COPPER RIDGE EXPLORATIONS INC.

Report on the 2006 Exploration Program on the Toby Zone, Scheelite Dome Project

June 11 to July September 4, 2006

Located in the Highet Creek Area
Mayo Mining District
NTS 115 P/9 and P/16
63° 47'N – 136° 15'W

-prepared by-

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May 24, 2007

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1.0 SUMMARY

The Scheelite Dome property, comprised of 508 contiguous claims, is located 25 kilometres northwest of Mayo in the Mayo Mining District of central Yukon. Copper Ridge owns 100% of the project, subject to an NSR.

The property is underlain by siliciclastic rocks of the Upper Proterozoic to Lower Cambrian Yusezyu Formation which have been intruded by Triassic metadiorite and more importantly, early Late Cretaceous granodiorite, diorite, lamprophyre and monzonite. These latter intrusive units are part of the Tombstone Plutonic Suite (TPS) which forms a narrow belt of east-west trending intrusions stretching 550 kilometres across the north-central Yukon. The TPS intrusions are spatially related to a wide range of base and precious metal occurrences including intrusion-hosted, sheeted gold veins and tungsten skarns at Dublin Gulch, high-grade Pb-Ag veins at Keno Hill and intrusion-hosted Au stringers and disseminations at Brewery Creek.

At Scheelite Dome, Intrusion-Related Gold System (IRGS) mineralization occurs in several different styles that are related to the Cretaceous TPS stocks and smaller intrusions. High-grade sulphide mineralization replaces limy horizons within metasedimentary rocks. Calc-silicate skarns with Au-W±Bi are developed in calcareous horizons adjacent to the Scheelite Dome stock. An extensive zone of discordant structurally-controlled quartz-sulphide veinlets and vein-faults is associated with the 3500 by 1500 metre Au-As-Sb soil anomaly centred over the Harvey-Rudolph Area and was the target of most of the previous drilling on the property. A similar zone of discordant quartz-sulphide veining has received limited drill-testing in the Héon Ridge Zone.

An area called the Toby Zone, located south of most of the previous work at Scheelite Dome, hosts the strongest coincident arsenic and bismuth soil geochemical anomaly discovered to date on the property. Prior to 2006, however, this anomaly had received no follow-up work. The 2006 program of prospecting and geophysical surveying was proposed and executed to further investigate this significant anomaly. Work completed included soil sampling, IP, magnetometer and VLF geophysical surveying and trenching.

Further work is justified on the Toby Zone and on the Scheelite Dome property in general. Specific recommendations for the Toby Zone include further prospecting and trenching followed by a non-contingent program of diamond drilling. Further work on the rest of the property based on the recommendations of Harris (2002) and Doherty (2003) is also justified.

The 2006 soil sampling program at the Toby Zone confirmed, clarified and expanded the of the results of the 1999 survey. Grouping of the anomalous coincident gold, arsenic and bismuth values suggests that there is a possible northeast trending control to the mineralization. The survey also expanded the coincident anomaly centred on Line 6E on the northwest part of the grid.

The 2006 prospecting program at the Toby Zone confirmed that the strong coincident gold arsenic and bismuth soil anomaly at the headwaters of Toby creek is reflecting local areas of gold mineralization in bedrock. This was further confirmed by the trenching program which uncovered several quartz-arsenopyrite veins hosted in strongly altered sediments that contained highly anomalous to economic grade gold mineralization.

The geophysical program identified several anomalous patterns worthy of follow up. The VLF survey demonstrated that an east trending conductive structure is associated with the mineralization. This feature has a strike length of at least a kilometre and could represent a conductive fault or a vein hosting metallic mineralization such as arsenopyrite. The IP survey identified 3 strongly chargeable zones in the centre of the grid. The most southerly of these correlates with disseminated pyrite around auriferous quartz veins. The source for the other two remains undefined as they occur at depth in areas of very little rock exposure. The magnetic survey defined a strongly magnetic body that occurs just to the south of the mineralization identified in the trenching. This feature could represent a buried intrusion at depth that could be the heat and metal source of the mineralization observed at surface.

2.0 INTRODUCTION AND TERMS OF REFERENCE

The Scheelite Dome property is owned 100 % by Copper Ridge Explorations Inc, subject to an NSR as discussed more fully below. During the period June 11 to July September 4, 2006, Copper Ridge conducted programs of detailed prospecting and rock sampling, line cutting, soil sampling, geophysical surveying and trenching on an area called the Toby Zone in the southwest part of the property. The project was designed and overseen by the author, the prospecting, rock sampling and soil sampling was conducted by Aurum Geological Consultants of Whitehorse and the line cutting and geophysical surveying, consisting of IP, magnetometer and VLF surveys, was conducted by Aurora Geosciences of Whitehorse. The trenching program was completed by Wilf's contracting of Mayo

The Scheelite Dome property is located 25 kilometres northwest of Mayo in the central Yukon (Figure 1). The area has seen intermittent exploration since 1916 when the first lode claims were staked. The most recent exploration on the property was conducted by Kennecott Canada Exploration Inc (Kennecott)., La Teko Resources Ltd (La Teko), Copper Ridge Explorations Inc and Yardley Capital Inc. from 1994 to 2003, targeting bulk tonnage gold deposits. Widespread Au-As soil anomalies, and both low and high grade Au mineralization were identified by systematic exploration by these operators.

The purpose of this report is to summarize the work and results completed to date on the property, to detail the results of the 2006 program and to provide recommendations for further work on the property.

3.0 DISCLAIMER

This report is based upon the results of fieldwork directed by the author, on publicly-available assessment reports, and on certain private reports prepared for and provided by Kennecott Canada Exploration Inc and Copper Ridge Explorations Inc. There is no reason to believe that any of this information is incorrect.

The author has relied on information provided by the Yukon Mining Recorder to describe the mineral tenure status of the property and believes, to the best of his knowledge, that this information is correct.

4.0 PROPERTY DESCRIPTION AND LOCATION

The Scheelite Dome property is located 25 kilometres northwest of Mayo in the central Yukon. The property falls within the Mayo Mining District on NTS map sheets 115P/16 and 115P/9 and is centred at 63° 47' north latitude and 136° 15' west longitude. The claims cover Scheelite Dome, a prominent topographic feature, and the upper portions of Highet and Johnson Creeks. The Scheelite Dome property consists of 508 contiguous quartz claims, including 14 fractional claims (Figure 2), covering approximately 10 km^2 (10,000 hectares). The mineral claims are registered in the name of Copper Ridge Explorations Inc. as outlined in Table 3.1.

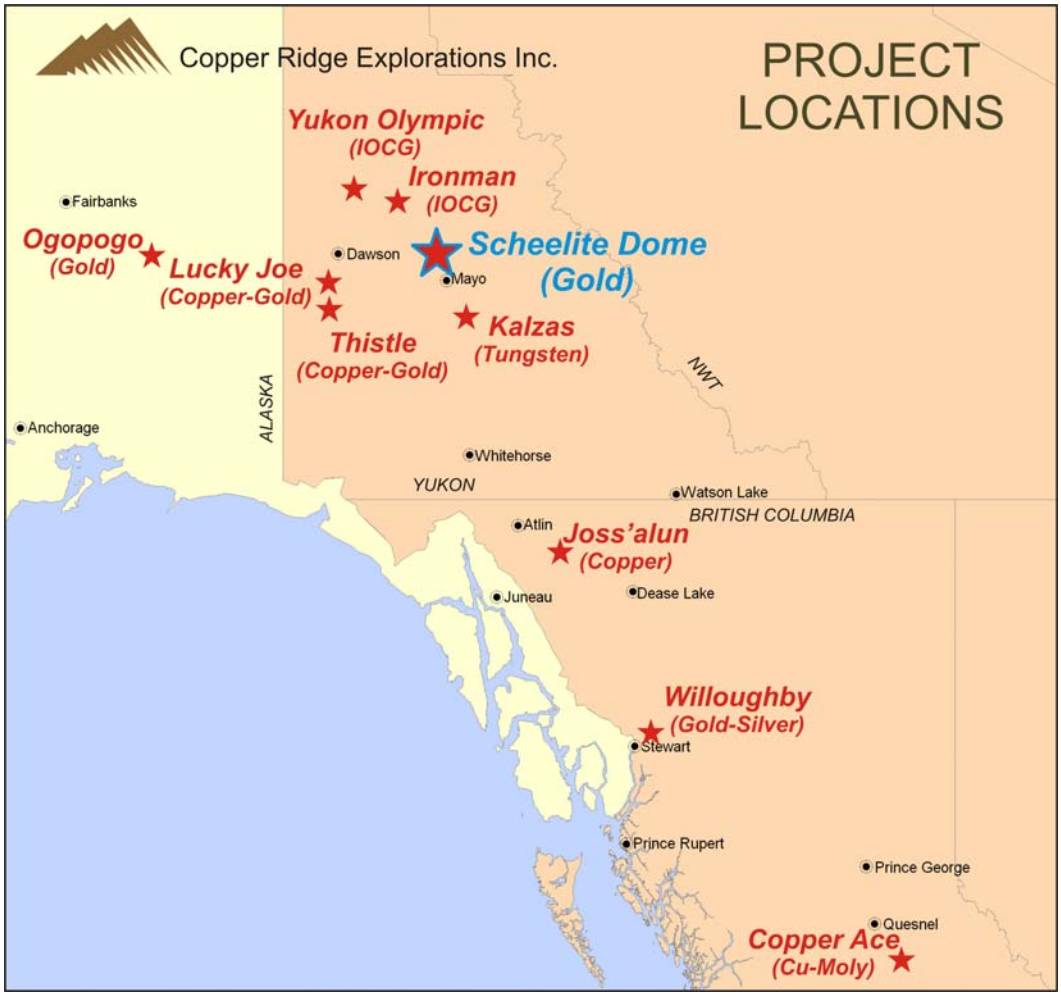
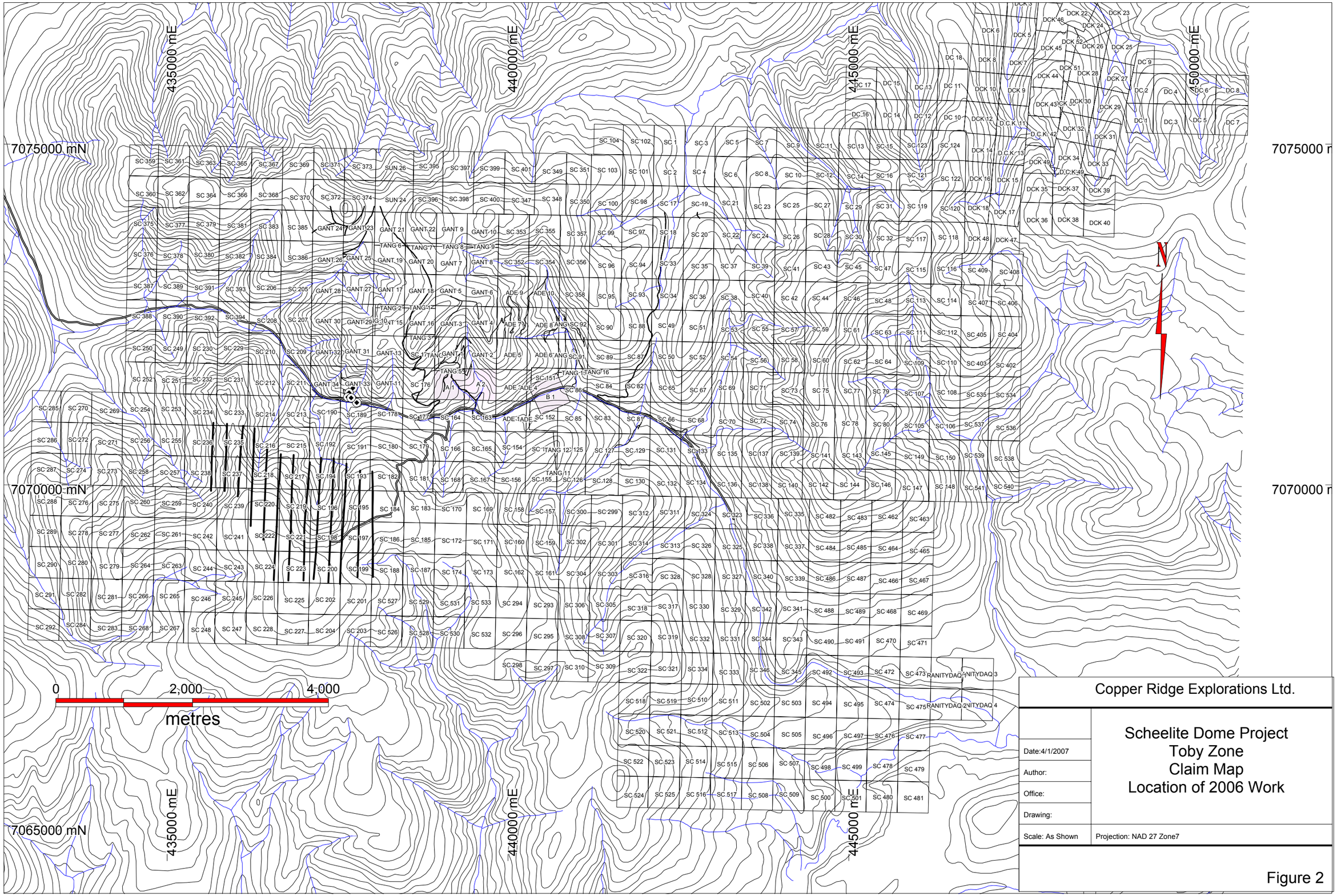


Figure 1 Location Map

The original staker of the Gant and Ade claims, Mr. Rudy Riepe, retains a 2% net smelter return (NSR) which can be purchased for $2,000,000. Kennecott retains a 2% net smelter return royalty on the remainder of the claims, of which 1% may be purchased for US$3,000,000. In addition, upon a decision being made to construct a mine, Kennecott shall receive a cash payment of US$1,000,000 if the decision is within five years of the agreement date (September 12, 2003), the payment increasing by 10% each year thereafter to a maximum of US$3,000,000. The A and B claims are owned by Mr. Ralph Barchen of Mayo, Yukon and are not part of the Scheelite Dome property. Kennecott surveyed most of the Gant and Ade claims plus a number of the SC claims with differentially corrected GPS (+/- 5 m accuracy). The Tang 1-16Fr claims were staked to cover fractions located by this survey.

A Class III Mining Land Use Permit is in effect for the Scheelite Dome property until June 22, 2011. Variances and amendments, however, should be acquired for each addition stage of work proposed, including the work proposed in this report.



Copper Ridge Explorations Ltd.	
	Scheelite Dome Project Toby Zone Claim Map Location of 2006 Work
Date:4/1/2007	
Author:	
Office:	
Drawing:	
Scale: As Shown	Projection: NAD 27 Zone7

Figure 2

TABLE 4.1 - CLAIM DATA*

Claim Name	Grant Number	No. of Claims	Expiry Date	Claim Name	Grant Number	No. of Claims	Expiry Date
SC331-334	YB44575- 578	4	May 19, 2008	Gant 1-11	YA83206-216	11	May 31, 2012
SC335-346	YB64197-208	12	May 31, 2008	Gant 13	YA83217	1	May 31, 2012
SC347-348	YB64209-210	2	May 31, 2012	Gant 15-34	YA83218-237	20	May 31, 2016
SC349-351	YB64211-213	3	May 31, 2008	Ade 1-10	YA83747-756	10	May 31, 2008
SC352-372	YB64214-234	21	May 31, 2012	SC 1-64	YB42504-567	64	May 31, 2012
SC 373-374	YB64392-393	2	May 31, 2012	SC 65-80	YB43132-147	16	May 31, 2016
SC375-394	YB64235-254	20	May31, 2012	SC 81-84	YB43175-178	4	May 31, 2014
SC395	YB64255	1	May 31,2008	SC 85 -87	YB43319-321	3	May 31, 2016
SC396	YB64256	1	May 31, 2012	SC 88	YB43322	1	May 31, 2012
SC397	YB64257	1	May 31, 2008	SC 89-92	YB43323-326	4	May 31, 2016
SC398	YB64258	1	May 31, 2012	SC 93-94	YB43327-328	2	May 31, 2012
SC399	YB64259	1	May 31, 2008	SC 95	YB43329	1	May 31, 2016
SC400	YB64260	1	May 31, 2012	SC 96 - 124	YB43330-358	29	May 31, 2012
SC401-409	YB64261-269	9	May 31,2008	SC 125 -138	YB43359-372	14	May 31, 2016
SC 496	YB64707	1	May 31, 2011	SC 139 - 150	YB43373-384	12	May 31, 2012
SC498-517	YB64709-728	20	May 31, 2011	SC 151	YB43769	1	May 31, 2012
SC518-533	YB64729-744	16	May 31, 2015	SC 152-188	YB43730-766	37	May 31, 2016
SC 534	YC01099	1	June 12, 2008	SC 189-204	YB43770-785	16	May 31, 2016
SC 535	YC01096	1	June 12, 2008	SC 205-208	YB43786-789	4	May 31, 2013
SC 536	YC01097	1	June 12, 2008	SC 209-210	YB43767-768	2	May 31, 2016
SC 537	YC01098	1	June 12, 2008	SC 211-292	YB43790- 871	82	May 31, 2013
Tang 1-6Fr	YB80826-831	6	May 31, 2012	SC 293-326	YB44537-570	34	May19, 2012
Tang 7-9Fr	YB80832-834	3	June 9, 2012	SC 327	YB44571	1	May 19,2008
Tang 10Fr	YB80835	1	May 31, 2012	SC 328	YB44572	1	May 19, 2012
Tang 11-12Fr	YB80836-837	2	June 9, 2012	SC 329	YB44573	1	May 19, 2008
Tang 13-14Fr	YC01093-094	2	June 12, 2011	SC 330	YB44574	1	May 19, 2012
Tang 15Fr	YC01092	1	June 12, 2011				
Tang 16Fr	YC01095	1	June 12, 2011	Total		508	

*Dependent on the acceptance of the assessment credits for the work detailed in this report

5.0 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

Access to the property from Mayo is via the Silver Trail, leading to Elsa and Keno City, and the Minto Lake road, from which the Highet Creek road branches off at 11 kilometres. The Highet Creek road leads to the Morrison Creek and Scheelite Dome roads. Only the Silver Trail is maintained during the winter months. Alternate access to the property is by helicopter based in Mayo. The 1994 through 1999 exploration programs were based out of a camp established on the property. The 2007 program was supported from the Silver Trail Inn located on the Silver Trail highway.

The area was subjected to Pleistocene glaciation with the exception of ridge and hill tops. Hillsides are covered by talus and scree. Valleys are generally floored with glacial debris and glacio-fluvial outwash. Patches of permafrost can be found throughout the property, especially on north-facing slopes. Rock outcrops are rare, and largely restricted to ridges, cliffs and creek bottoms. Soils consist of talus fines and glacio-fluvial deposits.

Scheelite Dome, at an elevation of 1597 metres, is a prominent hill within the Stewart Plateau. Steep hills with local cliffs and felsenmeer-covered ridges are cut by a dendritic drainage system. Elevations on the property range from approximately 850 to 1600 metres. Vegetation in the valley bottoms consists of alder, birch, balsam fir and white and black spruce. Ground cover in areas of thin tree cover consists of alpine plants, 'buck brush' (alder), dwarf willow and moss. The tree-line is at about 1525 metres.

The climate is characterized by low precipitation and a wide temperature range. Winters are cold, and temperatures of -30° C to -40° C are common. Summers are moderately cool to hot, with daily highs of 15° C to 30° C. Scheelite Dome, being a prominent peak, attracts frequent rain shower activity during the summer months. The property is generally snow-free from early June to mid September.

6.0 HISTORY

The earliest activity in the area consisted of small scale placer mining following the discovery of placer gold in 1884 on Johnson Creek and later in 1903, by John Hiatt, in Highet Creek. Highet Creek has produced the largest amount of placer gold in the Mayo area and remains active the present. The first recorded lode exploration on the property dates back to 1916 when J.A. Anderson and R. McNeil discovered and located claims over the Hawthorne vein. In 1933, local prospectors and placer miners J. Hawthorne and R. Rasmussen re-staked and hand trenched the Hawthorne Vein. These claims were optioned to United Keno Hill Mining Limited in 1948 who constructed roads and bulldozer trenched. The results of their program are not publicly available. A.H. Moisey purchased the claims from J. Hawthorne in 1965 and conducted bulldozer trenching. J. Hawthorne re-staked the claims when they lapsed and carried out additional trenching in 1969 and 1970. In the 1920’s and 1930’s hand trenching by the Cantin family over the current B claim (not part of the Scheelite Dome property) exposed weak skarn mineralization with disseminated mineralization in siliceous horizons (Hulstein and Zuran, 1997).

TABLE 6.1 - LODE MINERAL EXPLORATION HISTORY

Year	Company	Program	Sample Type	# of Samples	Analyzed For	Analytical Technique
1916	J.A. Anderson R. McNeil	Staked Hawthorne Vein				
1920's, 1930's	Cantin Family	Hand Trenching				
1933	J. Hawthorne R. Rasmussen	Hand Trenching Hawthorne Vein				
1943	T. McKay	Hand Trenching Cominco Zone				
1948	United Keno Hill Mining Limited	Road construction, Bulldozer Trenching				
1965	A.H. Moisey	Bulldozer Trenching				
1969	G. Elvins	Mapping	Soil			
1969-70	J. Hawthorne	Trenching				
1970(?)	International Minerals and Chemical Corp.	Bulldozer Trenching	Soil			
1979	Cominco Ltd.	Mapping, Bulldozer Trenching	Soil	144	Cu, Pb, Zn, Ag Sn, Au Mo W	Cu, Pb, Zn, Ag: HNO_3±A.R./A.A. Sn: XRF, Au: A.R./A.A. Mo: HNO_3 / colourimetric W: dithiol colourimetric
		3 ddh's: 271.9 metres	Silt	26	Cu, Pb, Zn, Ag Sn, Au Mo W	Cu, Pb, Zn, Ag: HNO_3±A.R./A.A. Sn: XRF, Au: A.R./A.A. Mo: HNO_3 / colourimetric W: dithiol colourimetric
			Heavy Mineral Concentrate	27	Cu, Pb, Zn, Ag Sn, Au Mo W	Cu, Pb, Zn, Ag: HNO_3±A.R./A.A. Sn: XRF, Au: A.R./A.A. Mo: HNO_3 / colourimetric W: dithiol colourimetric
1991	H6000 Holdings Ltd.	Trenching, Road Construction	Grid Soil	734	Au, As	n/a

TABLE 6.1 - LODE MINERAL EXPLORATION HISTORY (cont'd)

1994-96	Kennecott Canada Exploration Inc.	Prospecting, Mapping, Road Construction	Traverse, Grid Soil	1994-96 Total: 4075	Au + 32 elements	-150# split, Au: FA/AA (30g) 32-element A.R./I.C.P.
			Stream Sediment	1994-96 Total: 232	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
			Rock	1994-96 Total: 3302	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
			Heavy Mineral Concentrate	n/a	Au +33 elements	Instrumental Neutron Activation
1995	Kennecott	Prospecting, Mapping, Traverse, Grid Soil; Stream Sediment 19 Trenches: 1.23 km	Rock, Core		Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
		8 NQ ddh's: 1035.0 m				
1995-96	Kennecott	Helicopter-borne EM, VLF, Mag		1275 km		
1996	Kennecott		Grid Soil		Au + 32 elements	-150# split, Au: FA/AA (30g) 32-element A.R./I.C.P.
1997	Kennecott	Mapping, GPS surveying	Soil	158	Au + 32 elements	-150# split, Au: FA/AA (30g) 32-element A.R./I.C.P.
		13 RC Holes: 1052.3 m	RC chip	765	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
		8 Trenches: 1757 m	Rock	760	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
1998	La Teko Resources Ltd.		Grid Soil	107	Au + 32 elements	-80# split, Au: FA/AA (10g) 32-element A.R./I.C.P.
			Rock	11	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
		7 ddh's: 1268.0 m	Core	934	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
	IP Resistivity	IP Resistivity		12.4 km		
1999	Copper Ridge Explorations Inc.		Grid Soil	690	Au + 34 elements	-150# split, Au: FA/AA (30g) 34-element A.R./I.C.P.
			Rock	60	Au + 34 elements	Au: FA/AA (30g) 34-element A.R./I.C.P.
		Ground Magnetometer		54.55 km		
		13 ddh's: 1357.5 m	Core	994	Au + 32 elements	Au: FA/AA (30g) 32-element A.R./I.C.P.
2003	Yardley Capital Inc	7.8 km of IP and Magnetometry				
		310 m Diamond Drilling in 5 holes	Core	253	Au + 36 elements	ICP/MS and Fire Assay

With the onset of the Second World War, the Geological Survey of Canada, led by R. Thompson, focused on the source of placer scheelite, as tungsten was a strategic metal for the war effort. In 1942, Thompson located a source of scheelite on the north side of Scheelite Dome. This occurrence was staked by J.F. Winter and then sold to T. McKay who hand-trenched the showing in 1943. The occurrence was re-staked as the Ursus claims in 1961 by the Dualco Syndicate, consisting of Highland Bell Area Mines Limited, Dome Mines, Ventures Limited and Lake Expanse, and re-staked again by G. Elvins as the Dark claims. In 1969 soil sampling and mapping over the Dark claims returned weakly anomalous tungsten values. International Minerals and Chemical Corp. conducted additional soil sampling and bulldozer trenching after optioning the claims from G. Elvins. The occurrence was re-staked in 1977 by R. Grant, and re-staked again in 1978 by G. Dickson who subsequently optioned the claims to Cominco Ltd. (Hulstein and Zuran, 1997).

Cominco Ltd. conducted soil sampling, geological mapping, bulldozer trenching and diamond drilling in 1979. Three holes totalling 271.9 metres tested a calc-silicate skarn zone in the meta-sediments west of the Scheelite Dome intrusion. Their best drill results included 0.95 g/t Au over 7.9 metres. All samples were analysed at Cominco's Exploration Research Laboratory in Vancouver, B.C. Cominco Ltd. staked the Ben claims in 1980 to follow up anomalous heavy mineral concentrate samples from Bennett Creek (Hulstein and Zuran, 1997).

R. Riepe staked the Gant and Pearl claims in 1986 and the Ade claims in 1987. Following the discovery of the Fort Knox deposit in east-central Alaska, H6000 Holdings Ltd. staked a large group of claims over the Minto Lake and Scheelite Dome intrusions and optioned the Gant and Ade claims in 1991. Their endeavours, including soil sampling, trenching and road building, failed to locate significant intrusion-hosted gold mineralization at Scheelite Dome. After the H6000 claim holdings lapsed, Kennecott Canada Exploration Inc. staked the SC claims from west of Scheelite Dome, east to beyond Bennett Creek and optioned Mr. Reipe's Gant and Ade claims in 1994 and 1995. Extensive work by Kennecott during the period 1994 to 1997 included soil geochemistry, geophysics and reverse circulation and diamond drilling. This work demonstrated that a significant amount of gold mineralization was hosted in the metamorphic sediments surrounding the Scheelite Dome stock.

La Teko acquired the property from Kennecott in 1998 and carried out further programs of geochemistry, geophysics and drilling. Copper Ridge acquired the property in 1999 and carried out additional drilling. Copper Ridge briefly optioned the property to Golden Patriot resources in 2003, who carried out a program of geophysics and diamond drilling on the Tom zone. Despite significant drill results including 1.7 m of 24.4 g/t Au, Golden Patriot terminated the option in 2004. No further work was done on the property until 2006.

The previous work on Scheelite Dome is summarized in Table 6.1 and documented in reports by Hulstein,1996 and 1997, Caulfield 1999, Harris 2000 and 2002 and Doherty 2003.

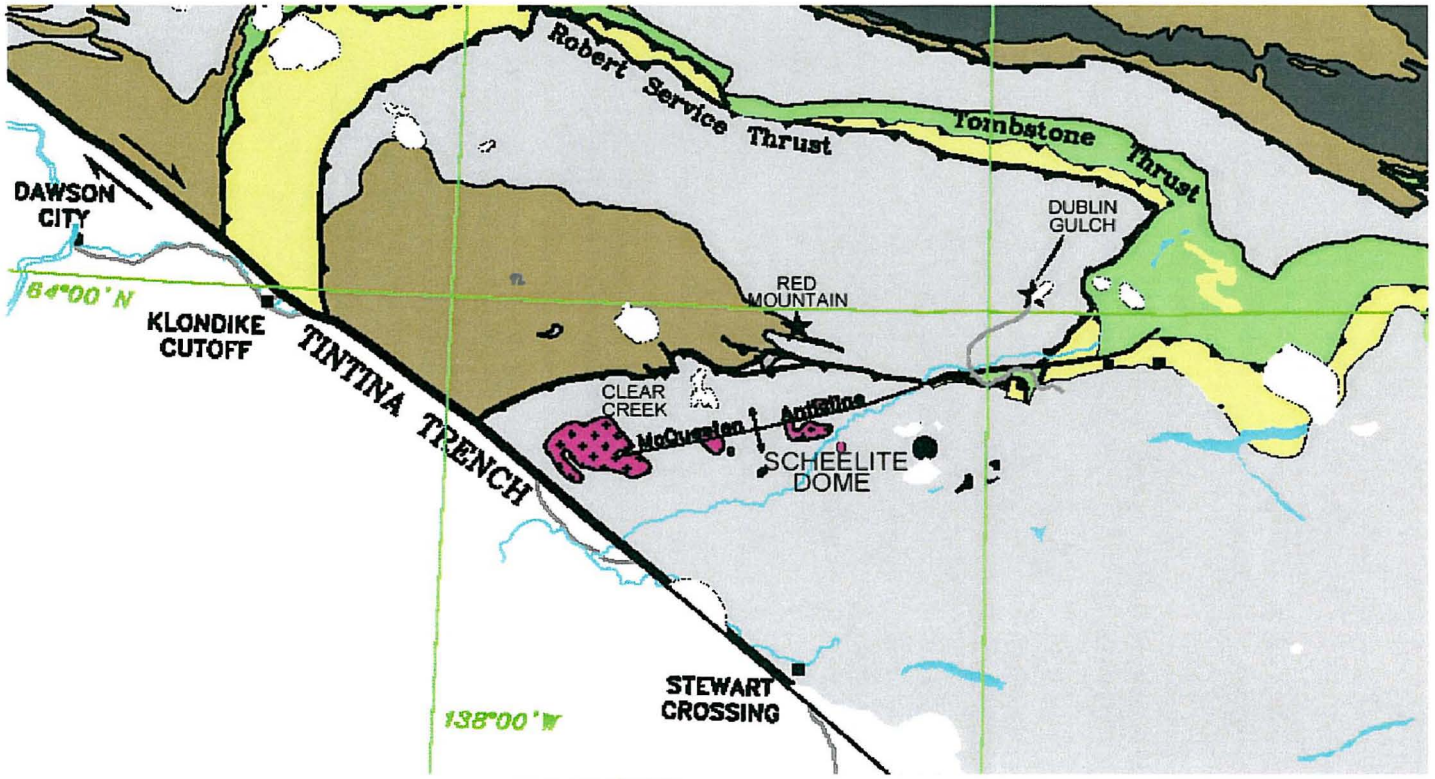
7.0 GEOLOGICAL SETTING

7.1 Regional Geology

Rocks of the Scheelite Dome area are part of western Selwyn Basin, the site of Late Proterozoic and Middle Palaeozoic basinal clastic sedimentation. The Selwyn Basin was bounded during this time by the Mackenzie-Ogilvie Platform to the north and the Cassiar Platform to the south and west. The regional geology has been recently mapped at 1:50,000 scale by Murphy (1997).

In the Mayo area, Selwyn Basin rocks are imbricated by the Jura-Cretaceous Dawson, Tombstone, and Robert Service thrusts (Murphy and Héon, 1995). The Robert Service thrust typically juxtaposes Upper Proterozoic Hyland Group rocks, including those of the Scheelite Dome area, against Mississippian shelf sedimentary units including the 'Keno Hill Quartzite' (Figure 3). The underlying Tombstone thrust sheet of Selwyn Basin rocks are juxtaposed against an immediate footwall of Devonian (?) to Late Jurassic clastics of the Earn Group (?). An intense strain zone affects much of the Tombstone thrust sheet and extends upward well into the Robert Service thrust sheet. Hyland Group rocks are underlain in the west by Ordovician to Silurian Road River Group basinal sediments.

The above rocks and thrust sheets are intruded by the Tombstone Plutonic Suite (TPS) a suite of 92.5-90.5 Ma intermediate to felsic intrusions. Compositionally the TPS range from clinopyroxenite, gabbro, and rare tinguaite to granite (Mortenson et al., 1997). Most intrusions are granodiorite, quartz monzonite, monzogranite, monzonite, quartz syenite or syenite. The smaller bodies, such as the Scheelite Dome and Minto Lake intrusions, typically consist of more felsic to intermediate compositions and are metaluminous (Murphy, 1997). Porphyritic, aplitic and lamprophyre dikes cut both intrusions and the host rocks.



LATE CRETACEOUS
- MCQUESTEN PLUTONIC SUITE (64-67 Ma)
- RHYOLITE (91.7 Ma)
- TOMBSTONE PLUTONIC SUITE (90-95 Ma)

PROTEROZOIC TO PALEOZOIC PERICRATONIC SEDIMENTS
- MISSISSIPPIAN
- DEVONIAN TO MISSISSIPPIAN
- ORDOVICIAN TO DEVONIAN
- LATE PROTEROZOIC TO EARLY PALEOZOIC
- MIDDLE PROTEROZOIC

- GOLD PROSPECTS
- THRUST FAULT
- FAULT
- ROAD

0 50
kilometres

YARDLEY CAPITAL INC.

SCHEELITE DOME GOLD PROJECT

REGIONAL GEOLOGY

	Date: June 2008	Scale: 1:1,250,000	Figure: 3
	KVK Jury: UTMBNAD27	Yardley Project: Mayo	
	Area: 115P/8,16	Study Area: Yukon	

The TPS forms a narrow (50 km wide), east-west trending belt, 550 kilometres long, across north-central Yukon from Dawson City to the Yukon-Northwest Territories border (Mortenson et al., 1997). The TPS is truncated in the west by the Tintina Fault Zone, a Cretaceous-Tertiary dextral strike slip fault with an estimated 450 kilometres of displacement. Restoration of this displacement aligns a similar suite of intrusions, including the Fort Knox intrusion (host to the Fort Knox deposit) in the Fairbanks area, on the west side of the fault zone.

The TPS intrusions are spatially associated with a wide range of base and precious metal occurrences, which in some cases are genetically related to the magmatism. Types and styles of mineralization include the following: sheeted vein systems hosted within the intrusions (Fort Knox, Dublin Gulch, Sheeted Zone at Scheelite Dome), sheeted veins within meta-sediments (Harvey-Rudolph Area at Scheelite Dome), disseminations and stringers in intrusions (Brewery Creek), skarns adjacent to intrusions (Marn, Cominco Zone, Tom Zone at Scheelite Dome), quartz-sulphide veins within hornfels zones (Hawthorne Vein at Scheelite Dome), sediment-hosted stratabound sulphide replacement (Tom Zone at Scheelite Dome), and disseminated, stringer and breccia-hosted mineralization external to the hornfels zone (Highet Creek zone at Scheelite Dome). The characteristic metal assemblage of TPS related deposits is Au-W-Bi-As-Sb-Te-Mo±Cu±Pb±Sn. With a few exceptions, tin-silver bearing breccias, veins and skarns are spatially associated with younger (64-67) Ma McQuesten two-mica granites, while tungsten-gold bearing skarns and sheeted veins are associated with the TPS (Emond, 1992; Murphy, 1997).

Regionally, placer gold deposits draining the topographic highs formed by the Tombstone intrusions include Dublin Gulch and Haggert Creek, draining the Dublin Gulch gold deposit; Clear and Left Clear Creek draining the Clear Creek intrusions; Highet, Sabbath and Johnson Creeks draining Scheelite Dome; Duncan and Lightning Creeks draining the Keno Hill area and Arizona and Gem Creeks draining Red Mountain.

A tabulated geologic history of the Mayo area with associated mineralization is presented below.

TABLE 7.1 - GEOLOGIC HISTORY OF THE MAYO AREA

(modified from Hulstein and Zuran, 1997)

Age	Event/Lithology	Mineralization
Quaternary	Alluvium/colluvium, glacial till	Placer gold deposits
Tertiary	450 km dextral movement on the Tintina Fault/warping; volcanics & hypabyssal intrusives, volcaniclastics & clastics	Au in veins & stockworks (Grew Creek)
Earliest Tertiary-Latest Cretaceous (67-64 Ma)	McQuesten Plutonic Suite; two mica granite, quartz monzonite, rhyolite flows and intrusives: faulting and brecciation, clastic sedimentation	Sn-Ag in veins, breccias (Oliver Creek, Zeta)
Cretaceous (92.5-90.5 Ma)	Tombstone Plutonic Suite; biotite-hornblende quartz monzonite, granodiorite, quartz diorite, rhyolite dykes: faulting	Au+/-W+/-Bi in veins, stockworks & breccias, rhyolites (Dublin Gulch, Brewery Creek) Pb-Zn-Ag in veins (Keno Hill), Au in calc silicates (Wayne), U,REE in veins, stockworks & disseminations (Tombstone Mtn), Sn-Mo in stockwork (Two Buttes), W in skarns (Dublin Gulch)
Jurassic-Cretaceous	Faulting; Dawson, Tombstone & Robert Service Thrusts; Tombstone Strain Zone	
Triassic	gabbro, diorite	
Mississippian	Keno Hill quartzite	
Devonian-Mississippian	Earn Group; shales, conglomerates	Stratiform Pb-Zn-Ag-Ba, VMS (Marg)
Unconformity		
Ordovician-Devonian	Road River Group; limestone and shale	Stratiform Pb-Zn
Unconformity		
Upper Proterozoic - Lower Palaeozoic	Hyland Group; 'grit', arenite, phyllite, greenstone	

Source: Murphy and Héon, 1995; Emond, 1992, Hart et al, 2000.

7.2 Property Geology

The property is underlain by the Yusezyu Formation, a siliciclastic unit of the Upper Proterozoic-Lower Cambrian Hyland Group. The meta-sedimentary rocks include highly foliated, interlayered muscovite-chlorite phyllites, quartzo-feldspathic and micaceous psammites ('dirty quartzites'), and gritty psammites that locally form massive outcrops. Recrystallized limestone and calc-silicate (chlorite, actinolite, calcite, quartz, and diopside) outcrops are best exposed on the north side of the property although pods and boudins of marble and limy psammites can be found throughout the property.

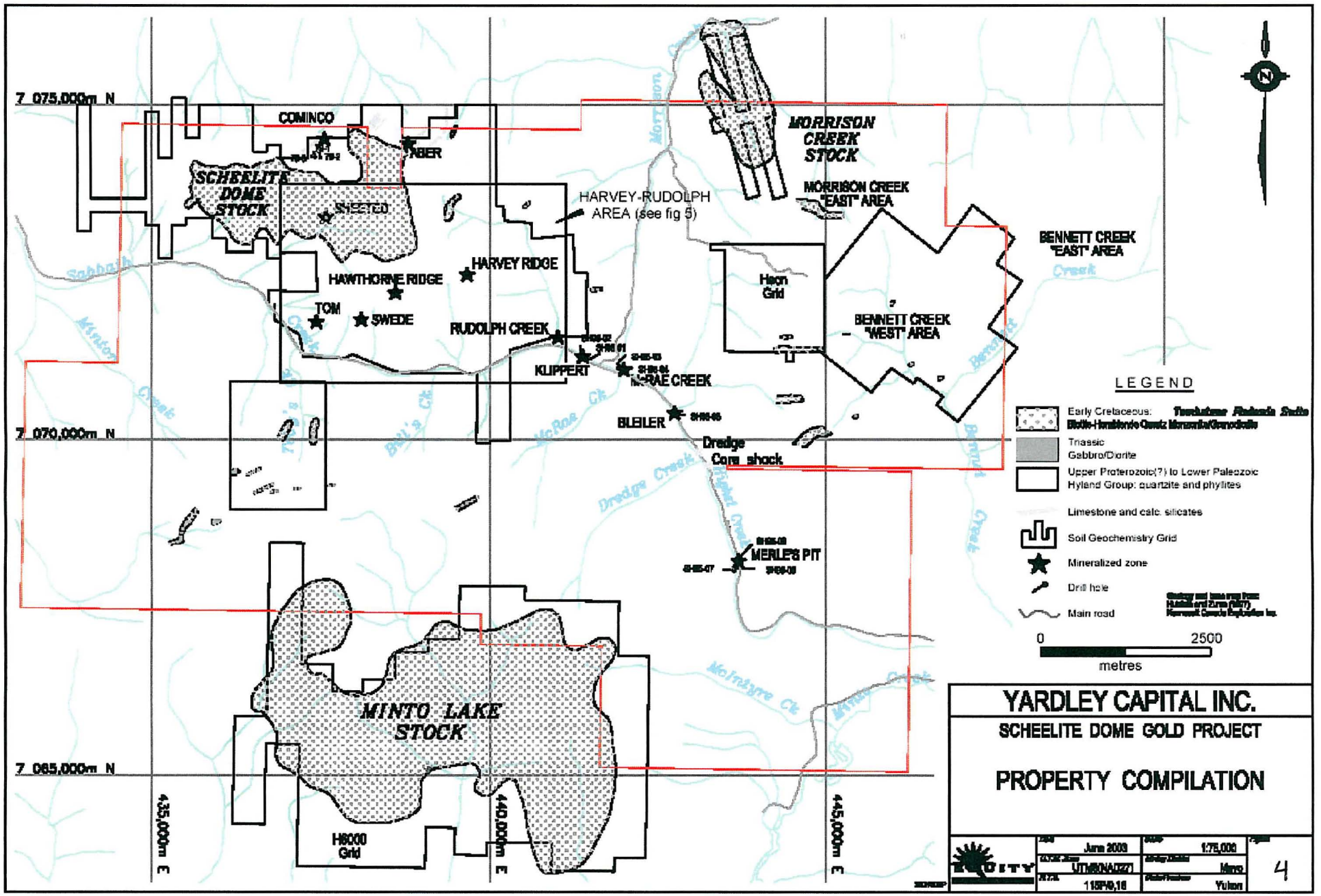
The most prominent intrusive rocks on the property are three quartz monzonite and granodiorite stocks; the Scheelite Dome, Morrison Creek and Minto Lake stocks (Figure 4). The level of exposure varies but the compositionally similar stocks are comprised largely of medium- to coarse-grained, hornblende- and biotite-bearing granodiorite. These rocks are massive and blocky and weather grey with rare chloritized fracture surfaces. Fresh surfaces show hypidiomorphic texture and are unfoliated with the exception of local, weakly developed flow banding. These igneous rocks form part of the early Late Cretaceous (92.5 to 90.5 Ma, Hart et al, 2000) TPS suite of intrusions. These stocks are enveloped by thermal metamorphic aureoles that are apparent in the helicopter-borne magnetic surveys and characterized by the development of andalusite, biotite, recrystallized quartz and pyrrhotite.

Older foliated 'diorite' bodies as intersected in drill hole SH98-09 are likely Triassic in age. They also outcrop as a series of resistant, east-west trending, discordant dykes on the Héon grid. One such diorite dyke in this area displays a weak foliation that is sub parallel to foliation in the enclosing meta-sediments.

Narrow lamprophyre dykes are present throughout the property and tend to occupy fracture and fault zones. They are calcareous and weather brown to light grey with dark brown fresh surfaces. The lamprophyre dykes commonly contain fine-grained biotite and minor pyrrhotite. Felsic dykes of very fine-grained to aphanitic aplite, rhyodacite, porphyritic trachyte and quartz monzonite are also present and may be related to the TPS intrusions.

7.2.1 Ductile Deformation

The property is located on the south-dipping limb of the southwest-trending McQuesten Antiform, within the Tombstone Strain Zone (Murphy, 1997). This package of rocks lies above the northeast-directed Tombstone Thrust. Jura-Cretaceous S2 foliation developed along axial planes to isoclinal folds of S1 foliation, which appears parallel to compositional layering. These F2 folds are southwest striking, shallowly-plunging, northwest-verging and tight to isoclinal and have produced a strong, southwest-trending, moderately southeast-dipping foliation. This fabric affects the meta-sedimentary rocks, and is the most prominent ductile fabric on the property. The poles to this S2 foliation form a single cluster with an average orientation of 054°/41°SE. The southeast dip of the foliation reflects the property's position on the southern limb of the McQuesten Antiform, a broad, open fold which postdates the main deformation and intrusion of the Tombstone Intrusions.


7 075,000m N
7 070,000m N
7 065,000m N
435,000m E
440,000m E
445,000m E
COMINCO
ABER
SCHEELITE DOME STOCK
SHEETCO
HARVEY-RUDOLPH AREA (see fig 5)
MORRISON CREEK STOCK
MORRISON CREEK "EAST" AREA
BENNETT CREEK "EAST" AREA
BENNETT CREEK "WEST" AREA
HARVEY RIDGE
HAWTHORNE RIDGE
TOM
SWEDE
RUDOLPH CREEK
KLIPPERT
McRAE CREEK
BLEILER
Dredge Corn shack
MERLE's PIT
MINTO LAKE STOCK
H8000 Grid
Hern Grid
Sabbath Creek
Minton Creek
Bell's Ck
McRae Ck
Dredge Creek
McIntyre Ck
Bennett Creek
LEGEND
Early Cretaceous: Tombstone Plutonic Suite
Biotite-Hornblende Quartz Monzonite/Granodiorite
Triassic
Gabbro/Diorite
Upper Proterozoic(?) to Lower Paleozoic
Hyland Group: quartzite and phyllites
Limestone and calc. silicates
Soil Geochemistry Grid
Mineralized zone
Drill hole
Main road
0
2500
metres
YARDLEY CAPITAL INC.
SCHEELITE DOME GOLD PROJECT
PROPERTY COMPILATION
June 2009
1:75,000
Mayo
Yukon
4

7.2.2 Brittle Deformation

The above foliation is crosscut by three sets of moderate- to steeply-dipping fault, shear, fracture and joint structures that trend east-west to east-northeast, northwest and north-south:

- Steeply-dipping, north-south faults are the earliest set of brittle structures and are associated with coarse, massive, barren bull quartz. These regularly-spaced faults (Rudolph, Harvey, Swede, and Tom Faults) appear to form a radial pattern that emanates from the Minto Lake Stock to the south.

- A period of east-west compression and north-south extension produced a series of northwest faults, east-striking vein sets and north-south crenulations. The set of northwest faults are closely-spaced, left-lateral and moderately to steeply dipping, and are particularly well-developed in the Harvey - Rudolph and Héon - Bennett areas. The best surface example of one of these faults is the Hawthorne Structure, striking 318°/56°NE.

- The east-west compressional event acting upon the northwest faults created a tensional environment that resulted in the formation of east-west striking, shallowly to moderately dipping veins, centred on 274°/39°N. The lamprophyre and monzonite dykes were also largely emplaced along this orientation. Fracturing at a similar orientation is present throughout the property. Almost all of the quartz+arsenopyrite veins are discordant to foliation and planar, even though folded, lenticular, folioform quartz veining is probably more abundant. In addition, some planar concordant veins were noted in outcrop, roughly following foliation, as noted in the bluffs above the Tom Zone, but clearly post-dating ductile deformation.

Steeply-dipping north-south veins are rare, although discordant fracturing is common in this orientation. These veins and fractures are particularly prevalent along steep, north-south kinks and crenulations in the S2 foliation, which may have developed during east-west shortening along axial planes.

8.0 DEPOSIT TYPES

Geological and geochemical evidence indicates that occurrences on the Scheelite Dome property are of many styles related to the intrusion of the Scheelite Dome Stock. These occurrences range from discordant sheeted quartz veins hosted in both the intrusion and the thermally metamorphosed meta-sediments, Au±W skarns, concordant sulphide replacements of meta-sedimentary horizons, and auriferous disseminated sulphides within intrusions. These mineralization styles are characteristic of a recently recognized class of Intrusion Related Gold Deposits (IRGS).

IRGS deposits are important producers of Au in Canada, Alaska and worldwide. Significant deposits include the large tonnage, low grade Fort Knox Mine and Donlin Creek deposit in Alaska, the Brewery Creek Mine and Dublin Gulch deposit in Yukon, Kidston and Timbarra in Australia, and Vasilkovskoe in Kazakhstan. The Pogo deposit in east-central Alaska may also be a high-grade example of an IRGS deposit. Mineralization styles at these deposits vary greatly in response to, among other factors, structural environment, host rocks and crustal level of development. The unifying link between these deposits is a link to moderately reduced I- and S-type intrusions with lithophile elemental associations, in particular associated with Au-Bi-W-As-Te-Mo±Sn±Cu±Pb±Sb anomalies and occurrences. IRGS deposits in Yukon and Alaska are invariably associated with Cretaceous intrusions.

The causative intrusions commonly form belts generated in continental settings and well inboard of subduction zones. Intrusions are felsic to intermediate and commonly display evidence of higher degrees of fractionation, including aplitic dykes and sills. The intrusions vary with depth of emplacement from large batholiths to stocks, pipes and plutons to porphyritic sills, dykes and domes. Extensive thermal metamorphic aureoles are commonly developed about these intrusions and typically comprise biotite, andalusite, sillimanite, quartz, cordierite and pyrrhotite. The deficiency of magnetite in the moderately reduced intrusions and presence of pyrrhotite in the metamorphic aureole leads to a distinct regional geophysical signature for these systems consisting of a magnetic low enclosed by a relative magnetic high.

On a deposit scale structure, lithology and distance from intrusion impart important controls on mineralization style. Sheeted and stockwork quartz-sulphide veins are commonly hosted within the intrusions. These vein sets typically have low total sulphide contents, comprising pyrite, pyrrhotite, and arsenopyrite with lesser native bismuth, tetradymite, bismuthinite, molybdenite and scheelite. Alteration associated with the veins is absent to very weak and comprises the development of potassium or albitic feldspar, sericite, or carbonate vein selvages. Au±W and Au±Cu skarns are located within or immediately adjacent to the intrusions. Au±W skarns are comprised of pyroxene, biotite and garnet with pyrrhotite, chalcopyrite, scheelite, and bismuthinite, and Au±Cu skarns are comprised of hedenbergitic pyroxene, almandine garnet and wollastonite, with pyrrhotite, chalcopyrite, bismuthinite and Au.

Mineralization hosted in the country rocks varies greatly and is typically located in the hornfelsed aureoles of the intrusions. These styles include replacements of, and disseminations within calcareous and non-calcareous hornfels, hydrothermal breccias, sheeted and stockwork veinlets, skarns, shear-related and epizonal mineralization. Replacement mineralization consists of disseminated to semi-massive pyrrhotite, auriferous arsenopyrite and bismuthinite. Hydrothermal breccias are most commonly structurally-related, although magmato-hydrothermal breccias are also present. Several deposits are comprised of sub-parallel, sheeted and stockwork quartz±sulphide veinlets that typically host low volumes (<3 volume %) of pyrite±arsenopyrite±pyrrhotite. Skarns developed distal to intrusions contain amphibole, chlorite, calcite and epidote with pyrrhotite, arsenopyrite, chalcopyrite, and scheelite. Shear-related mineralization varies from large quartz veins in ductile regimes to brittle gouge-filled sulphide-rich shear zones and disseminated mineralization adjacent to shear zones. Sulphide minerals include arsenopyrite, pyrite, pyrrhotite, stibnite, jamesonite, tetrahedrite, boulangerite, galena, bismuthinite and other Bi-species, molybdenite, sphalerite and Au. Epizonal

mineralization is characterized by structurally-controlled quartz-sulphide veinlets, stockworks, breccias and disseminations with arsenopyrite, pyrite and later stibnite. Rheologic controls are also evident in the epizonal deposits as fracture-controlled mineralization is preferentially hosted in more brittle host rocks.

IRGS deposits also exhibit chemical zonations; proximal deposits have a strong Au-Bi-Te-W-Mo-As±Cu elemental association and shallower or more distal styles of mineralization have a contrasting metal assemblage of Au-As-Sb-Hg±Pb±Zn±Ag.

9.0 MINERALIZATION

Alteration and mineralization on the Scheelite Dome property is related to the Tombstone Plutonic Suite stocks and smaller intrusive bodies. Auriferous zones related to the TPS, occur in several different styles and lithologies and can be separated into three categories, concordant, discordant and skarn mineralization.

Concordant Mineralization:

Sulphide minerals, comprised of arsenopyrite and locally, pyrite marcasite and pyrrhotite, are found as concordant replacements in several zones. Limy horizons within the meta-sedimentary package are particularly receptive hosts for this style of mineralization. Concordant, undeformed quartz±arsenopyrite±pyrite veins have been noted in the Tom Zone and Toby's Creek area. These structurally-controlled veins occur where the S_2 foliation has opened under a tensional environment. This veining is commonly accompanied by sulphides, principally arsenopyrite, disseminated along the S_2 foliation.

Discordant Mineralization:

The most prevalent discordant mineralization consists of structurally-controlled quartz-sulphide veinlets that are the main source of the Au-As-Sb soil anomaly and comprise the bulk of the gold mineralization intersected in the drilling. The veins crosscut both the meta-sediments and the Scheelite Dome stock, and occur within and external to the contact metamorphic aureole surrounding the Scheelite Dome Stock. Alteration envelopes and selvages associated with this mineralization include sericite, silica, biotite and tourmaline. Coarser quartz-sulphide fault-veins and disseminated mineralization hosted in intrusive and meta-sedimentary rocks are also significant styles of discordant mineralization.

Skarn Mineralization:

Zones of auriferous garnet-wollastonite-quartz-tremolite skarn with disseminations and blebs of pyrrhotite, scheelite and chalcopyrite are found on the north side of the Scheelite Dome Stock. Contact skarn mineralization consisting of calc-silicate (diopside), biotite, and chlorite is also found associated with biotite lamprophyre dykes in SH99-16.

In addition to the mineralization styles noted above, early synmetamorphic quartz-chlorite-pyrrhotite±chalcopyrite veins are prevalent throughout the property. These veins are easily identified by the presence of chlorite and are distinguished by their irregular pinch and swell foliation-parallel habit. In any of the core drilling to date, the percentage of folioform veins far exceeds that of the later, gold-bearing, discordant

veins. These early quartz veins are not thought to be auriferous. It was apparent from the drilling that late stage calcite and iron-carbonate veining crosscuts all earlier vein types. This veining tends to occupy microfractures, and as it does not contain any sulphide minerals, it is not expected be gold-bearing.

9.1 Tom Zone

The Tom Zone concordant mineralization consists of exposures of a lens of calcareous rocks along a road cut over 100 metres. Mineralization varies from disseminated and semi-massive sulphides within limy quartzites to coarse-grained sulphide mineralization in calc-silicate skarn. J. Mair (pers. comm., 2003) has examined the skarn mineralization and recognized two main assemblages; an earlier actinolite-plagioclase skarn with pyrrhotite, pyrite, arsenopyrite, chalcopyrite and native bismuth and a strong Au-Bi-Te±As-Cu association, and a second assemblage of phlogopite with arsenopyrite, lesser pyrrhotite and pyrite and high W, Bi, Te and Au grades. Mair also suggests that the second assemblage may overprint an earlier sulphide-poor W skarn that is characterized by diopside and plagioclase. A medium-grained monzonitic intrusion immediately north of this zone is likely related to this mineralization.

TABLE 9.1 - TOM ZONE SIGNIFICANT INTERSECTIONS

Hole No.	From (metres)	To (metres)	Intercept Width (metres)	Intercept Width (feet)	Gold gm/tonne	Gold oz/ton
SH03-29	20.12	21.34	1.22	4.0	5.06	0.149
SH03-30	5.00	11.40	6.40	21.0	7.09	0.207
including	8.60	10.30	1.70	5.58	24.42	0.72
	10.30	11.40	1.10	3.61	1.12	0.032
	23.16	24.10	0.94	3.08	1.98	0.058
SH03-31	No	Significant	values			
SH03-32	84.12	89.92	5.80		2.55	
Including	85.50	86.87	1.37		10.00	
SH03-33	12.19	12.80	0.61		3.53	

Kennecott sampled a number of discordant quartz-arsenopyrite veins up to 10 cm wide from the Tom Zone. These veins are similar to those encountered in the Rudolph Gulch to Hawthorne Ridge area and locally returned excellent Au grades and visible Au. Sample #12650 was collected from an area where these veins exceeded 1/m in density and returned 585 ppb Au.

The Tom Fault is a steeply-dipping north-south fault that consists of a core of silicified sulphide cemented breccia (#312162) flanked by bleaching and oxidation (#312163). O'Dea (1999) postulates that these north-south faults may be mineralized upon reactivation.

Other concordant mineralization is exposed in the bluffs above the Tom Zone skarn (#312036) and in the Toby's Creek valley (#312043) south of the Tom Zone and consists of structurally-controlled, quartz-sulphide veins paralleling the S2 foliation.

9.2 Rudolph Gulch to Hawthorne Ridge Zone

The main target of the 1997 through 1999 exploration programs was an extensive area (1.5 by 4.0 km) of strongly anomalous Au-As soil geochemistry and widespread quartz-sulphide veining within the meta-sediments. Quartz veinlets are typically less than 1 cm wide, contain arsenopyrite and pyrite and are preferentially hosted in more brittle lithologies such as more quartzite-rich units or monzonites. The veinlets are dominantly east-striking with moderate to steep northerly dips. East-west, north-south, and northwest-striking fault structures are prevalent in this area. O'Dea (1999) believes that east-west directed compression acting upon an array of northwest-striking faults has resulted in left-lateral displacement along these faults and that the north-dipping veinlets have propagated in tensional environments from the northwest-striking faults. Although no bismuth minerals were identified in the drilling, it is clear from the correlation coefficient for 1998 and 1999 core samples that gold correlates better with bismuth (0.595) than arsenic (0.390) or antimony (0.104).

The northwest-striking faults, such as the Hawthorne Vein, are up to 1.0 metres wide and exhibit multiple stages of quartz-sulphide mineralization. They are comprised of quartz, quartz-arsenopyrite, and late massive sulphide stibnite ± jamesonite ± sphalerite ± pyrite ± galena phases.

Steeply-dipping north-south faults are present at regular intervals across this zone. Rudolph Creek is host to one of these structures that was tested by hole SH99-28. The hole encountered an interval of bleached, sericite-altered quartzose phyllite that has been brecciated by 30-40% massive milky quartz. This quartz vein material, however, which probably represents the steeply east-dipping Rudolph Fault, did not return anomalous Au values.

Disseminated sulphides are hosted in both intrusive and meta-sedimentary units, although the bulk of disseminated sulphides are found outside of the intrusives. Disseminated arsenopyrite, pyrite and pyrrhotite are disseminated throughout the meta-sedimentary units in zones of greater permeability, such as in more porous, quartzite-rich units, or in zones of increased fracturing. Areas of disseminated mineralization are typically altered by sericite and silica or less commonly biotite or muscovite (#312048), and are often found enveloping the quartz-sulphide veins described above. This disseminated mineralization is particularly well-developed in monzonite dykes intersected in holes RC97-11, SH98-10 and SH99-24.

TABLE 9.2 - RUDOLPH GULCH TO HAWTHORNE RIDGE ZONE SIGNIFICANT INTERSECTIONS

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
RC97-2	38.10	41.15	3.05	1285	1433	1.5	29

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
RC97-3	4.57	7.62	3.05	1887	1845	4.5	54
And	60.96	62.48	1.52	1000	590	<2	8
RC97-4	9.14	13.72	4.58	2012	1331	1.3	7
RC97-5	18.29	19.81	1.52	1010	1320	<2	10
RC97-7	0.00	113.54	113.54*	169	755	1.0	16
and	80.77	82.30	1.53	1410	340	2	<1
RC97-10	65.53	70.10	4.57	1318	2650	21.3	30
RC97-11	15.24	19.81	4.57	1195	4010	12.7	118
and	35.05	36.58	1.53	1700	3390	26.0	128
and	48.77	57.91	9.14	1012	3960	2.0	68
RC97-13	19.81	21.34	1.53	1430	5420	2.0	158
SH98-09	88.5	90.0	1.5	1065	9990	10	1
SH98-10	80.0	94.9	14.9	1043	3647	11	62
and	173.1	174.6	1.5	1030	1530	1	18
SH98-11	99.8	111.9	12.1	1073	1358	10	14
and	160.9	164.5	3.6	2120	865	15	31
and	170.5	171.3	0.8	1650	1145	10	12
SH98-12	16.3	24.0	7.7	3668	2194	66	451
including	20.5	21.9	1.5	10560	2200	150	414
SH98-14	65.6	85.6	20.0	1037	1127	1	8
including	66.6	75.2	8.6	1295	1388	2	12
and	108.3	109.1	0.8	1675	2400	2	2130
SH99-16	71.6	72.8	1.2	1.29 g/t	10367	1.5	21
and	85.5	87.0	1.5	1.37 g/t	4254	22	44
and	210.5	211.0	0.5	1.75 g/t	16400	16	25
SH99-17	45.9	47.4	1.5	1.83 g/t	2308	1.5	1.5
and	147.2	148.7	1.5	1.30 g/t	664	16	27
and	191.8	192.7	0.9	1.30 g/t	23546	7	1862
SH99-19	18.6	19.2	0.6	1.43 g/t	4658	86	16316
and	28.2	29.7	1.5	1.51 g/t	481	28	64
and	32.0	33.1	1.1	1.29 g/t	2865	32	1.5
SH99-20	29.0	29.8	0.8	5.90 g/t	2395	79	119
SH99-21	14.7	16.2	1.5	1.47 g/t	523	46	53
and	45	46.5	1.5	2.91 g/t	482	16	154
SH99-23	49.6	54.1	4.5	3.66 g/t	6131	20	214
including	52.6	54.1	1.5	7.64 g/t	14059	23	172
SH99-24	6.2	12.1	5.9	2.41 g/t	9562	11	226
including	7.6	9.1	1.5	3.04 g/t	6626	12	367
and	49.3	51.7	2.4	1.09 g/t	15898	2	1167
including	49.3	50.3	1.0	1.23 g/t	13193	1.5	353
SH99-25	104.5	105.6	1.1	1.02 g/t	5150	5	26
SH99-28	51.2	53.8	2.6	1.03 g/t	8852	13	17
and	131.8	133.2	1.4	1.16 g/t	19370	1.5	24592

Note: For weighted averages, Bi and Sb values below detection (<2 ppm) are assigned a value of 1 ppm, As and Sb values above detection (>10000 ppm) are assigned a value of 10000 ppm.

9.3 Héon Ridge Zone

Like the Rudolph Gulch to Hawthorne Ridge Zone, the Héon Ridge Zone is an extensive Au-As soil geochemical anomaly underlain by quartz-sulphide veinlets hosted in meta-sedimentary rocks outside of the Scheelite Dome metamorphic aureole. The east-striking, north-dipping veins have also developed in a tensional environment related to east-west compression imposed on northwest-striking faults, the Héon and Héon North faults. Although grab samples of the veining in this zone returned up to 21.6 g/t Au, similar grades were not returned in limited drilling in 1999.

TABLE 9.3 - HÉON RIDGE ZONE SIGNIFICANT INTERSECTIONS

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
SH99-26	3.0	74.7	71.7	28	655	3	26
including	57.9	58.4	0.5	1.06 g/t	7436	13	45
SH99-27	4.2	80.5	76.3	62	1478	5	33
including	32.7	33.1	0.4	938	34322	26	101
and	40.0	40.4	0.4	935	18334	7	89

Note: For weighted averages, Bi and Sb values below detection (<2 ppm) are assigned a value of 1 ppm, As and Sb values above detection (>10000 ppm) are assigned a value of 10000 ppm.

Similar mineralization has been noted in the Bennett Creek West area immediately east of the Héon Ridge Zone, including a sample returning 1,340 ppb Au (Murphy and Héon, 1995). Cominco also collected a sample of gossanous quartzite with a lens of pyrrhotite that contained 5,600 ppb Au and anomalous Cu and W.

9.4 Sheeted Zone

The Scheelite Dome stock hosts a sheeted array of quartz-muscovite-scheelite-tourmaline veinlets. The Sheeted Zone lies along the projection of the Hawthorne Vein-Fault on the north side of Scheelite Dome. Three sets of veins have been recognized in this zone; milky feldspar-quartz veinlets, cut by white to light grey quartz±feldspar, and finally white to grey quartz veinlets. The last two vein sets contain minor arsenopyrite and are thought to be associated with Au mineralization. The veinlets are enclosed by narrow envelopes of sericite with bleaching and silicification. Soil sampling and subsequent bulldozer trenching returned discouraging results and follow-up sampling by Kennecott returned values of less than 100 ppb Au.

9.5 Bleiler Zone

The Bleiler Zone is comprised of a calcareous, compositionally banded muscovite-biotite-quartz-potassium feldspar schist that varies from <1 metre to <20 metres thick. This zone is exposed by the workings of placer operations in Highet Creek. The schist unit is locally mineralized with 1-3% marcasite, pyrite, pyrrhotite and arsenopyrite. Trenches of these exposures identified zones of clay with white and grey quartz and brecciated quartzite with anomalous Au values. The Bleiler Zone was tested by drill hole SH95-05 and returned a 4.4 metre wide intersection of silicified schist with pyrrhotite and pyrite that averaged 1.2 g/t Au.

TABLE 9.4 - BLEILER ZONE SIGNIFICANT INTERSECTIONS

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
SH95-05	69.05	73.46	4.41	1162	390	62	1

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
and	75.89	76.19	0.30	705	406	36	<2
and	80.77	81.12	0.35	2780	606	144	<2
and	89.52	90.12	0.60	2260	372	214	<2
and	91.73	92.03	0.30	530	8	30	<2

Note: For weighted averages, Bi and Sb values below detection (<2 ppm) are assigned a value of 1 ppm, As and Sb values above detection (>10,000 ppm) are assigned a value of 10,000 ppm.

9.6 Klippert and McRae Creek Zones

These zones, located approximately 400 metres apart along Highet Creek, are hosted within gently-dipping phyllitic quartzites, quartzites and phyllite. Mineralization is located within quartzite, calc-silicate (and possibly skarnified horizons), quartz veins and clay-rich thrust fault zones. Sulphide mineralization consists of disseminated to semi-massive folioform arsenopyrite in discontinuous bands <10 cm thick. Phyllitic units are locally clay- and coarse arsenopyrite-rich and are cut by sub-horizontal shearing. Discordant quartz veining in these zones is hosted in more brittle lithologies and has been postulated as feeder structures for the replacement-style mineralization. Numerous rock samples from this zone exceed 1.0 g/t Au and 10,000 ppm As, although this mineralization is not continuous. The Klippert and McRae Zones were tested by, respectively, drill holes SH95-01 and –02, and SH95-03 and –04.

TABLE 9.5 - KLIPPERT AND MCRAE CREEK ZONES SIGNIFICANT INTERSECTIONS

Hole No.	From (m)	To (m)	Length (m)	Au (ppb)	As (ppm)	Bi (ppm)	Sb (ppm)
SH95-01	24.60	24.90	0.30	1010	>10000	60	4
	46.85	47.31	0.46	1160	5200	22	2
	50.75	53.75	3.00	612	9410	33	2
SH95-02	29.57	32.00	2.43	1036	6322	5	2
SH95-03	83.75	83.95	0.20	3690	>10000	52	24
	90.60	91.84	1.24	1065	4535	6	9
	126.50	127.98	1.48	660	404	4	<2
SH95-04	127.53	128.63	1.10	540	5990	10	4
	133.75	134.45	0.70	710	388	12	2
	142.65	144.78	2.13	475	1010	6	4

Note: For weighted averages, Bi and Sb values below detection (<2 ppm) are assigned a value of 1 ppm, As and Sb values above detection (>10,000 ppm) are assigned a value of 10,000 ppm.

9.7 Merle's Pit Zone

This zone is exposed in placer workings as a gently undulating grey gouge fault zone that is 0.5 to 1.0 metres wide. The fault contains brecciated quartz with arsenopyrite and scorodite and cuts variably bleached, sericitized and hematitized phyllitic quartzite and phyllite. Grab samples have returned up to 7,560 ppb Au and chip samples have returned a weighted average of 696 ppb Au over an average width of 2.5

metres. Drill holes testing this zone averaged <75% recovery through the target horizon and returned only anomalous Au values (to a maximum of 435 ppb Au) that may have suffered from poor recovery through the zone.

9.8 Cominco and Aber Zones

These zones are comprised of recrystallized and skarnified limestone along the northern margin of the Scheelite Dome stock. In 1979 drill testing of the Cominco Zone garnet-wollastonite-quartz-tremolite Au-W skarn returned 0.95 g/t Au over 7.9 metres. Kennecott collected samples of calc-silicate skarn with pyrrhotite that returned 680 to 5720 ppb Au and non-mineralized calc-silicate skarn yielded Au values less than 740 ppb Au. The Aber Zone is a Au-Bi-W skarn comprised of prograde and retrograde phases. The prograde phase is comprised of pyrrhotite, scheelite and chalcopyrite and the retrograde actinolite phase contains scheelite. Mineralized samples from trenches returned up to 8.2 g/t Au.

