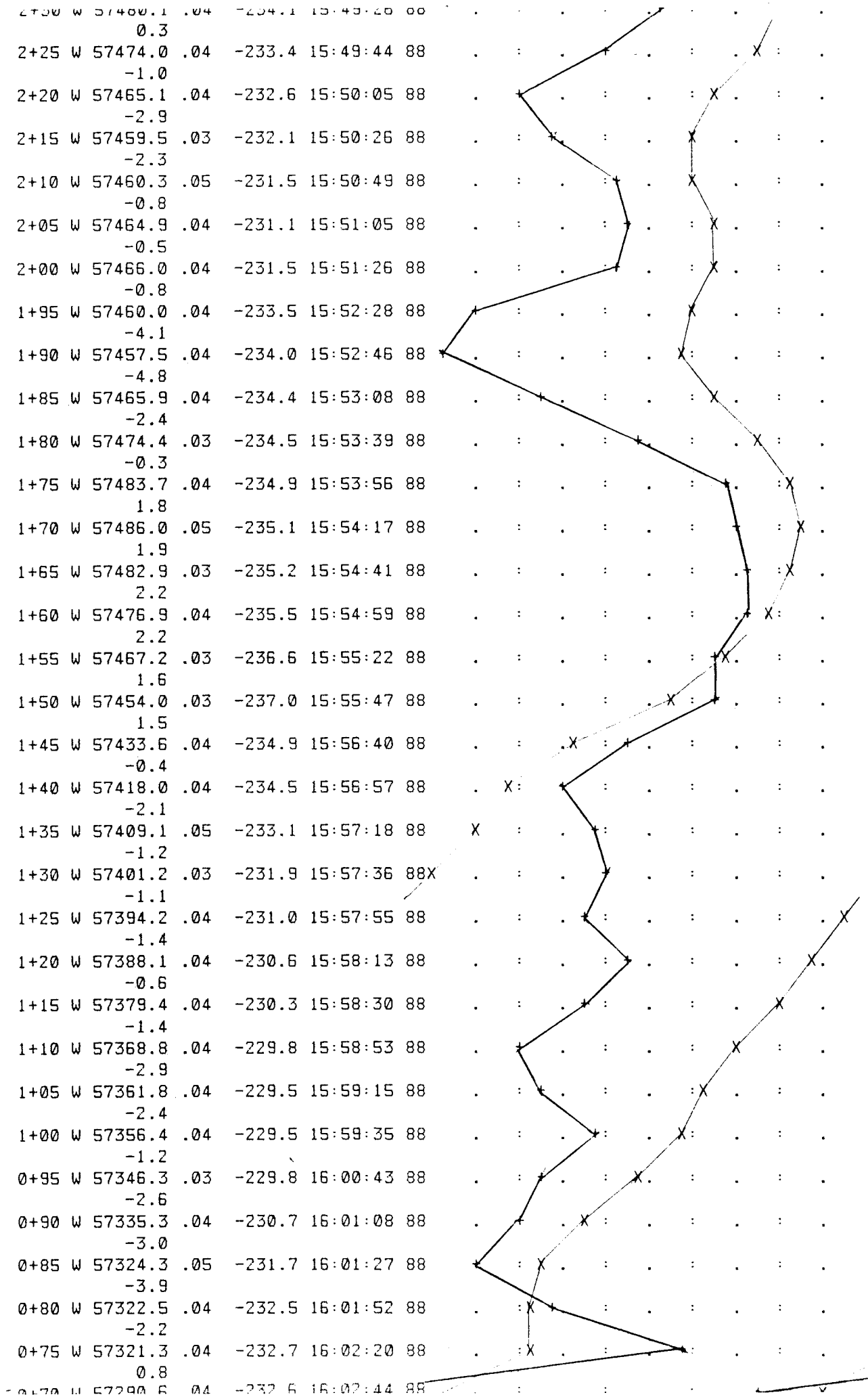
1800

0+85 W 57411.6	.04	-234.7	14:01:20	88
-4.4				
0+80 W 57419.2	.04	-233.4	14:02:09	88
-1.5				
0+75 W 57421.0	.04	-232.6	14:02:28	88
-4.4				
0+70 W 57435.6	.04	-232.4	14:02:46	88
-1.1				
0+65 W 57452.2	.04	-232.2	14:03:02	88
0.4				
0+60 W 57466.1	.04	-232.2	14:03:21	88
-0.3				
0+55 W 57478.9	.04	-232.3	14:03:44	88
-2.1				
0+50 W 57497.6	.04	-231.8	14:10:02	88
0.7				
0+45 W 57509.3	.04	-231.3	14:11:21	88
3.6				
0+40 W 57507.3	.04	-230.5	14:11:50	88
3.2				
0+35 W 57497.3	.04	-230.8	14:12:28	88
1.4				
0+30 W 57483.5	.04	-231.1	14:12:46	88
-0.3				
0+25 W 57471.7	.03	-231.2	14:13:08	88
-0.6				
0+20 W 57464.3	.03	-230.7	14:13:27	88
-0.8				
0+15 W 57458.2	.04	-230.1	14:13:43	88
-1.9				
0+10 W 57465.1	.04	-229.3	14:14:01	88
2.3				
0+05 W 57455.0	.04	-228.6	14:14:33	88
1.3				
0+00 E 57434.0	.04	-226.7	14:15:08	88
-3.7				
0+05 E 57416.0	.04	-221.7	14:16:36	88
-4.4				
0+10 E 57403.2	.04	-221.7	14:16:57	88
-10.6				
0+15 E 57448.6	.04	-221.6	14:17:45	88
-1.8				
0+20 E 57488.3	.04	-221.4	14:18:19	88
7.8				
0+25 E 57495.2	.04	-224.1	14:19:38	88
10.1				
0+30 E 57459.5	.03	-225.0	14:19:56	88
-3.9				
0+35 E 57446.4	.04	-226.7	14:20:35	88
-4.6				
0+40 E 57439.2	.04	-227.2	14:20:55	88
-10.4				
0+45 E 57467.6	.04	-229.4	14:21:30	88
-2.8				
0+50 E 57490.3	.04	-230.8	14:22:09	88
5.9				
0+55 E 57480.9	.04	-231.1	14:24:50	88
-0.9				
0+60 E 57476.1	.04	-230.4	14:26:18	88
-5.1				



Line: 19+50 S Date: 19 MAR 89 #129
 POSITION FIELD ERR DRIFT TIME DS

1950



SWAMP CREEK MAGNETICS PROJECT
FOR: CANADA TUNGSTEN
MARCH 20, 1989

BY: ON-LINE EXPLORATION SVS. INC.
11976 WILDERNESS DRIVE
ANCHORAGE, ALASKA 99516

PRINTER WIDTH= 80 CHAR.S
ENTER 40, 80 OR 130

PRINTER WIDTH= 80 CHAR.S

TOTAL FIELD FULL SCALE= 100 GAMMAS
ENTER NEW SCALE (0 IF N/A)

TOTAL FIELD FULL SCALE= 100 GAMMAS

GRADIENT FULL SCALE= 10 GAMMAS
ENTER NEW SCALE (0 IF N/A)

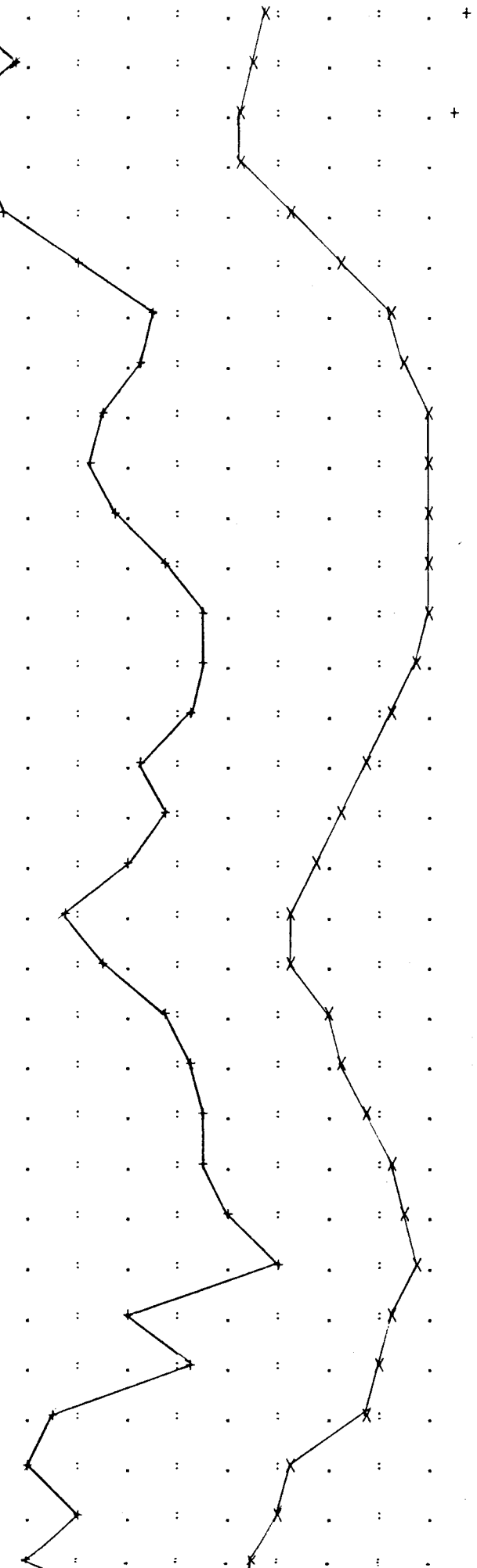
GRADIENT FULL SCALE= 10 GAMMAS

EDA OMNI-IV Tie-line MAG Ser #255007
TOTAL FIELD DATA (Base stn. corrected)
& GRADIENT
Date: 20 MAR 89
Operator: 5001
Reference field: 57450.0
Datum subtracted: 0.0
Records: 336
Bat: 15.6 Volt Lithium: 3.68 Volt
Last time update: 3/14 7:12:00
Start of print: 3/20 17:49:36

Base stn. Pos: 0+00 E Line: 0+00 N
Last time update: 3/14 7:12:00
Start of print: 3/20 17:49:27

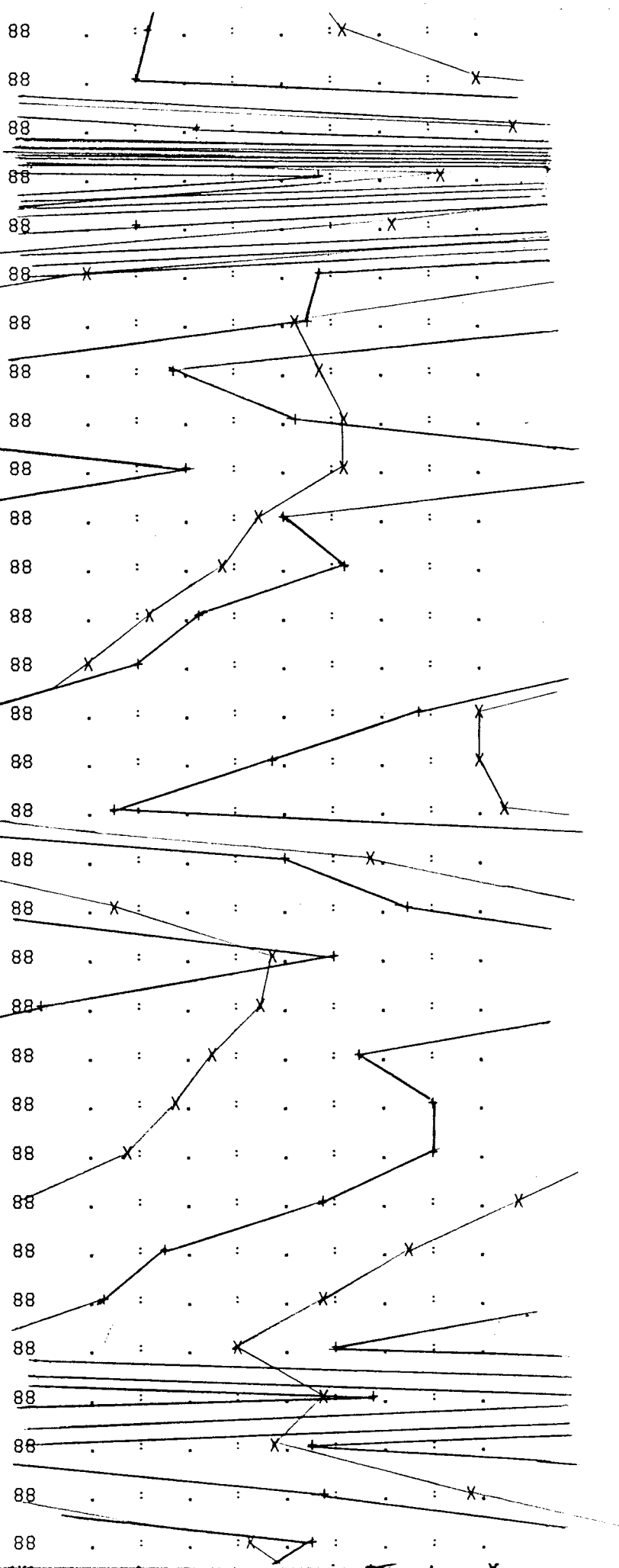
POSITION	FIELD	E	DRIFT	TIME	DS
2+30 W	57457.0	.06	-275.7	9:53:07	88
	-5.2				
2+25 W	57455.5	.05	-275.4	9:54:18	88
	-4.2				
2+20 W	57451.6	.06	-274.2	9:54:59	88
	-5.5				
2+15 W	57453.2	.06	-274.3	9:55:21	88
	-5.1				
2+10 W	57463.0	.05	-275.3	9:55:53	88
	-4.5				
2+05 W	57473.4	.05	-275.7	9:56:17	88
	-3.0				
2+00 W	57482.1	.06	-276.0	9:56:34	88
	-1.4				
1+95 W	57486.1	.06	-278.7	9:58:11	88
	-1.8				
1+90 W	57489.3	.06	-277.2	9:58:38	88
	-2.4				
1+85 W	57490.2	.05	-277.4	9:59:07	88
	-2.8				
1+80 W	57490.7	.05	-275.9	9:59:28	88
	-2.2				
1+75 W	57490.6	.05	-275.5	9:59:45	88
	-1.2				
1+70 W	57489.4	.05	-275.2	10:00:05	88
	-0.6				
1+65 W	57486.4	.05	-275.4	10:00:19	88
	-0.6				
1+60 W	57482.1	.06	-275.8	10:00:43	88
	-0.7				
1+55 W	57476.3	.06	-276.3	10:01:06	88
	-1.7				
1+50 W	57472.1	.05	-277.2	10:01:39	88
	-1.3				
1+45 W	57467.8	.05	-278.7	10:02:41	88
	-1.9				
1+40 W	57462.8	.06	-278.2	10:03:02	88
	-3.3				
1+35 W	57463.5	.06	-277.7	10:03:23	88
	-2.6				
1+30 W	57469.8	.04	-277.2	10:03:48	88
	-1.2				
1+25 W	57473.6	.06	-277.1	10:04:26	88
	-0.8				
1+20 W	57478.2	.05	-277.0	10:04:43	88
	-0.6				
1+15 W	57481.6	.06	-276.8	10:04:58	88
	-0.5				
1+10 W	57484.5	.05	-277.0	10:05:15	88
	-0.1				
1+05 W	57487.2	.06	-277.4	10:05:32	88
	0.9				
1+00 W	57481.5	.04	-277.4	10:05:46	88
	-2.0				
0+95 W	57481.0	.05	-275.5	10:06:49	88
	-0.8				
0+90 W	57476.4	.04	-274.8	10:07:13	88
	-3.5				
0+85 W	57463.7	.05	-273.9	10:07:45	88
	-3.9				
0+80 W	57460.5	.05	-273.2	10:08:02	88
	-3.0				
0+75 W	57454.9	.04	-272.9	10:08:15	88

2100



2106

0+65 W	57462.2	.05	-273.3	10:08:47	88
	-2.8				
0+60 W	57491.0	.05	-274.0	10:09:02	88
	-3.0				
0+55 W	57598.0	.05	-273.9	10:09:17	88
	18.2				
0+50 W	57781.9	.07	-273.7	10:09:33	88
	90.7				
0+45 W	57672.5	.05	-275.4	10:11:01	88
	37.1				
0+40 W	57510.2	.05	-274.6	10:11:24	88
	-9.3				
0+35 W	57453.1	.04	-272.5	10:12:04	88
	-9.4				
0+30 W	57457.1	.04	-272.9	10:12:35	88
	-2.2				
0+25 W	57461.9	.05	-271.2	10:13:03	88
	0.3				
0+20 W	57461.3	.04	-270.1	10:13:24	88
	7.9				
0+15 W	57445.1	.04	-269.9	10:13:45	88
	0.1				
0+10 W	57437.2	.05	-270.2	10:14:01	88
	1.2				
0+05 W	57422.6	.05	-269.9	10:14:18	88
	-1.8				
0+00 E	57410.6	.05	-269.9	10:14:34	88
	-3.0				
0+05 E	57390.9	.04	-269.3	10:17:34	88
	-7.3				
0+10 E	57389.3	.05	-267.2	10:18:15	88
	-10.3				
0+15 E	57394.1	.04	-268.0	10:19:06	88
	-13.5				
0+20 E	57466.4	.04	-267.2	10:19:31	88
	0.0				
0+25 E	57513.9	.05	-267.1	10:20:29	88
	2.5				
0+30 E	57546.3	.04	-265.9	10:20:54	88
	11.1				
0+35 E	57544.8	.04	-264.9	10:21:18	88
	4.9				
0+40 E	57535.0	.04	-264.5	10:21:49	88
	1.5				
0+45 E	57527.0	.04	-264.6	10:22:11	88
	2.9				
0+50 E	57518.2	.05	-265.0	10:22:42	88
	2.9				
0+55 E	57496.8	.05	-262.3	10:26:48	88
	0.8				
0+60 E	57473.8	.04	-262.0	10:27:05	88
	-2.6				
0+65 E	57457.8	.04	-262.7	10:27:23	88
	-3.7				
0+70 E	57440.6	.03	-262.5	10:27:43	88
	-9.1				
0+75 E	57456.3	.04	-262.9	10:28:19	88
	21.7				
0+80 E	57448.7	.04	-264.5	10:29:16	88
	-9.4				
0+85 E	57487.0	.05	-264.2	10:29:35	88
	0.7				
0+90 E	57542.2	.04	-263.1	10:29:58	88
	10.5				



44
12/1/88

44-3
12/1/88

44-3

44-3

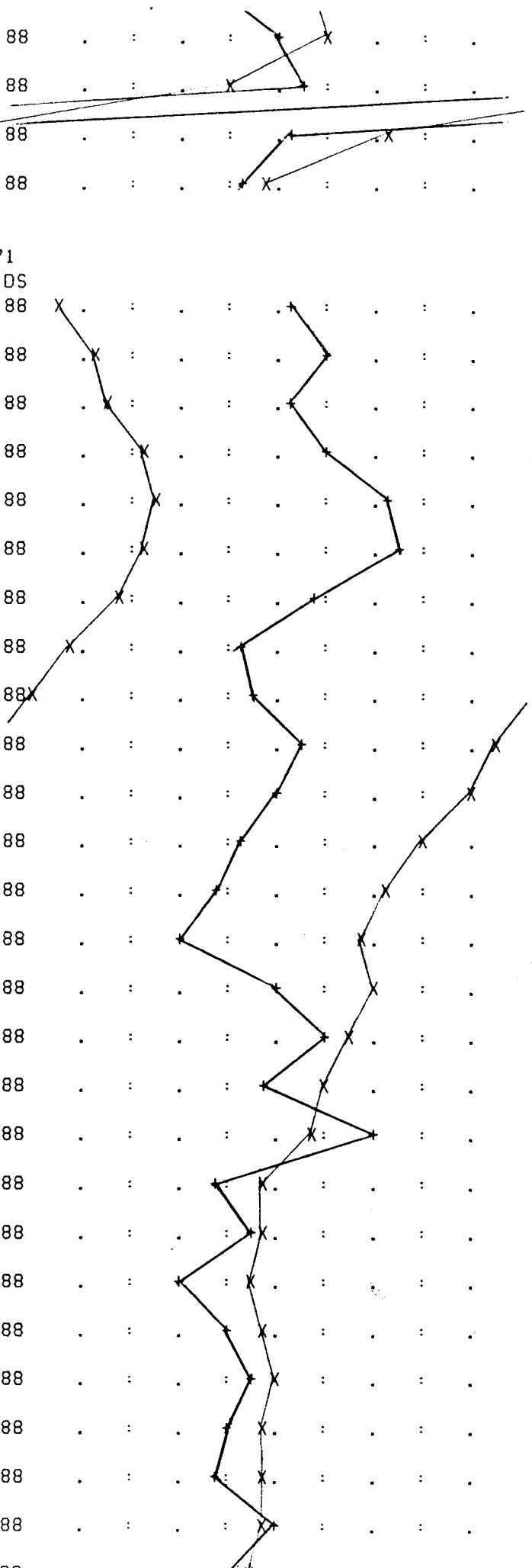
44-3

2100

1+00 E	57560.0	.05	-261.2	10:32:58	88
	10.1																			
1+05 E	57540.0	.04	-259.5	10:33:22	88
	10.4																			
1+10 E	57473.2	.05	-258.1	10:33:43	88
	-9.8																			
1+15 E	57448.0	.04	-257.2	10:34:06	88
	-10.8																			

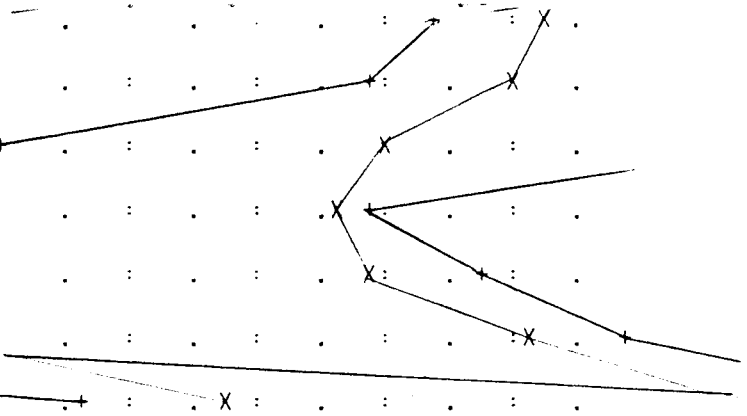
Line: 22+50 S Date: 20 MAR 89 #71
 POSITION FIELD ERR DRIFT TIME DS

2+20 W	57505.4	.05	-251.1	11:10:48	88
	0.3																			
2+15 W	57512.7	.04	-252.5	11:11:37	88
	0.9																			
2+10 W	57516.2	.05	-252.0	11:11:55	88
	0.2																			
2+05 W	57521.3	.04	-251.4	11:12:20	88
	0.9																			
2+00 W	57524.4	.05	-250.7	11:12:45	88
	2.3																			
1+95 W	57523.1	.05	-250.7	11:14:16	88
	2.5																			
1+90 W	57517.2	.04	-250.9	11:14:37	88
	0.8																			
1+85 W	57507.7	.04	-251.3	11:14:52	88
	-0.7																			
1+80 W	57499.1	.05	-251.6	11:15:09	88
	-0.6																			
1+75 W	57495.0	.05	-251.8	11:15:27	88
	0.4																			
1+70 W	57489.7	.04	-252.1	11:15:44	88
	0.1																			
1+65 W	57481.1	.05	-252.3	11:15:57	88
	-0.7																			
1+60 W	57471.9	.05	-251.6	11:16:11	88
	-1.3																			
1+55 W	57467.8	.05	-250.3	11:16:26	88
	-1.9																			
1+50 W	57469.3	.04	-249.7	11:17:29	88
	0.1																			
1+45 W	57466.2	.04	-249.5	11:17:44	88
	0.9																			
1+40 W	57460.9	.04	-249.1	11:17:59	88
	-0.2																			
1+35 W	57458.3	.04	-249.2	11:18:12	88
	1.9																			
1+30 W	57448.1	.05	-249.6	11:18:26	88
	-1.3																			
1+25 W	57447.1	.05	-250.3	11:18:40	88
	-0.4																			
1+20 W	57446.1	.04	-251.1	11:18:55	88
	-1.9																			
1+15 W	57446.6	.04	-251.3	11:19:08	88
	-1.1																			
1+10 W	57449.2	.05	-250.7	11:19:22	88
	-0.5																			
1+05 W	57448.5	.04	-251.5	11:19:40	88
	-0.9																			
1+00 W	57447.2	.04	-252.9	11:19:52	88
	-1.3																			
0+95 W	57447.4	.05	-250.9	11:20:49	88
	0.0																			



2250

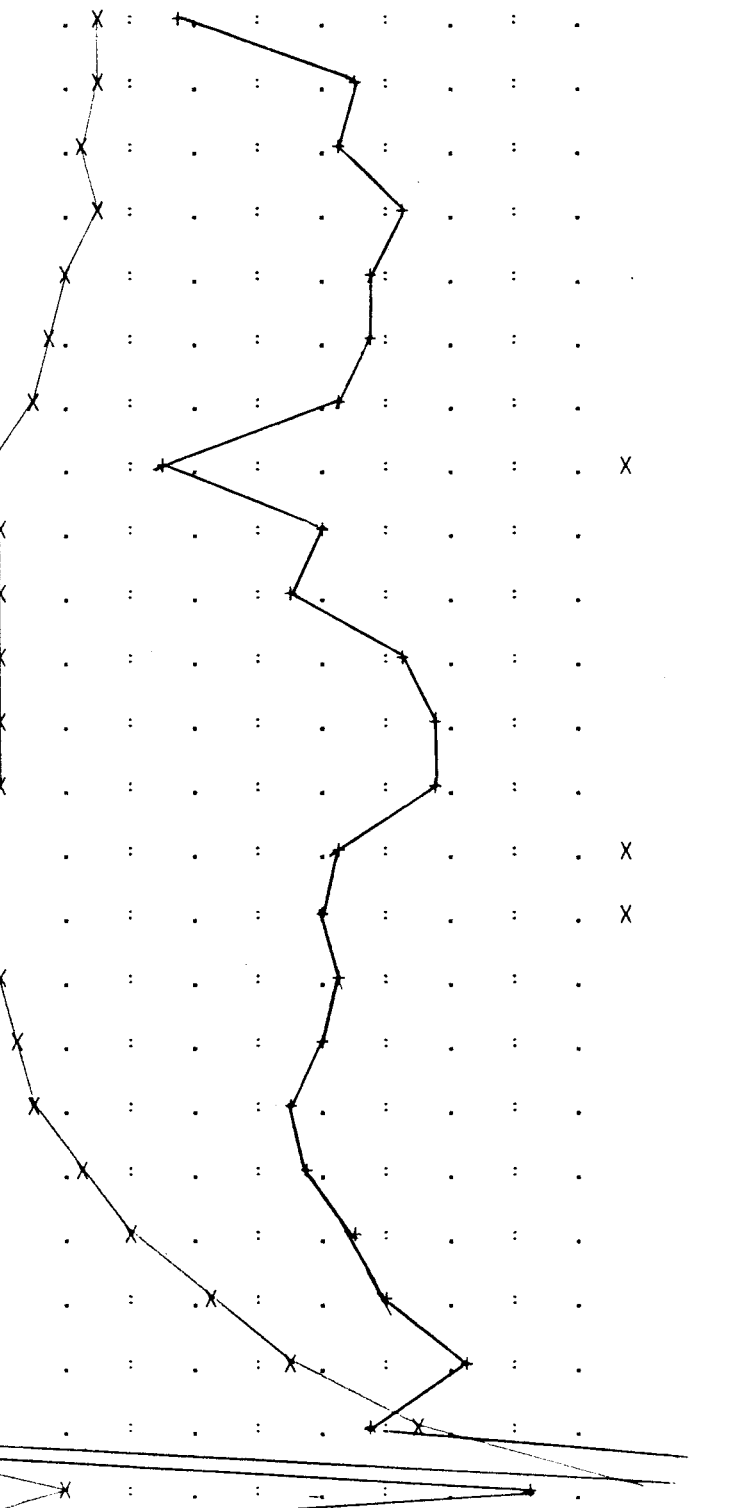
0+80 E	57486.0	.04	-240.8	11:34:06 88
	1.7			
0+85 E	57479.1	.04	-240.9	11:34:36 88
	0.7			
0+90 E	57460.5	.04	-241.5	11:34:58 88
	-5.1			
0+95 E	57452.2	.03	-240.2	11:35:30 88
	-9.3			
1+00 E	57456.8	.04	-240.4	11:36:49 88
	-7.4			
1+05 E	57482.7	.03	-240.8	11:37:20 88
	-5.3			
1+10 E	57534.5	.04	-240.0	11:38:16 88
	6.2			



BREAK IN SLOPE

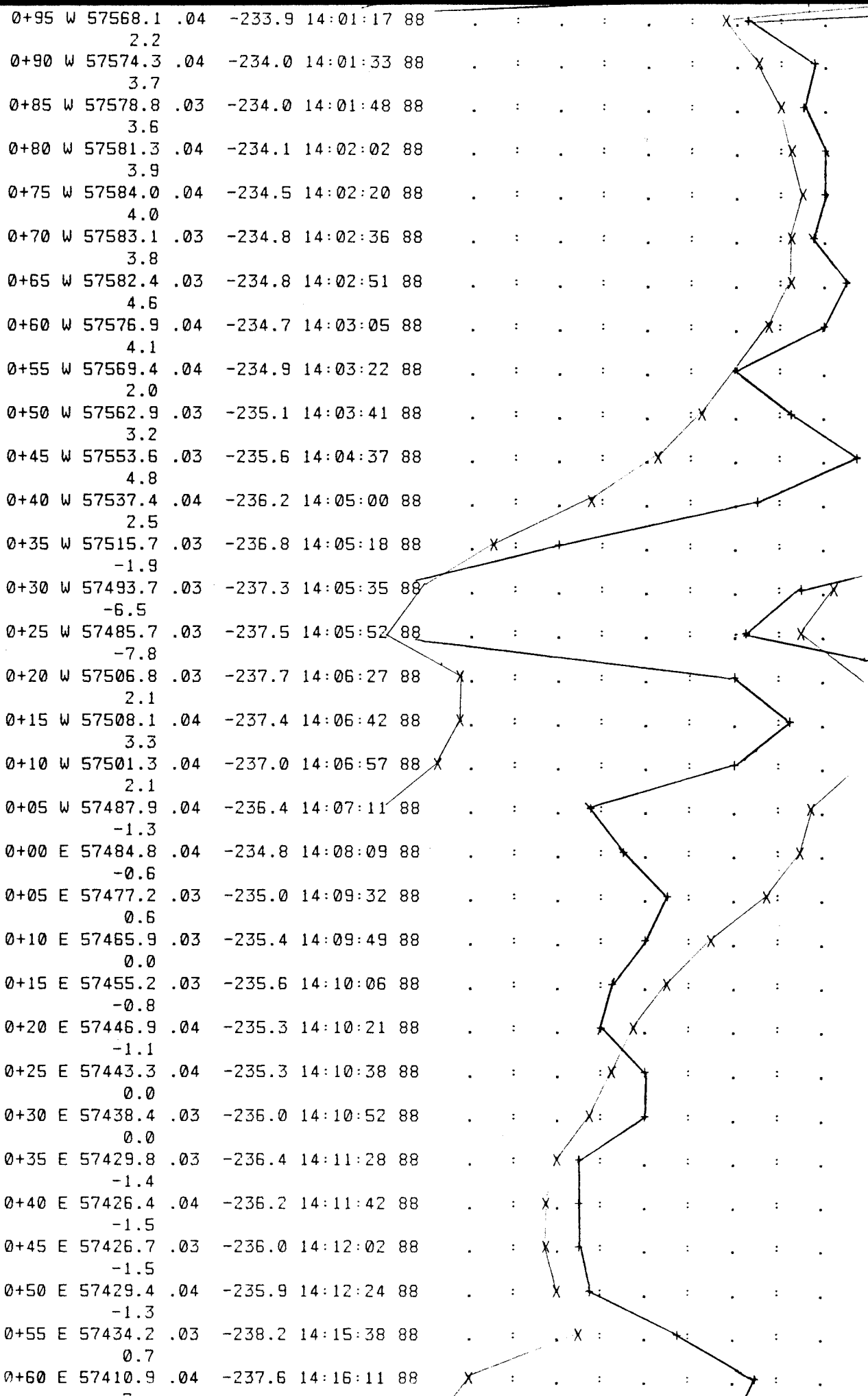
Line: 24+00 S Date: 20 MAR 89 #138

POSITION	FIELD	ERR	DRIFT	TIME	DS
2+15 W	57515.3	.03	-235.9	13:50:15 88	
	-2.2				
2+10 W	57515.3	.03	-236.1	13:50:57 88	
	0.5				
2+05 W	57513.7	.04	-236.0	13:51:26 88	
	0.3				
2+00 W	57515.1	.03	-235.7	13:51:45 88	
	1.3				
1+95 W	57510.9	.04	-234.7	13:52:37 88	
	0.7				
1+90 W	57508.6	.03	-235.2	13:53:02 88	
	0.8				
1+85 W	57504.7	.04	-235.2	13:53:29 88	
	0.2				
1+80 W	57497.2	.03	-235.5	13:54:00 88	
	-2.4				
1+75 W	57500.3	.03	-236.0	13:54:47 88	
	-0.1				
1+70 W	57499.5	.03	-235.5	13:55:23 88	
	-0.6				
1+65 W	57500.6	.03	-235.6	13:56:11 88	
	1.3				
1+60 W	57499.4	.04	-235.4	13:56:31 88	
	1.7				
1+55 W	57499.3	.04	-235.2	13:56:46 88	
	1.8				
1+50 W	57498.1	.04	-234.9	13:57:06 88	
	0.2				
1+45 W	57497.8	.03	-234.8	13:57:54 88	
	0.0				
1+40 W	57500.3	.03	-234.5	13:58:11 88	
	0.3				
1+35 W	57503.1	.04	-234.3	13:58:26 88	
	0.1				
1+30 W	57505.5	.03	-234.3	13:58:41 88	
	-0.4				
1+25 W	57511.4	.04	-234.4	13:58:57 88	
	-0.2				
1+20 W	57520.3	.04	-234.6	13:59:10 88	
	0.5				
1+15 W	57532.2	.04	-234.7	13:59:22 88	
	1.0				
1+10 W	57544.5	.03	-234.5	13:59:43 88	
	2.3				
1+05 W	57563.8	.04	-234.1	13:59:59 88	
	0.7				
1+00 W	57609.4	.03	-234.3	14:00:16 88	



INITIAL

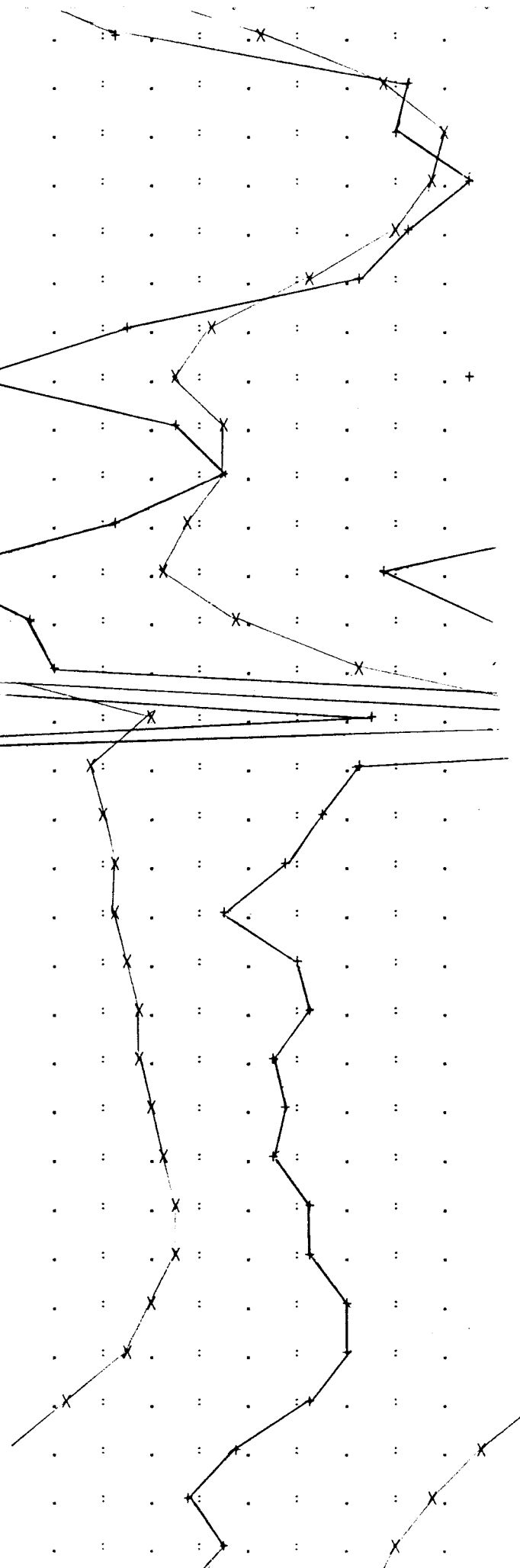
2400



DH-7

2400
CREEK

	0+75 E	57452.4	.04	-236.9	14:17:12	88
		-2.8				
	0+80 E	57476.5	.04	-237.3	14:17:28	88
		3.3				
	0+85 E	57490.5	.03	-237.4	14:17:45	88
		3.0				
	0+90 E	57487.0	.03	-238.1	14:18:22	88
		4.4				
	0+95 E	57480.6	.04	-238.5	14:18:44	88
		3.3				
245 →	1+00 E	57463.4	.03	-239.2	14:19:51	88
		2.2				
	1+05 E	57442.5	.04	-239.1	14:21:08	88
		-2.5				
	1+10 E	57435.3	.03	-239.4	14:21:27	88
		-5.4				
	1+15 E	57443.8	.03	-239.6	14:21:45	88
		-1.4				
	1+20 E	57446.1	.03	-240.0	14:22:12	88
		-0.4				
	1+25 E	57438.6	.03	-240.5	14:22:31	88
		-2.8				
	1+30 E	57432.4	.03	-240.2	14:22:48	88
		-7.3				
	1+35 E	57448.5	.03	-240.0	14:23:11	88
		-4.6				
	1+40 E	57473.2	.04	-240.2	14:23:35	88
		-3.9				
METAL STAPLE REBAR	1+45 E	57530.0	.03	-239.6	14:24:02	88
		22.4				
	1+50 E	57518.2	.04	-241.5	14:25:01	88
		2.3				
	1+55 E	57519.8	.03	-241.7	14:27:49	88
		1.4				
	1+60 E	57521.6	.04	-242.4	14:28:39	88
		0.8				
	1+65 E	57522.9	.03	-242.9	14:29:04	88
		-0.4				
	1+70 E	57525.9	.04	-243.2	14:29:27	88
		0.9				
	1+75 E	57528.0	.03	-243.1	14:29:47	88
		1.2				
	1+80 E	57528.3	.04	-242.8	14:30:10	88
		0.6				
	1+85 E	57530.4	.04	-242.9	14:30:32	88
		0.7				
	1+90 E	57532.9	.03	-243.1	14:30:58	88
		0.4				
	1+95 E	57534.2	.04	-243.3	14:31:15	88
		1.2				
	2+00 E	57533.9	.04	-243.5	14:31:44	88
		1.2				
	2+05 E	57531.2	.03	-249.6	14:49:34	88
		1.9				
	2+10 E	57524.1	.03	-250.0	14:49:52	88
		1.9				
	2+15 E	57512.7	.04	-250.2	14:50:05	88
		1.2				
	2+20 E	57498.6	.03	-250.5	14:50:19	88
		-0.2				
	2+25 E	57487.4	.03	-250.7	14:50:35	88
		-1.3				
	2+30 E	57481.0	.04	-250.8	14:50:51	88
		-0.5				