9.9 Toby Zone

The Toby Zone occurs south of Highet and Sabbath creeks and south of the Tom Zone. Very little work had been done in this area prior to 1999. A total of at most a couple of days of prospecting had yielded rock samples grading up to 3.2 g/t Au, but no significant zones of alteration or mineralization were noted. Based on the local gold values, Copper Ridge completed a soil sampling program over the Toby Zone in 1999 which consisted of the collection of 500 samples from a 200 m by 50 m grid. While the gold values returned from this survey where generally moderate in comparison to the results from other areas, the survey outlined the strongest coincident arsenic and bismuth anomalies on the property. These anomalies were never followed up.

10.0 2006 EXPLORATION PROGRAM

The 2006 exploration program focused on the Toby Zone in order to follow up the soil sampling program completed in 1999.

The 2006 program consisted of detailed prospecting and the completion of soil geochemical and IP, magnetometer and VLF geophysical surveys over 21 line kilometres of grid (Figure 2). A total of 143 rock samples were collected during the prospecting program and a total of 456 soil samples were collected during the soil sampling program. This work was followed up by a trenching program during which 1.43 km of trenches were excavated and a total of 657 chip and grab samples were collected.

The line cutting and geophysics were completed by Aurora Geosciences of Whitehorse while the prospecting and soil sampling was conducted by Aurum Geological Consultants of Whitehorse. The trenching was completed by Wilf's contracting of Mayo and the trench sampling was done by Aurum Geological Consultants. The project was

supervised by J. Greg Dawson PGeo, who visited the property several times during the course of the field work.

The total cost of the 2006 program was $265, 687.12

10.1 Prospecting

The prospecting concentrated mainly around upper reaches of Toby creek where the previous soil sampling had defined a strong coincident arsenic and bismuth soil geochemical anomaly. Sample locations with sample numbers are shown in Figure 5. Proportional bubble plots for gold, arsenic and bismuth are shown in Figures 6 through 8 respectively. Sample locations and descriptions are included in Appendix A and analytical data is included in Appendix B.

The prospecting defined several areas of strong alteration and silicification in the upper reaches of Toby Creek. The alteration was often associated with disseminated pyrite and locally blebby to disseminated arsenopyrite. Gold values were generally low in these rocks.

The prospecting also found subrcop rocks containing veins of "frothy" quartz and massive arsenopyrite. These samples always contained gold, ranging from several hundred ppb to 5.4 g/t Au in sample 404994. A review of the data shows that high arsenic values are generally but not always accompanied by high gold values while high bismuth values are always accompanied by high gold values. This confirms previous work which demonstrated a strong correlation between gold and bismuth in the Scheelite Dome mineralized systems.

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

439000 mE

N

404911
404910
404939
404909
404912
404908
404907
404906
404905
404917
404918
404919
404922
404925
404926
404927
404924
404923
404921
404920
404916
404913
404902
404914
404915
404903
404928
404904
404929
404970
404969
115679
115680
115681
115682
115670
115671
115672
115673
404941
404930
404931
404934
404942
404943
404933
404971
115676
115677
115678
115700
115692
115691
115689
115690
115688
115696
115697
115695
115698
115693
115683
404937
404936
404935
115684
115685
115686
115687
404932
404945
404946
404949
115674
404972
404947
404948
404968
404967
404973
404974
404975
404976
404977
404979
404978
404980
404982
404983
404985
404986
404989
404991
404994
404962
404988
404987
404964
404966
404965
404995
404990
404938
404940
404960
404959
405003
405010
405007
405009
405011
405008
404958
405006
405005
405004
405002
405000
404999
405001
404997-98
404996
404961
404992
404993
404952
404951
404953
404954

0 500 1,000

metres

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone
Rock Sample Locations
And Sample Numbers

Date:4/1/2007
Author:
Office:
Drawing:
Scale: As Shown
Projection: NAD 27 Zone7

Figure 5

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

439000 mE

N

Rock Samples
ppm As

- 7,500 to 10,000
- 1,500 to 7,500
- 500 to 1,500
- 200 to 500
- 0 to 200

0 500 1,000

metres

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone
Arsenic in Rock Samples

Date:4/1/2007

Author:

Office:

Drawing:

Scale: As Shown

Projection: NAD 27 Zone7

Figure 7

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

439000 mE

N

0 500 1,000

metres

Rock Samples
ppm Bi

	100 to 596	(9)
	50 to 100	(5)
	15 to 50	(7)
	4 to 15	(8)
+	0 to 4	(110)

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone
Bismuth in Rock Samples

Date:4/1/2007

Author:

Office:

Drawing:

Scale: As Shown

Projection: NAD 27 Zone7

Figure 6

10.2 Geophysics

The geophysical survey was completed on a grid with 200 m space lines. IP survey was done on with a 50 m dipole spacing while the VLF and magnetometer readings were taken at 25 m spacings along the lines. The results of the geophysical survey were not received prior to the conclusion of the prospecting program so could not be used to guide the prospecting. A report on the geophysical surveys is included in full as Appendix C in Volume II.

10.2.1 IP Survey

The modelled chargeability and resistivity results are shown in Figures 9 and 10 respectively. These figures are included in the body of the report for discussion purposes only. Better resolution copies of the figures are included in Appendix C.

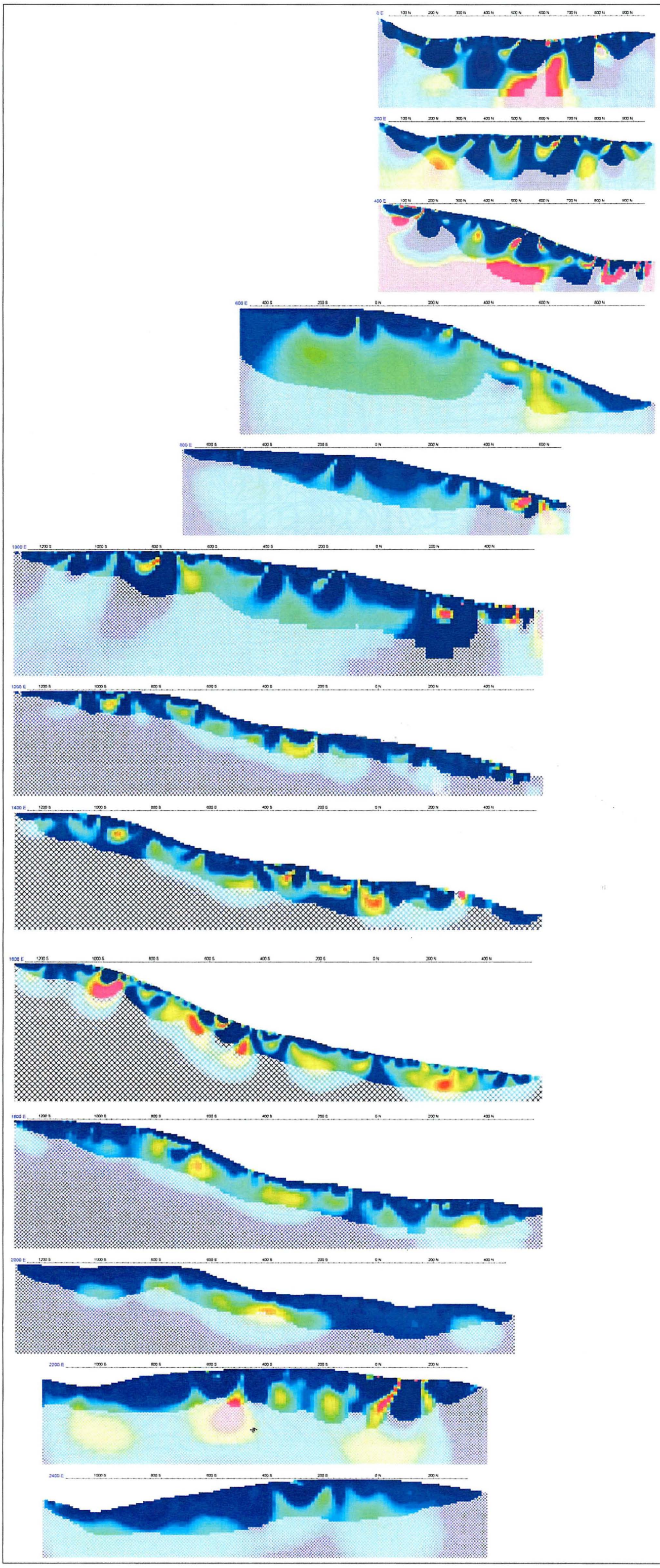
The chargeability survey defined several areas of relatively discreet and near surface high chargeability, most notably on the north end of line 2200E, the south end of line 1600E, both ends of line 1000E and the south end of line 800E. These could be caused by structurally or stratigraphically controlled zones of disseminated sulphide mineralization developed in the meta-sediments. Prospecting and trenching has demonstrated that the anomaly on the south end of Line 16E correlates with strong disseminated pyrite mineralization developed around auriferous quartz veins, but the source of the other anomalies remains to be determined.

Two quite large and deeper chargeability anomalies are defined in the centres of lines 400E and 00E. These could be caused by larger bodies of skarn hosted mineralization developed in the meta-sediments around an unexposed intrusive body at depth.

The resitivity data show several broad areas of lower resistivity (i.e., higher conductivity) on lines 2000E through 1400E. One discreet area of near surface low resistivity occurs at the north end line of 800E and numerous other discreet areas of low to moderate resistivity occur throughout the grid. These areas lower resistivity do not in general correspond to the areas of high chargeability. The area of low resistivity on the south end of line 2000E, however, does coincide with the location of the higher gold values obtained in the rock samples.

10.2.2 Magnetic Survey

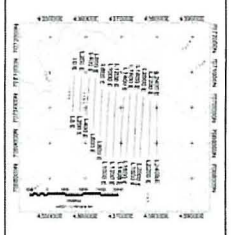
The main feature of the 2006 ground magnetic survey over the Toby Zone is the strongly magnetic signature on the east and south part of the grid area (Figure 11). Further interpretation remains to be done, but this feature could be reflecting unexposed magnetic intrusive body at depth.

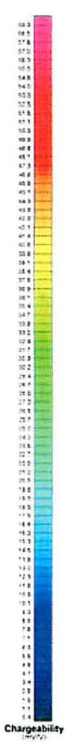


STACKED MODELLED CHARGEABILITY SECTIONS

Dipole-Dipole Array

Modified Pole-Dipole Array





Scale 1:4000

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
SCHEELITE DOME PROPERTY, TOBY ZONE
STACKED CHARGEABILITY MODELS

NTS: 115 P/09 & 115 P/16 — Mining District: Mayo
Grid: Local — Job: KRX-06-02 VT
Date: Aug 10, 2006 — Figure

AURORA GEOSCIENCES LTD.

Figure 9

Figure 10

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
SCHEELITE DOME PROPERTY, TOBY ZONE
STACKED RESISTIVITY MODELS

Scale 1:4000

Resistivity (Ohm-metres)

STACKED MODELLED RESISTIVITY SECTIONS

Dipole-Dipole Array

Modified Pole-Dipole Array

REFERENCE FIELD : 57,500 nT
INSTRUMENT : GEM GSM-19T (GPS)
GRIDDING ALGORITHM : MINIMUM CURVATURE
GRID CELL SIZE : 25 m
FILTER : DESPIKED, WIDTH: 1, THRESHOLD: 50 nT
GRID HANNING FILTER : 3 PASSES
DATA FILE : Scheelite Dome 2006 Mag.gdb
OPERATOR : GF
STATION SEPARATION : 12.5 m
LINE-KM SURVEYED THIS SHEET : 19.9 km
DATES SURVEYED : July 11-14, 2006

Trench 1
Trench 2
Trench 3
Trench 4
Trench 5
Trench 6
Trench 7
Trench 8
266 m
90 m
598 m
268 m

0 250 500
metres

0 125 250
metres

Vertical Magnetic Gradient
(RT/m)

Scale 1:5000
100 0 100 200 300
metres
NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.
SCHEELITE DOME PROPERTY, TOBY ZONE
CALCULATED VERTICAL DERIVATIVE
COLOUR CONTOURED MAP

Loc: Yukon Territory
NTS Sheet: 115P/09 & 115P/16
Proj: UTM Zone 8N
Job: KRX-06-03-YT

Date: Aug 07, 2006
Mining District: Mayo
Datum: NAD27 (Yukon)
Drawn by: DH
Appendix F

AURORA GEOSCIENCES LTD.

Figure 11

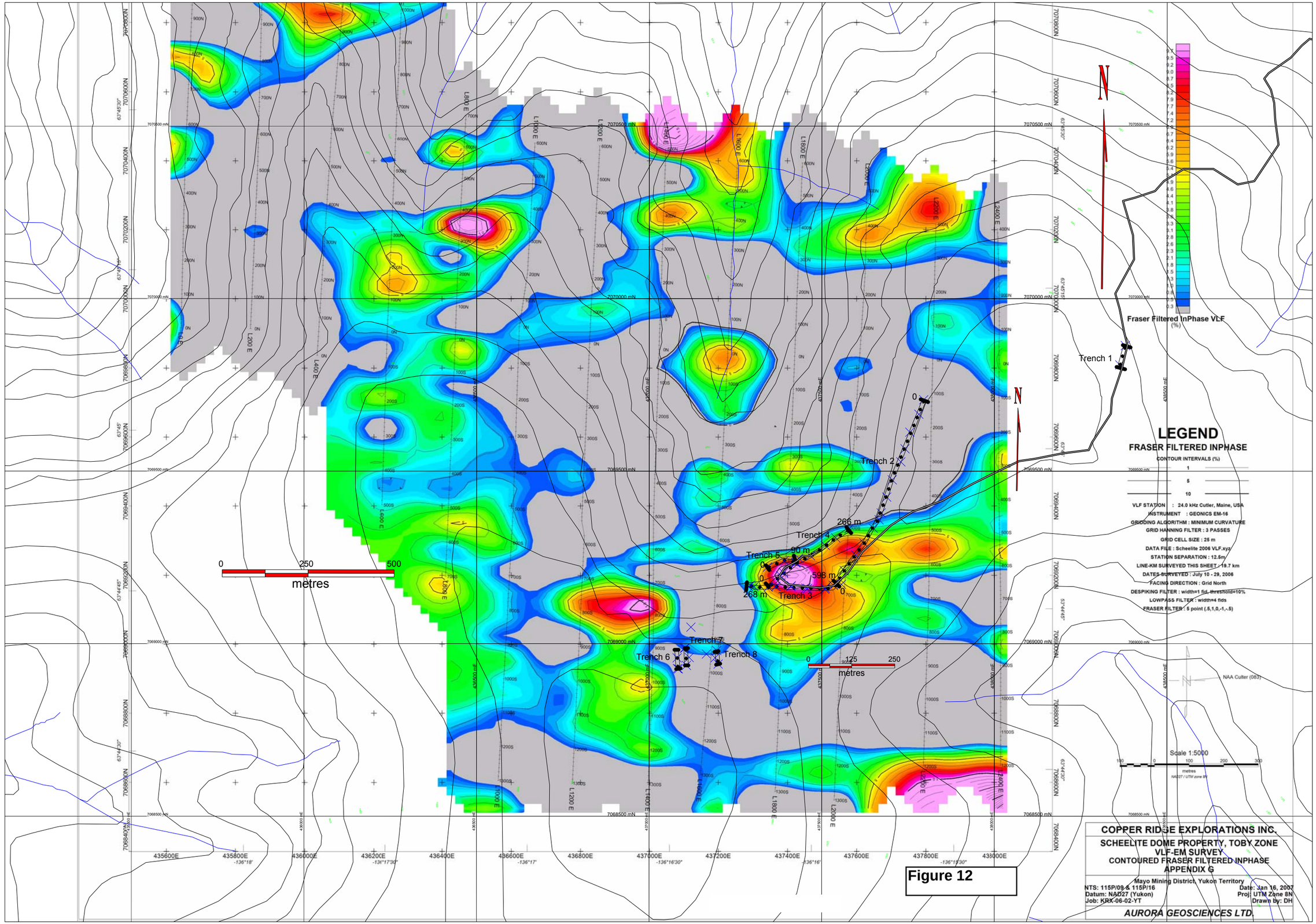

Fraser Filtered InPhase VLF (%)
Trench 1
Trench 2
Trench 3
Trench 4
Trench 5
Trench 6
Trench 7
Trench 8
266 m
80 m
598 m
268 m
0
250
500
metres
0
125
250
metres
N
LEGEND
FRASER FILTERED INPHASE
CONTOUR INTERVALS (%)
1
5
10
VLF STATION : 24.0 kHz Cutler, Maine, USA
INSTRUMENT : GEONICS EM-16
GRIDDING ALGORITHM : MINIMUM CURVATURE
GRID HANNING FILTER : 3 PASSES
GRID CELL SIZE : 25 m
DATA FILE : Scheelite 2006 VLF.xyz
STATION SEPARATION : 12.5m
LINE-KM SURVEYED THIS SHEET : 19.7 km
DATES SURVEYED : July 10 - 29, 2006
FACING DIRECTION : Grid North
DESPIKING FILTER : width=1 fid, threshold=10%
LOWPASS FILTER : width=4 fids
FRASER FILTER : 5 point (.5,1,0,-1,-.5)
NAA Cutler (083)
Scale 1:5000
metres
NAD27 / UTM zone 8N
COPPER RIDGE EXPLORATIONS INC.
SCHEELITE DOME PROPERTY, TOBY ZONE
VLF-EM SURVEY
CONTOURED FRASER FILTERED INPHASE
APPENDIX G
Mayo Mining District, Yukon Territory
NTS: 115P/09 & 115P/16
Datum: NAD27 (Yukon)
Job: KRX-06-02-YT
Date: Jan 16, 2007
Proj: UTM Zone 8N
Drawn by: DH
AURORA GEOSCIENCES LTD.

Figure 12

10.2.3 VLF Survey

VLF (very low frequency) surveys are sensitive to a wide variety of conductive to semi conductive features in the earths surface. They are therefore useful in defining geologic structures and contacts as well as conductive metallic mineralization. An initial evaluation of the VLF data at the Toby zones shows that a strongly to moderately conductive feature is coincident with the mineralization found in trenches 4 and 5 and occurs just up hill from the strong coincident Au-As-Bi soil anomaly (Figure 12). This structure trends just north of east for at least one kilometre and likely reflects a fault or vein hosted metallic mineralization such as arsenopyrite.

The survey showed several other isolated areas of high conductivity, but these anomalies have yet to be correlated with known mineralization.

10.3 Soil Sampling

The soil sampling was completed on the same grid as the geophysical survey. The 200 m spaced lines of the grid were placed to fall between the 200 m space lines of the 1999 survey such that the Toby zone is now covered with a grid of 100 m spaced lines. Samples were collected at 50 m spaced stations, except in the areas of previous anomalies, where samples were collected at 25 m spacings. Sample locations with sample characteristics are included in Appendix A and analytical results are included in Appendix B

The results of the soil sampling essentially confirmed and further defined the anomalous results from the 1999 survey. Values are locally moderately to strongly anomalous in Au and Sb and locally strongly to very strongly anomalous in As and Bi. Bubble plots are shown for gold, arsenic, bismuth and antimony on figures 13, 14, 15 and 16 respectively.

The strong coincident Au-Bi-As anomaly at the headwaters of Toby creek was confirmed and slightly expanded. The coincident Au-As-Bi anomaly on the west side of the drainage immediately west of Toby creek was also confirmed and expanded.

A review of the overall pattern of the anomalous Au, As and Bi values suggest that the values are grouped into 3 northeast trending zones. Whether this is a function of structure, stratigraphy or overburden characteristics remains to be determined.

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

N

0 250 500
metres

Toby Zone 2006 Soils Au ppb

- 95 to 301 (97 Percentile)
- 52 to 95 (90 Percentile)
- 25 to 52 (75 Percentile)
- \+ 0 to 25

Toby Zone 1999 Soils Au ppb

- 80 to 800 (97 percentile)
- 50 to 80 (90 Percentile)
- 25 to 50 (75 percentile

Trench 1
0
Trench 2
260 m
Trench 4
90 m
Trench 5
0
0
598 m
0
268 m
Trench 3
Trench 7
Trench 6
Trench 8

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone Soil Geochemistry
Au ppb

Date:7/3/2007	
Author: JGD	
Office:	
Drawing:	
Scale: 1:15000	Projection: UTM Zone 8 (NAD 27 for Canada)

Figure 13

7071000 mN

7070000 mN

7069000 mN

437000 mE

438000 mE

436000 mE

N

Toby Zone 2006 Soils As ppm

- 2,094 to 6,450
- 1,180 to 2,094
- 600 to 1,180
- 0 to 600

Toby Zone 1999 Soils As ppm

- 2,280 to +10,000
- 1,180 to 2,280
- 582 to 1,180
- 0 to 582

0 250 500

metres

Trench 1

Trench 2

Trench 3

Trench 4

Trench 5

Trench 6

Trench 7

Trench 8

0

260 m

90 m

0

598 m

0

0

268 m

Copper Ridge Explorations Ltd.	
Date:7/3/2007	Scheelite Dome Project Toby Zone Soil Geochemistry As ppm
Author: JGD	
Office:	
Drawing:	
Scale: 1:15000	Projection: UTM Zone 8 (NAD 27 for Canada)

Figure 14

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

N

0 250 500

metres

Toby Zone Soils Bi ppm

- 11 to 611 (97 percentile)
- 6.5 to 11 (90 percentile)
- 3.3 to 6.5 (50 percentile)
- 0 to 3.3

Toby Zone 1999 Soils Bi ppn

- 10 to 100 (97 percentile)
- 6 to 10 (90 percentile)
- 2 to 6 (50 percentile)
- 0 to 2

Trench 1

Trench 2

Trench 3

Trench 4

Trench 5

Trench 6

Trench 7

Trench 8

0

260 m

90 m

598 m

68 m

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone Soil Geochemistry
Bi ppm

Date:7/3/2007
Author: JGD
Office:
Drawing:
Scale: 1:15000
Projection: UTM Zone 8 (NAD 27 for Canada)

Figure 15

7071000 mN

7070000 mN

7069000 mN

436000 mE

437000 mE

438000 mE

N

0 250 500
metres

Toby Zone 2006 Soils Sb ppm

- 30.9 to 169
- 14.1 to 30.9
- 6.7 to 14.1
- 0 to 6.7

Toby Zone 1999 Soils Sb ppm

- 28 to 122
- 14 to 28
- 8 to 14
- 0 to 8

Trench 1
0
Trench 2
260 m
Trench 4
90 m
Trench 5
0
598 m
0
268 m
Trench 3
0
Trench 7
Trench 6
Trench 8

Copper Ridge Explorations Ltd.

Scheelite Dome Project
Toby Zone Soil Geochemistry
Sb ppm

Date:7/3/2007
Author: JGD
Office:
Drawing:
Scale: 1:15000
Projection: UTM Zone 8 (NAD 27 for Canada)

Figure 16

10.4 Trenching Program

The above programs were followed up with 1358 m of excavator trenching and sampling in 8 trenches at the upper southeast end of the Toby Cirque. Significant results from the trenching and sampling program are summarized in Table 9.9.1 and Trench locations are shown on Figures 11 and 12. It is apparent that the best trenching target on the Toby Zone was over the cluster of anomalous samples on the upper southeast side of the Toby cirque.

Compilation and interpretation of the earlier conducted geophysical surveys and prospecting, mapping, and rock/soil sampling focused the trenching program to areas of coincident gold in soil and IP anomalies. The 2006 trenching area underlain by a poorly exposed sequence of interbedded, foliated, variably quartz-rich sericite phyllite and dirty quartzites with lesser limey quartzite horizons. A less than five metre wide dark grey fine-grained biotite quartz porphyry dyke is exposed cutting the layered sedimentary units (in the vicinity of trench #2). Bedrock exposure is poor and limited to talus scree, felsemeer and rare 1-3 metre wide outcrops along the southeast rim of Toby Creek cirque. Recessive gullies locally represented the surface expression of northwest/southeast trending fault systems later exposed in trenching as limonitic gouge and intense fracture zones especially at the south end of trench #2 and eastern end of trench #3.

Mineralization consists of irregular zones of silicification with narrow frothy quartz and coarse-grained arsenopyrite stringers and veins or poddy disseminations along foliation within the phyllite unit (commonly at the lower contact with the quartzite). Both vein and disseminated styles of mineralization tend to be concordant with S_2 foliation with generally narrow (cm scale) quartz ± arsenopyrite stringers locally crosscutting the foliation. Abundant scorodite, lesser realgar and local bismuthinite were observed in these mineralized areas as well as a thick coating of dull black manganese along the fracture surfaces of the mineralized unit. Typically the strongly mineralized areas were flanked by more widespread carbonate alteration that may represent a favourable reactive limey host.

Due to the poddy discontinuous nature of the exposed mineralization and the fractured nature of the host rock, clear orientations of the mineralization were difficult to define. Zones in excess of 20 metres in width were outlined during the trenching program. Trench #2 exposed a greater than 10m zone of significant gold and coincident arsenic and bismuth in an area of fractured rusty phyllite with 1cm wide cockade quartz stringers with cores of massive arsenopyrite as well as disseminated arsenopyrite along foliation. Intense hematite and limonite envelopes flank the quartz and arsenopyrite stringers and bismuthinite crystals were noted in association with the arsenopyrite along foliation. A major fault system was unearthed at the south end of Trench #2 and the east half of trench #3 as unconsolidated limonitic gouge and intensely fractured and altered rock with discontinuous arsenopyrite and quartz stringers and veins. A 20 metre long zone of mineralized quartzite was exposed towards the western end of trench #3 and consists of arsenopyrite and quartz veins in siliceous quartzite with abundant scorodite and limonite. Possible strike of mineralization interpreted from the orientation

of the sharp margins of a prominent 40 cm wide resistive knob of arsenopyrite/quartz vein at 217 metres along the trench is 060/30NW.

Trench #4 yielded significant gold values in quartzite with disseminated arsenopyrite (locally coarse grained). Two grab samples (400904 and 400906) collected at 30 m and 125 m respectively returned 1.88 gm/t and 2.47 gm/t Au from blebby coarse arsenopyrite collected from green oxidized quartzites with some red limonite staining. The northern section of this trench cut across a recessive gully and exposed unconsolidated sericitized phyllite and limonitic/hematized clay gouge. This fault zone likely correlates with the sheared material found in the eastern end of trench #3.

Trenches #6-8 exposed an east-west trending quartz/arsenopyrite/pyrite vein system as well as sulphide poor locally auriferous quartz vein fragments and boulders. Permafrost was encountered in trenches 7 and 8 due to the steep north facing exposure and therefore bedrock was not found at the bottom of the trenches. Mineralization consists of frothy porous scorodite and arsenopyrite in a quartz matrix hosted in a quartzite grit unit. Mineralized quartz/arsenopyrite veins and alteration appears along the foliation/bedding contact between the mica-rich phyllite and gritty quartzite units with bedding attitudes recorded as 086/36S.

TABLE 10.2 - TOBY ZONE SIGNIFICANT TRENCH RESULTS

Trench #	Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Au ppb (ICP-MS)	As ppm	Sb ppm	Bi ppm	Au g/t FA
06-1	NSV										
06-2	400951	596	596	0	TR06-2	grab	2695.6	>10000	309.2	606.1	2.89
06-2	400952	592	594	2	TR06-2	chip	4233.3	>10000	498.6	1509	4.21
06-2	400570	290.5	291.5	1	TR06-2	chip	717.5	>10000	19.5	21.9	0.71
06-2	400571	290.5	290.5	0	TR06-2	grab	8014.1	>10000	316.8	192.5	7.48
06-2	400572	288	290.5	2.5	TR06-2	chip	55.2	1109	2.1	4.9	
06-2	400573	286.5	288	1.5	TR06-2	chip	136.3	3314.4	4.4	10.7	
06-2	400574	284	286.5	2.5	TR06-2	chip	8.2	438.9	1.4	1	
06-2	400576	282	284	2	TR06-2	chip	567.1	3235.2	3.7	35.2	0.58
06-2	400577	280	282	2	TR06-2	chip	1289.3	>10000	22.1	68.1	1.26
06-03	400613	8	11	3	TR06-3	chip	495.7	9440.7	14.3	61.5	
06-03	400614	11	14	3	TR06-3	chip	128.6	2649.9	8.8	16.1	
06-03	400661	112	115	3	TR06-3	chip	2010.1	>10000	62.2	415.9	1.81
06-03	400662	115	115	0	TR06-3	grab	14925.6	>10000	694.1	>2000	11.75
06-03	400670	130.5	130.5	0	TR06-3	grab	3468	>10000	247.6	506.1	3.05
06-03	400671	131	132	1	TR06-3	chip	736	>10000	40.3	105.1	0.75
06-03	400672	132	135	3	TR06-3	chip	2758.1	>10000	182.1	427.4	2.28
06-03	400710	203	203	0	TR06-3	grab	5440.8	>10000	282.1	1057.5	4.59
06-03	400711	203	205	2	TR06-3	chip	9.6	907.9	1.8	2.6	
06-03	400712	205	207	2	TR06-3	chip	41.6	1260.4	2.7	8.5	
06-03	400713	207	209	2	TR06-3	chip	336.7	>10000	49	173.7	
06-03	400714	209	210.5	1.5	TR06-3	chip	1258.5	>10000	99.5	354.7	1.24
06-03	400715	210.5	211.5	1	TR06-3	chip	10	1156.8	2.4	3	

Trench #	Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Au ppb (ICP-MS)	As ppm	Sb ppm	Bi ppm	Au g/t FA
06-03	400716	211.5	213	1.5	TR06-3	chip	1878	>10000	201.8	931.3	1.88
06-03	400717	213	215	2	TR06-3	chip	72.5	6683.5	24.8	46.2	
06-03	400718	215	216	1	TR06-3	chip	68.7	7874.7	26.1	34.2	
06-03	400719	216	217	1	TR06-3	chip	60	>10000	30.5	21.3	
06-03	400720	217.5	217.5	0	TR06-3	grab	7565.7	>10000	567.8	1866.6	6.65
06-03	400721	217.5	217.5	0	TR06-3	grab	6150.2	>10000	484.6	1350.6	5.62
06-03	400722	217	218	1	TR06-3	chip	8933.1	>10000	192.8	1484.8	8.1
06-03	400723	218	219	1	TR06-3	chip	182.1	>10000	38.8	43.1	
06-03	400724	219	220	1	TR06-3	chip	1352.9	>10000	83.7	312.9	1.31
06-04	400809	37	40	3	TR06-4	Chip:	4.4	456	2.3	1	
06-04	400810	41.5	41.5	0	TR06-4	grab	5212.1	>10000	303.2	889.6	4.15
06-04	400811	40	43	3	TR06-4	Chip	16.4	405	2	1.1	
06-04	400904	Al's Grab	30		TR06-4	grab	2112.9	>10000	418.7	244.5	1.88
06-04	400906	Al's Grab	125		TR06-4	grab	2417	>10000	121.9	288.2	2.47
06-05	NSV										
06-06	400931	27	27	0	TR06-6	grab	737.9	>10000	38.1	132.9	0.79
06-07	405066	21.5	21.5	0	TR06-7	grab	208.7	>10000	16.1	171.3	
06-07	405067	21	23	2	TR06-7	chip	130.5	>10000	21.9	93.3	
06-07	405068	23	23	0	TR06-7	grab	300.6	>10000	21	51.1	
06-07	405069	23	24	1	TR06-7	chip	176.9	>10000	11.8	17.9	
06-07	405070	24.3	24.3	0	TR06-7	grab	728.9	>10000	52.9	460.6	0.71
06-07	405071	23	24	1	TR06-7	chip	12.5	1195.3	7.8	11.8	
06-07	405072	23.5	23.5	0	TR06-7	grab	321.3	>10000	43.5	316.2	
06-07	405073	24	25	1	TR06-7	chip	29.4	2025.6	11	15.7	
06-07	405074	25	26	1	TR06-7	chip	58.5	>10000	12.7	28.7	
06-07	405076	26	27	1	TR06-7	chip	15.6	1694.3	11.5	7.8	
06-07	405077	26	26	0	TR06-7	grab	599.5	>10000	33	357.2	0.59
06-07	405078	26.5	26.5	0	TR06-7	grab	2.7	282.1	3.3	1.1	
06-07	405079	27	28	1	TR06-7	chip	22	487.3	10	10.4	
06-07	405080	28	29	1	TR06-7	chip	461.5	>10000	13.9	40.1	
06-07	405081	29	30	1	TR06-7	chip	139.8	2632.5	10.3	2.6	
06-07	405089	40	40	0	TR06-7	grab	665.7	>10000	346.7	136.3	0.69
06-07	405093	43.5	44.5	1	TR06-7	chip	495.6	>10000	206.7	9.2	
06-07	405094	43.5	43.5	0	TR06-7	grab	867.9	>10000	412.2	6.4	0.89
06-08	405106	14	14	0	TR06-8	grab	4460	>10000	327.5	1424.5	4.29
06-08	405107	17	18	1	TR06-8	chip	1453.9	>10000	85.3	444.7	1.37
06-08	405108	18	20	2	TR06-8	chip	334.6	>10000	15	105.2	

11.0 DRILLING

No drilling was undertaken during the 2006 field season.

12.0 SAMPLING METHOD AND APPROACH

The soil samples were collected in gussetted “Kraft” paper sample bags with a mattock from the “B” or upper “C” soil horizons. Sample depth was generally between 10 and 30 centimetres. Good soil was encountered at most sites, except were extensive talus covered occurred. Generally about 500 grams of material was collected. All soil samples were identified with a unique sample number using a booklet with a two part sample tag. One part of the tag with the number went in the sample bag while the other part of the tag, also with the number, remained in the booklet and was marked with the GPS coordinates of the sample. The colour, depth and texture of the samples and the nature of the sample site location were described in a separate notebook. Samples were dried at camp prior to packaging for shipment to Vancouver.

The rock sampling conducted during the first phase of the 2006 program consisted of the collection of grab samples from talus and local outcrop. The samples, generally weighing between 1 and 3 kilograms, were collected in industry standard plastic sample bags. The sampling conducted during the trenching program consisted of the collection of 1 to 3 m chip samples along the base of the trench. Samples generally weighed between 3 and 8 kilograms. All rock samples were identified with unique sample number using a booklet with a two part sample tag. One part of the tag with the number went in the plastic sample bag and the bag sealed with a plastic “zap strap.” The other part of the tag, also with the number, remained in the booklet and was marked with either the GPS coordinates of the sample or the trench location of the sample In most cases, the sample was described by a geologist.

13.0 SAMPLE PREPARATION, ANALYSES AND SECURITY

All soil and rock samples were analyzed by Acme Analytical using the 1DX ICP-MS analytical method on a 15 gram sub-sample. A more precise description of this method is included with the analytical results in Appendix B.

14.0 DATA VERIFICATION

At this early stage of the prospecting program at the Toby Zone, a rigorous system of quality control was not put in place. One standard sample and one blank sample was included with the shipment of rocks to Acme Analytical. The analysis of these quality control samples was within acceptable limits. As well, Acme Analytical employs a system of in-house quality control including the repeat of sample analysis, the analysis of standards and the inclusion of blank material. The results of these analyses were included in the results sent to Copper Ridge and were within acceptable limits.

15.0 INTERPRETATION AND CONCLUSIONS

Exploration on the Scheelite Dome property over the last 15 years has targeted Tombstone Plutonic Suite (TPS) style gold mineralization. Significant work programs including five separate drilling programs (33 core holes 4292 m and 17 RC holes 1035 m); airborne magnetic coverage over most of the property, extensive trenching and soil and rock sampling and IP surveys have outlined a number of attractive targets in a number of zones. The Harvey Ridge Zone, the Rudolph Creek Zone and the Tom Zone have been drill tested and shown to host potentially economic gold mineralization. The Toby Zone remains to be drill tested and a number of other target areas (e.g. the Héon Zone, Bennett Creek area, prospects along Highet Creek) are deserving of further work.

The 2006 soil sampling program at the Toby Zone confirmed, clarified and expanded the results of the 1999 survey. Grouping of the anomalous coincident gold, arsenic and bismuth values suggests that there is a possible northeast trending control to the mineralization. The survey also expanded the coincident anomaly centred on Line 6E on the northwest part of the grid.

The 2006 prospecting program at the Toby Zone confirmed that the strong coincident gold arsenic and bismuth soil anomaly at the headwaters of Toby creek is reflecting local areas of gold mineralization in rock. This was further confirmed by the trenching program which uncovered several quartz-arsenopyrite veins hosted in strongly altered sediments that contained highly anomalous to economic grade gold mineralization.

The geophysical program identified several anomalous patterns worthy of follow up. The VLF survey demonstrated that an east trending conductive structure is associated with the mineralization. This feature has a strike length of at least a kilometre and could represent a conductive fault or a vein hosting metallic mineralization such as arsenopyrite. The IP survey identified 3 strongly conductive zones in the centre of the grid. The most southerly of these is known to be associated with disseminated pyrite around auriferous quartz veins but source for the other two remains undefined as they occur at depth in areas of very little rock exposure. The magnetic survey showed that a strongly magnetic body occurs just to the south of the mineralization identified in the trenching. This feature could represent a buried intrusion at depth that could be the heat and metal source of the mineralization observed at surface.

16.0 RECOMMENDATIONS

Further work is recommended at the Toby Zone. As a first phase, this work should include interpretation of the geophysical data, followed by detailed prospecting and mapping to attempt to identify and sample any surface manifestations of the observed geophysical anomalies. Surface mechanical trenching should then be completed over areas with defined mineralization and over priority geophysical targets. A recommended budget for the first phase is $75,000.

A non-contingent second phase program should include 1000 m of drilling to test un-exposed targets identified by the geophysical program and to test targets identified in the first phase program. A recommended budget for this program is $300,000

In addition, it must be emphasized that many of the recommendations put forward by Stewart Harris in 2000 and 2002 and Al Doherty in 2003 regarding other parts of the Scheelite Dome property have never been carried out. In order to most efficiently move the property forward as a whole, these recommendations should be incorporated into any proposed work at the Toby zone. If such is the case, the proposed budget figures should be revised accordingly.

17.0 STATEMENT OF COSTS

Labour **Arum Geological**	J. van Randen, Geologist: 51.5 days @ $625 per day	$	32,187.50
	Milada Pardovicova, Prospector: 38.5 days @ $300 per day		11,550
	Al Doherty, Geologist: 10 days @ $500.00 per day		10,000
	Jordan Marr, Sampler: 48 days @ $270 per day		12,960
	Paul Siggers, Sampler: 42 days @ $270 per day		11,340
	Rickey Breger, Jr. Geologist: 14 days @ $375 per day		5,250
	Louise Levesque, Sampler, First Aid: 12 days @ $375 per day		4,500
	Subtotal Labour		**$87,787.50**
Geochemistry **Acme Analytical**	456 Soil samples @ $15.77 per sample		7,191.12
	143 Rock Samples (prospecting) @ $19.08 per sample		2,768.16
	657 Rock Samples (trenching) @ 19.08 per sample		12,535.56
	Subtotal Geochemistry	**$**	**22,494.84**
Geophysics **Aurora Geosciences**	Line cutting: 21 km @$1,582.38 per line km		33,230.00
	Surveys: 21 km @$2,365.33 per line km		65,672.00
	Logistal Support		12,136,60
	Data Analysis		2,117.50
	Subtotal Geophysics	**$**	**113,215.50**
Living Expenses	216 man days @ $35.00 per man day		7,560
	Subtotal Living Expenses	**$**	**7,560.00**
Air Support **Trans North**	Helicopter: 11.5 hours @ $1,123.68 per hour		12,922.28
	Subtotal Air Support	**$**	**12,922.28**
Trench / Road **Wilf's Contracting**	D8: 22.5 hours @ $200 per hour		4,500.00
	Excavator: 84.4 hours @ $126 per hour		10,647
	Mob / Demob: 13 hours @ $120 per hour		1,560
	Subotal Trench / Road		**16,707**
Report **Copper Ridge**	Report Writing		5,000.00
	Subtotal Report Writing	**$**	**5,000.00**
TOTAL		**$**	**265,687.12**

Cost Breakdown

Soil Sampling	Cost
Labour	$12,150.00
Analysis	$7,191.12
Accommodation	$1,575.00
Air Support	$4,307.43
Report	$1,250.00
Total	$26,473.55
Cost per soil sample	$58.06

Prospecting	Cost
Labour	$27,643.75
Analysis	$2,768.16
Accommodation	$2,248.75
Air Support	$4,307.43
Report	$1,250.00
Total	$38,218.09
Cost per prospecting sample	$267.26

Geophysics	Cost
Line cutting and surveying	$98,902.00
Logistical support	$12,136.60
Data analysis	$2,117.50
Air Support	$4,307.43
Report	$1,250.00
Total	$118,713.53
Cost per line kilometer	$5,653.03

Trenching	Cost
Labour	$47,993.75
Analysis	$12,535.56
Accommodation	$3,736.25
Excavator	$10,647.00
mob /demob	$780.00
Report	$1,250.00
Total	$76,942.56
Cost per meter	$56.66

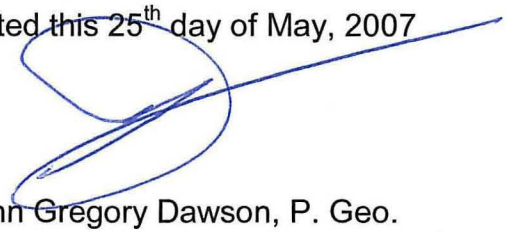
Road Building	Cost
D8	$4,500.00
Mob / demob	$780.00
Total	$5,280.00
Cost per kilometer	$1,552.94

18.0 STATEMENT OF QUALIFICATIONS

I, John Gregory Dawson, do hereby declare that;

1. I am currently employed as Vice President Exploration for Copper Ridge Explorations Inc. of 500 - 625 Howe Street Vancouver, British Columbia V6C 2T6.
2. I graduated with a Bachelor Science degree from the University of British Columbia in 1987 and a Masters of Science degree from Queens' University in 1991.
3. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia, Registration Number 19882.
4. I have worked as a geologist for a total of 20 years since graduation from University, and prior to graduation, as a student and or geotechnician for a period of 11 additional years.
5. I have read the definition of "Qualified Person" set out in National Instrument 43-101("NI 43-101") and certify that by reason of my education, affiliation with a professional association and past relevant work experience, I fulfil the requirements to be a "Qualified Person" for the purposes of NI 43-101.
6. I am not aware of any material fact or material change with respect to the subject matter of this report, the omission to disclose which makes this report misleading.
7. I am not independent of the issuer applying all tests in Section 1.5 of NI 43-101 in that I am an employee of Copper Ridge Explorations Inc and hold shares and options in the Company.

Dated this 25th day of May, 2007



John Gregory Dawson, P. Geo.

19.0 REFERENCES

Baker, T. (2003): Intrusion-Related Gold Deposits: Explorable Characteristics; in Gold Short Course Notes presented at the 2003 Cordilleran Exploration Roundup, Vancouver, B.C.

Baker, T., Lang, J.R. and Mortensen, J.K. (1998). Characteristics of Mineralization Associated with Intrusions of the Mid-Cretaceous Tombstone-Tungsten Magmatic Belt; Mineral Deposit Research Unit, Department of Earth and Ocean Sciences, University of British Columbia.

Caulfield, D.A. (1999): 1998 Geological, Geochemical, Geophysical and Diamond Drilling Program on the Scheelite Dome Property; Report submitted for assessment credit.

Doherty, A. (2003): Report on the Tom Zone Drilling Program Scheelite Dome Project. Prepared for Golden Patriot Mining Inc.

Emond, D.S. (1992): Petrology and Geochemistry of Tin and Tungsten Mineralized Plutons, McQuesten River region, central Yukon; in Yukon Geology v. 3; Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, p. 167-195.

Harris, S. (2000): 1999 Geological, Geochemical, Geophysical and Diamond Drilling Report on the Scheelite Dome Property; Private report prepared for Copper Ridge Explorations Inc.

Harris, S (2002): Summary Report on the Scheelite Dome Project. Prepared for Yardley Capital Inc.

Hart, C.J.R., Baker, T., Burke, M. (2000): New Exploration Concepts for Country-Rock-Hosted, Intrusion-Related Gold Systems: Tintina Gold Belt in Yukon; in The Tintina Gold Belt: Concepts, Exploration, and Discoveries Special Volume 2; B.C. and Yukon Chamber of Mines, pp 145-172.

Hart, C.J.R., McCoy, D.T., Goldfarb, R.J., Smith, M., Roberts, P., Hulstein, R., Bakke, A.A., Bundtzen, T.K. (2002): Geology, Exploration, and Discovery in the Tintina Gold Province, Alaska and Yukon; in Society of Economic Geologists Special Publication 9, 2002, pp. 241-274.

Hulstein, R. and Zuran, R. (1996): Assessment Report on 1996 Geophysical Work at the SC 1-525 Claims; Private report prepared for Kennecott Canada Exploration Inc.

Hulstein, R. and Zuran, R. (1997): Assessment Report on 1997 Drilling and Trenching Work, Scheelite Dome Project; Private report prepared for Kennecott Canada Exploration Inc.

Mair, J.L., Hart, C.J.R., Goldfarb, R.J., O'Dea, M., Harris, S. (2000): Geology and Metallogenic Signature of Gold Occurrences at Scheelite Dome, Tombstone Gold Belt; Yukon Territory, in Yukon Exploration and Geology 1999; Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada. pp 165-176.

Mortensen, J.K., Lang, J.R., Poulsen, K.H. and Murphy, D.C. (1997): Geology and Metallogeny of the Tombstone Plutonic Suite: A Progress Report; in Regional and System-scale Controls on the Formation of Copper and/or Gold Magmatic-hydrothermal Mineralization; Mineral Deposit Research Unit, Department of Earth and Ocean Sciences, University of British Columbia.

Murphy, D.C., (1997): Geology of the McQuesten River Region, Northern McQuesten and Mayo Map Areas, Yukon Territory (115P/14,15,16; 105M/13,14); Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, Bulletin 6, 122 pp.

Murphy, D.C. and Héon, D. (1995): Geology and Mineral Occurrences of Seattle Creek Map Area (NTS 115P/16), Western Selwyn Basin; in Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, p. 59-71.

Murphy, D.C. and Héon, D. (1996): Geological Map of Sprague Creek Map Area (NTS 115P/15), Western Selwyn Basin; Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada, Open-File 1996-3, 1:50,000 scale.

O'Dea, M.G. (1999): Structural Framework and Targeting Strategy for the Scheelite Dome Area, Yukon Territory; Private report prepared for Copper Ridge Explorations Inc.

O'Dea, M.G., Carlson, G., Harris, S., Fields, M. (2000): Structural and Metallogenic Framework for the Scheelite Dome Deposit, Yukon Territory; in The Tintina Gold Belt: Concepts, Exploration, and Discoveries Special Volume 2; B.C. and Yukon Chamber of Mines, pp 115-129.

Power, M.A. (1998): Induced Polarization Survey at the Scheelite Dome Property, Mayo District, Yukon Territory; Private report prepared for La Teko Resources Ltd.

Power, M.A. (1999): Inversion of Induced Polarization Data from the Scheelite Dome Property, Mayo Area, YT; Private report prepared for Copper Ridge Explorations Inc.

Wall, V. (1999): Pluton-related Thermal Aureole Gold; Short course presented at the Yukon Geoscience Forum, November 20, 1999.

Yukon Minfile; Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada.