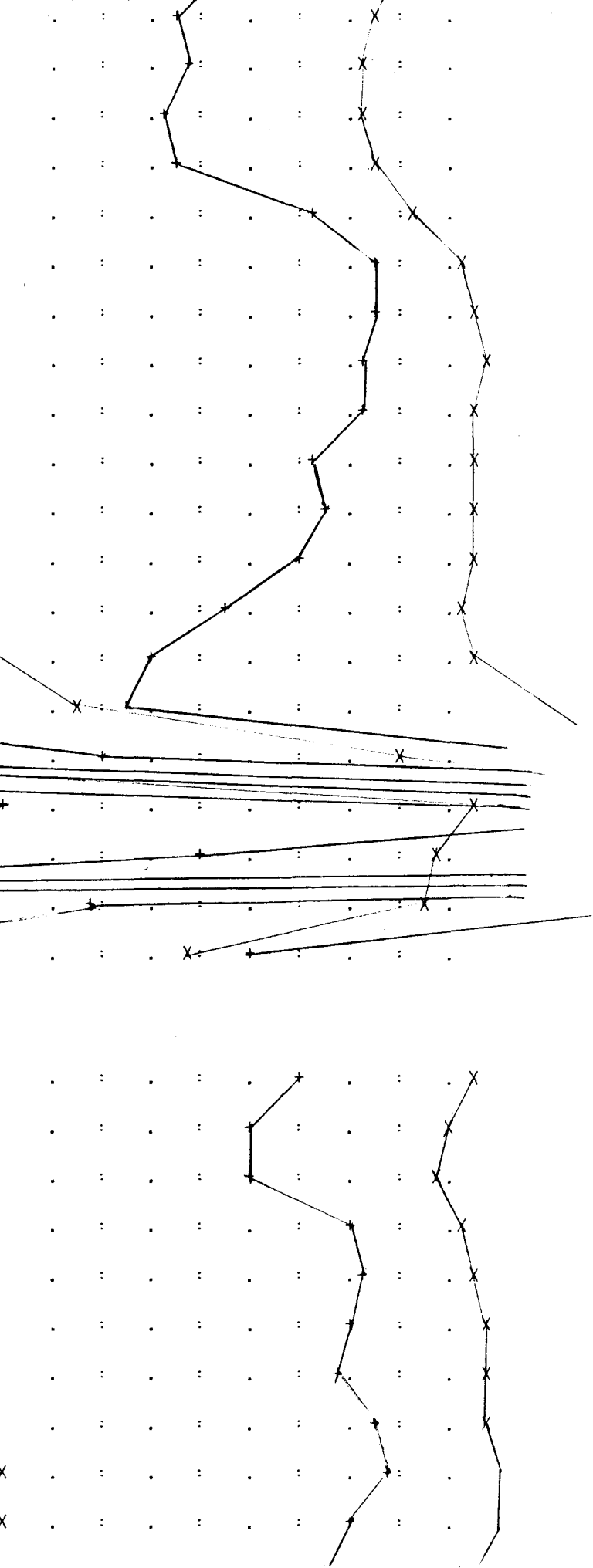


2+35 E 57476.0 .03 -250.9 14:51:05 88
 -1.4
 2+40 E 57473.5 .03 -251.1 14:51:21 88
 -1.2
 2+45 E 57471.3 .04 -251.2 14:51:36 88
 -1.7
 2+50 E 57473.9 .04 -251.5 14:51:55 88
 -1.4
 2+55 E 57483.1 .03 -252.2 14:52:44 88
 1.3
 2+60 E 57491.3 .03 -252.6 14:52:59 88
 2.4
 2+65 E 57495.4 .03 -252.3 14:53:18 88
 2.6
 2+70 E 57496.4 .03 -251.9 14:53:35 88
 2.2
 2+75 E 57495.9 .03 -251.9 14:53:52 88
 2.3
 2+80 E 57495.1 .03 -251.8 14:54:08 88
 1.3
 2+85 E 57494.8 .04 -251.6 14:54:24 88
 1.4
 2+90 E 57493.8 .04 -251.4 14:54:40 88
 1.1
 2+95 E 57491.3 .04 -251.3 14:54:54 88
 -0.5
 3+00 E 57494.5 .04 -251.3 14:55:11 88
 -2.0
 3+05 E 57514.3 .04 -250.6 14:59:55 88
 -2.6
 3+10 E 57581.1 .03 -250.5 15:00:11 88
 7.0
 3+15 E 57693.9 .03 -250.1 15:00:42 88
 44.9
 3+20 E 57686.9 .03 -249.6 15:01:05 88
 38.9
 3+25 E 57585.1 .04 -249.8 15:01:28 88
 6.8
 3+30 E 57536.3 .04 -250.0 15:01:46 88
 0.0

DH2 →

2400

DH.4
CASING →

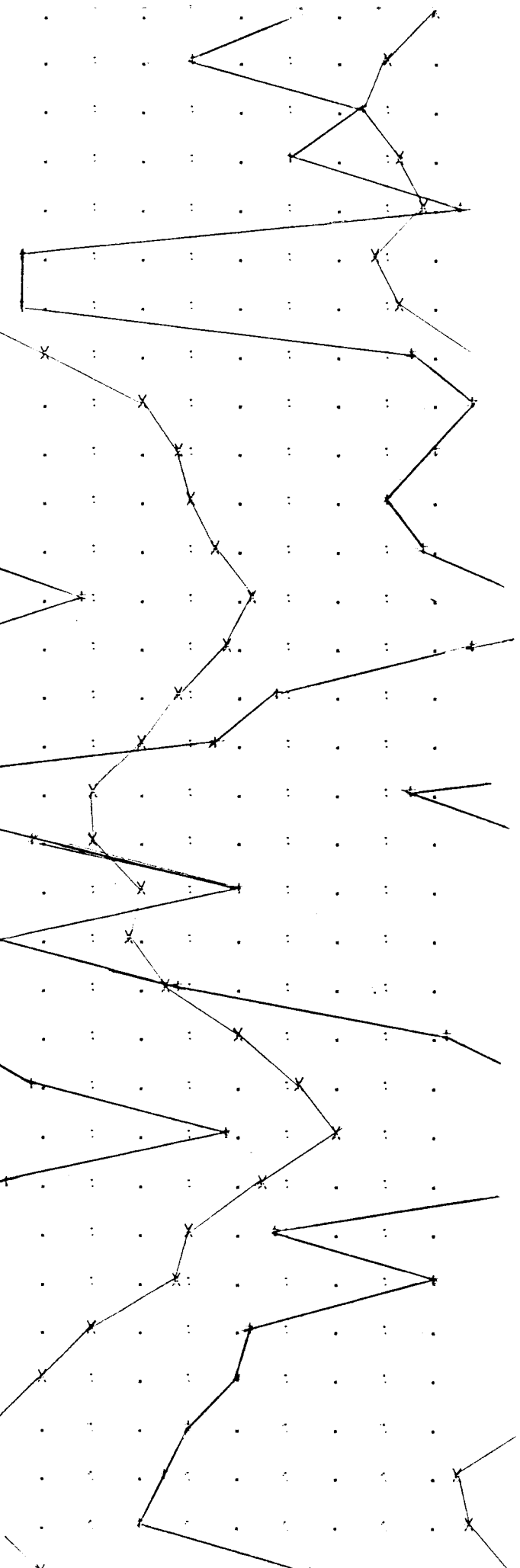


Line: 25+50 S Date: 20 MAR 89 #248
 POSITION FIELD ERR DRIFT TIME DS

2+15 W 57495.0 .04 -233.6 15:39:59 88
 1.1
 2+10 W 57489.1 .04 -232.2 15:40:57 88
 0.0
 2+05 W 57486.9 .04 -231.5 15:41:16 88
 -0.1
 2+00 W 57491.6 .04 -231.7 15:42:13 88
 2.1
 1+95 W 57496.1 .04 -231.0 15:42:30 88
 2.3
 1+90 W 57496.6 .04 -231.5 15:42:48 88
 1.9
 1+85 W 57497.0 .04 -231.9 15:43:03 88
 1.7
 1+80 W 57498.7 .04 -234.0 15:45:18 88
 2.4
 1+75 W 57499.9 .03 -233.8 15:45:39 88X
 2.7
 1+70 W 57499.0 .04 -232.1 15:46:40 88X
 1.9

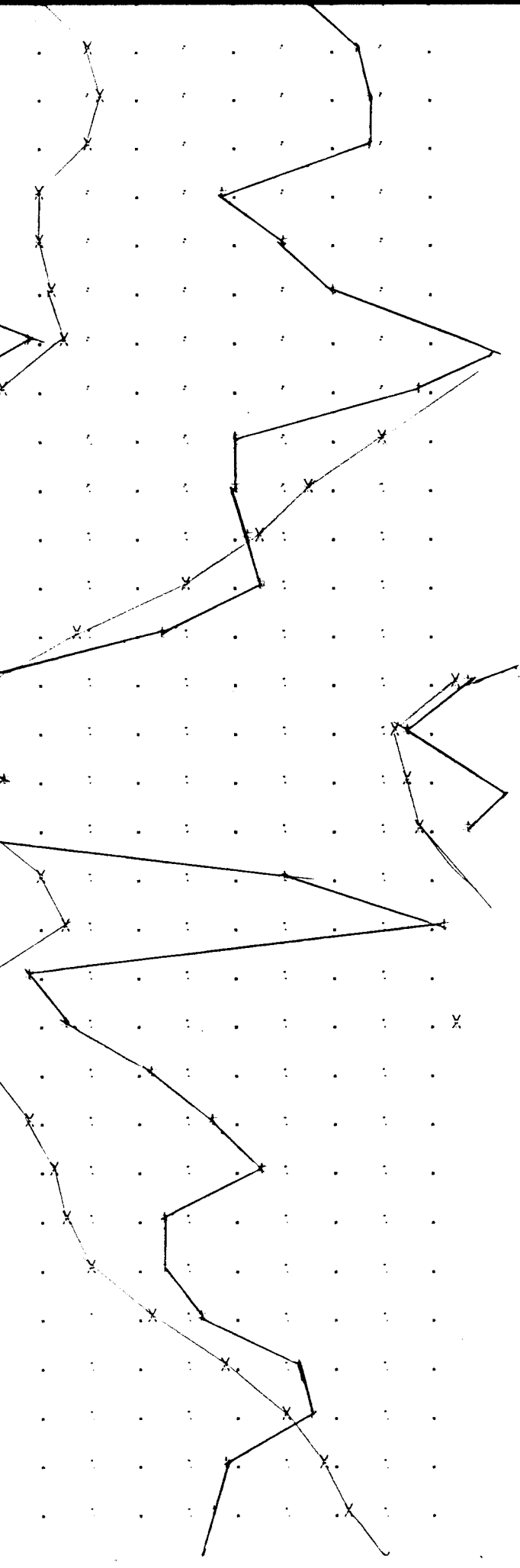
2550

1:55 W 57483.3	.04	-232.0	15:52:00	00
1.3				
1:50 W 57481.1	.03	-232.3	15:52:00	00
-1.1				
1:45 W 57475.0	.03	-232.3	15:52:20	00
2.6				
1:40 W 57481.7	.04	-231.7	15:52:50	00
0.9				
1:35 W 57487.0	.03	-231.3	15:53:11	00
4.5				
1:30 W 57477.0	.04	-231.4	15:53:31	00
-4.4				
1:25 W 57482.0	.03	-231.5	15:53:47	00
-4.4				
1:20 W 57510.3	.03	-231.6	15:54:02	00
3.4				
1:15 W 57530.2	.03	-231.6	15:54:17	00
4.8				
1:10 W 57537.7	.04	-231.7	15:54:33	00
4.0				
1:05 W 57538.8	.04	-231.7	15:54:51	00
3.1				
1:00 W 57545.2	.03	-231.5	15:55:12	00
3.7				
0:55 W 57551.0	.04	-231.0	15:55:50	00
5.8				
0:50 W 57547.7	.03	-231.1	15:56:13	00
4.7				
0:45 W 57537.1	.04	-231.5	15:56:27	00
0.7				
0:40 W 57530.8	.03	-231.4	15:56:42	00
-0.5				
0:35 W 57518.7	.04	-231.2	15:56:57	00
-6.5				
0:30 W 57518.4	.03	-231.4	15:57:11	00
-4.2				
0:25 W 57531.0	.03	-232.0	15:57:20	00
0.0				
0:20 W 57528.0	.03	-232.2	15:57:52	00
-5.1				
0:15 W 57535.0	.04	-232.1	15:58:13	00
-1.3				
0:10 W 57548.5	.04	-231.8	15:58:29	00
4.2				
0:45 W 57562.5	.04	-230.7	15:58:33	00
5.7				
0:40 W 57570.0	.04	-231.0	15:58:47	00
0.8				
0:35 W 57555.2	.04	-231.3	16:00:00	00
5.3				
0:30 W 57538.3	.03	-231.0	16:00:14	00
0.0				
0:25 W 57537.0	.03	-230.7	16:00:27	00
3.8				
0:20 W 57521.2	.04	-230.8	16:00:45	00
0.3				
0:15 W 57508.0	.03	-231.2	16:01:01	00
0.1				
0:10 W 57501.1	.04	-231.1	16:01:14	00
-1.0				
0:05 W 57495.5	.04	-230.8	16:01:30	00
-1.6				
0:00 C 57490.4	.03	-230.8	16:01:47	00
-2.1				
0:05 C 57511.0	.07	-230.2	16:02:35	00



2550

0:10 E 57520.0	.04	=230.2	16:02:52	00
2.5				
0:15 E 57523.7	.03	=230.3	16:03:00	00
2.0				
0:20 E 57510.0	.04	=230.3	16:03:26	00
2.7				
0:25 E 57510.0	.03	=230.1	16:03:41	00
=0.2				
0:30 E 57510.2	.03	=228.6	16:03:50	00
0.8				
0:35 E 57511.3	.03	=228.4	16:04:10	00
2.0				
0:40 E 57514.2	.04	=228.3	16:04:34	00
5.0				
0:45 E 57503.1	.03	=228.0	16:04:51	00
3.0				
0:50 E 57470.0	.04	=228.7	16:05:00	00
=0.1				
0:55 E 57464.0	.04	=227.8	16:06:15	00
=0.1				
0:60 E 57453.0	.03	=228.1	16:06:32	00
0.2				
0:65 E 57430.0	.04	=227.0	16:06:40	00
0.5				
0:70 E 57410.0	.03	=227.3	16:07:07	00
=1.0				
0:75 E 57390.2	.03	=226.3	16:07:23	00
=5.3				
0:80 E 57383.0	.03	=226.3	16:07:40	00
=0.5				
0:85 E 57384.0	.03	=227.3	16:08:01	00
=4.7				
0:90 E 57380.4	.03	=227.5	16:08:21	00
=5.3				
0:95 E 57411.0	.03	=227.0	16:08:40	00
1.1				
1:00 E 57410.3	.04	=227.0	16:10:30	00
4.3				
1:05 E 57380.0	.03	=227.0	16:12:20	00
=4.2				
1:10 E 57384.0	.03	=227.5	16:12:43	00
=3.5				
1:15 E 57401.2	.04	=226.0	16:13:00	00
=1.0				
1:20 E 57400.2	.04	=227.0	16:13:10	00
=0.5				
1:25 E 57413.0	.04	=227.0	16:13:30	00
0.4				
1:30 E 57414.0	.02	=227.0	16:13:54	00
=1.5				
1:35 E 57421.2	.04	=226.1	16:14:17	00
=1.4				
1:40 E 57433.0	.03	=225.0	16:14:30	00
=0.0				
1:45 E 57447.0	.03	=225.0	16:14:52	00
1.2				
1:50 E 57460.0	.03	=224.4	16:16:13	00
1.5				
1:55 E 57460.0	.03	=223.0	16:18:20	00
=0.2				
1:60 E 57472.0	.03	=222.7	16:18:40	00
=0.0				



T

2

APPENDIX IV

TABLE 3 PAY GRAVEL INTERCEPTS

TABLE 4 PAY GRAVEL RESERVES

FILE:SWBHGRDS.WK1

MOOSEHORN RANGE PLACER EXPLORATION PROJECT
 SWAMP CREEK DEFINITION DRILLING PROGRAM
 FEBRUARY - MARCH 1989
 GOLD INTERCEPT DATA

BHID	FROM (ft)	TO (ft)	LENGTH (ft)	FROM (m)	TO (m)	LENGTH (m)	VOLUME (l)	Au (mg)	GRADE (fopbcm)	GRADE (fgpbcm)	GRADE (fopbcy)	LN(GRAD) (fgpbcm)	LN(GRAD) (fopbcy)	WEIGHT (kg)	NOTES
800-1	12	18	6	3.7	5.5	1.8	18.0	5.806	0.32	0.37	0.009	-0.992	-4.697	30.0	GRAV +BRK Au
800-2A	14	16	2	4.3	4.9	0.6	2.5	0						4.5	GRAV
	16	18	2	4.9	5.5	0.6	5.0	0.01						8.0	GRAV
	18	20	2	5.5	6.1	0.6	14.0	3	0.21	0.25	0.006	-1.401	-5.106	27.0	GRAV
	20	22	2	6.1	6.7	0.6	7.0	0.01						9.0	GRAV
	22	24	2	6.7	7.3	0.6	12.0	1	0.08	0.10	0.002	-2.345	-6.051	17.0	GRAV
	24	25	1	7.3	7.6	0.3	10.5	1	0.10	0.11	0.003	-2.212	-5.917	26.0	GRAV/HBFP PPYY V/
800-3	12	14	2	3.7	4.3	0.6	21.0	0.327	0.02	0.02	0.000	-4.023	-7.728	31.0	GRAV ^+BRK Au
	14	16	2	4.3	4.9	0.6	16.5	0						27.0	GRAV
	16	18	2	4.9	5.5	0.6	16.5	0						27.0	GRAV
	18	20	2	5.5	6.1	0.6	16.0	0						25.0	GRAV
	20	22	2	6.1	6.7	0.6	15.0	0						25.0	GRAV
	22	24	2	6.7	7.3	0.6	17.0	0						26.0	GRAV
850-1	0	4	4	0.0	1.2	1.2	11.0	18.354	1.67	1.92	0.047	0.652	-3.054	19.0	GRAV
	4	6	2	1.2	1.8	0.6	10.0	14.6	1.46	1.68	0.041	0.519	-3.186	16.0	GRAV
850-2	6	8	2	1.8	2.4	0.6	6.0	35.219	5.87	6.75	0.166	1.910	-1.796	11.0	GRAV/GRDI
	8	10	2	2.4	3.0	0.6	11.0	92.657	8.42	9.69	0.238	2.271	-1.435	20.0	GRDI
850-3	16	18	2	4.9	5.5	0.6	1.0	0						1.5	GRAV
850-4	12	14	2	3.7	4.3	0.6	4.0	0.01						4.0	GRAV
	14	16	2	4.3	4.9	0.6	4.0	0						7.0	GRAV
	16	18	2	4.9	5.5	0.6	18.0	0						27.0	GRAV/HBFP PPYY?
850-5	4	6	2	1.2	1.8	0.6	17.0	0						22.0	GRAV
	6	8	2	1.8	2.4	0.6	13.0	0						19.0	GRAV
	8	10	2	2.4	3.0	0.6	14.0	0						22.0	GRAV/HBFP PPYY
900-1	4	10	6	1.2	3.0	1.8	11.0	140.371	12.76	14.68	0.361	2.686	-1.020	22.0	GRAV/QZ10-11 V*6/
900-2	4	10	6	1.2	3.0	1.8	8.0	72.176	9.02	10.38	0.255	2.339	-1.366	18.0	GRAV
950-1	0	8	8	0.0	2.4	2.4	9.0	12.141	1.35	1.55	0.038	0.439	-3.267	20.0	GRAV
950-2	0	2	2	0.0	0.6	0.6	2.5	7.967	3.19	3.66	0.090	1.299	-2.407	6.0	GRAV
	2	4	2	0.6	1.2	0.6	6.0	6.661	1.11	1.28	0.031	0.244	-3.461	12.0	GRAV
	4	6	2	1.2	1.8	0.6	8.0	0.01						15.5	GRAV
	6	8	2	1.8	2.4	0.6	5.0	25.730	5.15	5.92	0.145	1.778	-1.928	9.5	GRAV
950-4	12	14	2	3.7	4.3	0.6	4.0	0						8.0	GRAV
	14	16	2	4.3	4.9	0.6	12.0	0						22.5	GRAV
950-5	13	14	1	4.0	4.3	0.3	3.0	0						6.0	GRAV
	14	16	2	4.3	4.9	0.6	13.5	0						26.0	GRAV
	16	18	2	4.9	5.5	0.6	18.0	0						33.0	GRAV
1000-1	0	2	2	0.0	0.6	0.6	5.0	0						9.0	GRAV
	2	4	2	0.6	1.2	0.6	1.0	0						3.0	GRAV
	4	6	2	1.2	1.8	0.6	3.0	0.5	0.17	0.19	0.005	-1.652	-5.358	4.0	GRAV
	6	8	2	1.8	2.4	0.6	1.0	0.01	0.01	0.01	0.000	-4.465	-8.171	4.0	GRAV
	8	10	2	2.4	3.0	0.6	5.0	1	0.20	0.23	0.006	-1.470	-5.175	8.0	GRAV
	10	12	2	3.0	3.7	0.6	11.0	4.572	0.42	0.48	0.012	-0.738	-4.444	23.0	GRAV
	12	14	2	3.7	4.3	0.6	7.0	1	0.14	0.16	0.004	-1.806	-5.512	12.0	GRAV
1000-2	0	8	8	0.0	2.4	2.4	18.0	22.820	1.27	1.46	0.036	0.377	-3.329	48.0	GRAV/GRDI8-12V*2/
1000-3	0	2	2	0.0	0.6	0.6	4.0	0						8.0	GRAV HAND PANNED
	2	6	4	0.6	1.8	1.2	6.0	0						12.5	GRAV
	6	8	2	1.8	2.4	0.6	7.0	17.135	2.45	2.82	0.069	1.035	-2.671	15.5	GRAV
	8	10	2	2.4	3.0	0.6	11.5	6.212	0.54	0.62	0.015	-0.476	-4.182	21.0	GRAV
	10	12	2	3.0	3.7	0.6	3.5	1	0.29	0.33	0.008	-1.113	-4.819	7.5	GRAV