APPENDIX A - SAMPLE LOCATIONS AND DESCRIPTIONS

Soil Sample Descriptions

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%c	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD 27	UTM	8V	437407	7069865	1438.7	L18E050N	404749	25	l.brown	30	S	35	5	15		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437423	7069940	1293.3	L18E100N	404750	30	l.brown	30	S	35	5	15		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437431	7069993	1286.9	L18E150N	404751	25	l.brown	40	S		5	15	next to talus slope	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437410	7070033	1333.5	L18E200N	404752	25	l.brown	40	S		5	25	thick moss,rooty	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437423	7070098	1286	L18E250N	404753	30	l.brown	40	S	35	20	15		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437432	7070117	1290.5	L18E300N	404754	35	l.brown	40	S	40	20	10	quartz chips	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437438	7070170	1292	L18E350N	404755	30	l.brown	40	S		20	10	next to talus slope	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437436	7070216	1292	L18E400N	no sample								talus slope	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437454	7070276	1255.5	L18E450N	404756	25	l.brown	50	N		15	10	talus slope	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437438	7070317	1268.3	L18E500N	404757	25	l.brown	50	W		15	20		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437448	7070370	1250.3	L18E550N	404758	30	d.brown	50	NW		10	10		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437440	7070421	1277.1	L18E600N	404759	25	red brown	40	N		10	10		Scheelite	Toby	June 27,2006
						STANDARD CDN/CGS/1	404760											
NAD 27	UTM	8V	437419	7069778	1314.9	L18E050S	404761	35	d.brown	40	N		15	10	mica	Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437415	7069732	1327.7	L18E100S	404762	35	d.grey,brov	50	SW		10	15		Scheelite	Toby	June 27,2006
NAD 27	UTM	8V	437425	7069717	1379.8	L18E150S	404763	35	d.brown	60	SW	30	15	15		Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437417	7069643	1338.7	L18E200S	404764	25	d.brown	60	SW	30	15	20		Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437411	7069596	1356.7	L18E250S	404765	20	l.brown	60	SW	30	5	15		Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437413	7069546	1369.2	L18E300S	404766	30	l.brown	60	SW	30	10	15		Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437405	7069497	1392.6	L18E350S	404767	20	l.brown	5	SW	30	10	10	mica,mud,sample fi	Scheelite	Toby	June 28,2006
			437407	7069447		L18E400S	404768	30	goldish,ora	20	SW	30	10	10	mica	Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437402	7069396	1408.8	L18E450S	404769	30	goldish,ora	20	NW		15	10	mica	Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437399	7069349	1417.9	L18E500S	404770	35	goldish,ora	15	NW		15	15	mica,red rock chips	Scheelite	Toby	June 28,2006
NAD 27	UTM	8V	437396	7069307	1457.9	L18E550S	404748	30	rusty	10	N	45	25	10		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437403	7069270	1511.5	L18E600S	no sample				N	45			snow patch	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437392	7069213	1510.6	L18E650S	404747	30	rusty	5	N	45	20	15		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437388	7069164	1514.6	L18E700S	404746	30	l.brown	5	N	45	5	10	mud	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437384	7069110	1524.9	L18E750S	404745	35	rusty	30	N		10	5	mud	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437384	7069060	1520.6	L18E800S	404744	35	rusty	30	N		10	5	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437382	7069017	1537.4	L18E850S	404743	55	rusty	20	N		10	5		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437380	7068968	1539.2	L18E900S	404742	70	rusty	30	NE		15	5	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437378	7068919	1544.4	L18E950S	404740	55	l.brown	40	NE		15	5		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437378	7068919	1544.4	L18E950S	404741	55	l.brown	40	NE		15	5	DUPLICATE of 404	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437374	7068872	1547.5	L18E1000S	404739	40	rusty	40	NE		10	5	very rusty,orange	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437372	7068824	1548.1	L18E1050S	404738	30	d.brown	50	NE		10	10		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437370	7068771	1548.7	L18E1100S	404737	60	brown,rust	25	NE		10	5		Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437370	7068726	1546.6	L18E1150S	404736	55	dark grey	10	NE	10	10			Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437356	7068621	1550.5	L18E1200S	404735	55	yellowish b	30	NE		5	5	mud	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437362	7068626	1557.8	L18E1250S	404734	50	yellowish b	30	NE		5	5	mud	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	437363	7068571	1552	L18E1300S	404733	25	d.brown	10	NE		20	15	very rocky,rock san	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	435848	7069965	1344.2	L200E050N	no sample				SW	25			rocky slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435852	7070020	1348.7	L200E100N	no sample				SW	25			rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435845	7070069	1350.9	L200E150N	404888	30	d.brown	15	SW	25	15	15	rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435856	7070119	1335.3	L200E200N	404889	40	l.brown	15	SW	25	50	20	rocky slope with wil	Scheelite	Toby	July 3,2006
						BLANK	404890											
NAD 27	UTM	8V	435852	7070156	1357.9	L200E250N	no sample				SW	25			rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435855	7070215	1348.4	L200E300N	404891	40	l.brown	80	SW	25	5	5	rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435855	7070260	1352.4	L200E350N	404892	40	d.brown	5	SW	25	15	10	rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435857	7070308	1352.7	L200E400N	404893	35	d.brown	5	SW	40	15	15	rocky slope with wil	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435863	7070358	1339.6	L200E450N	no sample				SW	45			talus slope,rock sar	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435870	7070392	1352.4	L200E500N	no sample				SW	45			steep scree slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435860	7070460	1328	L200E550N	no sample				SW	45			steep scree slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435874	7070510	1334.4	L200E600N	404894	20	d.brown	10	SW	30	20	15	edge of scree slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435851	7070532	1334.7	L200E650N	404895	25	l.brown	40	SW	20	5	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435868	7070602	1345.7	L200E700N	404896	30	l.brown,gre	20	SW	20	40	20		Scheelite	Toby	July 3,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD 27	UTM	8V	435866	7070652	1347.5	L200E750N	404897	35	l.brown	75	SW	20	15	15		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435870	7070702	1357.9	L200E800N	404898	45	orange bro	75	SW	20	10	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435870	7070751	1355.4	L200E850N	404899	50	orange bro	70	SW	20	10	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435877	7070800	1341.7	L200E900N	404900	70	grey	15	SW	20	5	5		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435877	7070852	1344.2	L200E950N	405269	75	grey	5	SW	20	15	5	silvery	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	435877	7070897	1363.4	L200E1000N	405270	75	grey	80	SW	20	5	5	silvery	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	438021	7069867	1529.8	L24E50N	404701	40	d.brown,re	20	ridge		5	20	very rocky,rusty qu	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438018	7069919	1524.9	L24E100N	404702	45	d.brown,re	25	ridge		10	25	very rocky,rusty qu	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438013	7069959	1524	L24E150N	404703	45	l.brown,ora	20	N		20	15	very rocky,rusty qu	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438016	7070016	1503.3	L24E200N	404704	40	l.brown	5	N		30	20	very rocky,rusty qu	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438017	7070063	1506	L24E250N	404705	42	d.brown	5	N		30	15	very rocky,rusty qu	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438026	7070118	1507.8	L24E300N	404706	45	d.brown	20	N		30	15	mud,rocky,snow pa	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438011	7070164	1483.5	L24E350N	404707	45	l.brown	5	N		15	15	mud,hit ice,close to	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438011	7070208	1477.7	L24E400N	no sample	ice	l.brown		N				hit ice,snowpatch	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438026	7069785	1528.3	L24E050S	404708	65	l.brown	20	ridge		15	15	rusty rock chips	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438018	7069714	1525.2	L24E100S	404709	60	l.brown	20	ridge		15	10	rusty rock chips	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438017	7069665	1524.9	L24E150S	404710	62	l.brown	10	ridge		5	20		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438017	7069618	1520.3	L24E200S	404711	74	l.brown	25	S		5	15	muddy	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438018	7069562	1525.5	L24E250S	404712	62	l.brown,ora	10	S		20	15	rusty,sandy	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438005	7069523	1523.7	L24E300S	404713	55	l.brown	5	S		20	15	rusty,black rock chi	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438012	7069471	1517	L24E350S	404714	42	l.brown	20	S		15	25		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438014	7069422	1508.2	L24E400S	404715	70	l.brown	20	S		10	20		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438019	7069367	1493.5	L24E450S	404716	85	l.brown	15	S		15	15	black rock chips	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438022	7069321	1499.9	L24E500S	404717	65	l.brown,rus	15	S		25	20		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438017	7069270	1475.8	L24E550S	404719	50	l.brown	15	S		20	20	rusty rock chips	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438015	7069227	1463.3	L24E600S	404719	60	l.brown	25	S		20	15		Scheelite	Toby	June 25,2006
						BLANK	404720											
NAD 27	UTM	8V	438015	7069174	1463.3	L24E650S	404721	55	l.brown	30	S		20	15	very rocky,rusty roc	Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438018	7069120	1464.9	L24E700S	404722	50	l.brown	20	S		25	15		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438014	7069079	1444.1	L24E750S	404723	70	l.brown	15	S		15	15		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438016	7069033	1436.8	L24E800S	404724	50	l.brown	20	S		15	15		Scheelite	Toby	June 25,2006
NAD 27	UTM	8V	438018	7068982		L24E850S	404725	35	l.brown,gre	50	S		5	5	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438015	7068934	1431	L24E900S	404726	70	rusty	10	S	30	5	5	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438017	7068887	1412.4	L24E950S	404727	35	l.brown,rus	15	S	25	10	10	mica,hitting frozen	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438015	7068841	1417.9	L24E1000S	404728	55	rusty,l.brow	10	N	35	15	10	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438016	7068795	1424.3	L24E1050S	404729	85	l.brown	80	N	15	5	5	rusty,black rock chi	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438016	7068746	1425.2	L24E1100S	404730	90	d.brown	15	N	15	10	5	rusty,black rock chi	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438017	7068694	1432.3	L24E1150S	404731	35	l.brown	15	N	25	15	10	mica	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	438015	7068653	1463.3	L24E1200S	404732	60	d.brown,ru	10	N		15	5	rusty rock chips,mic	Scheelite	Toby	June 26,2006
NAD 27	UTM	8V	436049	7069957	1449.3	L400E50N	404887	25	orange bro	10	SW	35	15	20	rocky slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436054	7070012	1462.1	L400E100N	404886	30	orange bro	40	SW	45	15	10	rocky slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436049	7070079	1466.7	L400E150N	404885	20	d.browb	10	SW	45	15	25	talus slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436057	7070115	1463	L400E200N	no sample				SW	45			talus slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436053	7070153	1457.9	L400E250N	404884	30	l.brown	10	SW	45	20	15		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436066	7070206	1450.2	L400E300N	no sample				ridge				too rocky	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436065	7070253	1440.2	L400E350N	404883	25	red brown	10	ridge		10	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436069	7070304	1443.5	L400E400N	404882	20	red brown	10	ridge		10	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436067	7070351	1427.7	L400E450N	404881	25	orange bro	15	E	40	10	10		Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436076	7070399	1412.1	L400E500N	no sample				E	40			talus slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436073	7070445	1400.6	L400E550N	no sample				E	40			talus slope	Scheelite	Toby	July 3,2006
NAD 27	UTM	8V	436080	7070496	1398.1	L400E600N	no sample				E	40			talus slope	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436080	7070543	1376.8	L400E650N	404880	40	orange bro	5	E	40	35	15	mica,talus slope	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436097	7070609	1364.6	L400E700N	404879	35	orange bro	15	E	40	15	15	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436088	7070637	1363.7	L400E750N	404878	30	orange bro	85	E	40	5	5	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436094	7070690	1370.7	L400E800N	no sample				E	40			overgrown talus slo	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436104	7070751	1352.1	L400E850N	404877	35	d.brown	10	E	40	30	10		Scheelite	Toby	July 2,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD 27	UTM	8V	436104	7070779	1331.7	L400E900N	404876	35	d.brown	5	E	40	50	10	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436106	7070833	1316.7	L400E950N	404875	75	dark grey	85	E	35	10	5	mica?	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436110	7070872	1308.8	L400E1000N	404874	80	l.brown	90	E		35	5	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436244	7069852	1487.7	L600E50S	404855	35	l.brown	10	N		5	5	mud	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436236	7069800	1510	L600E100S	404854	50	l.brown	30	N		50	5	mica,black rock chi	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436233	7069754	1506.3	L600E150S	404853	75	l.brown	25	NW		5	5		Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436231	7069703	1508.8	L600E200S	404852	40	orange bro	15	W		5	5	mud,mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436230	7069656	1521.6	L600E250S	404851	35	l.brown	15	W		5	5	mud	Scheelite	Toby	July 1,2006
						DUPLICATE	404800								DUPLICATE of 404851			
NAD 27	UTM	8V	436228	7069606	1526.4	L600E300S	404799	30	d.brown	10	W		30	15	very rocky	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436220	7069562	1531	L600E350S	404798	60	l.brown	80	W		5	5	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436227	7069504	1526.4	L600E400S	no sample				W				talus slope,rock sar	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436222	7069454	1513.3	L600E450S	404797	35	l.brown	80	W		5	5	edge of talus slope	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436225	7069407	1524.9	L600E500S	404796	50	grey brown	65	W		5	5	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436243	7069948	1471.3	L600E050N	404856	40	yellow brov	20	N	30	30	10	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436242	7069993	1456	L600E100N	404857	35	l.brown	25	N	40	20	10	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436239	7070050	1446.9	L600E150N	404858	70	orange gre	50	NE	20	15	5	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436248	7070095	1427.1	L600E200N	404859	55	grey	20	NE		15	5	mica	Scheelite	Toby	July 1,2006
NAD 27	UTM	8V	436247	7070140	1411.5	L600E250N	404860	35	l.brown	10	NE	40	40	15	very rocky	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436249	7070187	1403.9	L600E300N	404861	35	d.brown	5	NE	40	55	20	very rocky sample	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436254	7070234	1376.5	L600E350N	404862	30	orange bro	15	NE	40	15	10	mica,outcrop	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436250	7070287	1372.5	L600E400N	404863	25	l.brown	15	NE	40	15	15	outcrop	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436243	7070319	1324.1	L600E450N	no sample				NE	40			sediment.outcrop	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436277	7070387	1337.2	L600E500N	no sample				NE	40			edge of outcrop	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436262	7070425	1321.3	L600E550N	no sample				NE	40			talus slope,rock sar	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436259	7070462	1282	L600E600N	404864	30	l.brown	10	NE	40	30	10	lots of mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436257	7070518	1276.8	L600E650N	404865	30	l.brown	10	NE	20	25	10	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436278	7070569	1272.5	L600E700N	404866	25	l.brown	5	NE	20	20	10	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436265	7070608	1255.8	L600E750N	404867	35	l.brown	25	NE	20	15	15	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436267	7070656	1262.2	L600E800N	404868	25	l.brown	20	NE	40	20	10	mica	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436271	7070705	1261.3	L600E850N	404869	35	d.brown	10	NE	40	15	20		Scheelite	Toby	July 2,2006
						STANDARD CDN/CGS/5	404870											
NAD 27	UTM	8V	436289	7070741	1275.6	L600E900N	404871	30	d.brown	20	NE	40	50	15		Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436268	7070819	1256.1	L600E950N	404872	35	d.brown,gr	15	NE	40	50	15		Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436276	7070863	1257.3	L600E1000N	404873	25	l.brown	50	NE	40	15	10	dried out seasonal	Scheelite	Toby	July 2,2006
NAD 27	UTM	8V	436438	7069943	1474.6	L800E050N	404786	50	l.brown	80	N		15	10	mud,rusty chips	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436435	7069994	1463.6	L800E100N	404787	60	brown,oran	60	N		5	5	mud	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436427	7070042	1460.6	L800E150N	404788	25	brown,oran	5	N		20	5	hit ice	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436444	7070076	1420.1	L800E200N	404789	25	l.brown	5	NW		40	10	snowpatch,talus slo	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436452	7070128	1403.3	L800E250N	404790	35	l.brown,rus	5	NW		40	10	gravely,lots of mica	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436445	7070174	1385.6	L800E300N	404791	50	l.brown	50	NW		25	10	treeline,mica	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436448	7070218	1362.8	L800E350N	no sample	15	l.brown	ice	NW				permafrost	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436449	7070270	1355.4	L800E400N	no sample	15	l.brown	ice	NW				permafrost	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436449	7070316	1345.1	L800E450N	404792	60	l.brown	50	NW		5	5	mud	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436451	7070361	1329.2	L800E500N	no sample				W				talus slope	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436458	7070405	1314.6	L800E550N	no sample				W				talus slope	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436460	7070453	1286.3	L800E600N	404793	35	brown	35	NW		40	15	talus slope	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436462	7070494	1267.1	L800E650N	404794	30	d.brown	20	NW		30	10		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436466	7070536	1248.2	L800E700N	404795	35	d.brown	20	NW		30	10	huge quartzite with	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436434	7069841	1509.7	L800E050S	404771	60	yellowish b	20	NW		5	15	black,rusty rock chi	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436432	7069797	1507.8	L800E100S	404772	65	orange	5	NW		10	5	very orange	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436433	7069750	1526.1	L800E150S	404773	55	d.brown	15	NW		10	15	mud	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436429	7069698	1527.4	L800E200S	404774	70	l.brown	90	NW		0	5	clay	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436432	7069647	1536.5	L800E250S	404775	50	l.brown	90	NW		10	15		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436415	7069593	1537.1	L800E300S	404776	65	l.brown	90	NW		5	5		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436426	7069544	1544.1	L800E350S	404777	55	orange	5	NW		15	5		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436422	7069499	1549.9	L800E400S	404778	55	brown,oran	10	NW		5	5	mica,rusty chips,qu	Scheelite	Toby	June 30,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD 27	UTM	8V	436423	7069447	1547.2	L800E450S	404779	75	dark grey	90	ridge		10	5	lots of mica	Scheelite	Toby	June 30,2006
						BLANK	404780											
NAD 27	UTM	8V	436418	7069398	1543.5	L800E500S	404781	65	d.brown,gr	25	ridge		5	10	grey layer,black roc	Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436425	7069363	1545.3	L800E550S	404782	75	l.brown	85	W		5	5		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436418	7069305	1542.6	L800E600S	404783	80	l.brown,gre	35	W		15	10		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436414	7069250	1545.9	L800E650S	404784	70	l.brown,gre	20	W		15	15		Scheelite	Toby	June 30,2006
NAD 27	UTM	8V	436410	7069202	1542	L800E700S	404785	70	l.brown,gre	20	W		15	15		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	435648	7069962	1246.3	L00E50N	404848	50	brown	60	NW	20	20	10		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435647	7070018	1243	L00E100N	404849	50	brown	50	W	20	10	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435638	7070075	1278.9	L00E150N	404850	55	brown	50	W	20	15	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435655	7070103	1239	L00E200N	405251	70	brown	65	W	20	15	10	note new sample s	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435655	7070164	1241.8	L00E250N	405252	75	brown/dark	60	W	40	15	20	near outcrop, large	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435654	7070212	1240.2	L00E300N	405253	50	orange bro	40	W	30	15	10	the outcrop/subcrop	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435655	7070258	1246	L00E350N	405254	55	brown	40	W	25	10	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435655	7070310	1242.1	L00E400N	405255	50	brown	25	W	10	50	5	very rocky soil	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435659	7070357	1244.2	L00E450N	405256	75	grey-brown	40	W	5	30	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435653	7070404	1256.1	L00E500N	405257	70	brown	40	W	20	15	2		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435662	7070457	1268.3	L00E550N	405258	55	brown	20	W	20	40	5	rocky soil	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435659	7070506	1263.7	L00E600N	405259	65	grey-brown	20	W	30	50	2		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435668	7070558	1267.1	L00E650N	405260	70	brown	65	W	30	15	2		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435666	7070609	1270.4	L00E700N	405261	70	brown	70	W	30	10	10		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435665	7070653	1272.5	L00E750N	405262	90	brown	70	W	40	15	2	DUPLICATE OF S/	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435673	7070699	1274.7	L00E800N	405263	90	brown	70	W	40	15	2	DUPLICATE OF S/	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435673	7070699	1274.7	L00E800N	405264	55	brown	60	W	35	15	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435670	7070750	1262.2	L00E850N	405265	70	brown w/gr	65	W	35	15	2		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435671	7070806	1274.7	L00E900N	405266	25	brown	50	W	20	25	15	hit pfrost at soil leve	Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435679	7070834	1265.2	L00E950N	405267	60	light brown	40	W	10	10	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	435672	7070898	1286.6	L00E1000N	405268	65	grey-brown	50	W	10	30	5		Scheelite	Toby	July 3,2006
NAD27	UTM	8V	436561	7068601	1538.6	L10E1300S	404808	45	brown	40	NW	5	30	10	hit pfrost	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436566	7068650	1545	L10E1250S	404809	65	brown	30	NW	5	20	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436566	7068701	1536.2	L10E1200S	404810	45	brown	30	W	5	15	5		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436580	7068763	1539.5	L10E1150S	404811	50	brown	20	W	10	40	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436568	7068818	1540.8	L10E1100S	404812	85	brown	50	W	10	20	2	a small subcrop in a	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436573	7068843	1546.9	L10E1050S	404813	50	brown	40	SW	10	40	5	very rocky soil	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436579	7068899	1555.4	L10E1000S	404814	65	brown/light	45	SW	10	15	5		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436584	7068945	1554.2	L10E950S	404815	60	brown	35	SW	5	10	5		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436583	7068998	1565.8	L10E900S	404816	55	brown w/ g	20	SW	5	25	2	small subcrop in ar	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436587	7069048	1562.7	L10E850S	404817	55	brown w/gr	30	SW	5	20	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436585	7069093	1565.8	L10E800S	404818	65	brown w/gr	30			20	2	on ridge	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436589	7069144	1565.8	L10E750S	404819	65	brown	25			15	5	on ridge	Scheelite	Toby	June 30,2006
							404820								STANDARD INSEF	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436593	7069222	1556.9	L10E700S	404821	65	light brown	30			25	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436596	7069263	1557.2	L10E650S	404822	65	brown/rust	60			25	5	very rocky soil	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436601	7069289	1548.7	L10E600S	404823	25	dark brown	65	N	5	15	15	hit pfrost at soil leve	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436598	7069321	1557.2	L10E550S	404824	60	brown	60			15	5	large subcrop 25 m	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436607	7069391	1547.5	L10E500S	404825	55	brown	40			10	5	still on ridge	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436616	7069460	1541.7	L10E450S	404826	45	brown	65			5	5	hit pfrost at soil leve	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436616	7069476	1545	L10E400S	404827	60	brown	40			10	2	some tinges of orar	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436615	7069536	1535.6	L10E350S	404828	50	brown	30			5	2	extremely rocky soi	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436619	7069587	1517.3	L10E300S	404829	50	brown	20	NE	5	20	10	extremely rocky soi	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436632	7069640	1523.7	L10E250S	404830	45	brown	20	NE	10	30	10	extremely rocky soi	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436625	7069681	1497.8	L10E200S	404831	25	brown	60	NE	10	15	15	hit pfrost at soil leve	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436631	7069739	1505.1	L10E150S	404832	40	brown	50	NE	10	40	15	hit pfrost at soil leve	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436627	7069787	1498.4	L10E100S	404833	50	brown	15	NE	15	50	15	extremely rocky soi	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436631	7069828	1485	L10E50S	404834	40	brown	30	NE	25	15	15	hit pfrost at soil leve	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436641	7069936	1445.7	L10E50N	404835	70	dark brown	40	E	25	10	10	very rocky soil	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436634	7069978	1445.7	L10E100N	404836	50	dark brown	20	E	40	25	5	very rocky soil	Scheelite	Toby	July 2,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD27	UTM	8V	436636	7070051	1440.8	L10E150N	404837	50	dark brown	20	E	40	25	10	very rocky soil; hit p	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436643	7070097	1447.2	L10E200N	404838	50	brown	30	E	40	30	2	didn't hit pfrost	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436647	7070128	1422.2	L10E250N	404839	65	brown	50	E	10	10	2		Scheelite	Toby	July 2,2006
							404840									Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436645	7070192	1407.6	L10E300N	404841	65	brown	30	E	10	30	2		Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436649	7070217	1388.7	L10E350N	404842	70	brown w/or	20	E	10	25	2		Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436637	7070281	1389.6	L10E400N	404843	65	brown	30	NE	20	50	2		Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436663	7070315	1364	L10E450N	404844	55	brown	25	N	40	50	2	extremely rocky soi	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436660	7070358	1350.3	L10E500N	404845	50	brown	40	N	10	45	2	extremely rocky soi	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436672	7070403	1346	L10E550N	404846	60	light brown	50	N	10	15	2	soil less rocky	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436662	7070447	1316.4	L10E600N	404847	70	light brown	60	N	10	15	2	soil less rocky	Scheelite	Toby	July 2,2006
NAD27	UTM	8V	436859	7070459	1319.8	L12E600N	404568	65	brown	25	NE	10	30	2		Scheelite	Toby	June 28,2006
NAD27	UTM	8V	436846	7070409	1319.2	L12E550N	404569	55	brown	40	NE	10	25	5	station near subcro	Scheelite	Toby	June 28,2006
NAD27	UTM	8V	436858	7070359	1346.3	L12E500N	404570	25	light brown	15	E	35	50	5	took sample from p	Scheelite	Toby	June 28,2006
NAD27	UTM	8V	436858	7070319	1327.4	L12E450N	404571	25	light brown	15	E	45	50	5	took sample from p	Scheelite	Toby	June 28,2006
NAD27	UTM	8V	436844	7070249	1339.9	L12E400N	404572	55	brown	40	NE	40	15	5		Scheelite	Toby	June 28,2006
NAD27	UTM	8V	436837	7070210	1348.7	L12E350N	404573	60	brown	5	E	45	50	10		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436837	7070150	1350.3	L12E300N	404574	75	brown	20	E	45	30	5		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436833	7070105	1350.9	L12E250N	404575	100	brown	30	E	45	25	5	30 m from large out	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436861	7070060	1336.9	L12E200N	404576	70	brown	30	E	40	20	2		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436829	7070003	1345.2	L12E150	404577	50	brown	20	NE	40	15	2		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436833	7069974	1387.1	L12E100N	404578	50	brown	50	NE	10	10	5		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436829	7069921	1401.8	L12E50N	404579	50	brown	30			10	5		Scheelite	Toby	June 29,2006
NAD27	UTM	8V					404580								BLANK INSERTED	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436827	7069817	1417.9	L12E50	404581	100	brown	60	NE	20	20	2		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436819	7069760	1399.9	L12E100N	404582	75	light brown	50	NE	20	15	2		Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436814	7069732	1436.5	L12E150N	404583	110	brown	80	NE	35	10	2	very large subcrop	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436822	7069668	1448.7	L12E200N	404584	50	dark brown	30	E	40	20	10	now in subcrop are	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436822	7069626	1464.6	L12E250N	404585	75	brown	50	E	50	50	10	very rocky soil	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436821	7069575	1469.4	L12E300N	404586	65	brown	40	E	45	10	10	very rocky soil; in s	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436803	7069515	1489.9	L12E350N	404587	75	dark brown	50	NE	45	50	10	sample taken unde	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436810	7069479	1500.2	L12E400N	404588	85	light brown	25	N	30	50	2	sample taken unde	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436810	7069427	1499.6	L12E450N	404589	85	light brown	40	NE	20	40	2	near ridge; outcrop	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436812	7069390	1510	L12E500N	404590	75	brown	60	NE	15	20	2	near ridge; past abo	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436806	7069335	1531.6	L12E550N	404591	65	brown	60	NE	15	15	2	near ridge; past abo	Scheelite	Toby	June 29,2006
NAD27	UTM	8V	436808	7069289	1533.4	L12E600N	404592	45	brown	30	NE	10	40	15	on ridge; very rocky	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436803	7069240	1539.2	L12E650N	404593	30	brown	60	NE	10	20	10	on ridge; hit pfrost a	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436810	7069177	1552	L12E700N	404594	50	brown	60	NE	5	20	10	very rocky soil	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436804	7069129	1561.2	L12E750N	404595	45	brown	50	NE	5	40	5	on ridge; rocky soil	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436802	7069086	1569.1	L12E800N	404596	60	light grey	40			40	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436802	7069056	1568.8	L12E850N	404597	45	brown	40			20	10	soil contains lots of	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436795	7068989	1577	L12E900N	404598	55	brown	60			30	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436791	7068936	1577.9	L12E950N	404599	50	brown/oran	30			30	5	DUPLICATE OF SA	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436791	7068936	1577.9	L12E950N	404600	50	brown/oran	30			30	5	DUPLICATE OF SA	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436788	7068899	1577.9	L12E1000N	404801	55	brown	30			15	10	still on ridge	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436791	7068859	1586.2	L12E1050N	404802	65	light brown	30			15	5	large subcrop all ar	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436792	7068781	1574.9	L12E1100N	404803	85	light brown	15	NW	5	10	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436781	7068770	1583.7	L12E1150N	404804	70	brown	25	NW	5	10	5	small subcrop arou	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436789	7068712	1575.5	L12E1200N	404805	45	brown	60	NW	5	30	15	extremely rocky sur	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436779	7068647	1581.3	L12E1250N	404806	70	brown with	30	NW	5	10	2		Scheelite	Toby	June 30,2006
NAD27	UTM	8V	436777	7068603	1577.3	L12E1300N	404807	35	brown	60	NW	5	10	5	hit pfrost at soil leve	Scheelite	Toby	June 30,2006
NAD27	UTM	8V	437226	7069897	1248.8	L16E0050	404556	75	brown	70	N	5	15	2	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437233	7069959	1251.2	L16E0100N	404557	50	brown	40			30	5	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437230	7069996	1227.4	L16E0150N	404558	60	brown	30	W	5	30	10	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437220	7070047	1253.3	L16E0200N	404559	30	orange-bro	25			25	15	near creek, bottom	Scheelite	Toby	June 27,2006
	UTM	8V					404560								STANDARD INSEF	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437220	7070091	1204.6	L16E0250N	404561	75	dark brown	10	N	5	60	15	mostly rocks in soil	Scheelite	Toby	June 27,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	%_rx_chip	%_organic	notes	Property	Zone	Date
NAD27	UTM	8V	437231	7070128	1198.5	L16E0300N	404562	25	dark brown	10	N	5	50	20	took from pfrost--m	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437232	7070173	1196.3	L16E0350N	404563	40	brown	70	N	5	30	15	took from pfrost, sti	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437246	7070237	1195.1	L16E0400N	404564	45	brown	60	N	5	15	15	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437234	7070282	1196.3	L16E0450N	404565	50	dark brown	20	W	5	15	30	near creek, rocky s	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437232	7070340	1192.1	L16E0500N	404566	85	brown	60	N	5	60	2	near creek, rocky s	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437235	7070390	1183.2	L16E0550N	No Sample	35							No Sample--too roc	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437233	7070407	1178.4	L16E0600N	404567	50	brown	10	N	5	30	10	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437156	7068621	1584.7	L16N1300S	404534	45	brown	90			5	2	hit pfrost at soil leve	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437163	7068676	1589.8	L16E1250S	404535	50	brown	10			30	5	hit pfrost at soil leve	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437165	7068719	1580.4	L16E1200S	404536	55	dark brown	50			20	15	extremely rocky soi	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437168	7068793	1574.3	L16E1150S	404537	65	brown	35			10	5	soil less rocky; stop	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437178	7068819	1572.2	L16E1100S	404538	50	brown	50			20	10	stopped by clay	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437176	7068845	1579.2	L16E1050S	404539	70	light brown	30	E	5	10	5	DUPLICATE OF 40	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437176	7068845	1579.2	L16E1050S	404540	70	light brown	30	E	55	10	5	DUPLICATE OF 40	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437178	7068919	1570.9	L16E1000S	404541	65	brown	15	E	5	50	5	extremely rocky soi	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437180	7068964	1559.7	L16E950S	No Sample	60	light brown		N	40			dug hole 10m from	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437178	7069023	1549.3	L16E900S	No Sample	15	brown		N	35			near outcrop	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437187	7069060	1527	L16E850S	404542	90	brown	80	N	40	15	2	very rocky soil. Dug	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437187	7069118	1509.7	L16E800S	404543	75	brown	90	N	20	10	5	very wet and rocky.	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437182	7069180	1511.2	L16E750S	404544	45	light brown	75	N	20	20	2	took sample from p	Scheelite	Toby	June 27,2006
	UTM	8V				L16E700					N				could not sample--s	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437194	7069244	1458.5	L16E650S	404545	75	light brown	60	N	35	20	5	very rocky soil. Nea	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437191	7069294	1450.2	L16E600S	404546	50	brown	50	N	35	40	5	very rocky soil. Hit	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437205	7069330	1417.6	L16E550S	404547	80	brown	40			15	5	less rocky	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437194	7069378	1409.1	L16E500S									large outcrop--no s	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437212	7069434	1391.7	L16E450S	404548	100	brown	30	N	40	40	2	large outcrop in are	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437204	7069457	1337.2	L16E400S	404549	80	brown	60	N	35	30	5	outcrop continues--	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437204	7069518	1356.7	L16E350S	404550	75	light brown	15	N		40	5	spruce trees thick n	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437213	7069571	1337.8	L16E300S		60			N	60			covered in subcrop	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437210	7069609	1316.4	L16E250S	404551	50	brown	40	N	35	40	5	took sample from p	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437216	7069655	1297.5	L16E200S	404552	70	silver-brow	15	N	30	70	20	sample mostly rock	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437216	7069681	1232.9	L16E150S	404553	70	dark brown	5	N	15	80	2	sample mostly rock	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437219	7069757	1275.9	L16E100S	404554	40	dark brown	20			30	10	near creek now--ve	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437210	7069808	1268.9	L16E50S	404555	50	brown	70	N	15	10	2	near creek	Scheelite	Toby	June 27,2006
NAD27	UTM	8V	437823	7070216	1463.6	L22E400N	404501	50	rusty browr	0	NW		85	2	very rocky soil	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437829	7070178	1468.2	L22E350N	404502	45	rusty browr	80	NW	20	10	5	very rocky soil	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437814	7070141	1473.4	L22E300N	404503	45	brown	70	NW	20	15	5	large subcrop surro	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437824	7070070	1480.4	L22E250N	404504	45	brown	50	W	10	40	5	rocky soil. Stopped	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437822	7070006	1480.4	L22E200N	404505	45	brown	30	W	10	30	10	very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437823	7069971	1488.3	L22E150N	404506	40	brown	20	W	10	50	10	very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437820	7069922	1491.4	L22E100N	404507	40	brown	15	W	10	50	15	very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437819	7069870	1500.8	L22E50N	404508	50	brown	90	W	10	5	5	stopped by hard cla	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437809	7069776	1506.6	L22E50S	404509	45	brown	20	NW	10	15	5	soil less rocky here	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437814	7069721	1512.4	L22E100S	404510	40	brown	80	NW	10	10	5		Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437809	7069680	1514.9	L22E150S	404511	50	brown	80	W	5	2	2	on ridge, very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437801	7069615	1508.5	L22E200S	404512	45	brown	15	W	5	15	15	on ridge, very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437812	7069578	1522.8	L22E250S	404513	50	brown	75			10	5	on ridge, very rocky	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437810	7069541	1524.3	L22E300S	404514	50	brown	80			2	5	took sample from p	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437812	7069477	1521	L22E350S	404515	50	brown	80			2	5	took sample from p	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437811	7069428	1519.1	L22E400S	404516	55	brown	50			25	5	fewer rocks--mostly	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437809	7069379	1514.6	L22E450S	404517	45	brown	40	S	5	20	10	fewer rocks--mostly	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437812	7069334	1515.8	L22E500S	404518	55	brown	35	S	5	10	5	fewer rocks--mostly	Scheelite	Toby	June 25,2006
NAD27	UTM	8V	437810	7069279	1513.3	L22E550S	404519	70	brown	45	S	5	10	10	fewer rocks--mostly	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437812	7069256	1498.7	L22E600S	404520								BLANK SAMPLE IN	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437812	7069256	1498.7	L22E600S	404521	85	orange-bro	20	S	10	15	5	hitting rock	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437804	7069165	1494.4	L22E650S	404522	80	brown	40	S	10	5	2	hitting rock	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437802	7069131	1490.2	L22E700S	404523	85	light brown	40	S	10	15	2	hitting rock	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437803	7069077	1485.9	L22E750S	404524	75	orange-bro	30	SE	8	10	2		Scheelite	Toby	June 26,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD27	UTM	8V	437806	7069035	1482.2	L22E800S	404525	130	brown	50	SE	8	10	2		Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437806	7068975	1475.8	L22E850S	404526	65	brown	20	SE	20	30	5	starting to head do	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437796	7068948	1465.5	L22E900S	404527	140	brown	60	SE	25	15	2	further into gully--te	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437795	7068891	1446.9	L22E950S	404528	130	brown	60	SE	40	5	2	further into gully--te	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437797	7068836	1439.6	L22E1000S	404529	85	brown	70	E	5	15	5	in bottom of gully	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437791	7068784	1438.7	L22E1050S	404530	110	brown	60	NE	8	10	5		Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437788	7068733	1446.3	L22E1100S	404531	80	brown	70	NE	10	5	2		Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437785	7068687	1458.8	L22E1150S	404532	65	brown	10	NE	10	40	2	soil very rocky now	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	437797	7068640	1477.1	L22E1200S	404533	45	brown	10	NE	10	60	2	took sample from p	Scheelite	Toby	June 26,2006
NAD27	UTM	8V	435646	7069920	1253.6	BL00E	404647	40	brown	80			35	60	v. rocky, lots of org.	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435699	7069906	1264.3	BL50E	404646	45	brown	80	SW	20	35	60	v. rocky, lots of org.	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435732	7069911	1317.3	BL100E	404645	35	brown	80	SW	25	40	20	d. grey flakes, oran	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435797	7069914	1315.8	BL150E	404644	30	brown	80	SW	25	60	10	orange chips, qtz cl	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435837	7069906	1337.8	BL200E	404643	35	brown/ d.br	80	SW	30	70	15	orange chips, ox'd c	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435894	7069915	1375	BL250E	404642	30	L. brown	60	SW	25	70	15	orange chips, ox'd c	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435947	7069918	1402.1	BL300E	404641	35	L. brown	60	SW	35	70	25	DUPLICATE of 404	Scheelite dome	Toby	June 27,2006
NAD28	UTM	8V	435947	7069918	1402.1	BL300E	404640	35	L. brown	60	SW	35	70	25	DUPLICATE of 404	Scheelite dome	Toby	June 27,2006
NAD27	UTM	8V	435988	7069912	1440.2	BL350E	404639	45	L. brown	60	SW	30	70	5	musc flakes/chips,	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436042	7069910	1451.8	BL400E	404638	40	L. brown	60	SW	30	70	5	musc flakes/chips,	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436086	7069922	1457.9	BL450E	404637	45	L. brown	60	SW	20	50	10	musc flakes/chips,	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436141	7069904	1480.1	BL500E	404636	35	brown	80	NW	20	20	5	orange rock w/ red	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436186	7069903	1489.9	BL550E	404635	30	brown	80	NW	15	15	10	orange and musc. (	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436235	7069899	1487.4	BL600E	404634	45	brown w/ b	80	NE	15	15	15	orange and musc fl	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436283	7069897	1482.2	BL650E	404633	35	L. brown	80	N	15	20	5	orange rocks, musc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436335	7069897	1486.2	BL700E	404632	50	brown	80	N	15	15	5	orange rocks, musc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436387	7069898	1497.5	BL750E	404631	45	brown	80	N	15	15	5	orange rocks, musc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436434	7069895	1490.5	BL800E	404630	30	brown	80	N	15	30	5	orange rocks, qtz, p	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436479	7069887	1481.3	BL850E	404629	35	brown	80	N	15	30	10	orange rocks, p. fro	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436534	7069885	1479.8	BL900E	no sample	20	d. brown/black		NE	15			organic pfrost, 7 ho	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436583	7069882	1465.8	BL950E	404628	35	d. brown	80	NE	15	30	15	orange, flakey, qtz,	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436635	7069879	1451.8	BL1000E	404627	35	d. brown	80	NE	25	20	25	orange, flakey, qtz,	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436681	7069879	1440.2	BL1050E	404626	45	brown	50	NE	5	25	15	orange/red ox'd roc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436730	7069876	1424.6	BL1100E	404625	50	brown	15	NE	20	25	10	orange/red ox'd roc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436777	7069869	1415.8	BL1150E	404624	35	brown	40	NE	30	25	10	ornage flakey, musc	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436832	7069882	1428.3	BL1200E	404623	45	brown w/ d	40	N	25	25	30	orange and musc. f	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436877	7069862	1405.1	BL1250E	404622	40	brown w/ g	60	NE	20	25	15	orange and musc. f	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436925	7069861	1378.6	BL1300E	404621	40	brown	70	NE	30	25	10	orange and musc. f	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	436983	7069852	1359.1	BL1350E	404619	50	brown w/ o	50	SE	25	70	5	orange and musc. f	Scheelite dome	Toby	June 26,2006
NAD27	UTM	8V	437029	7069877	1321.6	BL1400E	404618	30	brown w/ d	80	SE	25	60	20	orange/red ox'd roc	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437065	7069842	1283.2	BL1450E	404617	40	d. brown	80	SE	25	10	15	orange, qtz, musc.	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437124	7069850	1291.4	BL1500E	404616	30	brown	30	SE	20	40	10	orange, qtz, musc.	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437173	7069841	1259.7	BL1550E	404615	30	brown	70	SE	20	50	10	orange, qtz, musc.,	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437222	7069830	1252.4	BL1600E	404614	35	brown w/ b	80	SE	5	50	10	orange, qtz, musc.,	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437240	7069847	1276.8	BL1650E	404613	60	brown w/ d	60			20	20	some orange rock a	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437319	7069839	1266.7	BL1700E	404612	50	d. brown	80			20	5	at valley bottom, to	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437388	7069781	1154.3	BL1750E	404611	40	brown	60	NW	25	70	20	v. rocky, orange chi	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437419	7069834	1313.1	BL1800E	404610	40	brown	80	NW	25	50	10	v. rocky, orange chi	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437462	7069834	1350.6	BL1850E	no sample	30	brown and orange		NW	30			v. rocky w. p/frost a	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437518	7069836	1362.2	BL1900E	404609	35	brown	50	NW	25	50	15	orange rock	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437567	7069832	1398.4	BL1950E	404608	40	brown	10	NW	40	50	15	v. rocky, orange, tre	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437618	7069829	1424.6	BL2000E	404607	45	brown	20	NW	20	60	10	v. rocky, orange an	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437667	7069827	1439.3	BL2050E	no sample	40	d. brown/ black		NW	35	90	10	steep slope, v. rock	Scheelite dome	Toby	June 25,2006
						BL2100	no sample				NW					Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437767	7069825	1492.3	BL2150E	404606	35	brown	80	NW	15	30	15	orange flakes	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437812	7069823	1512.4	BL2200E	404605	40	brown	80	NW	5	70	10	v. rocky, orange an	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437872	7069816	1513.9	BL2250E	404604	45	brown	80	NW	5	25	10	p. frost at bottom, o	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437915	7069821	1523.4	BL2300E	404603	45	brown	80			15	5	orange rock chips,	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437969	7069818	1529.5	BL2350E	404602	50	brown	20			20	5	orange rock chips,	Scheelite dome	Toby	June 25,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD27	UTM	8V	438015	7069815	1525.2	BL2400E	404601	55	brown	30			25	5	orange rock chips,	Scheelite dome	Toby	June 25,2006
NAD27	UTM	8V	437023	7070435	1266.4	L14E600N	404677	45	brown	80	E	45	50	20	v. rocky w/ org. Ora	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437023	7070384	1251.2	L14E550N	404676	45	brown	80	SE	45	50	30	v. rocky w/ org. Ora	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437022	7070330	1241.1	L14E500N	404675	35	brown/ d. b	80	E	30	30	50	v. rocky w/ org. Ora	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437023	7070285	1238.1	L14E450N	no sample	40			NE	15			black org. down 40	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437015	7070236	1256.1	L14E400N	no sample	30			NE	15			only rock and orgar	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437019	7070189	1272.5	L14E350N	no sample				E	20			only rock. Talus fan	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437021	7070147	1294.5	L14E300N	no sample				NE	40			only rock. Talus fan	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437024	7070092	1298.4	L14E250N	no sample				E	35			only rock. Talus fan	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437025	7070070	1329.8	L14E200N	no sample	20			E	30			only rock and orgar	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437026	7070011	1336.5	L14E150N	404674	25	l. brown	80	E	40	25	35	mostly rock/ org. or	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437026	7069959	1335.9	L14E100N	no sample	20			E	30			mostly rock/org., th	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437032	7069895	1337.8	L14E50N	404673	45	L. brown	80	E	25	15	5	orange pebbles/chi	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437021	7069806	1342.9	L14E50S	404672	35	brown	80	NE	40	30	30	musc. And orange f	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437032	7069752	1350.6	L14E100S	404671	30	brown	80	E	40	30	30	v. rocky w/ org. ora	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437021	7069708	1342	L14E150S	404670	35	brown	60	E	30	60	30	v. rocky w/ org. ora	Scheelite dome	Toby	June 29,2006
NAD27	UTM	8V	437019	7069662	1356.4	L14E200S	404669	25	l. brown	60	E	35	15	50	talus w/ organic, sa	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437014	7069610	1359.7	L14E250S	404668	65	L. brown/ta	80	E	25	15	10	musc. and orange c	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437011	7069561	1367	L14E300S	404667	45	d. brown	80	E	25	20	10	musc. and orange c	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437013	7069507	1377.1	L14E350S	404666	45	brwon	40	E	30	40	10	musc. And orange c	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437012	7069455	1388.4	L14E400S	no sample	40			NE	35			v. rocky, only grave	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437014	7069422	1421.3	L14E450S	404665	30	L. brown/ta	60	N	20	60	30	v. rocky, three hole	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437013	7069373	1431.6	L14E500S	no sample				NE	35			rock w/ thin layer of	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437013	7069326	1446.6	L14E550S	404664	35	d. brown	80	E	20	15	60	talus w/ organic, sa	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437010	7069275	1458.2	L14E600S	404663	45	brown	50	NE	20	40	10	orange chips/ musc	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437005	7069231	1479.8	L14E650S	404662	35	brown	60	NE	20	60	15	v. rocky, sample 5n	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437011	7069176	1482.2	L14E700S	404661	45	brown	80	N	30	25	5	orange and musc. (	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437008	7069135	1507.5	L14E750S	404659	50	orangie brc	50	NE	25	40	5	orange chips, musc	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437002	7069094	1541.7	L14E800S	404658	65	orange/ rec	30	NE	10	30	5	orange and musc. f	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437008	7069038	1543.2	L14E850S	404657	45	brown	40	NE	20	70	10	v. rocky, orange chi	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437005	7068992	1563.3	L14E900S	404656	45	d. brown	70	NE	20	70	10	v. rocky, orange chi	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437004	7068940	1563.6	L14E950S	404655	50	d. brown	70	E	10	70	5	v. rocky, orange chi	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437003	7068892	1575.5	L14E1000S	404654	45	orangie brc	50	E	10	70	5	v. rocky, orange fla	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437004	7068842	1583.4	L14E1050S	404653	50	orangie brc	30	E	5	25	10	orange chips, ox'd c	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437002	7068797	1591.7	L14E1100S	404652	45	orangie brc	50	E	5	30	15	lots of orange flake	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437000	7068748	1595	L14E1150S	404651	45	d. brown	60			10	5	orange flakes/chips	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437000	7068701	1594.1	L14E1200S	404650	55	d. brown w	60			15	5	musc. And orange f	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437003	7068654	1584	L14E1250S	404649	45	d. brown	80			15	15	orange/red pebbles	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	436996	7068597	1598.7	L14E1300S	404648	40	d. brown	80			20	10	musc., pfrost at bot	Scheelite dome	Toby	June 28,2006
NAD27	UTM	8V	437241	7070149	1196.3	L16E325N	404690	35	brown/ d.br	80	N	5	25	10	musc. Flakes, oran	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437229	7070203	1193.3	L16E375N	404689	35	brown/ d.br	80	N	5	5	5	musc. Flakes, oran	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437237	7070254	1179	L16E425N	404688	80	brown/ d.br	90	N	5	5	5	thick muddy clay wi	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437242	7070292	1182.9	L16E475N	404687	50	d. brown	60	N	5	70	25	gravelly, lots of ora	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437240	7070353	1172.6	L16E525N	404686	40	brown	50	N	5	50	10	gravelly, lots of ora	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437240	7070390	1172.9	L16E575N	404685	40	brown	80	N	5	15	15	large ox'd qtz rocks	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437432	7070158	1300.9	L18E325N	404678	40	brown	80	W	15	15	5	orange flakes/ chip	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437434	7070209	1303.3	L18E375N	404679	50	brown	60	W	40	15	50	v. steep slope w/ ta	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437434	7070251	1290.5	L18E425N	404681	50	brown	60	NW	25	30	30	v. rocky. Orange pe	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437435	7070295	1272.2	L18E475N	404682	75	brown	80	NW	35	20	5	orange pebbles, mu	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437436	7070344	1261.3	L18E525N	404683	70	brown	80	W	35	20	5	orange pebbles, mu	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437439	7070395	1292.4	L18E575N	404684	35	brown	80	SW	20	25	10	orange rocks/chips,	Scheelite dome	Toby	July 1,2006
NAD27	UTM	8V	437407	7069464	1373.4	L18E375S	405214	85	brown	60	NW	30	60	15	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437405	7069425	1422.2	L18E425S	405215	75	brown	60	NW	25	60	5	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437402	7069380	1426.2	L18E475S	405216	70	l. brown	50	NW	25	40	10	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437399	7069329	1441.7	L18E525S	405217	55	l. brown	50	NW	20	60	5	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437411	7069286	1441.1	L18E575S	no sample									Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437393	7069260	1476.8	L18E600S	405218	45	orangie brc	70	NW	30	60	10	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%	aspect	slope	% rx chip	% organic	notes	Property	Zone	Date
NAD27	UTM	8V	437393	7069239	1488.3	L18E625S	405219	40	l. brown	50	NW	30	60	10	v. rocky, musc. Flak	Scheelite dome	Toby	July 3,2006
																Scheelite dome	Toby	
NAD27	UTM	8V	437633	7070317	1373.7	L20E500N	404691	60	brown	40	W	20	15	5	orange flakes/ chur	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437633	7070263	1365.8	L20E450N	404692	30	brown	80	W	30	30	40	edge of talus: mostl	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437631	7070215	1383.8	L20E400N	404693	65	brown	60	NW	25	15	5	orange chunks, mu	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437634	7070164	1403.9	L20E350N	404694	65	brown	70	W	30	20	5	orange chunks, mu	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437628	7070118	1407.3	L20E300N	404695	50	brown	40	W	30	30	15	orange chunks, mu	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437629	7070068	1400.9	L20E250N	404696	45	brown	70	W	30	15	30	talus/ org. deep. Or	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437629	7070021	1403.9	L20E200N	404697	60	brown	40	SW	20	25	10	orange chunks/chip	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437629	7069962	1386.8	L20E150N	404698	35	brown	60	SW	35	10	40	orange chunks. Mu	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437624	7069927	1410.9	L20E100N	404699	65	brown	80	W	35	40	10	talus subcrop surro	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437618	7069878	1418.5	L20E50N	404700	60	brown	60	SW	35	30	15	DUPLICATE of 405	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437618	7069878	1418.5	L20E50N	405201	60	brown	60	SW	35	30	15	DUPLICATE of 404	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437619	7069782	1427.1	L20E50S	405202	85	brown	80	W	10	25	5	orange chunks, mu	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437608	7069723	1428.9	L20E100S	405203	70	brown	60	SW	30	30	15	orange and qtz chip	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437602	7069676	1432.9	L20E150S	405204	35	brown/ d. b	80	W	30	15	30	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437605	7069632	1439.3	L20E200S	405205	45	brown	60	W	30	30	15	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437603	7069582	1444.4	L20E250S	405206	50	brown	60	W	30	30	10	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437600	7069530	1439.6	L20E300S	405207	50	brown	60	NW	25	40	15	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437593	7069483	1452.7	L20E350S	405208	55	brown	60	NW	25	40	20	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437590	7069457	1460.9	L20E375S	405209	45	brown	60	NW	25	40	20	orange chips, musc	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437589	7069438	1460.9	L20E400S	405210	80	brown, orai	40	NW	25	50	5	orange flakes/chips	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437590	7069409	1455.7	L20E425S	405211	65	brown/ orai	30	NW	25	70	5	v. gravelly. Qtz chip	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437587	7069387	1471	L20E450S	no sample				NW	25			talus fan: intrusive,	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437585	7069359	1477.4	L20E475S	405212	50	brown	60	NW	30	50	5	talus subcrop: intru	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437587	7069338	1483.8	L20E500S	no sample				NW	30			talus fan, no sampl	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437580	7069317	1495	L20E525S	405213	90	brown/ orai	40	NW	30	60	5	gravelly. Musc flake	Scheelite dome	Toby	July 2,2006
NAD27	UTM	8V	437575	7069297	1507.8	L20E550S	405221	85	orangie brc	50	NW	30	60	5	gravelly, musc flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437575	7069269	1509.4	L20E575S	405222	30	brown/ d. b	70	NW	20	50	40	gravelly, w/ pfrost a	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437573	7069247	1515.8	L20E600S	405223	65	orange	40	NW	10	20	10	musc flakes, orang	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437572	7069221	1516.7	L20E625S	405224	45	brown/ d. b	80	NW	5	10	10	thick mud, orange c	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437571	7069193	1517.3	L20E650S	405225	55	brown	80	NW	5	10	5	thick mud, orange c	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437566	7069146	1523.4	L20E700S	405226	45	brown	60	NW	5	70	10	gravelly. Orange ch	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437561	7069096	1525.2	L20E750S	405227	50	brown w/ y	40			30	5	orange flakes, musc	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437560	7069052	1521	L20E800S	405228	80	yellowy brc	20			10	5	musc. Flakes	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437556	7068994	1521	L20E850S	405229	75	l. brown	40	SE	5	30	5	musc. chunks/flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437552	7068939	1517.9	L20E900S	405230	60	brown	30	SE	10	40	5	musc. chunks/flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437550	7068893	1515.5	L20E950S	405231	50	brown	30	SE	15	50	10	musc. chunks/flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437548	7068850	1511.2	L20E1000S	405232	70	brown	30	SE	15	30	10	musc. chunks/flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437546	7068799	1505.4	L20E1050S	405233	80	orangie brc	30	E	20	25	10	musc. chunks/flake	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437544	7068751	1508.2	L20E1100S	405234	75	brown	40	NE	15	30	5	musc chunks/flakes	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437542	7068698	1519.7	L20E1150S	405235	65	brown	40	NE	15	30	10	musc chunks/flakes	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437541	7068654	1525.8	L20E1200S	405236	60	brown	20	NE	10	50	5	musc chunks/flakes	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437534	7068601	1534.4	L20E1250S	405237	70	brown	80	NE	10	15	10	musc. flakes	Scheelite dome	Toby	July 3,2006
NAD27	UTM	8V	437537	7068554	1535	L20E1300S	405238	55	brown	30	NE	10	60	15	orange chunks/ chi	Scheelite dome	Toby	July 3,2006

Line 4 (redo along ri Note: Jo asked us to do 350m of ridge near line 4. We started on line 4 at 325N and headed along the ridge

NAD27	UTM	8V	436064	7070232	1446.3	L4R0325	405271	50	brown	30			40	10	on ridge; very rocky	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436059	7070259	1442.6	L4R0350	405272	45	brown	15			50	5	on ridge; very rocky	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436054	7070282	1442.9	L4R0375	405273	40	brown	10			40	15	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436048	7070306	1443.8	L4R0400	405274	40	brown	15			30	15	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436042	7070337	1445.1	L4R0425	405275	40	brown	15			40	10	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436050	7070356	1438.4	L4R0450	405276	50	brown	25			40	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436048	7070383	1433.8	L4R0475	no sample	40							Too rocky--no samp	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436049	7070411	1427.1	L4R0500	405277	35	dark brown	10			40	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436050	7070436	1424.9	L4R0525	405278	45	brown	20	NE	10	25	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436043	7070455	1421.3	L4R0550	405279	65	brown	40	NE	5	15	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436035	7070487	1420.4	L4R0575	405280	50	grey-brown	20			30	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436035	7070517	1419.8	L4R0600	405281	45	brown	20			30	2	very rocky soil	Scheelite	Toby	July 4,2006

Datum	Coordinat	Zone	Easting	Northing	elevation	waypoint_name	Assay_No	depth(cm)	colour	texture(%c	aspect	slope	%_rx_chip	%_organic	notes	Property	Zone	Date
NAD27	UTM	8V	436045	7070551	1418.5	L4R0625	405282	40	brown	15			20	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436044	7070576	1407.9	L4R0650	no sample	30							Too rocky--no sam	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436045	7070601	1402.4	L4R0675	405283	35	brown	10			25	15	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	436043	7070630	1396.6	L4R0700	405284	55	brown	10			40	5	very rocky soil	Scheelite	Toby	July 4,2006
NAD27	UTM	8V	437530	7068651	1538.9	CLAIM19629										Scheelite dome	Toby	
NAD 27	UTM	8V	437713	7068699	1471.6	YB43780									claim post	Scheelite	Toby	
NAD27	UTM	8V	437021	7070236	1252.1	L14E400SUB												

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
8V	436482	7070082	115670	*rusty qytz subcrop in ortage weathering thinly bedded phyllite (local strongly carbonate altered layers) with slickensides (nothing inplace for measurements) right above snow cornice on North facing slope, abundatnt silvery grey sericite mica along foliation; trace fine grained pyrite in quartz and rusty pits.*	603488	18	0.9	0.5	0.4
8V	436457	7070058	115671	*subcrop of calcareous orange weathering finelyh bedded phyllite with abundant quartz rich bedsseperated by silvery grey miceous folia; matriz reacts to HCl and angular peces in subcrop with <2% euhedral pyrite and lesser fine grained clots of arsenopyrite, common rusty boxwork pits.*	603488	245.5	406.9	90	473.9
8V	436631	7069897	115672		603488	32.7	1.2	1.5	2.6
8V	436630	7069835	115673		603488	17.4	1.5	0.7	2.2
8V	436573	7069341	115674		603488	42.3	0.9	0.5	0.3
	???	????	115675	*rock samples comes from Milada's line*	603488	182.5	0.25	1.3	1
8V	436832	7069862	115676		603488	27.1	3.4	0.5	0.4
8V	436828	7070016	115677		603488	26.3	3.6	0.7	0.8
8V	436842	7070104	115678		603488	36.8	2.8	0.5	0.5
8V	436783	7070400	115679		603488	2	0.5	0.1	0.1
8V	436636	7070290	115680		603488	299.5	4	0.4	0.5
8V	436654	7070215	115681		603488	67.5	5.8	0.6	1.5
8V	436660	7070175	115682		603488	37.6	0.5	0.5	0.2
8V	436901	7069859	115683		603488	92.3	2.3	1	0.5
8V	436901	7069859	115684		603488	30.2	2	1.2	0.5
8V	437030	7069821	115685		603488	209.8	1.6	1	0.9
8V	437030	7069821	115686		603488	91.4	0.25	0.5	0.1
8V	436996	7069795	115687		603488	979.5	8.8	1.3	0.3
8V	437018	7069961	115688		603488	77.3	2.2	8.1	0.7
8V	437028	7069996	115689		603488	58.4	4.5	1	1
8V	437028	7069996	115690		603488	54.5	1	1.8	0.4
8V	437031	7070010	115691		603488	129.4	1.2	1.7	0.2
8V	437031	7070010	115692	*STANDARAD CDN/CGS/1*	603488	13	476	4.6	0.5
8V	436907	7069881	115693		603488	50.3	3.8	4.4	0.2
8V	436878	7069949	115694		603488	73.4	1.1	0.9	0.3
8V	436887	7069939	115695		603488	20.7	0.8	0.6	0.1
8V	436887	7069939	115696		603488	1611.5	15.9	4	0.8
8V	436915	7069953	115697		603488	61.2	1.8	1.1	0.1
8V	436992	7069947	115698		603488	79.6	0.6	0.7	0.4
8V	436908	7070074	115700		603488	80.8	2.5	1.2	0.6
			404901		603488	8.4	0.6	0.4	0.2
8V	436382	7070009	404902		603488	22.7	1.5	1	0.3
8V	436382	7070009	404903		603488	73.2	335.7	2.8	50.5

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
8V	436367	7070004	404904		603488	21.6	5.5	13	1.1
8V	436293	7070021	404905		603488	37.1	3	0.3	0.2
8V	436128	7070126	404906		603488	5373.4	185.7	5.1	6
8V	436085	7070150	404907		603488	6.8	3	0.5	0.3
8V	436085	7070150	404908		603488	54.2	2.5	0.4	0.3
8V	436056	7070272	404909		603488	980.6	16.2	1.3	2.1
8V	436037	7070412	404910		603488	450.8	7	3.3	0.4
8V	436033	7070679	404911		603488	188.4	29.4	1.2	0.1
8V	436124	7070205	404912		603488	957.2	29.4	4.2	2.7
8V	436187	7070070	404913		603488	142.7	5.7	11	0.3
8V	436254	7070021	404914		603488	45.1	2	3.8	1.6
8V	436306	7070025	404915		603488	10	0.25	2.4	0.1
8V	436418	7070072	404916		603488	21	1.1	1.8	0.2
8V	436418	7070072	404917	*BLANK*	603488	8	6.2	0.6	0.1
8V	436497	7070151	404918		603662	21	0.7	0.8	0.1
8V	436511	7070187	404919		603662	120.2	1.7	3.9	0.6
8V	436535	7070175	404920		603662	104.6	663.4	12.3	266.3
8V	436535	7070175	404921		603662	162.6	31.8	0.9	6
8V	436556	7070190	404922		603662	13.9	4.4	0.2	1.8
8V	436558	7070225	404923		603662	58.9	2.8	1	0.9
8V	436562	7070251	404924		603662	332.2	12.4	0.5	3.9
8V	436550	7070272	404925		603662	308.1	2.8	0.4	0.3
8V	436570	7070327	404926		603662	81.7	2	0.5	0.3
8V	436626	7070299	404927		603662	604.5	437.7	217.5	507.4
8V	436510	7069959	404928		603662	471.5	39.3	41.6	67.9
8V	436529	7069943	404929		603662	23	4.9	2.9	6
8V	436507	7069819	404930		603662	77.4	1.6	2.3	1.7
8V	436436	7069794	404931		603662	91.4	1.8	8.7	1.1
8V	436229	7069491	404932		603662	24	0.9	3	0.5
8V	436364	7069731	404933		603662	27.2	0.25	1.2	0.5
8V	436539	7069782	404934		603662	12	1.6	1.4	0.5
8V	437130	7069851	404935		603662	295.7	26.5	1.3	3.3
8V	436996	7069845	404936		603662	200.7	4.7	1.7	2
8V	436920	7069862	404937		603662	75.6	3.2	1.6	0.8
8V	437589	7069438	404938		603662	24	0.25	0.7	0.2
8V	435863	7070358	404939		603662	192.8	0.25	2.5	0.3
8V	437590	7069410	404940		603662	351.7	36.7	1.5	2.6
8V	436646	7069880	404941		603662	6.9	1.6	0.8	0.5
8V	436657	7069831	404942		603662	35.7	1.9	0.9	1.1
8V	436690	7069778	404943		603662	16.9	28.2	0.3	3.2

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
			404944		603662	43.5	2.4	0.7	0.8
8V	436707	7069469	404945		603662	48.4	1.7	0.5	0.2
8V	436718	7069433	404946		603662	36.1	1	2.7	0.1
8V	436845	7069205	404947	*Huge spurs of calcareous silstone/quartzite phyllitic partings End of traverse above outcrop, turn above L1000E, above phyllite outcrop spors*	603662	462.8	1.5	1.9	0.7
8V	436859	7069185	404948	*15cm rusty quartz float in moss/subcrop; orange weathering quartzite/phyllite with <3% total sulfide as fine grained blebs and ??? Stringers, arsenopyrite>pyrite> ???, pus redish possible REALGAR crystals*	603662	523.4	1.1	1	0.2
8V	436560	7069397	404949	*5m^2 subrop of large 80cm sized boulders in phyllite(locally quartz rich); <3% arsenopyrite ,<pyrite in blebs up to 7mm in open spaces in fillings along discrete fractures in otherwise weakly rusty quartz vein material*	603662	234.2	3.2	1	1.7
8V	436528	7069464		*20m^2 blocky talus of grey weathering bi-quartz-feldsparporphyry intrusive with rare 2mmx8mm hornblend crystals*	603662				
			404950	*STANDARD CDN/CGS/5*	603662	6.3	112	1.9	0.2
8V	437761	7069766	404951	*Quartz stringers in slumped quartzite outcrop with fine grained sulfide?*	603662	36.6	10.5	0.4	1
8V	437763	7069757	404952	*0.7m chip of quartzite with sheeted quartz stringers up to 1cm wide*	603662	48.2	2.1	0.8	0.7
8V	437767	7069719	404953	*Grab of quartzite with 3 crosscutting quartz stringers <1cm wide*	603662	13.1	0.25	0.2	0.1
8V	437762	7069710	404954	*0.6m chip across across quartzite/phyllite with rusty parallel foliation*	603662	725	3.4	1.4	2.7
			404955	*8cm quartz vein cross cutting quartzite outcrop oriented 130/85E*	603662	251.7	6.4	4.3	4.9
			404956		603662	3752.5	26.2	29.4	2.3
	Coordinates of milada's		404957	*white quartz vein float with <1% arsenopyrite/ GO BACK TO THE FIELDBOOK*	603662	456.7	25.4	56.5	2.9
8V	437671	7069446	404958	*thinly bedded phyllite with rusty paintings with >10% fine grained arsenopyrite*	603662	>10000	1612.1	78.3	190.9
8V	437661	7069428	404959	*Very GOOLIE looking phyllite sulfide rich; 15% arsenopyrite in thinly banded quartz beds in phyllite*	603662	>10000	873.6	103	50.3
8V	437630	7069350	404960	*Bi-(quartzite) feldspar intrusive plus intense biotite? Lamprophyre dyke trending 070-090^o ; 10% ??? Arsenopyrite in thin bans in phyllite*	603662	>10000	321.7	11.4	24.6
8V	437597	7069303	404961	*shaley dull grey greasy phyllite with 2mm white quartz pitted layers. Scorodite on fractures*	603662	299.4	3.8	1.5	0.7
8V	437377	7069207	404962	*Grab of quartzite with 4cm white quartz vein cross cutting foliation; 2% arsenopyrite in blebs*	603662	518.9	5.7	3.8	4.2
			404963	*go back to the fieldbook*	603662	456.5	3.4	1.1	0.4
8V	437357	7069204	404964	*40cm white quartz float with coarse grained arsenopyrite <2%*	603662	274.3	4.6	0.7	0.5
8V	437303	7069176	404965	*Float 10^o below outcrop of rusty folded quartz with open space and scorodite in quartzite.*	603662	1547	16.2	3	2.1
8V	437274	7069177	404966	*Float of 10% arsenopyrite, ??? In finely laminated quartz rich phyllite*	603662	>10000	174.2	10.2	33.9
8V	436908	7069215	404967	*???*	603662	137.8	11	1.4	1.1
8V	436876	7069240	404968	*??*	603662	223.3	3.3	0.9	1.1
8V	436542	7070414	404969	*??*	603662	741	8.7	5.5	0.1

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
8V	436543	7070423	404970		603662	14.8	2.5	6.4	0.1
8V	438426	7071000		*Location of truck parked at head of Highet Creek pass*	603662				
8V	436686	7069661	404971	*Quartz in phyllite in outcrop*	603662	46	2.1	0.5	0.4
8V	436842	7069324	404972	*Intrusive outcrop with pyroxine, ?????*	603662	21.7	1.6	0.7	0.3
8V	436880	7069118	404973	*subcrop of silvery phyllite at head of cirque with concoidant quartz sweats up to 4cm, rusty with open space*	603662	65.3	1.2	0.8	0.4
8V	436887	7069113	404974	*quartz rusty open space, limonite cemented box work in silvery phyllite*	603662	88.1	0.25	3	0.1
8V	437000	7069082	404975	*outcrop/subcrop of block phyllite with calcareous beds ofwhite crystalline calcite up to 4cm wide*	603662	38.6	0.25	0.3	0.05
8V	437061	7069100	404976	*Slumped outcrop of folded phyllite with 20cm quartzite layer, rusty with 3cm quartz sweats and pits oxidized sulfide; pyrite and arsenopyrite*	603662	94.3	2.3	2.1	0.7
8V	437122	7069106	404977	*Grassy swampy creek head west of L16E; porous calcareous orange weathering phyllite with quartzite beds up to 4cm (subcrop west of major slump wet creek start).*	603662	301.5	2	1.4	0.7
8V	437134	7069105	404978	*Grab of rusty quartz float with blebs of pyrite/arsenopyrite along fractures in swampy grassy calcareous phyllite subcrop (??????)*	603662	108.5	0.25	0.8	1.5
8V	437127	7069110	404979	*2m N down slope of 404978, quartz rich pock marked quartzite arsenopyrite blebs in fractures, moss slope, talus debris*	603662	1595.1	3.1	14.9	2.9
8V	437263	7069165	404980	*Grab of silvery/rusty phyllitewith box work <1mm and pyrite (fine grained arsenopyrite) blebs, ??? 2-4mm rusty crosscutting stringers to foliation.*	603662	>10000	35.8	16.9	16.4
			404981???		603662	411.1	9.5	2.6	7.9
8V	437239	7069157	404982	*20% arsenopyrite in discrete/silvery in up to 5mm wide phyllite parallel foliation with scorodite around semi continuous arsenopyrite stringers; slumped talus almost outcrop, 75m E of Line ???? (sketch in the fieldbook)*	603662	>10000	273.4	60.6	75.1
8V	437255	7069169	404983	*Same talus as above; white yellow quartzite, rusty gragments and 10% 4mm round grey quartz eyes? Felsic intrusive? WHOLE ROCK ANALYSIS/ REP SAMPLE*	603662				
			404984???		603662	556	4.7	0.8	0.5
8V	437278	7069180	404985	*40cm^2 tabular jointed orange and weathering quartzite/phyllite with scorodite and fine grained stringers <4mm and blebs of arsenopyrite up to 6mm^2, sulfide cross foliation only slightly from phyllite to quartzite, 15% arsenopyrite. (sketch in the fieldbook).*	603662	>10000	171.3	76.3	32.1
8V	437296	7069182	404986	*15x20cm boulder talus of orange weathering quartzite (non calcarious) with fine grained pyrite in crystaling ?????? quartzite*	603662	197	5.2	9.7	0.4
8V	437324	7069178	404987	*White pitted scorodit, rich quartzite talus, sugary looking with vugs and fine grained arsenopyrite <2% visible.*	603662	2149.2	19.5	6.2	1.5
8V	437358	7069196	404988	*slumped outcrop of manganese stained folded phyllite with 2cm quartz stringers,lots of open space pits <1%sulfide.*	603662	320.4	6.1	4	3
8V	437340	7069211	404989	*Blebs of arsenopyrite in quartzite with up to 5%sulfide in sugary quartzite*	603662	1184.5	6.4	3.6	0.6

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
8V	437535	7069273	404990	Grab in 10cm^2 scree slope (just south of big outcrop along ridge) of grey fine grained phyllite quartzite cut by quartz stringers up to 8mm wide across foliation, pits limoniteand fine grained sulfide?	603662	83.8	0.6	4.2	0.2
8V	437570	7069299	404991	Grab of 30cm^2 quartz vein float with 1% ???? Arsenopyrite blebs along fracture in grass/moss covered phyllite knob.	603662	390.6	3.1	2.5	0.2
8V	437577	7069301	404992	Grab of siliceous phyllite with grey graphitic bands and quartz rich bands with 20% porosity as 2mm pits, limonite and scorodite.	603662	187	2.4	1.6	2.6
8V	437600	7069297	404993	?? very fractured possible faulted manganese rich veined in several directions; quartzite/phyllite in talus slope with 10% ????	603662	>10000	1907	203.5	285
8V	437584	7069304	404994	Solid sulfide! 3cm wide intensely rusty arsenopyrite and scorodite; 5cm^2 float; walked above snow cornice to find source in outcrop.	603662	>10000	5428	607.5	595.8
8V	437625	7069290			603662				
8V	437630	7069287	404995	Distinct recessive gully trending 85-90°,dug a pit and sampled rusty quartzite with 1mm pits coated in limonite.Trace of pyrite.	603662	1434.7	16.5	2.7	2.9
8V	437633	7069329	404996	Limonitic quartz rich phyllite with pale matrix filled by limonitic vugs and fine grained pyrite stringers along foliation.	603662	>10000	285.6	18.5	28.1
8V	437622	7069330	404997-98	Foliation 130/30S. Outcrop chip samples of quartzite and phyllite (0.8m) and 0.9m chip in quartzite(June 5th picture). Quartz along fracture in quartzite 015° /80E dip. Contact between phyllite/quartzite is 130°/255 (sketch in the fieldbook)	603662	386.8	56.8	1.8	1.7
8V	437627	7069355	404999	Bi-quartz poor intrusive with rare <2% feldspars in dyke trending downslope@ app.170° towards Paul find on L20E with pyrite in intrusive, locally looks like lamprophyre dyke	603662	1415.8	27.9	3	2.5
8V	437634	7069354	405000	Grab of black manganese stained talus with waxy pale quartzite layer with 2mm pits and steal grey layers.	603662	359.6	6.3	2.7	0.3
8V	437628	7069344	405001	Quartzite blocky talus with rusty sub parallel fractures and blebs of arsenopyrite and scorodite up to 3% overall with intense limonite/ .....???	603662	5630.1	38.9	7.3	12
8V	437654	7069394	405002	3 square cm fragmens on quartzite/phyllite talus of pure up to 1cm arsenopyrite banded veins ( ), intensely rusty.	603662	>10000	2163	155.9	119.3
8V	437651	7069386	405003	BLANK. Silvery phyllite talus slope but sample of granular pale quartzite with sub parallel fractures every 6cm and 3% coarse 6mm cubic blebs of arsenopyrite diss along fractures ( )	603662	13.2	5.7	0.6	0.1
8V	437656	7069394	405004	Grab of intense scorodite yellow green oxidation and 1cm+ width of pure arsenopyrite; intensily rusty outer surface ??quartzite bed	603662	598.5	4.4	2.3	0.6
8V	437668	7069392	405005	Grab of rusty quartz vein float ( ) with open space fracture and quartz crystal infill and arsenopyrite up to 6mm blocks along fracture.	603662	>10000	2048	249.1	112
8V	437669	7069430	405006	Outcrop of thinly laminated quartzite and phyllite on top oriented 025/20SE; no significant rust.	603662	938.4	21.3	3.6	1.4
8V	437682	7069458	405007	Grab of scorodite arsenopyrite vein material in quartzite/phyllite talus 10m South of outcrop described below.	603662	>10000	2871	109.7	495.9

Zone	Easting	Northing	Assay No.	Notes	Acme Cert	As ppm	Au ppb	Sb ppm	Bi ppm
8V	437684	7069455	405008	*0.5m chip across intenesely rusty phyllite outcrop with grey layers of fine grained arsenopyrite sub parallel to foliation up to 5% arsenopyrite; intense manganese foliation 030/29SE*	603662	3547.1	103	3.1	12.8
8V	437685	7069476	405009	*0.7m chip across phyllic outcrop with grainy quartz rich beds and very fine grained arsenopyrite along fractures <%1? . Foliation 048/26SE*	603662	943.2	19.6	2	25.3
8V	437685	7069492	405010	*0.45m chip across small outcrop in talus field of intensely rusty quartz rich phyllite with pits and blue fine grained arsenopyrite in matrix of select beds; arsenopyrite 25%*	603662	>10000	586	7.6	76.6
8V	437704	7069508	405011	*0.6m chip of rusty bed in phyllite with blueish arsenopyrite in beds of rusty quartz rich phyllite. Foliation 045/22E*	603662	3632	263.2	4.1	40.5
8V	437168	7069065	GDSD01	Grab of "frothy" qz vein apparently fol controlled in silicified qzt	605885	>10000	413.8	225	284.3
8V	437153	7068974	GDSD02	Select grab of silicified qzt with local .5 to 2 cm stwk of qz vns with local aspy and py. Py also diss in qzt.	605885	>10000	826.30	74.50	160.40
8V	437141	7068961	GDSD03	Grab of float in talus of silicified qzt with 15 % diss py (py is totally oxidized on margins) Py likely bedding/foliation controlled in qzt)	605885	951.90	32.70	152.50	71.00
8V	437145	7068966	GDSD04	Same location as 03: 4-5 cm lens in talus of coarse qzwith pathchy aspy and diss cubic py.	605885	>10000	137.10	10.30	30.60
8V	437120	7068964	GDSD05	40 by 20 cm block of silicified qzt with up to 5 % diss py aspy (also patchy in qz vnlts) and 1 % PY. Similar appearing boulders are fairly abund in area	605885	8013.90	82.60	15.00	12.00
8V	437099	7068957	GDSD06	40 by 60 cm talus boulder of qzt with str stwk of 1 to 5 mm qz vnlts, local patchy ASPY and cubic PY	605885	3366.70	55.20	21.60	1.40
8V	437078	7068947	GDSD07	3 cm qz vn as separate piece in subcrop, local massive ASPY, v. strongly oxidized	605885	824.20	31.10	201.90	23.00
8V	437056	7068930	GDSD08	large angular blcks of bx with rounded clasts of gry qz in strongly oxidized siliceous matrix: no visable unoxidized sulfides	605885	504.30	26.40	20.40	1.40
8V	437064	7068919	GDSD09	3 cm qa vn slumped from O/C. 20 to 30 % cubic Py	605885	2121.00	16.00	33.90	49.30
8V	437130	7068981	GDSD10	30 by 60 talus blk of white qz with abund FeOx and patches of ASPY. Not far from source	605885	6506.70	142.00	16.30	24.70
8V	437821	7069877	GDSD11	silicified lst with local PO and vuggy 3 mm qz vnlt: near strong IP anom on line 20	605885	190.50	7.30	1.30	4.70

SCHEELITE DOME - TRENCH **TR 06-1**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date R'cvd	Au ppb	As ppm	Sb ppm	Bi ppm
405301	2	2	0	TR06-1	grab	Sep 1/06	606035		1.4	216.8	2.8	1.9
405302	6	6	0	TR06-1	grab	Sep 1/06	606035		2.8	424.9	4	0.6
405303	9	11	2	TR06-1	chip	Sep 1/06	606035		3.2	389.1	6.4	5.4
405304	13	13	0	TR06-1	grab	Sep 1/06	606035		0.9	33.7	1.1	0.2
405305	15	16	1	TR06-1	chip	Sep 1/06	606035		46	1328.3	1.7	2.5
405306	16.5	17.5	1	TR06-1	chip	Sep 1/06	606035		2.3	604.9	2.3	0.2
405307	22	22	0	TR06-1	grab	Sep 1/06	606035		18	68.4	1	0.1
405308	23	23	0	TR06-1	grab	Sep 1/06	606035		0.25	27	0.4	0.1
405309	24.5	26	1.5	TR06-1	chip	Sep 1/06	606035		5.8	1697.9	3.7	1.1
405310	25	25	0	TR06-1	grab	Sep 1/06	606035		2.5	2520.3	4	0.4
405311	27	27	0	TR06-1	grab	Sep 1/06	606035		3.7	1276.6	2.6	0.5
405312	28	29	1	TR06-1	chip	Sep 1/06	606035		9.7	7154.8	3.3	0.8
405313	31	31	0	TR06-1	grab	Sep 1/06	606035		31.8	>10000	28.8	1.2
405314	31.2	31.2	0	TR06-1	grab	Sep 1/06	606035		10.3	>10000	10.6	1.2
405315	43	43	0	TR06-1	grab	Sep 1/06	606035		2	242.4	0.9	0.2
405316	49	49	0	TR06-1	grab	Sep 1/06	606035		2.8	74.1	1.2	0.5
405317	50	50	0	TR06-1	grab	Sep 1/06	606035		0.7	19.4	0.5	0.4

Total Samples: 17

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
400951	596	596	0	TR06-2	grab	20-Aug-06	A605775	05-Oct-06	2695.6	>10000	309.2	606.1	2.89
400952	592	594	2	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	4233.3	>10000	498.6	1509	4.21
400953	589	592	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	39.8	2383.2	8.8	14.3	
400954	586	589	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	21.9	1048.3	10.6	3.2	
400955	583	586	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	22.6	1339.9	8.5	10	
400956	580	583	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	38.4	1051.6	4.2	5.2	
400957	577	580	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	8.8	781.4	3.2	3.1	
400958	574	577	3	TR06-2	chip	20-Aug-06	A605775	05-Oct-06	14.9	815.8	2.3	2.1	
400959	570	571	1	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	17.2	1579.7	1.8	5.8	
400960	567	570	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	2.6	227.6	1.7	0.7	
400961	564	567	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	1.6	260	1.7	0.7	
400962	561	564	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	5.6	354.7	2	1.2	
400963	558	561	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	9.7	340.1	2.4	1.3	
400964	555	558	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	4.2	273.1	1.9	1.1	
400965	552	555	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	6	233	3.3	0.7	
400966	549	552	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	4.9	303.1	2.8	0.6	
400967	546	549	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	10.2	232.8	2.6	0.8	
400968	543	546	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	4.1	396.8	3.5	0.6	
400969	540	543	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	6	280.7	2	1	
400970	537	540	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	37.8	827.4	4.2	3.9	
400971	534	537	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	130.9	2918.6	3.2	6.5	
400972	531	534	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	20.7	509.6	1.6	2.1	
400973	528	531	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	16	373.2	1.3	1.9	
400974	525	528	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	6.4	376.4	1.4	1.1	
400975				TR06-2	BLANK: QFP - Haystack M	21-Aug-06	A605775	05-Oct-06	0.5	19.8	0.4	0.1	
400976	522.5	525	2.5	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	33.6	1474.1	4.1	3	
400977	520	522.5	2.5	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	48.1	1849.4	5.3	6	
400978	517	520	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	32.4	769.7	1.8	4.5	
400979	515	517	2	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	37.1	1253.3	3.2	4.4	
400980	512	515	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	21.3	937.7	1.7	2.9	
400981	509	512	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	270.9	8455.7	5.3	32.6	
400982	505.5	509	3.5	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	49	1004.5	1.1	6.4	
400983	503	505.5	2.5	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	14.3	503.8	1.6	1.9	
400984	500	503	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	8.5	359.2	1.6	1.3	
400985	497	500	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	5.5	444	1.8	2.1	
400986	494	497	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	18.6	805.1	2.7	4.8	
400987	491	494	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	41.3	784.4	2.2	6.8	
400988	488	491	3	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	9.6	277.1	1.5	1.8	
400989	486	488	2	TR06-2	chip	21-Aug-06	A605775	05-Oct-06	4.3	195.4	1.2	1.1	
400990	484	486	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	10.7	438.7	1.9	2.2	

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
400991	482	484	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	10.2	562.4	1.9	3.3	
400992	479	482	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	7.4	288.4	1.8	1.2	
400993	476	479	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	9.2	367.6	2.1	1.4	
400994	473	476	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	7	443.4	2.4	1.6	
400995	471	473	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	8.1	615.5	2.4	2.9	
400996	468	471	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	6.5	312	3.2	0.9	
400997	465	468	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	6.6	490.9	2.9	1.2	
400998	462	465	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	6	279.7	2.7	0.7	
400999	459	462	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	5.8	401.9	2.5	0.5	
401000				TR06-2	STANDARD:CDN-GS-10A	22-Aug-06	A605775	05-Oct-06	8891.9	459.6	52.7	<.1	10.31
400501	456	459	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	4.7	376	1.8	1.9	
400502	453	456	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	12.3	994.7	2.6	3.1	
400503	450	453	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	7.9	519.5	3.8	3	
400504	447	450	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	12.9	362	2.7	1.6	
400505	444.5	447	2.5	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	24.9	628.7	4.1	1.5	
400506	442	444.5	2.5	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	7.5	430.4	2.2	1.2	
400507	441	442	1	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	1.2	130.8	1.5	0.5	
400508	438	441	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	47.7	2964.6	5	9.6	
400509	435	438	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	10.7	758.7	3.1	2.5	
400510	432	435	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	9.5	557.9	3.7	1.3	
400511	429	432	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	4.6	497.3	2.3	0.9	
400512	426	429	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	127.1	2992.6	4.7	0.9	
400513	423	426	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	11.8	582.8	3.4	2	
400514	420	423	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	9.1	422.1	2.1	1.9	
400515	418	420	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	5.9	293.7	2.1	1.1	
400516	416	418	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	5.9	382.1	2.3	1.2	
400517	413	416	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	7.9	524.1	3.3	1.4	
400518	410	413	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	10.6	528.9	3.7	1.3	
400519	407	410	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	5.9	352.9	2	1.1	
400520	405.5	407	2.5	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	5.9	667.2	5.4	0.8	
400521	403	405.5	2.5	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	6	496.6	4.3	1.4	
400522	400	403	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	12.3	849.9	7.1	1.4	
400523	398	400	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	13.7	588.7	6.4	1.8	
400524	396	398	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	15.3	705.1	8.8	1.3	
400525				TR06-2	BLANK: QFP - Haystack M	22-Aug-06	A605775	05-Oct-06	0.9	18.4	0.4	0.2	
400526	394	396	2	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	8.7	505.5	10.9	1.8	
400527	393	394	1	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	3	323.3	7	0.6	
400528	390	393	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	0.9	108.2	3.9	0.1	
400529	387	390	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	<.5	153.2	4.9	0.1	
400530	384	387	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	<.5	164.2	3.4	0.1	

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
400531	381	384	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	6.2	555.8	16.7	0.7	
400532	378	381	3	TR06-2	chip	22-Aug-06	A605775	05-Oct-06	14.5	780.2	13.2	1.6	
400533	375	378	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	20.6	1093.9	21.5	2.6	
400534	372	375	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	14.3	1040.6	6	1.7	
400535	369	372	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	4.6	437.1	5.9	1	
400536	366	369	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	12.5	1023	5	1.5	
400537	363	366	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	22.1	1001.1	4.2	2.2	
400538	360	363	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	13.2	746.4	2.8	1.8	
400539	359	360	1	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	37	4938.3	7.1	4.1	
400540	356	359	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	76.7	1642.6	5.6	7.3	
400541	354	356	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	26.2	1065	5.2	2.9	
400542	352	354	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	65.2	734.4	4.1	4.9	
400543	349	352	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	33.9	513.5	3.8	2.8	
400544	346	349	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	68.7	472.4	2.9	5.3	
400545	343	346	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	29.4	743.6	2.6	1.9	
400546	341	343	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	17	709.7	2.9	2.3	
400547	338.5	341	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	11	342.2	2.4	1.5	
400548	336	338.5	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	113	1469.6	5.3	6.3	
400549	333	336	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	83.1	1955.5	4.1	6.3	
400550			0	TR06-2	Standard: CDN-GS-1C (0.9	23-Aug-06	A605884	10-Oct-06	862.2	324.7	27	0.2	
400551	330	333	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	74.5	1286.9	9.3	4.9	
400552	329	330	1	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	44.3	878.7	41	2.5	
400553	326	329	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	4.3	224.1	2.8	0.9	
400554	323.5	326	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	11	549.9	3.2	2.4	
400555	321	323.5	2.5	TR06-2	grab	23-Aug-06	A605884	10-Oct-06	15.6	4264.2	5.5	2.4	
400556	321	321	0	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	451.6	>10000	20.9	33.6	
400557	320	321	1	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	58	3558.9	10.8	8.4	
400558	318	320	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	12.5	807.6	2.5	1.6	
400559	315.5	318	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	40.5	1266.3	3.3	20.2	
400560	313	315.5	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	77.3	5569.4	5	6	
400561	310.5	313	2.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	3	196.6	0.8	0.8	
400562	310	310.5	0.5	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	2.1	156.7	0.7	0.5	
400563	307	310	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	8.5	290.7	1.2	0.8	
400564	304	307	3	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	2.9	95.5	0.8	0.2	
400565	302	304	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	3.5	163.7	4.4	0.5	
400566	300	302	2	TR06-2	chip	23-Aug-06	A605884	10-Oct-06	5.4	155.9	0.8	0.4	
400567	297	300	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	54	279.6	1.2	3.4	
400568	294	297	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	15.7	197.9	0.7	1.8	
400569	291.5	294	2.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	54.8	1467.3	2.2	4.6	
400570	290.5	291.5	1	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	717.5	>10000	19.5	21.9	

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
400571	290.5	290.5	0	TR06-2	grab	24-Aug-06	A605884	10-Oct-06	8014.1	>10000	316.8	192.5	
400572	288	290.5	2.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	55.2	1109	2.1	4.9	
400573	286.5	288	1.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	136.3	3314.4	4.4	10.7	
400574	284	286.5	2.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	8.2	438.9	1.4	1	
400575			0	TR06-2	BLANK: QFP - Haystack M	24-Aug-06	A605884	10-Oct-06	8.3	170.5	0.4	0.4	
400576	282	284	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	567.1	3235.2	3.7	35.2	
400577	280	282	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	1289.3	>10000	22.1	68.1	
400578	277	280	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	16.3	500	1.4	2.2	
400579	276	277	1	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	12.5	422.6	1.1	1	
400580	275	276	1	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	31.8	828.2	1.8	5.2	
400581	272	275	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	57	573.6	2.6	9	
400582	269	272	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	191.9	820.2	3	16.6	
400583	266	269	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	56.2	895.3	2.1	7.5	
400584	263	266	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	11	456.2	1.3	1.6	
400585	260	263	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	53.1	1292.9	2.1	4.6	
400586	257	260	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	14.6	454	1.6	1.6	
400587	254	257	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	7.8	517.9	1.4	1.1	
400588	252	254	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	20.9	1098.4	2.2	3.7	
400589	250	252	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	29.7	2015.2	2.1	3.1	
400590	249	250	1	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	12.3	530	1.3	1.7	
400591	246	249	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	25.6	780.9	1.9	2.2	
400592	244.5	246	1.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	33	511.7	1.6	3.7	
400593	243	244.5	1.5	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	9	551.4	1.6	1.2	
400594	240	243	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	6.7	373.5	1.1	0.8	
400595	237	240	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	34.2	891.5	1.9	3.1	
400596	234	237	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	4.2	167.8	0.9	0.5	
400597	231	234	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	8.5	206.9	1.2	0.9	
400598	228	231	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	9	534.9	2.5	1.4	
400599	225	228	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	5.7	224.3	0.8	1.1	
400600			0	TR06-2	Standard: CDN-GS-10A (9	24-Aug-06	A605884	10-Oct-06	8488.9	445.9	50.9	<.1	
400601	222	225	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	6.4	217.8	0.8	0.6	
400602	219	222	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	7.3	175.8	1	1.2	
400603	216	219	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	36.8	586	1.6	7.1	
400604	214	216	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	3	216.3	1.2	0.3	
400605	212	214	2	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	8.9	404.7	1.2	0.9	
400606	209	212	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	4.1	219.1	0.6	0.7	
400607	206	209	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	13.7	647.9	1	1.5	
400608	203	206	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	10	345.3	0.9	1.9	
400609	200	203	3	TR06-2	chip	24-Aug-06	A605884	10-Oct-06	3.6	206.9	0.7	0.9	