	20	22	2	6.1	6.7	0.6	8.0	0									13.5	GRAV?
	22	24	2	6.7	7.3	0.6	4.5	0									6.0	GRAV
	24	26	2	7.3	7.9	0.6	3.5	0.01									6.0	GRAV
	26	28	2	7.9	8.5	0.6	21.0	0									47.0	GRAV V CALC
	28	30	2	8.5	9.1	0.6	4.0	0									6.0	GRAV
	30	32	2	9.1	9.8	0.6	15.0	2	0.13	0.15	0.004	-1.875	-5.581			33.0	GRAV	
	32	34	2	9.8	10.4	0.6	7.5	0.5	0.07	0.08	0.002	-2.568	-6.274			29.5	GRAV/GRDI 34-36	
1500-1	14	16	2	4.3	4.9	0.6	13.0	2	0.15	0.18	0.004	-1.732	-5.438			24.0	GRAV ^V/2	
	16	18	2	4.9	5.5	0.6	9.0	0.5	0.06	0.06	0.002	-2.751	-6.456			14.0	GRAV	
	18	20	2	5.5	6.1	0.6	9.0	1	0.11	0.13	0.003	-2.057	-5.763			11.0	GRAV	
	20	22	2	6.1	6.7	0.6	12.0	3.207	0.27	0.31	0.008	-1.180	-4.886			20.0	GRAV	
	22	24	2	6.7	7.3	0.6	15.0	4.420	0.29	0.34	0.008	-1.082	-4.788			25.0	GRAV	
	24	26	2	7.3	7.9	0.6	9.0	14.001	1.56	1.79	0.044	0.582	-3.124			14.0	GRAV	
	26	28	2	7.9	8.5	0.6	3.0	0								7.0	GRAV	
	28	30	2	8.5	9.1	0.6	10.0	0.01								23.0	GRAV	
	30	32	2	9.1	9.8	0.6	18.0	3	0.17	0.19	0.005	-1.652	-5.358			28.0	GRAV	
	32	34	2	9.8	10.4	0.6	3.5	39.1	11.18	12.86	0.316	2.554	-1.152			10.0	GRAV/FP PPYY? V/2	
1500-2	16	18	2	4.9	5.5	0.6	14.0	1	0.07	0.08	0.002	-2.499	-6.205			20.0	GRAV ^+BRK Au	
	18	20	2	5.5	6.1	0.6	13.0	0.01								19.0	GRAV	
	20	22	2	6.1	6.7	0.6	10.0	15.211	1.52	1.75	0.043	0.559	-3.147			14.0	GRAV	
	22	24	2	6.7	7.3	0.6	15.0	14.258	0.95	1.09	0.027	0.089	-3.617			22.0	GRAV	
	24	26	2	7.3	7.9	0.6	14.0	28.990	2.07	2.38	0.059	0.868	-2.838			19.0	GRAV	
	26	28	2	7.9	8.5	0.6	13.0	50.773	3.91	4.49	0.110	1.502	-2.204			15.0	GRAV	
	28	30	2	8.5	9.1	0.6	12.0	27.549	2.30	2.64	0.065	0.971	-2.735			17.0	GRAV	
	30	34	4	9.1	10.4	1.2	29.0	19.4	0.67	0.77	0.019	-0.261	-3.967			40.0	GRAV +BRK Au	
1500-3	18	20	2	5.5	6.1	0.6	18.0	0.5	0.03	0.03	0.001	-3.444	-7.150			32.0	GRAV	
	20	22	2	6.1	6.7	0.6	8.0	0								14.0	GRAV	
	22	24	2	6.7	7.3	0.6	20.0	0.01								32.0	GRAV	
	24	26	2	7.3	7.9	0.6	7.0	1.881	0.27	0.31	0.008	-1.174	-4.880			11.0	GRAV	
	26	28	2	7.9	8.5	0.6	10.0	0								15.0	GRAV	
	28	30	2	8.5	9.1	0.6	9.0	1	0.11	0.13	0.003	-2.057	-5.763			18.0	GRAV +BRK Au	
1650-1	14	16	2	4.3	4.9	0.6	8.0	0								14.0	GRAV	
	16	18	2	4.9	5.5	0.6	6.0	0								12.0	GRAV	
	18	20	2	5.5	6.1	0.6	8.0	0								14.0	GRAV	
	20	22	2	6.1	6.7	0.6	5.0	0								8.0	GRAV	
	22	24	2	6.7	7.3	0.6	13.0	0.01								26.0	GRAV	
	24	26	2	7.3	7.9	0.6	7.0	0.01								12.0	GRAV	
	26	28	2	7.9	8.5	0.6	8.0	0.5	0.06	0.07	0.002	-2.633	-6.339			14.0	GRAV	
	28	30	2	8.5	9.1	0.6	10.0	0.01								20.0	GRAV	
	30	32	2	9.1	9.8	0.6	8.0	0.01								12.0	GRAV	
	32	34	2	9.8	10.4	0.6	22.0	13.798	0.63	0.72	0.018	-0.327	-4.033			37.0	GRAV	
1650-2	8	10	2	2.4	3.0	0.6	15.5	0								25.0	GRAV	
	10	12	2	3.0	3.7	0.6	7.0	0								11.0	GRAV	
	12	18	6	3.7	5.5	1.8	21.0	4.374	0.21	0.24	0.006	-1.429	-5.135			34.0	GRAV	
	18	20	2	5.5	6.1	0.6	13.0	5.803	0.45	0.51	0.013	-0.667	-4.373			21.0	GRAV	
	20	22	2	6.1	6.7	0.6	16.0	4.502	0.28	0.32	0.008	-1.128	-4.834			26.0	GRAV	
	22	24	2	6.7	7.3	0.6	12.5	2.590	0.21	0.24	0.006	-1.434	-5.140			20.0	GRAV	
	24	26	2	7.3	7.9	0.6	8.0	0								13.0	GRAV	
	26	28	2	7.9	8.5	0.6	11.0	0								18.0	GRAV	
	28	30	2	8.5	9.1	0.6	7.5	3.560	0.47	0.55	0.013	-0.605	-4.311			12.0	GRAV	
1650-3	22	26	4	6.7	7.9	1.2	6.0	0								15.0	GRAV	
	26	28	2	7.9	8.5	0.6	4.0	0.01								10.0	GRAV	
1650-4	22	24	2	6.7	7.3	0.6	8.0	0								15.0	GRAV	
	24	26	2	7.3	7.9	0.6	11.0	0								23.0	GRAV	
	26	30	4	7.9	9.1	1.2	12.0	0								24.0	GRAV	
	30	32	2	9.1	9.8	0.6	19.0	3.706	0.20	0.22	0.006	-1.495	-5.200			36.0	GRAV	

	32	34	2	9.8	10.4	0.6	21.0	0.01							44.0	GRAV
	34	36	2	10.4	11.0	0.6	6.0	0							14.0	GRAV
	36	38	2	11.0	11.6	0.6	18.0	8.411	0.47	0.54	0.013	-0.621	-4.327	37.0	GRAV	
	38	40	2	11.6	12.2	0.6	17.0	15.762	0.93	1.07	0.026	0.064	-3.642	32.0	GRAV	
	40	42	2	12.2	12.8	0.6	9.0	0.5	0.06	0.06	0.002	-2.751	-6.456	14.0	GRAV	
	42	44	2	12.8	13.4	0.6	17.0	49.893	2.93	3.38	0.083	1.216	-2.489	22.0	GRAV	
	44	46	2	13.4	14.0	0.6	10.0	35.0	3.50	4.03	0.099	1.394	-2.312	12.0	GRAV +BRK Au	
2100-1	14	16	2	4.3	4.9	0.6	9.0	0						13.0	GRAV	
	16	18	2	4.9	5.5	0.6	10.0	2.731	0.27	0.31	0.008	-1.158	-4.864	15.0	GRAV	
	18	20	2	5.5	6.1	0.6	10.0	1	0.10	0.11	0.003	-2.163	-5.869	16.0	GRAV	
	20	22	2	6.1	6.7	0.6	15.0	17.064	1.14	1.31	0.032	0.269	-3.437	25.0	GRAV	
	22	23	1	6.7	7.0	0.3	6.0	10.330	1.72	1.98	0.049	0.683	-3.023	18.0	GRAV/GRDI V/2	
2100-2	6	8	2	1.8	2.4	0.6	9.0	0						15.0	GRAV	
	8	10	2	2.4	3.0	0.6	9.0	0.01						14.0	GRAV	
	10	12	2	3.0	3.7	0.6	9.0	0.5	0.06	0.06	0.002	-2.751	-6.456	18.0	GRAV	
	12	14	2	3.7	4.3	0.6	4.0	5.556	1.39	1.60	0.039	0.468	-3.237	8.0	GRAV	
	14	16	2	4.3	4.9	0.6	11.0	0.5	0.05	0.05	0.001	-2.951	-6.657	19.0	GRAV	
	16	18	2	4.9	5.5	0.6	9.0	0.01						16.0	GRAV	
	18	20	2	5.5	6.1	0.6	12.0	4.770	0.40	0.46	0.011	-0.783	-4.489	18.0	GRAV	
	20	22	2	6.1	6.7	0.6	4.0	0.5	0.13	0.14	0.004	-1.940	-5.645	6.0	GRAV	
2100-3	24	26	2	7.3	7.9	0.6	16.0	0						25.0	GRAV	
	26	28	2	7.9	8.5	0.6	8.0	0						13.0	GRAV	
2100-4	42	44	2	12.8	13.4	0.6	25.0	0						40.0	GRAV	
	44	46	2	13.4	14.0	0.6	11.0	0						17.0	GRAV	
	46	48	2	14.0	14.6	0.6	17.0	0						26.0	GRAV	
	48	50	2	14.6	15.2	0.6	18.0	1.653	0.09	0.11	0.003	-2.248	-5.954	24.0	GRAV	
	50	52	2	15.2	15.8	0.6	11.0	3.844	0.35	0.40	0.010	-0.912	-4.617	16.0	GRAV	
	52	54	2	15.8	16.5	0.6	6.0	1.991	0.33	0.38	0.009	-0.963	-4.669	10.0	GRAV	
	54	56	2	16.5	17.1	0.6	6.0	1.829	0.30	0.35	0.009	-1.048	-4.754	11.0	GRAV	
	56	58	2	17.1	17.7	0.6	5.0	0.01						8.0	GRAV	
	58	60	2	17.7	18.3	0.6	8.0	0						13.0	GRAV	
	60	62	2	18.3	18.9	0.6	10.0	3.562	0.36	0.41	0.010	-0.893	-4.598	16.0	GRAV	
	62	64	2	18.9	19.5	0.6	8.0	7.622	0.95	1.10	0.027	0.091	-3.614	13.0	GRAV	
2400-5	8	10	2	2.4	3.0	0.6	6.0	0						12.0	GRAV	
	10	12	2	3.0	3.7	0.6	15.0	0						27.0	GRAV	
	12	14	2	3.7	4.3	0.6	7.0	0						13.0	GRAV	
	14	16	2	4.3	4.9	0.6	10.0	6.081	0.61	0.70	0.017	-0.358	-4.063	15.0	GRAV	
	16	18	2	4.9	5.5	0.6	7.0	1.875	0.27	0.31	0.008	-1.178	-4.883	11.0	GRAV	
	18	20	2	5.5	6.1	0.6	7.0	0						10.0	GRAV	
	20	22	2	6.1	6.7	0.6	7.0	0						9.0	GRAV	
	22	24	2	6.7	7.3	0.6	7.0	0						12.0	GRAV	
2400-6	6	8	2	1.8	2.4	0.6	3.0	0						5.0	GRAV	
	8	10	2	2.4	3.0	0.6	11.0	0						19.0	GRAV	
	10	12	2	3.0	3.7	0.6	20.0	4.721	0.24	0.27	0.007	-1.304	-5.010	32.0	GRAV	
	12	14	2	3.7	4.3	0.6	12.0	0						19.0	GRAV	
	14	16	2	4.3	4.9	0.6	7.0	0						14.0	GRAV	
	16	18	2	4.9	5.5	0.6	7.0	3.946	0.56	0.65	0.016	-0.433	-4.139	15.0	GRAV	
	18	20	2	5.5	6.1	0.6	7.0	5.5	0.79	0.91	0.022	-0.098	-3.804	15.0	GRAV +BRK Au	
2400-7	30	32	2	9.1	9.8	0.6	22.0	0						45.0	GRAV	
	32	34	2	9.8	10.4	0.6	6.0	0						10.0	GRAV V CALC	
2700-1	15	18	3	4.6	5.5	0.9	4.0	0						12.0	GRAV	
	18	20	2	5.5	6.1	0.6	8.0	0.5	0.06	0.07	0.002	-2.633	-6.339	15.0	GRAV	
	20	22	2	6.1	6.7	0.6	14.0	4.088	0.29	0.34	0.008	-1.091	-4.797	29.0	GRAV	
	22	24	2	6.7	7.3	0.6	9.0	0						16.0	GRAV	
	24	26	2	7.3	7.9	0.6	12.0	0.01						23.0	GRAV	
	26	28	2	7.9	8.5	0.6	11.0	0.01						18.0	GRAV	

	28	30	2	8.5	9.1	0.6	10.0	1	0.10	0.11	0.003	-2.163	-5.869	13.0	GRAV
	30	32	2	9.1	9.8	0.6	13.0	4.250	0.33	0.38	0.009	-0.978	-4.684	26.0	GRAV
	32	34	2	9.8	10.4	0.6	11.0	0						16.0	GRAV
	34	36	2	10.4	11.0	0.6	9.0	0						13.0	GRAV
	36	38	2	11.0	11.6	0.6	9.0	0						13.0	GRAV
	38	40	2	11.6	12.2	0.6	10.0	0						14.0	GRAV
	40	42	2	12.2	12.8	0.6	10.0	0.5	0.05	0.06	0.001	-2.856	-6.562	14.0	GRAV
	42	44	2	12.8	13.4	0.6	9.0	0						13.0	GRAV
	44	46	2	13.4	14.0	0.6	8.0	0.01						12.0	GRAV
	46	48	2	14.0	14.6	0.6	6.0	0.01						9.0	GRAV
	48	50	2	14.6	15.2	0.6	5.0	1	0.20	0.23	0.006	-1.470	-5.175	8.0	GRAV
	50	52	2	15.2	15.8	0.6	10.0	5.4	0.54	0.62	0.015	-0.475	-4.181	14.0	GRAV +BRK Au
2700-2	17	20	3	5.2	6.1	0.9	12.0	0						24.0	GRAV
	20	22	2	6.1	6.7	0.6	20.0	0						38.0	GRAV
	22	24	2	6.7	7.3	0.6	10.0	0						14.0	GRAV
	24	26	2	7.3	7.9	0.6	12.0	0						17.0	GRAV
	26	28	2	7.9	8.5	0.6	4.0	0.5	0.13	0.14	0.004	-1.940	-5.645	6.0	GRAV
	28	30	2	8.5	9.1	0.6	14.0	0.01						19.0	GRAV
	30	32	2	9.1	9.8	0.6	7.0	0						15.0	GRAV
	32	38	6	9.8	11.6	1.8	10.0	0						17.0	GRAV
2700-3	22	24	2	6.7	7.3	0.6	10.0	0						12.0	GRAV
	24	26	2	7.3	7.9	0.6	16.0	0.5	0.03	0.04	0.001	-3.326	-7.032	22.0	GRAV
	26	28	2	7.9	8.5	0.6	16.0	0.5	0.03	0.04	0.001	-3.326	-7.032	24.0	GRAV
	28	30	2	8.5	9.1	0.6	13.0	1.481	0.11	0.13	0.003	-2.032	-5.738	19.0	GRAV
	30	32	2	9.1	9.8	0.6	5.0	1.314	0.26	0.30	0.007	-1.197	-4.902	6.0	GRAV
	32	33	1	9.8	10.1	0.3	3.5	0.5	0.14	0.16	0.004	-1.806	-5.512	10.0	GRAV/GRDI V/2
2700-4	54	56	2	16.5	17.1	0.6	11.0	0						24.0	GRAV
	56	58	2	17.1	17.7	0.6	12.0	0						21.0	GRAV
	58	60	2	17.7	18.3	0.6	6.0	0.01						9.0	GRAV
	60	62	2	18.3	18.9	0.6	7.0	0						10.0	GRAV
2700-5	32	36	4	9.8	11.0	1.2	18.0	0						28.0	GRAV
	36	40	4	11.0	12.2	1.2	11.0	0						32.0	GRAV
	40	42	2	12.2	12.8	0.6	16.0	0						32.0	GRAV
	42	44	2	12.8	13.4	0.6	16.0	0						28.0	GRAV
	44	46	2	13.4	14.0	0.6	11.0	0						14.0	GRAV
	46	48	2	14.0	14.6	0.6	13.0	0						22.0	GRAV
	48	50	2	14.6	15.2	0.6	11.0	0						20.0	GRAV
	50	52	2	15.2	15.8	0.6	12.0	0						21.0	GRAV
	52	54	2	15.8	16.5	0.6	12.0	0						21.0	GRAV
	54	56	2	16.5	17.1	0.6	8.0	0						14.0	GRAV
	56	58	2	17.1	17.7	0.6	16.0	0						26.0	GRAV
	58	60	2	17.7	18.3	0.6	16.0	0						25.0	GRAV
	60	62	2	18.3	18.9	0.6	17.0	4.572	0.27	0.31	0.008	-1.174	-4.879	21.0	GRAV
	62	64	2	18.9	19.5	0.6	13.0	2.748	0.21	0.24	0.006	-1.414	-5.120	23.0	GRAV
3000-1	19	22	3	5.8	6.7	0.9	14.0	28.4	2.03	2.33	0.057	0.847	-2.859	32.0	GRAV +BRK Au
3000-2	26	30	4	7.9	9.1	1.2	19.0	0						33.0	GRAV
	30	32	2	9.1	9.8	0.6	15.0	0						22.0	GRAV
	32	34	2	9.8	10.4	0.6	13.0	0.5	0.04	0.04	0.001	-3.118	-6.824	19.0	GRAV
	34	36	2	10.4	11.0	0.6	11.0	0.5	0.05	0.05	0.001	-2.951	-6.657	17.0	GRAV
	36	38	2	11.0	11.6	0.6	11.0	0.01						16.0	GRAV
	38	40	2	11.6	12.2	0.6	9.0	0.01						12.0	GRAV
	40	44	4	12.2	13.4	1.2	5.5	3.751	0.68	0.78	0.019	-0.243	-3.949	35.0	GRAV/GRDI41-44 V/
3000-3	23	25	2	7.0	7.6	0.6	20.0	2.240	0.11	0.13	0.003	-2.049	-5.755	39.0	GRAV
	25	27	2	7.6	8.2	0.6	9.0	0						14.0	GRAV
	27	29	2	8.2	8.8	0.6	14.0	1	0.07	0.08	0.002	-2.499	-6.205	22.0	GRAV
	29	31	2	8.8	9.4	0.6	14.0	0						24.0	GRAV

	31	33	2	9.4	10.1	0.6	10.0	0									17.0	GRAV
	33	35	2	10.1	10.7	0.6	8.0	1.077	0.13	0.15	0.004	-1.866	-5.571				14.0	GRAV
	35	37	2	10.7	11.3	0.6	7.0	0									10.0	GRAV
	37	39	2	11.3	11.9	0.6	9.0	5.652	0.63	0.72	0.018	-0.325	-4.031				13.0	GRAV
	39	41	2	11.9	12.5	0.6	7.0	0									10.0	GRAV
	41	43	2	12.5	13.1	0.6	13.0	0.5	0.04	0.04	0.001	-3.118	-6.824				18.0	GRAV
	43	45	2	13.1	13.7	0.6	13.0	0.5	0.04	0.04	0.001	-3.118	-6.824				18.0	GRAV
3300-1	28	30	2	8.5	9.1	0.6	9.0	0									18.0	GRAV
	30	32	2	9.1	9.8	0.6	17.0	0									34.0	GRAV
	32	36	4	9.8	11.0	1.2	11.0	0									20.0	GRAV
	36	38	2	11.0	11.6	0.6	18.0	1	0.06	0.06	0.002	-2.751	-6.456				37.0	GRAV
	38	40	2	11.6	12.2	0.6	16.0	0.01									27.0	GRAV
	40	42	2	12.2	12.8	0.6	14.0	2.5	0.18	0.21	0.005	-1.583	-5.289				23.0	GRAV
3300-2	41	43	2	12.5	13.1	0.6	19.0	1.078	0.06	0.07	0.002	-2.730	-6.435				42.0	GRAV
	43	45	2	13.1	13.7	0.6	11.0	0									18.0	GRAV
	45	47	2	13.7	14.3	0.6	8.0	0									14.0	GRAV
	47	49	2	14.3	14.9	0.6	6.0	0									10.0	GRAV
	49	51	2	14.9	15.5	0.6	7.0	0									14.0	GRAV
	51	53	2	15.5	16.2	0.6	12.0	0									18.0	GRAV
	53	57	4	16.2	17.4	1.2	10.0	0									16.0	GRAV
	57	59	2	17.4	18.0	0.6	6.0	0.5	0.08	0.10	0.002	-2.345	-6.051				11.0	GRAV
3300-3	38	40	2	11.6	12.2	0.6	6.0	1.725	0.29	0.33	0.008	-1.107	-4.813				12.0	GRAV
	40	42	2	12.2	12.8	0.6	11.0	0.5	0.05	0.05	0.001	-2.951	-6.657				23.0	GRAV
	42	44	2	12.8	13.4	0.6	8.0	0									14.0	GRAV
	44	46	2	13.4	14.0	0.6	9.0	0									14.0	GRAV
	46	48	2	14.0	14.6	0.6	6.0	0									10.0	GRAV
	48	52	4	14.6	15.8	1.2	22.0	1.622	0.07	0.08	0.002	-2.468	-6.173				35.0	GRAV

NIL SAMPLES = 130
TR SAMPLES = 37

NUMBER =	300	300	134	134	134	134	134	299
MEAN =	11.0	4.699	1.03	1.18	0.029	-0.907	-4.613	19.2
STD DEV =	5.6	13.6	1.96	2.25	0.055	1.469	1.469	9.7
VAR =	31.8	183.7	3.83	5.07	0.003	2.159	2.159	94.6