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
405122	200	200	0	TR06-2	grab	Aug 31/06	A606035		7.5	332.6	1.4	0.9	
405123	197	200	3	TR06-2	chip	Aug 31/06	A606035		28.8	407	1.1	4.1	
405124	194	197	3	TR06-2	chip	Aug 31/06	A606035		69.1	296.3	1.4	7.5	
405125			0	TR06-2	Blank QFP Haystack Mtn.	Aug 31/06	A606035		2	7.2	0.3	0.2	
405126	191	194	3	TR06-2	chip	Aug 31/06	A606035		7	195.4	0.8	0.7	
405127	188	191	3	TR06-2	chip	Aug 31/06	A606035		64.1	162	1	2	
405128	185	188	3	TR06-2	chip	Aug 31/06	A606035		4.6	295.4	1	0.8	
405129	182	185	3	TR06-2	chip	Aug 31/06	A606035		8.7	390.7	1.7	3.1	
405130	185	185	0	TR06-2	grab	Aug 31/06	A606035		1.6	43	1.5	0.2	
405131	179	182	3	TR06-2	chip	Aug 31/06	A606035		17.3	337.5	1.2	2.3	
405132	176	179	3	TR06-2	chip	Aug 31/06	A606035		3.5	104.6	1.2	0.7	
405133	173	176	3	TR06-2	chip	Aug 31/06	A606035		15.7	268.5	0.9	3.1	
405134	173.2	173.2	0	TR06-2	grab	Aug 31/06	A606035		10.1	83.4	0.4	1.7	
405135	170	173	3	TR06-2	chip	Aug 31/06	A606035		11.6	224.5	0.7	1.6	
405136	167	170	3	TR06-2	chip	Aug 31/06	A606035		23.9	361	0.8	4.3	
405137	164	167	3	TR06-2	chip	Aug 31/06	A606035		7.6	279.4	1.1	1.2	
405138	161	164	3	TR06-2	chip	Aug 31/06	A606035		9.2	275.4	1.5	1.1	
405139	158	161	3	TR06-2	chip	Aug 31/06	A606035		109.6	211	2.3	18	
405140	155	158	3	TR06-2	chip	Aug 31/06	A606035		5.6	157.1	1.2	2.8	
405141	152	155	3	TR06-2	chip	Aug 31/06	A606035		5.8	76.6	0.5	1.3	
405142	149	152	3	TR06-2	chip	Aug 31/06	A606035		3.2	85.3	0.4	0.6	
405143	146	149	3	TR06-2	chip	Aug 31/06	A606035		2.3	120.3	0.5	0.9	
405144	143	146	3	TR06-2	chip	Aug 31/06	A606035		18.5	169.8	1.7	5.3	
405145	140	143	3	TR06-2	chip	Aug 31/06	A606035		4.2	140.2	0.9	0.9	
405146	137	140	3	TR06-2	chip	Aug 31/06	A606035		26.6	50.7	0.3	6	
405147	134	137	3	TR06-2	chip	Aug 31/06	A606035		1.2	30.2	0.3	0.3	
405148	131	134	3	TR06-2	chip	Aug 31/06	A606035		21.9	105.7	0.6	3.1	
405149	128	131	3	TR06-2	chip	Aug 31/06	A606035		2.6	108.4	0.5	0.4	
405150			0	TR06-2	Standard CDN-GS-10A	Aug 31/06	A606035		8532.4	453.9	51.1	<.1	10.27
405151	125	128	3	TR06-2	chip	Aug 31/06	A606035		8.1	252.1	2.5	1	
405152	122	125	3	TR06-2	chip	Aug 31/06	A606035		10.6	148	0.7	1.4	
405153	119	122	3	TR06-2	chip	Aug 31/06	A606035		2.8	103.1	1.2	0.2	
405154	112	112	0	TR06-2	grab	Aug 31/06	A606035		2.4	132.7	0.6	0.8	
405155	116	119	3	TR06-2	chip	Aug 31/06	A606035		4.2	120.5	0.6	0.5	
405156	113	116	3	TR06-2	chip	Aug 31/06	A606035		5.3	82.5	0.3	0.6	
405157	110	113	3	TR06-2	chip	Aug 31/06	A606035		20.7	45.6	0.3	2.3	
405158	107	110	3	TR06-2	chip	Aug 31/06	A606035		34.6	111.1	1.2	2.7	
405159	104	107	3	TR06-2	chip	Aug 31/06	A606035		15.9	90.5	0.5	1.8	
405160	101	104	3	TR06-2	chip	Aug 31/06	A606035		3.8	76.7	0.4	0.3	
405161	95	101	6	TR06-2	chip	Aug 31/06	A606035		17.4	63.2	0.7	2.3	

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
405162	99.5	99.5	0	TR06-2	grab	Aug 31/06	A606035		0.9	12.9	0.3	0.1	
405163	95	98	3	TR06-2	chip	Aug 31/06	A606035		9.5	845.8	4.2	1.1	
405164	92	95	3	TR06-2	chip	Aug 31/06	A606035		5.1	314.5	4.8	0.5	
405165	93	93	0	TR06-2	grab	Aug 31/06	A606035		1.4	43.7	4.1	0.9	
405166	89	92	3	TR06-2	chip	Aug 31/06	A606035		9	268.5	3.1	0.8	
405167	86	89	3	TR06-2	chip	Aug 31/06	A606035		4	131.3	2.6	0.3	
405168	83	86	3	TR06-2	chip	Aug 31/06	A606035		89.1	649.4	1.1	5.9	
405169	80	83	3	TR06-2	chip	Aug 31/06	A606035		40.1	51.4	0.6	3.2	
405170	77	80	3	TR06-2	chip	Aug 31/06	A606035		50.8	94.8	1.1	2.9	
405171	74	77	3	TR06-2	chip	Aug 31/06	A606035		5.1	96.2	0.8	0.3	
405172	71	74	3	TR06-2	chip	Aug 31/06	A606035		11.2	59.2	1.1	0.9	
405173	68	71	3	TR06-2	chip	Aug 31/06	A606035		242.8	499.8	2.3	3.3	
405174	65	68	3	TR06-2	chip	Aug 31/06	A606035		65.5	124.5	0.9	3.5	
405175			0	TR06-2	Blank QFP Haystack Mtn.	Aug 31/06	A606035		1.9	6.3	0.3	0.1	
405176	62	65	3	TR06-2	chip	Aug 31/06	A606035		22.1	298.3	2.8	1.8	
405177	59	62	3	TR06-2	chip	Aug 31/06	A606035		21.3	64.5	0.6	2.2	
405178	56	59	3	TR06-2	chip	Aug 31/06	A606035		20	168.6	1	2	
405179	53	56	3	TR06-2	chip	Aug 31/06	A606035		38.5	108.1	0.6	2.7	
405180	50	53	3	TR06-2	chip	Aug 31/06	A606035		21.3	174.8	0.8	3.4	
405181	47	50	3	TR06-2	chip	Aug 31/06	A606035		77.8	724.1	0.9	7.2	
405182	44	47	3	TR06-2	chip	Aug 31/06	A606035		20.2	113.5	0.5	2.3	
405183	41	44	3	TR06-2	chip	Aug 31/06	A606035		20.2	135.6	0.5	1.7	
405184	38	41	3	TR06-2	chip	Aug 31/06	A606035		11.3	160	1	0.9	
405185	37.2	37.2	0	TR06-2	grab	Aug 31/06	A606035		87.3	>10000	15	24.3	
405186	35	38	3	TR06-2	chip	Aug 31/06	A606035		83.2	110.6	0.9	9.1	
405187	32	35	3	TR06-2	chip	Aug 31/06	A606035		17.2	72.8	0.4	1.6	
405188	29	32	3	TR06-2	chip	Aug 31/06	A606035		13	130.1	0.9	1.7	
405189	26	29	3	TR06-2	chip	Aug 31/06	A606035		119.7	146.5	2.1	15.1	
405190	23	26	3	TR06-2	chip	Aug 31/06	A606035		561.3	137.9	2.1	30.7	0.5
405191	20	23	3	TR06-2	chip	Aug 31/06	A606035		28.8	25.3	0.4	1.8	
405192	17	20	3	TR06-2	chip	Aug 31/06	A606035		68.5	25.6	0.3	5.3	
405193	14	17	3	TR06-2	chip	Aug 31/06	A606035		19.3	15.2	0.3	1.3	
405194	11	14	3	TR06-2	chip	Aug 31/06	A606035		43.9	16.6	0.6	3.3	
405195	8	11	3	TR06-2	chip	Aug 31/06	A606035		21.7	97.1	2.3	1.9	
405196	8	8	0	TR06-2	grab	Aug 31/06	A606035		24.7	211.1	2.8	1.5	
405197	6	8	2	TR06-2	chip	Aug 31/06	A606035		8.5	12.8	0.4	1.1	
405198	3	4	1	TR06-2	chip	Aug 31/06	A606035		20.4	83.9	0.6	1.7	
405199	2	3	1	TR06-2	chip	Aug 31/06	A606035		9.8	45.4	0.6	1.1	
405200					Standard CDN-GS-1C	Aug 31/06	A606035		869.1	325.2	24.3	0.2	1.0

SCHEELITE DOME - TRENCH **TR 06-2**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au g/t
Total Samples (incl. blanks/standards):				238									

SCHEELITE DOME - TRENCH **TR 06-3**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au Fire Assay g/t
400610	1.25	1.25	0	TR06-3	grab	25-Aug-06	A605884	10-Oct-06	10.7	174.9	0.8	0.8	
400611	2	5	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.4	553.7	2.1	1.4	
400612	5	8	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	15.8	636.3	2.6	2.6	
400613	8	11	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	495.7	9440.7	14.3	61.5	
400614	11	14	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	128.6	2649.9	8.8	16.1	
400615	14	16	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	44.2	4091.1	7.3	29.2	
400616	16	17.5	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	510	>10000	67.6	519.2	
400617	17.5	19.5	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	74.5	9280.3	9.1	50.2	
400618	19.5	22	2.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	25	902.1	2.2	4.9	
400619	22	25	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	15.3	894.1	3.6	2.5	
400620	25	26	1	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	3.1	479.1	5.5	1.2	
400621	26	28	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	4.5	482.1	6.1	2.6	
400622	28	30.5	2.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	5.5	430.9	10.6	1.2	
400623	30.5	33	2.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.8	307.9	6.6	1.5	
400624	33	35	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.2	260.9	3.2	1.5	
400625			0	TR06-3	BLANK:	25-Aug-06	A605884	10-Oct-06	<.5	32	0.4	0.3	
400626	35	38	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	0.9	132.3	2.1	0.8	
400627	38	41	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	123.5	4201.8	8.5	62.6	
400628	41	44	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.9	605.1	6.7	3.3	
400629	44	47	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	3.3	466.9	5.7	1.6	
400630	47	49	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	31.1	839.9	4.5	2.9	
400631	49	51	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	7.9	689	12.9	1.7	
400632	51	54	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	6.6	698	13	6.6	
400633	54	55.5	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	5.5	643.1	9.6	1	
400634	55.5	57.5	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.8	488	4.2	0.5	
400635	57.5	59	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	5	502.5	4.3	1.1	
400636	59	61	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	2.9	344	3.3	0.6	
400637	61	62	1	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	3.4	363.7	4.7	1.1	
400638	62	63.5	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	18	687.7	4.8	7.7	
400639	63.5	66	2.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	23.1	1338.4	8.8	4.8	
400640	66	68	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	7.6	798.5	10	2.1	
400641	68	71	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	8.2	456	8	1.8	
400642	71	72	1	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	13.2	555.6	15.8	2.3	
400643	72	73.5	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	22.4	220.2	3.8	1.8	
400644	73.5	75	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	27.7	244.5	4.9	1.6	
400645	75	77	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	7.2	314.7	10.5	0.6	

SCHEELITE DOME - TRENCH **TR 06-3**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au Fire Assay g/t
400646	77	79	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	20.2	421.3	13	1.1	
400647	79	80	1	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	22.1	308.4	4.5	1.6	
400648	80	83	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	18.2	2195.8	10.3	6.2	
400649	83	86	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	41.5	2264.3	9.4	10.6	
400650			0	TR06-3	Standar	25-Aug-06	A605884	10-Oct-06	890.2	345.1	30.1	0.2	
400651	86	87.5	1.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	25.1	2030.8	12.8	6.3	
400652	87.5	90	2.5	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	22.9	1215.3	4.8	3.9	
400653	90	93	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	20.6	1584.3	4.3	6.4	
400654	93	96	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	12.8	1546.8	4.2	5.8	
400655	96	99	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	10.5	1847.1	4.7	3.7	
400656	99	101	2	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	10.8	2469	3.9	6.7	
400657	101	104	3	TR06-3	chip	25-Aug-06	A605884	10-Oct-06	24.1	3318.4	5.1	15.9	
400658	104	106	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	16.6	1296.5	3.2	6.4	
400659	106	109	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	146.2	9999.5	9.7	32	
400660	109	112	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	17.2	1218.6	2.6	5.1	
400661	112	115	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2010.1	>10000	62.2	415.9	
400662	115	115	0	TR06-3	grab	26-Aug-06	A605884	10-Oct-06	14925.6	>10000	694.1	>2000	
400663	115	117	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	24.6	2725	6.1	9.3	
400664	117	119	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	145.1	3979.7	8.2	39.6	
400665	119	122	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	32.9	1391.2	3.6	6.3	
400666	122	125	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	40.1	2351.7	4.9	9.8	
400667	125	127	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	15.5	998	4.1	4.9	
400668	127	129	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	21.8	2058.6	4.1	10	
400669	129	131	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	82.3	2785.8	7.6	13.2	
400670	130.5	130.5	0	TR06-3	grab	26-Aug-06	A605884	10-Oct-06	3468	>10000	247.6	506.1	
400671	131	132	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	736	>10000	40.3	105.1	
400672	132	135	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2758.1	>10000	182.1	427.4	
400673	135	136	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	15.3	783	2.3	3.2	
400674	134	136	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	9.3	1032.2	2.5	1.8	
400675			0	TR06-3	BLANK:	26-Aug-06	A605884	10-Oct-06	5.5	302.2	0.7	1.4	
400676	136	138	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	3.7	471.6	1.5	1	
400677	138	140.5	2.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	5.1	458.7	2.6	1.1	
400678	140.5	143	2.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.9	401.5	2.1	1	
400679	143	146	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.6	501.1	3.5	1.1	
400680	146	149	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	6.8	882.1	2.5	3.9	
400681	149	152	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	<.5	263.5	2.1	0.5	

SCHEELITE DOME - TRENCH **TR 06-3**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au Fire Assay g/t
400682	152	155	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	58.8	3415.7	8	9.5	
400683	155	158	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	10	1078.6	2.6	1	
400684	158	159	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.2	481.6	2	0.6	
400685	159	159.5	0.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	<.5	197.1	1.8	0.9	
400686	159.5	162	2.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.7	463.4	2.5	1	
400687	162	164.5	2.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	<.5	189.7	2	0.2	
400688	164.5	166.5	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	<.5	288.5	2.3	1	
400689	166.5	169	2.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	0.8	233.5	1.6	0.6	
400690	169	170	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2	191.4	1.7	0.6	
400691	170	172	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	0.9	148.7	1.3	0.2	
400692	172	174	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.2	872.2	4.1	0.4	
400693	174	175	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.2	168	1.5	0.5	
400694	175	178	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	4.2	442	2.6	1.8	
400695	178	181	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.1	201.9	2.1	0.3	
400696	181	184	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.7	155.3	1.8	0.5	
400697	184	187	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.9	200.2	3.2	0.4	
400698	187	188	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.8	500.6	1.6	0.4	
400699	188	190	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	7.6	1093.2	2.1	2.6	
400700			0	TR06-3	Standar	26-Aug-06	A605884	10-Oct-06	8324.3	444	50.2	<.1	
400701	190	190	0	TR06-3	grab	26-Aug-06	A605884	10-Oct-06	24.1	4164.8	32.4	46.4	
400702	190	191	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	6.8	5209.3	4.8	1	
400703	191	191.3	0.3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.9	310.1	1.5	0.6	
400704	191.3	194	2.7	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	31.4	4403.1	9.2	7.1	
400705	194	196	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	7.8	1035.1	3.4	1.3	
400706	196	199	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	29.2	2865.5	8.3	14.2	
400707	199	200	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	17.4	1919.7	8.6	5.5	
400708	200	201	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	30.2	1718	4.3	5.7	
400709	201	203	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	61.2	4814.8	8.2	8.3	
400710	203	203	0	TR06-3	grab	26-Aug-06	A605884	10-Oct-06	5440.8	>10000	282.1	1057.5	
400711	203	205	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	9.6	907.9	1.8	2.6	
400712	205	207	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	41.6	1260.4	2.7	8.5	
400713	207	209	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	336.7	>10000	49	173.7	
400714	209	210.5	1.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1258.5	>10000	99.5	354.7	
400715	210.5	211.5	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	10	1156.8	2.4	3	
400716	211.5	213	1.5	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1878	>10000	201.8	931.3	
400717	213	215	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	72.5	6683.5	24.8	46.2	

SCHEELITE DOME - TRENCH **TR 06-3**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	ACME Certificate	Date Received	Au (ppb)	As (ppm)	Sb (ppm)	Bi (ppm)	Au Fire Assay g/t
400718	215	216	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	68.7	7874.7	26.1	34.2	
400719	216	217	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	60	>10000	30.5	21.3	
400720	217.5	217.5	0	TR06-3	grab	26-Aug-06	A605885	06-Sep	7565.7	>10000	567.8	1866.6	6.65
400721	217.5	217.5	0	TR06-3	grab	26-Aug-06	A605885	06-Sep	6150.2	>10000	484.6	1350.6	5.62
400722	217	218	1	TR06-3	chip	26-Aug-06	A605885	06-Sep	8933.1	>10000	192.8	1484.8	8.1
400723	218	219	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	182.1	>10000	38.8	43.1	
400724	219	220	1	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1352.9	>10000	83.7	312.9	
400725			0	TR06-3	BLANK:	26-Aug-06	A605884	10-Oct-06	6.4	238.9	1.3	2	
400726	220	222	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	42.4	2938.2	11	13.8	
400727	222	224	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	8.8	863	4.1	4.9	
400728	224	226	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.9	1237.5	2.7	2	
400729	226	228	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	4.7	3051	5.3	1.8	
400730	228	230	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	18.1	564.6	3.1	3.7	
400731	230	233	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	10.5	1312.9	6	4.9	
400732	233	236	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.9	661.5	5.9	1.5	
400733	236	239	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	3.1	255.3	2.8	0.9	
400734	239	242	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	4.9	205.6	1.1	1.4	
400735	242	245	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.9	275.1	2.8	0.8	
400736	245	248	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	6	758.9	4	0.8	
400737	248	251	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	15.9	3620	5.1	1	
400738	251	254	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	1.2	181.9	1.8	0.5	
400739	254	257	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.4	225.8	1.3	1.2	
400740	257	260	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.1	245.5	1.5	0.6	
400741	260	263	3	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	2.7	169.7	1.7	0.9	
400742	263	265	2	TR06-3	chip	26-Aug-06	A605884	10-Oct-06	3.4	153.5	2.3	1.4	

TOTAL SAMPLES: **128**

SCHEELITE DOME - TRENCH **TR 06-4**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Rec'd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
400789	Bottom 25' Pit North End			TR06-4	Grab	Aug 27/06	605885		11752	>10000	268.2	1020	9.88
400790	Bottom 25' Pit North End			TR06-4	Grab	Aug 27/06	605885		66.8	1403.4	2.6	8.5	
400791	Bottom 25' Pit North End			TR06-4	Grab	Aug 27/06	605884		1.8	279.2	1.8	0.4	
400792	0.0	3.0	3.0	TR06-4	Chip, Qyartzite, Apy, Scorodite, pyrite	Aug 28/06	606251		205.9	>10000	26.1	202.5	
400793	3.0	6.0	3.0	TR06-4	Chip: Quartzite with serecite partings	Aug 28/06	606251		7.1	1623.7	2.7	3.8	
400794	6.0	9.0	3.0	TR06-4	Chip: Phyllite + serecite	Aug 28/06	606251		1.9	259.9	0.9	1.3	
400795			0.0	TR06-4	Grab of Qtz-Apy vein @ 7.5 m	Aug 28/06	606251		7.6	476	1.6	1.7	
400796	9.0	12.0	3.0	TR06-4	Chip: Quartzite with serecite partings, FEOX, Mno	Aug 28/06	Missing						
400797	12.0	15.0	3.0	TR06-4	Chip: Quartzite = Serecite, Tr Apy	Aug 28/06	Missing						
400798	15.0	18.0	3.0	TR06-4	Chip: green serecitized phyllite	Aug 28/06	Missing						
400799	18.0	21.0	3.0	TR06-4	Chip; Quartzite + serecite +FEOX, MNO	Aug 28/06	606251		12	1095.8	2.5	3.3	
400800			0.0	TR06-4	STANDARD CDN-GS-10-A	Aug 28/06	606251		8172.7	429.1	46	<.1	10.09
400801	21.0	22.0	1.0	TR06-4	Chip	Aug 28/06	606251		6.6	362.6	2.5	1	
400802	22.0	23.0	1.0	TR06-4	Chip: bleached serecitic quartzite	Aug 28/06	606251		28.7	2324.1	3.4	8.7	
400803	23.0	24.0	1.0	TR06-4	Chip: bleached serecitic quartzite	Aug 28/06	606251		50.2	6922	8.6	15.4	
400804	24.0	25.0	1.0	TR06-4	Chip: Quartzite plus Apy	Aug 28/06	606251		28.3	4904.9	9.4	8.5	
400805	25.0	28.0	3.0	TR06-4	Chip: grey-green very hard silicified serecetized siltstone	Aug 28/06	606251		5.8	1099	2.7	1.3	
400806	28.0	31.0	3.0	TR06-4	Chip: grey-green very hard silicified serecetized siltstone	Aug 28/06	606251		4	467.9	2	0.9	
400807	31.0	34.0	3.0	TR06-4	Chip: grey-green very hard silicified serecetized siltstone	Aug 28/06	606251		111.2	6912.7	8.8	11	
400808	34.0	37.0	3.0	TR06-4	Chip: Sericitized quartzite, diss Apy, hard silicified, FEOX	Aug 28/06	606251		4.3	371.4	2.3	0.6	
400809	37.0	40.0	3.0	TR06-4	Chip: Quartzite with serecite, FEOX	Aug 28/06	606251		4.4	456	2.3	1	
400810			0.0	TR06-4	GRAB, coarse arsenopyrite in quartzite 41.5 m	Aug 28/06	606251		5212.1	>10000	303.2	889.6	4.15
400811	40.0	43.0	3.0	TR06-4	Chip	Aug 28/06	606251		16.4	405	2	1.1	
400812	43.0	46.0	3.0	TR06-4	Chip	Aug 28/06	606251		71.9	2429.8	4.2	12.3	
400813	46.0	49.0	3.0	TR06-4	Chip	Aug 28/06	606251		1.2	751.1	2.3	0.7	
400814	49.0	52.0	3.0	TR06-4	Chip	Aug 28/06	606251		10.2	426.2	1.8	1.9	
400815	52.0	55.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		3.4	309.7	1.5	0.6	
400816	55.0	58.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		4	244.2	1.7	1.2	
400817	58.0	61.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		5.6	3534.5	3.2	1.5	
400818	61.0	64.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		3.1	289.9	1.3	1	
400819	64.0	67.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		1.9	390.3	0.9	0.6	
400820	67.0	70.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		1	187.8	0.8	0.5	
400821	70.0	73.0	3.0	TR06-4	Chip: graphitic horizon, chalky white altered rock with FEOX	Aug 28/06	606251		0.9	269.3	1.5	0.4	
400822	73.0	76.0	3.0	TR06-4	Chip: Green serecite schist strong foliation 140/22S	Aug 28/06	606251		3.3	498.7	1.6	1	
400823	76.0	79.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		7.4	1349.4	2.8	2.5	
400824	79.0	82.0	3.0	TR06-4	Chip: green soft serecite schist very well foliated	Aug 28/06	606251		8.5	973.4	3.9	1.8	
400825			0.0	TR06-4	BLANK-QFP-Haystack Mtn.	Aug 28/06	606251		<.5	25.4	0.3	0.1	
400826	82.0	85.0	3.0	TR06-4	Chip: green soft serecite schist intrlayered quaartzite bands	Aug 28/06	606251		11.5	535.2	2.6	2.9	
400827	85.0	88.0	3.0	TR06-4	Chip: rock becoming redish FEOX, hemstite poor exposure	Aug 28/06	606251		5.7	311.5	1.8	2.1	
400828	88.0	91.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		203.1	1454.2	10.6	43.8	
400829	91.0	94.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		27.7	985.6	4.2	2.2	
400830	94.0	97.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		6.6	432.1	2.4	1.7	
400831	97.0	100.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		24	933.4	5.1	4	
400832	100.0	103.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		16.9	948.7	4.6	3.7	
400833	103.0	106.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		24.9	1330.4	7.4	6.4	
400834	106.0	109.0	3.0	TR06-4	Chip: increasing colour, serecite schist with rafts of qtzite	Aug 28/06	606251		36.8	1351.5	6.3	6.5	
400835	109.0	112.0	3.0	TR06-4	Chip: frozen orange-red phyllite MNO, FEOX FAULT	Aug 28/06	606251		44.2	3580.7	9.7	10.1	
400836	112.0	115.0	3.0	TR06-4	Chip: frozen orange-red phyllite MNO, FEOX FAULT	Aug 28/06	606251		47.8	2391.4	8	8.9	
400837	115.0	118.0	3.0	TR06-4	Chip: frozen orange-red phyllite MNO, FEOX FAULT	Aug 28/06	606251		112.5	3442	15.8	19.4	

SCHEELITE DOME - TRENCH **TR 06-4**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Rec'd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
400838	118.0	121.0	3.0	TR06-4	Chip: frozen orange-red phyllite MNO, FEOX FAULT	Aug 28/06	606251		92	2295.9	11.5	20.8	
400839	121.0	124.0	3.0	TR06-4	Chip: frozen orange-red phyllite MNO, FEOX FAULT	Aug 28/06	606251		60.3	3425.7	6.1	7.7	
400840	124.0	127.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		10.1	866.9	6	1.7	
400841	127.0	130.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		9.5	855.8	4.2	1.4	
400842	130.0	133.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		47.4	3105.2	10	6.1	
400843	133.0	136.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		23.9	496.7	11.3	2.2	
400844	136.0	139.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		4.4	373.1	9.5	0.5	
400845	139.0	142.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		4.7	369	9.5	1.1	
400846	142.0	145.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		7.5	525.1	17.4	1.4	
400847	145.0	148.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		14.9	999	14.1	1.9	
400848	148.0	151.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		5.4	395.2	9.3	1	
400849	151.0	154.0	3.0	TR06-4	Chip; Quartzite bands in phyllite	Aug 28/06	606251		22.4	754.4	7.5	3	
400850				TR06-4	STANDARD-CDN-GS-1C		606251		867.8	313	25.7	0.2	
400851	154.0	157.0	3.0	TR06-4	Chip	Aug 29/06	606251		9.7	505.8	6.6	1.7	
400852	157.0	160.0	3.0	TR06-4	Chip	Aug 29/06	606251		13.9	552.1	6	1.9	
400853	160.0	163.0	3.0	TR06-4	Chip	Aug 29/06	606251		26	1402.2	11.4	6.3	
400854	163.0	166.0	3.0	TR06-4	Chip	Aug 29/06	606251		28.2	1189.3	10.4	4.6	
400855	166.0	168.0	2.0	TR06-4	Chip	Aug 29/06	606251		18.1	1146	10.5	3	
400856	168.0	171.0	3.0	TR06-4	Chip	Aug 29/06	606251		68.6	2549.3	11.6	15.9	
400857	171.0	174.0	3.0	TR06-4	Chip	Aug 29/06	606251		44.9	941.5	22.8	3.4	
400858	174.0	176.0	2.0	TR06-4	Chip	Aug 29/06	606251		85	1054.7	12.5	7	
400859	176.0	176.0	0.0	TR06-4	Chip	Aug 29/06	606251		4.4	159.8	11.9	0.5	
400860	178.0	178.0	0.0	TR06-4	Chip	Aug 29/06	606251		3.9	341.6	22	0.9	
400861	180.0	183.0	3.0	TR06-4	Chip	Aug 29/06	606251		5.4	374.4	15.9	1	
400862	183.0	186.0	3.0	TR06-4	Chip	Aug 29/06	606251		3.1	267.5	7.4	0.4	
400863	186.0	189.0	3.0	TR06-4	Chip	Aug 29/06	606251		6	338.3	7	0.4	
400864	189.0	192.0	3.0	TR06-4	Chip	Aug 29/06	606251		11.3	517.6	6.9	0.4	
400865	192.0	193.0	1.0	TR06-4	Chip	Aug 29/06	606251		29.2	1081.7	9.7	0.7	
400866	193.0	194.0	1.0	TR06-4	Chip	Aug 29/06	606251		13	675.8	8.4	0.6	
400867	194.0	195.0	1.0	TR06-4	Chip	Aug 29/06	606251		23.5	815.4	7.9	1	
400868	195.0	198.0	3.0	TR06-4	Chip	Aug 29/06	606251		18.4	307	3.7	0.6	
400869	198.0	201.0	3.0	TR06-4	Chip	Aug 29/06	606251		27.5	325.1	3.5	0.4	
400870	201.0	202.0	1.0	TR06-4	Chip	Aug 29/06	606251		82	529.2	4.7	0.8	
400871	202.0	205.0	3.0	TR06-4	Chip	Aug 29/06	606251		1.5	126.4	1.4	0.4	
400872	205.0	208.0	3.0	TR06-4	Chip	Aug 29/06	606251		5.5	625.8	3.4	1.2	
400873	208.0	211.0	3.0	TR06-4	Chip	Aug 29/06	606251		4.7	283.5	3.8	0.4	
400874	211.0	214.0	3.0	TR06-4	Chip	Aug 29/06	606251		3.5	156.8	2.7	0.3	
400875			0.0	TR06-4	BLANK-QFP-Haystack Mtn.	Aug 29/06	606251		0.9	13	0.3	0.1	
400876	214.0	215.0	1.0	TR06-4	Chip	Aug 29/06	606251		1.5	133.7	3	0.4	
400877	215.0	216.0	1.0	TR06-4	Chip	Aug 29/06	606251		4.3	359.5	4.3	2	
400878	216.0	219.0	3.0	TR06-4	Chip	Aug 29/06	606251		1.5	109.1	1.8	0.6	
400879	219.0	222.0	3.0	TR06-4	Chip	Aug 29/06	606251		29.2	480.9	2.1	3.2	
400880	222.0	225.0	3.0	TR06-4	Chip	Aug 29/06	606251		14.6	567.1	7	2.7	
400881	225.0	227.0	2.0	TR06-4	Chip	Aug 29/06	606251		21.3	454.7	2.8	2.2	
400882	227.0	230.0	3.0	TR06-4	Chip	Aug 29/06	606251		9.3	284.6	3.2	1.4	
400883	230.0	232.0	2.0	TR06-4	Chip	Aug 29/06	606251		6.6	378.3	2.8	2.6	
400884	232.0	235.0	3.0	TR06-4	Chip	Aug 29/06	606251		7.4	408.9	2.4	1.6	
400885	235.0	237.0	2.0	TR06-4	Chip	Aug 29/06	606251		24.7	554.1	4.2	3.8	
400886	237.0	239.0	2.0	TR06-4	Chip	Aug 29/06	606251		49.9	1170.9	6.3	6.8	

SCHEELITE DOME - TRENCH **TR 06-4**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Rec'd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
400887	239.0	241.0	2.0	TR06-4	Chip	Aug 29/06	606251		4.5	321.6	2.3	0.9	
400888	241.0	243.0	2.0	TR06-4	Chip	Aug 29/06	606251		42	779.5	5.4	3.3	
400889	243.0	245.0	2.0	TR06-4	Chip	Aug 29/06	606251		57.9	2414.5	11.7	8.9	
400890	245.0	247.0	2.0	TR06-4	Chip	Aug 29/06	606251		43.9	2923.5	5.7	7.4	
400891	247.0	249.0	2.0	TR06-4	Chip	Aug 29/06	606251		7.7	645.6	3.4	1.8	
400892	249.0	251.0	2.0	TR06-4	Chip	Aug 29/06	606251		6.2	340.7	2	0.7	
400893	251.0	253.0	2.0	TR06-4	Chip	Aug 29/06	606251		6.8	480.2	4.2	0.9	
400894	253.0	255.0	2.0	TR06-4	Chip	Aug 29/06	606251		<.5	270.7	2.6	0.6	
400895	255.0	255.5	0.5	TR06-4	Chip	Aug 29/06	606251		19.7	520.4	6	2	
400896	255.5	258.0	2.5	TR06-4	Chip	Aug 29/06	606251		150.9	1966.9	4.6	10.7	
400897	258.0	259.0	1.0	TR06-4	Chip	Aug 29/06	606251		42.6	744.6	10.2	2.3	
400898	259.0	260.0	1.0	TR06-4	Chip	Aug 29/06	606251		4.1	146.9	5.1	0.3	
400899	260.0	262.0	2.0	TR06-4	Chip	Aug 29/06	606251		19.2	805.6	4	1.4	
400900			0.0	TR06-4	STANDARD CDN-GS-10-A	Aug 29/06	606251		9850.9	457.4	53.5	<.1	10.24
400901	262.0	264.0	2.0	TR06-4	Chip	Aug 29/06	606251		24.7	1042.8	3.3	1.6	
400902	264.0	266.0	2.0	TR06-4	Chip	Aug 29/06	606251		18.3	1426.4	1.8	1.9	
400903	238.0	238.0	0.0	TR06-4	Chip	Aug 29/06	606251		2.3	107	1.1	0.2	
400904	Al's Grab	30.0		TR06-4	GRAB: Apy in green clayey, oxidized boxwork.	Aug 29/06	606251		2112.9	>10000	418.7	244.5	1.88
400905	Al's Grab	35.0		TR06-4	GRAB: of Quartzite with serecite pasrtings, clusters of Apy t	Aug 29/06	606251		54	2547.6	5.9	5.6	
400906	Al's Grab	125.0		TR06-4	Grab: Red ochre oxidized	Aug 29/06	606252		2417	>10000	121.9	288.2	2.47

TOTAL SAMPLES: **61.0**

SCHEELITE DOME - TRENCH **TR 06-5**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	certificate	Date	Au ppb	As ppm	Sb ppm	Bi ppm
400743	0	2	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	4.5	418.2	3.9	0.8
400744	2	4	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	4.5	308	5	0.6
400745	4	6	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	3.9	4961	10.8	1
400746	6	8	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	4.3	1051.8	6.6	0.7
400747	8	10	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	2.2	599.9	3.7	0.3
400748	10	12	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	2.5	543.8	4.1	0.5
400749	12	14	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	2.9	355.8	1.8	0.4
400750					Standard CDN-GS-1C		A605884	10-Oct-06	938.1	328.6	30.7	0.2
400751	14	16	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	4.8	127.4	0.8	0.3
400752	16	18	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	14.7	496.6	2.6	0.7
400753	18	20	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	1.7	209.7	1.8	0.9
400754	20	22	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	1	186.7	1.8	0.3
400755	22	24	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	3	170.2	2	0.5
400756	24	26	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	3.1	457.2	4	0.4
400757	26	28	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	14.8	511.4	4.2	4.4
400758	28	30	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	20.9	457.9	10.1	1.5
400759	30	32	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	12	323.2	7.7	1.6
400760	32	34	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	13.7	379	9.1	1.7
400761	34	36	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	18.1	716.8	11.4	1.2
400762	36	38	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	13	1129.6	5.8	2.4
400763	38	40	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	19.2	1014.1	6.1	3.5
400764	40	42	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	23.6	1761.6	5.1	13.3
400765	42	44	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	6.4	673.6	6.7	3.4
400766	44	46	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	36.5	1531.1	7	7.2
400767	46	48	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	13.1	701.4	5.6	4.7
400768	48	50	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	25.1	1429	7.3	7
400769	50	52	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	31.5	1482.5	10.1	11.1
400770	52	54	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	21.1	1262.7	12.1	5.5
400771	54	56	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	35.5	2387.9	13.2	6.5
400772	56	58	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	36.9	2450.5	13.7	12.4
400773	58	60	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	31.8	1734.3	12.1	6.4
400774	60	62	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	42.3	1767.2	8	5.6
400775					Blank QFP Haystack Mtn.	27-Aug-06	A605884	10-Oct-06	1.8	114.5	1.3	0.6
400776	62	64	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	14.1	1244.3	5.8	4.2
400777	64	66	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	35.4	2497	5.8	5.4
400778	66	68	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	55.3	3100.9	6.5	8.2
400779	68	70	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	46.2	2162.1	10	6.9
400780	70	72	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	28.3	1447.2	7	6.7
400781	72	74	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	32.9	1349.1	4.8	6.6
400782	74	76	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	23.1	1806.3	9.3	6
400783	76	78	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	7.8	629	4	2.1
400784	78	80	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	23.6	1673.1	6.4	4.6
400785	80	82	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	32	2248.9	4.6	7.4

SCHEELITE DOME - TRENCH **TR 06-5**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	certificate	Date	Au ppb	As ppm	Sb ppm	Bi ppm
400786	82	84	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	107.2	3996.1	6.8	14.6
400787	84	86	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	44	2274.5	4.6	8.2
400788	86	88	2	TR 06-5	chip	27-Aug-06	A605884	10-Oct-06	64.7	3999.6	6.2	14.5

TOTAL SAMPLES: **46**

SCHEELITE DOME - TRENCH **TR 06-6**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date Rcvd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
400907	1	3	2	TR06-6	chip	Aug 30/06	606251		7.3	1090.1	9	5.3	
400908	3	4.5	1.5	TR06-6	chip	Aug 30/06	606251		4	2951.7	10.4	21.1	
400909	4.5	5	0.5	TR06-6	chip	Aug 30/06	606251		<.5	441.1	7.4	1.8	
400910	5	7	2	TR06-6	chip	Aug 30/06	606251		2.5	368.7	5.2	2.6	
400911	7	7.5	0.5	TR06-6	chip	Aug 30/06	606251		5.1	447.9	6.5	2.1	
400912	7.5	8	0.5	TR06-6	chip	Aug 30/06	606251		291.7	>10000	213.3	89.9	
400913	8	8.75	0.75	TR06-6	chip	Aug 30/06			7.1	765	12.2	3	
400914	8.75	10	1.25	TR06-6	chip	Aug 30/06			7.3	1361.6	19.1	2.5	
400915	10	10	0	TR06-6	grab	Aug 30/06			3.2	247.3	2.2	4.1	
400916	10	12	2	TR06-6	chip	Aug 30/06			3.5	518.6	10.7	0.9	
400917	12	14	2	TR06-6	chip	Aug 30/06			5.8	624.6	13.2	1.2	
400918	14	15	1	TR06-6	chip	Aug 30/06			25.7	3836.4	15.9	18.3	
400919	15	17	2	TR06-6	chip	Aug 30/06			34.5	2776.1	33.8	26.3	
400920	17	18.5	1.5	TR06-6	chip	Aug 30/06			14.8	1100.7	16.2	7.7	
400921	18.5	20	1.5	TR06-6	chip	Aug 30/06			65.8	6426.1	37.5	39.9	
400922	20	21	1	TR06-6	chip	Aug 30/06			33.2	6178.6	26.2	23	
400923	21	22	1	TR06-6	chip	Aug 30/06			5.7	497	11.5	2	
400924	22	23	1	TR06-6	chip	Aug 30/06			65.2	3912.4	11.7	26.8	
400925			0	TR06-6	Blank QFP Haystack Mtn.	Aug 30/06			3	45	0.5	0.5	
400926	22.5	22.5	0	TR06-6	chip	Aug 30/06			4	202.2	2.7	1.3	
400927	23	24.75	1.75	TR06-6	chip	Aug 30/06	606035		31.1	4987.4	19.7	20.4	
400928	24.5	24.5	0	TR06-6	grab	Aug 30/06	606035		25.1	1025.7	5.2	5.1	
400929	24.75	24.75	0	TR06-6	chip	Aug 30/06	606035		15.2	1026.9	11.9	4.8	
400930	26	28	2	TR06-6	chip	Aug 30/06	606035		12.6	854.5	15.8	2.9	
400931	27	27	0	TR06-6	grab	Aug 30/06	606035		737.9	>10000	38.1	132.9	0.79
400932	28	30	2	TR06-6	chip	Aug 30/06	606035		7.3	518.4	22.1	6	
400933	30	32	2	TR06-6	chip	Aug 30/06	606035		10	648.3	12.7	2.7	
400934	32	32.8	0.8	TR06-6	chip	Aug 30/06	606035		5.6	568.8	8	1.8	
400935	32.8	33	0.2	TR06-6	chip	Aug 30/06	606035		14.2	973.7	4.7	4.3	
400936	33	34	1	TR06-6	chip	Aug 30/06	606035		6	575.3	9.8	1.3	
400937	34	35	1	TR06-6	chip	Aug 30/06	606035		66.7	1207.2	12.2	1.4	
400938	35	36.5	1.5	TR06-6	chip	Aug 30/06	606035		7	560.6	7.4	0.5	
400939	36.5	37	0.5	TR06-6	chip	Aug 30/06	606035		27.7	734.6	12.9	1.7	
400940	37	38	1	TR06-6	chip	Aug 30/06	606035		62.3	2640.9	11.8	10.2	
400941	38	39	1	TR06-6	chip	Aug 30/06	606035		29.1	971.1	8.8	1.2	
400942	39	39	0	TR06-6	grab	Aug 30/06	606035		24.8	756.4	10.5	2.6	
400943	39	40	1	TR06-6	chip	Aug 30/06	606035		7.3	243.1	12.9	1	
400944	40	41	1	TR06-6	chip	Aug 30/06	606035		16.4	836.9	13.4	2.4	
400945	41	42.5	1.5	TR06-6	chip	Aug 30/06	606035		7.6	592.1	8.8	7.6	

SCHEELITE DOME - TRENCH **TR 06-6**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date Rcvd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
400946	42.5	44	1.5	TR06-6	chip	Aug 30/06	606035		7.2	417.5	31.5	1.8	
400947	44	45.5	1.5	TR06-6	chip	Aug 30/06	606035		9.4	512	19.2	2	
400948	46	46	0	TR06-6	grab	Aug 30/06	606035		20.2	284.6	27	1.5	
400949	45	45	0	TR06-6	grab	Aug 30/06	606035		70.8	5393.8	100.5	150.7	
400950			0	TR06-6	Standard CDN-GS-1C	Aug 30/06	606035		831.5	333.1	25.8	0.3	

Total Samples (incl. blanks/standards): 44

SCHEELITE DOME - TRENCH **TR 06-7**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date Rcvd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
405051	46	46	0	TR06-7	grab	Aug 30/06	606035	11-Sep	375.7	>10000	31.3	49.2	
405052	1.5	3	1.5	TR06-7	chip	Aug 30/06	606035		3	498.4	4.2	2.5	
405053	3	5	2	TR06-7	chip	Aug 30/06	606035		7	628.4	4.8	2.4	
405054	5	7	2	TR06-7	chip	Aug 30/06	606035		4.6	369.3	2.2	1.5	
405055	7	9	2	TR06-7	chip	Aug 30/06	606035		2.8	628	3.7	1.2	
405056	9	11	2	TR06-7	chip	Aug 30/06	606035		121.3	>10000	5.9	24.5	
405057	11	12.5	1.5	TR06-7	chip	Aug 30/06	606035		14.5	1216.9	4.2	6.1	
405058	12.5	13.5	1	TR06-7	chip	Aug 30/06	606035		4.9	838.7	4.4	1.5	
405059	13.5	15	1.5	TR06-7	chip	Aug 30/06	606035		30.2	567	9	69.6	
405060	15	16	1	TR06-7	chip	Aug 30/06	606035		6.9	555.3	4.4	5.7	
405061	16	17	1	TR06-7	chip	Aug 30/06	606035		4.1	898.5	5.7	2.5	
405062	17	19	2	TR06-7	chip	Aug 30/06	606035		3	410.8	4.8	1.5	
405063	19	20	1	TR06-7	chip	Aug 30/06	606035		28.2	1522.2	13.1	46.8	
405064	19.5	19.5	0	TR06-7	grab	Aug 30/06	606035		8.9	234.2	5.2	2.2	
405065	20	21	1	TR06-7	chip	Aug 30/06	606035		7.6	1186.4	13.9	6.3	
405066	21.5	21.5	0	TR06-7	grab	Aug 30/06	606035		208.7	>10000	16.1	171.3	
405067	21	23	2	TR06-7	chip	Aug 30/06	606035		130.5	>10000	21.9	93.3	
405068	23	23	0	TR06-7	grab	Aug 30/06	606035		300.6	>10000	21	51.1	
405069	23	24	1	TR06-7	chip	Aug 30/06	606035		176.9	>10000	11.8	17.9	
405070	24.3	24.3	0	TR06-7	grab	Aug 30/06	606035		728.9	>10000	52.9	460.6	0.71
405071	23	24	1	TR06-7	chip	Aug 30/06	606035		12.5	1195.3	7.8	11.8	
405072	23.5	23.5	0	TR06-7	grab	Aug 30/06	606035		321.3	>10000	43.5	316.2	
405073	24	25	1	TR06-7	chip	Aug 30/06	606035		29.4	2025.6	11	15.7	
405074	25	26	1	TR06-7	chip	Aug 30/06	606035		58.5	>10000	12.7	28.7	
405075			0	TR06-7	Blank QFP Ha	Aug 30/06	606035		2.5	59.3	0.6	0.5	
405076	26	27	1	TR06-7	chip	Aug 30/06	606035		15.6	1694.3	11.5	7.8	
405077	26	26	0	TR06-7	grab	Aug 30/06	606035		599.5	>10000	33	357.2	0.59
405078	26.5	26.5	0	TR06-7	grab	Aug 30/06	606035		2.7	282.1	3.3	1.1	
405079	27	28	1	TR06-7	chip	Aug 30/06	606035		22	487.3	10	10.4	
405080	28	29	1	TR06-7	chip	Aug 30/06	606035		461.5	>10000	13.9	40.1	
405081	29	30	1	TR06-7	chip	Aug 30/06	606035		139.8	2632.5	10.3	2.6	
405082	30	31.5	1.5	TR06-7	chip	Aug 30/06	606035		12.5	1053.5	15.5	2.1	
405083	31.5	33	1.5	TR06-7	chip	Aug 30/06	606035		7.7	795.5	23.8	2	
405084	33	35	2	TR06-7	chip	Aug 30/06	606035		4.1	772.7	8.2	0.8	
405085	35	37	2	TR06-7	chip	Aug 30/06	606035		15.7	1544.7	10.9	2.8	
405086	37	39	2	TR06-7	chip	Aug 30/06	606035		50.4	4316	12.6	3.8	
405087	39	39.5	0.5	TR06-7	chip	Aug 30/06	606035		28.7	1707.4	18.7	8.3	

SCHEELITE DOME - TRENCH **TR 06-7**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date Rcvd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
405088	39.5	40	0.5	TR06-7	chip	Aug 30/06	606035		41.3	2428.4	32	43.5	
405089	40	40	0	TR06-7	grab	Aug 30/06	606035		665.7	>10000	346.7	136.3	0.69
405090	40	41	1	TR06-7	chip	Aug 30/06	606035		5.7	1216.3	25.8	1.8	
405091	41	43	2	TR06-7	chip	Aug 30/06	606035		10.1	2084.9	34.9	2.1	
405092	43	43.5	0.5	TR06-7	chip	Aug 30/06	606035		2.2	799.5	16.2	0.6	
405093	43.5	44.5	1	TR06-7	chip	Aug 30/06	606035		495.6	>10000	206.7	9.2	
405094	43.5	43.5	0	TR06-7	grab	Aug 30/06	606035		867.9	>10000	412.2	6.4	0.89
405095	45	45	0	TR06-7	grab	Aug 30/06	606035		38.8	3608.4	20.5	2.1	

Total Samples: 45 incl. blanks and standards

SCHEELITE DOME - TRENCH **TR 06-8**

Sample #	From (m)	To (m)	Length (m)	Trench #	Type	Date	Certificate	Date Rcvd	Au ppb	As ppm	Sb ppm	Bi ppm	Au g/t
405096	2.5	4	1.5	TR06-8	chip	Aug 30/06	606035		7.9	771.9	5.9	5.6	
405097	4	6	2	TR06-8	chip	Aug 30/06	606035		5.1	503.3	6.4	1.1	
405098	6	8	2	TR06-8	chip	Aug 30/06	606035		3.2	445.3	6.3	0.9	
405099	8	10	2	TR06-8	chip	Aug 30/06	606035		5.5	730.4	7.4	1.3	
405100			0	TR06-8	Standard CDN-GS-10A	Aug 30/06	606035		8946.3	449.9	48.2	<.1	10.17
405101	10	12	2	TR06-8	chip	Aug 30/06	606035		13.1	1236.2	9.5	2.3	
405102	12	12	0	TR06-8	grab	Aug 30/06	606035		206.8	9698.2	14.1	31	
405103	12	14	2	TR06-8	chip	Aug 30/06	606035		49.2	1983.3	4.6	2.1	
405104	14	15	1	TR06-8	chip	Aug 30/06	606035		11.1	556.9	3.1	1.4	
405105	16	16	0	TR06-8	grab	Aug 30/06	606035		146.8	6943.9	5.4	19.6	
405106	14	14	0	TR06-8	grab	Aug 30/06	606035		4460	>10000	327.5	1424.5	4.29
405107	17	18	1	TR06-8	chip	Aug 30/06	606035		1453.9	>10000	85.3	444.7	1.37
405108	18	20	2	TR06-8	chip	Aug 30/06	606035		334.6	>10000	15	105.2	
405109	20	21	1	TR06-8	chip	Aug 30/06	606035		8.7	710.2	1.6	2.7	
405110	21	23	2	TR06-8	chip	Aug 30/06	606035		23.9	931.1	1.7	6.1	
405111	23	24	1	TR06-8	chip	Aug 30/06	606035		20.2	1420.2	3.3	2.5	
405112	24	24.4	0.4	TR06-8	chip	Aug 30/06	606035		2.1	73.5	1.1	0.1	
405113	24.4	26	1.6	TR06-8	chip	Aug 30/06	606035		3.3	334.3	2	0.5	
405114	26	28	2	TR06-8	chip	Aug 30/06	606035		6.3	485.4	1.7	0.5	
405115	28	29.5	1.5	TR06-8	chip	Aug 30/06	606035		2.1	312.7	3.7	0.3	
405116	29.5	31.5	2	TR06-8	chip	Aug 30/06	606035		2	283.9	1.7	0.6	
405117	31.5	33	1.5	TR06-8	chip	Aug 30/06	606035		2	316.7	3	1.1	
405118	33	35	2	TR06-8	chip	Aug 30/06	606035		2.8	292.8	2.7	0.7	
405119	35	37	2	TR06-8	chip	Aug 30/06	606035		5.7	396.8	3.1	0.6	
405120	37	39	2	TR06-8	chip	Aug 30/06	606035		19.5	846.7	8.1	2.3	
405121	39	39	0	TR06-8	grab	Aug 30/06	606035		21.5	1882.9	9.3	3.6	

Total Samples: 26 Incl. Blanks/Standards

APPENDIX B - ANALYTICAL DATA

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A607039

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Greg Dawson

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	4.1	7.2	64	<.1	3.5	4.3	523	1.80	<.5	2.6	.5	3.9	59	.1	<.1	.1	39	.46	.068	6	9	.55	187	.099	1	.84	.051	.46	.1	.01	1.8	.3	<.05	5	<.5	-
397501	4.7	779.3	8.3	55	.2	6.3	6.6	240	4.56	<.5	1.4	2.6	4.9	64	.4	<.1	.3	145	.22	.038	12	20	1.82	678	.155	1	2.83	.072	1.33	.2	<.01	15.8	.3	.44	10	5.0	3.00
397502	6.0	59.8	6.2	5	.4	.6	.7	15	1.88	<.5	.4	3.5	8.6	45	<.1	<.1	.5	3	.01	.016	14	4	.03	79	.005	<1	.23	.158	.20	.1	.01	2.1	.1	.82	1	7.1	3.00
397503	1.1	92.9	3.2	15	<.1	.9	1.0	82	1.43	<.5	2.2	4.9	13.1	24	<.1	.1	.3	11	.03	.018	16	5	.41	85	.047	1	.88	.040	.38	.1	<.01	1.4	.1	.27	3	1.1	6.00
397504	1.3	64.3	3.6	20	.1	1.1	6.6	50	3.78	<.5	2.7	7.2	9.2	17	<.1	.1	1.0	6	.02	.017	7	5	.20	23	.012	1	.47	.040	.31	.2	.01	.8	.2	3.78	2	6.7	6.00
397505	.8	101.2	4.0	27	.1	1.7	5.9	123	1.81	<.5	3.1	14.5	12.2	18	.2	<.1	.8	10	.13	.028	16	7	.38	79	.042	1	.66	.036	.31	.1	.01	1.6	.2	1.37	2	1.7	6.50
397506	1.6	210.6	3.9	27	<.1	3.5	10.7	166	3.16	<.5	2.5	8.3	7.3	10	<.1	.1	.3	59	.09	.026	7	16	.93	57	.088	1	1.35	.029	.68	<.1	.01	5.7	.3	1.98	5	2.4	6.50
397507	3.9	66.6	2.8	30	<.1	1.1	6.4	92	3.19	<.5	2.1	7.4	7.3	4	.1	.1	1.2	5	.05	.013	10	6	.25	35	.010	1	.49	.019	.28	.1	.01	.8	.1	3.43	1	4.5	7.20
RE 397507	3.8	66.1	2.7	32	<.1	1.2	6.0	91	3.19	.6	2.1	7.5	7.3	4	.1	.1	1.2	4	.05	.013	10	6	.24	31	.009	<1	.47	.019	.26	.1	.01	.8	.1	3.32	1	4.8	-
RRE 397507	3.7	69.8	3.8	33	<.1	.9	5.7	93	3.22	.7	2.2	5.9	7.9	4	.1	.1	1.2	5	.05	.013	11	4	.25	36	.008	<1	.47	.019	.26	.1	.01	.6	.1	3.21	1	4.6	-
397508	1.6	83.5	2.1	23	<.1	1.2	3.2	87	1.42	<.5	2.5	2.6	12.3	3	.2	.1	.7	3	.03	.014	9	6	.19	59	.010	<1	.41	.029	.22	.1	<.01	.4	.1	1.29	1	2.2	6.20
397509	5.5	29.6	2.6	9	<.1	.6	3.2	17	1.63	<.5	1.9	1.6	9.6	3	<.1	<.1	.6	1	.02	.012	9	4	.02	50	.001	<1	.26	.014	.16	<.1	<.01	.3	<.1	1.73	1	2.0	4.00
397510	.7	38.0	2.2	19	<.1	1.4	.8	65	.36	<.5	.6	1.6	.9	17	<.1	.1	<.1	2	.04	.005	2	13	.07	38	.004	<1	.29	.051	.04	.1	<.01	.5	<.1	<.05	1	<.5	5.00
397511	5.5	30.1	3.1	14	<.1	.9	4.1	23	2.76	.9	3.0	1.0	11.4	3	.1	.1	1.1	2	.05	.020	10	5	.03	50	.002	<1	.26	.015	.16	.1	<.01	.3	<.1	3.02	1	3.2	5.50
397512	3.5	32.7	2.8	31	.1	1.4	6.9	117	2.87	<.5	2.6	3.0	10.8	5	.3	<.1	1.0	5	.09	.028	22	6	.29	43	.018	<1	.51	.025	.33	.1	<.01	1.0	.1	3.01	2	3.0	5.90
397513	1.3	17.9	1.7	11	<.1	1.7	8.2	34	3.06	<.5	3.0	5.8	9.4	5	.1	<.1	.9	5	.07	.026	16	4	.21	43	.010	<1	.40	.010	.25	.1	<.01	.5	.1	3.16	1	4.4	3.00
397514	2.5	110.5	2.5	34	.1	7.7	20.3	226	6.11	<.5	2.1	9.0	2.8	57	.4	.1	.6	68	.29	.050	9	12	1.67	36	.097	1	1.59	.035	.95	.1	.01	5.8	.4	5.06	5	5.8	4.70
397515	3.1	13.2	1.4	22	<.1	2.2	8.3	63	2.57	<.5	1.6	2.0	5.2	13	.1	<.1	.3	13	.09	.028	9	5	.47	49	.021	1	.61	.018	.36	<.1	<.01	1.1	.2	2.23	1	3.0	7.10
397516	2.4	16.0	1.5	7	<.1	1.3	4.9	37	2.25	<.5	2.5	.7	5.4	8	.1	<.1	.4	2	.22	.022	12	6	.09	44	.005	<1	.34	.018	.18	.1	<.01	.6	.1	2.26	1	3.1	6.60
397517	5.2	47.4	5.2	43	1.5	6.8	16.7	274	4.87	1.4	1.7	4.0	2.1	24	.1	5.5	.6	64	.54	.034	8	18	1.74	20	.090	1	1.76	.048	.89	.1	.02	6.3	.4	3.53	5	4.9	4.60
397518(pulp)	6.6	61.0	19.3	102	2.0	16.0	7.7	155	3.01	327.4	.1	940.6	.5	7	.4	36.0	.2	16	.18	.040	8	27	.09	26	.002	2	.35	.004	.22	.5	3.94	1.7	4.0	2.00	2	10.1	-
397519(rock)	1.7	10.9	13.3	66	<.1	4.7	5.8	491	2.86	4.8	1.8	<.5	10.1	98	.1	.3	.1	67	.90	.186	27	9	.53	488	.186	1	.99	.119	.18	.8	.01	4.9	<.1	<.05	5	<.5	2.70
397520	1.4	19.2	1.5	12	<.1	1.7	8.7	36	3.18	<.5	2.5	5.9	8.5	6	.1	<.1	.8	5	.08	.024	16	5	.21	24	.011	<1	.44	.012	.27	.1	.01	.7	.1	3.29	1	4.0	3.10
STANDARD DS7	20.8	108.7	70.0	395	.9	55.3	9.4	631	2.41	49.6	5.2	68.5	4.9	93	6.6	6.3	4.7	86	.94	.079	14	166	1.05	378	.121	38	.97	.082	.44	3.8	.21	2.5	4.3	.15	5	3.8	-

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: DRILL CORE R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

11-02-06 A09:39 OUT

Data 1 FA ____ **DATE RECEIVED:** SEP 25 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A606251R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Au** gm/mt	Sample gm
400800 (pulp)	10.09	7.3
400810	4.15	29.2
400850 (pulp)	1.02	7.3
400900 (pulp)	10.24	7.3
400904	1.88	29.2
400906	2.47	29.2
STANDARD SL20	5.95	29.2

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: ROCK PULP

10-30-06 P06:03 OUT

Data 1 FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.) 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A606251 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	2.8	2.9	44	<.1	11.4	4.7	534	1.86	1.0	2.9	<.5	4.6	65	<.1	<.1	.1	36	.54	.071	8	11	.58	202	.131	<1	1.04	.088	.51	.1	<.01	2.1	.3	<.05	5	<.5	-
400792	.3	59.5	17.4	15	.5	8.3	2.4	68	2.69	>10000	.6	205.9	9.2	21	.4	26.1	202.5	5	.02	.012	13	12	.08	73	.004	4	.44	.012	.21	1.9	.01	.8	.2	.33	1	13.7	5.10
400793	.2	29.2	16.0	17	<.1	15.0	5.8	111	1.41	1623.7	1.0	7.1	11.8	13	.3	2.7	3.8	6	.02	.016	22	13	.12	87	.007	3	.54	.014	.28	.1	<.01	.9	.2	<.05	2	.7	6.90
400794	.2	24.9	6.6	25	<.1	19.0	8.2	164	1.59	259.9	1.0	1.9	8.8	7	.1	.9	1.3	7	.02	.022	19	14	.15	89	.011	6	.69	.013	.41	<.1	.01	1.1	.3	<.05	2	<.5	5.40
400795	.3	17.5	8.0	7	.1	6.5	3.2	70	.90	476.0	.3	7.6	1.4	9	.1	1.6	1.7	2	.05	.026	5	14	.04	62	.002	2	.20	.007	.08	<.1	.01	.4	.1	<.05	1	<.5	1.30
RE 400795	.2	18.7	8.1	7	.1	7.5	3.3	70	.90	475.5	.3	4.3	1.5	9	.1	1.5	1.6	2	.05	.025	5	14	.04	63	.002	3	.19	.007	.08	<.1	.01	.4	.1	<.05	1	<.5	-
400799	.3	23.2	6.5	12	<.1	7.0	2.7	65	1.26	1095.8	.6	12.0	7.6	10	.1	2.5	3.3	4	.02	.009	14	13	.06	66	.003	8	.45	.014	.20	.1	.01	.8	.2	<.05	1	.6	7.40
400800 (pulp)	8.0	57.8	3.6	41	9.0	240.2	11.4	157	3.12	429.1	.1	8172.7	.4	5	<.1	46.0	<.1	15	.12	.035	6	270	.06	27	.002	1	.29	.006	.20	.7	6.73	1.4	8.5	1.89	1	27.3	-
400801	.2	35.1	6.5	13	.1	12.9	3.5	54	1.48	362.6	.6	6.6	8.0	5	.1	2.5	1.0	4	.01	.014	15	10	.04	52	.002	5	.47	.013	.20	<.1	.03	.8	.1	<.05	1	1.0	3.00
400802	.2	38.3	8.4	16	.2	9.7	4.1	82	1.80	2324.1	.9	28.7	10.3	17	.2	3.4	8.7	6	.01	.019	22	14	.11	81	.003	5	.60	.013	.29	.1	.02	1.1	.3	.07	2	2.5	3.10
400803	.3	37.1	13.2	10	.2	4.0	2.1	62	2.42	6922.0	.6	50.2	9.1	33	.2	8.6	15.4	4	.01	.018	20	12	.06	78	.003	3	.39	.009	.29	.2	.02	.8	.2	.07	2	2.2	3.10
400804	.3	27.7	11.3	12	.2	4.8	1.7	70	2.07	4904.9	.6	28.3	9.9	13	.2	9.4	8.5	8	.01	.018	17	19	.18	73	.005	4	.65	.013	.27	.1	.01	1.1	.3	<.05	2	1.8	2.40
400805	.2	27.3	5.2	27	<.1	10.7	5.2	164	2.19	1099.0	1.0	5.8	8.3	12	.1	2.7	1.3	9	.07	.041	19	21	.45	49	.007	3	1.10	.009	.28	<.1	<.01	1.2	.3	<.05	3	.7	6.40
400806	.2	33.9	4.5	42	<.1	19.5	7.5	187	2.97	467.9	1.7	4.0	13.6	12	.1	2.0	.9	12	.06	.044	31	23	.64	82	.020	3	1.73	.011	.52	<.1	<.01	1.5	.6	<.05	4	.6	6.10
400807	.4	54.9	11.7	20	.4	7.7	3.8	87	2.70	6912.7	1.1	111.2	10.0	12	.1	8.8	11.0	7	.05	.040	25	15	.31	64	.009	2	.92	.011	.37	.7	.01	1.1	.4	.10	2	3.0	6.20
400808	.2	23.8	4.1	20	<.1	7.8	4.5	134	1.52	371.4	.7	4.3	9.3	5	.1	2.3	.6	9	.01	.010	17	21	.27	35	.003	1	.76	.015	.13	<.1	<.01	1.0	.2	<.05	2	<.5	5.60
400809	.2	28.9	4.8	28	<.1	14.0	7.2	150	1.73	456.0	.7	4.4	8.5	7	.1	2.3	1.0	8	.02	.010	17	16	.27	44	.003	4	.77	.010	.15	<.1	<.01	1.0	.2	<.05	2	<.5	7.10
400810	.5	80.4	124.3	13	8.1	6.8	5.1	34	14.41	>10000	.6	5212.1	5.6	6	.5	303.2	889.6	2	.01	.012	4	7	.02	30	.002	2	.14	.004	.07	1.0	.10	.6	.2	2.64	<1	>100	.80
400811	.2	25.8	4.6	21	<.1	14.3	5.4	132	1.29	405.0	.7	16.4	7.8	8	.1	2.0	1.1	4	.04	.009	16	10	.13	39	.002	3	.54	.009	.14	<.1	.01	.8	.1	<.05	1	<.5	6.90
400812	.3	40.7	6.5	25	.2	18.9	5.2	175	1.74	2429.8	.9	71.9	8.1	10	.1	4.2	12.3	4	.04	.010	18	11	.10	60	.001	6	.71	.008	.21	.1	.01	.9	.2	<.05	1	1.3	6.60
400813	.2	37.7	4.8	16	.1	12.3	4.7	78	1.47	751.1	.8	1.2	9.1	8	.1	2.3	.7	3	.03	.013	18	9	.06	57	.001	5	.48	.011	.19	<.1	.01	.9	.2	<.05	1	<.5	6.10
400814	.2	24.2	3.9	14	<.1	10.6	4.3	63	1.37	426.2	.6	10.2	8.3	6	<.1	1.8	1.9	4	.02	.012	16	11	.04	65	.001	7	.42	.012	.21	<.1	.01	.9	.1	<.05	1	<.5	7.50
400815	.2	35.2	5.1	15	<.1	8.2	3.5	48	1.84	309.7	1.0	3.4	10.9	8	.1	1.5	.6	4	.04	.033	23	9	.04	70	.002	6	.45	.014	.24	<.1	<.01	.9	.2	<.05	1	<.5	6.00
400816	.3	41.9	5.4	36	<.1	12.9	4.0	68	2.42	244.2	1.1	4.0	12.7	8	.1	1.7	1.2	7	.02	.023	28	14	.20	66	.002	7	1.03	.013	.27	<.1	<.01	1.5	.2	<.05	2	<.5	5.70
400817	.3	54.2	4.7	13	.1	7.2	3.6	40	2.20	3534.5	1.1	5.6	9.1	7	.1	3.2	1.5	4	.02	.033	20	11	.03	41	.001	7	.40	.011	.21	<.1	.01	1.4	.2	.06	1	2.2	6.10
400818	.4	64.4	3.0	29	.2	12.3	5.6	91	3.14	289.9	1.6	3.1	14.5	8	<.1	1.3	1.0	4	.02	.053	44	7	.02	36	.001	5	.38	.008	.21	<.1	.02	1.0	.1	<.05	1	<.5	7.50
400819	.3	107.1	3.2	49	<.1	20.2	10.3	96	3.44	390.3	2.5	1.9	18.5	9	<.1	.9	.6	5	.03	.077	47	8	.03	37	.001	5	.52	.012	.21	<.1	.02	1.4	.1	<.05	1	.5	5.30
400820	.4	81.4	2.6	75	<.1	49.4	17.8	268	4.09	187.8	3.1	1.0	18.5	10	<.1	.8	.5	5	.05	.077	55	6	.02	33	.001	5	.45	.011	.19	.3	.02	1.6	.1	<.05	1	<.5	5.80
400821	.4	45.9	4.6	48	.1	27.8	10.6	208	3.21	269.3	1.4	.9	11.2	8	<.1	1.5	.4	3	.03	.040	31	7	.05	32	.001	5	.64	.020	.19	<.1	.02	1.1	.2	<.05	1	<.5	4.30
400822	.4	64.1	5.3	61	<.1	49.4	20.1	450	3.80	498.7	2.0	3.3	14.5	10	<.1	1.6	1.0	6	.07	.060	43	10	.10	45	.001	8	.75	.009	.24	.1	.03	1.8	.2	<.05	1	<.5	5.10
400823	.3	55.0	8.3	17	.1	17.7	12.8	422	3.27	1349.4	.8	7.4	14.0	9	<.1	2.8	2.5	5	.10	.045	24	8	.06	50	.001	6	.55	.009	.21	<.1	.01	1.5	.2	<.05	1	1.0	6.20
400824	.4	105.4	8.9	28	.2	27.0	21.8	702	2.99	973.4	1.5	8.5	11.6	9	.1	3.9	1.8	5	.08	.042	29	8	.09	69	.001	5	.65	.009	.22	.1	.01	2.1	.2	<.05	1	.7	7.10
400825	1.1	12.4	17.3	68	<.1	4.6	6.6	578	2.98	25.4	2.2	<.5	10.5	92	.2	.3	.1	72	1.00	.168	27	9	.60	440	.215	1	1.06	.150	.22	.8	<.01	4.7	.1	<.05	6	<.5	1.20
400826	.3	68.6	8.6	30	.2	28.5	21.9	944	1.95	535.2	1.1	11.5	10.7	7	.1	2.6	2.9	5	.06	.030	23	8	.09	70	.001	7	.73	.011	.21	<.1	.01	1.5	.2	<.05	1	.6	5.40
400827	.3	42.0	9.6	45	.1	45.4	7.9	517	2.14	311.5	.8	5.7	12.0	11	.1	1.8	2.1	6	.09	.016	26	8	.13	45	.001	6	.75	.016	.19	<.1	.01	1.5	.1	<.05	1	<.5	5.90
STANDARD DS7	20.7	105.6	67.4	404	.8	54.9	9.5	616	2.37	47.3	4.8	59.0	4.3	70	6.2	5.8	4.4	85	.92	.077	12	170	1.04	367	.121	37	.97	.076	.44	3.8	.19	2.5	4.1	.21	5	3.4	-

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

10-13-06 P05:02 OUT

Data f FA ____ DATE RECEIVED: SEP 7 2006 DATE REPORT MAILED:.....

Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	2.9	3.3	44	<.1	4.0	4.1	519	1.93	2.0	2.7	.6	4.4	61	<.1	.1	.1	39	.51	.070	8	10	.57	203	.111	4	.95	.079	.51	.1	<.01	2.0	.4	<.05	5	<.5	-
400828	.3	99.5	46.2	37	.9	43.6	13.4	460	2.65	1454.2	1.6	203.1	12.7	14	.1	10.6	43.8	5	.14	.036	35	8	.09	69	.001	6	.56	.010	.22	.6	.03	2.0	.2	<.05	1	<.5	5.00
400829	.2	64.9	5.9	30	.1	44.4	10.7	361	2.88	985.6	.9	27.7	9.9	17	.1	4.2	2.2	5	.14	.019	20	6	.17	46	<.001	4	.80	.008	.16	.1	.01	1.5	.1	<.05	1	.5	8.00
400830	.2	46.0	4.3	22	<.1	30.0	5.8	318	2.51	432.1	.7	6.6	6.9	16	<.1	2.4	1.7	3	.19	.020	15	8	.22	38	<.001	4	.84	.007	.14	<.1	.01	1.1	.1	<.05	1	<.5	6.00
400831	.1	140.0	8.7	32	.2	40.1	12.1	492	3.41	933.4	1.1	24.0	13.1	20	.1	5.1	4.0	12	.32	.030	32	12	.28	62	.001	4	1.15	.012	.18	.4	.05	2.7	.2	<.05	3	.5	8.70
400832	.2	97.9	8.1	33	.2	33.1	13.0	539	3.26	948.7	1.1	16.9	12.7	31	.1	4.6	3.7	10	.91	.104	30	9	.22	62	.001	5	1.10	.006	.18	.2	.05	2.1	.2	<.05	2	.6	7.30
400833	.2	128.5	10.9	35	.4	31.7	11.7	730	2.74	1330.4	1.2	24.9	11.6	22	.1	7.4	6.4	5	.45	.051	32	6	.13	73	<.001	10	.68	.005	.19	.1	.02	2.3	.2	<.05	1	<.5	8.30
400834	.2	137.7	9.8	57	.3	39.7	14.9	554	3.21	1351.5	1.1	36.8	16.4	23	.2	6.3	6.5	10	.46	.075	42	10	.20	68	.001	7	1.07	.007	.21	.5	.03	2.5	.3	<.05	2	<.5	6.60
400835	.5	173.5	18.4	51	.5	29.6	15.7	277	4.40	3580.7	1.2	44.2	16.0	16	.2	9.7	10.1	8	.13	.049	28	8	.10	62	.001	7	.73	.006	.22	.1	.04	2.2	.3	<.05	1	3.3	8.10
400836	.3	174.9	9.2	39	.3	48.4	25.7	433	2.69	2391.4	1.7	47.8	15.9	12	.3	8.0	8.9	7	.11	.028	37	8	.10	56	.001	5	.80	.008	.19	.1	.05	2.0	.2	<.05	1	1.2	8.90
400837	.6	133.5	18.9	32	.6	19.6	9.7	209	3.23	3442.0	1.1	112.5	12.1	13	.3	15.8	19.4	6	.07	.021	34	8	.04	96	.001	7	.46	.005	.21	1.0	.03	1.8	.2	<.05	1	1.4	9.10
400838	.5	157.4	18.5	34	.4	20.4	12.4	259	3.47	2295.9	1.3	92.0	14.0	11	.4	11.5	20.8	7	.06	.027	31	8	.10	111	.001	5	.77	.007	.19	.1	.02	1.8	.2	<.05	2	2.3	5.60
400839	.2	92.3	10.0	29	.2	24.9	11.8	380	2.68	3425.7	1.2	60.3	14.8	30	.2	6.1	7.7	7	.10	.023	34	8	.11	96	.001	7	.76	.008	.26	.1	.02	2.7	.2	<.05	2	.6	8.90
400840	.2	49.1	9.3	24	.1	28.5	8.2	454	2.00	866.9	.9	10.1	14.4	11	.1	6.0	1.7	5	.18	.018	31	10	.12	100	.001	9	.74	.011	.20	.6	.01	1.9	.1	<.05	1	<.5	9.10
400841	.2	50.6	9.7	21	.1	20.7	8.5	418	2.04	855.8	.9	9.5	14.0	10	<.1	4.2	1.4	5	.08	.021	28	7	.11	84	.001	4	.72	.008	.19	.1	.02	1.7	.2	<.05	1	<.5	5.80
400842	.3	62.7	12.3	25	.1	22.4	9.3	444	2.26	3105.2	1.0	47.4	13.5	14	.1	10.0	6.1	5	.10	.023	27	8	.09	67	.001	5	.64	.006	.19	.1	.02	1.8	.2	<.05	1	1.1	8.50
400843	.2	22.7	8.3	11	.2	8.3	3.4	131	1.22	496.7	.6	23.9	9.8	13	.1	11.3	2.2	2	.05	.015	22	11	.03	44	.001	5	.31	.004	.12	1.1	<.01	.9	.1	<.05	1	<.5	7.50
400844	.2	23.8	6.4	17	<.1	8.7	4.3	134	1.32	373.1	.7	4.4	13.7	9	<.1	9.5	.5	2	.05	.014	26	8	.02	57	<.001	4	.31	.004	.16	.1	<.01	1.0	.1	<.05	1	<.5	5.30
400845	.2	21.0	8.5	15	.1	10.1	4.5	111	1.09	369.0	.5	4.7	11.0	8	.1	9.5	1.1	2	.02	.012	23	9	.02	55	.001	6	.33	.004	.17	.1	.01	.8	.1	<.05	1	<.5	5.90
400846	.3	27.9	7.9	18	.2	10.9	4.7	156	1.40	525.1	.7	7.5	11.0	8	.1	17.4	1.4	4	.05	.020	24	10	.03	54	.001	7	.37	.004	.19	.9	.01	1.0	.1	<.05	1	<.5	6.50
400847	.1	32.4	12.6	8	.2	4.5	2.2	42	1.28	999.0	.7	14.9	10.3	11	.1	14.1	1.9	2	.02	.009	22	10	.03	50	.001	6	.30	.003	.16	.1	.01	1.0	.1	<.05	1	<.5	4.20
400848	.2	21.6	9.4	16	.3	8.9	3.6	85	1.26	395.2	.6	5.4	9.1	8	.1	9.3	1.0	3	.03	.011	20	9	.05	54	.001	8	.37	.005	.16	.1	<.01	.9	.1	<.05	1	<.5	3.70
RE 400848	.2	20.7	9.1	16	.3	8.6	3.5	83	1.22	408.2	.6	7.1	9.1	8	.1	9.0	1.0	3	.03	.011	20	9	.05	54	.001	8	.39	.005	.16	.1	<.01	.9	.1	<.05	1	<.5	-
400849	.2	47.2	10.4	21	.3	14.1	5.5	340	1.68	754.4	.7	22.4	14.1	10	.2	7.5	3.0	5	.14	.018	31	12	.15	95	.001	4	.75	.007	.20	.8	<.01	1.3	.2	<.05	2	<.5	7.20
400850 (pulp)	6.6	60.5	18.0	104	1.9	14.4	8.0	140	3.01	313.0	.1	867.8	.5	5	.3	25.7	.2	16	.19	.039	7	27	.09	24	.002	2	.36	.005	.22	.3	3.68	1.6	3.7	2.14	2	8.6	-
400851	.1	29.9	13.7	28	.2	15.9	4.9	395	1.34	505.8	.6	9.7	12.4	9	.2	6.6	1.7	5	.13	.016	23	11	.13	66	.001	2	.62	.013	.14	<.1	.01	1.5	.1	<.05	1	<.5	3.70
400852	.2	33.5	9.7	20	.2	13.2	5.7	443	1.46	552.1	.6	13.9	10.6	27	.1	6.0	1.9	8	.90	.014	22	12	.19	66	.004	4	.70	.013	.15	.1	.01	1.7	.1	<.05	2	<.5	3.30
400853	.2	122.0	15.8	32	.3	23.3	11.6	400	2.74	1402.2	.9	26.0	15.5	19	.3	11.4	6.3	15	.30	.044	33	18	.42	90	.002	3	1.31	.007	.21	.7	<.01	2.4	.2	<.05	4	.9	6.10
400854	.2	115.1	14.8	38	.3	25.7	11.0	392	2.73	1189.3	1.1	28.2	15.5	14	.3	10.4	4.6	15	.32	.036	29	17	.43	81	.004	2	1.40	.006	.19	<.1	.01	2.3	.2	<.05	4	.7	6.20
400855	.2	69.5	29.2	63	.4	34.6	11.8	436	2.75	1146.0	.9	18.1	15.4	16	.9	10.5	3.0	10	.42	.025	31	14	.43	72	.001	<1	1.42	.004	.15	<.1	.01	1.6	.1	<.05	4	.8	4.30
400856	.2	154.0	79.2	142	1.7	25.0	11.1	402	3.20	2549.3	1.1	68.6	15.9	20	7.8	11.6	15.9	14	.35	.033	33	16	.32	96	.002	3	1.32	.005	.18	.2	.02	2.7	.2	<.05	4	1.7	6.10
400857	.2	44.5	12.9	33	.2	15.7	8.5	289	2.25	941.5	1.1	44.9	12.7	19	.2	22.8	3.4	9	.26	.030	32	10	.21	85	.002	5	.85	.007	.22	.1	.02	2.3	.2	<.05	2	<.5	5.10
400858	.2	70.6	35.9	57	.6	13.3	6.7	287	1.78	1054.7	.7	85.0	10.6	12	2.7	12.5	7.0	9	.18	.018	22	12	.20	78	.003	3	.89	.008	.17	.1	.01	1.4	.1	<.05	2	<.5	2.20
400859	.2	16.3	8.2	14	<.1	8.7	3.2	182	.98	159.8	.4	4.4	8.0	10	.1	11.9	.5	5	.14	.012	18	13	.19	89	.006	<1	.67	.011	.21	.6	<.01	.8	.2	<.05	2	<.5	4.60
400860	.3	68.0	9.2	31	.1	27.5	9.0	266	2.18	341.6	1.3	3.9	13.6	25	.1	22.0	.9	14	.40	.018	30	17	.48	74	.017	1	1.34	.016	.33	.1	<.01	2.1	.3	<.05	4	<.5	6.30
STANDARD DS7	20.6	106.0	69.4	410	.9	55.7	9.7	639	2.39	48.2	4.9	68.5	4.6	72	6.3	6.0	4.5	85	.94	.079	13	175	1.06	375	.123	39	.99	.079	.46	3.9	.20	2.6	4.2	.21	5	3.1	-

Sample type: ROCK. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data A FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	6.9	3.5	47	<.1	4.2	4.5	539	1.92	8.9	2.8	1.2	4.4	64	.1	.2	.1	36	.54	.077	7	14	.58	208	.132	2	.99	.090	.52	1.1	<.01	2.1	.4	<.05	5	<.5	-
400861	.1	56.4	7.6	38	.1	31.4	11.9	374	2.20	374.4	1.1	5.4	14.1	27	.2	15.9	1.0	12	.52	.021	27	15	.39	87	.008	1	1.19	.013	.28	.1	<.01	1.9	.3	<.05	3	<.5	7.00
400862	.4	27.7	7.9	17	.1	10.1	4.3	216	1.47	267.5	.5	3.1	10.1	14	.1	7.4	.4	6	.29	.014	15	12	.23	65	.005	1	.62	.013	.19	1.0	<.01	1.0	.1	<.05	2	<.5	5.60
400863	.2	34.5	4.7	33	<.1	9.9	4.0	106	1.94	338.3	.9	6.0	9.7	10	.1	7.0	.4	6	.07	.015	17	12	.32	79	.005	1	.85	.013	.28	<.1	<.01	1.0	.2	<.05	2	<.5	5.00
400864	.2	45.5	6.3	20	.1	6.9	2.6	79	2.28	517.6	.8	11.3	11.9	12	<.1	6.9	.4	3	.08	.024	24	6	.17	64	.003	1	.53	.010	.22	<.1	<.01	.8	.1	<.05	2	<.5	6.00
400865	.4	68.2	9.3	38	.2	15.7	6.5	118	3.18	1081.7	1.4	29.2	15.5	17	.2	9.7	.7	7	.13	.024	32	10	.23	107	.004	2	.89	.012	.36	.6	.01	1.5	.3	<.05	2	.6	3.50
400866	.5	36.2	10.1	16	.2	9.1	2.7	90	2.19	675.8	.8	13.0	13.3	9	.1	8.4	.6	2	.07	.020	34	6	.06	71	.001	1	.40	.009	.23	<.1	.01	.9	.1	<.05	1	.6	3.80
400867	.4	73.8	6.5	31	.2	29.0	15.4	295	2.19	815.4	1.1	23.5	13.8	15	.2	7.9	1.0	2	.12	.026	30	8	.10	66	.002	1	.59	.013	.19	.1	<.01	1.0	.1	<.05	1	<.5	5.10
400868	.2	28.2	8.9	23	.1	19.3	7.9	389	1.82	307.0	.9	18.4	12.6	53	.1	3.7	.6	5	2.02	.023	28	8	.22	65	.003	1	.72	.018	.17	<.1	.01	1.3	.1	<.05	2	<.5	5.30
400869	.2	23.0	9.1	20	.1	14.2	4.3	437	1.41	325.1	.6	27.5	10.9	36	.1	3.5	.4	5	1.04	.015	22	10	.21	60	.003	2	.69	.013	.13	.1	.01	1.3	.1	<.05	2	<.5	6.40
400870	.3	50.2	12.1	33	.3	21.9	9.0	281	3.11	529.2	1.3	82.0	17.5	66	.2	4.7	.8	14	1.43	.022	30	17	.44	53	.006	<1	1.19	.015	.23	.3	<.01	2.0	.2	<.05	3	<.5	4.80
400871	.2	13.7	14.1	16	.2	16.3	7.0	1020	1.97	126.4	.9	1.5	10.9	332	.1	1.4	.4	16	9.51	.017	22	17	.43	42	.012	<1	1.37	.065	.17	<.1	<.01	3.0	.2	<.05	4	<.5	6.00
400872	.3	55.8	11.3	22	.3	22.6	9.0	421	2.90	625.8	1.2	5.5	15.6	63	.1	3.4	1.2	10	2.17	.024	29	13	.31	43	.004	1	.90	.012	.16	.1	<.01	1.7	.1	<.05	3	.7	7.40
400873	.1	18.6	11.5	11	.1	12.1	4.9	860	1.54	283.5	.6	4.7	8.7	222	.1	3.8	.4	5	9.15	.019	18	8	.26	32	.003	<1	.68	.008	.11	.3	<.01	1.7	.1	<.05	2	<.5	4.40
400874	.1	10.9	11.9	10	<.1	8.9	3.9	951	1.22	156.8	.5	3.5	6.3	258	.1	2.7	.3	4	9.98	.012	15	7	.27	30	.003	1	.59	.010	.09	<.1	<.01	1.3	.1	<.05	1	<.5	6.20
400875	.9	11.8	15.4	61	<.1	4.0	5.5	426	2.79	13.0	1.6	.9	9.7	71	.1	.3	.1	64	.86	.167	24	7	.50	444	.175	<1	.91	.105	.16	.6	<.01	3.7	.1	<.05	5	<.5	1.30
400876	.2	20.4	9.4	7	<.1	10.6	7.5	711	1.40	133.7	.5	1.5	8.5	292	<.1	3.0	.4	5	9.93	.037	17	9	.23	29	.003	<1	.55	.010	.10	.3	<.01	1.4	.1	<.05	2	<.5	3.70
400877	.3	48.9	9.5	16	.2	20.9	12.0	425	2.80	359.5	1.0	4.3	14.8	70	.1	4.3	2.0	12	2.79	.033	24	16	.40	54	.003	1	1.12	.007	.18	<.1	.01	2.1	.2	<.05	4	<.5	3.40
400878	.2	21.3	5.2	15	<.1	14.0	6.8	555	1.58	109.1	1.1	1.5	14.9	110	<.1	1.8	.6	11	4.61	.018	18	17	.39	41	.018	<1	.87	.018	.19	.3	<.01	1.8	.2	<.05	3	.7	5.30
400879	.5	108.3	7.3	18	.2	16.6	7.8	241	3.25	480.9	2.5	29.2	16.4	66	.1	2.1	3.2	19	1.07	.068	22	22	.48	69	.019	<1	1.35	.049	.23	.1	<.01	1.9	.2	.15	4	.7	4.80
400880	.4	112.9	11.4	25	.3	27.1	11.9	292	3.31	567.1	1.7	14.6	18.9	39	.2	7.0	2.7	17	.71	.036	22	22	.62	75	.015	<1	1.55	.018	.27	.3	<.01	2.2	.3	.07	5	.6	6.40
RE 400880	.3	114.5	11.7	25	.3	26.9	12.2	293	3.34	563.5	1.9	18.0	19.2	38	.2	7.2	2.7	17	.71	.035	23	22	.62	78	.016	1	1.58	.018	.28	.3	.01	2.3	.3	.07	5	.7	-
400881	.7	91.0	10.5	27	.2	41.8	17.5	567	3.19	454.7	2.4	21.3	16.7	42	.1	2.8	2.2	25	.99	.036	33	26	.59	58	.010	<1	1.60	.028	.20	.1	.01	2.4	.2	<.05	5	.5	2.20
400882	.3	75.5	7.0	27	.2	38.7	12.0	380	2.96	284.6	1.6	9.3	17.1	29	.1	3.2	1.4	23	.68	.029	41	28	.68	72	.019	<1	1.82	.038	.32	.3	<.01	3.1	.3	<.05	6	.6	4.70
400883	.4	72.6	7.6	18	.2	22.9	9.4	386	2.25	378.3	.9	6.6	15.8	15	.1	2.8	2.6	10	.35	.027	35	13	.38	59	.005	<1	1.04	.012	.22	<.1	<.01	1.4	.2	<.05	3	.7	2.10
400884	.3	67.4	9.1	19	.1	27.6	9.6	409	2.14	408.9	.9	7.4	12.6	53	<.1	2.4	1.6	11	1.93	.025	41	15	.33	64	.003	1	1.09	.010	.21	.4	.01	1.9	.2	<.05	3	<.5	5.30
400885	.4	102.7	10.5	26	.2	25.8	9.0	412	2.84	554.1	1.0	24.7	14.6	31	.2	4.2	3.8	12	1.01	.025	32	14	.35	66	.004	2	1.30	.015	.25	.1	.01	2.3	.3	<.05	3	.5	5.00
400886	.3	101.3	25.6	55	.3	25.3	9.8	516	3.12	1170.9	.8	49.9	15.2	42	1.3	6.3	6.8	9	1.23	.026	35	12	.29	76	.002	3	1.27	.010	.24	.4	.02	2.1	.3	<.05	3	.8	2.40
400887	.1	26.9	9.9	37	<.1	12.6	5.5	502	1.63	321.6	.7	4.5	10.9	128	.6	2.3	.9	3	5.29	.019	23	6	.17	43	.001	3	.67	.011	.14	.1	.01	1.7	.1	<.05	1	.5	3.80
400888	.5	103.0	11.2	19	.3	23.9	8.3	252	2.67	779.5	.8	42.0	11.9	40	.2	5.4	3.3	9	1.59	.033	23	13	.20	70	.002	4	1.07	.012	.20	.6	.03	2.2	.2	<.05	3	.7	5.10
400889	.5	107.9	12.7	21	.3	22.2	10.0	354	3.24	2414.5	.8	57.9	10.5	46	.3	11.7	8.9	7	1.97	.032	23	10	.13	53	.001	4	.74	.006	.17	.1	.02	2.2	.2	<.05	2	.9	6.40
400890	.4	59.8	11.8	21	.2	20.2	9.9	417	2.40	2923.5	.8	43.9	14.2	90	.1	5.7	7.4	4	2.74	.020	33	8	.12	55	.001	4	.66	.009	.18	.6	.01	1.9	.2	<.05	1	<.5	5.50
400891	.4	48.0	8.6	21	.1	19.2	7.2	319	1.83	645.6	.7	7.7	13.1	47	.1	3.4	1.8	8	1.93	.025	25	10	.18	64	.001	3	.83	.007	.16	<.1	.01	2.0	.1	<.05	2	.5	1.70
400892	.3	36.8	4.9	21	<.1	15.1	5.5	238	1.25	340.7	.4	6.2	6.6	59	<.1	2.0	.7	3	1.92	.011	16	11	.08	44	.001	2	.40	.009	.12	1.0	.01	1.1	.1	<.05	1	1.1	2.00
400893	.2	55.0	7.3	24	.1	21.2	10.2	403	2.22	480.2	.7	6.8	11.9	61	.1	4.2	.9	5	2.88	.021	28	6	.26	52	.001	6	.87	.006	.18	<.1	.01	2.6	.1	<.05	1	.7	4.60
STANDARD DS7	20.5	106.8	69.7	410	.9	56.4	9.5	629	2.39	48.1	4.9	65.9	4.4	69	6.4	5.9	4.5	84	.91	.079	11	172	1.05	374	.118	38	.97	.076	.45	3.9	.21	2.5	4.2	.22	5	3.5	-

Sample type: ROCK. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Data (FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	2.5	3.3	49	<.1	3.8	4.1	541	1.86	10.4	3.0	<.5	4.6	58	<.1	.1	.1	37	.50	.074	7	13	.56	194	.124	3	.92	.067	.48	.9	.01	1.9	.3	<.05	5	<.5	-
400894	.1	46.7	10.4	55	.2	22.3	9.5	403	2.40	270.7	.8	<.5	14.1	87	1.3	2.6	.6	10	3.37	.049	27	14	.30	75	.004	7	1.05	.012	.24	.5	.01	3.3	.2	<.05	3	.6	3.70
400895	.3	91.8	5.1	29	.1	18.0	8.2	320	1.82	520.4	.4	19.7	7.2	30	.9	6.0	2.0	3	1.45	.010	15	12	.19	43	.001	4	.63	.005	.13	<.1	.02	1.5	.1	.07	2	.6	3.00
RE 400895	.3	91.9	5.1	27	.1	18.5	8.1	320	1.84	534.3	.4	17.1	7.3	30	.8	5.7	1.9	4	1.46	.010	14	11	.19	41	.001	2	.65	.005	.13	<.1	.02	1.6	.1	.07	1	<.5	-
400896	.2	170.8	7.4	21	.2	18.9	9.3	331	3.15	1966.9	.8	150.9	15.8	40	.2	4.6	10.7	13	.94	.023	27	15	.29	67	.004	2	1.18	.020	.17	.5	.01	2.2	.1	<.05	4	.5	4.00
400897	.2	64.7	8.5	24	.1	14.2	6.0	341	2.36	744.6	.8	42.6	13.6	75	.2	10.2	2.3	4	2.39	.031	26	8	.24	60	.001	6	.85	.011	.18	.1	.01	1.8	.1	<.05	2	.8	2.80
400898	2.5	11.2	11.3	107	<.1	6.1	12.4	1023	3.69	146.9	1.7	4.1	6.4	369	.8	5.1	.3	30	6.49	.262	23	32	1.19	125	.003	14	1.05	.018	.28	.7	.01	16.2	.2	.06	2	.7	3.80
400899	.6	31.6	7.5	36	<.1	11.1	7.5	466	1.98	805.6	.9	19.2	9.6	45	.1	4.0	1.4	6	1.93	.066	20	12	.11	55	.001	7	.66	.011	.16	.3	.01	4.6	.1	<.05	1	.7	3.50
400900 (pulp)	8.6	62.6	3.7	44	9.9	265.4	12.0	146	3.13	457.4	.1	9850.9	.4	6	.1	53.5	<.1	14	.12	.036	7	311	.06	26	.002	1	.28	.006	.19	1.1	6.96	1.2	9.1	1.77	1	22.3	-
400901	.2	61.2	10.2	24	.1	19.9	9.3	300	2.04	1042.8	.9	24.7	12.2	42	.1	3.3	1.6	4	1.45	.046	28	8	.25	64	.001	4	.77	.009	.18	.6	.03	2.6	.2	<.05	2	<.5	4.30
400902	.1	76.6	10.0	21	.1	20.9	9.4	317	2.32	1426.4	.9	18.3	14.5	51	.1	1.8	1.9	5	2.19	.027	33	6	.15	78	.001	2	.73	.010	.19	.1	.03	2.4	.2	<.05	2	.5	6.00
400903	.2	16.2	5.2	11	<.1	8.2	3.9	454	.99	107.0	.5	2.3	9.9	57	<.1	1.1	.2	<1	2.85	.010	21	6	.14	37	.001	2	.46	.019	.11	.4	.01	1.1	.1	<.05	1	.5	1.50
400904	.5	117.0	113.1	21	4.1	4.5	11.4	36	19.65	>10000	1.3	2112.9	12.5	38	.6	418.7	244.5	6	.03	.054	15	9	.03	60	.003	2	.39	.006	.16	1.3	.09	1.1	.3	1.36	2	25.7	1.60
400905	.3	42.3	9.9	17	.2	5.5	1.9	95	1.71	2547.6	.9	54.0	9.7	9	.1	5.9	5.6	6	.02	.009	17	20	.25	30	.003	1	.63	.012	.11	1.1	.01	1.0	.2	.07	2	1.0	.40
400906	1.3	115.4	27.4	28	2.4	16.8	14.4	573	22.66	>10000	2.2	2417.0	10.7	427	.3	121.9	288.2	4	.33	.048	33	6	.05	103	.001	7	.49	.011	.40	.1	.07	3.3	.3	.60	1	24.7	.30
400907	.4	71.5	11.8	22	.2	25.4	8.6	486	1.97	1090.1	1.0	7.3	12.5	16	.1	9.0	5.3	2	.20	.018	25	9	.03	55	.001	5	.38	.013	.20	.9	.01	1.2	.1	<.05	1	1.0	3.70
400908	.3	104.9	23.0	19	.4	22.1	15.2	493	2.33	2951.7	1.6	4.0	14.2	25	.1	10.4	21.1	1	.06	.023	32	5	.03	71	.001	4	.36	.009	.17	.1	.01	1.7	.2	<.05	1	.6	3.70
400909	.3	33.6	9.4	19	.1	16.1	5.0	447	1.25	441.1	.6	<.5	12.7	16	.1	7.4	1.8	<1	.07	.013	24	8	.03	38	.001	4	.31	.004	.16	1.0	.01	.9	.1	<.05	1	<.5	1.80
400910	.2	39.2	8.3	16	.1	11.4	4.2	144	1.70	368.7	.7	2.5	17.0	12	<.1	5.2	2.6	<1	.06	.012	27	6	.02	35	.001	6	.31	.005	.16	.1	.01	.7	.1	<.05	1	.5	3.40
400911	.2	29.0	11.5	16	.1	15.4	6.7	281	1.15	447.9	.5	5.1	12.5	14	.1	6.5	2.1	<1	.11	.014	25	7	.03	49	.001	4	.35	.006	.19	.9	.01	.9	.1	<.05	1	<.5	1.30
400912	.6	115.0	257.5	40	2.5	3.0	1.8	73	7.03	>10000	.4	291.7	4.9	8	1.7	213.3	89.9	<1	.02	.036	14	5	.02	66	.001	2	.19	.007	.11	.4	.04	.8	.1	.09	1	15.1	.90
STANDARD DS7	20.9	105.9	69.6	413	.9	55.9	9.9	635	2.41	54.9	4.9	86.2	4.5	68	6.2	5.9	4.6	85	.93	.077	12	177	1.06	373	.124	40	.97	.075	.44	4.0	.20	2.5	4.3	.22	5	4.0	-

Sample type: ROCK. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Data 1 FA ___

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A606035R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Au** gm/mt	Sample gm
400931	.79	29.2
RE 400931	.80	29.2
400950 (pulp)	1.03	7.3
405070	.71	29.2
405077	.59	29.2
405089	.69	29.2
405094	.89	29.2
405100 (pulp)	10.17	7.3
405106	4.29	29.2
405107	1.37	29.2
405150 (pulp)	10.27	7.3
405190	.50	29.2
405200 (pulp)	1.00	7.3
STANDARD SL20	6.12	29.2

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: ROCK PULP
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

10-30-06 P06:05 OUT

Data 1 FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A606035 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.6	2.7	2.5	43	<.1	3.8	4.1	504	1.72	<.5	2.4	1.1	3.8	45	<.1	<.1	.1	34	.48	.071	6	10	.56	189	.104	1	.85	.058	.44	.3	.01	1.8	.3	<.05	5	<.5	-
400913	.3	67.2	9.2	45	.1	30.4	14.7	341	2.98	765.0	1.5	7.1	16.6	12	.1	12.2	3.0	4	.05	.030	51	6	.05	62	.001	5	.35	.007	.22	.1	.01	1.6	.2	<.05	1	<.5	1.0
RE 400913	.3	68.8	9.3	47	.1	30.2	15.5	339	3.04	782.9	1.5	7.5	16.9	12	<.1	12.1	3.1	4	.05	.030	50	6	.05	61	.001	6	.36	.007	.22	.1	.01	1.5	.2	<.05	1	.7	-
400914	.5	49.1	12.8	39	.2	22.8	10.1	458	2.35	1361.6	1.2	7.3	13.9	14	.2	19.1	2.5	4	.07	.026	32	6	.02	43	<.001	8	.30	.004	.17	.1	.01	1.9	.2	<.05	1	<.5	1.3
400915	.1	20.7	2.0	3	.2	2.9	1.0	39	.67	247.3	.1	3.2	.9	2	<.1	2.2	4.1	2	.02	.005	3	15	.01	16	<.001	3	.06	.002	.04	<.1	.01	.3	<.1	<.05	<1	<.5	1.3
400916	.4	46.7	8.3	63	.1	30.8	12.2	265	3.36	518.6	1.8	3.5	20.4	12	<.1	10.7	.9	3	.07	.046	60	6	.02	39	.001	6	.28	.004	.22	.1	.01	1.3	.1	<.05	<1	<.5	2.0
400917	.3	54.8	8.5	48	.1	27.7	12.1	257	3.23	624.6	1.4	5.8	17.9	12	.1	13.2	1.2	4	.04	.024	55	9	.03	74	.001	9	.50	.008	.34	.1	.01	1.5	.2	<.05	1	<.5	2.2
400918	.7	44.9	11.7	39	.4	19.4	7.9	201	2.75	3836.4	1.0	25.7	16.1	11	.1	15.9	18.3	4	.04	.022	37	10	.03	47	.001	7	.32	.006	.20	.2	.01	1.2	.1	<.05	1	1.7	1.9
400919	.2	80.3	12.6	42	1.1	19.8	9.5	394	2.67	2776.1	.8	34.5	10.8	9	.1	33.8	26.3	3	.05	.025	29	7	.03	40	.001	6	.30	.004	.16	.1	.02	1.5	.1	<.05	1	1.1	2.5
400920	.6	63.8	9.8	36	.4	22.7	9.2	304	2.77	1100.7	1.0	14.8	12.9	10	.1	16.2	7.7	3	.03	.025	36	9	.03	47	.001	4	.30	.005	.20	.1	.01	1.3	.1	<.05	1	.9	1.5
400921	.3	240.8	9.5	25	.8	17.3	8.9	258	4.48	6426.1	.8	65.8	13.3	21	.1	37.5	39.9	3	.08	.030	34	9	.03	50	.001	6	.31	.005	.21	.1	.03	1.6	.2	<.05	1	3.7	1.5
400922	.6	121.7	8.3	25	.5	18.2	6.3	130	3.11	6178.6	.8	33.2	13.7	15	.1	26.2	23.0	3	.06	.020	34	7	.02	47	.001	7	.28	.005	.21	.2	.02	1.4	.2	<.05	1	3.1	1.2
400923	.1	24.7	5.1	6	.2	4.1	1.4	40	.76	497.0	.3	5.7	8.5	8	<.1	11.5	2.0	1	.04	.013	15	15	.01	42	.001	3	.20	.003	.14	.1	<.01	.5	.1	<.05	<1	.7	2.7
400924	.6	39.7	6.0	8	.3	6.0	2.2	51	1.23	3912.4	.5	65.2	9.5	13	.1	11.7	26.8	1	.06	.016	17	17	.02	49	.001	5	.24	.004	.16	.1	<.01	.7	.1	<.05	1	1.6	2.5
400925	1.1	10.8	17.3	65	<.1	4.3	5.5	459	2.89	45.0	1.7	3.0	9.0	72	.2	.5	.5	71	.93	.162	24	10	.57	439	.180	1	.99	.116	.18	.6	.01	4.0	.1	<.05	6	<.5	1.4
400926	.1	8.1	1.2	2	<.1	1.4	.4	20	.38	202.2	.1	4.0	.9	2	<.1	2.7	1.3	1	.02	.002	2	28	<.01	10	.001	3	.05	.002	.03	<.1	.01	.2	<.1	<.05	<1	<.5	3.5
400927	.4	47.0	8.5	13	.3	7.1	2.6	60	1.48	4987.4	.6	31.1	9.6	14	.2	19.7	20.4	2	.06	.013	18	13	.02	43	.001	4	.25	.003	.15	.1	<.01	.9	.1	<.05	<1	1.9	3.9
400928	.2	9.1	1.9	3	.2	1.9	.6	23	.47	1025.7	.1	25.1	.8	2	.1	5.2	5.1	<1	.01	.002	2	18	<.01	9	<.001	2	.04	.002	.03	.1	.01	.2	<.1	<.05	<1	.7	1.2
400929	.7	50.8	9.7	20	.3	10.8	5.3	131	1.70	1026.9	.8	15.2	9.5	12	.1	11.9	4.8	3	.06	.016	22	13	.02	49	.001	5	.27	.004	.17	.1	.01	1.1	.1	<.05	1	1.3	1.7
400930	.6	66.0	6.4	32	.2	22.9	11.9	189	2.44	854.5	1.2	12.6	16.7	14	.1	15.8	2.9	4	.09	.040	47	9	.02	61	.001	3	.31	.005	.25	.2	.01	1.5	.1	<.05	1	.9	3.0
400931	.7	57.9	11.7	5	1.1	9.3	8.4	81	2.46	>10000	.9	737.9	2.1	44	.1	38.1	132.9	1	.07	.012	4	14	.01	29	<.001	2	.09	.002	.07	.2	.02	.5	.1	.61	<1	15.4	.7
400932	.9	52.1	5.6	37	.2	20.9	7.7	179	2.37	518.4	.9	7.3	10.4	12	.1	22.1	6.0	5	.04	.025	30	9	.02	48	<.001	3	.23	.005	.21	.3	.01	1.0	.2	<.05	<1	1.2	3.1
400933	.3	38.7	5.8	18	.2	12.1	5.2	125	1.52	648.3	.8	10.0	8.6	16	.1	12.7	2.7	4	.04	.013	19	11	.02	44	.001	3	.24	.003	.16	.2	<.01	.8	.1	<.05	1	<.5	1.5
400934	.5	32.7	5.5	19	.1	11.4	4.7	123	1.42	568.8	.8	5.6	9.3	21	.1	8.0	1.8	4	.08	.011	14	11	.03	46	.001	4	.30	.005	.15	.1	<.01	.8	.1	<.05	1	<.5	2.5
400935	.2	25.6	2.1	3	.1	3.5	2.5	29	.81	973.7	.2	14.2	1.1	6	.1	4.7	4.3	1	.04	.013	2	16	.01	13	.001	2	.06	.002	.04	.1	.01	.2	<.1	.31	<1	.8	.6
400936	.6	27.3	9.6	21	.2	11.4	5.7	202	1.29	575.3	.7	6.0	8.1	8	.1	9.8	1.3	2	.06	.015	15	12	.02	51	.001	2	.26	.003	.17	.1	<.01	.6	.1	<.05	1	.7	2.0
400937	.2	36.0	11.6	25	1.0	12.0	5.9	179	1.56	1207.2	1.0	66.7	9.8	15	.3	12.2	1.4	2	.07	.011	20	8	.02	58	.001	3	.26	.003	.20	.1	.02	.8	.1	<.05	1	.8	1.4
400938	.7	29.4	8.0	31	.1	19.0	9.9	146	1.81	560.6	1.3	7.0	16.0	9	.1	7.4	.5	3	.03	.030	43	5	.02	94	.001	3	.28	.004	.36	.1	.01	1.0	.1	<.05	1	1.0	1.5
400939	.3	36.1	18.3	15	.4	9.2	4.8	113	1.47	734.6	.7	27.7	12.4	13	.2	12.9	1.7	2	.05	.014	23	9	.02	77	.001	2	.28	.003	.21	.1	.01	.9	.1	<.05	1	<.5	.7
400940	.4	12.8	13.6	13	.1	9.9	4.7	280	1.24	2640.9	.5	62.3	10.1	8	.1	11.8	10.2	2	.08	.012	18	9	.02	74	.001	8	.27	.003	.20	.1	<.01	.9	.1	.11	<1	1.6	1.5
400941	.2	9.1	8.5	9	.1	3.9	2.0	81	.69	971.1	.4	29.1	10.6	8	.1	8.8	1.2	2	.03	.010	19	9	.02	83	.001	7	.22	.003	.21	.1	<.01	.8	.1	<.05	1	<.5	1.0
400942	.5	17.3	10.4	13	.6	8.0	3.1	112	.79	756.4	.4	24.8	7.6	7	.2	10.5	2.6	2	.03	.010	16	10	.02	86	.001	10	.24	.003	.19	.1	.01	.9	.1	<.05	1	<.5	1.2
400943	.3	26.5	10.1	16	.4	9.9	4.2	97	.61	243.1	.4	7.3	9.3	10	.2	12.9	1.0	2	.04	.019	19	9	.02	61	.001	8	.25	.003	.20	.1	.01	1.2	.1	<.05	1	<.5	1.5
400944	.5	33.4	11.3	10	.4	6.4	3.1	95	.87	836.9	1.0	16.4	10.4	10	.1	13.4	2.4	3	.06	.030	23	11	.02	74	.001	10	.28	.003	.23	.2	<.01	1.0	.1	<.05	1	.5	1.9
400945	.1	23.4	8.5	9	.2	5.0	1.9	45	.81	592.1	.7	7.6	10.3	8	<.1	8.8	7.6	2	.03	.009	18	12	.02	62	.001	9	.22	.003	.20	.1	<.01	.9	.1	<.05	1	<.5	2.8
STANDARD DS7	21.1	108.7	69.4	414	.9	56.0	9.7	638	2.43	50.5	5.0	72.9	4.5	72	6.5	6.0	4.6	85	.95	.081	13	202	1.06	379	.125	40	1.00	.082	.45	4.3	.20	2.6	4.3	.26	5	3.4	-

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

10-16-06 P04:40 OUT

Data f FA ____ **DATE RECEIVED:** SEP 11 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL

Copper Ridge Exploration Inc. PROJECT Scheelite Dome FILE # A606035 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	10.1	40.4	49	6.1	3.7	4.3	527	1.98	.9	2.8	3.5	4.4	62	.3	7.7	.1	35	.53	.072	8	8	.56	203	.118	2	.99	.082	.48	.1	<.01	2.1	.3	<.05	5	<.5	-
400946	.6	54.2	97.8	52	27.9	8.8	4.1	154	1.36	417.5	.6	7.2	11.0	9	.9	31.5	1.8	3	.05	.015	23	9	.05	74	.002	10	.37	.009	.23	.1	.01	1.0	.1	<.05	1	<.5	2.1
400947	.5	48.3	30.3	48	2.4	21.3	10.3	564	2.25	512.0	.5	9.4	8.4	48	.3	19.2	2.0	8	1.17	.018	17	10	.43	64	.003	8	.81	.006	.16	.1	.01	1.4	.1	<.05	2	.7	2.0
400948	.5	38.6	50.8	29	14.8	10.1	2.8	1364	1.64	284.6	.4	20.2	7.4	387	.6	27.0	1.5	3	8.82	.022	14	6	.09	32	<.001	15	.23	.002	.12	.2	.02	2.1	.1	.06	<1	<.5	1.0
400949	.5	34.7	209.0	4	2.8	2.2	1.2	31	2.90	5393.8	.3	70.8	5.5	5	.1	100.5	150.7	2	.01	.013	7	8	.01	40	.001	9	.19	.004	.14	.1	.02	.6	.1	1.85	<1	5.3	1.0
400950 (pulp)	7.0	57.2	18.0	96	2.0	14.5	8.2	148	3.11	333.1	.1	831.5	.4	5	.4	25.8	.3	16	.18	.039	7	25	.07	24	.002	2	.30	.004	.19	.5	3.85	1.5	3.9	2.13	1	8.5	-
405051	.5	18.2	51.5	11	11.9	5.5	10.9	53	2.35	>10000	.5	375.7	3.4	18	.4	31.3	49.2	1	.06	.005	4	11	.01	28	.001	3	.14	.003	.09	.1	.06	.3	.2	.86	<1	20.3	1.6
405052	.3	37.4	14.3	18	1.0	13.5	5.7	189	1.56	498.4	.7	3.0	9.7	15	<.1	4.2	2.5	6	.05	.011	19	8	.03	72	.001	5	.38	.010	.16	<.1	.01	.8	.1	<.05	1	<.5	1.8
RE 405052	.3	38.6	14.7	17	.9	13.6	5.6	187	1.54	460.3	.7	2.3	9.9	15	.1	4.0	2.4	4	.06	.011	19	8	.04	71	.001	6	.39	.011	.17	.1	.01	.9	.1	<.05	1	<.5	-
405053	.4	40.2	18.6	25	2.6	16.5	6.1	140	1.62	628.4	.8	7.0	13.5	19	.1	4.8	2.4	4	.11	.031	28	7	.05	82	.001	4	.51	.009	.22	.1	.01	.9	.1	<.05	1	<.5	3.3
405054	.3	21.1	11.6	19	.6	12.4	4.6	163	1.49	369.3	.6	4.6	9.0	15	<.1	2.2	1.5	3	.06	.012	18	8	.04	48	.001	5	.45	.009	.15	<.1	.01	.9	.1	<.05	1	<.5	3.0
405055	.6	42.3	15.9	36	2.5	19.6	10.1	193	2.42	628.0	1.2	2.8	13.9	16	.1	3.7	1.2	3	.06	.020	32	7	.02	50	.001	6	.37	.007	.22	.1	.01	1.2	.2	<.05	1	.5	2.2
405056	.5	51.7	10.4	27	.7	17.7	7.0	175	3.87	>10000	1.0	121.3	13.0	40	.1	5.9	24.5	4	.06	.044	29	8	.02	57	.001	6	.37	.005	.24	.5	.03	1.6	.2	<.05	1	7.2	3.4
405057	.7	50.3	14.3	31	2.1	21.6	9.6	234	2.93	1216.9	1.2	14.5	18.2	24	.1	4.2	6.1	4	.06	.029	41	7	.03	60	.001	6	.42	.006	.25	.1	<.01	1.4	.1	<.05	1	.8	2.1
405058	.6	80.3	5.8	53	.3	34.9	13.9	354	3.97	838.7	1.6	4.9	17.4	20	.1	4.4	1.5	4	.04	.029	53	6	.02	68	.001	4	.37	.007	.27	.2	.02	1.4	.2	<.05	1	<.5	1.7
405059	.8	45.8	13.9	28	2.2	19.2	6.8	213	2.12	567.0	.8	30.2	11.7	14	.1	9.0	69.6	2	.04	.014	28	6	.02	60	.001	5	.30	.006	.22	.1	<.01	1.0	.1	<.05	1	.5	2.5
405060	.8	45.9	6.9	17	.4	12.9	5.4	176	1.63	555.3	.7	6.9	9.1	13	.1	4.4	5.7	1	.05	.011	20	7	.02	45	.001	4	.28	.004	.15	.1	<.01	.9	.1	<.05	1	<.5	2.5
405061	.4	64.8	12.4	20	1.2	17.5	7.7	232	2.22	898.5	.8	4.1	9.0	19	<.1	5.7	2.5	4	.09	.015	15	6	.03	88	.001	7	.45	.005	.22	.1	.01	1.4	.2	<.05	1	1.0	1.9
405062	.3	56.1	6.7	16	.3	12.3	5.1	105	1.50	410.8	.7	3.0	8.5	13	.1	4.8	1.5	2	.07	.009	15	6	.03	74	.001	4	.36	.003	.18	<.1	.01	.9	.1	<.05	1	<.5	3.0
405063	.2	51.1	15.9	11	1.0	6.9	2.5	62	1.38	1522.2	.6	28.2	7.8	26	.1	13.1	46.8	1	.06	.007	14	6	.02	82	.001	4	.27	.003	.16	.1	.01	.8	.1	<.05	1	.9	1.8
405064	.2	13.9	4.5	3	.4	2.5	1.0	40	.59	234.2	.2	8.9	1.2	6	.1	5.2	2.2	<1	.01	.002	2	7	<.01	21	<.001	1	.07	.002	.04	.1	<.01	.3	<.1	<.05	<1	<.5	1.5
405065	.4	51.5	9.7	14	.9	8.5	3.4	78	1.61	1186.4	.7	7.6	9.5	26	.1	13.9	6.3	1	.07	.008	15	7	.02	80	.001	4	.28	.004	.17	.1	<.01	.6	.1	<.05	1	<.5	1.6
405066	.4	162.1	14.5	11	1.2	5.8	2.2	71	5.12	>10000	.8	208.7	15.1	80	.2	16.1	171.3	4	.07	.043	33	7	.02	94	.001	6	.33	.006	.25	.5	.06	4.9	.3	.09	1	24.5	1.0
405067	.5	175.2	13.5	20	.9	17.2	6.7	132	4.53	>10000	1.0	130.5	13.2	76	.3	21.9	93.3	5	.10	.022	27	6	.02	82	<.001	6	.34	.007	.20	.3	.03	2.2	.3	.06	1	6.8	3.4
405068	.3	338.3	14.2	9	1.1	3.1	2.1	70	9.56	>10000	1.6	300.6	16.7	43	.1	21.0	51.1	12	.05	.099	15	10	.02	48	.004	5	.31	.005	.14	.1	.03	8.7	.5	.16	1	42.5	.8
405069	.4	57.2	20.0	5	1.4	3.7	2.7	53	1.75	>10000	.7	176.9	8.4	40	.1	11.8	17.9	1	.02	.009	12	8	.01	46	.001	4	.24	.004	.17	.1	<.01	.8	.1	.19	1	5.4	2.2
405070	.4	156.3	21.0	6	1.3	2.7	.9	68	11.33	>10000	.7	728.9	6.6	15	.1	52.9	460.6	2	.05	.035	16	5	.01	34	.001	5	.27	.009	.13	.9	.02	2.1	.2	.11	1	>100	2.5
405071	.3	51.5	13.6	8	.4	5.8	2.3	51	1.38	1195.3	.5	12.5	10.2	25	.1	7.8	11.8	2	.05	.009	18	8	.02	66	.001	3	.24	.006	.19	.1	.01	.7	.1	<.05	1	1.0	2.1
405072	.4	151.5	12.9	6	1.8	4.1	2.1	75	11.08	>10000	.7	321.3	6.2	16	.1	43.5	316.2	2	.06	.070	8	5	.01	38	.001	7	.30	.014	.11	.5	.02	2.4	.3	.15	1	>100	2.7
405073	.5	93.6	16.2	14	.5	10.7	4.3	101	2.46	2025.6	.7	29.4	11.9	24	.1	11.0	15.7	5	.07	.014	23	9	.04	90	.001	5	.46	.005	.29	.1	.01	1.1	.2	<.05	1	1.7	2.0
405074	.4	84.5	11.9	19	.7	15.1	6.5	109	3.21	>10000	1.0	58.5	10.9	17	.2	12.7	28.7	4	.08	.019	20	7	.05	79	.001	7	.58	.007	.24	.2	.01	1.9	.2	<.05	1	7.2	1.9
405075	1.0	12.3	16.7	67	.1	4.8	6.2	506	3.11	59.3	1.9	2.5	10.0	88	.1	.6	.5	73	1.03	.173	26	9	.59	449	.204	2	1.11	.148	.22	.7	<.01	4.5	.1	<.05	6	<.5	1.0
405076	.5	52.4	20.3	23	.5	21.8	11.6	152	2.64	1694.3	1.0	15.6	11.1	15	.1	11.5	7.8	3	.10	.013	20	7	.06	70	.001	4	.69	.006	.24	.1	.01	1.0	.1	<.05	1	1.3	1.2
405077	.4	308.7	13.1	8	1.0	4.4	2.2	89	10.63	>10000	1.5	599.5	9.4	23	.1	33.0	357.2	11	.06	.066	11	7	.02	47	.002	7	.31	.007	.12	.3	.02	4.5	.3	.12	1	67.1	1.7
405078	.3	7.1	8.2	3	1.3	1.9	.5	39	.53	282.1	.1	2.7	.9	3	.1	3.3	1.1	<1	.03	.001	2	10	<.01	6	<.001	5	.05	.002	.03	<.1	<.01	.2	<.1	<.05	<1	<.5	1.0
STANDARD DS7	21.0	108.0	70.0	411	.9	55.8	9.4	631	2.41	48.9	4.8	68.8	4.4	70	6.3	5.8	4.6	84	.93	.079	13	166	1.05	381	.121	40	.97	.077	.45	3.9	.21	2.5	4.3	.21	5	3.3	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	6.2	2.9	42	<.1	5.1	4.1	518	1.85	11.9	2.9	1.0	4.5	67	<.1	.1	.1	37	.55	.072	7	10	.58	199	.123	2	1.03	.091	.51	.1	<.01	2.3	.3	<.05	5	.5	-
405079	.4	36.6	11.7	9	.2	5.9	3.4	230	1.18	487.3	.6	22.0	7.2	17	.1	10.0	10.4	4	.46	.008	15	10	.04	151	.001	7	.39	.007	.22	.1	.01	.6	.1	.09	1	.5	2.1
405080	.4	53.7	17.6	13	.4	9.0	3.8	156	2.41	>10000	.9	461.5	13.6	52	.1	13.9	40.1	5	.28	.026	21	8	.07	160	.001	8	.46	.006	.31	.3	<.01	1.4	.2	.19	1	5.3	1.7
405081	.3	50.1	7.6	36	.2	16.9	7.5	155	2.88	2632.5	1.3	139.8	15.8	17	.1	10.3	2.6	6	.06	.034	40	9	.03	93	.001	7	.52	.009	.40	.1	.02	1.6	.2	.11	1	1.8	1.7
405082	.5	47.2	8.0	31	.2	23.9	11.4	324	2.81	1053.5	.9	12.5	14.1	15	.1	15.5	2.1	6	.07	.029	35	11	.02	63	.001	10	.49	.010	.29	.1	.01	1.6	.2	.06	1	.9	3.0
405083	.4	40.9	6.5	49	.1	45.5	16.1	710	3.57	795.5	1.1	7.7	9.2	19	.1	23.8	2.0	9	.28	.147	29	18	.04	63	.001	19	.60	.009	.31	.1	.01	2.4	.3	.06	1	.9	3.5
405084	.2	22.8	5.4	19	<.1	12.8	4.9	187	1.41	772.7	.7	4.1	8.0	10	.2	8.2	.8	5	.06	.011	16	12	.02	33	.001	6	.30	.005	.14	.1	.01	.9	.1	<.05	1	.8	2.6
405085	.3	29.3	9.2	27	.2	13.2	4.5	105	1.98	1544.7	.7	15.7	8.0	15	.1	10.9	2.8	5	.07	.018	20	13	.02	48	.001	9	.42	.008	.23	.1	.01	1.1	.1	<.05	1	1.0	3.3
405086	.3	20.7	7.5	25	.2	12.6	5.0	193	1.95	4316.0	.7	50.4	7.4	21	.2	12.6	3.8	4	.06	.011	15	12	.02	32	.001	8	.33	.005	.16	.1	.01	.9	.1	.11	1	1.7	3.5
405087	.3	76.9	9.9	76	.4	38.3	19.5	1088	3.52	1707.4	1.5	28.7	10.8	46	.3	18.7	8.3	7	.09	.034	33	9	.02	64	.001	8	.56	.015	.31	.1	.01	2.1	.2	<.05	1	.5	2.2
405088	.8	251.5	15.6	47	1.4	29.3	15.6	417	3.77	2428.4	1.1	41.3	11.1	15	.5	32.0	43.5	6	.04	.024	30	7	.03	52	.001	7	.43	.008	.29	.1	<.01	1.2	.2	.06	1	2.2	1.7
405089	.9	79.7	92.5	23	2.6	18.7	33.5	37	18.15	>10000	.3	665.7	2.6	11	1.2	346.7	136.3	3	<.01	.010	3	6	.02	25	.002	10	.27	.004	.16	<.1	.03	.7	.2	6.04	<1	63.4	1.0
405090	.4	77.7	9.3	71	.2	43.6	20.5	1085	3.59	1216.3	1.4	5.7	12.8	11	.4	25.8	1.8	6	.04	.023	39	7	.04	54	<.001	6	.44	.013	.26	<.1	.02	1.8	.2	<.05	<1	.9	1.0
405091	.4	60.4	12.8	115	.2	50.1	22.6	1060	4.07	2084.9	1.6	10.1	11.3	15	.5	34.9	2.1	6	.09	.029	38	9	.05	70	.001	10	.53	.018	.31	.2	<.01	2.0	.1	.07	1	1.0	4.3
405092	.3	38.3	10.4	51	.3	23.6	11.4	402	2.55	799.5	.8	2.2	8.8	13	.3	16.2	.6	6	.04	.014	20	11	.02	55	.001	10	.40	.011	.20	.1	<.01	1.4	.1	<.05	1	<.5	2.0
405093	.6	36.1	46.4	28	1.6	12.3	7.9	117	5.45	>10000	.5	495.6	5.5	31	1.2	206.7	9.2	4	.03	.009	9	13	.02	49	.001	9	.36	.008	.21	.1	.01	.9	.1	1.73	1	11.2	3.7
405094	.7	22.0	17.5	30	.8	12.5	6.8	116	9.54	>10000	.9	867.9	5.8	68	1.3	412.2	6.4	5	.40	.247	11	8	.03	70	.002	10	.44	.011	.31	.2	<.01	1.7	.2	2.43	<1	14.4	1.4
405095	.3	53.2	25.7	71	.5	20.5	11.5	578	2.81	3608.4	.5	38.8	4.2	19	2.2	20.5	2.1	5	.04	.011	6	9	.02	47	<.001	13	.35	.006	.19	.1	.01	2.5	.2	<.05	1	.7	2.0
405096	.3	29.7	8.6	21	.1	13.2	7.7	287	1.69	771.9	.6	7.9	7.2	10	<.1	5.9	5.6	4	.02	.018	17	12	.02	53	.001	8	.37	.012	.17	.1	<.01	1.1	.1	<.05	1	.7	2.5
405097	.4	41.2	6.1	34	<.1	23.0	9.6	413	2.40	503.3	1.0	5.1	10.9	13	.1	6.4	1.1	6	.02	.019	24	14	.03	66	.001	8	.57	.016	.24	<.1	<.01	1.6	.2	<.05	1	1.2	4.0
RE 405097	.4	43.9	6.7	35	.1	23.7	9.8	407	2.42	503.4	1.0	5.6	11.4	13	<.1	6.1	1.2	6	.02	.019	24	13	.03	66	.001	10	.56	.015	.23	.1	<.01	1.6	.2	<.05	1	1.1	-
405098	.3	23.4	5.4	27	<.1	21.2	8.3	306	1.70	445.3	.7	3.2	7.8	15	<.1	6.3	.9	4	.02	.011	17	12	.03	59	.001	11	.42	.007	.16	.1	<.01	1.3	.1	<.05	1	<.5	3.2
405099	.3	30.0	5.9	31	<.1	23.6	10.7	349	2.05	730.4	1.1	5.5	10.4	22	<.1	7.4	1.3	5	.03	.015	26	13	.04	84	.001	13	.56	.010	.25	.1	<.01	1.3	.2	<.05	1	.7	3.3
405100 (pulp)	9.9	61.0	3.6	40	7.8	363.9	14.1	166	3.07	449.9	.1	8946.3	.4	5	.1	48.2	<.1	17	.11	.037	6	424	.06	26	.002	1	.29	.005	.20	1.0	6.96	1.4	8.7	2.11	1	23.4	-
405101	.4	31.5	8.7	32	.1	22.0	13.4	424	2.44	1236.2	1.2	13.1	10.8	22	<.1	9.4	2.3	6	.03	.022	29	8	.04	77	<.001	10	.50	.011	.26	<.1	.02	1.3	.2	<.05	<1	.5	1.3
405102	.2	14.8	30.8	9	1.3	7.5	2.9	54	1.65	9698.2	.5	206.8	6.2	93	.1	14.1	31.0	4	.04	.014	11	11	.04	61	.001	6	.41	.007	.18	<.1	.03	.9	.2	.28	1	6.3	.7
405103	.2	22.0	6.7	15	.1	16.0	5.7	121	1.38	1983.3	.6	49.2	9.9	15	<.1	4.6	2.1	4	.03	.014	17	12	.08	53	.001	6	.50	.016	.18	.1	.02	.9	.2	<.05	1	1.2	1.4
405104	.2	22.8	6.9	16	<.1	11.0	4.3	135	1.49	556.9	.7	11.1	9.7	12	<.1	3.1	1.4	6	.03	.014	17	13	.10	62	.002	8	.56	.020	.21	<.1	.01	1.1	.2	<.05	2	.6	.9
405105	.2	14.5	8.9	10	.2	7.4	3.8	94	1.65	6943.9	.4	146.8	6.3	36	<.1	5.4	19.6	5	.06	.015	10	19	.14	45	.002	6	.53	.019	.18	.2	.01	.9	.2	.22	2	5.4	1.4
405106	.5	210.7	114.1	16	16.9	2.9	3.1	331	16.92	>10000	.7	4460.0	9.5	8	1.6	327.5	1424.5	<1	<.01	.195	5	4	<.01	22	.002	6	.16	.014	.09	.2	.10	1.1	<.1	.54	<1	53.7	.9
405107	.5	153.6	56.8	15	5.4	5.7	2.9	224	7.39	>10000	.7	1453.9	8.8	22	.9	85.3	444.7	4	.02	.134	20	6	.03	73	.002	9	.41	.022	.31	.1	.05	1.2	.2	.29	1	24.0	.4
405108	.3	58.9	15.3	38	1.3	26.5	15.2	487	3.74	>10000	1.4	334.6	12.8	12	.2	15.0	105.2	6	.03	.041	31	9	.05	68	.001	7	.55	.012	.30	.1	.03	1.2	.2	<.05	1	5.3	1.5
405109	.5	45.0	8.6	83	<.1	46.4	25.6	1622	3.72	710.2	2.1	8.7	13.3	14	.1	1.6	2.7	8	.05	.030	39	8	.03	80	<.001	9	.51	.013	.32	.1	.03	1.9	.2	<.05	1	.8	.5
405110	.4	38.2	10.3	77	.2	37.2	17.1	1070	3.62	931.1	1.6	23.9	10.7	16	<.1	1.7	6.1	10	.07	.034	29	11	.04	72	.001	13	.65	.018	.31	.1	.03	2.0	.1	<.05	2	.6	1.5
405111	.3	28.0	6.0	28	<.1	18.9	7.4	269	2.09	1420.2	.9	20.2	8.3	12	.1	3.3	2.5	6	.03	.020	21	10	.04	62	.001	8	.50	.010	.24	.1	.01	1.1	.2	<.05	1	.8	.7
STANDARD DS7	20.6	107.6	69.1	411	.9	55.1	9.3	632	2.99	49.3	4.8	71.7	4.4	69	6.3	5.8	4.5	84	.93	.078	11	164	1.06	376	.111	38	.97	.076	.44	3.8	.20	2.6	4.2	.20	5	4.3	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	2.0	2.4	43	<.1	3.5	3.9	498	1.73	7.9	2.6	1.9	3.5	46	<.1	.2	.1	33	.43	.076	6	11	.56	191	.098	1	.84	.039	.47	.1	<.01	1.6	.4	<.05	5	<.5	-
405112	.5	4.8	.6	4	<.1	4.4	1.6	59	.46	73.5	.2	2.1	.8	2	<.1	1.1	.1	2	.02	.006	3	16	.01	5	<.001	2	.07	.006	.03	.1	<.01	.2	<.1	<.05	<1	<.5	1.4
405113	.2	53.4	5.6	53	<.1	36.5	15.1	1081	3.33	334.3	1.4	3.3	10.8	14	.1	2.0	.5	5	.08	.041	40	7	.04	38	<.001	5	.34	.006	.14	.1	.02	1.1	.1	<.05	<1	<.5	2.0
405114	.7	31.9	3.2	29	<.1	23.4	9.1	461	2.23	485.4	1.0	6.3	7.6	12	<.1	1.7	.5	3	.05	.023	25	9	.02	29	<.001	4	.23	.006	.14	.1	.01	.9	.1	<.05	<1	<.5	2.5
405115	.2	13.4	3.4	15	<.1	9.5	5.6	205	1.21	312.7	.6	2.1	8.4	9	<.1	3.7	.3	4	.05	.013	19	11	.02	21	<.001	3	.21	.006	.10	.1	.01	.8	.1	<.05	1	<.5	2.2
405116	.6	41.5	4.4	41	<.1	33.6	12.1	363	2.86	283.9	1.1	2.0	9.6	13	<.1	1.7	.6	5	.06	.033	35	10	.02	34	<.001	4	.30	.005	.16	.1	.02	1.3	.1	<.05	1	.7	3.2
405117	.5	78.4	5.9	51	.1	65.2	21.7	312	5.14	316.7	.9	2.0	9.0	15	<.1	3.0	1.1	11	.08	.072	33	17	.06	39	.001	5	.52	.005	.15	.1	.06	2.8	.2	<.05	1	.9	1.6
RE 405117	.5	71.3	5.7	54	.1	65.9	21.4	305	5.12	317.6	1.0	3.7	9.4	15	<.1	3.0	1.2	11	.08	.073	33	17	.06	39	.001	4	.53	.005	.15	.1	.07	2.8	.2	<.05	1	.7	-
405118	.5	42.0	6.0	46	<.1	43.8	16.7	306	2.93	292.8	1.1	2.8	9.7	15	.1	2.7	.7	4	.10	.068	31	10	.03	41	.001	4	.40	.006	.16	.1	.02	1.7	.1	<.05	1	.5	1.7
405119	.2	33.5	6.5	32	.2	21.4	8.2	210	2.13	396.8	.8	5.7	9.1	9	.1	3.1	.6	2	.04	.022	31	7	.02	43	<.001	2	.26	.005	.17	.1	.01	.8	.1	<.05	1	<.5	2.5
405120	.5	36.8	20.0	43	.4	22.3	9.1	248	2.33	846.7	1.0	19.5	9.2	11	.4	8.1	2.3	3	.05	.019	32	7	.02	53	<.001	3	.27	.006	.20	.1	<.01	.9	.1	<.05	1	.7	2.2
405121	.6	90.9	10.0	74	.2	40.5	14.4	328	5.59	1882.9	1.6	21.5	9.5	17	.1	9.3	3.6	8	.05	.047	37	12	.02	40	<.001	4	.37	.006	.15	.1	.03	3.0	.2	<.05	1	1.0	1.0
405122	.5	27.1	2.4	7	<.1	6.5	4.0	108	.83	332.6	.4	7.5	6.4	8	.2	1.4	.9	5	.06	.022	13	15	.07	75	.004	1	.32	.013	.13	.4	<.01	.5	.1	<.05	1	.5	1.7
405123	.2	73.1	6.4	32	.2	30.7	10.9	184	2.38	407.0	1.5	28.8	12.0	52	.1	1.1	4.1	22	.48	.019	20	23	.49	124	.031	1	1.92	.086	.33	.3	.01	2.4	.3	<.05	6	1.8	1.9
405124	.3	64.9	6.9	21	.2	20.5	6.1	188	2.02	296.3	1.0	69.1	11.5	43	.2	1.4	7.5	15	.34	.018	20	21	.39	87	.026	1	1.22	.036	.23	1.4	<.01	1.8	.2	<.05	4	.8	2.5
405125	1.1	12.0	14.6	65	<.1	4.5	6.3	476	2.99	7.2	2.0	2.0	9.6	84	.2	.3	.2	72	1.00	.179	26	10	.58	507	.202	1	1.02	.137	.20	.7	<.01	4.2	.1	<.05	6	.8	2.8
405126	.2	37.4	4.0	29	<.1	29.4	10.6	171	2.30	195.4	1.5	7.0	14.9	65	.2	.8	.7	25	.65	.045	26	28	.60	166	.036	2	2.18	.115	.54	.2	<.01	2.6	.5	<.05	7	.6	3.9
405127	.3	74.6	5.5	29	.1	31.4	10.4	175	2.60	162.0	1.4	64.1	10.0	51	.1	1.0	2.0	28	.53	.018	18	31	.66	115	.041	2	2.23	.139	.46	.7	<.01	3.1	.4	.12	7	1.1	3.0
405128	.2	64.0	4.7	62	.1	42.8	15.9	242	4.35	295.4	1.8	4.6	14.6	42	.1	1.0	.8	32	.24	.046	31	22	1.19	258	.104	1	2.68	.031	1.00	.1	<.01	2.7	1.1	<.05	8	.8	1.6
405129	.2	44.8	7.0	28	.1	18.9	7.6	147	1.92	390.7	1.2	8.7	11.8	24	.2	1.7	3.1	14	.18	.037	21	18	.37	129	.017	2	1.10	.023	.33	.2	.01	1.6	.3	.07	4	.9	4.4
405130	.5	6.5	.7	3	<.1	2.4	.7	34	.38	43.0	.1	1.6	.5	2	.1	1.5	.2	2	.03	.003	1	16	.02	23	.002	<1	.08	.003	.03	.2	<.01	.2	<.1	<.05	<1	<.5	1.1
405131	.2	36.1	7.9	30	<.1	15.7	12.1	226	1.72	337.5	1.0	17.3	10.6	16	.2	1.2	2.3	13	.14	.012	19	20	.33	79	.024	2	.87	.026	.24	.2	.01	1.8	.2	<.05	3	<.5	3.5
405132	.4	14.1	12.2	41	.1	25.9	14.6	321	1.34	104.6	.7	3.5	11.1	67	.2	1.2	.7	13	.21	.011	22	21	.31	54	.027	1	.84	.031	.21	.2	.01	2.2	.2	<.05	3	<.5	2.0
405133	.2	37.5	4.4	31	<.1	15.9	5.9	142	2.12	268.5	.9	15.7	12.2	34	.1	.9	3.1	21	.21	.026	25	24	.57	113	.035	<1	1.48	.042	.61	.3	.01	2.1	.5	<.05	5	.5	3.5
405134	.5	8.1	1.8	2	<.1	2.1	1.0	33	.41	83.4	.1	10.1	.4	5	<.1	.4	1.7	1	.02	.003	1	13	.01	10	.003	1	.07	.003	.02	.3	<.01	<.1	<.1	<.05	<1	<.5	1.5
405135	.2	27.3	10.8	38	.1	15.7	5.6	327	1.12	224.5	.4	11.6	7.1	39	.4	.7	1.6	13	.50	.013	15	19	.19	61	.024	1	.76	.031	.15	.2	<.01	1.3	.1	<.05	3	.9	3.5
405136	.4	32.7	11.0	30	.2	20.9	7.6	253	2.06	361.0	.9	23.9	8.6	83	.3	.8	4.3	19	.57	.017	20	22	.31	120	.034	1	1.49	.085	.26	.5	<.01	2.2	.1	<.05	5	.8	3.3
405137	.3	45.3	7.8	30	.2	29.9	11.6	191	2.06	279.4	1.0	7.6	9.7	135	.2	1.1	1.2	22	.57	.018	22	25	.36	91	.035	1	1.75	.085	.30	.3	.01	2.3	.2	.06	6	.7	3.9
405138	.2	44.1	7.9	34	.1	29.5	8.3	194	1.94	275.4	.8	9.2	9.7	72	.2	1.5	1.1	23	.44	.017	20	26	.41	125	.037	1	1.58	.067	.28	.3	.01	2.5	.2	<.05	6	.5	3.5
405139	.3	48.3	5.5	31	.2	21.5	6.5	245	1.86	211.0	.6	109.6	9.4	52	.2	2.3	18.0	17	.48	.014	19	21	.33	111	.024	1	1.42	.056	.21	.8	.01	1.8	.1	<.05	4	1.1	4.0
405140	.2	24.2	4.6	13	.2	11.9	4.8	219	.89	157.1	.4	5.6	6.4	21	.2	1.2	2.8	8	.36	.013	12	15	.17	63	.015	3	.59	.022	.11	.2	.01	.9	.1	<.05	2	.7	1.5
405141	.3	24.3	3.5	24	<.1	22.2	11.1	289	1.08	76.6	.7	5.8	9.6	57	.2	.5	1.3	12	.62	.010	17	19	.18	97	.031	2	.90	.034	.12	.3	<.01	1.6	.1	<.05	3	.5	2.5
405142	.2	21.2	3.8	20	<.1	14.2	5.3	356	1.05	85.3	.7	3.2	9.6	59	.3	.4	.6	12	1.01	.013	18	19	.22	76	.031	3	.91	.053	.16	.2	<.01	1.5	.1	<.05	3	.6	4.5
405143	.4	121.4	6.8	35	.2	24.7	10.0	192	2.42	120.3	1.4	2.3	17.4	100	.2	.5	.9	21	.51	.045	31	25	.41	134	.055	2	1.64	.074	.47	.2	<.01	2.5	.2	.16	6	.6	6.0
405144	.2	42.0	5.8	42	.1	26.3	10.9	351	1.60	169.8	.9	18.5	12.8	104	.5	1.7	5.3	16	.96	.019	24	22	.34	99	.039	2	1.38	.061	.28	.3	<.01	2.1	.2	<.05	4	<.5	4.0
STANDARD DS7	20.9	111.9	70.3	410	.9	55.8	9.7	629	2.39	49.7	4.9	79.2	4.6	72	6.4	5.9	4.6	84	.94	.082	14	195	1.05	381	.126	40	.99	.085	.45	4.1	.20	2.5	4.3	.23	5	3.6	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	2.2	2.6	44	<.1	3.8	4.5	492	1.78	4.5	2.7	<.5	4.1	44	<.1	<.1	.1	33	.46	.076	7	13	.57	189	.115	3	.85	.065	.48	.1	<.01	1.9	.3	<.05	4	<.5	-
405145	.2	37.0	5.6	53	.1	30.4	13.5	299	1.55	140.2	.9	4.2	12.0	94	.2	.9	.9	15	.70	.018	21	19	.28	74	.037	2	1.34	.077	.27	.2	<.01	2.0	.2	.08	5	<.5	4.6
405146	.6	111.4	5.9	29	.3	16.3	7.4	200	1.34	50.7	1.0	26.6	10.5	61	.2	.3	6.0	15	.94	.014	19	21	.25	48	.037	2	1.16	.095	.23	.3	<.01	2.2	.1	.06	4	<.5	4.1
405147	.1	15.1	5.1	23	<.1	14.5	5.5	334	.78	30.2	.6	1.2	7.8	83	.3	.3	.3	12	1.65	.012	17	15	.17	37	.030	3	.97	.080	.13	.2	<.01	1.3	.1	<.05	3	<.5	1.5
405148	.5	41.5	4.6	23	.2	18.6	7.1	279	.98	105.7	.7	21.9	8.9	85	.2	.6	3.1	10	.83	.012	15	16	.23	49	.027	3	.99	.064	.13	.8	<.01	1.6	.1	<.05	3	<.5	1.5
405149	.1	14.1	4.3	24	<.1	17.5	5.4	349	.82	108.4	.6	2.6	8.2	84	.2	.5	.4	10	.84	.010	16	14	.20	39	.028	3	.93	.060	.07	.7	<.01	1.6	<.1	<.05	3	<.5	1.7
405150 (pulp)	8.8	56.5	4.4	39	7.9	329.8	12.6	161	3.05	453.9	.1	8532.4	.3	5	.1	51.1	<.1	15	.11	.035	6	353	.06	27	.002	3	.29	.005	.20	.9	7.05	1.3	8.1	2.06	1	24.2	-
405151	.3	35.8	6.8	29	.2	13.4	5.4	169	1.09	252.1	.9	8.1	10.0	45	.1	2.5	1.0	10	.43	.012	17	16	.17	63	.018	3	.79	.024	.16	.2	<.01	1.3	.1	<.05	3	<.5	4.5
405152	.2	34.4	5.6	30	.1	23.0	11.4	226	1.45	148.0	1.2	10.6	12.5	54	.3	.7	1.4	13	.39	.018	22	20	.27	88	.034	2	1.19	.039	.26	.2	<.01	2.2	.2	<.05	4	<.5	3.9
405153	1.2	21.2	.9	2	<.1	2.1	.7	27	.38	103.1	.1	2.8	.8	2	.1	1.2	.2	2	.01	.002	3	14	.01	13	.002	3	.06	.004	.02	.3	.01	.3	<.1	<.05	<1	<.5	.5
405154	.3	30.8	8.7	31	.1	21.0	7.7	159	1.46	132.7	1.1	2.4	11.7	83	.1	.6	.8	16	.60	.017	22	23	.28	255	.043	3	1.37	.072	.32	.3	.01	2.6	.2	<.05	5	<.5	4.5
405155	.5	42.8	6.4	63	.1	35.9	11.9	231	2.51	120.5	1.6	4.2	14.9	176	.2	.6	.5	24	1.42	.160	35	25	.46	105	.067	4	2.30	.149	.55	.6	.01	3.2	.3	.07	7	<.5	5.0
RE 405155	.4	44.9	6.7	66	.2	39.0	12.3	239	2.61	127.8	1.6	3.6	15.9	182	.2	.6	.5	24	1.45	.166	38	26	.47	110	.066	2	2.38	.154	.58	.6	.01	3.1	.3	.06	8	<.5	-
405156	.3	37.0	4.8	50	.1	22.5	8.5	213	2.16	82.5	1.5	5.3	15.1	116	.3	.3	.6	23	.93	.024	28	26	.47	114	.072	6	2.04	.126	.59	.8	.01	3.2	.3	.09	7	<.5	5.5
405157	.5	44.5	5.7	47	.1	39.2	15.9	249	1.63	45.6	1.1	20.7	13.1	123	.2	.3	2.3	20	1.06	.025	26	26	.36	98	.060	3	1.94	.155	.39	1.7	.01	2.9	.2	<.05	7	<.5	5.0
405158	.2	39.3	5.0	39	.1	23.7	10.9	166	1.79	111.1	.8	34.6	9.7	51	.1	1.2	2.7	15	.43	.022	18	21	.32	126	.026	2	1.34	.067	.29	.6	.01	2.2	.2	<.05	4	<.5	4.7
405159	.6	39.4	6.6	43	.1	30.2	12.3	257	1.70	90.5	1.0	15.9	13.4	92	.2	.5	1.8	19	.66	.024	23	24	.38	108	.048	3	1.45	.065	.39	.3	.02	2.7	.2	<.05	6	<.5	4.4
405160	.2	29.2	6.9	41	.1	31.9	15.1	254	1.42	76.7	1.0	3.8	12.3	57	.2	.4	.3	17	.67	.018	22	21	.24	87	.048	4	1.19	.049	.28	.2	<.01	2.5	.2	<.05	4	<.5	4.5
405161	.4	24.9	7.4	119	.1	42.2	20.3	566	1.16	63.2	.7	17.4	9.7	57	.3	.7	2.3	11	1.14	.012	20	18	.24	110	.037	4	.96	.071	.23	.3	<.01	1.8	.2	<.05	3	<.5	1.7
405162	.2	5.8	.6	3	<.1	2.2	.6	30	.57	12.9	.1	.9	1.0	3	<.1	.3	.1	2	.02	.002	2	12	.02	12	.006	1	.09	.009	.03	.1	.01	.3	<.1	<.05	<1	<.5	1.3
405163	.5	34.0	5.5	24	.1	21.2	14.3	194	1.64	845.8	1.2	9.5	10.0	25	.2	4.2	1.1	10	.14	.014	24	14	.19	181	.016	3	.82	.015	.28	.3	.01	1.4	.2	<.05	3	<.5	3.1
405164	.5	34.3	9.9	27	.1	10.9	4.0	80	2.34	314.5	1.7	5.1	11.9	31	.1	4.8	.5	15	.10	.024	30	16	.30	110	.016	2	.99	.019	.43	.4	.01	1.7	.3	.08	3	<.5	4.4
405165	.7	10.1	1.3	2	<.1	1.8	.6	25	.40	43.7	.1	1.4	.4	2	<.1	4.1	.9	<1	.01	.002	1	20	.01	12	.001	3	.05	.003	.02	.1	.01	.2	<.1	<.05	<1	<.5	3.0
405166	.3	44.6	6.2	43	.1	36.9	15.0	199	2.50	268.5	1.8	9.0	12.0	39	.1	3.1	.8	12	.20	.035	26	16	.32	128	.019	3	1.22	.019	.34	2.0	.01	1.8	.2	<.05	3	<.5	3.8
405167	.5	25.0	2.3	49	<.1	17.4	7.1	133	2.82	131.3	.9	4.0	10.8	12	.1	2.6	.3	22	.09	.017	30	21	.59	113	.024	5	1.53	.014	.53	.1	<.01	2.5	.3	<.05	5	<.5	3.2
405168	.3	39.7	8.8	21	.2	16.2	7.8	220	1.54	649.4	.8	89.1	8.5	37	.3	1.1	5.9	11	.76	.014	22	15	.24	103	.024	3	.85	.029	.31	2.6	.01	1.6	.2	.07	3	<.5	2.5
405169	.5	20.9	7.1	20	<.1	18.0	6.3	254	1.13	51.4	.5	40.1	8.7	24	.2	.6	3.2	11	.35	.013	17	18	.21	104	.031	3	.70	.036	.19	3.7	.01	1.4	.1	<.05	3	<.5	3.5
405170	.3	37.6	5.8	22	.1	16.3	7.1	116	1.67	94.8	1.2	50.8	14.1	32	.1	1.1	2.9	15	.15	.016	25	22	.30	119	.037	3	1.07	.032	.41	.3	<.01	2.0	.2	<.05	4	<.5	4.6
405171	.2	27.0	5.2	27	<.1	11.2	5.4	80	2.10	96.2	1.2	5.1	13.9	19	.1	.8	.3	15	.09	.014	28	18	.36	171	.041	1	1.10	.030	.64	.6	.01	1.7	.3	.07	4	<.5	3.5
405172	.1	18.4	9.4	16	<.1	13.9	5.6	178	1.02	59.2	.5	11.2	8.3	20	.2	1.1	.9	7	.30	.009	14	13	.14	43	.022	1	.60	.027	.11	1.5	.01	1.2	.1	<.05	2	<.5	1.9
405173	.4	37.6	5.1	34	.1	25.2	10.1	368	1.62	499.8	1.1	242.8	10.6	43	.3	2.3	3.3	12	.35	.018	26	17	.37	103	.023	2	1.07	.027	.32	.2	.01	1.8	.3	<.05	3	<.5	1.5
405174	.2	24.5	9.3	37	.1	24.6	7.3	250	1.17	124.5	.7	65.5	9.6	52	.2	.9	3.5	11	.69	.013	17	15	.23	62	.036	3	1.05	.081	.16	2.5	<.01	1.8	.1	<.05	3	<.5	1.6
405175	1.2	11.9	13.1	62	<.1	4.7	6.0	464	2.94	6.3	1.9	1.9	9.7	78	.2	.3	.1	69	.96	.164	24	8	.59	464	.196	1	.99	.154	.20	.7	<.01	4.8	.1	<.05	6	<.5	2.4
405176	.2	29.3	8.6	35	.1	19.3	5.8	279	1.56	298.3	.8	22.1	11.0	40	.3	2.8	1.8	11	.62	.018	23	17	.25	86	.024	6	1.09	.028	.23	1.3	<.01	1.8	.2	<.05	4	<.5	3.9
405177	.1	12.4	6.4	24	<.1	9.5	3.7	246	.83	64.5	.5	21.3	7.1	43	.3	.6	2.2	8	1.08	.009	13	18	.18	46	.029	7	.75	.032	.10	2.0	<.01	1.5	.1	<.05	2	<.5	4.0
STANDARD DS7	20.9	107.3	68.6	411	.9	54.9	9.5	634	2.40	48.4	4.8	69.6	4.4	71	6.4	5.8	4.5	85	.95	.079	13	171	1.05	371	.122	39	.99	.089	.44	3.9	.20	2.6	4.2	.20	5	3.4	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	4.2	1.8	2.5	42	<.1	3.9	3.6	510	1.76	.8	2.9	.9	3.9	50	<.1	<.1	.1	33	.48	.073	6	12	.57	199	.113	<1	.89	.056	.50	.1	<.01	2.1	.3	<.05	4	<.5	-
405178	30.1	16.5	7.4	36	.1	14.2	4.4	276	1.30	168.6	.6	20.0	8.3	52	.2	1.0	2.0	10	.58	.013	14	16	.20	49	.026	4	.66	.027	.13	2.1	.01	1.7	.1	.07	2	<.5	2.6
405179	4.4	18.6	7.3	25	.1	10.2	3.5	303	.93	108.1	.6	38.5	7.7	49	.4	.6	2.7	11	1.26	.013	13	17	.20	45	.031	3	.69	.042	.14	3.6	.01	1.5	.1	<.05	3	<.5	2.5
405180	1.4	33.7	9.2	30	.1	12.8	5.9	212	1.18	174.8	.7	21.3	8.9	39	.3	.8	3.4	10	.76	.012	14	17	.18	60	.027	1	.81	.054	.15	1.9	<.01	1.6	.1	<.05	3	<.5	4.0
405181	2.2	19.1	7.9	29	.2	13.4	5.2	304	.89	724.1	.5	77.8	7.0	46	.5	.9	7.2	11	1.28	.011	13	15	.17	47	.025	2	.75	.059	.13	7.5	.01	1.6	.1	<.05	3	.6	2.5
405182	.9	15.2	7.6	25	.1	9.1	3.4	243	.76	113.5	.4	20.2	7.2	42	.4	.5	2.3	9	.77	.009	13	16	.14	48	.027	2	.65	.031	.09	1.3	<.01	1.6	<.1	<.05	2	<.5	2.1
405183	1.5	40.7	10.7	34	.2	26.9	9.0	244	1.75	135.6	.9	20.2	10.8	109	.3	.5	1.7	16	.86	.030	20	18	.30	117	.036	2	1.72	.089	.30	1.6	<.01	2.6	.2	<.05	5	<.5	4.4
405184	.7	17.6	7.7	29	.1	13.0	4.7	240	1.24	160.0	.6	11.3	9.8	37	.3	1.0	.9	9	.27	.012	17	12	.19	92	.013	3	.65	.017	.21	.6	<.01	1.5	.1	<.05	2	<.5	3.8
405185	1.3	72.9	32.9	20	2.8	7.3	5.2	196	2.52	>10000	.6	87.3	8.0	90	.9	15.0	24.3	7	.92	.012	12	11	.17	51	.010	2	.96	.073	.10	71.1	<.01	1.3	.1	.85	3	7.4	.7
405186	.7	18.3	7.7	28	.2	15.8	4.7	223	.96	110.6	.4	83.2	7.6	28	.3	.9	9.1	11	.61	.010	12	13	.27	86	.019	2	.93	.047	.10	1.3	.01	1.6	.1	<.05	3	.5	1.6
405187	.9	9.2	6.7	24	<.1	8.9	2.4	302	.68	72.8	.3	17.2	6.8	61	.5	.4	1.6	7	.74	.008	12	13	.15	49	.026	4	.62	.028	.06	.5	<.01	1.3	.1	<.05	2	<.5	3.5
405188	.5	12.9	9.1	21	.1	8.6	2.8	285	.68	130.1	.3	13.0	7.7	30	.3	.9	1.7	6	.60	.009	12	15	.14	54	.020	2	.61	.027	.06	1.1	<.01	1.3	.1	<.05	2	<.5	3.7
405189	.9	15.7	6.5	24	.2	6.3	3.6	100	.82	146.5	.4	119.7	4.8	8	.2	2.1	15.1	4	.14	.008	11	10	.04	34	.001	4	.33	.005	.07	.6	<.01	1.2	.1	<.05	1	<.5	2.2
405190	.5	17.8	7.9	34	.3	13.7	4.2	187	1.07	137.9	.6	561.3	9.4	26	.4	2.1	30.7	10	.37	.013	17	16	.16	81	.015	5	.71	.030	.11	9.3	.01	1.7	.1	<.05	2	<.5	3.1
405191	.8	12.3	5.7	30	<.1	12.4	4.0	279	.81	25.3	.6	28.8	8.7	126	.4	.4	1.8	12	1.29	.011	14	17	.23	103	.042	5	1.50	.153	.09	.5	<.01	1.8	.1	<.05	5	<.5	3.6
405192	.4	17.8	7.0	42	.1	23.5	6.3	410	.89	25.6	.7	68.5	9.5	95	.7	.3	5.3	10	1.39	.013	20	15	.25	101	.038	2	1.14	.113	.12	1.2	<.01	1.6	.1	<.05	4	<.5	3.9
405193	.5	16.3	5.8	31	<.1	11.0	3.7	235	.79	15.2	.6	19.3	9.4	33	.4	.3	1.3	8	.91	.009	13	15	.21	68	.034	5	.86	.033	.17	1.3	<.01	1.7	.1	<.05	3	<.5	3.7
405194	.4	12.9	6.5	26	<.1	14.2	4.6	298	.75	16.6	.4	43.9	9.6	37	.4	.6	3.3	6	.90	.008	14	17	.18	54	.034	2	.79	.055	.08	1.1	<.01	1.5	.1	<.05	3	<.5	4.5
405195	.5	35.2	8.1	42	.1	18.8	9.3	304	1.59	97.1	1.1	21.7	12.3	54	.3	2.3	1.9	14	.52	.017	22	18	.36	113	.035	1	1.32	.064	.24	.6	<.01	2.3	.2	<.05	5	.6	5.5
405196	.4	77.3	5.4	61	.1	31.7	17.2	295	2.44	211.1	1.5	24.7	13.7	60	.3	2.8	1.5	20	.34	.019	30	20	.69	175	.043	2	1.88	.026	.38	1.1	<.01	3.2	.4	<.05	6	.5	2.7
405197	.8	8.9	2.9	13	<.1	5.3	1.3	123	.48	12.8	.3	8.5	6.2	21	.2	.4	1.1	6	.47	.008	9	11	.07	57	.022	1	.49	.025	.05	.2	<.01	.9	<.1	<.05	2	<.5	1.0
RE 405197	.8	8.3	3.0	13	<.1	4.7	1.5	125	.49	13.2	.3	9.9	6.5	22	.1	.4	1.1	7	.49	.007	9	12	.07	59	.023	1	.50	.026	.05	.2	.01	1.0	<.1	<.05	2	<.5	-
405198	.3	14.1	7.3	25	<.1	12.0	4.7	168	.93	83.9	.6	20.4	11.3	64	.3	.6	1.7	11	.82	.010	17	16	.18	97	.034	2	1.06	.093	.14	2.4	<.01	1.7	.1	<.05	4	<.5	4.9
405199	.6	23.9	6.6	21	<.1	10.4	3.4	103	1.17	45.4	.6	9.8	10.4	17	.1	.6	1.1	12	.14	.012	13	16	.23	222	.025	1	.70	.035	.19	.9	<.01	1.6	.1	<.05	3	.6	2.7
405200 (pulp)	6.9	55.9	18.0	99	1.9	15.0	8.2	146	3.03	325.2	.1	869.1	.4	5	.3	24.3	.2	15	.17	.041	7	27	.08	24	.002	2	.30	.004	.21	.4	3.80	1.7	3.9	2.29	2	10.0	-
405301	.2	42.2	4.2	40	<.1	11.1	3.1	28	2.84	216.8	1.2	1.4	15.2	10	.2	2.8	1.9	10	.03	.024	37	8	.09	50	.003	4	.68	.010	.31	.1	.02	1.2	.2	<.05	3	.7	.7
405302	.3	35.6	3.0	33	<.1	5.3	2.2	19	2.08	424.9	.8	2.8	12.3	8	.3	4.0	.6	8	.01	.019	38	6	.04	46	.002	4	.46	.008	.32	<.1	.01	.9	.2	<.05	4	<.5	.8
405303	.4	35.0	8.2	40	.2	17.1	5.8	135	2.72	389.1	1.2	3.2	14.3	20	.2	6.4	5.4	21	.02	.029	40	17	.38	101	.028	3	1.36	.012	.51	.1	.01	1.9	.5	.08	4	<.5	1.5
405304	.5	6.7	.9	13	<.1	6.8	1.7	52	.77	33.7	.1	.9	.8	2	<.1	1.1	.2	3	.01	.004	3	11	.17	13	.002	1	.29	.003	.05	<.1	<.01	.4	<.1	<.05	1	<.5	1.5
405305	.4	49.8	3.9	20	.2	9.4	2.2	111	2.11	1328.3	.7	46.0	9.1	24	.2	1.7	2.5	15	.02	.008	12	19	.37	76	.004	3	.94	.023	.11	<.1	<.01	1.9	.2	.10	4	1.1	1.0
405306	.3	31.1	4.3	29	<.1	18.1	4.0	167	1.93	604.9	1.1	2.3	11.9	8	<.1	2.3	.2	15	.04	.008	17	20	.40	59	.003	2	.91	.015	.16	<.1	.01	2.4	.2	<.05	4	.6	1.0
405307	.2	15.3	4.3	47	<.1	33.9	6.6	228	2.22	68.4	.5	18.0	10.2	9	.1	1.0	.1	26	.04	.010	14	32	.58	139	.034	2	1.51	.025	.48	.1	.01	3.0	.5	<.05	7	<.5	.8
405308	.4	2.7	.3	2	<.1	2.2	.8	29	.35	27.0	.1	<.5	.4	1	<.1	.4	.1	<1	.01	.004	1	11	.01	8	.001	<1	.06	.003	.01	<.1	<.01	.2	<.1	<.05	<1	<.5	1.5
405309	.2	85.9	4.3	15	<.1	14.1	2.5	228	2.18	1697.9	.6	5.8	12.4	13	<.1	3.7	1.1	15	.05	.007	10	22	.45	39	.007	3	1.09	.018	.11	<.1	<.01	2.4	.1	.14	4	1.8	1.0
405310	.4	27.9	2.4	11	<.1	7.1	5.5	96	1.43	2520.3	.4	2.5	1.2	34	.1	4.0	.4	5	.04	.010	8	15	.27	71	.002	1	.33	.003	.04	<.1	<.01	1.3	.1	<.05	2	.9	1.2
STANDARD DS7	20.6	110.0	69.1	412	.9	55.0	9.6	630	2.41	48.6	4.9	68.4	4.4	70	6.5	5.8	4.5	84	.95	.078	12	172	1.06	371	.121	38	.98	.076	.44	3.9	.20	2.5	4.2	.20	5	3.5	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	4.5	2.5	2.7	43	<.1	3.7	4.0	521	1.78	1.0	2.8	5.2	4.0	58	<.1	<.1	.1	36	.49	.071	7	14	.54	190	.113	<1	.88	.047	.46	.1	.01	2.1	.3	<.05	5	<.5	-
405311	.3	51.1	1.3	9	.1	5.8	2.4	118	1.67	1276.6	.3	3.7	1.4	22	<.1	2.6	.5	5	.03	.004	8	14	.22	65	.002	1	.32	.006	.05	<.1	<.01	1.1	.1	<.05	2	.5	1.5
405312	.3	53.9	2.7	24	<.1	32.5	11.1	260	2.75	7154.8	.3	9.7	4.1	85	.1	3.3	.8	18	.08	.004	13	22	.86	39	.004	2	1.31	.023	.13	<.1	.01	2.5	.2	.08	4	1.4	1.5
405313	.3	7.9	1.7	18	<.1	18.8	28.3	166	4.09	>10000	1.6	31.8	9.1	182	.1	28.8	1.2	14	.06	.010	12	20	.70	74	.010	4	1.29	.008	.35	.1	.01	1.8	.4	.90	5	4.3	1.5
405314	.3	19.2	3.3	24	.2	8.2	6.3	82	2.17	>10000	.6	10.3	3.6	72	.1	10.6	1.2	7	.04	.008	13	17	.39	783	.003	1	.71	.008	.16	.1	<.01	1.4	.7	.13	3	1.6	.6
405315	.3	7.9	1.1	3	<.1	2.8	1.6	35	.46	242.4	.5	2.0	1.9	5	.1	.9	.2	1	.01	.005	8	13	.02	34	.002	4	.15	.003	.07	.1	<.01	.3	.1	<.05	<1	<.5	.7
405316	.4	46.8	10.4	117	<.1	29.4	15.2	463	4.89	74.1	2.2	2.8	14.6	35	<.1	1.2	.5	36	.05	.026	44	52	1.25	99	.023	<1	2.84	.023	.18	<.1	.01	3.7	.1	<.05	10	.6	1.0
405317	.2	15.5	4.1	39	<.1	23.9	8.6	486	2.04	19.4	.7	.7	16.6	48	.1	.5	.4	22	.57	.037	27	28	.69	232	.067	2	1.39	.032	.28	.5	<.01	3.1	.2	<.05	4	<.5	1.0
STANDARD DS7	21.1	108.9	70.2	421	.9	56.5	9.8	643	2.43	50.7	5.0	74.5	4.6	85	6.4	5.7	4.5	86	.96	.079	14	197	1.07	377	.126	39	1.01	.082	.45	3.9	.21	3.0	4.3	.21	5	3.8	-