FREQUENCY DISTRIBUTION	n	130	37	80	16	12	7	1	4	2	3	1	2	1	1	0	1	1	1
LOWER CLASS LIMIT		0	0.01	5	10	15	20	25	30	35	40	45	50	60	70	80	90	100	150

BHID	FROM (ft)	TO (ft)	LENGTH (ft)	FROM (m)	TO (m)	LENGTH (m)	VOLUME (l)	Au (mg)	GRADE (foplcm)	GRADE (fgpbcm)	GRADE (fopbcy)	LN (GRAD) (fgpbcm)	LN (GRAD) (fopbcy)	WEIGHT (kg)	NOTES
SOYA-1	10	22	12	3.0	6.7	3.7	24.0	0						45.0	? 12-14 NO SAMPLE
SOYA-2	13	14	1	4.0	4.3	0.3	7.0	0.5	0.07	0.08	0.002	-2.499	-6.205	14.0	GRAV
	14	16	2	4.3	4.9	0.6	12.0	2.074	0.17	0.20	0.005	-1.616	-5.321	20.0	GRAV
	16	18	2	4.9	5.5	0.6	5.0	0.5	0.10	0.11	0.003	-2.163	-5.869	10.0	GRAV
	18	20	2	5.5	6.1	0.6	7.0	0						13.0	GRAV
	20	22	2	6.1	6.7	0.6	12.0	0.01						20.0	GRAV
	22	24	2	6.7	7.3	0.6	10.0	0.5	0.05	0.06	0.001	-2.856	-6.562	18.0	GRAV
	24	26	2	7.3	7.9	0.6	13.0	0.5	0.04	0.04	0.001	-3.118	-6.824	20.0	GRAV/GRDI?
SOYA-3	19	20	1	5.8	6.1	0.3	8.0	12.982	1.62	1.87	0.046	0.624	-3.082	18.0	GRAV
	20	22	2	6.1	6.7	0.6	12.0	41.037	3.42	3.93	0.097	1.369	-2.336	20.0	GRAV
	22	24	2	6.7	7.3	0.6	14.0	44.065	3.15	3.62	0.089	1.286	-2.419	24.0	GRAV
	24	26	2	7.3	7.9	0.6	12.0	24.2	2.02	2.32	0.057	0.842	-2.864	20.0	GRAV +BRK Au
SOYA-4	8	10	2	2.4	3.0	0.6	15.0	0.01						26.0	GRAV
	10	11	1	3.0	3.4	0.3	7.0	1.628	0.23	0.27	0.007	-1.319	-5.025	25.0	GRAV/GRDI V/2
SOYA-5	18	20	2	5.5	6.1	0.6	12.0	0.01						25.0	GRAV
	20	22	2	6.1	6.7	0.6	16.0	9.700	0.61	0.70	0.017	-0.361	-4.066	32.0	GRAV
	22	24	2	6.7	7.3	0.6	15.0	0.5	0.03	0.04	0.001	-3.261	-6.967	26.0	GRAV
	24	26	2	7.3	7.9	0.6	9.0	0.5	0.06	0.06	0.002	-2.751	-6.456	13.0	GRAV

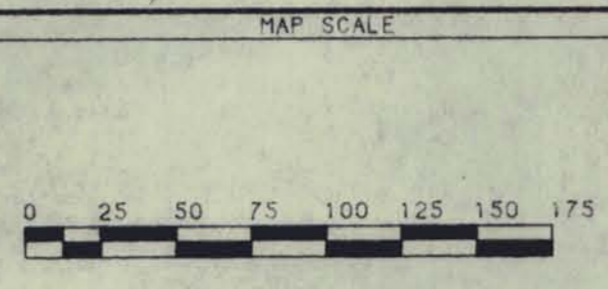
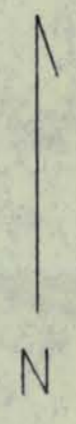
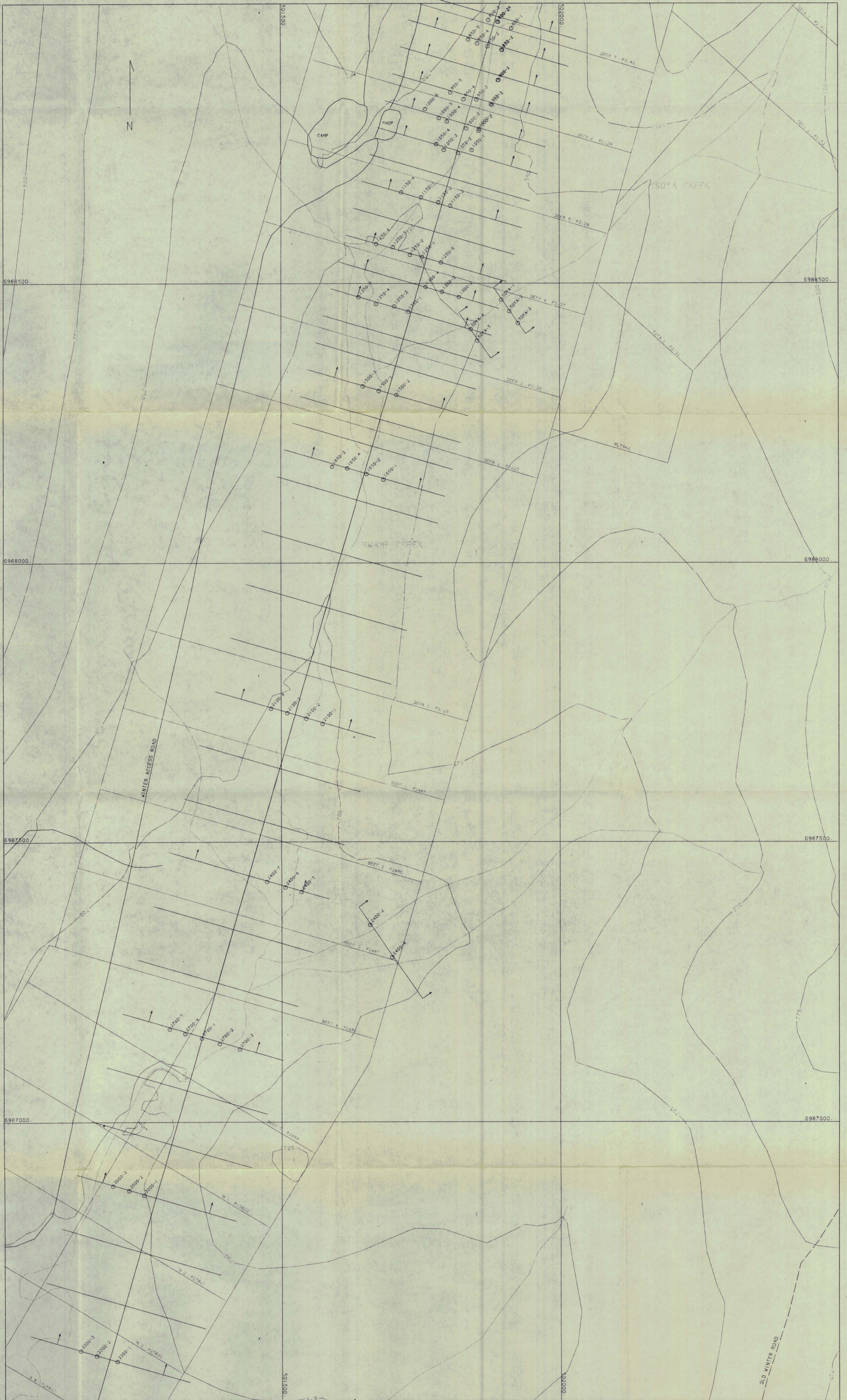
26	28	2	7.9	8.5	0.6	7.0	0							10.0 GRAV
28	30	2	8.5	9.1	0.6	11.5	35.966	3.13	3.60	0.088	1.280	-2.426		54.0 GRAV/GRDI 30-34
														~V CALC/
					NUMBER =	20	20	14	14	14	14	14	20	
		NIL SAMPLES =	3		MEAN =	11.4	8.735	1.05	1.21	0.030	-1.039	-4.744	22.7	
		TR SAMPLES =	3		STD DEV =	4.2	14.6	1.29	1.48	0.036	1.745	1.745	10.6	
					VAR =	17.7	212.5	1.65	2.19	0.001	3.046	3.046	113.2	

FILE:SWGRVRES.WK1

 MOOSEHORN RANGE EXPLORATION PROJECT
 SWAMP CREEK MINE
 PAY GRAVEL RESERVES - 1989 RESULTS

BHID	THICK (m)	GRADE (fgpbcm)	SECT (fgpbcm)	GRAD (bcm)	VOLUME (bcm)	GOLD (g)	DB (bcm)	SR	SECT (fopbcm)	GRAD (bcm)	VOLUME (bcy)	GOLD (oz)	DB (bcy)
800-1	1.8	0.37											
800-2A	3.3	0.07											
800-3	3.6	0	0.10		2848	294	8285	2.9	0.003		3725	9	10836
850-1	1.8	1.84											
850-2	1.2	8.22											
850-3	0.6	0	3.66		6690	24485	5460	0.8	0.090		8750	787	7141
900-1	1.8	14.68											
900-2	1.8	10.38	12.53		8610	107883	9350	1.1	0.308		11261	3468	12229
950-1	2.4	1.55											
950-2	2.4	2.72											
950-4	1.2	0	1.71		7135	12187	9330	1.3	0.042		9332	392	12202
1000-1	4.3	0.15											
1000-2	3.7	1.46											
1000-3	3.7	0.63											
1000-4	2.4	0											
1000-5	1.9	0.19	0.55		14010	7652	16290	1.2	0.013		18323	246	21305
1050-1	3.0	0.87											
1050-2	2.1	1.33											
1050-3	3.0	0.15											
1050-4	2.4	0	0.56		16523	9210	4073	0.2	0.014		21610	296	5327
1150-1	3.7	1.05											
1150-2	2.5	0.65											
1150-4	1.2	0.35	0.80		21840	17502	32330	1.5	0.020		28564	563	42284
1250-2	4.0	0.72											
1250-3	3.1	0.43	0.59		25238	14976	22090	0.9	0.015		33008	481	28891
1350-1	2.4	1.23											
1350-3	4.0	0.29											
1350-4	3.7	0.63	0.64		35800	22838	35238	1.0	0.016		46822	734	46087
1500-1	5.8	0.98											
1500-2	5.5	1.55											
1500-3	3.6	0.08	0.97		78510	76387	96540	1.2	0.024		102681	2456	126262
1650-1	6.1	0.08											
1650-2	6.7	0.21											
1650-3	1.8	0											
1650-4	7.3	0.78	0.35		212040	73478	202530	1.0	0.009		277321	2362	264884
2100-1	2.7	0.60											
2100-2	4.9	0.29											
2100-3	1.2	0											
2100-4	6.7	0.25	0.30		330075	100428	513563	1.6	0.007		431696	3229	671675

AT-18	1.8	1.28	0.93	14010	13002	16290	1.2	0.023	18323	418	21305
1050-1	3.0	0.87									
1050-2	2.1	1.33									
1050-3	3.0	0.15									
1050-4	2.4	0.00									
AT-01	1.8	1.00									
AT-02	1.9	1.90									
AT-03	2.0	2.05									
AT-19	0.3	0.56									
AT-20	2.3	1.84	1.05	16523	17325	4073	0.2	0.026	21610	557	5327
1150-1	3.7	1.05									
1150-2	2.5	0.65									
1150-4	1.2	0.35	0.80	21840	17502	32330	1.5	0.020	28564	563	42284
		TOTAL	2.03	77656	157876	85118	1.1	0.050	101564	5076	111324

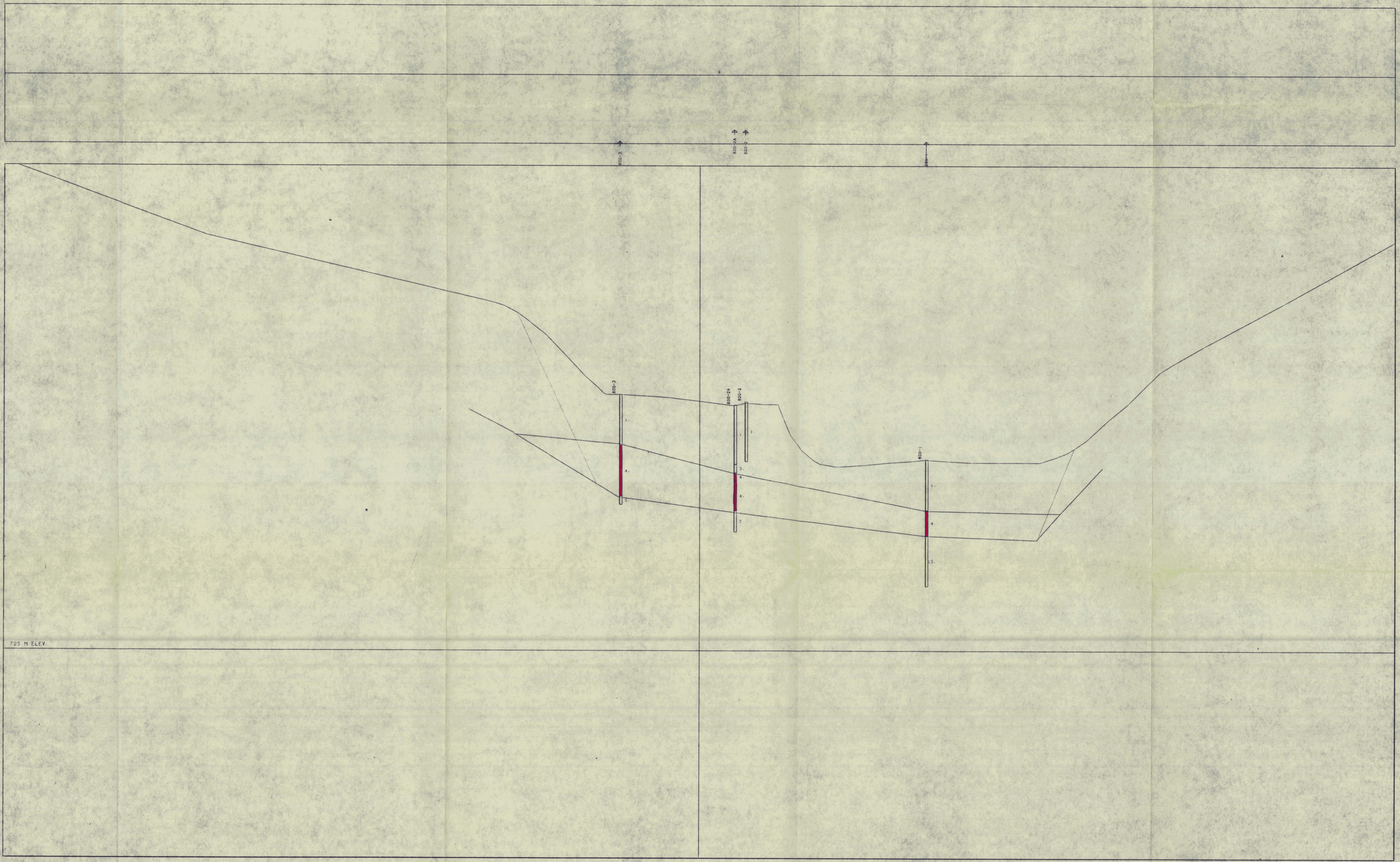


REV.	DATE	MADE BY	DESCRIPTION
1			
2			
3			
4			
5			

MOOSEHORN RANGE PLACER EXPLORATION PROJECT
 SWAMP CREEK DEFINITION DRILLING PROGRAM
 FIGURE 3

NTS 115N-2	
DATE: APR. 1989	
MAP INDEX NUMBER	DRAWING NUMBER
1:2500.	3

M206V1 15-N-2
 120113
 (2)

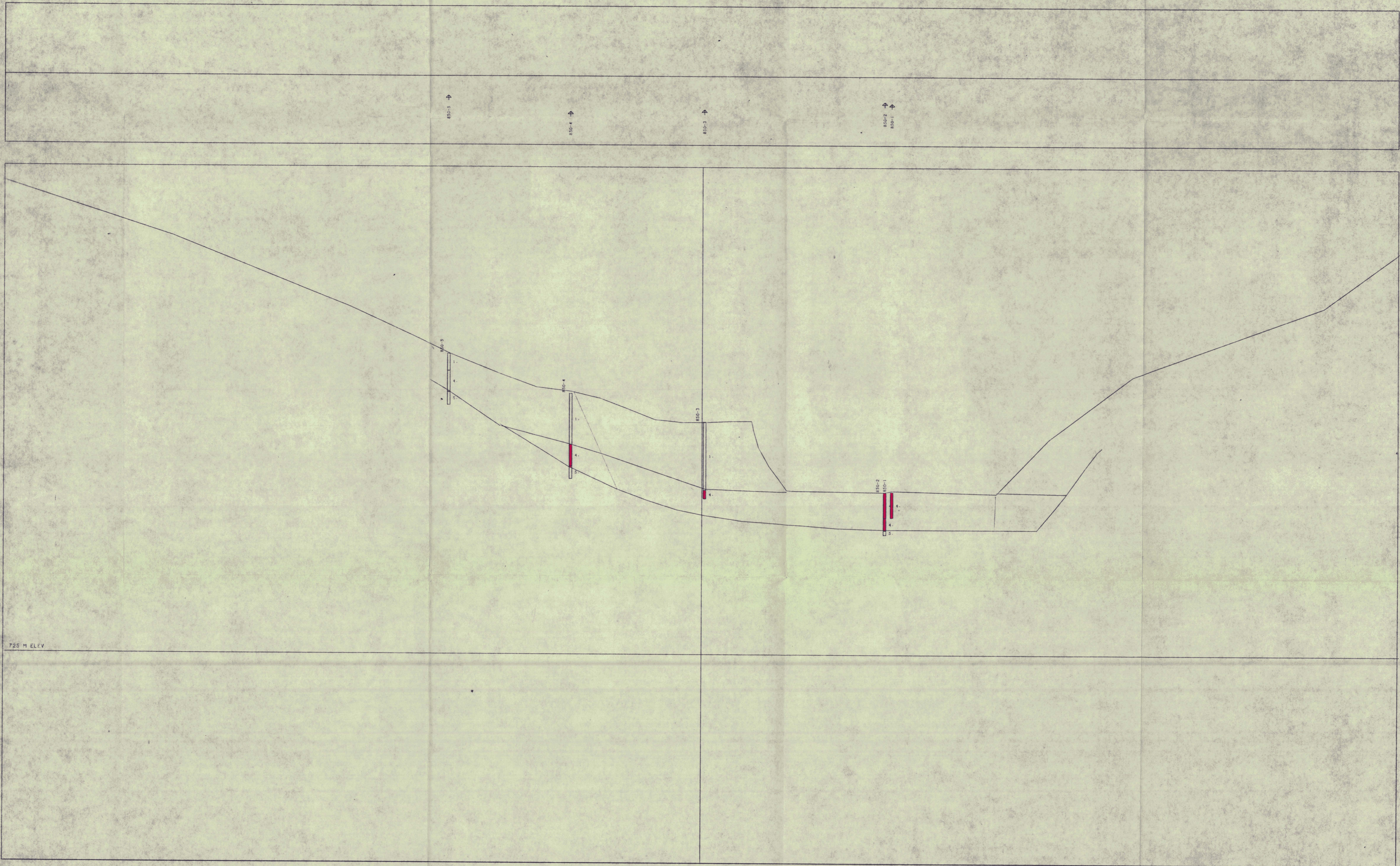


120113

MAP # 115-N-2
④

MAP SCALE		NO. DATE MADE BY DESCRIPTION				MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 800 S		HORZ SCALE = 1:250 VERT SCALE = 1:125																										
		<table border="1"> <tr><td>1</td><td></td><td></td><td></td><td></td></tr> <tr><td>2</td><td></td><td></td><td></td><td></td></tr> <tr><td>3</td><td></td><td></td><td></td><td></td></tr> <tr><td>4</td><td></td><td></td><td></td><td></td></tr> <tr><td>5</td><td></td><td></td><td></td><td></td></tr> </table>				1					2					3					4					5					OFFICE DEPARTMENT		MAP INDEX NUMBER SCALE DRAWING NUMBER	
1																																		
2																																		
3																																		
4																																		
5																																		
		DATE DRAWN BY CHECKED APPROVED						1" = 6.35 4																										
		04-14-89																																

BASILINE

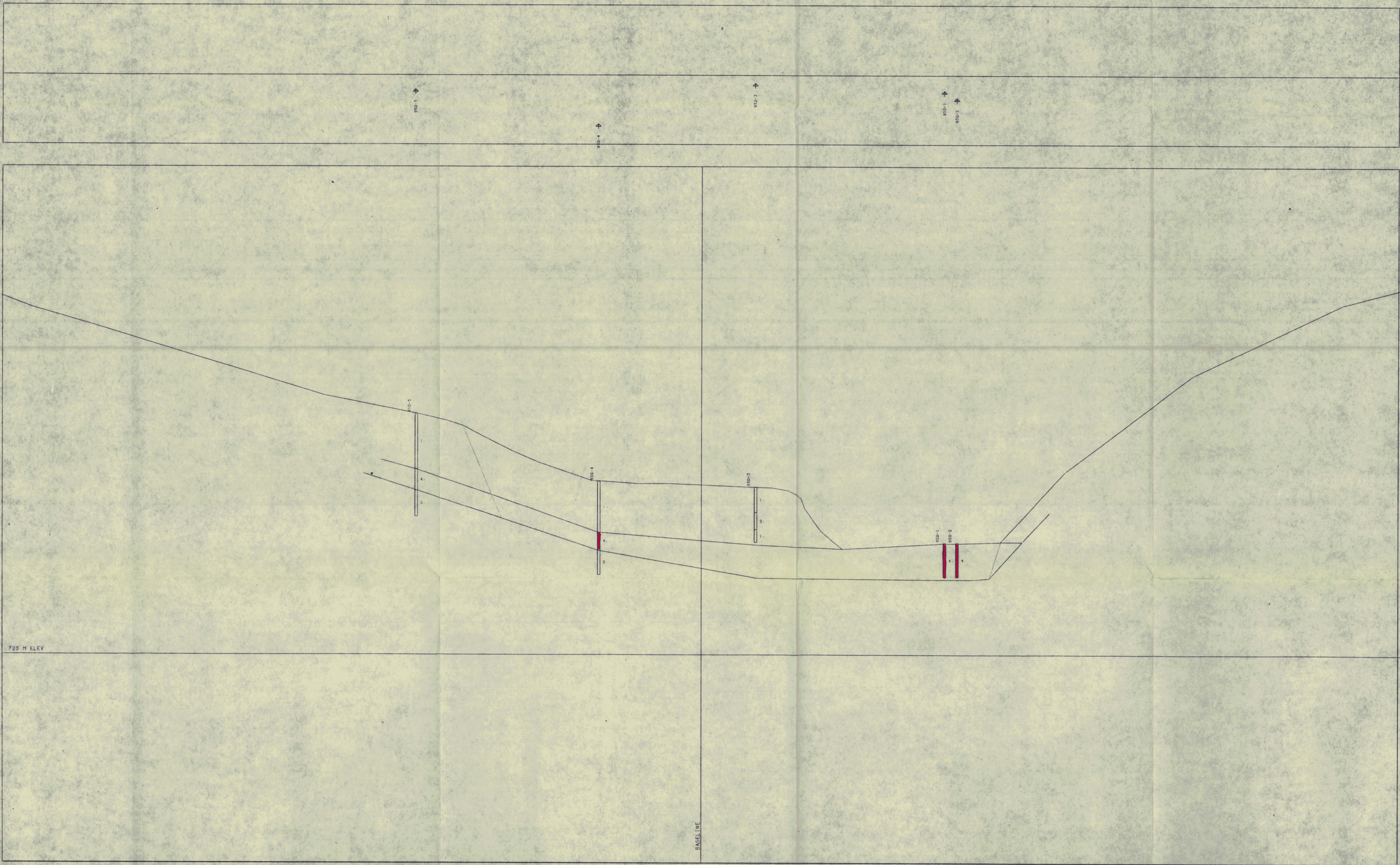


725 M ELEV

120 115
MAP# 115-N-2
5

MAP SCALE		NO DATE MADE BY DESCRIPTION		MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 850 S		HORZ SCALE = 1:250 VERT SCALE = 1:125		
1						MAP INDEX NUMBER	SCALE	DRAWING NUMBER
2							1" = 6.35	5
3								
4								
5								
DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT			
04-14-89								

BASELINE



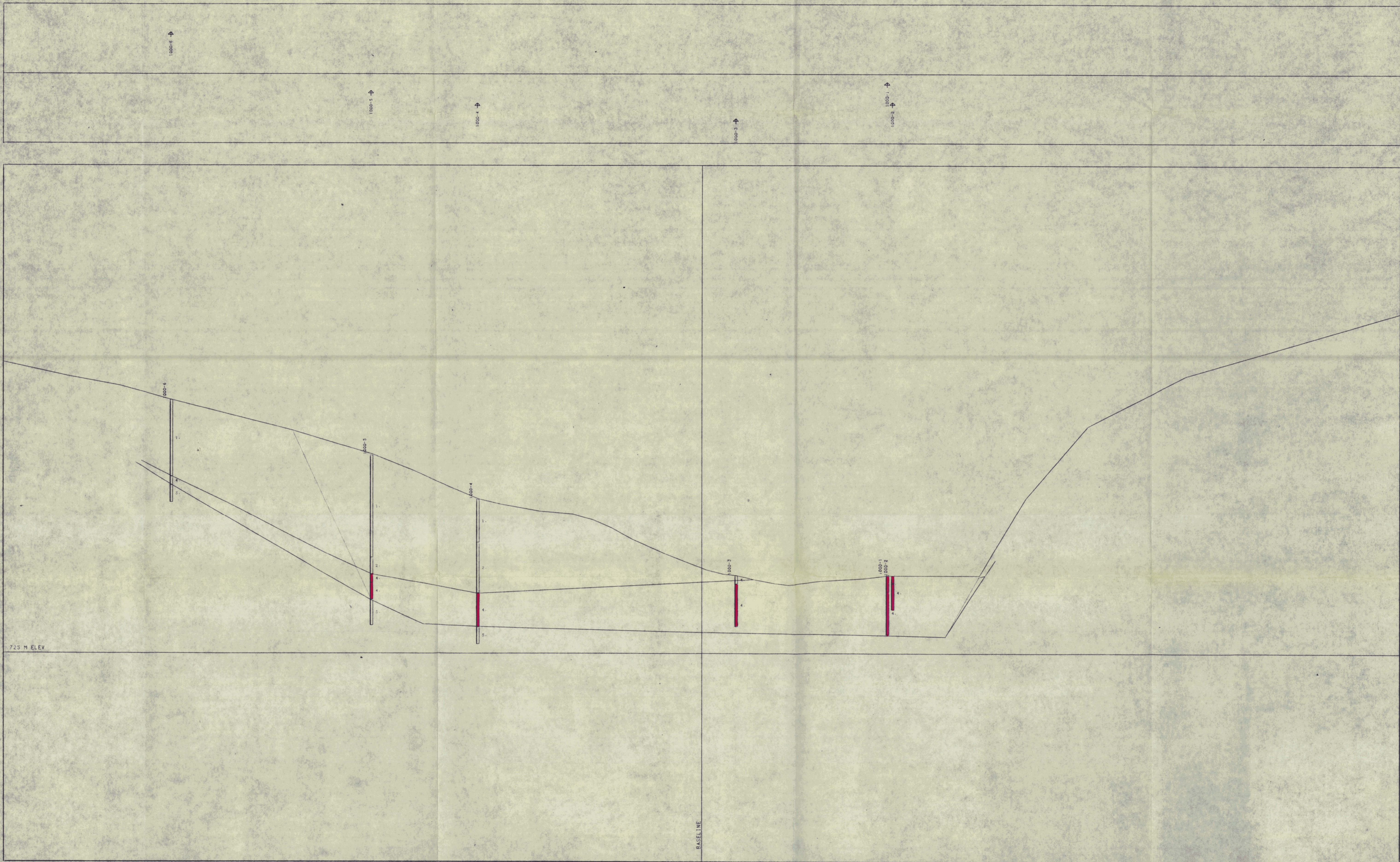
725 M ELEV

BASELINE

120113

MAP# 115-N-2

MAP SCALE		NO.		DATE	MADE BY	DESCRIPTION	MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 950 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
		1							MAP INDEX NUMBER	SCALE
		2							1" = 6.35	DRAWING NUMBER
		3								7
		4								
		5								
DATE	DRAWN BY	CHECKED	APPROVED	OFFICE	DEPARTMENT					
04-14-89										



120113
MAP # 115-10-2

REVISIONS		MAP SCALE		NO DATE MADE BY DESCRIPTION		MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 1000 S		HORZ SCALE = 1:250 VERT SCALE = 1:125		
1								MAP INDEX NUMBER	SCALE	DRAWING NUMBER
2						OFFICE	DEPARTMENT	1" = 6.35		8
3										
4										
5										
				DATE	DRAWN BY	CHECKED	APPROVED			
				04-14-89						

1150-4

1150-1

1150-2

1150-3

1150-4

1150-1

1150-2

1150-3

725 M ELEV

BASELINE

120113

10

MAP# 115-10-2

MAP SCALE

NO	DATE	MADE BY	DESCRIPTION
1			
2			
3			
4			
5			

DATE	DRAWN BY	CHECKED	APPROVED
04-14-89			

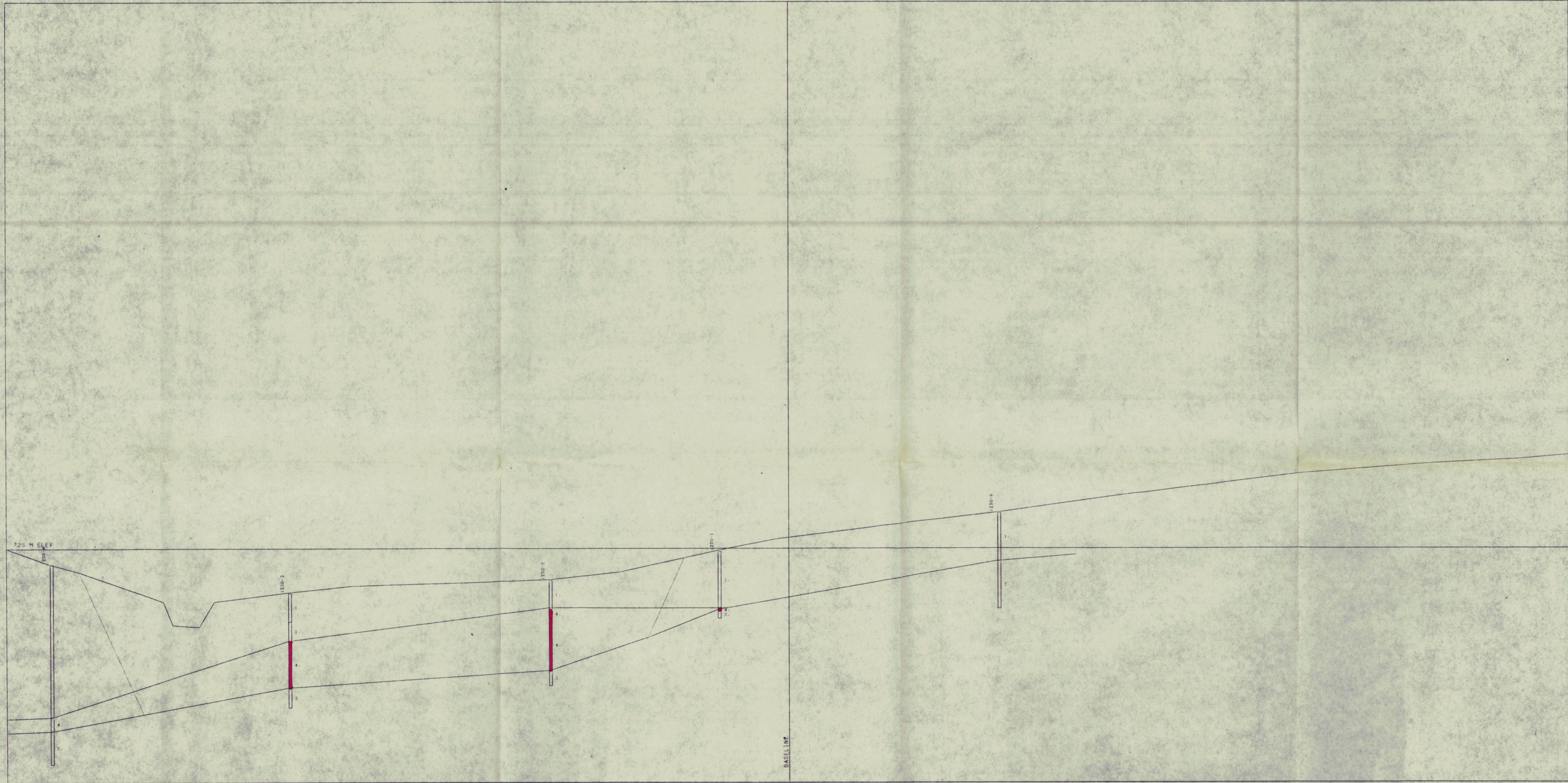
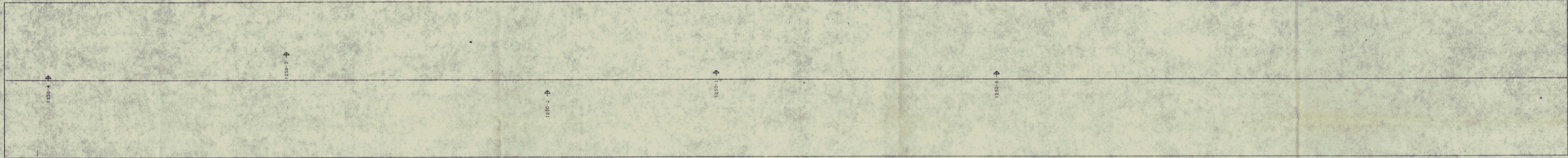
MOOSEHORN RANGE DRILL PROGRAM
1989
SECTION 1150 S

HORZ SCALE = 1:250
 VERT SCALE = 1:125

OFFICE DEPARTMENT

MAP INDEX NUMBER SCALE DRAWING NUMBER

1" = 6.35 10

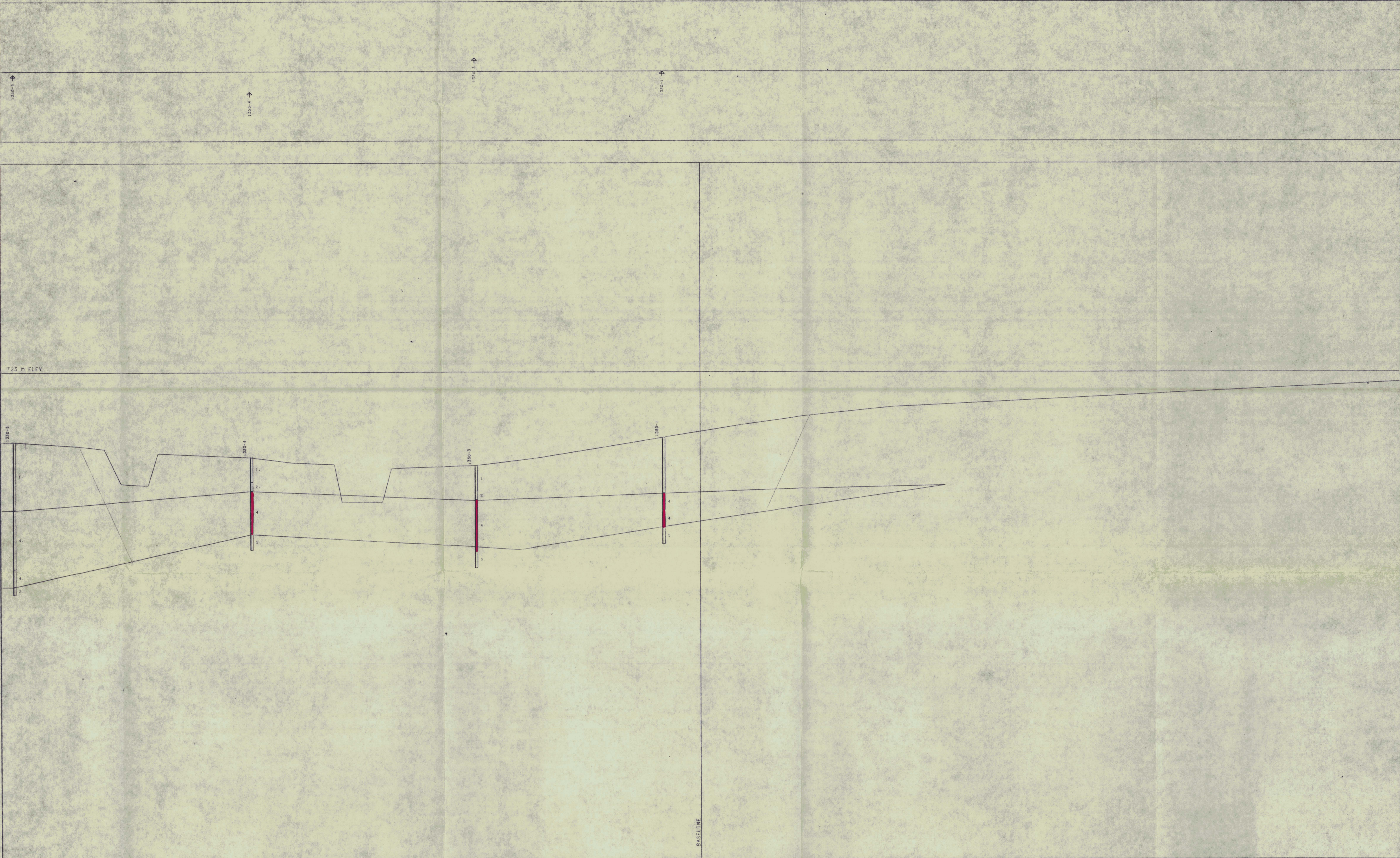


120113

(11)

MPP-N-2

MAP SCALE		NO		DATE	MADE BY	DESCRIPTION	MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 1250 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
		1					OFFICE		DEPARTMENT	MAP INDEX NUMBER
		2								SCALE
		3								1" = 6.35
		4								DRAWING NUMBER
		5								II
		DATE		DRAWN BY	CHECKED	APPROVED				
		04-14-89								

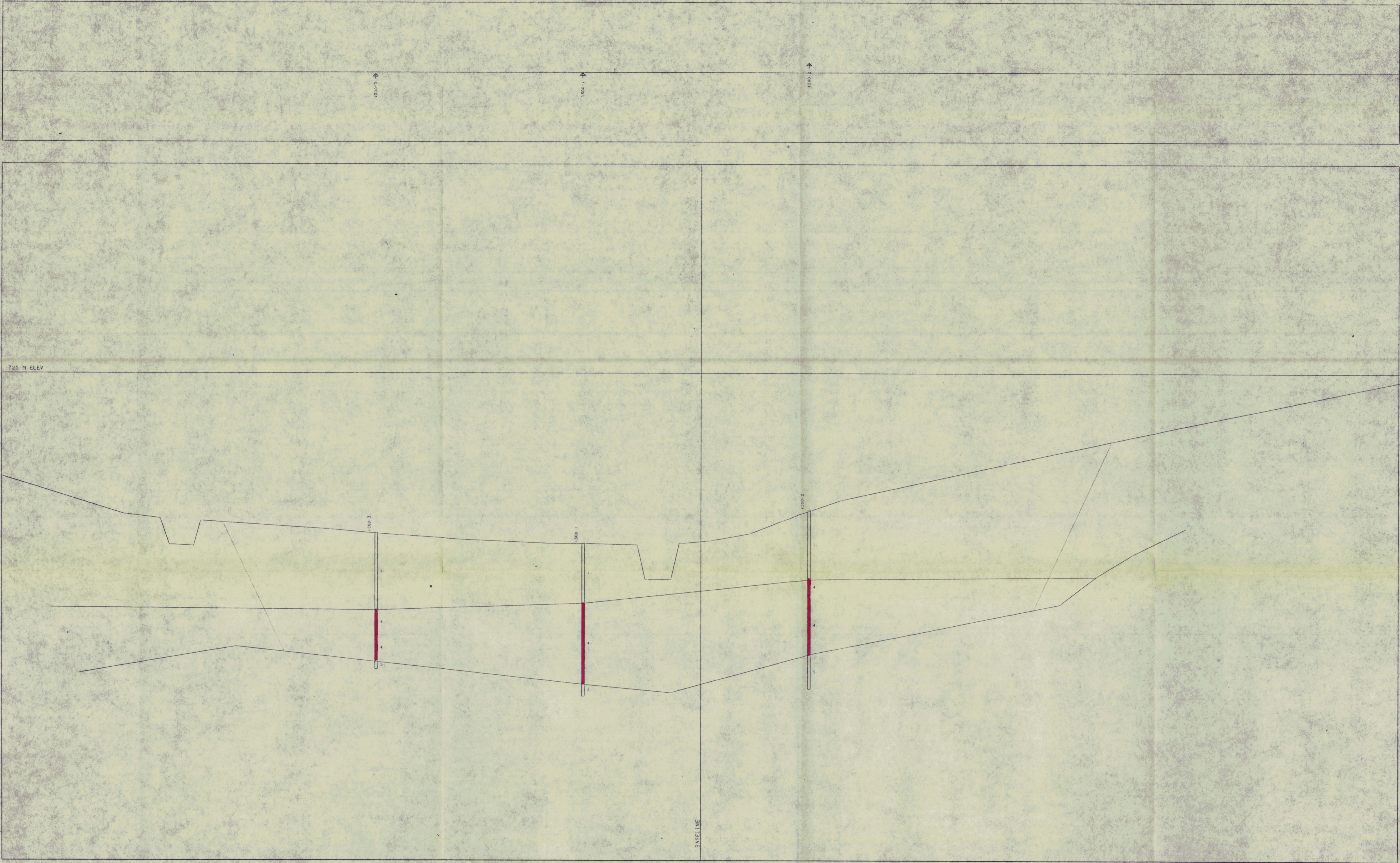


120113

(2)