Sample type: ROCK R150.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data f FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605885R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Au** gm/mt
400720	6.65
400721	5.62
400722	8.10
400789	9.88
GDSD02	.88
STANDARD SL20	6.12

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE PULP

10-30-06 P06:08 OUT

Data 4 FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605885

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. vanRanden

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.5	3.0	5.1	44	<.1	4.5	4.2	537	1.90	12.8	2.9	3.9	4.3	65	<.1	.1	.1	37	.52	.075	8	20	.58	222	.124	2	1.01	.096	.51	.1	<.01	2.1	.3	<.05	5	<.5	-
400720	.8	139.7	316.4	10	21.8	1.8	6.8	18	21.01	>10000	.4	7565.7	4.4	5	.8	567.8	1866.6	5	.01	.026	3	8	.02	33	.006	3	.14	.004	.09	.5	.42	1.4	.2	2.55	1	>100	7.40
400721	.5	139.3	348.6	10	18.3	2.0	5.5	21	19.02	>10000	.5	6150.2	5.4	8	.9	484.6	1350.6	5	.01	.035	3	9	.01	57	.006	2	.14	.003	.11	.5	.30	1.5	.2	1.82	1	>100	7.20
400722	.6	150.9	276.8	8	14.4	1.0	.9	12	11.85	>10000	.3	8933.1	4.1	15	.8	192.8	1484.8	5	<.01	.040	5	8	.01	47	.004	5	.15	.004	.15	.5	.38	1.3	.1	.18	1	92.7	3.60
400789	3.4	191.0	22.1	3	4.4	1.3	5.5	25	29.65	>10000	.2	11752.0	1.5	2	.2	268.2	1020.0	9	.02	.004	1	5	.01	4	.001	<1	.08	.006	.01	5.2	.06	1.2	<.1	4.80	1	>100	1.00
400790	.1	13.0	13.6	22	.2	11.6	5.2	623	1.74	1403.4	.7	66.8	10.5	385	.2	2.6	8.5	17	10.79	.017	16	23	.44	49	.019	1	.89	.067	.17	.2	.01	3.1	.1	.06	4	1.0	1.80
GDSD 01	.4	127.3	43.2	10	7.4	2.0	1.0	79	5.73	>10000	1.3	413.8	6.2	30	.7	225.0	284.3	2	.07	.051	14	4	.01	63	.001	7	.19	.005	.10	.1	.18	3.7	.2	.06	<1	31.3	1.10
GDSD 02	.4	58.0	134.2	6	5.0	3.1	1.2	30	3.36	>10000	.4	826.3	7.7	21	.2	74.5	160.4	2	.01	.015	12	7	.02	140	.001	5	.19	.004	.16	.2	.01	.7	.1	.80	<1	12.5	1.60
RE GDSD 02	.5	61.6	139.6	6	5.3	3.4	1.2	32	3.57	>10000	.4	884.7	8.3	23	.3	79.8	173.4	2	.01	.017	13	7	.02	147	.001	6	.20	.005	.17	.3	.02	.7	.1	.84	<1	11.9	-
GDSD 03	.2	74.0	26.0	8	1.9	5.1	1.7	12	5.67	951.9	.4	32.7	8.0	6	<.1	152.5	71.0	2	.01	.010	7	5	.01	15	.001	7	.14	.002	.12	.1	.19	.6	.1	4.60	<1	9.0	1.40
GDSD 04	.4	41.9	6.3	12	.2	14.4	5.1	60	2.94	>10000	.9	137.1	10.6	9	<.1	10.3	30.6	3	.04	.060	19	8	.01	86	.001	7	.24	.005	.21	.4	.01	1.5	.2	.51	<1	13.8	1.20
GDSD 05	.3	25.0	6.9	10	.3	7.4	3.7	29	1.63	8013.9	.5	82.6	11.5	5	.1	15.0	12.0	3	.01	.018	17	7	.02	76	.001	5	.28	.005	.23	.2	.01	1.0	.1	.23	1	4.5	1.30
GDSD 06	.2	21.4	7.4	6	.6	3.9	1.6	56	.94	3366.7	.3	55.2	5.9	13	.1	21.6	1.4	1	.02	.010	8	7	.01	137	<.001	9	.15	.002	.11	.1	<.01	.6	.1	.09	<1	<.5	1.30
GDSD 07	.2	103.6	21.6	7	4.2	2.4	1.1	24	4.40	824.2	.3	31.1	5.3	5	<.1	201.9	23.0	2	.01	.011	8	6	.01	74	.001	9	.16	.002	.12	<.1	.36	.6	.2	1.19	<1	9.6	1.10
GDSD 08	.1	12.3	31.2	8	.4	2.1	1.0	20	.71	504.3	.2	26.4	6.2	8	.2	20.4	1.4	1	.01	.006	12	6	.01	37	.001	9	.15	.003	.13	<.1	<.01	.6	.1	<.05	<1	<.5	1.50
GDSD 09	.2	117.3	23.5	11	1.8	5.9	3.1	67	2.57	2121.0	.4	16.0	6.0	9	<.1	33.9	49.3	3	.01	.010	11	6	.04	75	.001	6	.21	.004	.12	.1	.02	1.1	.1	.21	1	3.2	.90
GDSD 10	.2	7.4	24.7	3	.2	3.5	4.9	53	1.14	6506.7	.6	142.0	3.9	28	.1	16.3	24.7	1	.04	.005	6	8	.01	45	<.001	2	.12	.003	.11	<.1	<.01	.4	.1	.17	<1	7.5	1.40
GDSD 11	.4	42.6	14.1	41	.2	28.5	13.8	180	2.19	190.5	2.0	7.3	12.7	14	.2	1.3	4.7	25	.10	.013	18	28	.57	191	.049	<1	1.60	.029	.59	.1	.01	2.3	.5	.07	5	.5	1.50
STANDARD D	20.5	109.9	68.4	414	.9	55.0	9.6	625	2.41	49.2	4.9	69.6	4.4	69	6.3	5.5	4.4	84	.93	.079	12	162	1.05	362	.120	38	.96	.074	.44	3.8	.19	2.6	4.2	.20	5	3.6	-

Standard is STANDARD DS7.

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.

(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.

- SAMPLE TYPE: Rock R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

09-27-06 P04:41 OUT

Data FA _____ **DATE RECEIVED:** SEP 6 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605884R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. van Randen

SAMPLE#	Au** gm/mt	Sample gm
400550(pulp)	1.06	14.6
400570	.71	29.2
400571	7.48	29.2
400576	.58	29.2
400577	1.26	29.2
400600(pulp)	9.14	14.6
400616	.51	29.2
RE 400616	.50	29.2
400650(pulp)	.96	14.6
400661	1.81	29.2
400662	11.75	29.2
400670	3.05	29.2
400671	.75	29.2
400672	2.28	29.2
400700(pulp)	9.43	14.6
400710	4.59	29.2
400714	1.24	29.2
400716	1.88	29.2
400724	1.31	29.2
400750(pulp)	.98	14.6
STANDARD SL20	5.90	29.2

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: ROCK PULP
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

11-23-06 P01:16 OUT

Data FA ____ **DATE RECEIVED:** NOV 13 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Jacky Wang

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605884 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: J. vanRanden

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.4	1.7	3.1	42	<.1	3.3	3.9	500	1.84	1.0	3.1	<.5	4.7	60	<.1	<.1	.1	35	.53	.075	9	9	.55	197	.116	1	1.00	.072	.47	1.5	<.01	3.1	.3	<.05	5	.8	-
400533	.9	105.7	11.9	47	.1	36.1	11.9	269	3.04	1093.9	2.0	20.6	14.8	21	.5	21.5	2.6	13	.19	.059	37	15	.12	129	.003	8	.87	.009	.23	.8	.01	3.5	.2	<.05	2	1.4	5.8
400534	.9	169.2	8.5	33	.1	45.4	9.3	268	3.42	1040.6	1.9	14.3	13.6	44	.2	6.0	1.7	43	.41	.061	26	38	.59	133	.023	6	2.56	.050	.22	.2	.01	5.2	.3	<.05	8	2.1	10.6
400535	.7	59.8	7.1	19	<.1	23.1	6.1	124	1.97	437.1	1.5	4.6	12.7	26	.2	5.9	1.0	19	.11	.016	23	23	.25	100	.010	4	1.05	.013	.27	.6	<.01	2.7	.3	<.05	3	1.5	8.0
400536	.3	120.2	8.5	36	.2	22.8	10.5	206	2.70	1023.0	1.5	12.5	12.9	68	.5	5.0	1.5	24	.58	.022	14	25	.54	87	.029	2	2.27	.138	.20	.2	.01	3.9	.2	.14	7	1.7	7.1
400537	.9	123.0	10.3	99	.2	26.3	10.4	197	2.72	1001.1	2.5	22.1	12.2	55	3.0	4.2	2.2	30	.30	.027	18	32	.44	73	.030	2	1.71	.076	.21	1.8	<.01	4.0	.2	.07	5	2.0	7.6
400538	.6	90.1	8.0	55	.2	22.5	7.1	163	2.49	746.4	2.3	13.2	11.2	54	2.8	2.8	1.8	28	.31	.025	18	29	.47	71	.027	1	1.75	.081	.23	.1	<.01	3.8	.2	.08	6	1.8	4.3
400539	.6	164.7	9.9	163	.2	28.5	10.0	208	3.73	4938.3	1.5	37.0	11.3	119	2.8	7.1	4.1	30	.24	.028	16	28	.51	112	.013	2	2.60	.036	.19	3.9	<.01	4.1	.2	<.05	7	2.1	4.3
400540	.2	98.5	11.4	93	.2	25.8	9.8	200	2.45	1642.6	1.9	76.7	11.8	45	3.6	5.6	7.3	26	.27	.038	18	24	.47	65	.028	2	1.77	.037	.25	.6	.01	3.8	.2	<.05	5	1.5	9.4
400541	.6	68.4	6.7	65	.1	20.3	7.3	227	2.16	1065.0	1.7	26.2	11.0	42	.6	5.2	2.9	22	.19	.028	19	27	.43	70	.028	2	1.46	.020	.27	.5	<.01	3.4	.3	<.05	5	1.2	3.8
400542	.4	94.2	7.3	77	.2	26.7	10.5	302	2.68	734.4	2.0	65.2	14.5	47	.5	4.1	4.9	25	.26	.023	25	26	.47	73	.036	2	1.71	.034	.30	1.0	.01	4.0	.3	<.05	6	1.5	5.5
400543	.4	76.6	7.4	80	.2	24.6	8.9	292	2.49	513.5	1.5	33.9	14.1	29	.6	3.8	2.8	24	.26	.024	21	27	.56	64	.044	1	1.69	.047	.37	.3	<.01	4.4	.4	<.05	6	1.2	3.8
400544	.1	101.5	6.9	42	.2	27.0	10.9	331	2.65	472.4	1.3	68.7	12.0	39	.2	2.9	5.3	26	.36	.021	18	27	.57	63	.043	2	1.76	.103	.27	.2	<.01	4.6	.3	.10	7	1.6	7.1
400545	.4	91.5	6.8	40	.3	27.9	10.4	252	2.68	743.6	1.5	29.4	13.3	52	.1	2.6	1.9	28	.43	.050	22	29	.58	77	.040	2	2.08	.101	.36	.4	.01	5.0	.4	<.05	8	1.7	5.3
400546	.3	136.3	6.7	30	.2	34.7	11.1	256	3.32	709.7	2.1	17.0	16.0	64	.1	2.9	2.3	30	.44	.030	28	28	.57	90	.043	3	2.48	.102	.35	.1	.01	4.9	.4	<.05	7	1.7	4.3
400547	.3	62.4	5.6	18	<.1	14.3	5.0	189	1.57	342.2	1.1	11.0	12.8	23	.1	2.4	1.5	12	.17	.017	17	16	.31	69	.017	2	1.04	.040	.20	.3	<.01	2.4	.1	<.05	4	1.2	4.6
400548	.2	100.4	8.6	57	.2	21.0	9.1	372	2.22	1469.6	1.1	113.0	13.1	42	.4	5.3	6.3	19	.33	.025	20	19	.42	70	.013	2	1.61	.067	.18	1.7	.01	3.5	.2	<.05	5	1.5	7.3
400549	.3	159.0	8.3	23	.3	30.7	9.1	213	2.92	1955.5	1.2	83.1	13.2	64	.1	4.1	6.3	29	.55	.026	21	28	.65	71	.029	2	2.59	.118	.24	.9	.01	5.5	.3	.15	8	2.7	5.3
400550 (pulp)	6.4	56.3	17.7	101	1.9	15.9	8.5	145	2.98	324.7	.1	862.2	.4	5	.3	27.0	.2	19	.16	.038	8	28	.09	24	.002	2	.35	.004	.21	.4	3.86	2.3	3.8	2.18	2	10.7	-
400551	.1	61.1	29.3	18	.5	6.8	3.6	172	1.35	1286.9	.7	74.5	10.7	20	.1	9.3	4.9	7	.13	.022	21	11	.14	67	.003	4	.62	.007	.19	.1	<.01	1.8	.1	<.05	2	1.2	7.4
400552	.5	84.8	15.9	21	1.2	12.0	4.7	74	2.00	878.7	1.0	44.3	17.1	25	.3	41.0	2.5	6	.07	.018	49	6	.06	74	.001	5	.50	.007	.24	.4	.01	1.8	.2	<.05	1	1.2	3.3
400553	.1	20.7	4.5	11	<.1	6.1	3.5	147	.95	224.1	.4	4.3	10.4	6	.1	2.8	.9	4	.05	.011	20	10	.07	79	.003	4	.41	.013	.17	.1	.01	.9	.1	<.05	1	.9	6.4
400554	.3	45.4	8.0	15	.1	9.3	4.5	134	1.23	549.9	.6	11.0	10.9	10	.2	3.2	2.4	6	.05	.011	20	12	.16	72	.007	2	.63	.012	.22	.4	.01	1.6	.2	<.05	2	1.5	4.9
400555	.2	94.3	7.4	42	.2	38.4	14.2	166	3.11	4264.2	1.6	15.6	15.1	46	.1	5.5	2.4	30	.29	.021	26	29	.77	117	.043	2	2.24	.069	.66	.9	<.01	5.5	.7	.20	8	2.8	5.1
400556	1.2	42.5	26.5	23	.7	32.8	13.3	120	3.13	>10000	1.1	451.6	7.0	54	.1	20.9	33.6	14	.23	.011	17	15	.41	52	.011	2	1.10	.039	.18	18.0	<.01	2.5	.2	.83	4	10.7	.7
RE 400556	1.1	40.8	25.9	23	.8	32.3	12.8	118	3.11	>10000	1.1	443.6	6.5	52	.1	20.5	33.0	13	.23	.010	16	15	.41	50	.011	1	1.06	.037	.16	17.6	<.01	2.3	.2	.82	3	10.6	-
400557	.2	66.5	18.7	55	.3	36.8	16.5	212	3.38	3558.9	2.2	58.0	17.2	55	.1	10.8	8.4	29	.41	.024	34	29	.80	123	.050	<1	2.45	.088	.83	1.2	.01	5.7	.9	.14	9	2.0	2.8
400558	.5	75.5	6.0	46	.1	35.5	14.2	219	3.17	807.6	1.7	12.5	17.2	64	.1	2.5	1.6	32	.38	.038	32	26	.80	132	.053	1	2.42	.068	.69	1.2	.01	5.3	.8	.08	8	1.3	5.0
400559	.2	85.6	23.8	43	.8	24.4	10.7	243	3.01	1266.3	1.9	40.5	15.9	89	.1	3.3	20.2	26	.27	.026	32	24	.68	93	.048	1	2.10	.054	.57	10.0	<.01	5.0	.7	<.05	7	2.4	5.4
400560	.4	54.5	8.0	30	.2	16.8	7.9	148	2.42	5569.4	1.5	77.3	14.9	39	.1	5.0	6.0	16	.14	.016	23	19	.45	79	.026	1	1.23	.035	.39	2.3	.01	3.0	.4	.21	5	3.0	4.0
400561	.1	32.9	3.1	21	<.1	11.4	5.2	107	1.71	196.6	1.1	3.0	13.3	21	<.1	.8	.8	13	.09	.011	22	17	.36	81	.031	1	.94	.027	.29	.1	<.01	2.8	.3	<.05	4	1.2	4.9
400562	.4	15.3	4.3	20	<.1	11.9	5.7	217	1.29	156.7	1.0	2.1	12.5	18	<.1	.7	.5	10	.10	.011	22	14	.30	99	.032	1	.79	.018	.42	.6	.01	2.0	.3	<.05	3	.6	1.8
400563	.2	38.7	3.8	18	<.1	18.6	8.5	249	1.55	290.7	.9	8.5	9.7	19	<.1	1.2	.8	13	.16	.020	19	14	.32	93	.029	1	.98	.034	.30	.2	.01	2.8	.3	<.05	4	.9	6.3
400564	.3	14.8	3.1	19	<.1	14.5	5.8	146	1.41	95.5	.7	2.9	12.9	7	<.1	.8	.2	9	.07	.012	26	12	.24	97	.030	2	.72	.014	.38	.6	<.01	1.8	.3	<.05	2	.6	6.4
400565	.2	14.0	17.5	20	<.1	10.1	3.9	448	1.12	163.7	.5	3.5	9.8	29	.1	4.4	.5	6	.61	.017	19	11	.09	86	.008	5	.50	.015	.20	.1	.01	1.6	.1	<.05	1	.6	5.7
STANDARD DS7	20.7	108.6	69.6	407	.9	54.6	9.4	628	2.39	48.2	5.0	68.4	4.6	70	6.3	6.1	4.6	84	.94	.082	14	168	1.05	373	.126	39	.99	.080	.46	4.0	.20	3.7	4.2	.20	15	3.8	-

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: Rock R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

10-12-06 P01:09 OUT

Data___ FA ____ DATE RECEIVED: SEP 6 2006 DATE REPORT MAILED:.....

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

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ACME ANALYTICAL

Copper Ridge Exploration Inc. PROJECT Scheelite Dome FILE # A605884 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.4	1.9	3.2	40	<.1	3.7	4.0	493	1.76	3.6	3.0	.9	4.5	61	<.1	<.1	.1	34	.50	.084	8	8	.54	199	.123	1	.97	.074	.50	1.5	<.01	2.1	.4	<.05	5	<.5	-
400566	.2	17.5	9.1	20	<.1	14.8	5.2	386	1.33	155.9	.7	5.4	9.7	89	.1	.8	.4	14	1.77	.015	17	15	.23	84	.036	3	1.26	.135	.26	.2	<.01	2.1	.1	<.05	4	<.5	5.0
400567	.5	66.6	7.7	23	<.1	19.1	6.2	324	1.99	279.6	1.0	54.0	15.6	49	.1	1.2	3.4	19	.76	.029	23	19	.40	97	.042	2	1.51	.124	.25	1.8	.01	2.5	.2	<.05	4	.6	4.3
400568	.2	18.1	5.5	13	<.1	8.2	4.0	179	1.22	197.9	.8	15.7	17.1	20	.1	.7	1.8	11	.40	.015	24	13	.21	91	.028	2	.67	.034	.24	.1	.01	1.5	.1	<.05	2	<.5	5.0
400569	.4	29.2	7.9	13	<.1	9.1	4.2	136	1.27	1467.3	.8	54.8	14.1	16	.1	2.2	4.6	7	.06	.011	24	11	.15	91	.010	2	.52	.023	.21	1.1	.01	1.1	.1	<.05	2	.6	5.5
400570	.3	34.2	5.3	16	.3	13.6	7.6	148	3.11	>10000	1.2	717.5	11.4	52	.1	19.5	21.9	11	.24	.016	24	12	.22	173	.005	3	.72	.031	.23	.2	<.01	1.5	.2	.61	2	7.9	2.6
400571	3.7	22.9	14.8	11	2.0	19.7	32.8	96	23.50	>10000	2.2	8014.1	3.2	440	.1	316.8	192.5	4	2.11	.009	26	5	.05	27	.005	1	.34	.023	.15	.9	.06	.8	.2	5.28	1	>100	.3
400572	.2	73.0	7.9	32	.2	31.7	10.2	319	2.21	1109.0	1.6	55.2	14.8	50	<.1	2.1	4.9	19	.23	.026	29	20	.41	92	.033	2	1.45	.066	.38	.8	.01	2.9	.3	<.05	5	<.5	3.3
400573	.4	124.5	9.0	32	.3	22.9	9.1	341	3.19	3314.4	1.8	136.3	16.1	80	.1	4.4	10.7	22	.51	.062	31	23	.47	82	.031	2	1.82	.111	.28	7.3	.01	3.1	.2	.09	6	2.5	5.4
400574	.3	89.1	11.2	38	.2	23.0	7.4	186	2.94	438.9	2.1	8.2	20.3	65	.1	1.4	1.0	25	.37	.024	27	24	.55	98	.056	2	2.17	.115	.55	.2	<.01	3.5	.5	.09	7	.8	2.9
400575	1.4	12.6	18.3	68	<.1	5.3	6.3	454	2.98	170.5	2.2	8.3	11.5	83	.2	.4	.4	68	.91	.190	27	8	.55	485	.209	2	.95	.124	.19	1.1	.01	4.6	.1	<.05	6	<.5	1.1
400576	.4	90.7	9.4	28	.4	14.2	6.9	160	2.99	3235.2	2.4	567.1	20.7	94	.1	3.7	35.2	18	.23	.062	44	19	.44	120	.040	2	1.52	.067	.45	9.1	.01	2.5	.5	.20	5	1.3	5.9
400577	1.2	55.5	8.9	15	1.6	15.6	5.9	205	4.06	>10000	.9	1289.3	12.0	73	.1	22.1	68.1	12	.24	.019	19	12	.27	63	.008	1	.81	.036	.21	51.8	.01	1.5	.1	.98	3	15.9	4.1
400578	.2	49.8	8.1	15	.1	16.3	6.1	238	1.46	500.0	.7	16.3	11.4	23	<.1	1.4	2.2	9	.13	.012	21	11	.19	74	.008	1	.62	.033	.21	.4	.01	1.2	.1	<.05	2	<.5	6.3
400579	.3	33.9	5.7	16	<.1	13.0	4.9	266	1.36	422.6	1.0	12.5	11.7	25	.1	1.1	1.0	9	.11	.013	18	12	.18	76	.012	1	.59	.027	.22	.8	.01	1.2	.1	<.05	2	.8	2.2
400580	.3	57.3	11.7	20	.1	22.4	9.7	496	1.63	828.2	1.0	31.8	10.4	35	.1	1.8	5.2	12	.15	.017	20	14	.19	71	.016	1	.79	.039	.18	.9	.01	1.5	.1	<.05	2	1.0	2.4
400581	.4	68.2	4.5	16	.2	12.4	5.3	125	1.63	573.6	1.2	57.0	13.4	14	<.1	2.6	9.0	10	.08	.014	27	12	.26	80	.013	2	.72	.024	.30	.9	.01	1.0	.3	<.05	2	.5	6.9
RE 400581	.4	59.1	4.3	16	.2	11.9	5.1	124	1.58	557.4	1.1	42.8	12.5	13	.1	2.5	8.6	9	.07	.012	25	12	.25	77	.012	1	.70	.022	.30	.9	.01	1.1	.3	<.05	3	.5	-
400582	2.0	125.8	8.9	24	.2	18.7	6.4	202	2.22	820.2	1.3	191.9	12.1	49	.1	3.0	16.6	17	.45	.016	21	16	.41	70	.022	1	1.49	.092	.27	.4	.01	2.3	.2	.14	5	2.0	7.8
400583	.4	67.6	7.6	20	.3	11.1	4.1	215	1.32	895.3	.7	56.2	9.3	23	.3	2.1	7.5	8	.13	.013	17	11	.15	61	.008	1	.61	.031	.19	.8	.01	1.1	.1	<.05	2	.8	4.6
400584	.2	39.4	4.2	11	<.1	9.1	3.6	147	1.09	456.2	.6	11.0	10.4	9	.1	1.3	1.6	6	.10	.013	17	8	.13	70	.007	1	.48	.017	.23	.3	<.01	.8	.1	<.05	1	<.5	5.7
400585	.4	74.4	7.4	29	.2	25.0	6.6	190	2.21	1292.9	1.2	53.1	13.4	31	.1	2.1	4.6	17	.24	.019	25	17	.43	83	.017	1	1.19	.042	.27	.9	.01	2.1	.3	<.05	4	.7	6.3
400586	.1	53.5	4.7	36	.1	18.2	6.3	139	2.43	454.0	1.4	14.6	18.4	23	.1	1.6	1.6	17	.17	.021	29	18	.49	98	.036	<1	1.34	.038	.59	.1	.01	2.1	.5	<.05	4	.7	6.8
400587	.3	41.6	4.6	29	<.1	18.5	7.5	119	1.96	517.9	1.4	7.8	17.3	29	.1	1.4	1.1	15	.19	.022	24	17	.42	79	.028	1	1.25	.043	.46	.5	.01	1.8	.5	<.05	4	<.5	6.5
400588	.1	93.0	5.5	10	.2	9.8	3.5	72	1.34	1098.4	1.0	20.9	10.6	18	.2	2.2	3.7	9	.11	.011	13	9	.19	83	.009	1	.72	.036	.25	.1	<.01	1.1	.2	<.05	2	1.5	5.1
400589	.5	57.2	10.6	19	.2	13.0	6.5	245	1.50	2015.2	.9	29.7	11.2	43	.2	2.1	3.1	10	.24	.012	16	14	.19	62	.011	1	.83	.069	.16	1.2	<.01	1.3	.1	<.05	3	1.4	4.0
400590	.1	32.4	11.2	19	<.1	11.8	4.9	224	1.11	530.0	.6	12.3	8.9	18	.3	1.3	1.7	9	.14	.013	14	12	.17	49	.010	1	.62	.035	.14	.3	<.01	1.2	.1	<.05	2	<.5	3.0
400591	.5	67.5	5.0	27	.1	22.4	9.5	283	2.10	780.9	1.0	25.6	12.8	27	.1	1.9	2.2	14	.20	.017	20	18	.37	61	.016	2	1.08	.057	.20	.7	.01	2.1	.2	<.05	4	.9	5.5
400592	.2	37.4	15.0	25	.2	17.7	7.9	252	1.44	511.7	.9	33.0	15.4	53	.3	1.6	3.7	11	.29	.019	23	19	.21	58	.023	1	.94	.071	.23	.5	.01	1.8	.2	<.05	3	<.5	4.9
400593	.3	78.8	13.3	43	.2	26.6	11.2	330	2.68	551.4	1.4	9.0	14.1	125	.5	1.6	1.2	25	.85	.024	20	28	.51	67	.056	1	2.46	.179	.40	.7	<.01	3.4	.3	.07	7	.9	3.9
400594	.2	52.5	5.5	46	.2	24.8	11.9	288	2.70	373.5	1.4	6.7	15.2	96	.1	1.1	.8	23	.57	.019	32	27	.58	90	.052	1	1.97	.123	.47	.3	<.01	3.2	.3	<.05	6	.6	4.1
400595	.3	77.7	11.2	57	.2	34.5	13.4	353	2.85	891.5	1.4	34.2	13.1	111	.3	1.9	3.1	32	1.04	.019	25	34	.58	79	.048	1	2.72	.155	.38	2.3	<.01	4.7	.4	<.05	9	.8	6.9
400596	.1	18.4	9.4	44	<.1	12.9	7.0	329	1.65	167.8	.8	4.2	10.9	45	.4	.9	.5	22	.70	.013	17	23	.38	42	.050	1	1.29	.078	.23	.2	.01	3.6	.1	<.05	5	<.5	5.8
400597	.2	21.5	20.1	52	.1	17.3	8.9	427	1.73	206.9	.9	8.5	10.1	135	.5	1.2	.9	24	2.66	.016	21	27	.36	53	.061	2	1.98	.153	.25	.6	.01	3.9	.2	<.05	7	<.5	4.7
400598	.2	84.0	8.6	43	.2	26.1	11.2	220	2.61	534.9	1.2	9.0	13.5	58	.2	2.5	1.4	25	.63	.015	22	28	.62	72	.044	1	1.93	.112	.33	.2	.01	3.8	.3	<.05	7	1.9	5.8
STANDARD DS7	20.5	107.2	70.3	412	.9	55.4	9.7	624	2.38	50.0	5.0	71.3	4.5	72	6.5	6.0	4.6	84	.94	.080	14	169	1.05	370	.126	39	.98	.077	.45	3.9	.20	2.6	4.2	.20	5	3.3	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data C FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	6.8	2.5	36	<.1	3.2	3.4	504	1.76	1.2	2.4	<.5	3.6	47	<.1	<.1	.1	35	.46	.068	6	8	.55	171	.104	1	.87	.053	.42	.1	<.01	1.6	.3	<.05	4	<.5	-
400599	.1	14.1	6.1	33	<.1	8.9	4.0	235	1.22	224.3	.6	5.7	8.3	45	.2	.8	1.1	14	.95	.011	12	15	.27	36	.030	2	.86	.053	.15	.2	<.01	2.1	.1	<.05	3	<.5	7.8
400600 (pulp)	8.8	57.9	3.7	38	8.0	315.0	12.5	165	3.04	445.9	.1	8488.9	.4	5	.1	50.9	<.1	15	.11	.038	6	350	.07	28	.002	2	.28	.006	.20	1.0	6.81	1.5	9.0	2.13	1	23.4	-
400601	.2	17.2	5.9	60	<.1	12.5	5.8	284	1.45	217.8	.7	6.4	10.2	45	.2	.8	.6	18	.81	.014	14	18	.31	54	.035	2	.98	.056	.21	.3	.02	2.4	.2	<.05	4	<.5	7.3
400602	.1	26.2	5.5	23	<.1	8.9	3.9	305	1.16	175.8	.6	7.3	9.5	46	.3	1.0	1.2	11	1.00	.011	13	14	.21	33	.028	2	.66	.037	.10	1.5	.01	1.6	.1	<.05	3	<.5	5.6
400603	.2	51.6	8.8	35	.2	11.8	6.2	297	1.87	586.0	.9	36.8	10.5	32	.2	1.6	7.1	14	.29	.015	17	15	.30	51	.029	2	.90	.043	.23	3.4	.01	2.2	.2	<.05	3	.9	6.8
400604	.6	34.3	2.6	32	<.1	13.0	4.3	111	1.60	216.3	1.0	3.0	12.2	20	.1	1.2	.3	14	.10	.013	22	14	.37	71	.026	1	.97	.029	.32	.2	.01	1.5	.3	<.05	4	<.5	4.2
400605	.2	94.4	5.8	29	.1	24.1	11.1	177	2.47	404.7	1.6	8.9	15.7	62	.1	1.2	.9	22	.37	.020	24	19	.48	121	.056	2	1.72	.077	.49	.6	.01	2.5	.5	.22	5	.5	4.7
400606	.3	44.3	6.1	27	.2	6.6	3.5	112	2.21	219.1	1.4	4.1	14.8	37	.1	.6	.7	16	.13	.015	28	16	.45	143	.061	1	1.14	.028	.52	.1	.01	2.0	.4	.13	4	<.5	5.8
400607	.3	61.3	9.7	27	.2	11.9	7.3	137	2.48	647.9	1.3	13.7	15.4	40	.1	1.0	1.5	19	.18	.016	24	17	.50	105	.055	2	1.26	.036	.53	.2	.01	2.4	.5	.14	4	.6	7.5
RE 400607	.3	58.3	9.3	27	.2	12.3	7.8	135	2.44	638.7	1.3	12.5	14.7	40	.1	1.0	1.4	20	.18	.016	24	17	.49	100	.055	1	1.25	.033	.51	.2	.01	2.3	.5	.14	4	<.5	-
400608	.3	42.9	8.3	27	.1	18.5	8.7	195	1.82	345.3	1.2	10.0	12.1	38	.2	.9	1.9	17	.33	.016	19	17	.48	87	.046	1	1.33	.061	.40	.6	.01	2.3	.3	<.05	4	<.5	6.1
400609	.4	40.5	8.1	32	.2	24.4	10.4	298	2.26	206.9	1.3	3.6	11.6	170	.4	.7	.9	25	2.48	.019	22	22	.34	69	.057	3	3.50	.279	.25	.3	.01	3.0	.2	.14	11	<.5	5.5
400610	.3	37.0	1.6	8	<.1	8.3	2.6	72	.98	174.9	.2	10.7	1.3	3	<.1	.8	.8	4	.03	.006	4	11	.15	11	.002	2	.25	.004	.05	<.1	<.01	.5	.1	<.05	1	<.5	3.1
400611	.2	76.6	6.8	51	.1	25.0	9.1	175	3.10	553.7	1.0	2.4	15.2	13	.1	2.1	1.4	15	.18	.030	34	17	.55	56	.006	1	1.21	.009	.23	.1	.02	1.5	.3	<.05	5	<.5	6.7
400612	.2	85.0	9.5	33	.2	21.2	9.7	350	2.87	636.3	.8	15.8	13.1	27	.1	2.6	2.6	20	.80	.028	26	23	.61	73	.016	4	1.38	.025	.30	.1	<.01	2.8	.4	<.05	5	<.5	6.9
400613	.3	136.3	29.5	49	1.2	22.4	10.6	495	3.93	9440.7	1.8	495.7	12.7	92	1.3	14.3	61.5	13	1.43	.044	29	13	.25	65	.004	5	.79	.009	.22	4.0	.01	2.6	.2	<.05	2	2.4	7.4
400614	.1	132.4	10.1	24	.3	27.5	11.1	331	3.02	2649.9	1.4	128.6	12.7	28	.1	8.8	16.1	13	.24	.061	34	11	.25	63	.002	5	.76	.006	.21	.5	.01	2.7	.2	<.05	2	2.0	9.1
400615	.2	134.1	9.7	28	.4	26.6	10.8	270	3.63	4091.1	2.3	44.2	16.0	62	.2	7.3	29.2	11	.14	.034	39	12	.34	109	.004	3	.92	.006	.25	1.1	.01	2.3	.2	<.05	3	1.8	5.7
400616	.3	280.4	54.6	18	4.1	12.2	9.3	103	10.76	>10000	2.4	510.0	10.3	249	.8	67.6	519.2	8	.32	.046	21	8	.15	51	.002	2	.55	.011	.24	64.6	.04	1.2	.2	1.82	2	57.6	3.9
400617	.2	142.8	15.7	22	.7	21.5	7.5	126	3.25	9280.3	2.1	74.5	16.5	100	.1	9.1	50.2	7	.26	.036	44	6	.14	43	.001	4	.52	.005	.23	1.7	.01	1.6	.2	<.05	1	2.4	5.2
400618	.2	114.2	6.6	49	.2	39.3	14.0	234	3.51	902.1	2.8	25.0	23.0	12	.1	2.2	4.9	5	.15	.053	65	6	.19	43	.001	3	.65	.004	.18	.1	.01	1.3	.1	<.05	2	.8	5.8
400619	.2	68.8	6.1	37	.1	31.9	13.3	263	3.20	894.1	2.4	15.3	20.4	19	.1	3.6	2.5	8	.18	.047	57	8	.27	45	.001	3	.92	.005	.20	.1	.01	1.5	.2	<.05	2	.8	6.1
400620	.1	34.5	9.5	42	.1	26.9	10.1	425	2.53	479.1	1.0	3.1	15.4	19	.1	5.5	1.2	12	.45	.049	40	14	.55	38	.004	1	1.45	.005	.23	.1	<.01	1.7	.3	<.05	4	<.5	5.4
400621	.1	22.2	10.7	30	.1	18.1	7.8	555	2.00	482.1	.7	4.5	11.1	78	.2	6.1	2.6	12	2.52	.022	30	13	.42	47	.003	<1	1.16	.005	.19	<.1	<.01	1.9	.1	<.05	3	<.5	6.0
400622	.2	34.4	14.3	39	.2	21.6	10.0	664	2.48	430.9	.7	5.5	14.5	93	.2	10.6	1.2	15	3.03	.042	38	16	.42	65	.005	2	1.22	.005	.22	<.1	.01	2.4	.2	<.05	4	<.5	9.8
400623	.1	22.1	12.5	32	.2	18.6	7.8	560	2.12	307.9	.6	2.8	12.9	145	.2	6.6	1.5	12	5.89	.030	36	11	.34	56	.004	3	1.01	.004	.21	<.1	.01	2.2	.2	<.05	3	<.5	11.9
400624	.1	21.9	9.6	22	.1	12.1	5.6	472	1.48	260.9	.6	2.2	10.1	186	.1	3.2	1.5	13	6.28	.017	22	14	.35	40	.012	3	.77	.013	.16	<.1	<.01	2.1	.2	<.05	3	<.5	6.5
400625	1.7	10.2	14.0	65	<.1	6.3	6.3	499	2.93	32.0	2.0	<.5	10.3	88	.2	.4	.3	70	.96	.185	28	7	.57	533	.209	1	.98	.121	.20	.8	.01	4.6	.1	<.05	5	<.5	1.0
400626	.1	11.8	9.2	18	<.1	8.2	3.6	432	1.22	132.3	.4	.9	10.2	180	.1	2.1	.8	9	6.58	.013	21	11	.23	29	.006	4	.65	.012	.14	<.1	<.01	1.6	.2	<.05	2	<.5	6.5
400627	.2	93.3	29.2	23	1.0	21.0	10.5	393	3.37	4201.8	1.1	123.5	14.6	128	.1	8.5	62.6	11	2.76	.049	40	11	.27	108	.005	3	.94	.012	.23	.9	.02	2.2	.2	<.05	3	.9	10.2
400628	.1	42.6	13.9	43	.3	22.3	9.8	574	2.68	605.1	.9	2.9	15.1	136	.4	6.7	3.3	23	5.19	.041	36	24	.52	68	.016	3	1.36	.010	.32	.1	.01	3.8	.4	<.05	6	<.5	9.4
400629	.1	27.2	11.6	36	.2	18.9	8.3	453	2.44	466.9	.8	3.3	14.1	88	.1	5.7	1.6	15	2.49	.031	33	17	.41	62	.012	3	1.18	.014	.26	<.1	.01	2.6	.2	<.05	4	<.5	5.9
400630	.2	20.5	10.7	29	.2	18.8	7.5	406	2.15	839.9	.8	31.1	14.4	30	.1	4.5	2.9	12	.63	.025	32	12	.35	54	.003	6	1.13	.010	.19	.3	.02	2.0	.2	<.05	3	<.5	6.1
400631	.2	38.4	13.7	30	.3	18.4	8.5	404	2.21	689.0	1.0	7.9	16.1	15	.2	12.9	1.7	11	.28	.037	35	13	.38	50	.005	3	1.14	.005	.23	<.1	.01	2.3	.2	<.05	3	.5	7.9
STANDARD DS7	20.8	111.2	71.2	408	.9	56.1	9.6	630	2.39	48.4	5.1	63.4	4.6	72	6.2	5.9	4.7	84	.94	.081	13	168	1.06	373	.125	39	.97	.081	.44	3.9	.20	2.6	4.3	.20	5	3.3	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data P FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.5	1.8	3.6	44	<.1	3.6	5.5	542	1.86	.6	3.3	<.5	4.9	76	<.1	<.1	.1	36	.63	.071	9	12	.58	214	.144	1	1.39	.125	.57	.1	<.01	2.7	.4	<.05	5	<.5	-
400632	.3	118.5	21.7	34	.3	128.7	20.2	527	2.89	698.0	.8	6.6	14.9	18	.3	13.0	6.6	14	.37	.040	32	20	.44	72	.004	6	1.50	.017	.35	<.1	.02	2.5	.3	.27	4	.5	8.0
400633	.2	47.6	12.9	34	.1	35.8	11.5	568	2.09	643.1	.9	5.5	16.2	20	.1	9.6	1.0	11	.34	.079	31	15	.31	111	.008	9	1.30	.010	.53	<.1	.01	2.3	.3	<.05	4	<.5	5.9
RE 400633	.2	48.8	13.3	33	.1	32.7	11.3	573	2.12	655.7	.9	4.2	16.4	19	.2	9.5	1.0	11	.34	.082	31	15	.32	109	.007	9	1.30	.010	.49	.1	<.01	2.1	.3	<.05	4	<.5	-
400634	.2	20.0	10.6	12	<.1	12.6	4.9	240	1.21	488.0	.5	2.8	12.0	12	.1	4.2	.5	3	.19	.039	20	9	.13	80	.002	7	.71	.009	.24	<.1	.01	1.0	.1	<.05	1	<.5	8.5
400635	.2	31.7	15.4	9	<.1	18.3	5.0	96	1.13	502.5	.4	5.0	15.1	10	.1	4.3	1.1	3	.14	.017	24	10	.11	91	.002	12	.69	.011	.31	<.1	<.01	.9	.1	<.05	2	<.5	3.6
400636	.3	18.1	10.0	8	<.1	6.2	2.6	134	1.03	344.0	.3	2.9	12.0	9	.1	3.3	.6	3	.14	.009	20	11	.12	75	.002	9	.61	.014	.28	<.1	<.01	.9	.1	<.05	1	<.5	5.2
400637	.2	21.7	9.0	6	<.1	9.5	3.4	79	1.04	363.7	.4	3.4	11.0	6	.1	4.7	1.1	2	.09	.009	18	12	.08	72	.002	12	.59	.005	.28	<.1	.01	.8	.1	<.05	1	<.5	4.5
400638	.2	50.0	8.1	8	.2	11.3	4.9	150	1.41	687.7	.4	18.0	12.1	15	<.1	4.8	7.7	3	.17	.042	21	10	.10	74	.001	9	.62	.005	.28	<.1	.02	1.2	.1	<.05	1	.5	7.9
400639	.2	63.4	15.2	40	.2	34.2	19.7	777	2.95	1338.4	.9	23.1	14.8	14	.8	8.8	4.8	10	.22	.027	36	12	.20	101	.002	15	1.40	.010	.33	.1	.02	2.8	.2	<.05	3	.6	8.1
400640	.3	54.0	16.0	39	.2	27.6	13.3	696	3.00	798.5	1.2	7.6	15.6	13	.2	10.0	2.1	8	.12	.036	37	9	.10	148	.001	17	1.03	.006	.38	.1	.01	3.0	.3	<.05	2	.5	4.6
400641	.1	25.5	13.6	20	.1	17.8	7.1	716	1.62	456.0	.5	8.2	8.0	143	.1	8.0	1.8	4	4.52	.019	20	8	.06	49	.001	16	.66	.003	.27	.1	.01	2.3	.2	<.05	1	<.5	6.3
400642	.2	23.2	20.9	17	.2	9.4	2.3	52	1.46	555.6	.9	13.2	14.9	24	.2	15.8	2.3	6	.10	.013	34	7	.03	101	.001	13	.55	.004	.31	.1	<.01	1.7	.2	<.05	2	<.5	6.6
400643	.2	8.6	13.3	4	.1	2.9	.9	36	.73	220.2	.3	22.4	6.9	15	<.1	3.8	1.8	3	.05	.006	23	8	.03	105	.001	21	.53	.004	.36	.1	<.01	1.0	.3	<.05	2	.6	5.3
400644	.3	7.2	15.1	4	.2	1.8	.7	25	.75	244.5	.3	27.7	6.8	13	.1	4.9	1.6	4	.02	.006	23	7	.03	103	.001	22	.48	.004	.37	.1	<.01	.8	.2	.06	1	<.5	8.6
400645	.2	12.7	8.8	8	<.1	4.2	1.2	33	1.02	314.7	.5	7.2	8.3	9	.1	10.5	.6	4	.05	.007	18	11	.03	67	.001	14	.46	.004	.26	.1	<.01	1.4	.2	<.05	1	<.5	4.0
400646	.2	13.1	10.4	10	.1	4.8	1.6	40	1.17	421.3	.4	20.2	6.1	5	<.1	13.0	1.1	3	.03	.008	20	7	.03	78	.001	17	.45	.004	.33	.1	<.01	1.2	.2	<.05	1	<.5	5.8
400647	.2	13.7	7.5	6	.1	5.5	1.5	54	.78	308.4	.4	22.1	5.9	7	.1	4.5	1.6	3	.04	.006	23	8	.04	69	.001	28	.55	.004	.29	.1	.01	1.0	.2	<.05	1	.5	4.0
400648	.5	118.5	11.2	32	.2	28.8	16.9	365	3.31	2195.8	1.7	18.2	13.8	19	.3	10.3	6.2	9	.21	.040	31	9	.20	139	.001	12	1.06	.009	.29	.1	.02	3.1	.2	<.05	2	1.6	11.1
400649	.3	106.7	18.1	46	.3	28.6	15.3	424	2.92	2264.3	1.9	41.5	14.3	18	1.0	9.4	10.6	9	.15	.031	36	11	.19	138	.001	13	1.07	.011	.36	.1	.03	2.9	.3	<.05	2	2.0	12.5
400650 (pulp)	6.8	59.4	18.7	101	1.9	15.7	8.6	152	3.11	345.1	.1	890.2	.4	5	.3	30.1	.2	16	.18	.039	7	28	.09	24	.002	2	.31	.004	.20	.5	3.71	1.7	3.9	2.20	2	10.3	-
400651	.6	147.5	17.5	74	.3	70.0	52.5	1458	3.94	2030.8	2.3	25.1	16.8	18	.4	12.8	6.3	11	.20	.042	51	12	.36	148	.001	7	1.56	.009	.31	<.1	.03	2.7	.4	<.05	4	.8	3.3
400652	.3	92.5	9.6	52	.2	47.2	37.3	1104	3.26	1215.3	1.7	22.9	14.9	18	.1	4.8	3.9	15	.11	.035	31	18	.35	166	.004	9	1.50	.017	.40	.1	.01	2.9	.3	<.05	4	.8	7.4
400653	.4	102.2	12.1	38	.2	28.0	11.8	230	3.17	1584.3	2.0	20.6	17.8	17	.1	4.3	6.4	10	.10	.032	47	11	.16	113	.001	8	1.19	.016	.35	.1	.02	3.1	.3	<.05	2	1.2	9.5
400654	.3	135.7	13.8	61	.3	70.8	42.0	833	3.46	1546.8	1.7	12.8	17.8	14	.2	4.2	5.8	14	.07	.034	34	15	.17	125	.002	8	1.30	.029	.33	.1	.03	3.1	.3	<.05	4	1.3	8.2
400655	.4	147.7	13.4	27	.4	14.5	9.9	130	6.00	1847.1	1.3	10.5	16.3	12	.1	4.7	3.7	13	.05	.042	23	14	.17	153	.003	6	.97	.018	.32	.2	.01	2.2	.2	<.05	4	4.2	11.3
400656	.3	196.8	11.5	40	.4	21.2	12.8	145	6.20	2469.0	1.5	10.8	14.0	15	.2	3.9	6.7	9	.07	.046	39	11	.10	115	.001	6	.88	.015	.32	.1	.02	2.2	.2	<.05	2	2.6	7.4
400657	.5	161.9	14.4	56	.4	41.2	12.4	110	5.33	3318.4	1.8	24.1	16.5	22	.1	5.1	15.9	13	.09	.039	32	13	.12	141	.001	7	1.22	.020	.33	1.0	.04	3.2	.3	<.05	3	1.5	7.7
400658	.2	129.1	10.0	63	.2	118.7	67.3	1414	3.31	1296.5	1.3	16.6	13.6	13	.1	3.2	6.4	15	.05	.031	26	16	.25	174	.003	6	1.48	.018	.31	.1	.02	3.1	.4	<.05	4	.6	6.1
400659	.4	75.4	16.4	16	.4	8.0	2.7	64	4.28	9999.5	1.5	146.2	16.1	15	.1	9.7	32.0	15	.06	.049	33	19	.25	131	.002	7	1.20	.015	.35	.1	.02	3.7	.3	.09	4	5.4	6.5
400660	.2	33.5	5.4	9	.1	12.9	4.8	149	1.82	1218.6	.4	17.2	9.1	7	<.1	2.6	5.1	6	.02	.019	22	11	.05	77	.001	7	.55	.028	.26	.1	.02	1.5	.2	<.05	1	1.1	6.1
400661	.5	78.3	93.5	20	3.2	9.8	6.5	68	5.39	>10000	1.0	2010.1	12.4	10	.2	62.2	415.9	11	.05	.039	22	14	.13	106	.002	5	.87	.019	.31	.2	.06	2.5	.2	1.00	3	13.7	7.2
400662	1.6	189.6	480.3	23	18.8	8.8	47.0	33	25.86	>10000	.6	14925.6	5.8	5	1.2	694.1	>2000	6	.01	.026	7	8	.04	13	.004	2	.49	.008	.19	.7	.27	1.2	.2	7.62	2	94.6	2.6
400663	.5	63.1	16.5	21	.3	11.8	2.8	120	3.43	2725.0	1.6	24.6	14.2	14	.1	6.1	9.3	14	.08	.048	31	16	.25	141	.004	4	1.24	.015	.32	.1	.01	2.6	.3	<.05	4	1.9	6.1
400664	.4	64.1	18.6	18	.6	11.0	3.2	81	2.76	3979.7	.9	145.1	11.8	11	<.1	8.2	39.6	10	.04	.034	21	14	.17	114	.003	5	.90	.023	.33	<.1	.01	1.9	.3	.11	3	2.5	7.2
STANDARD DS7	20.7	108.4	70.2	414	.9	55.2	9.8	628	2.38	48.8	5.0	72.3	4.6	71	6.4	6.0	4.7	84	.94	.079	13	176	1.05	369	.125	39	.98	.077	.44	3.9	.20	2.6	4.2	.19	5	3.4	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.4	3.3	3.6	48	<.1	3.8	4.1	529	1.86	1.4	2.9	<.5	4.0	58	.1	<.1	.1	35	.50	.078	7	12	.57	208	.119	1	.93	.066	.51	.7	<.01	2.5	.4	<.05	5	<.5	-
400665	.5	101.0	9.4	41	.2	25.9	24.9	398	3.38	1391.2	1.4	32.9	14.1	11	.1	3.6	6.3	14	.07	.042	16	17	.41	97	.004	3	1.37	.010	.27	.4	<.01	2.3	.2	<.05	4	2.5	7.5
400666	.2	106.3	10.4	42	.2	19.1	6.2	205	3.86	2351.7	1.4	40.1	16.6	12	.1	4.9	9.8	16	.09	.057	31	19	.48	97	.004	2	1.63	.010	.28	.1	.01	2.8	.3	<.05	5	2.8	7.0
400667	.5	69.3	8.8	23	.2	18.5	4.0	124	2.43	998.0	1.1	15.5	14.1	8	.1	4.1	4.9	10	.04	.025	17	13	.24	59	.003	2	1.01	.013	.17	.6	.01	1.9	.1	<.05	2	1.2	5.8
400668	.3	45.0	13.5	20	.2	7.9	3.4	113	2.10	2058.6	.7	21.8	12.7	7	.1	4.1	10.0	6	.02	.022	24	9	.11	58	.002	3	.58	.017	.22	<.1	.01	1.3	.1	.06	1	1.5	7.1
400669	1.0	37.7	11.5	13	.3	7.1	2.9	55	2.00	2785.8	.6	82.3	10.6	7	.1	7.6	13.2	6	.02	.019	17	13	.09	59	.001	3	.51	.010	.16	2.5	.01	1.2	.1	<.05	1	1.8	5.1
400670	.5	98.8	189.5	8	5.8	2.8	2.1	31	7.75	>10000	.3	3468.0	4.2	2	.2	247.6	506.1	4	<.01	.026	7	8	.03	68	.002	3	.27	.006	.17	1.7	.11	1.0	.2	.57	1	21.9	.7
400671	.2	86.6	32.3	19	1.0	6.7	7.0	42	3.71	>10000	.7	736.0	14.6	12	.4	40.3	105.1	5	.02	.023	21	8	.08	113	.001	2	.50	.007	.19	1.0	.02	1.1	.3	.50	1	6.6	3.6
400672	1.6	176.2	59.8	10	2.9	9.8	15.4	28	12.03	>10000	1.0	2758.1	10.2	6	.2	182.1	427.4	6	.01	.035	9	12	.04	52	.002	3	.38	.005	.18	4.1	.06	2.7	.2	2.63	1	56.9	5.9
RE 400672	1.3	176.3	57.6	10	2.7	10.2	14.9	28	11.86	>10000	1.0	2613.7	9.7	6	.2	172.5	411.6	5	.01	.035	8	11	.04	48	.002	3	.37	.004	.16	3.6	.06	2.6	.2	2.65	1	54.1	-
400673	.6	42.1	4.8	53	<.1	17.4	4.6	85	2.47	783.0	2.0	15.3	16.6	8	.1	2.3	3.2	7	.02	.029	53	9	.11	52	.002	3	.61	.012	.20	.5	.01	1.2	.1	<.05	1	.8	3.2
400674	.4	52.7	6.4	51	.1	15.2	6.4	101	3.28	1032.2	2.3	9.3	17.0	11	<.1	2.5	1.8	6	.03	.051	53	9	.10	56	.001	5	.66	.013	.24	<.1	.02	1.7	.1	<.05	1	1.4	7.1
400675	1.4	11.2	16.8	62	<.1	4.3	5.7	453	2.87	302.2	1.9	5.5	10.1	86	.2	.7	1.4	64	.93	.172	25	9	.54	535	.190	1	.96	.119	.20	1.3	<.01	4.4	.1	<.05	5	<.5	1.5
400676	.4	42.9	4.9	54	<.1	13.3	4.5	103	3.49	471.6	1.7	3.7	14.9	9	<.1	1.5	1.0	7	.02	.051	40	12	.14	55	.001	4	.67	.012	.23	.8	.01	1.8	.2	<.05	2	.7	4.8
400677	.2	24.6	5.8	34	<.1	13.4	6.6	171	2.64	458.7	1.0	5.1	9.3	7	.1	2.6	1.1	12	.03	.022	14	20	.52	77	.010	2	1.30	.008	.39	.1	.01	1.7	.5	<.05	4	.9	7.3
400678	.8	22.3	6.3	28	<.1	13.1	5.3	142	1.71	401.5	.9	2.9	9.6	10	.1	2.1	1.0	8	.07	.024	17	18	.23	86	.005	4	.81	.011	.30	2.0	<.01	1.2	.2	<.05	2	<.5	5.8
400679	.4	35.0	6.2	23	<.1	12.6	6.7	225	1.79	501.1	1.1	2.6	8.9	14	.1	3.5	1.1	6	.06	.019	17	11	.12	80	.004	5	.66	.007	.22	.7	.01	1.1	.2	<.05	2	.8	8.4
400680	.2	27.3	8.8	16	.1	7.7	2.9	89	1.69	882.1	.7	6.8	9.0	8	.1	2.5	3.9	5	.03	.011	17	11	.07	71	.001	6	.53	.006	.25	<.1	.02	1.1	.2	<.05	1	.6	8.5
400681	.9	15.5	6.5	20	<.1	10.2	5.7	138	1.52	263.5	.7	<.5	9.6	9	.1	2.1	.5	5	.05	.011	18	14	.08	75	.001	5	.52	.008	.21	2.2	.01	1.0	.1	<.05	1	<.5	6.4
400682	.3	44.7	8.5	16	.2	11.1	3.6	79	1.64	3415.7	.6	58.8	8.9	13	.1	8.0	9.5	4	.03	.011	17	12	.05	59	.001	3	.45	.004	.16	1.0	.01	1.0	.1	<.05	1	2.2	5.8
400683	.2	26.1	5.5	15	<.1	8.6	4.5	104	1.82	1078.6	.7	10.0	9.1	6	.1	2.6	1.0	6	.02	.017	13	10	.06	53	.001	4	.48	.008	.16	.1	.01	1.1	.1	<.05	1	1.0	6.9
400684	.9	30.0	4.9	13	<.1	6.4	2.7	58	1.67	481.6	.9	2.2	6.9	7	.1	2.0	.6	7	.01	.022	10	15	.04	48	.001	4	.47	.007	.17	2.3	.03	1.3	.2	<.05	1	1.7	3.0
400685	.3	77.2	4.9	113	.2	31.9	18.3	197	5.17	197.1	1.9	<.5	25.9	6	.1	1.8	.9	5	.01	.107	46	9	.02	75	.001	6	.44	.007	.25	.1	.09	1.4	.2	<.05	1	.5	1.7
400686	.2	22.5	4.9	25	<.1	13.2	5.1	131	1.64	463.4	.8	1.7	10.0	6	<.1	2.5	1.0	7	.02	.016	16	14	.13	61	.003	4	.69	.008	.17	<.1	.02	1.3	.2	<.05	2	.6	6.3
400687	.6	16.2	4.8	35	<.1	17.9	7.1	178	1.87	189.7	.8	<.5	9.4	6	.3	2.0	.2	7	.04	.021	20	18	.25	71	.003	3	.87	.011	.19	1.4	.01	1.1	.2	<.05	2	<.5	6.9
400688	.3	22.3	5.2	30	<.1	16.2	12.6	259	1.64	288.5	.8	<.5	9.0	7	1.2	2.3	1.0	5	.01	.013	21	13	.11	60	.001	3	.64	.006	.16	.7	.01	1.1	.2	<.05	1	.5	5.9
400689	.2	21.5	4.5	19	<.1	29.9	5.5	511	1.24	233.5	.6	.8	6.5	6	.1	1.6	.6	4	.03	.012	13	13	.10	45	.003	3	.38	.013	.12	.1	<.01	.8	.1	<.05	1	.7	5.1
400690	.8	12.1	3.1	8	<.1	5.5	3.1	110	.73	191.4	.3	2.0	3.5	6	.2	1.7	.6	2	.01	.005	13	16	.02	31	.001	5	.22	.004	.10	2.6	.01	.5	.1	<.05	<1	<.5	3.0
400691	.4	11.5	1.6	6	<.1	5.6	1.7	52	.65	148.7	.3	.9	2.5	2	.1	1.3	.2	2	<.01	.004	5	15	.03	16	.001	2	.17	.002	.06	1.0	.01	.4	.1	<.05	1	<.5	9.3
400692	.2	24.7	3.6	25	<.1	5.6	2.0	49	1.18	872.2	.5	2.2	6.5	7	.1	4.1	.4	4	.01	.009	13	10	.10	48	.001	3	.37	.004	.14	<.1	.01	.6	.1	<.05	1	.7	7.3
400693	.9	24.6	3.5	13	<.1	12.1	4.4	80	1.35	168.0	.6	2.2	6.6	6	.2	1.5	.5	3	.01	.013	26	12	.02	50	.001	6	.33	.006	.21	1.9	.03	.7	.2	<.05	1	.5	2.1
400694	.5	53.3	4.4	45	.1	35.3	16.6	349	3.02	442.0	1.6	4.2	14.8	10	.2	2.6	1.8	7	.02	.033	44	12	.17	79	.004	5	.91	.007	.37	.5	.03	1.5	.4	<.05	2	<.5	5.2
400695	.1	45.1	3.1	69	<.1	32.0	12.2	174	3.70	201.9	1.7	2.1	17.5	10	.2	2.1	.3	11	.04	.047	43	17	.59	78	.009	3	1.63	.012	.45	<.1	.01	1.5	.4	<.05	4	<.5	6.8
400696	.6	24.4	4.9	58	<.1	25.8	9.0	358	3.21	155.3	1.5	2.7	14.3	7	.1	1.8	.5	11	.05	.039	35	24	.75	47	.008	3	1.74	.010	.30	1.3	<.01	1.7	.3	<.05	5	.7	8.9
400697	.5	26.9	6.7	95	<.1	27.8	13.4	543	4.68	200.2	2.0	1.9	18.6	12	.2	3.2	.4	13	.10	.072	53	27	1.00	48	.005	2	2.35	.018	.18	.3	.01	2.2	.1	<.05	6	<.5	4.3
STANDARD DS7	20.2	107.0	69.9	405	.9	48.3	9.3	618	2.36	48.0	5.0	62.1	4.5	71	6.3	6.0	4.6	84	.92	.081	12	165	1.04	367	.121	38	.97	.082	.44	3.8	.20	2.5	4.2	.19	5	3.4	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.5	3.6	4.0	44	<.1	4.3	4.3	518	1.90	.7	3.1	<.5	4.3	63	<.1	<.1	<.1	36	.52	.081	8	14	.57	193	.128	1	.94	.077	.50	1.1	.01	2.2	.3	<.05	5	<.5	-
400698	.4	25.4	5.6	64	<.1	24.2	9.4	368	3.61	500.6	1.4	1.8	14.1	8	.1	1.6	.4	16	.07	.036	28	27	.84	51	.009	2	1.93	.010	.31	.3	.01	1.7	.3	<.05	5	<.5	4.3
400699	.1	23.3	5.5	15	<.1	4.4	1.9	75	1.59	1093.2	.5	7.6	9.8	6	.1	2.1	2.6	10	.04	.020	13	17	.28	49	.004	2	.72	.009	.19	<.1	.01	1.0	.2	<.05	2	1.0	5.2
400700 (pulp)	8.0	51.7	3.6	37	7.7	240.9	11.1	161	3.06	444.0	.1	8324.3	.4	5	<.1	50.2	<.1	15	.11	.034	6	269	.06	27	.002	1	.27	.005	.19	.8	6.96	1.3	8.3	1.89	1	20.7	-
400701	.3	24.1	150.3	10	.9	1.7	.3	16	1.07	4164.8	.4	24.1	5.4	16	.4	32.4	46.4	2	<.01	.007	10	9	.02	56	.001	4	.18	.003	.14	.7	.07	.4	.1	<.05	1	1.9	5.0
400702	.2	22.4	5.1	20	<.1	12.5	7.0	97	2.16	5209.3	.8	6.8	15.1	15	.1	4.8	1.0	12	.04	.030	19	21	.50	85	.004	3	1.04	.014	.27	<.1	.01	1.5	.4	.09	3	1.9	2.8
400703	.5	12.0	2.6	5	<.1	3.2	.9	35	.75	310.1	.3	1.9	2.5	3	<.1	1.5	.6	3	.01	.007	5	17	.06	25	.002	2	.20	.006	.08	1.4	<.01	.4	.1	<.05	1	<.5	3.1
RE 400703	.4	10.7	2.2	5	<.1	3.5	.9	34	.77	294.6	.3	2.6	2.4	3	.1	1.4	.6	2	.01	.007	5	15	.06	23	.001	1	.20	.006	.07	1.2	.01	.4	.1	<.05	1	<.5	-
400704	.1	15.7	10.2	11	.2	4.2	1.4	27	1.08	4403.1	.4	31.4	6.7	8	.5	9.2	7.1	3	.01	.009	16	10	.04	92	.001	5	.26	.004	.19	<.1	.01	.7	.1	<.05	1	1.5	7.0
400705	.3	20.0	5.2	15	<.1	8.8	2.9	58	1.66	1035.1	1.2	7.8	11.6	10	.1	3.4	1.3	6	.07	.036	23	11	.10	91	.004	4	.65	.006	.28	.6	.01	1.1	.2	<.05	2	.8	6.0
400706	.2	30.5	14.6	16	.2	7.7	2.9	37	1.32	2865.5	.6	29.2	7.8	19	.6	8.3	14.2	3	.02	.014	16	10	.05	126	.002	6	.35	.006	.22	<.1	.01	.8	.2	<.05	1	1.2	6.6
400707	.4	24.9	8.5	14	.2	5.2	2.1	27	.85	1919.7	.5	17.4	5.1	23	.3	8.6	5.5	4	.01	.008	13	13	.05	69	.002	3	.27	.004	.18	.8	.01	.6	.2	<.05	1	.9	4.9
400708	.1	23.3	6.4	12	.2	7.1	3.1	47	1.19	1718.0	.9	30.2	8.7	12	.1	4.3	5.7	4	.01	.009	20	8	.04	79	.001	4	.38	.005	.18	<.1	.02	.8	.1	<.05	1	.8	2.6
400709	.3	21.9	10.1	12	.2	5.5	2.0	52	1.27	4814.8	.5	61.2	8.6	7	.2	8.2	8.3	5	.01	.011	16	13	.06	68	.003	4	.36	.009	.17	.9	<.01	.8	.1	<.05	1	1.5	5.5
400710	.2	43.3	197.5	9	14.2	1.2	.8	30	9.59	>10000	.5	5440.8	1.6	3	.8	282.1	1057.5	3	.01	.032	17	7	.01	47	.003	1	.11	.002	.04	.3	.19	.6	.1	<.05	1	66.0	2.4
400711	.4	19.7	3.8	19	<.1	11.4	4.3	93	1.57	907.9	.9	9.6	10.3	7	.1	1.8	2.6	10	.02	.015	21	13	.22	105	.014	3	.82	.010	.44	.6	.02	1.2	.4	<.05	2	.5	4.6
400712	.2	24.2	4.8	10	.2	8.4	6.0	83	1.17	1260.4	.8	41.6	6.8	11	<.1	2.7	8.5	4	.01	.011	16	9	.07	80	.003	3	.41	.009	.20	<.1	.01	.6	.2	<.05	1	.8	5.3
400713	.4	42.8	39.3	12	1.7	4.9	2.6	50	3.25	>10000	.7	336.7	8.7	29	.4	49.0	173.7	5	.01	.014	17	10	.09	128	.005	4	.48	.007	.27	1.0	.02	.9	.2	.67	1	17.2	8.2
400714	.2	95.5	51.4	10	2.1	4.2	8.2	47	6.77	>10000	.7	1258.5	7.0	45	.7	99.5	354.7	4	.01	.012	12	7	.05	61	.004	3	.43	.005	.21	>100	.09	.7	.3	2.09	1	38.8	3.1
400715	.3	33.2	5.2	24	<.1	8.7	2.5	97	1.97	1156.8	.7	10.0	10.1	17	.1	2.4	3.0	18	.03	.017	19	24	.41	78	.040	2	1.24	.012	.47	.6	<.01	1.9	.5	<.05	4	.9	2.6
400716	.2	110.0	172.0	21	6.1	4.8	2.3	51	10.30	>10000	.6	1878.0	7.0	15	.7	201.8	931.3	7	<.01	.014	10	10	.14	50	.011	4	.58	.005	.22	.6	.10	1.0	.2	1.98	2	55.4	4.3
400717	.5	32.6	26.4	19	.7	9.1	4.5	102	1.93	6683.5	.6	72.5	7.3	14	.2	24.8	46.2	9	.01	.011	14	21	.20	78	.011	2	.60	.012	.22	1.3	.01	1.2	.3	<.05	2	2.8	3.9
400718	.2	54.4	33.4	33	.5	6.4	2.3	50	2.90	7874.7	.7	68.7	8.5	37	.8	26.1	34.2	6	.01	.014	22	9	.08	137	.004	8	.52	.006	.28	.5	.01	1.0	.3	.07	2	3.3	4.0
400719	.4	36.0	106.8	22	.7	3.1	1.3	28	2.17	>10000	.6	60.0	8.0	29	.9	30.5	21.3	5	.01	.013	19	8	.05	87	.005	4	.34	.004	.26	.6	.03	.9	.2	<.05	1	3.9	3.3
400723	.1	35.5	52.5	16	.9	5.4	2.5	31	2.21	>10000	.4	182.1	5.6	17	.3	38.8	43.1	4	.01	.013	16	8	.04	80	.002	6	.36	.004	.24	.1	.02	.8	.2	<.05	1	5.9	4.3
400724	.4	51.1	102.4	12	4.2	5.5	2.6	43	3.72	>10000	.9	1352.9	9.0	28	.3	83.7	312.9	4	.01	.015	18	10	.05	71	.002	4	.45	.006	.19	.7	.09	1.0	.3	.16	1	24.2	3.2
400725	.9	12.5	19.3	70	<.1	4.7	6.2	473	3.01	238.9	2.1	6.4	10.8	86	.2	1.3	2.0	70	.97	.192	26	8	.59	426	.205	1	.99	.124	.19	.6	.01	4.5	.1	<.05	5	<.5	1.6
400726	.3	34.1	11.7	18	.2	9.0	3.3	68	1.64	2938.2	1.0	42.4	9.5	25	.1	11.0	13.8	10	.02	.019	18	16	.19	72	.005	4	.84	.011	.24	.5	.01	1.5	.3	<.05	3	2.1	6.3
400727	.2	28.3	6.7	21	<.1	9.5	3.0	85	1.63	863.0	1.2	8.8	9.6	14	.1	4.1	4.9	8	.03	.017	17	11	.20	75	.005	3	.90	.009	.30	<.1	.01	1.2	.3	<.05	2	1.0	6.2
400728	.5	44.4	7.7	37	<.1	22.6	9.3	128	2.09	1237.5	1.8	2.9	13.1	11	.3	2.7	2.0	5	.03	.022	23	11	.09	69	.002	4	.59	.008	.27	.5	.01	1.2	.2	<.05	1	.6	5.4
400729	.2	38.1	6.6	23	<.1	11.1	4.1	100	2.52	3051.0	1.5	4.7	8.9	9	.2	5.3	1.8	4	.03	.023	21	9	.03	46	.001	6	.37	.010	.17	<.1	<.01	1.2	.2	<.05	1	.9	4.3
400730	.4	17.3	5.3	11	<.1	4.2	2.0	62	1.19	564.6	.5	18.1	8.5	5	.1	3.1	3.7	5	.01	.011	17	12	.03	39	.002	6	.35	.009	.15	.5	.01	.9	.2	<.05	1	<.5	5.3
400731	.1	23.2	6.2	9	<.1	3.2	1.5	36	1.51	1312.9	.5	10.5	7.2	5	.1	6.0	4.9	5	.01	.009	19	9	.03	42	.001	5	.33	.008	.18	<.1	<.01	.8	.2	<.05	1	.6	6.1
400732	.6	30.5	12.1	12	<.1	6.8	2.5	51	1.73	661.5	.7	2.9	7.8	5	.2	5.9	1.5	3	.01	.012	18	12	.03	54	.001	6	.38	.006	.18	.9	<.01	.8	.1	<.05	1	<.5	7.7
400733	.2	21.4	4.6	16	<.1	6.4	2.5	79	1.42	255.3	.6	3.1	7.3	4	.1	2.8	.9	6	.01	.013	13	11	.13	54	.003	3	.67	.008	.16	<.1	<.01	.9	.1	<.05	2	<.5	6.6
STANDARD DS7	20.6	109.3	70.4	407	.9	54.6	9.4	622	2.38	48.5	5.1	62.3	4.6	75	6.3	5.9	4.6	83	.93	.083	12	169	1.06	368	.121	40	.97	.076	.44	3.8	.20	2.5	4.2	.20	4	3.6	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data C FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.3	2.8	3.3	39	<.1	3.8	4.0	508	1.72	.8	2.8	2.3	3.7	48	<.1	.1	.1	34	.47	.073	7	10	.56	177	.106	1	.88	.063	.46	.6	<.01	1.8	.3	<.05	5	<.5	-
400734	.2	35.2	4.7	49	<.1	39.8	18.8	316	2.36	205.6	.9	4.9	8.5	5	.1	1.1	1.4	8	.01	.018	23	13	.16	61	.002	5	.72	.014	.25	<.1	.01	1.2	.1	<.05	2	<.5	6.5
RE 400734	.3	36.9	4.9	50	<.1	42.6	19.3	318	2.37	209.5	.9	3.2	8.4	5	.1	1.2	1.3	8	.01	.018	22	12	.17	63	.003	5	.73	.014	.26	<.1	.01	1.2	.2	<.05	2	<.5	-
400735	.6	41.8	6.3	34	<.1	23.4	8.2	141	2.34	275.1	1.0	1.9	8.6	5	.1	2.8	.8	8	.01	.016	21	19	.23	69	.003	6	.87	.013	.25	1.6	.01	1.2	.2	<.05	2	<.5	8.1
400736	.4	50.0	5.4	21	.1	12.9	4.9	52	2.02	758.9	1.3	6.0	7.1	12	.2	4.0	.8	8	.02	.021	25	14	.11	68	.002	7	.68	.011	.23	.7	.02	1.5	.2	<.05	2	.9	6.3
400737	.3	65.5	7.2	42	.1	17.2	7.2	125	3.22	3620.0	1.3	15.9	9.6	16	.1	5.1	1.0	6	.02	.029	34	9	.09	166	.001	5	.62	.015	.26	.1	.01	1.3	.2	<.05	1	1.1	4.3
400738	.7	37.6	11.2	61	<.1	12.8	6.1	219	3.15	181.9	1.8	1.2	12.9	8	.1	1.8	.5	9	.05	.045	28	16	.41	91	.004	3	1.10	.008	.28	1.3	.01	1.4	.1	<.05	3	<.5	6.4
400739	.6	46.6	13.8	64	.3	25.8	10.3	197	3.29	225.8	2.0	2.4	14.0	7	.2	1.3	1.2	8	.02	.039	46	14	.33	87	.002	5	1.09	.011	.29	.5	.01	1.6	.1	<.05	3	.6	4.3
400740	.2	25.6	8.5	32	<.1	11.8	6.0	97	1.96	245.5	1.2	2.1	9.1	5	.1	1.5	.6	4	.01	.020	31	8	.11	61	.001	4	.54	.008	.23	<.1	.01	.8	.1	<.05	1	<.5	6.1
400741	.9	26.6	8.7	32	<.1	15.1	6.5	116	2.00	169.7	1.5	2.7	11.1	10	.1	1.7	.9	7	.05	.038	36	17	.23	88	.002	4	.84	.012	.29	2.1	.01	1.1	.1	<.05	2	<.5	6.4
400742	.6	29.0	8.3	58	<.1	19.9	9.5	265	3.26	153.5	1.4	3.4	12.4	6	<.1	2.3	1.4	13	.02	.023	29	22	.67	81	.006	2	1.67	.010	.29	.6	<.01	1.6	.2	<.05	5	<.5	6.0
400743	.2	36.3	5.3	12	<.1	7.5	3.2	76	1.42	418.2	.6	4.5	8.0	5	.1	3.9	.8	3	.02	.012	18	10	.04	36	.001	6	.34	.006	.14	.1	.01	.8	.1	<.05	1	<.5	4.0
400744	.8	27.0	4.9	18	<.1	14.4	3.4	70	1.53	308.0	.7	4.5	8.0	7	.1	5.0	.6	5	.02	.014	21	14	.06	53	.001	7	.51	.009	.20	2.1	.01	.9	.1	<.05	1	<.5	8.0
400745	.4	63.7	8.1	30	<.1	15.9	7.7	146	3.25	4961.0	1.1	3.9	10.0	7	.1	10.8	1.0	7	.02	.022	28	11	.07	44	.001	6	.55	.008	.20	.6	.02	1.7	.2	<.05	1	1.8	3.7
400746	.2	57.4	6.8	29	.1	18.7	5.8	138	3.42	1051.8	1.1	4.3	11.1	10	<.1	6.6	.7	7	.03	.023	28	10	.07	51	.001	6	.62	.012	.21	<.1	.01	1.6	.2	.06	2	1.4	6.2
400747	.7	42.3	4.7	32	<.1	23.0	9.0	181	2.48	599.9	.9	2.2	8.9	11	.1	3.7	.3	5	.02	.024	27	12	.09	37	.001	6	.53	.007	.17	1.8	.01	1.3	.2	<.05	1	<.5	4.5
400748	.5	41.6	5.2	40	<.1	16.9	6.6	145	2.94	543.8	1.1	2.5	10.3	9	<.1	4.1	.5	6	.02	.028	29	13	.05	41	.001	7	.43	.010	.21	.8	.01	1.6	.2	<.05	1	.9	4.2
400749	.3	30.0	5.7	45	<.1	28.0	9.0	305	2.94	355.8	1.2	2.9	10.4	8	<.1	1.8	.4	5	.02	.022	34	8	.05	37	<.001	4	.35	.011	.17	.1	.02	1.2	.1	<.05	1	<.5	4.1
400750 (pulp)	6.5	58.6	18.5	100	1.8	14.0	7.9	147	3.09	328.6	.1	938.1	.4	5	.3	30.7	.2	17	.17	.042	8	29	.09	22	.002	2	.33	.005	.21	.6	3.69	1.4	3.9	2.20	2	8.9	-
400751	.5	47.2	3.0	88	<.1	47.1	15.8	419	4.23	127.4	2.1	4.8	14.8	18	.1	.8	.3	7	.01	.020	63	8	.03	40	<.001	6	.38	.018	.19	.7	.03	1.7	.1	<.05	1	<.5	4.3
400752	.5	41.6	4.8	36	<.1	24.5	9.5	191	2.48	496.6	1.0	14.7	10.8	8	.1	2.6	.7	6	.03	.023	32	11	.15	44	.001	5	.63	.009	.19	.6	.02	.9	.1	<.05	1	<.5	5.5
400753	.3	24.7	9.9	55	<.1	23.2	11.1	341	2.50	209.7	1.2	1.7	9.5	6	.1	1.8	.9	6	.02	.026	33	9	.06	29	<.001	4	.36	.008	.14	.1	.02	1.3	.1	<.05	1	<.5	5.2
400754	.8	32.5	5.4	44	<.1	13.4	9.3	235	2.57	186.7	1.4	1.0	10.1	6	.1	1.8	.3	7	.02	.024	33	12	.04	32	.001	6	.42	.009	.18	1.8	.02	1.4	.1	<.05	1	<.5	6.9
400755	.5	37.8	5.4	56	<.1	22.1	10.8	241	2.87	170.2	1.5	3.0	11.0	6	<.1	2.0	.5	6	.02	.032	39	10	.05	33	.001	5	.48	.018	.16	.6	.02	1.3	.1	<.05	1	<.5	4.8
400756	.4	44.4	5.9	30	<.1	15.1	9.7	164	2.88	457.2	1.6	3.1	10.6	9	<.1	4.0	.4	6	.03	.029	36	6	.08	33	.001	5	.55	.011	.16	<.1	.02	1.5	.1	<.05	1	<.5	6.4
400757	.5	59.1	10.6	35	.1	19.4	9.3	121	2.91	511.4	1.0	14.8	8.6	8	.1	4.2	4.4	6	.05	.020	19	12	.13	33	.001	6	.71	.005	.20	1.5	.01	1.8	.2	<.05	1	.5	5.5
400758	.5	51.1	8.3	27	.2	18.6	7.0	107	2.35	457.9	1.2	20.9	11.8	4	.2	10.1	1.5	4	.02	.015	30	8	.05	39	.001	8	.44	.004	.21	.7	.01	1.4	.2	<.05	1	<.5	7.0
400759	.3	32.9	8.9	20	.1	9.5	3.8	44	1.70	323.2	.8	12.0	8.5	4	<.1	7.7	1.6	3	.02	.016	22	8	.04	41	.001	8	.32	.004	.19	.1	.01	1.4	.1	<.05	1	<.5	5.9
400760	.8	32.9	7.3	23	.2	9.4	7.7	126	2.09	379.0	.7	13.7	12.3	3	<.1	9.1	1.7	3	.02	.020	25	11	.03	40	.001	10	.31	.003	.17	2.3	.01	1.1	.1	<.05	1	<.5	4.8
400761	.5	49.7	6.2	30	.2	14.8	6.1	64	2.29	716.8	1.0	18.1	14.2	6	.1	11.4	1.2	4	.03	.025	42	8	.05	53	.001	7	.41	.005	.23	.7	.01	1.4	.1	<.05	1	<.5	9.8
400762	.4	66.9	11.2	18	.3	10.9	4.0	74	2.70	1129.6	1.4	13.0	12.1	8	.1	5.8	2.4	4	.06	.049	32	8	.09	55	.001	8	.57	.005	.21	.1	.02	2.1	.2	<.05	1	.6	4.0
400763	.9	72.9	15.0	23	.3	13.1	5.5	133	3.09	1014.1	1.4	19.2	13.8	18	.2	6.1	3.5	5	.12	.071	34	11	.16	60	.001	6	.74	.006	.23	1.9	.02	1.9	.2	<.05	1	<.5	9.0
400764	.5	106.0	17.7	30	.3	25.9	8.7	191	2.92	1761.6	1.2	23.6	11.4	12	.2	5.1	13.3	5	.11	.032	21	10	.12	46	.001	6	.75	.006	.19	.6	.02	1.5	.2	<.05	1	.9	4.4
400765	.3	59.8	11.0	38	.1	26.6	11.7	346	2.65	673.6	1.2	6.4	14.6	12	.1	6.7	3.4	5	.07	.022	25	9	.12	50	.001	6	.73	.008	.23	<.1	.02	1.5	.2	<.05	1	<.5	4.0
400766	.8	97.9	11.5	33	.2	31.4	14.3	593	2.53	1531.1	1.5	36.5	12.8	16	.2	7.0	7.2	4	.10	.030	29	11	.12	54	.001	5	.56	.006	.20	2.0	.02	1.6	.2	<.05	1	<.5	8.8
STANDARD DS7	21.2	108.6	71.5	410	.9	55.3	9.7	635	2.41	49.4	5.2	70.1	4.4	71	6.4	6.1	4.6	85	.95	.080	15	182	1.06	377	.127	39	1.00	.086	.45	4.0	.20	2.5	4.3	.19	6	4.0	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data f FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	2.0	3.2	43	<.1	3.3	4.1	517	1.82	9.4	3.2	<.5	4.4	70	<.1	<.1	.1	36	.55	.085	7	9	.57	191	.127	2	1.00	.072	.54	.1	<.01	2.3	.4	<.05	5	<.5	-
400767	.3	49.8	11.3	27	.1	29.6	9.3	494	2.56	701.4	.9	13.1	14.5	17	.1	5.6	4.7	5	.10	.017	22	9	.16	88	.001	12	.90	.013	.27	.1	.01	1.8	.2	<.05	1	.5	5.5
400768	.3	63.5	13.1	33	.2	23.3	12.7	429	2.51	1429.0	1.5	25.1	12.7	14	.1	7.3	7.0	5	.08	.026	29	8	.05	76	.001	17	.57	.005	.34	.1	.01	2.3	.2	<.05	1	<.5	8.2
400769	.4	65.1	13.2	30	.2	20.6	8.1	504	2.44	1482.5	1.5	31.5	14.2	17	.1	10.1	11.1	5	.11	.022	26	7	.05	74	.001	13	.56	.007	.28	.2	.01	2.1	.2	<.05	1	<.5	6.9
RE 400769	.3	70.0	13.7	31	.2	20.9	8.9	505	2.46	1504.5	1.5	44.3	14.2	18	.2	10.2	11.5	5	.11	.021	27	7	.05	75	.001	13	.55	.008	.29	.2	.01	2.2	.2	<.05	1	<.5	-
400770	.3	72.5	10.9	37	.2	25.7	10.7	483	2.57	1262.7	1.5	21.1	14.6	14	.2	12.1	5.5	5	.12	.033	36	6	.04	86	.001	13	.54	.007	.27	.1	.01	2.5	.2	<.05	1	.6	9.5
400771	.4	104.8	8.3	34	.2	27.2	12.8	473	3.06	2387.9	1.9	35.5	15.2	20	.2	13.2	6.5	6	.17	.052	40	7	.04	90	.001	15	.58	.006	.34	.2	.02	3.2	.3	<.05	1	<.5	8.1
400772	.3	124.8	9.0	31	.2	32.2	14.8	368	3.47	2450.5	1.6	36.9	15.8	17	.1	13.7	12.4	6	.13	.040	44	7	.06	90	.001	11	.66	.006	.33	.1	.01	2.7	.2	<.05	1	.9	9.7
400773	.3	94.3	8.8	29	.2	28.2	13.9	300	3.17	1734.3	1.5	31.8	15.2	15	.1	12.1	6.4	7	.12	.039	39	7	.06	90	.001	14	.66	.009	.33	.1	.02	2.6	.2	<.05	1	1.1	7.8
400774	.3	111.0	8.2	36	.2	35.2	15.5	414	3.49	1767.2	1.5	42.3	17.1	20	.1	8.0	5.6	11	.23	.057	44	10	.19	103	.001	11	1.11	.011	.37	.1	.02	3.1	.2	<.05	2	.9	8.9
400775	1.2	15.9	18.2	68	<.1	5.6	7.2	523	3.06	114.5	2.0	1.8	10.4	89	.2	1.3	.6	69	.98	.188	28	8	.60	510	.201	2	1.06	.123	.21	.8	<.01	4.8	.1	<.05	5	<.5	1.0
400776	.3	64.3	8.1	26	.1	28.0	11.5	472	2.68	1244.3	1.0	14.1	12.6	17	.1	5.8	4.2	7	.20	.043	34	8	.11	107	.001	10	.83	.013	.33	1.2	.01	2.1	.2	<.05	2	.8	6.6
400777	.3	87.6	8.4	27	.2	31.1	14.0	450	3.15	2497.0	1.2	35.4	14.4	23	.1	5.8	5.4	9	.19	.040	37	9	.20	88	.001	7	.92	.012	.26	.7	.01	2.5	.2	<.05	2	.8	9.4
400778	.3	94.8	10.2	29	.2	32.9	14.0	581	3.52	3100.9	1.4	55.3	15.7	24	.1	6.5	8.2	8	.16	.039	38	8	.12	97	.001	9	.82	.010	.28	.1	.02	2.6	.2	<.05	1	.6	9.5
400779	.3	94.9	9.4	29	.2	36.8	15.8	645	3.27	2162.1	1.5	46.2	13.6	17	.1	10.0	6.9	6	.16	.043	40	7	.10	87	.001	9	.67	.009	.26	.1	.02	2.4	.2	<.05	1	.6	9.3
400780	.3	88.4	8.6	29	.2	35.2	14.8	475	3.12	1447.2	1.4	28.3	13.4	14	.1	7.0	6.7	8	.13	.037	36	7	.08	100	.001	9	.66	.012	.30	.1	.01	2.3	.2	<.05	1	.5	9.4
400781	.2	92.5	8.4	28	.2	36.1	13.2	616	2.95	1349.1	1.2	32.9	12.6	24	.1	4.8	6.6	7	.49	.034	33	7	.06	85	.001	9	.55	.011	.27	.6	.01	2.3	.2	<.05	1	.5	8.7
400782	.2	149.5	10.7	38	.3	31.4	17.4	558	3.20	1806.3	1.1	23.1	12.7	18	.1	9.3	6.0	8	.22	.033	33	7	.06	81	.001	10	.60	.008	.27	.1	.03	2.6	.2	<.05	1	.7	9.5
400783	.2	67.3	5.1	26	1.0	25.9	6.5	296	2.24	629.0	.9	7.8	8.9	14	.1	4.0	2.1	5	.25	.021	21	8	.18	53	.001	5	.72	.012	.18	<.1	.02	1.4	.2	<.05	1	.9	6.0
400784	.3	135.3	12.7	58	.7	50.2	20.7	642	3.67	1673.1	1.4	23.6	16.5	21	.2	6.4	4.6	10	.23	.052	44	9	.24	92	.001	14	1.19	.007	.31	.1	.04	3.0	.3	<.05	2	.9	8.5
400785	.3	122.5	11.5	50	.3	46.3	17.7	492	3.66	2248.9	1.5	32.0	16.6	22	.1	4.6	7.4	10	.24	.046	43	9	.25	68	.001	8	1.17	.005	.24	.1	.04	3.0	.3	<.05	2	1.2	9.0
400786	.4	113.0	20.0	50	.6	40.6	13.7	394	3.99	3996.1	1.5	107.2	14.8	30	.1	6.8	14.6	10	.21	.051	38	7	.22	58	.001	10	1.08	.005	.23	.1	.04	2.5	.3	<.05	2	1.8	6.3
400787	.2	126.1	9.8	39	.3	39.1	18.1	430	3.36	2274.5	1.5	44.0	13.4	23	.2	4.6	8.2	10	.29	.043	41	9	.20	85	.001	9	1.15	.007	.27	<.1	.02	2.6	.2	<.05	2	1.0	6.7
400788	.5	155.5	13.7	31	.6	21.6	14.5	218	4.38	3999.6	1.5	64.7	16.8	19	.2	6.2	14.5	9	.11	.053	33	8	.12	79	.001	9	.90	.006	.28	.1	.04	2.4	.3	<.05	2	2.1	10.4
400791	.1	8.7	7.1	22	.1	16.3	2.4	718	1.39	279.2	.4	1.8	8.0	141	.2	1.8	.4	15	8.26	.012	14	19	.47	54	.031	<1	1.30	.019	.22	.1	<.01	2.7	.2	<.05	4	<.5	1.1
STANDARD DS7	20.8	109.4	71.2	413	.9	54.6	9.4	629	2.39	47.8	5.1	65.7	4.6	72	6.3	6.2	4.7	84	.93	.079	13	168	1.05	375	.124	39	.97	.069	.44	3.9	.20	2.5	4.2	.20	5	3.7	-

Sample type: Rock R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605775R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Au** gm/mt
400951	2.89
400952	4.21
401000 (pulp)	10.31
STANDARD SL20	6.02

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: ROCK PULP

10-27-06 P01:31 OUT

Data Log FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605775 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.4	2.7	2.9	46	<.1	7.0	5.4	489	1.71	5.7	2.3	.8	3.7	46	<.1	.1	.2	33	.39	.081	6	40	.59	197	.108	1	.89	.032	.47	.1	<.01	1.8	.3	<.05	4	<.5	-
400501	.2	45.8	7.6	42	.2	25.2	10.4	468	2.44	376.0	1.1	4.7	14.0	105	.3	1.8	1.9	22	2.23	.018	21	26	.56	58	.039	1	1.34	.050	.41	.3	<.01	3.0	.4	<.05	5	.7	6.1
400502	.5	93.3	8.9	25	.3	25.4	10.7	211	3.22	994.7	2.6	12.3	14.7	91	.1	2.6	3.1	25	.85	.095	23	26	.53	74	.037	1	1.55	.060	.38	.2	<.01	3.0	.4	.13	6	1.3	3.7
400503	.3	60.3	10.7	18	.2	18.8	8.1	221	1.79	519.5	1.8	7.9	16.4	34	.1	3.8	3.0	13	.61	.019	22	15	.28	70	.009	2	.88	.029	.21	.2	<.01	1.8	.2	<.05	3	.5	3.3
400504	.2	59.2	8.7	42	.1	23.8	10.0	386	2.69	362.0	1.4	12.9	16.8	34	.1	2.7	1.6	17	1.04	.026	29	19	.52	64	.015	1	1.18	.016	.30	.2	<.01	2.3	.3	<.05	4	<.5	6.1
400505	.2	72.8	8.4	44	.2	31.5	13.0	322	3.05	628.7	1.4	24.9	16.2	36	.1	4.1	1.5	22	.45	.028	31	26	.66	95	.029	1	1.56	.036	.44	.1	<.01	3.0	.5	<.05	6	<.5	5.3
400506	.5	95.5	7.0	49	.1	22.0	11.0	176	4.14	430.4	2.1	7.5	16.2	71	.1	2.2	1.2	26	.21	.026	29	28	.61	86	.063	1	1.77	.048	.61	.4	<.01	3.0	.7	.09	6	1.0	3.7
400507	.2	17.3	10.5	30	<.1	15.3	6.5	726	1.48	130.8	1.0	1.2	9.6	253	.4	1.5	.5	17	6.95	.020	17	21	.35	32	.037	1	.94	.064	.18	.1	<.01	3.0	.2	.08	4	<.5	2.2
400508	.7	138.9	9.1	29	.4	24.9	9.5	166	4.04	2964.6	2.6	47.7	16.0	111	.2	5.0	9.6	25	.32	.026	25	27	.46	73	.044	1	1.79	.077	.40	2.6	<.01	2.9	.4	.20	6	1.8	7.8
400509	.4	97.9	8.5	25	.2	24.7	11.4	253	2.51	758.7	1.6	10.7	12.1	50	.2	3.1	2.5	20	.29	.026	23	21	.40	72	.027	<1	1.46	.057	.28	.2	<.01	2.6	.3	<.05	5	.6	7.1
400510	.2	63.9	10.0	33	.2	25.2	9.1	304	1.69	557.9	1.3	9.5	16.4	21	.7	3.7	1.3	13	.16	.034	25	15	.25	67	.009	1	.85	.021	.20	.5	.01	1.8	.2	<.05	3	<.5	7.8
400511	1.2	60.9	10.0	26	.1	19.9	6.0	186	1.61	497.3	2.2	4.6	13.6	23	.5	2.3	.9	21	.10	.018	22	20	.25	62	.012	2	.74	.016	.20	.1	<.01	1.5	.2	<.05	2	.7	3.5
RE 400511	1.2	70.8	9.5	29	.1	23.0	6.2	193	1.66	517.7	2.2	4.7	13.7	24	.5	2.4	.9	22	.10	.017	22	22	.26	64	.012	1	.76	.015	.21	.1	<.01	1.5	.2	<.05	2	.9	-
400512	1.6	86.6	9.7	42	.2	35.9	10.8	218	2.70	2992.6	3.5	127.1	13.5	50	.6	4.7	10.3	37	.24	.025	24	30	.42	97	.024	1	1.51	.015	.30	.6	.01	2.4	.3	.05	4	1.4	8.5
400513	.3	62.5	11.8	46	.1	22.4	8.6	249	1.92	582.8	1.2	11.8	11.1	33	.8	3.4	2.0	17	.17	.024	21	16	.34	80	.021	1	1.13	.023	.21	.1	.01	2.1	.2	<.05	4	<.5	5.0
400514	.3	56.1	10.1	38	.2	21.9	7.7	579	2.25	422.1	1.0	9.1	11.1	134	.7	2.1	1.9	21	4.03	.018	21	22	.45	64	.031	1	1.65	.100	.19	.4	<.01	2.8	.2	<.05	5	<.5	5.0
400515	.2	38.5	12.1	37	.2	17.4	7.4	588	2.21	293.7	.7	5.9	9.3	244	.7	2.1	1.1	22	7.54	.030	16	23	.46	45	.037	1	1.72	.117	.19	.1	<.01	2.9	.2	.12	6	.5	2.7
400516	.2	59.6	8.5	27	.2	20.5	9.8	382	2.24	382.1	.9	5.9	11.7	118	.5	2.3	1.2	15	3.37	.017	20	18	.32	53	.020	1	1.26	.064	.17	.2	.01	2.2	.2	<.05	4	.5	6.1
400517	.2	46.3	6.6	34	.1	21.2	9.2	256	2.26	524.1	1.1	7.9	11.9	84	.3	3.3	1.4	13	2.04	.029	25	15	.38	64	.021	1	1.09	.012	.31	.1	<.01	1.7	.3	<.05	3	<.5	6.7
400518	.2	48.2	6.5	42	<.1	26.2	10.7	259	2.54	528.9	1.3	10.6	14.8	21	.3	3.7	1.3	17	.25	.038	28	20	.51	61	.023	2	1.37	.014	.38	.3	<.01	1.9	.5	<.05	4	<.5	5.2
400519	.2	54.7	7.8	37	.1	23.7	9.4	220	2.21	352.9	1.4	5.9	12.5	53	.1	2.0	1.1	22	.68	.041	26	24	.51	65	.038	1	1.45	.052	.35	.1	.01	2.3	.4	<.05	5	<.5	3.8
400520	.2	50.3	8.0	56	.1	27.9	13.2	319	2.75	667.2	1.3	5.9	13.3	47	.3	5.4	.8	24	.39	.024	28	24	.56	71	.039	1	1.62	.016	.35	.4	<.01	2.4	.4	<.05	5	<.5	4.4
400521	.2	68.0	9.6	37	<.1	21.1	9.5	263	2.19	496.6	1.1	6.0	12.7	27	.3	4.3	1.4	17	.23	.020	23	18	.39	79	.026	2	1.20	.021	.29	.1	<.01	2.2	.3	<.05	4	<.5	3.4
400522	.3	79.5	7.7	46	.1	30.3	12.5	305	2.86	849.9	1.9	12.3	15.4	37	.3	7.1	1.4	29	.32	.030	32	28	.54	70	.033	2	1.66	.013	.39	.4	.01	2.6	.5	<.05	5	<.5	9.3
400523	.2	87.1	8.6	38	.1	22.6	9.8	259	2.41	588.7	1.4	13.7	12.9	24	.4	6.4	1.8	18	.16	.026	23	17	.44	75	.015	2	1.07	.019	.23	1.4	<.01	2.0	.2	<.05	4	.5	2.8
400524	.5	40.1	9.0	72	.2	17.8	11.8	772	3.97	705.1	1.4	15.3	10.0	49	.8	8.8	1.3	66	.62	.159	25	105	1.33	200	.095	2	2.46	.018	.39	.6	.01	9.3	.3	<.05	7	<.5	3.4
400525	1.7	11.4	14.7	65	<.1	5.2	6.3	487	3.01	18.4	2.1	.9	10.1	81	.2	.4	.2	71	.98	.177	28	8	.57	592	.208	1	1.02	.132	.21	.8	<.01	5.0	.1	<.05	5	<.5	1.0
400526	.3	62.8	14.2	67	.1	19.4	8.9	442	2.77	505.5	1.3	8.7	11.7	34	1.5	10.9	1.8	37	.38	.080	22	44	.76	113	.082	2	1.59	.019	.22	.4	.01	4.5	.2	<.05	5	<.5	2.9
400527	.2	69.1	6.3	29	.1	14.6	6.3	226	2.18	323.3	1.0	3.0	11.2	26	.4	7.0	.6	18	.18	.022	16	17	.34	57	.025	2	1.00	.026	.17	.1	<.01	2.5	.1	<.05	4	.7	2.8
400528	.7	23.4	7.6	114	.1	8.4	13.4	1131	5.04	108.2	1.4	.9	9.3	57	.7	3.9	.1	95	1.26	.272	18	117	2.20	95	.204	3	3.01	.020	.08	.5	.02	9.2	.1	<.05	10	<.5	6.1
400529	.3	10.4	8.2	126	<.1	10.8	14.5	1239	5.25	153.2	1.2	<.5	9.8	52	.9	4.9	.1	109	1.23	.280	16	153	2.40	116	.194	3	3.16	.021	.08	.6	.02	11.0	.1	<.05	12	<.5	5.2
400530	.4	12.9	8.2	114	<.1	9.2	12.0	1151	5.08	164.2	1.3	<.5	9.5	61	.8	3.4	.1	108	1.42	.263	18	143	2.32	230	.233	2	3.26	.030	.25	.5	.01	11.8	.2	<.05	11	<.5	6.2
400531	.3	57.2	8.8	54	.1	20.9	10.0	518	2.72	555.8	1.0	6.2	11.6	31	.4	16.7	.7	32	.46	.064	22	41	.66	155	.050	3	1.51	.026	.28	.3	.01	4.4	.2	<.05	5	<.5	4.2
400532	.3	85.3	8.9	51	.1	30.8	12.0	483	3.54	780.2	1.4	14.5	13.1	34	.5	13.2	1.6	35	.54	.086	31	40	.65	175	.064	4	1.63	.018	.27	.7	.02	5.0	.3	<.05	5	.7	9.3
400951	.4	137.5	122.0	12	4.9	7.4	16.1	36	14.95	>10000	.7	2695.6	4.5	82	.3	309.2	606.1	3	.05	.009	11	5	.04	38	.003	1	.38	.011	.16	2.5	.05	.7	.1	4.65	1	80.8	1.0
STANDARD DS7	20.8	110.4	69.4	412	.9	54.9	9.6	635	2.40	48.2	5.0	74.9	4.6	72	6.6	6.1	4.6	85	.94	.079	14	167	1.05	377	.126	36	.99	.078	.45	3.9	.20	2.6	4.3	7.19	5	3.8	-

GROUP 1DX - 30 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

10-05-06 A10:46 OUT

Data___ FA ____ DATE RECEIVED: SEP 6 2006 DATE REPORT MAILED:.....

Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

ACME ANALYTICAL

Copper Ridge Exploration Inc. PROJECT Scheelite Dome FILE # A605775 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	3.4	5.9	48	.1	7.9	4.5	535	1.86	31.7	3.0	.5	4.8	59	<.1	.3	.3	36	.54	.070	10	17	.60	202	.125	2	1.07	.083	.49	.6	<.01	2.1	.4	<.05	5	<.5	-
400952	.4	80.5	262.5	19	15.6	9.0	8.2	155	18.48	>10000	.6	4233.3	4.9	48	.9	498.6	1509.0	5	.12	.010	4	6	.05	36	.003	1	.31	.012	.10	2.8	.09	.8	.1	3.85	1	>100	3.0
400953	.2	83.9	16.6	54	.3	23.4	10.3	317	2.88	2383.2	1.1	39.8	15.2	57	1.4	8.8	14.3	25	.55	.025	18	26	.54	91	.043	2	2.22	.091	.30	.1	.01	3.1	.4	<.05	7	1.4	3.0
400954	.2	46.7	11.8	58	.2	20.4	8.8	249	2.51	1048.3	1.1	21.9	17.3	29	.7	10.6	3.2	15	.54	.041	28	18	.36	86	.006	1	1.16	.028	.26	.4	.01	1.7	.2	<.05	4	<.5	5.4
400955	.2	60.9	9.4	28	.2	22.2	10.8	363	2.58	1339.9	1.0	22.6	15.1	45	.2	8.5	10.0	14	1.36	.034	32	16	.34	80	.008	1	1.13	.023	.24	.1	.01	1.8	.2	<.05	3	.7	2.9
400956	.2	47.1	10.0	23	.2	17.7	8.7	372	1.99	1051.6	1.0	38.4	13.9	56	.1	4.2	5.2	14	2.11	.020	21	18	.40	81	.023	2	1.22	.050	.27	1.0	<.01	2.3	.2	<.05	4	<.5	4.6
400957	.3	64.5	8.2	30	.2	26.0	10.0	307	2.70	781.4	1.1	8.8	16.0	74	.1	3.2	3.1	26	1.38	.025	25	27	.57	71	.036	1	2.31	.130	.34	.1	<.01	3.3	.4	<.05	8	<.5	3.1
400958	.3	95.7	9.1	27	.2	24.4	10.1	179	3.27	815.8	1.7	14.9	16.6	65	<.1	2.3	2.1	26	.41	.037	25	24	.62	104	.041	2	2.31	.084	.47	.1	.01	3.1	.5	.07	7	<.5	4.5
400959	.1	45.8	12.0	49	.2	17.3	8.0	953	2.73	1579.7	.7	17.2	9.8	528	.2	1.8	5.8	27	12.74	.073	17	27	1.14	91	.040	2	2.56	.135	.32	1.8	.01	3.2	.4	<.05	8	.5	1.4
RE 400959	.2	47.5	11.6	47	.2	16.7	8.1	931	2.69	1575.8	.7	17.4	9.4	519	.2	1.8	5.7	27	12.61	.076	17	28	1.14	95	.042	3	2.54	.135	.33	1.8	.01	3.1	.4	<.05	8	<.5	-
400960	.3	36.6	9.5	28	.1	17.1	8.3	350	2.15	227.6	.8	2.6	11.1	77	.3	1.7	.7	15	2.50	.019	22	15	.38	80	.012	2	1.14	.055	.22	.1	.01	2.2	.2	<.05	4	<.5	4.0
400961	.2	39.1	11.8	34	.1	18.9	8.1	332	2.14	260.0	.7	1.6	13.3	112	.3	1.7	.7	18	2.26	.041	23	18	.45	86	.020	2	1.28	.075	.30	.3	<.01	2.4	.3	<.05	4	<.5	2.9
400962	.2	55.8	8.4	24	.1	19.9	9.8	283	2.29	354.7	.8	5.6	12.4	37	.1	2.0	1.2	18	.62	.026	24	17	.50	81	.013	2	1.32	.046	.26	.1	<.01	2.1	.2	<.05	4	<.5	6.2
400963	.2	46.1	7.3	34	.1	24.2	10.6	295	2.49	340.1	.8	9.7	12.4	57	.1	2.4	1.3	24	.86	.015	23	23	.60	115	.029	2	1.75	.078	.40	.7	<.01	3.1	.4	.08	5	<.5	4.2
400964	.2	41.9	8.5	34	.1	20.3	8.7	422	2.41	273.1	.8	4.2	13.9	103	.1	1.9	1.1	19	3.20	.025	27	21	.52	82	.018	2	1.36	.032	.34	.3	<.01	2.6	.3	<.05	5	<.5	5.4
400965	.1	24.9	10.7	42	<.1	19.1	8.8	517	2.25	233.0	.8	6.0	12.2	121	.1	3.3	.7	18	4.94	.023	27	21	.47	52	.017	1	1.21	.019	.27	.1	.01	2.9	.3	<.05	5	<.5	3.4
400966	.2	33.7	9.8	40	<.1	17.7	8.9	437	2.28	303.1	.9	4.9	14.8	92	.1	2.8	.6	15	3.86	.042	29	17	.40	71	.012	2	1.13	.018	.25	.2	<.01	2.3	.2	<.05	4	<.5	3.4
400967	.1	28.0	7.2	38	<.1	19.3	7.6	274	2.07	232.8	.5	10.2	13.4	31	.1	2.6	.8	17	1.14	.017	26	20	.51	50	.013	1	1.21	.018	.22	<.1	<.01	2.1	.2	<.05	5	<.5	5.6
400968	.1	50.1	4.9	41	<.1	25.4	10.0	199	2.81	396.8	.6	4.1	13.3	19	<.1	3.5	.6	21	.34	.041	31	19	.72	76	.013	1	1.83	.020	.41	.3	<.01	2.4	.4	<.05	5	<.5	6.9
400969	.2	43.9	11.3	26	.1	18.5	7.7	345	2.04	280.7	.6	6.0	12.7	77	.1	2.0	1.0	14	2.26	.030	29	15	.47	79	.018	2	1.23	.014	.36	.1	<.01	2.0	.4	<.05	4	<.5	6.6
400970	.3	122.3	8.7	38	.3	33.4	13.3	290	4.32	827.4	1.1	37.8	14.5	30	.1	4.2	3.9	25	.68	.034	29	24	.73	78	.028	1	1.91	.018	.49	.2	<.01	3.2	.6	<.05	7	1.1	5.5
400971	.2	98.3	7.4	35	.3	23.3	13.6	188	3.55	2918.6	1.1	130.9	17.0	37	.1	3.2	6.5	23	.44	.035	26	26	.67	117	.020	1	1.81	.016	.44	.4	<.01	2.7	.6	<.05	6	.8	4.1
400972	.2	67.9	6.6	34	.1	26.4	10.6	341	2.88	509.6	.9	20.7	14.9	39	<.1	1.6	2.1	27	.80	.029	26	27	.78	87	.034	1	2.15	.058	.45	.1	<.01	3.2	.5	<.05	7	<.5	5.9
400973	.2	51.5	8.9	39	.2	27.0	11.8	594	3.01	373.2	.9	16.0	11.9	142	.1	1.3	1.9	32	4.01	.039	23	31	.80	91	.044	1	2.43	.140	.47	.4	<.01	4.6	.5	.09	9	<.5	5.5
400974	.2	50.3	7.0	28	.1	21.0	8.4	333	2.56	376.4	.9	6.4	12.0	43	.1	1.4	1.1	21	1.44	.021	27	20	.49	99	.018	2	1.41	.038	.36	<.1	.01	2.7	.4	<.05	5	.5	6.1
400975	.7	9.7	13.8	59	<.1	4.5	5.6	387	2.86	19.8	1.7	.5	10.2	82	.1	.4	.1	58	.95	.172	27	7	.57	581	.174	<1	1.11	.117	.19	.8	<.01	4.6	.1	<.05	6	<.5	.7
400976	.3	98.9	13.0	33	.3	25.4	10.5	282	3.38	1474.1	.9	33.6	11.6	42	.2	4.1	3.0	9	.30	.031	32	7	.20	86	.001	5	.90	.011	.21	.1	.06	3.4	.2	<.05	2	.5	3.0
400977	.6	89.7	33.5	38	.4	22.3	8.8	261	3.34	1849.4	.8	48.1	11.0	48	.4	5.3	6.0	8	1.02	.035	32	7	.10	90	<.001	6	.81	.009	.20	.3	.05	3.7	.2	<.05	2	<.5	8.0
400978	.3	91.2	10.1	33	.2	26.6	12.0	441	3.30	769.7	1.0	32.4	14.9	24	.1	1.8	4.5	16	.63	.034	37	13	.13	138	.001	5	1.02	.018	.26	.1	.04	3.2	.2	<.05	3	<.5	4.2
400979	.4	85.6	14.5	29	.3	23.7	8.8	337	2.96	1253.3	.8	37.1	12.6	60	.2	3.2	4.4	9	2.12	.043	34	8	.07	86	.001	5	.64	.012	.20	.3	.05	2.9	.2	<.05	2	.5	4.4
400980	.2	75.8	8.7	26	.2	24.7	9.6	379	2.44	937.7	.9	21.3	15.1	62	.1	1.7	2.9	8	2.76	.042	37	8	.10	88	.001	3	.60	.013	.21	.2	.02	2.2	.1	<.05	2	.6	5.8
400981	.4	80.6	13.7	28	.4	26.3	13.0	469	3.57	8455.7	1.3	270.9	14.4	67	.1	5.3	32.6	9	1.83	.032	35	8	.08	131	.001	2	.73	.011	.23	.4	.03	3.1	.2	<.05	2	1.5	9.1
400982	.3	79.1	13.1	33	.4	23.8	9.6	651	2.87	1004.5	1.0	49.0	13.9	165	.1	1.1	6.4	13	6.81	.040	40	10	.09	97	<.001	5	.80	.016	.20	<.1	.04	4.1	.2	<.05	2	.9	6.9
400983	.1	45.2	8.9	28	.2	16.2	7.0	450	1.93	503.8	.5	14.3	11.3	49	.2	1.6	1.9	14	1.59	.021	30	16	.20	74	.004	2	.88	.022	.22	.3	.01	2.7	.2	<.05	3	.8	4.6
400984	.2	35.9	11.1	32	.2	20.7	8.0	689	2.52	359.2	.9	8.5	12.6	179	.2	1.6	1.3	23	6.06	.031	30	22	.51	66	.035	<1	1.50	.040	.25	.1	.01	3.7	.2	<.05	6	<.5	9.0
STANDARD DS7	20.8	112.6	70.7	411	.9	55.8	9.6	636	2.42	68.0	5.1	69.9	4.9	71	6.6	6.2	4.7	85	.95	.080	14	167	1.06	377	.128	41	1.00	.080	.45	3.9	.20	2.6	4.3	.20	5	3.1	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data f FA ____

ACME ANALYTICAL

Copper Ridge Exploration Inc. PROJECT Scheelite Dome FILE # A605775 Page 3

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample kg
G-1	.1	1.9	6.1	46	.1	3.8	4.3	528	1.82	2.5	2.9	<.5	4.2	53	<.1	.2	.1	35	.47	.078	8	15	.58	218	.116	1	.91	.056	.46	.1	<.01	1.9	.3	<.05	5	<.5	-
400985	.2	37.2	11.1	38	.2	21.4	9.8	496	2.41	444.0	.9	5.5	12.2	131	.2	1.8	2.1	28	3.53	.028	23	29	.57	97	.046	1	1.99	.109	.30	.4	<.01	3.8	.3	<.05	8	<.5	4.5
400986	.3	68.8	13.5	33	.3	27.4	12.9	464	3.24	805.1	1.1	18.6	15.0	154	.2	2.7	4.8	33	2.24	.044	26	35	.64	151	.049	1	2.70	.148	.31	.2	.01	4.5	.4	<.05	9	.5	4.9
400987	.2	74.1	9.4	31	.2	20.7	10.5	462	2.70	784.4	1.1	41.3	16.1	170	.2	2.2	6.8	23	1.89	.032	23	26	.55	138	.038	1	1.95	.090	.34	.4	.01	3.4	.4	<.05	7	.8	10.0
400988	.1	46.8	8.2	30	.1	19.2	8.7	530	1.99	277.1	1.1	9.6	12.0	150	.2	1.5	1.8	16	4.37	.024	21	19	.40	66	.031	1	1.11	.042	.25	.1	.01	2.5	.3	<.05	4	<.5	6.4
400989	.1	19.1	7.7	21	.1	10.0	5.0	532	1.31	195.4	.6	4.3	11.4	116	.1	1.2	1.1	12	3.70	.015	17	16	.29	50	.030	<1	.79	.044	.15	.6	<.01	2.0	.2	<.05	3	.5	2.2
400990	.2	62.3	7.9	32	.1	20.9	8.7	247	2.25	438.7	1.2	10.7	13.4	49	.1	1.9	2.2	18	.73	.022	19	22	.48	70	.032	1	1.56	.072	.33	.1	.01	2.6	.4	<.05	5	.6	4.1
400991	.2	40.8	9.3	33	.2	21.3	9.4	358	2.23	562.4	1.1	10.2	12.2	73	.2	1.9	3.3	19	1.21	.024	20	23	.48	80	.034	<1	1.68	.076	.33	.4	<.01	2.8	.3	<.05	5	.9	4.7
400992	.2	43.0	10.0	28	.2	18.8	7.4	509	2.11	288.4	1.0	7.4	11.4	188	.2	1.8	1.2	17	3.83	.024	17	20	.49	48	.032	<1	1.42	.056	.29	.1	<.01	2.5	.4	<.05	5	.5	6.3
400993	.2	57.1	11.7	29	.2	20.3	7.5	207	2.34	367.6	1.3	9.2	13.4	100	.1	2.1	1.4	23	.78	.026	22	24	.57	67	.031	<1	1.74	.080	.39	.3	<.01	2.9	.4	<.05	6	.7	5.0
400994	.2	70.4	9.9	25	.2	23.3	8.5	194	2.08	443.4	1.2	7.0	11.1	71	.1	2.4	1.6	19	.53	.044	18	22	.51	59	.019	1	1.60	.073	.21	.1	<.01	2.5	.2	<.05	5	.8	6.6
400995	.2	84.2	10.9	37	.2	31.0	10.8	409	3.00	615.5	1.3	8.1	13.9	138	.2	2.4	2.9	34	1.55	.076	22	35	.71	67	.045	2	2.85	.191	.34	.3	<.01	4.5	.4	<.05	9	.8	4.3
400996	.2	36.8	7.5	68	<.1	28.3	11.1	118	2.80	312.0	2.2	6.5	21.8	39	.1	3.2	.9	14	.17	.035	41	19	.62	87	.027	<1	1.52	.018	.65	.1	<.01	1.8	.7	<.05	5	<.5	7.5
400997	.2	49.6	8.5	49	.1	24.3	9.4	332	2.42	490.9	1.4	6.6	13.1	67	.2	2.9	1.2	20	.77	.117	26	24	.54	72	.027	1	1.44	.033	.34	.3	<.01	2.7	.3	<.05	5	<.5	5.9
400998	.2	47.4	7.7	50	.1	24.4	10.4	218	2.56	279.7	1.3	6.0	16.8	63	.1	2.7	.7	21	.65	.025	28	23	.59	99	.046	1	1.60	.057	.53	.1	<.01	2.9	.6	<.05	5	<.5	5.8
400999	.2	30.8	8.6	57	<.1	20.1	10.0	138	2.45	401.9	1.0	5.8	17.8	50	.1	2.5	.5	16	.16	.021	27	20	.52	131	.028	<1	1.32	.023	.50	.2	<.01	1.8	.5	<.05	5	.6	6.9
RE 400999	.2	32.4	8.4	59	<.1	20.9	10.5	142	2.52	396.7	1.1	6.5	17.1	52	.1	2.3	.5	16	.16	.021	27	20	.53	125	.029	1	1.37	.023	.52	.2	<.01	1.8	.5	<.05	5	<.5	-
401000(pulp)	8.4	59.5	3.8	42	7.9	307.9	12.6	158	3.06	459.6	.1	8891.9	.3	5	.1	52.7	<.1	15	.11	.039	6	326	.07	30	.002	2	.29	.006	.19	.9	6.53	1.4	8.9	1.99	1	24.6	-
STANDARD DS7	20.8	109.1	69.1	405	.9	55.2	9.5	631	2.40	47.8	4.9	80.3	4.6	71	6.5	5.8	4.6	84	.94	.079	13	166	1.05	366	.126	39	.98	.078	.44	3.8	.20	2.6	4.2	.19	5	3.5	-

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 1 FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605327R

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Greg Dawson

SAMPLE#	Au** gm/mt
405032	1.04
405033	3.22
405034	4.80
405035	1.50
STANDARD SL20	6.12

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: CORE PULP

10-30-06 P06:07 OUT

Data 1 FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

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ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9001 Accredited Co.)