MAP # 115-N-2

MAP SCALE		NO		DATE		MADE BY		DESCRIPTION		MOOSEHORN RANGE DRILL PROGRAM		HORZ SCALE = 1:250	
		1								1989		VERT SCALE = 1:125	
		2								SECTION 1350 S			
		3											
		4											
		5											
		DATE		DRAWN BY		CHECKED		APPROVED		OFFICE		DRAWING NUMBER	
		04-14-89										12	

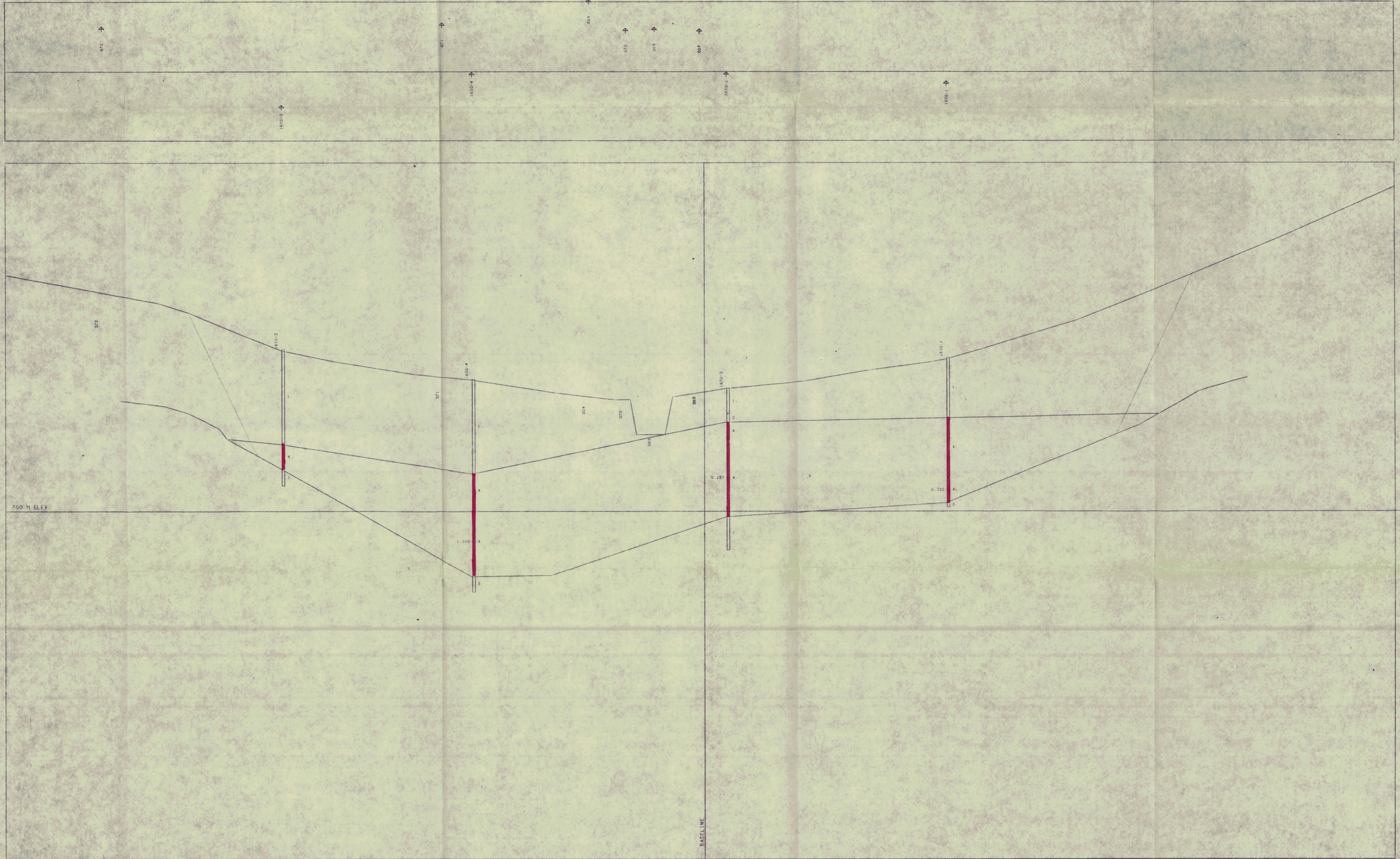


120113

(13)

MAP# 115-N-2

MAP SCALE		NO. DATE MADE BY DESCRIPTION		MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 1500 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
		REVISIONS 1 2 3 4 5				OFFICE DEPARTMENT _____	
		DATE DRAWN BY CHECKED APPROVED					
		04-14-89					

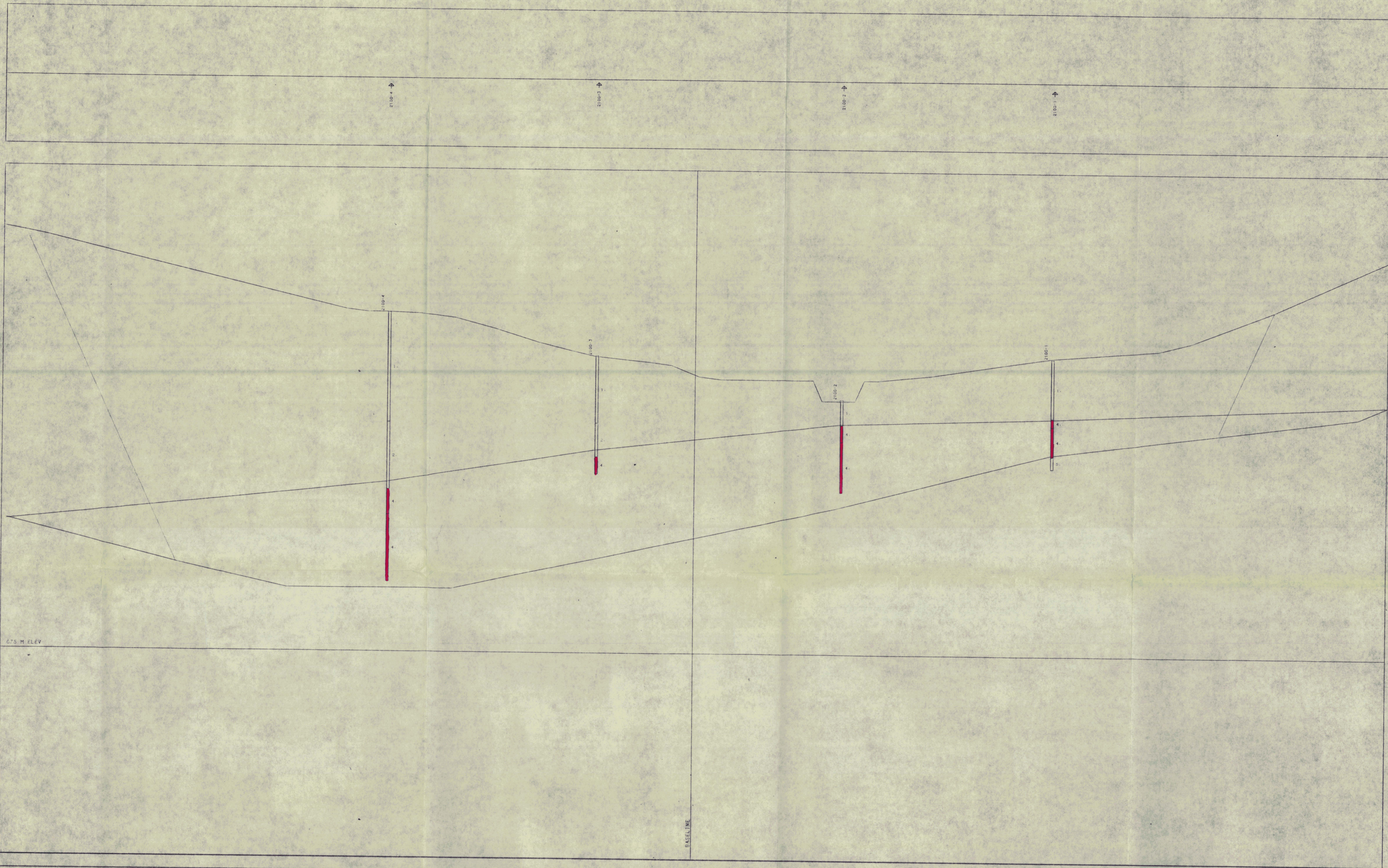


12C113

14

MAP# 15-N-2

REFLECTIONS		MAP SCALE		MOOSEHORN RANGE DRILL PROGRAM				HORZ SCALE = 1:250		
NO	DATE	MADE BY	DESCRIPTION	1989				VERT SCALE = 1:125		
DATE	DRAWN BY	CHECKED	APPROVED	OFFICE		DEPARTMENT		MAP INDEX NUMBER	SCALE	DRAWING NUMBER
04-14-89								1" = 6.35	14	



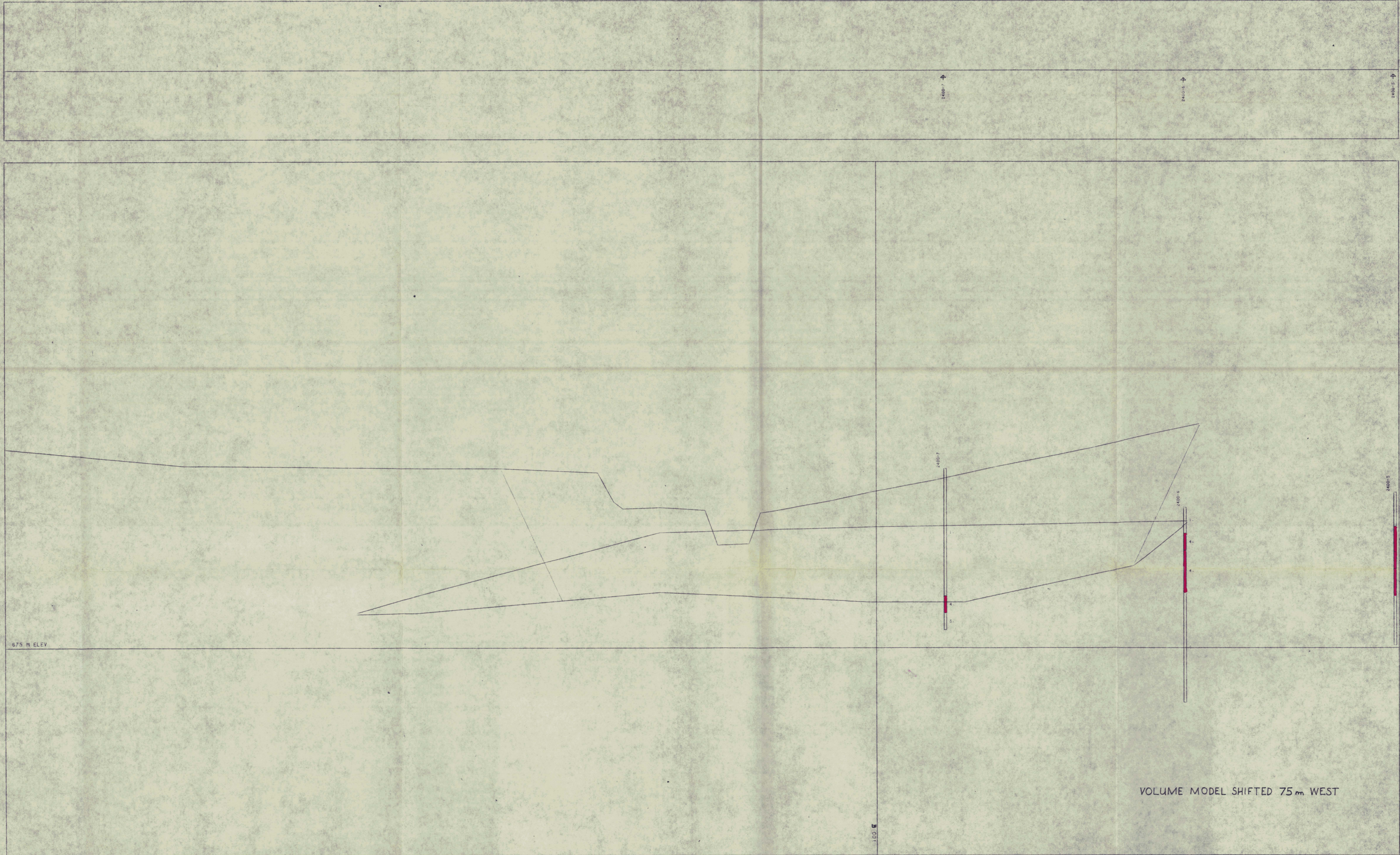
675 M ELEV

120119

(15)

MAP# 115-N-2

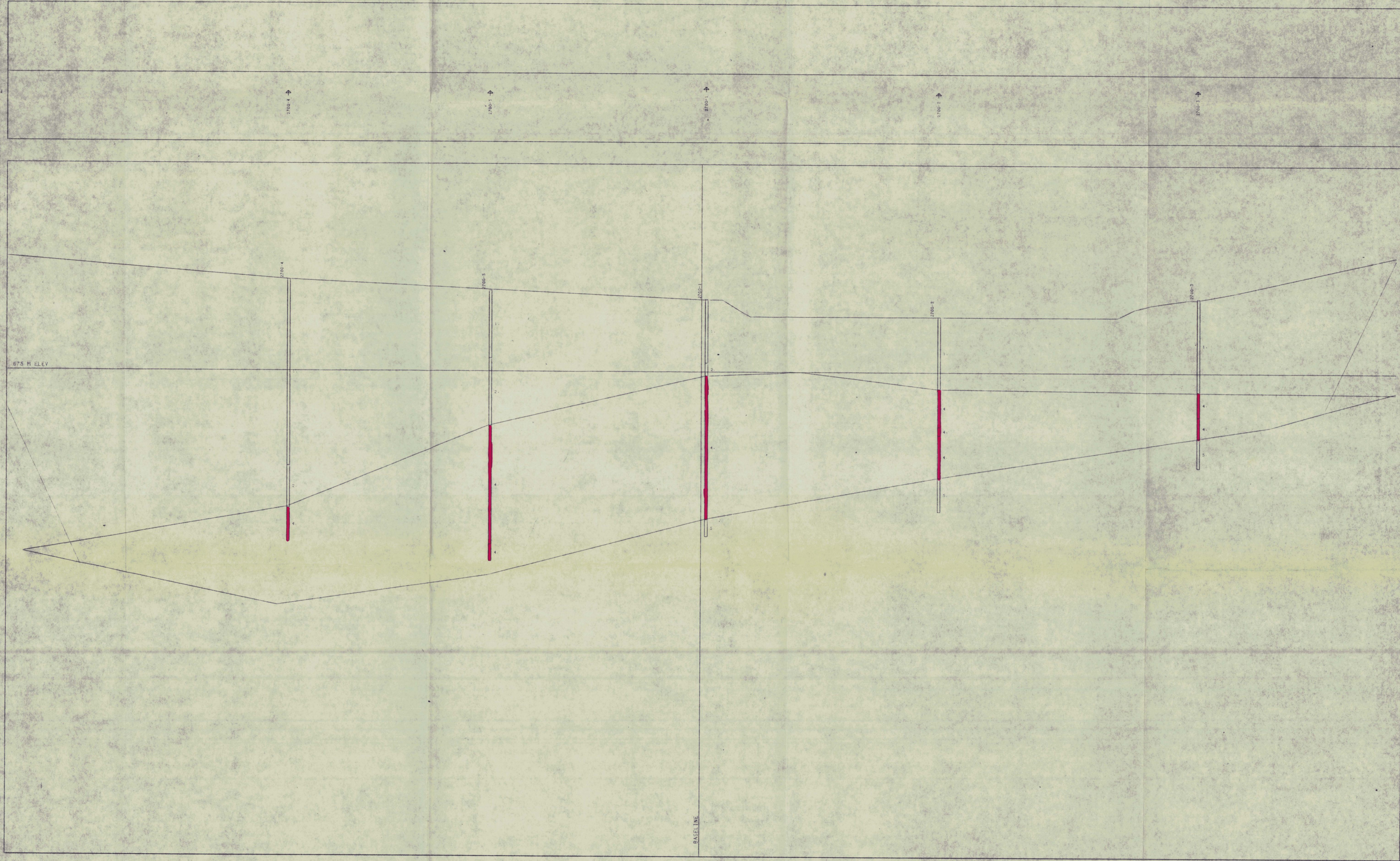
MAP SCALE		<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th style="writing-mode: vertical-rl; transform: rotate(180deg);">REVISED</th> <th>NO</th> <th>DATE</th> <th>MADE BY</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td></tr> </tbody> </table>				REVISED	NO	DATE	MADE BY	DESCRIPTION																										MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 2100 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
REVISED	NO	DATE	MADE BY	DESCRIPTION																																			
		<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>DATE</th> <th>DRAWN BY</th> <th>CHECKED</th> <th>APPROVED</th> </tr> </thead> <tbody> <tr> <td>04-14-89</td> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>		DATE	DRAWN BY	CHECKED	APPROVED	04-14-89				<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>OFFICE</th> <th>DEPARTMENT</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> </tr> </tbody> </table>		OFFICE	DEPARTMENT			<table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>MAP INDEX NUMBER</th> <th>SCALE</th> <th>DRAWING NUMBER</th> </tr> </thead> <tbody> <tr> <td> </td> <td>1" = 6.35</td> <td>15</td> </tr> </tbody> </table>		MAP INDEX NUMBER	SCALE	DRAWING NUMBER		1" = 6.35	15														
DATE	DRAWN BY	CHECKED	APPROVED																																				
04-14-89																																							
OFFICE	DEPARTMENT																																						
MAP INDEX NUMBER	SCALE	DRAWING NUMBER																																					
	1" = 6.35	15																																					



VOLUME MODEL SHIFTED 75m WEST

MAP# 115-N-2
 120113
 (16)

MAP SCALE		NO		DATE	MADE BY	DESCRIPTION	MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 2400 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
		1					OFFICE	DEPARTMENT	MAP INDEX NUMBER	SCALE
		2							1" = 6.35	DRAWING NUMBER
		3								16
		4								
		5								
DATE	DRAWN BY	CHECKED	APPROVED							
04-14-89										

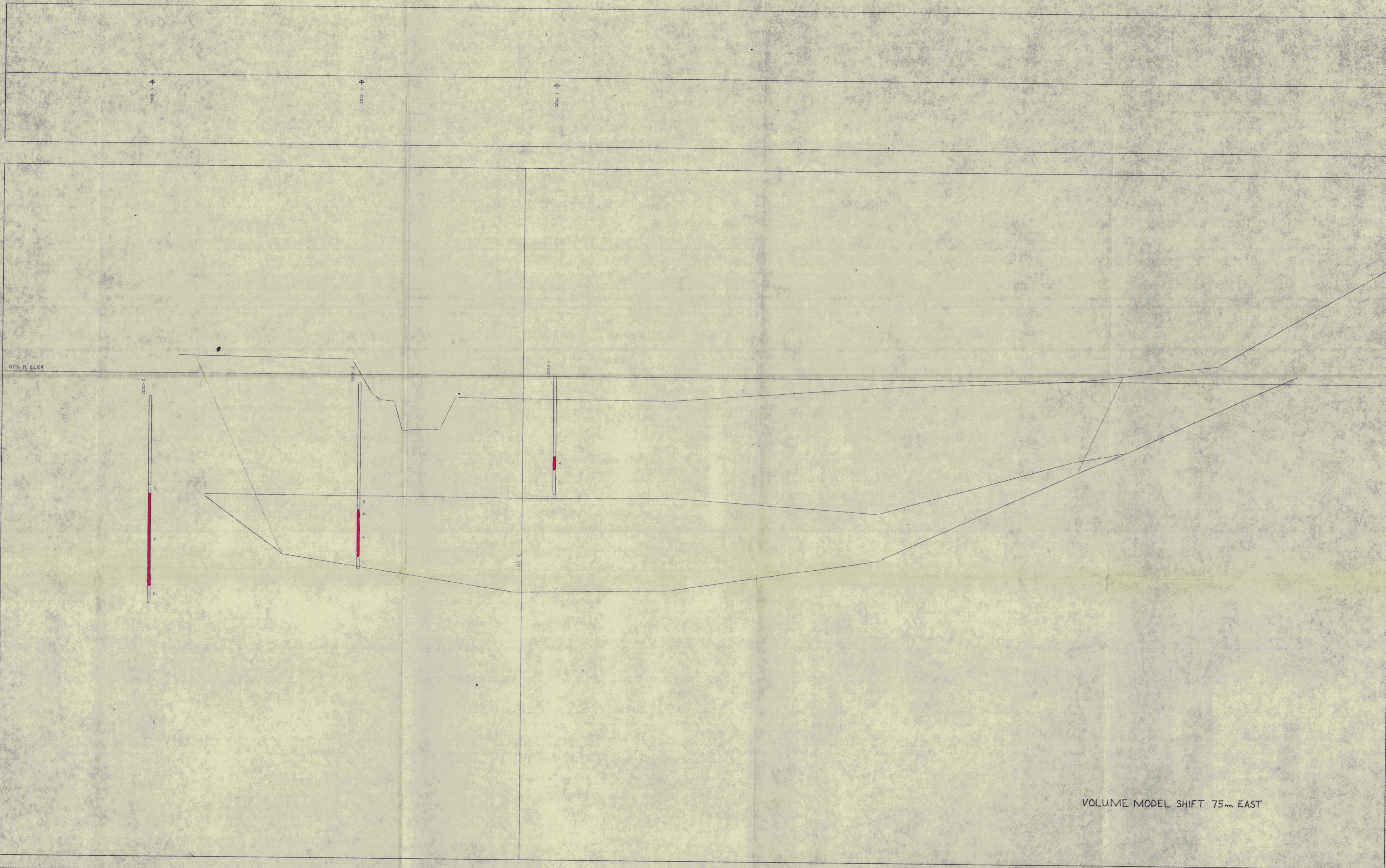


12E113

17

MAP# 115-N-2

MAP SCALE		NO		DATE	MADE BY	DESCRIPTION	MOOSEHORN RANGE DRILL PROGRAM			HORZ SCALE = 1:250		
		1					1989			VERT SCALE = 1:125		
		2					SECTION 2700 S			MAP INDEX NUMBER		
		3								SCALE		
		4								1" = 6.35		
		5								DRAWING NUMBER		
			DATE	DRAWN BY	CHECKED	APPROVED	OFFICE			DEPARTMENT		
			04-14-89							17		

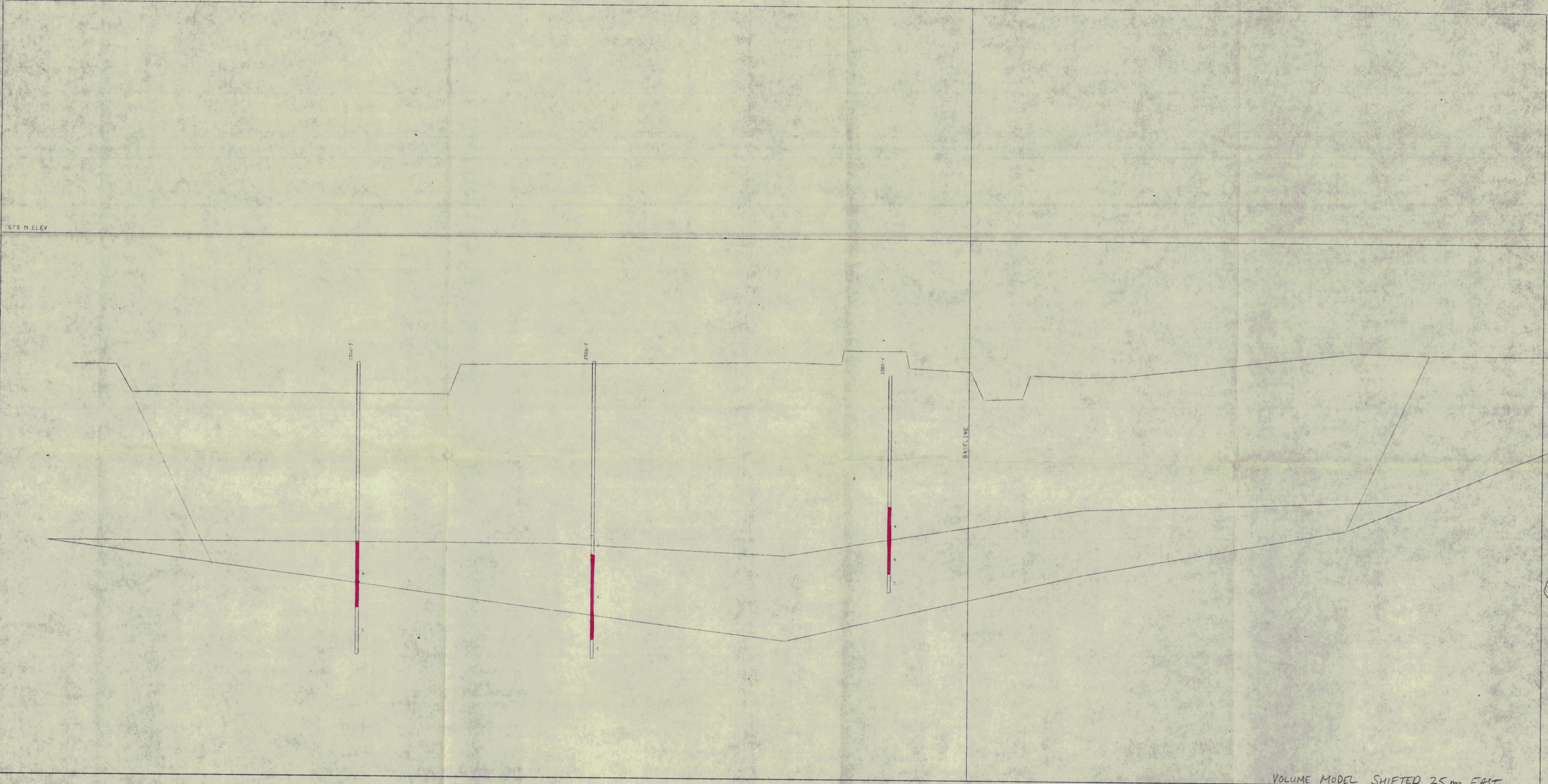
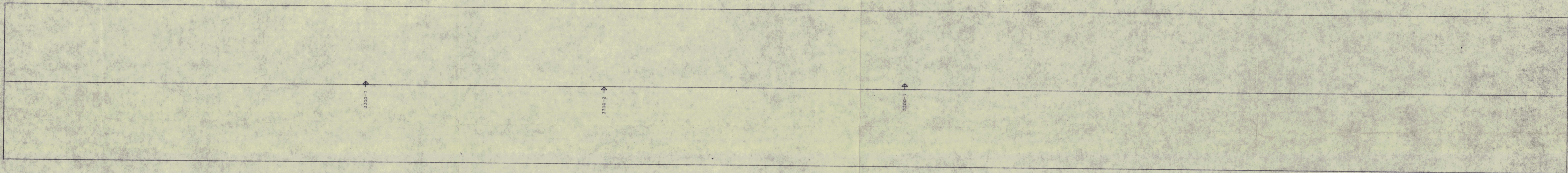


VOLUME MODEL SHIFT 75m. EAST

120113

MAP# 115-N-2 (18)

MAP SCALE		NO.		DATE	MADE BY	DESCRIPTION	MOOSEHORN RANGE DRILL PROGRAM 1989 SECTION 3000 S		HORZ SCALE = 1:250 VERT SCALE = 1:125	
		1					OFFICE		DEPARTMENT	MAP INDEX NUMBER
		2								SCALE
		3								DRAWING NUMBER
		4								1" = 6.35
		5								18
		6								
		7								
		8								
		9								
		10								
		11								
		12								
		13								
		14								
		15								
		16								
		17								
		18								
		19								
		20								
		21								
		22								
		23								
		24								
		25								
		26								
		27								
		28								
		29								
		30								
		31								
		32								
		33								
		34								
		35								
		36								
		37								
		38								
		39								
		40								
		41								
		42								
		43								
		44								
		45								
		46								
		47								
		48								
		49								
		50								
		51								
		52								
		53								
		54								
		55								
		56								
		57								
		58								
		59								
		60								
		61								
		62								
		63								
		64								
		65								
		66								
		67								
		68								
		69								
		70								
		71								
		72								
		73								
		74								
		75								
		76								
		77								
		78								
		79								
		80								
		81								
		82								
		83								
		84								
		85								
		86								
		87								
		88								
		89								
		90								
		91								
		92								
		93								
		94								
		95								
		96								
		97								
		98								
		99								
		100								



12C113

19

MAP# 115-N-2

VOLUME MODEL SHIFTED 25m EAST

MAP SCALE		NO		DATE		MADE BY		DESCRIPTION		MOOSEHORN RANGE DRILL PROGRAM		HORZ SCALE = 1:250	
		1								1989		VERT SCALE = 1:125	
		2								SECTION 3300 S		MAP INDEX NUMBER	
		3										SCALE	
		4										1" = 6.35	
		5										DRAWING NUMBER	
		DATE		DRAWN BY		CHECKED		APPROVED		OFFICE		DEPARTMENT	
		04-14-89										19	

CANADA TUNGSTEN MINING CORPORATION LIMITED
 MOOSEHORN EXPLORATION PROJECT
 SWAMP CREEK
 MAP 1 OF 4

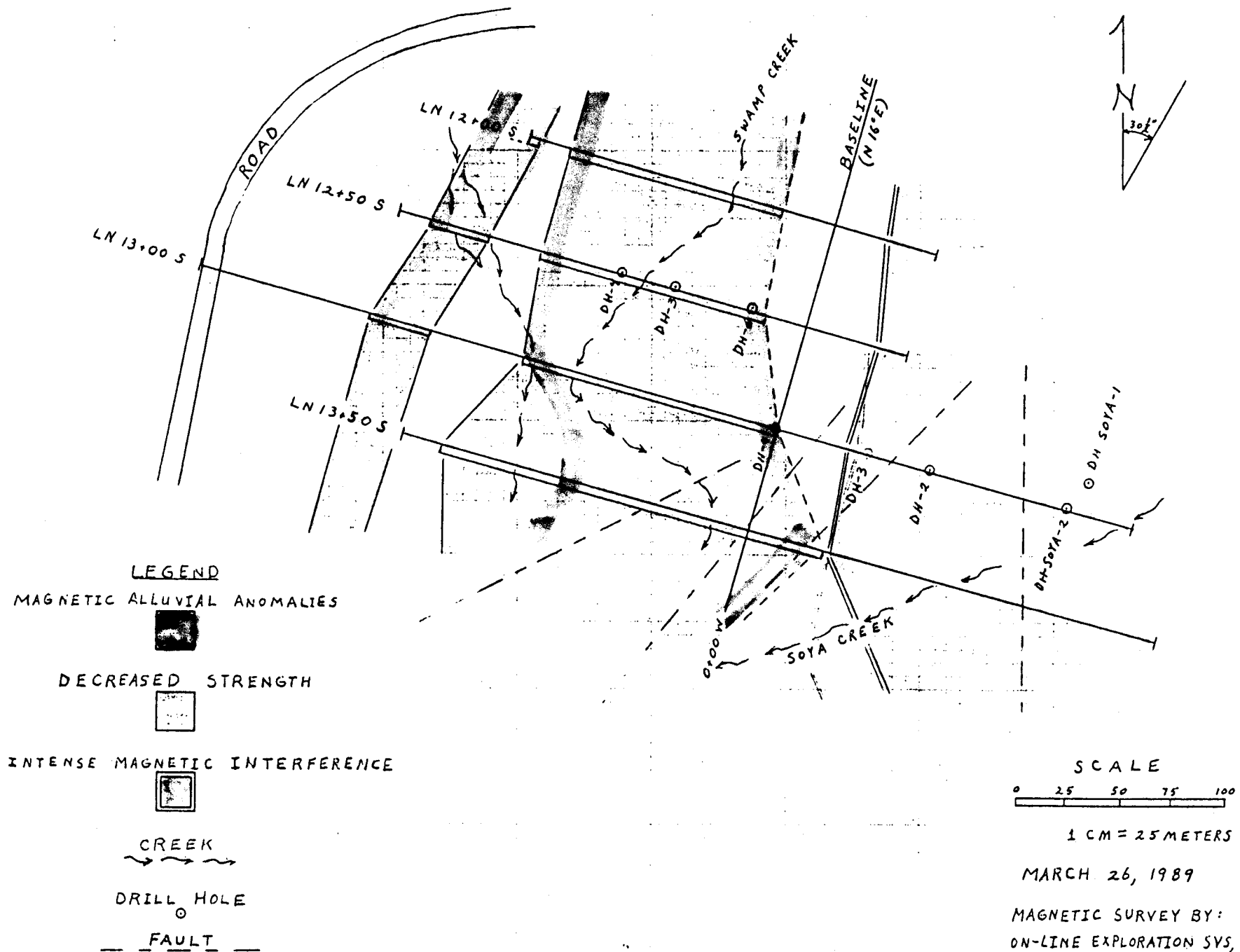


FIGURE 20-A

CANADA TUNGSTEN MINING CORPORATION LIMITED
 MOOSEHORN EXPLORATION PROJECT
 SWAMP CREEK
 MAP 2 OF 4

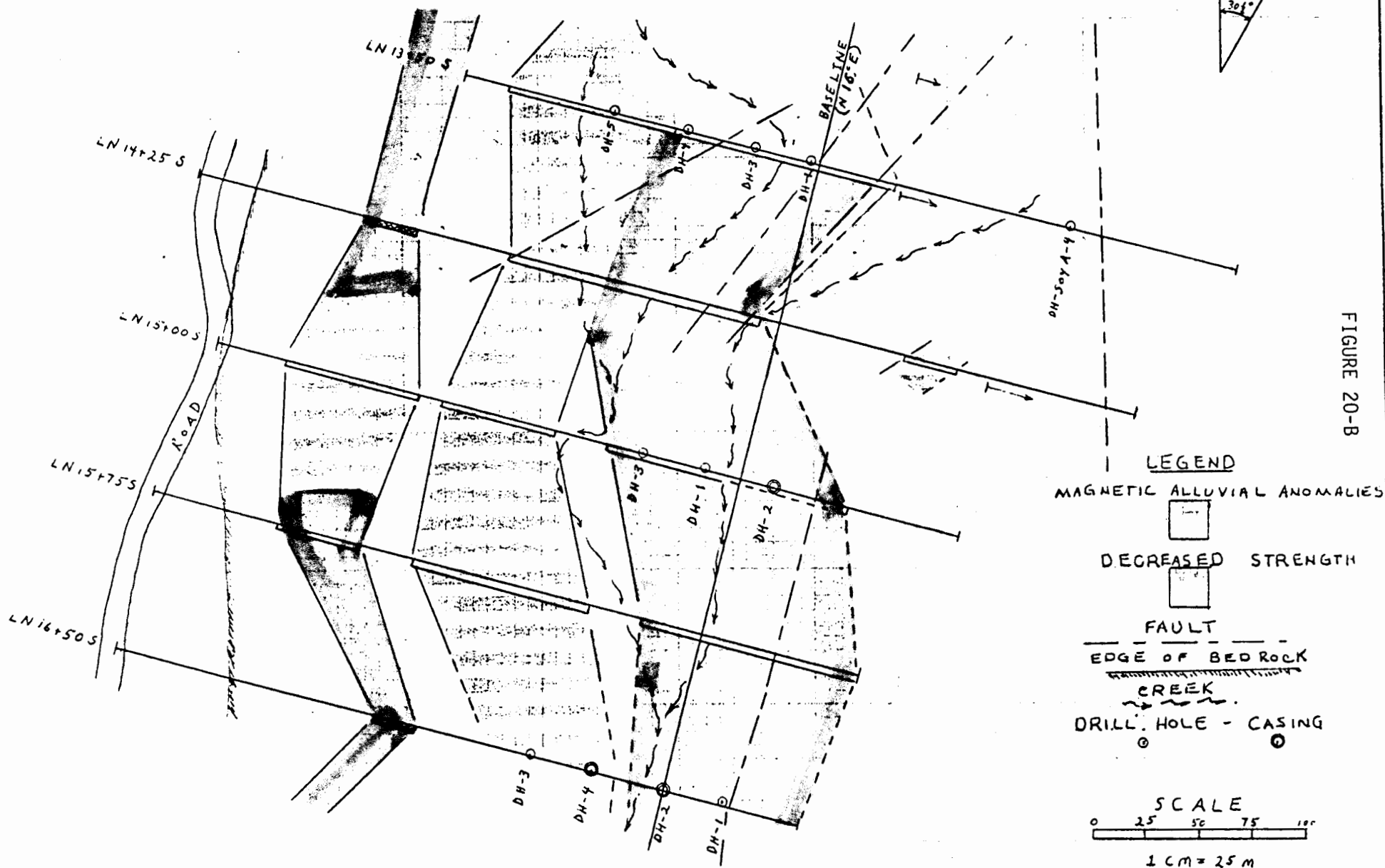
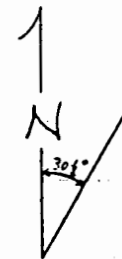







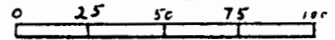


FIGURE 20-B

LEGEND

- MAGNETIC ALLUVIAL ANOMALIES 
- DECREASED STRENGTH 
- FAULT 
- EDGE OF BED ROCK 
- CREEK 
- DRILL HOLE - CASING  

SCALE



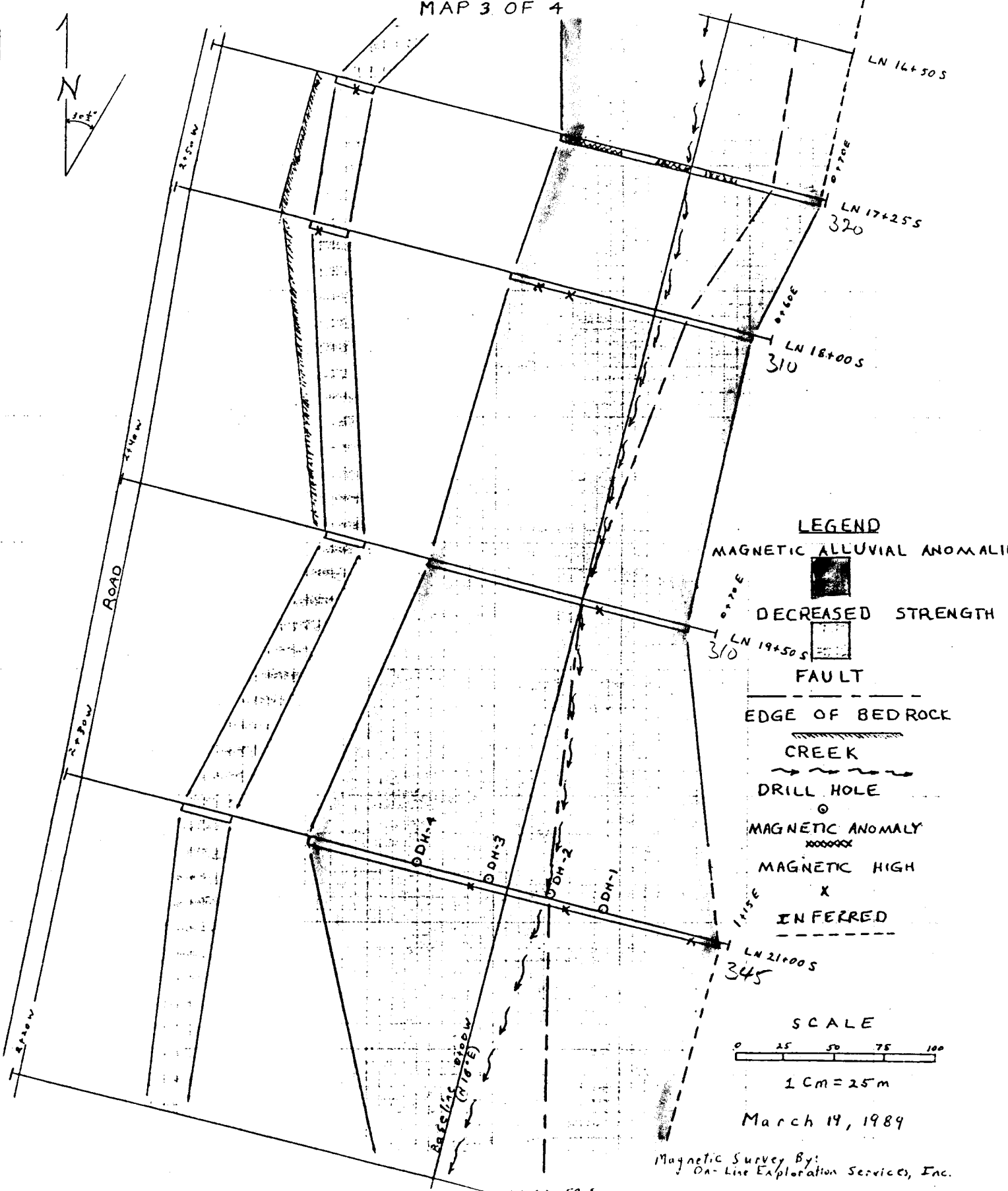
1 CM = 25 M

March 16, 1989

Magnetic Survey By: On-Line Exploration Services, Inc.

FIGURE 20-C

CANADA TUNGSTEN MINING CORPORATION LIMITED
MOOSE HORN EXPLORATION PROJECT
SWAMP CREEK
MAP 3 OF 4



LEGEND

MAGNETIC ALLUVIAL ANOMALIES



DECREASED STRENGTH



FAULT

EDGE OF BED ROCK

CREEK

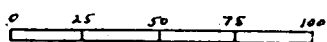
DRILL HOLE

MAGNETIC ANOMALY

MAGNETIC HIGH

INFERRED

SCALE



1 CM = 25 m

March 14, 1989

Magnetic Survey By:
On-Line Exploration Services, Inc.

LN 22+50 S