WHOLE ROCK ICP ANALYSIS

Copper Ridge Exploration Inc. File # A603663
500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	SiO2 %	Al2O3 %	Fe2O3 %	MgO %	CaO %	Na2O %	K2O %	TiO2 %	P2O5 %	MnO %	Cr2O3 %	Ba ppm	Ni ppm	Sr ppm	Zr ppm	Y ppm	Nb ppm	Sc ppm	LOI %	TOT/C %	TOT/S %	SUM %
404999	52.45	14.84	7.98	5.44	7.91	1.28	3.54	1.19	.71	.15	.032	1167	17	476	171	44	19	30	4.3	.32	.01	100.05
404983	87.49	5.83	2.22	.54	.17	1.04	.86	.24	.03	.02	.004	373	6	86	176	11	5	4	1.4	.08	.02	99.92
405250	89.21	5.37	1.03	.20	.04	.73	2.05	.18	.04	.01	.002	560	10	32	210	7	8	2	1.1	.05	.01	100.06
STANDARD SO-18/CSC	58.19	14.11	7.66	3.34	6.39	3.69	2.14	.69	.83	.39	.550	525	55	414	278	33	22	25	1.9	3.16	4.21	100.04

GROUP 4A - 0.200 GM SAMPLE BY LIBO2/LI2B4O7 FUSION, ANALYSIS BY ICP-ES. (LIBO2/LI2B4O7 FUSION MAY NOT BE SUITABLE FOR MASSIVE SULFIDE OR HIGH BARITE SAMPLES.) LOI BY LOSS ON IGNITION. TOTAL C & S BY LECO. (NOT INCLUDED IN THE SUM)

-

- SAMPLE TYPE: ROCK R150

Data P FA ____ **DATE RECEIVED:** JUL 13 2006 **DATE REPORT MAILED:**.....2006-08-03 P03:54

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A603663

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	1.4	2.1	2.4	46	<.1	4.3	4.2	542	1.87	<.5	2.6	<.5	4.0	55	<.1	<.1	.1	30	.48	.076	7	5	.55	201	.119	1	.93	.054	.48	.2	.01	1.8	.3	<.05	5	<.5
404999	1.0	11.4	6.2	98	<.1	7.6	12.1	832	4.79	23.1	1.4	<.5	8.6	150	.2	4.1	.1	73	2.80	.309	20	73	1.99	309	.282	3	3.74	.135	.43	.5	.03	6.1	.2	<.05	10	<.5
404983	.6	33.4	18.9	21	.3	9.0	3.2	106	1.48	39.2	.5	8.2	7.2	5	.1	.7	3.6	9	.04	.011	4	16	.24	196	.008	2	.60	.017	.09	.1	<.01	1.1	.1	<.05	2	<.5
405250	.4	5.3	9.9	6	<.1	3.0	1.2	40	.49	89.1	.3	2.4	9.4	3	<.1	5.3	.1	8	.02	.013	16	9	.02	53	.002	3	.18	.012	.15	.1	.01	.2	.1	<.05	<1	<.5
STANDARD DS7	21.7	112.9	72.2	424	.9	57.4	9.8	640	2.46	48.7	5.0	87.6	4.5	72	6.5	5.9	4.6	86	.96	.080	14	168	1.08	373	.128	40	.98	.078	.44	4.0	.21	2.5	4.3	.22	5	3.9

GROUP 1DX - 30 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150

2006-08-03 P01:14

Data P FA ____ **DATE RECEIVED:** JUL 13 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

ASSAY CERTIFICATE

Copper Ridge Exploration Inc. File # A603662R
500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Au** gm/mt
404920	.89
404958	1.67
404959	.78
404993	2.07
404994	6.12
405002	2.29
405005	2.34
405007	3.07
405010	.64
STANDARD SL20	6.12

GROUP 6 - PRECIOUS METALS BY FIRE ASSAY FROM 1 A.T. SAMPLE, ANALYSIS BY ICP-ES.
- SAMPLE TYPE: ROCK PULP

10-30-06 P06:06 OUT

Data 1 FA ____ **DATE RECEIVED:** OCT 21 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Clarence Leong

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.) 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A603662 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	2.3	2.5	50	<.1	6.3	4.6	545	1.89	<.5	2.3	1.1	4.0	63	<.1	<.1	<.1	37	.56	.084	7	54	.61	229	.131	1	.92	.060	.48	.1	<.01	2.1	.3	<.05	5	<.5
404918	.2	8.8	.9	3	<.1	2.4	.8	57	.50	21.0	<.1	.7	.7	2	<.1	.8	.1	<1	.17	.001	1	16	.01	6	.001	4	.04	.013	.02	.1	<.01	.1	<.1	<.05	<1	<.5
404919	.2	11.5	5.5	19	<.1	7.4	4.3	222	1.07	120.2	.4	1.7	9.1	9	.3	3.9	.6	2	.24	.012	17	12	.04	90	.002	5	.30	.020	.25	.2	<.01	.6	.1	<.05	1	<.5
404920	1.4	25.5	32.1	6	2.4	2.9	1.5	57	.75	104.6	.4	663.4	3.9	2	.1	12.3	266.3	<1	.02	.003	6	17	.01	25	.002	3	.11	.009	.07	.1	.01	.3	<.1	.06	<1	.8
404921	.2	15.4	6.5	20	<.1	8.2	3.5	262	1.10	162.6	.5	31.8	13.4	5	.3	.9	6.0	3	.06	.010	22	13	.06	87	.005	1	.35	.019	.25	.5	.01	.7	.1	<.05	1	<.5
RE 404921	.2	14.5	6.4	22	<.1	7.7	3.4	264	1.10	162.8	.4	23.3	13.7	5	.3	1.0	6.2	4	.06	.010	22	13	.06	82	.005	2	.36	.020	.27	.5	<.01	.7	.1	<.05	1	<.5
404922	.2	5.7	16.6	8	<.1	2.1	.9	394	.73	13.9	.1	4.4	1.1	750	.4	.2	1.8	1	12.52	.003	3	9	.14	13	.002	1	.10	.008	.03	.1	.01	.8	<.1	<.05	<1	<.5
404923	.6	25.6	12.3	24	<.1	14.1	5.2	175	1.21	58.9	1.0	2.8	9.4	7	.1	1.0	.9	6	.09	.010	12	14	.22	39	.012	1	.55	.014	.14	.3	.01	.8	.1	<.05	2	<.5
404924	.2	5.7	1.2	2	<.1	5.6	2.0	68	.46	332.2	.1	12.4	.3	44	.1	.5	3.9	<1	.77	.002	1	17	.02	4	<.001	<1	.05	.004	.01	.3	<.01	.1	<.1	<.05	<1	<.5
404925	.2	2.1	.3	1	<.1	3.3	1.6	34	.35	308.1	<.1	2.8	.1	1	<.1	.4	.3	<1	.01	<.001	<1	18	.01	2	<.001	1	.02	.003	.01	.2	.01	.1	<.1	<.05	<1	<.5
404926	.3	15.3	.6	14	<.1	7.6	2.3	138	1.30	81.7	.2	2.0	.5	2	<.1	.5	.3	4	.02	.002	2	22	.28	2	.002	1	.48	.005	.01	.1	.01	.6	<.1	<.05	2	<.5
404927	.2	37.0	719.4	7	10.7	77.7	17.5	167	.66	604.5	1.1	437.7	6.0	3	.3	217.5	507.4	2	.03	.015	14	19	.03	36	.001	13	.24	.005	.14	.2	.02	.7	.1	<.05	<1	2.5
404928	.2	23.8	305.6	59	1.8	101.2	20.3	483	2.84	471.5	1.7	39.3	16.8	115	.3	41.6	67.9	43	1.93	.031	45	53	.76	165	.083	3	2.88	.247	.39	.2	.01	6.5	.3	<.05	10	1.5
404929	.1	22.0	15.2	44	.2	13.2	5.1	238	1.53	23.0	.6	4.9	11.4	54	.3	2.9	6.0	23	1.81	.012	19	34	.39	56	.081	1	1.02	.092	.34	.3	.01	4.4	.2	<.05	5	<.5
404930	.8	35.0	12.2	99	.2	21.3	13.8	611	3.90	77.4	3.7	1.6	17.6	95	.3	2.3	1.7	117	1.02	.084	33	152	1.93	615	.228	2	3.45	.197	1.08	.5	<.01	12.9	1.3	<.05	11	<.5
404931	.2	9.8	9.6	14	.1	10.1	4.4	371	.93	91.4	.4	1.8	12.0	20	.5	8.7	1.1	2	.81	.011	26	12	.03	68	.001	10	.27	.004	.15	.2	<.01	1.0	.1	<.05	1	<.5
404932	.6	16.4	27.2	136	.2	19.3	13.8	771	3.69	24.0	3.6	.9	15.8	79	1.3	3.0	.5	108	1.40	.080	30	141	1.92	493	.175	1	2.92	.104	.77	.4	.01	11.1	.7	<.05	10	<.5
404933	.1	9.9	9.1	25	.1	13.0	6.0	236	1.25	27.2	.9	<.5	13.1	41	.3	1.2	.5	13	1.21	.013	16	22	.24	224	.058	1	.65	.038	.21	.1	.01	1.7	.2	.09	3	<.5
404934	.2	26.0	7.8	30	.1	15.9	9.1	316	1.74	12.0	.9	1.6	8.0	25	.2	1.4	.5	17	1.79	.014	15	27	.45	126	.061	2	.82	.055	.27	.2	<.01	2.5	.2	<.05	4	.6
404935	.2	48.0	3.3	10	<.1	7.9	3.1	136	1.47	295.7	.7	26.5	2.7	34	.1	1.3	3.3	8	.46	.020	4	22	.20	56	.016	2	.61	.008	.06	.8	<.01	1.2	.1	<.05	2	.6
404936	.2	39.0	3.8	13	<.1	6.2	1.9	78	1.25	200.7	1.3	4.7	11.2	3	.1	1.7	2.0	5	.03	.009	11	16	.17	60	.013	2	.61	.009	.26	.1	.01	.8	.2	<.05	1	.5
404937	.2	10.0	3.6	14	<.1	5.8	2.0	96	1.00	75.6	.4	3.2	10.4	4	<.1	1.6	.8	5	.03	.008	11	18	.11	47	.015	1	.39	.010	.23	.1	<.01	.6	.1	<.05	1	<.5
404938	.2	2.8	4.6	5	<.1	1.6	.3	32	.35	24.0	<.1	<.5	1.0	1	.1	.7	.2	<1	.01	.001	2	21	.01	21	.001	1	.06	.002	.05	.1	<.01	.2	<.1	<.05	<1	<.5
404939	.2	11.3	.8	10	<.1	8.4	3.8	159	.81	192.8	.3	<.5	1.9	9	<.1	2.5	.3	2	.08	.037	6	17	.11	22	.001	2	.26	.005	.12	.3	.01	.4	.1	<.05	1	<.5
404940	1.1	61.0	5.7	47	<.1	23.0	14.3	550	3.60	351.7	2.6	36.7	14.4	128	.1	1.5	2.6	121	2.19	.084	18	176	1.95	130	.186	14	3.74	.300	.27	.6	.01	7.6	.3	.34	13	.8
404941	.1	.9	24.9	70	.3	.2	.7	793	.26	6.9	.4	1.6	4.7	149	3.9	.8	.5	2	13.85	.013	13	5	.02	59	.038	3	.78	.155	.04	.3	<.01	.5	<.1	<.05	2	<.5
404942	.5	136.7	11.6	54	.4	46.1	20.8	452	4.56	35.7	2.5	1.9	19.8	180	.2	.9	1.1	37	2.89	.086	36	51	.88	143	.090	2	4.24	.380	.91	.2	.01	5.6	.7	1.39	12	1.8
404943	.1	11.4	12.8	31	.1	15.8	5.9	491	1.00	16.9	1.4	28.2	10.3	642	.7	.3	3.2	10	13.18	.048	26	17	.22	84	.051	2	3.00	.200	.12	.3	.01	1.7	.1	.06	8	.5
404944	.3	18.7	22.3	47	.1	22.3	12.1	1196	1.97	43.5	.7	2.4	9.8	96	1.1	.7	.8	16	2.94	.025	28	26	.39	182	.080	1	1.09	.084	.18	.2	.01	3.2	.3	<.05	4	<.5
404945	.2	8.4	1.0	4	<.1	2.8	.8	46	.44	48.4	<.1	1.7	.2	6	.1	.5	.2	1	.16	.002	1	18	.03	5	.001	<1	.07	.003	.01	.2	.01	.1	<.1	<.05	<1	<.5
404946	.2	4.7	8.7	5	<.1	2.8	1.0	37	.44	36.1	.3	1.0	9.0	5	.1	2.7	.1	1	.06	.023	13	15	.02	55	.003	3	.16	.011	.17	<.1	<.01	.3	.1	<.05	<1	<.5
404947	.1	19.7	3.1	3	<.1	5.6	2.0	67	.47	462.8	.1	1.5	1.0	3	.1	1.9	.7	<1	.07	.002	3	20	.01	26	<.001	<1	.05	.002	.02	.1	.01	.2	<.1	.07	<1	<.5
404948	.2	3.6	.5	1	<.1	1.9	.5	43	.52	523.4	<.1	1.1	.2	1	<.1	1.0	.2	<1	.01	.001	1	20	.01	11	.001	3	.03	.003	.02	.1	.01	.1	<.1	<.05	<1	<.5
404949	.2	8.7	2.2	1	.1	2.4	1.1	46	.62	234.2	.3	3.2	.1	1	<.1	1.0	1.7	<1	.01	.001	<1	20	.01	5	<.001	1	.02	.002	.01	.4	<.01	.1	<.1	<.05	<1	<.5
404950(pulp)	13.1	1522.6	5.5	60	.4	539.0	20.5	612	4.52	6.3	.3	112.0	1.5	81	.2	1.9	.2	60	1.28	.066	5	629	.84	153	.112	4	1.59	.128	.24	1.6	.24	4.4	.1	.97	5	3.2
STANDARD DS7	20.7	108.6	70.1	412	.9	55.0	9.6	629	2.38	47.9	4.9	68.8	4.4	71	6.4	6.0	4.7	81	.93	.080	12	160	1.06	370	.125	39	.97	.074	.43	3.8	.20	2.5	4.2	.22	4	3.3

GROUP 1DX - 30 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

* Fire Assay recommended for Au >1000 ppb

2006-08-03 A11:01

Data h FA ____ DATE RECEIVED: JUL 13 2006 DATE REPORT MAILED:.....

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	1.8	2.1	43	<.1	5.7	4.1	518	1.80	<.5	2.1	<.5	3.5	52	<.1	<.1	.1	37	.52	.080	6	49	.58	203	.122	<1	.87	.049	.51	.1	<.01	1.7	.3	<.05	5	<.5
404951	.2	14.1	3.3	18	<.1	4.9	2.3	90	.98	36.6	.7	10.5	10.9	26	<.1	.4	1.0	11	.12	.007	16	20	.17	85	.038	<1	.56	.037	.20	1.6	<.01	1.2	.1	<.05	3	<.5
404952	.2	18.7	6.0	33	<.1	11.6	2.4	194	1.24	48.2	.7	2.1	14.0	28	.4	.8	.7	9	.19	.012	23	18	.17	128	.025	2	.68	.066	.18	.6	<.01	1.3	.1	<.05	2	<.5
404953	.1	6.0	6.3	25	<.1	8.1	4.2	162	1.26	13.1	.6	<.5	17.0	40	.2	.2	.1	15	.24	.011	21	27	.27	105	.062	<1	.90	.055	.34	.3	<.01	1.9	.1	<.05	4	<.5
404954	.2	35.1	8.9	27	.2	9.9	3.8	147	1.85	725.0	1.0	3.4	16.9	47	.4	1.4	2.7	20	.25	.013	21	28	.32	130	.052	2	1.17	.106	.37	.6	<.01	2.7	.2	<.05	5	<.5
404955	.3	26.1	12.0	7	.2	5.4	2.0	116	.96	251.7	.4	6.4	.2	1	.3	4.3	4.9	2	.03	.002	2	15	.01	6	.001	1	.05	.003	.01	.8	<.01	.1	<.1	<.05	<1	<.5
404956	5.1	154.2	16.2	146	.2	99.7	44.4	719	25.31	3752.5	5.9	26.2	4.3	10	2.3	29.4	2.3	18	.03	.041	33	11	.08	38	.001	5	.71	.006	.07	3.2	.02	1.2	.2	.08	1	1.2
404957	.3	43.9	1.6	3	.2	4.3	1.4	49	1.40	456.7	.3	25.4	.7	2	.1	56.5	2.9	1	.01	.002	2	15	.01	48	.001	5	.07	.003	.05	.5	.02	.2	<.1	.10	<1	<.5
404958	.5	158.8	16.1	20	.8	39.3	22.5	169	11.81	>10000	1.6	1612.1	17.6	151	.1	78.3	190.9	37	1.06	.017	27	35	.69	74	.022	<1	3.76	.277	.24	10.3	.03	5.1	.3	3.98	12	23.3
404959	1.1	332.5	7.6	10	.6	50.1	165.4	143	13.44	>10000	1.2	873.6	14.4	113	.1	103.0	50.3	14	1.50	.015	19	19	.25	24	.008	2	2.86	.318	.05	>100	.03	1.9	.3	5.54	9	35.6
404960	.3	196.8	9.1	16	.4	18.8	27.7	334	3.82	>10000	.8	321.7	11.9	95	.2	11.4	24.6	20	1.23	.015	11	23	.41	61	.016	1	2.84	.243	.19	3.2	.01	2.7	.2	.90	9	6.0
404961	.3	70.2	3.4	34	.1	8.6	5.1	83	2.68	299.4	2.2	3.8	26.6	135	.1	1.5	.7	17	.10	.030	46	28	.55	121	.083	1	1.51	.029	.99	.1	<.01	1.9	.9	.18	5	<.5
404962	.2	11.3	6.4	4	<.1	3.8	.7	39	.67	518.9	.2	5.7	3.4	5	<.1	3.8	4.2	2	.02	.003	11	15	.03	48	.001	6	.25	.005	.18	.3	<.01	.5	.1	<.05	<1	<.5
404963	.1	8.8	.8	2	<.1	2.5	2.0	30	.51	456.5	.1	3.4	1.6	2	<.1	1.1	.4	2	.01	.002	3	16	.01	33	.001	3	.08	.004	.06	.2	<.01	.3	.1	<.05	<1	<.5
404964	.3	3.2	.6	1	<.1	1.6	.5	29	.44	274.3	<.1	4.6	.1	1	<.1	.7	.5	<1	<.01	<.001	<1	18	<.01	8	<.001	1	.01	.002	<.01	.3	.01	<.1	<.1	<.05	<1	<.5
404965	.2	74.3	5.8	10	.2	3.8	1.6	49	2.35	1547.0	.7	16.2	6.1	17	.1	3.0	2.1	6	.03	.021	14	24	.16	43	.002	1	.45	.013	.17	.1	<.01	.7	.2	<.05	2	2.0
404966	.3	26.4	8.1	16	.1	9.2	6.5	93	3.49	>10000	.9	174.2	12.2	18	.1	10.2	33.9	12	.02	.014	18	28	.43	223	.006	3	1.20	.021	.40	.1	<.01	1.4	.4	.65	4	13.3
404967	.3	34.9	7.3	47	.1	19.4	8.3	200	3.41	137.8	2.4	11.0	26.8	59	<.1	1.4	1.1	36	.56	.041	32	40	.96	136	.121	1	2.81	.165	1.15	.1	<.01	4.6	1.0	.14	10	<.5
404968	.4	97.6	3.5	14	.2	22.3	10.1	209	2.23	223.3	.6	3.3	5.6	49	<.1	.9	1.1	9	1.10	.014	6	25	.27	41	.020	1	.88	.077	.29	.2	<.01	1.6	.3	.37	3	<.5
404969	.2	4.8	.4	3	<.1	7.1	6.8	27	.37	741.0	.1	8.7	.1	1	<.1	5.5	.1	1	.01	.002	<1	17	<.01	3	.001	<1	.03	.002	.01	.1	<.01	.2	<.1	<.05	<1	<.5
404970	.7	26.5	3.0	86	.1	41.6	14.0	280	4.42	14.8	1.5	2.5	13.0	15	.1	6.4	.1	17	.04	.060	46	31	.76	63	.008	3	2.04	.028	.27	.2	<.01	2.2	.1	<.05	6	<.5
RE 404970	.7	26.4	3.3	89	.1	41.8	13.9	272	4.23	31.0	1.6	2.5	13.7	16	.1	6.9	.2	16	.04	.062	49	31	.74	66	.008	1	2.00	.029	.28	.2	<.01	2.3	.1	<.05	6	<.5
404971	.3	21.6	6.7	55	<.1	29.3	11.7	467	2.90	46.0	.8	2.1	7.9	198	.1	.5	.4	15	4.57	.065	23	26	.83	71	.048	1	1.59	.031	.55	.1	<.01	2.3	.5	<.05	5	<.5
404972	1.3	17.3	6.8	97	<.1	20.0	12.9	641	3.58	21.7	4.0	1.6	16.3	104	.1	.7	.3	124	2.11	.081	27	158	1.92	774	.274	1	3.04	.148	1.51	.8	.01	14.8	1.0	.13	10	<.5
404973	.4	37.1	4.4	37	<.1	21.2	7.4	248	2.62	65.3	.7	1.2	8.0	14	<.1	.8	.4	17	.11	.024	14	29	.58	153	.028	<1	1.38	.023	.42	.2	.01	2.1	.5	<.05	4	<.5
404974	.4	74.4	3.4	74	<.1	21.1	7.0	509	6.28	88.1	.5	<.5	3.5	8	.1	3.0	.1	32	.05	.014	6	20	1.52	115	.008	3	2.80	.058	.06	.1	<.01	3.9	<.1	<.05	10	.5
404975	.2	4.0	5.0	9	<.1	4.7	2.1	2037	.46	38.6	.1	<.5	3.7	83	.1	.3	<.1	2	2.97	.011	8	9	.05	54	.005	<1	.14	.010	.04	.1	.01	.5	.1	<.05	1	<.5
404976	.1	43.0	3.3	16	<.1	20.3	9.5	727	1.09	94.3	.3	2.3	3.7	195	.1	2.1	.7	2	2.63	.014	13	12	.09	34	.001	2	.25	.008	.08	.1	<.01	.8	.1	<.05	1	.5
404977	.3	70.2	3.2	33	.1	9.2	4.9	84	2.67	301.5	2.2	2.0	25.4	126	.1	1.4	.7	17	.11	.030	45	28	.54	112	.080	1	1.49	.030	.95	.2	<.01	1.9	.9	.18	5	<.5
404978	.2	14.3	5.1	2	<.1	2.7	.7	38	.59	108.5	.1	<.5	.4	1	<.1	.8	1.5	1	.02	.006	1	16	.02	23	.001	<1	.04	.002	.01	.2	<.01	.2	<.1	.07	<1	<.5
404979	2.0	23.8	15.3	10	.1	8.0	4.5	228	1.32	1595.1	.3	3.1	7.9	5	.4	14.9	2.9	4	.04	.010	16	12	.04	119	.002	2	.24	.020	.15	<.1	.01	.9	.1	<.05	1	.6
404980	.4	79.2	10.5	23	.5	7.7	2.8	64	3.07	>10000	2.7	35.8	16.0	10	.7	16.9	16.4	10	.02	.023	20	16	.24	353	.002	5	.92	.016	.31	.1	.01	1.4	.5	.12	3	2.3
404981	.2	11.8	5.2	1	.2	1.6	.7	36	.60	411.1	.1	9.5	.2	2	<.1	2.6	7.9	1	<.01	.001	<1	16	<.01	15	<.001	3	.03	.003	.01	.2	.01	.2	.1	<.05	<1	<.5
404982	.9	57.7	32.7	5	.8	12.7	8.1	51	3.62	>10000	1.2	273.4	10.2	26	.6	60.6	75.1	3	.03	.023	17	15	.08	194	.002	6	.55	.020	.34	.3	.02	.8	.4	.88	2	20.0
404984	.2	2.4	.3	1	<.1	1.9	1.1	32	.45	556.0	<.1	4.7	.1	3	<.1	.8	.5	3	.05	.023	1	20	<.01	3	<.001	2	.02	.002	.01	.2	.01	.2	<.1	<.05	<1	<.5
STANDARD DS7	20.6	108.5	73.5	411	.9	54.3	9.6	625	2.39	48.3	5.1	68.1	4.6	72	6.3	6.2	4.7	84	.93	.080	12	158	1.05	370	.123	39	.96	.075	.43	3.9	.20	2.4	4.2	.22	5	3.6

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	7.9	269.4	558	10.1	5.8	4.2	563	2.07	215.1	2.9	1.2	4.4	77	6.1	129.2	.1	37	.59	.074	9	16	.58	213	.140	2	1.12	.121	.51	.3	.04	2.6	.3	<.05	5	<.5
404985	.7	61.6	233.9	766	2.5	12.8	10.5	113	4.18	>10000	1.0	171.3	9.3	15	10.1	76.3	32.1	16	.05	.011	12	32	.61	100	.018	3	1.37	.024	.19	.2	.06	2.2	.3	1.14	4	18.6
404986	.2	11.9	33.3	57	.2	5.3	1.3	48	.93	197.0	.7	5.2	7.7	3	.6	9.7	.4	5	.01	.013	14	16	.06	38	.002	3	.40	.024	.12	<.1	.01	.6	.1	<.05	1	.8
404987	.2	37.3	19.7	38	.6	4.7	1.6	47	2.08	2149.2	.6	19.5	8.8	8	.5	6.2	1.5	7	.01	.014	21	17	.10	102	.002	5	.54	.021	.23	<.1	.02	1.2	.2	<.05	1	2.1
404988	.3	85.8	17.9	58	.2	39.4	13.8	222	2.09	320.4	1.2	6.1	8.4	119	.4	4.0	3.0	14	1.62	.022	17	21	.37	45	.012	2	.86	.009	.18	.1	.01	1.6	.1	<.05	2	<.5
404989	.1	26.3	10.5	32	.2	12.5	4.3	116	1.79	1184.5	1.3	6.4	9.0	14	.1	3.6	.6	13	.06	.012	15	23	.44	77	.006	3	1.05	.024	.24	<.1	<.01	1.4	.3	<.05	3	.5
404990	.3	8.5	14.6	14	<.1	4.3	1.8	41	.62	83.8	.3	.6	10.4	4	.1	4.2	.2	2	.03	.009	20	11	.04	111	.002	3	.31	.019	.19	<.1	.01	.3	.1	<.05	1	<.5
404991	.2	3.4	4.4	8	.1	2.6	1.7	32	.42	390.6	<.1	3.1	.1	1	.1	2.5	.2	1	.01	.001	<1	22	<.01	2	<.001	<1	.02	.002	.01	<.1	<.01	.1	<.1	<.05	<1	<.5
404992	.2	54.6	11.1	31	.2	25.3	9.8	620	2.35	187.0	1.0	2.4	11.8	141	.2	1.6	2.6	19	5.70	.018	16	28	.51	79	.039	2	1.44	.085	.31	.1	.01	2.9	.3	.07	5	.7
404993	.8	15.1	25.9	9	2.5	7.9	28.3	158	13.79	>10000	2.2	1907.0	10.2	455	.2	203.5	285.0	4	1.96	.010	17	9	.11	49	.005	2	.46	.016	.47	13.8	.02	1.1	.2	2.00	1	75.7
404994	1.2	17.5	91.2	7	4.6	33.3	74.4	23	31.73	>10000	.8	5428.0	.4	19	.3	607.5	595.8	<1	.09	.003	1	3	.01	23	.001	<1	.06	.002	.02	2.8	.15	<.1	.1	9.08	<1	>100
404995	.2	17.1	9.2	21	.2	13.8	4.9	357	1.56	1434.7	.8	16.5	19.7	31	.2	2.7	2.9	11	1.06	.014	32	17	.28	119	.005	2	.77	.035	.21	<.1	<.01	2.3	.1	<.05	2	.7
404996	.3	86.0	13.2	25	.3	20.7	11.4	481	3.53	>10000	1.1	285.6	11.8	61	.2	18.5	28.1	17	2.08	.022	18	21	.39	123	.011	2	1.14	.056	.20	.2	.01	2.5	.2	.62	3	7.7
404997	.3	122.8	10.6	45	.2	29.3	10.5	414	3.63	386.8	1.7	56.8	18.5	86	.2	1.8	1.7	32	1.06	.026	32	36	.62	123	.058	1	2.63	.196	.60	.2	.01	4.3	.5	.08	9	1.1
404998	.2	14.3	12.1	11	.1	4.9	2.1	120	.90	1415.8	.4	27.9	11.4	8	.2	3.0	2.5	2	.13	.010	22	11	.04	97	.002	2	.41	.027	.20	.1	.01	.5	.1	<.05	1	.8
405000	.1	9.0	11.5	17	<.1	9.6	4.1	224	1.04	359.6	.4	6.3	17.4	11	.1	2.7	.3	6	.09	.011	31	13	.14	77	.007	5	.60	.044	.20	<.1	.01	1.2	.1	<.05	2	<.5
405001	.2	17.3	21.7	7	.7	5.2	2.5	95	1.03	5630.1	.6	38.9	7.2	31	.1	7.3	12.0	2	.16	.021	15	10	.03	76	.002	4	.31	.025	.19	.1	.01	.7	.1	.08	1	1.6
405002	2.1	60.8	86.6	12	5.4	7.8	13.8	117	13.01	>10000	1.5	2163.0	6.2	343	.4	155.9	119.3	11	.77	.013	13	9	.15	59	.002	2	.47	.015	.30	>100	<.01	1.0	.2	3.18	2	41.8
405003(pulp)	.5	25.2	6.0	40	<.1	30.4	7.8	357	1.91	13.2	.8	5.7	4.5	65	.3	.6	.1	42	3.06	.098	15	36	.75	163	.073	1	.79	.025	.07	.2	.03	2.8	.1	<.05	3	<.5
405004	.2	51.0	5.3	10	<.1	4.5	2.4	49	1.24	598.5	.5	4.4	11.2	5	.1	2.3	.6	6	.02	.009	23	13	.11	61	.003	2	.42	.034	.16	.3	<.01	.7	.1	<.05	1	.8
405005	4.1	34.2	115.9	6	10.2	2.3	7.3	43	11.19	>10000	.7	2048.0	3.0	37	.7	249.1	112.0	2	.03	.008	5	6	.02	31	.001	2	.17	.004	.12	70.9	<.01	.4	.1	2.45	1	83.6
405006	.3	56.6	3.8	6	<.1	4.1	2.2	55	1.01	938.4	.3	21.3	4.8	4	.1	3.6	1.4	5	.02	.006	12	13	.03	26	.001	2	.20	.011	.07	.3	<.01	.5	<.1	<.05	<1	<.5
RE 405006	.2	59.1	3.7	7	<.1	4.4	2.3	54	.99	802.8	.3	22.4	5.0	4	.1	3.6	1.4	4	.02	.006	12	14	.03	27	.001	2	.19	.011	.08	.3	.01	.4	<.1	<.05	1	.5
405007	.7	93.3	79.6	43	2.1	11.9	19.9	98	12.49	>10000	.7	2871.0	7.0	189	.1	109.7	495.9	11	.10	.015	14	15	.19	35	.006	1	.78	.033	.19	94.9	.02	1.7	.1	3.83	3	66.8
405008	.2	435.8	11.7	24	.4	30.2	10.8	180	5.55	3547.1	1.4	103.0	17.3	122	.1	3.1	12.8	42	1.37	.026	14	42	.85	142	.030	2	5.17	.380	.32	11.8	.01	5.3	.4	1.15	17	11.3
405009	.2	128.7	27.3	26	.4	17.4	6.7	141	2.72	943.2	1.1	19.6	11.0	22	.1	2.0	25.3	12	.10	.012	13	19	.32	83	.013	1	1.01	.054	.28	.6	.01	1.7	.2	.07	3	1.0
405010	.3	560.9	15.8	17	2.4	33.6	33.5	105	5.79	>10000	1.1	586.0	15.6	80	.2	7.6	76.6	29	.67	.064	18	25	.51	79	.018	3	3.57	.164	.20	14.4	.02	4.3	.2	1.62	12	13.5
405011	.5	260.7	8.4	22	.4	17.7	7.5	132	4.87	3632.0	1.4	263.2	20.9	85	.1	4.1	40.5	28	.77	.043	23	30	.58	126	.033	2	3.00	.227	.38	1.3	.01	3.5	.3	1.08	9	5.3
STANDARD DS7	21.2	108.9	72.6	413	.9	55.5	9.8	629	2.40	49.7	5.1	67.7	4.6	72	6.4	6.1	4.8	86	.93	.080	12	164	1.07	376	.127	40	.98	.074	.44	3.9	.20	2.5	4.2	.23	4	3.9

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ___

ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.) 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A603661 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.8	2.3	52	<.1	7.1	4.7	615	2.14	<.5	2.6	<.5	4.1	61	<.1	<.1	<.1	41	.63	.099	7	69	.68	224	.128	<1	.99	.066	.50	<.1	<.01	1.9	.3	.11	5	<.5
404678	.8	11.3	8.9	48	<.1	12.8	5.7	229	2.32	83.7	.7	5.4	1.3	9	.2	1.2	.8	37	.07	.035	12	19	.32	75	.025	1	1.15	.005	.05	.3	.02	1.2	.2	<.05	4	1.0
404679	1.0	29.8	18.4	82	.3	18.7	8.8	491	2.68	610.8	1.1	94.0	1.4	20	.8	5.9	7.0	35	.13	.063	16	19	.36	144	.019	3	1.30	.008	.06	.8	.03	1.3	.2	.07	4	.6
404680(pulp)	.6	24.2	5.5	38	<.1	30.3	8.0	350	1.93	8.9	.8	3.8	4.3	61	.3	.6	.1	39	2.82	.094	13	34	.79	173	.076	<1	.86	.027	.07	.3	.03	2.5	.1	.12	3	<.5
404681	1.2	14.1	12.0	68	<.1	15.6	7.4	332	2.69	133.8	.7	9.8	2.3	14	.3	1.2	.9	49	.12	.042	13	25	.38	104	.035	<1	1.54	.006	.05	.5	.03	1.6	.2	<.05	5	.9
404682	.8	14.2	10.4	47	<.1	13.9	6.5	264	2.19	131.6	.9	26.1	1.3	16	.2	1.1	1.0	41	.19	.040	14	21	.33	117	.031	1	1.25	.006	.06	.6	.02	1.2	.2	<.05	4	<.5
404683	.7	28.8	13.9	67	.1	21.2	10.6	321	2.74	273.0	.9	72.6	5.5	38	.4	3.7	3.0	35	.17	.043	17	22	.41	129	.037	1	1.61	.007	.09	.6	.03	1.9	.2	<.05	5	.5
404684	.7	25.1	7.3	56	.2	18.3	6.9	193	2.20	166.0	1.0	21.9	1.6	17	.2	2.6	1.3	31	.15	.050	15	18	.35	113	.027	1	1.17	.006	.07	.7	.03	1.2	.2	<.05	4	<.5
404685	.8	14.9	8.2	49	<.1	12.6	5.2	139	2.06	60.9	.9	15.7	1.1	13	.1	1.0	.8	35	.11	.037	14	19	.33	111	.026	<1	1.21	.006	.05	.5	.02	1.2	.1	<.05	4	.8
404686	.5	46.0	14.3	77	.2	26.4	12.9	424	3.26	1166.2	2.1	67.4	8.0	35	.5	8.0	5.2	23	.40	.073	32	21	.44	112	.018	2	1.26	.012	.12	1.6	.03	2.1	.2	<.05	4	.9
404687	.6	52.0	25.1	155	.3	30.8	16.5	870	3.75	1555.1	2.5	52.5	6.9	89	2.3	5.4	8.0	35	1.10	.081	32	30	.54	127	.038	28	2.00	.030	.20	.7	.04	3.0	.3	<.05	8	1.5
404688	.6	31.1	29.1	60	.5	19.2	8.9	364	2.61	1121.5	1.5	60.3	2.5	25	.3	14.2	5.5	33	.27	.060	21	20	.37	155	.019	2	1.25	.007	.08	.7	.03	1.8	.2	<.05	4	.5
404689	.7	20.0	10.1	46	.2	15.3	5.2	137	2.18	161.2	1.2	10.6	.7	12	.1	3.1	.9	33	.10	.055	14	21	.34	111	.020	1	1.14	.006	.07	.6	.04	1.0	.2	<.05	4	1.0
404690	.7	21.3	12.1	58	.1	18.1	8.2	331	2.27	265.7	.9	15.3	3.2	13	.2	3.7	1.3	29	.15	.058	16	20	.38	97	.028	1	1.01	.005	.07	.9	.01	1.6	.1	<.05	3	<.5
404691	.8	17.1	8.6	54	<.1	15.7	7.0	250	2.21	154.2	.9	9.1	1.7	13	.3	1.5	1.1	36	.14	.062	17	20	.32	104	.029	1	1.04	.006	.06	.5	.02	1.4	.1	<.05	4	.7
404692	1.3	28.7	17.8	57	.1	14.4	6.8	201	2.53	210.9	1.6	5.1	1.5	18	.3	1.7	2.0	39	.06	.092	24	22	.30	106	.031	2	1.36	.009	.10	.3	.02	1.4	.2	<.05	5	1.1
404693	1.0	39.4	10.4	73	<.1	23.7	11.6	314	2.74	494.7	1.4	24.9	5.9	23	.3	3.8	3.4	39	.17	.067	22	24	.46	139	.044	<1	1.35	.007	.14	.8	.03	2.3	.3	<.05	4	1.0
404694	.7	25.7	10.1	59	<.1	19.9	10.0	308	2.50	120.3	1.3	8.3	3.4	20	.2	1.0	1.3	34	.14	.063	20	22	.42	162	.035	<1	1.33	.006	.10	.3	.02	1.8	.2	<.05	4	.6
404695	.7	24.6	9.7	61	<.1	21.1	11.6	331	2.55	323.4	1.2	7.1	5.0	26	.3	1.7	2.6	33	.17	.081	20	20	.37	143	.036	1	1.04	.006	.11	.4	.02	1.6	.2	<.05	3	.7
404696	1.1	26.1	10.6	74	<.1	22.7	8.6	295	2.97	221.8	1.3	5.5	1.3	12	.2	2.6	.9	41	.08	.063	19	26	.44	118	.031	2	1.49	.006	.11	.2	.03	1.4	.2	<.05	5	1.0
404697	.9	22.8	8.8	56	<.1	21.8	12.8	364	2.47	114.3	1.1	8.2	3.5	41	.2	1.5	.9	34	.15	.068	17	20	.36	110	.032	<1	1.18	.006	.09	.3	.02	1.7	.1	<.05	4	<.5
404698	.8	16.7	10.0	47	<.1	17.6	6.1	160	2.55	180.7	.9	5.4	2.4	15	.2	2.1	.9	39	.09	.040	17	22	.33	85	.032	1	1.27	.006	.07	.3	.03	1.5	.2	<.05	4	.6
404699	1.1	32.9	12.6	95	.1	28.2	11.2	388	3.62	413.3	1.6	9.9	3.3	16	.2	8.2	1.9	38	.12	.061	23	26	.43	120	.025	2	1.41	.006	.10	.5	.02	1.9	.2	<.05	5	.8
404700	.7	18.6	9.9	68	<.1	18.5	11.1	438	2.48	73.1	1.3	14.1	3.4	12	.3	1.4	.6	37	.12	.060	19	22	.38	160	.033	1	1.18	.005	.07	.5	.02	2.1	.1	<.05	3	.6
404796	.7	29.8	126.3	128	.5	27.8	11.1	446	2.73	215.9	1.2	3.0	4.5	16	2.7	39.2	.8	33	.17	.050	25	22	.40	171	.022	1	1.26	.005	.09	.2	.02	2.1	.2	<.05	4	.6
404797	.9	20.6	91.4	93	.1	20.7	10.3	372	2.41	129.4	1.3	2.6	3.6	19	1.4	24.0	.6	41	.18	.071	17	30	.42	125	.040	2	1.23	.006	.08	.3	.02	2.3	.2	<.05	3	.5
RE 404797	1.0	21.4	90.6	93	.1	22.5	11.2	385	2.52	131.1	1.3	4.6	3.5	19	1.3	23.9	.6	42	.17	.072	17	31	.44	124	.041	2	1.27	.006	.07	.4	.02	2.4	.2	<.05	4	.6
404798	.7	24.5	45.2	95	.3	25.6	10.7	420	2.83	142.2	1.2	3.1	5.8	18	.9	8.1	.6	37	.15	.056	23	29	.47	169	.035	1	1.37	.006	.09	.3	.02	2.3	.2	<.05	4	.5
404799	1.1	16.5	20.8	64	<.1	17.8	6.8	282	2.82	102.2	.8	5.9	2.6	17	.4	4.4	.6	54	.14	.048	16	42	.55	149	.064	1	1.43	.006	.09	.3	.02	2.8	.2	<.05	5	.6
404800	.8	21.4	33.3	78	.2	21.7	9.0	322	2.78	88.4	1.0	3.3	4.2	16	.4	3.9	.6	50	.15	.052	19	38	.55	134	.052	1	1.52	.006	.10	.3	.02	2.8	.2	<.05	5	.8
404823	.8	22.3	22.3	61	.1	21.4	9.1	270	2.89	224.7	1.2	4.3	1.9	17	.4	4.3	.7	39	.16	.059	23	25	.37	120	.018	1	1.29	.007	.09	.1	.03	1.8	.2	<.05	4	.7
404824	.8	35.7	10.2	54	<.1	26.6	12.6	311	3.12	269.2	2.6	8.3	7.1	14	.4	2.9	1.1	29	.08	.048	41	19	.33	126	.018	1	1.19	.005	.06	.1	.02	2.3	.2	<.05	4	<.5
404825	.6	20.9	29.7	95	<.1	23.8	11.8	420	2.61	190.1	1.1	6.0	2.8	11	1.4	4.5	1.4	31	.09	.040	26	20	.35	115	.025	1	1.40	.005	.12	.2	.02	1.8	.4	<.05	5	1.2
404826	.6	16.1	10.3	48	<.1	16.2	6.8	228	1.99	37.2	.8	2.0	2.9	10	.2	1.2	.2	30	.10	.047	15	17	.34	82	.025	2	1.10	.004	.05	.2	.02	1.7	.1	<.05	3	.5
404827	.6	18.8	10.9	61	<.1	20.4	8.1	258	2.14	87.8	.7	2.4	3.6	14	.2	1.1	.6	33	.14	.045	15	20	.36	89	.030	1	1.18	.006	.07	.2	.02	1.7	.1	<.05	4	<.5
STANDARD DS7	20.1	106.4	68.6	394	.9	54.1	9.0	618	2.33	49.5	4.8	65.5	4.4	69	6.2	5.8	4.4	83	.92	.078	12	160	1.05	365	.120	38	.97	.076	.43	3.8	.19	2.5	4.2	.21	5	3.8

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILI
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

Data ✓ FA ____ DATE RECEIVED: JUL 13 2006 DATE REPORT MAILED: 2006-08-02 A10:43

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.5	2.6	49	<.1	6.3	4.6	551	1.85	<.5	2.9	<.5	4.5	57	<.1	<.1	.1	38	.59	.096	6	63	.65	208	.125	2	.95	.059	.49	<.1	<.01	1.9	.4	<.05	4	<.5
404828	.7	19.7	8.8	48	<.1	21.8	10.9	296	2.14	232.8	.7	6.3	5.1	20	.3	1.4	1.4	26	.13	.041	13	17	.33	110	.026	1	1.09	.006	.07	.3	.02	1.8	.2	<.05	3	.5
404829	.6	56.5	43.6	75	.4	24.0	16.6	432	3.67	1935.2	1.8	31.2	10.8	40	1.9	11.4	15.3	24	.10	.051	25	23	.51	216	.043	1	1.51	.019	.26	.7	.02	2.4	.5	.12	4	.6
404830	.7	26.2	11.7	61	.3	19.8	8.6	297	2.27	311.0	1.2	23.0	5.9	17	.7	2.0	1.7	27	.16	.061	16	19	.40	134	.028	1	1.12	.006	.10	.5	.02	1.8	.2	<.05	3	.7
404831	.8	28.4	24.5	86	.4	23.2	7.3	226	2.67	461.3	1.4	7.2	2.8	16	.8	3.9	3.6	33	.12	.056	18	25	.50	154	.025	1	1.62	.008	.14	.2	.04	2.0	.4	<.05	5	.6
404832	.8	33.9	24.6	76	.4	24.8	10.8	464	2.78	387.4	1.4	9.2	2.5	21	.5	6.7	2.8	36	.25	.061	20	27	.47	140	.026	1	1.66	.010	.12	.5	.03	2.2	.3	<.05	5	.9
404833	.7	42.6	19.6	82	.4	25.3	10.3	482	2.75	396.9	1.3	23.2	7.1	47	1.0	4.2	4.0	38	.53	.069	21	27	.50	140	.043	2	1.53	.045	.15	1.3	.04	2.9	.4	<.05	5	.7
404834	.8	28.1	12.9	72	.3	23.2	9.9	410	2.68	289.3	1.4	14.2	2.5	21	.2	2.3	2.4	38	.25	.058	16	29	.53	146	.035	2	1.71	.008	.12	.4	.03	2.2	.3	<.05	5	.5
404835	.7	20.7	16.2	69	.2	18.8	9.1	401	2.52	128.4	1.6	7.0	2.9	26	.2	2.4	1.2	46	.36	.053	15	38	.53	179	.035	3	1.46	.010	.07	.4	.04	3.4	.2	<.05	5	.8
RE 404835	.7	19.3	17.1	65	.2	18.2	9.2	420	2.56	122.8	1.6	3.8	3.0	27	.3	2.4	1.2	45	.36	.053	15	37	.54	185	.032	3	1.46	.011	.07	.4	.04	3.3	.2	<.05	4	.8
404836	.5	27.2	15.0	86	.3	23.0	10.1	453	2.71	65.9	1.6	4.1	6.1	53	.9	1.3	.6	43	.90	.057	21	39	.67	242	.063	3	2.04	.060	.15	.7	.03	3.9	.3	<.05	6	1.0
404837	.6	35.6	25.7	84	.5	25.7	11.6	552	3.12	107.2	1.4	18.1	6.6	64	.9	2.9	3.1	41	.95	.060	31	31	.57	202	.045	3	2.03	.059	.12	.7	.04	3.8	.2	<.05	6	1.2
404838	.6	24.2	18.5	72	.3	27.1	10.6	353	2.91	100.5	1.1	9.6	9.7	25	.4	2.2	2.6	34	.25	.043	29	27	.53	157	.056	1	1.65	.013	.19	.5	.03	2.9	.3	<.05	5	.5
404839	.7	30.3	40.4	83	.5	27.5	12.2	518	2.97	195.7	1.8	17.6	7.6	50	.6	3.7	2.5	38	.61	.077	30	28	.55	150	.039	2	1.87	.048	.13	.5	.04	3.5	.2	<.05	6	<.5
404840	.5	22.2	6.2	37	<.1	30.5	8.2	345	1.87	7.4	.8	2.3	4.8	73	.3	.6	.1	44	3.15	.093	13	36	.78	170	.082	2	.85	.024	.08	.3	.02	3.2	.1	<.05	3	.5
404841	.4	27.9	16.8	77	.4	26.0	10.0	348	2.78	203.9	.9	21.9	7.7	23	.4	4.9	5.8	29	.45	.056	29	19	.42	136	.039	2	1.18	.009	.15	.5	.03	2.6	.2	<.05	4	.9
404842	.8	36.2	12.4	52	.3	19.8	7.6	306	2.69	444.6	1.4	66.3	5.4	29	.3	2.1	9.2	30	.35	.057	22	22	.40	166	.024	<1	1.22	.010	.09	1.0	.03	2.3	.2	<.05	4	.9
404843	.8	21.9	11.2	49	.1	18.5	8.2	275	2.38	220.4	1.1	10.6	1.5	13	.2	2.1	2.0	35	.12	.054	18	19	.29	171	.016	<1	1.17	.005	.05	.4	.03	1.5	.2	<.05	4	.5
404844	.9	41.1	11.6	67	.1	30.3	15.0	473	3.07	528.0	1.6	14.1	5.0	16	.2	5.4	3.4	28	.12	.070	22	20	.35	107	.011	1	1.18	.005	.06	.4	.03	1.8	.2	<.05	3	.8
404845	1.0	23.4	10.8	48	<.1	17.5	6.4	199	2.42	354.3	1.1	28.5	1.2	12	.2	2.8	2.6	34	.07	.055	20	19	.29	102	.014	1	1.10	.006	.07	.5	.03	1.2	.2	<.05	4	1.1
404846	.7	14.2	9.1	42	<.1	14.9	5.5	168	2.16	110.1	1.0	4.0	.9	11	.2	1.3	.8	35	.11	.047	15	20	.33	90	.020	<1	1.07	.004	.05	.3	.03	1.4	.1	<.05	3	.6
404847	.7	20.4	8.9	50	<.1	17.6	8.2	238	2.16	196.8	.8	10.6	2.9	9	.2	4.8	1.7	26	.09	.053	16	16	.29	99	.017	1	1.06	.004	.05	.4	.04	1.8	.2	<.05	3	.8
404848	.5	32.1	37.3	77	.3	25.6	9.9	323	3.41	221.0	1.5	45.6	12.2	23	.5	14.6	3.7	16	.48	.058	39	17	.41	82	.010	1	1.13	.005	.11	.4	.02	2.1	.2	<.05	3	.6
404849	.9	25.1	9.0	54	<.1	21.2	9.0	237	2.55	331.5	1.3	4.7	4.0	10	.3	1.6	1.3	31	.09	.057	19	20	.44	82	.019	<1	1.30	.005	.05	.3	.03	1.7	.1	<.05	3	1.1
404850	.9	86.6	13.8	65	.2	40.4	23.0	859	3.29	2093.8	2.1	23.2	9.3	26	.4	4.2	8.7	42	.22	.086	24	28	1.11	290	.053	1	2.15	.010	.35	2.2	.03	4.6	.6	<.05	6	1.1
404851	.7	16.2	32.8	69	.2	20.1	7.6	294	2.48	79.0	1.0	3.0	3.7	13	.4	4.1	.6	42	.13	.046	16	34	.52	124	.040	1	1.49	.005	.08	.3	.02	2.6	.2	<.05	4	.7
404852	.7	20.1	22.1	63	.3	22.6	9.2	335	2.58	90.0	.8	3.2	4.6	13	.3	4.1	1.0	34	.16	.046	17	24	.42	137	.027	1	1.32	.005	.08	.3	.03	2.3	.2	<.05	4	1.3
404853	.7	20.3	27.9	68	.2	24.1	8.9	357	2.89	111.0	1.0	2.7	4.0	13	.4	5.5	.7	32	.16	.051	23	23	.40	203	.019	1	1.47	.004	.09	.2	.04	2.1	.2	<.05	4	.9
404854	.7	29.6	64.7	140	.6	32.1	14.8	783	2.87	262.5	1.0	10.6	10.9	18	2.8	39.1	.8	17	.28	.051	36	14	.26	192	.010	1	.93	.005	.10	.2	.04	3.3	.1	<.05	2	.6
404855	.3	22.0	53.2	75	.4	24.5	9.3	339	2.66	137.1	1.0	12.5	10.9	21	.7	19.3	.4	23	.43	.057	31	20	.43	136	.038	1	1.15	.006	.18	.2	.03	2.9	.3	<.05	3	.5
404856	.3	35.2	36.7	123	.4	36.0	15.7	711	3.37	203.0	1.0	11.8	13.0	54	2.7	13.5	3.5	29	1.88	.089	35	24	.64	153	.023	1	1.71	.011	.24	.2	.03	3.5	.4	<.05	6	.7
404857	.3	24.7	23.5	88	.4	24.4	9.6	340	2.68	105.0	.8	4.3	7.5	62	1.7	5.3	1.2	29	1.51	.056	25	22	.49	132	.031	1	1.32	.029	.16	.3	.04	2.7	.2	<.05	4	.6
404858	.4	35.4	47.0	100	.5	31.8	13.4	537	3.18	176.8	1.2	6.5	15.1	25	1.9	10.6	2.5	26	.54	.055	44	25	.57	113	.026	2	1.55	.010	.28	.2	.01	3.1	.3	<.05	5	.6
404859	1.0	57.1	16.5	69	.3	26.6	14.6	381	3.34	401.7	1.6	26.2	8.3	13	.5	5.1	3.5	31	.11	.079	31	22	.38	97	.017	2	1.22	.004	.12	1.0	.03	2.0	.4	<.05	4	1.1
404860	1.1	49.6	14.4	76	.1	31.8	15.5	410	3.18	249.8	1.9	13.3	8.6	12	.3	3.8	1.4	31	.10	.068	32	22	.43	104	.019	1	1.28	.005	.09	.4	.03	1.9	.2	<.05	4	.8
STANDARD DS7	20.1	111.0	68.5	405	.9	55.0	9.5	615	2.33	47.0	4.8	69.9	4.3	66	6.2	5.7	4.4	84	.90	.078	11	160	1.06	360	.120	40	.96	.073	.43	3.7	.20	2.4	4.1	.20	4	3.6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data K FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.3	2.4	47	<.1	6.8	4.6	612	2.01	<.5	2.4	2.2	4.4	59	<.1	<.1	.1	41	.65	.095	6	68	.67	229	.130	1	.94	.063	.51	.1	<.01	2.1	.3	<.05	5	<.5
404861	.8	35.3	11.3	63	.1	22.2	9.5	319	2.80	168.9	1.3	16.5	3.2	8	.3	3.6	1.1	27	.07	.053	26	18	.32	66	.011	2	.94	.005	.06	.5	.02	1.2	.2	<.05	3	<.5
404862	.8	45.7	11.1	56	.1	24.3	12.6	352	2.79	752.8	1.5	39.1	4.1	13	.2	1.9	7.0	27	.12	.057	21	20	.38	123	.016	1	1.05	.005	.08	.9	.03	1.6	.2	<.05	3	.5
404863	.9	45.8	12.2	62	<.1	26.3	13.7	423	2.96	561.0	1.5	15.3	3.9	12	.2	2.4	2.0	29	.09	.054	25	23	.43	94	.015	2	1.18	.005	.09	.4	.02	1.3	.2	<.05	3	.9
404864	.5	52.0	11.3	70	.1	30.0	14.8	497	3.31	563.6	1.9	21.4	8.8	20	.2	7.2	2.1	19	.12	.058	31	16	.41	85	.009	1	1.02	.005	.07	.3	.01	1.2	.1	<.05	3	<.5
404865	.5	108.7	256.4	243	.8	83.5	41.1	1021	5.01	1236.0	3.6	151.1	22.5	37	4.3	169.1	3.9	7	.04	.052	47	12	.34	69	.002	1	1.00	.006	.12	.1	.03	1.4	.2	.10	2	<.5
404866	.4	58.3	19.2	79	.2	35.1	14.2	395	3.66	799.8	1.9	27.9	10.7	13	.3	12.9	1.5	13	.05	.046	39	14	.37	59	.004	1	.94	.004	.08	.2	.02	1.2	.2	<.05	3	.5
404867	.5	18.6	60.4	44	.3	11.9	3.6	107	1.67	300.2	.9	17.6	.3	11	.7	27.7	1.4	18	.04	.040	23	10	.17	90	.004	1	.78	.004	.08	.2	.03	.4	.2	<.05	3	.5
404868	.7	25.6	38.6	57	.3	13.4	7.5	264	2.79	1357.6	1.0	112.9	9.6	21	.5	18.1	6.5	23	.05	.036	23	15	.26	92	.015	<1	.91	.008	.11	.2	.02	1.3	.2	.10	3	.7
404869	.7	12.8	20.8	38	<.1	11.9	5.6	251	1.87	404.6	.7	27.3	2.9	10	.2	6.2	1.2	25	.06	.037	17	12	.21	75	.015	<1	.74	.004	.08	.2	.02	.9	.1	<.05	3	.6
404870	11.0	1310.5	5.3	47	.3	385.2	15.9	511	3.82	15.4	.3	106.7	1.4	65	.1	1.7	.2	56	1.11	.057	4	531	.74	134	.089	4	1.33	.110	.21	1.2	.23	3.4	.1	.91	4	2.9
404871	.8	18.1	21.7	47	.3	12.3	4.5	187	1.87	326.3	.9	51.1	.9	14	.5	10.7	2.2	26	.08	.039	17	13	.32	91	.010	1	.89	.005	.08	.2	.03	.9	.2	<.05	3	<.5
404872	1.9	119.5	6.7	84	.2	39.6	24.5	918	4.40	154.4	1.8	52.9	15.9	99	.6	4.4	4.8	55	.72	.052	39	41	2.02	164	.091	1	3.58	.067	.78	.4	.01	4.0	1.0	.11	9	.8
404873	1.1	84.6	35.3	158	.8	44.3	22.0	1104	4.27	595.5	2.1	91.8	16.8	30	1.4	142.3	3.8	43	.48	.057	50	31	1.26	120	.049	1	1.96	.024	.34	.2	.01	4.4	.6	<.05	6	<.5
404874	2.1	63.9	48.4	143	1.0	42.4	16.7	1270	4.25	939.2	1.7	63.1	12.3	35	1.3	38.6	6.3	66	.74	.064	36	39	2.56	172	.086	1	3.11	.031	.55	.3	.03	6.5	.7	<.05	10	.9
404875	10.8	141.6	30.1	137	.6	52.0	25.9	1692	5.24	265.4	3.9	18.2	16.6	35	.9	13.4	3.2	172	.79	.103	24	77	4.52	161	.127	1	4.71	.008	1.28	.3	.01	9.0	1.5	<.05	16	1.9
404876	.8	41.0	59.3	96	.5	23.2	17.3	648	2.93	741.2	2.1	193.6	6.6	29	1.9	23.8	.8	23	.08	.062	25	14	.23	79	.012	1	.92	.011	.10	.3	.03	1.3	.1	.06	2	.6
404877	.7	20.1	23.4	70	.1	20.8	15.3	733	2.39	551.9	.8	37.9	5.6	15	1.0	5.7	1.3	27	.12	.068	16	16	.30	97	.019	<1	.92	.004	.07	.4	.03	1.5	.1	<.05	2	.6
404878	.8	11.7	11.0	31	<.1	9.3	4.1	122	1.75	242.4	.6	6.6	3.8	8	.2	1.8	.6	43	.06	.023	15	15	.19	62	.020	1	.93	.003	.03	.3	.02	1.3	.1	<.05	4	.8
404879	.8	18.7	16.0	62	.2	20.1	9.6	286	2.74	163.6	.9	11.4	4.4	10	.6	3.8	.4	43	.09	.047	16	23	.35	100	.032	<1	1.41	.005	.05	.3	.04	1.8	.1	<.05	4	.5
404880	.7	36.0	9.8	58	.1	22.4	9.1	280	2.64	698.9	1.3	28.1	6.5	16	.6	7.7	1.4	28	.07	.044	29	17	.27	92	.016	1	.99	.004	.09	.3	.03	1.4	.2	<.05	3	.8
404881	.7	19.9	10.5	46	<.1	19.6	9.1	289	2.30	513.7	.7	10.4	4.4	10	.1	1.4	1.1	29	.09	.040	16	16	.32	106	.021	1	1.01	.004	.07	.4	.02	1.5	.2	<.05	3	.5
404882	1.1	18.8	10.9	43	<.1	16.2	7.8	249	2.46	96.2	.8	7.2	4.3	9	.1	.9	.3	44	.08	.027	13	24	.34	103	.030	1	1.46	.006	.05	.3	.04	2.1	.1	<.05	4	<.5
404883	.8	27.6	12.1	54	.1	25.7	12.5	305	2.51	216.5	.8	7.1	5.8	8	.2	5.0	.4	28	.05	.025	19	17	.29	80	.017	2	1.23	.005	.05	.2	.04	1.9	.1	<.05	3	.9
404884	.8	17.1	10.4	43	<.1	17.1	8.3	347	2.17	104.3	.8	16.3	2.0	9	.2	3.7	.3	30	.08	.045	17	16	.26	74	.020	1	.98	.004	.05	.3	.03	1.2	.1	<.05	3	.7
404885	.6	30.8	8.1	38	<.1	14.4	5.4	131	2.09	40.2	.6	8.8	2.3	8	.2	2.0	.3	25	.07	.046	14	14	.24	40	.018	1	.82	.003	.04	.8	.03	1.1	.2	<.05	2	1.0
RE 404885	.6	31.7	8.0	42	<.1	14.4	5.3	129	2.05	42.5	.7	8.4	2.3	7	.1	2.1	.3	24	.06	.042	15	15	.22	42	.017	1	.78	.003	.03	.8	.03	1.1	.2	<.05	3	.6
404886	.8	22.1	16.1	36	.1	11.3	4.1	119	2.56	140.9	.8	11.5	5.9	7	.2	3.7	1.5	28	.05	.040	20	17	.21	44	.016	<1	.99	.004	.06	.3	.04	1.4	.2	<.05	3	.7
404887	1.0	25.4	10.3	40	.2	9.8	3.7	158	2.79	55.4	.7	13.4	2.0	10	.1	1.7	1.2	36	.04	.048	19	20	.28	54	.020	1	1.22	.004	.07	.3	.04	1.2	.2	.07	4	1.1
404888	.7	20.8	10.5	44	.1	14.5	5.6	150	1.95	202.5	1.1	4.1	.4	9	.1	1.4	1.0	28	.06	.054	19	19	.31	80	.011	<1	1.13	.006	.05	.2	.03	.9	.2	<.05	4	.6
404889	.9	20.8	15.1	45	<.1	13.8	4.7	146	2.15	293.6	.9	5.4	1.3	8	.2	1.5	1.4	31	.06	.037	17	19	.33	66	.014	1	1.05	.005	.05	.3	.02	1.0	.2	<.05	4	<.5
404890	.5	24.8	6.1	40	<.1	31.3	7.9	366	1.91	7.9	.9	4.9	4.7	70	.3	.6	.1	46	3.02	.097	15	38	.79	172	.085	2	.87	.028	.08	.2	.03	3.0	.1	.07	3	<.5
404891	.8	34.8	9.2	47	<.1	16.7	6.3	208	2.45	493.8	.9	7.9	2.2	11	.1	1.5	3.2	41	.08	.041	16	24	.55	90	.027	1	1.39	.005	.07	.4	.03	1.8	.3	<.05	5	.9
404892	.7	89.6	17.2	71	.3	33.8	17.4	814	3.69	2349.8	1.9	109.4	6.1	22	.2	14.1	12.9	29	.15	.067	28	17	.35	135	.015	2	.92	.005	.07	1.0	.02	2.7	.2	<.05	2	.6
404893	.7	28.8	9.1	52	<.1	19.6	8.3	296	2.50	758.5	1.0	18.7	5.0	13	.1	2.8	2.5	38	.10	.046	19	23	.48	116	.025	2	1.27	.006	.11	.4	.03	1.9	.3	<.05	4	<.5
STANDARD DS7	20.6	108.2	67.8	409	.9	55.2	9.6	623	2.38	47.5	4.8	68.5	4.3	66	6.1	5.8	4.4	86	.91	.077	11	162	1.04	362	.121	38	.95	.073	.44	3.8	.19	2.5	4.1	.21	4	3.1

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data k FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.7	2.4	52	<.1	7.3	5.2	593	2.12	<.5	2.6	<.5	4.5	60	<.1	<.1	.1	42	.65	.099	7	69	.65	217	.137	<1	1.00	.068	.50	.1	<.01	2.3	.4	<.05	5	<.5
404894	.7	25.9	11.5	53	.1	16.4	7.2	334	2.41	180.3	1.2	9.9	1.9	9	.3	3.9	.7	28	.07	.046	24	16	.30	79	.010	<1	1.01	.004	.05	.2	.03	1.0	.1	<.05	4	<.5
404895	.7	18.3	8.2	53	<.1	15.4	7.4	289	2.13	181.8	.9	11.3	2.3	9	.3	1.5	.6	31	.09	.055	17	18	.32	99	.021	1	.99	.004	.04	.4	.02	1.5	.1	<.05	3	.8
404896	.9	8.8	12.2	33	<.1	8.9	2.8	82	1.47	87.7	.6	7.6	.3	6	.2	3.6	.4	27	.04	.025	16	14	.19	55	.008	<1	.83	.004	.04	.2	.02	.5	.1	<.05	4	.7
404897	.9	27.9	22.9	69	<.1	18.7	7.8	254	2.43	270.3	1.2	12.2	3.9	8	.5	14.2	.6	31	.06	.037	21	20	.33	90	.016	<1	1.12	.003	.05	.3	.02	2.1	.1	<.05	3	.7
404898	.8	20.2	31.8	60	<.1	15.0	6.6	199	2.76	373.5	.7	18.2	3.0	8	.4	8.5	.9	34	.06	.038	22	20	.29	76	.012	<1	1.11	.005	.06	.2	.02	1.5	.2	<.05	3	<.5
404899	.8	16.9	45.2	64	.3	15.5	8.5	385	2.49	194.6	.8	9.9	1.0	8	.6	18.3	.4	31	.05	.049	16	19	.31	77	.012	<1	1.19	.004	.06	.1	.04	1.0	.1	<.05	4	<.5
404900	.7	35.9	12.7	184	.3	44.5	23.0	2033	5.26	670.3	.9	17.5	14.1	58	1.2	4.3	3.8	100	1.10	.094	35	48	5.19	487	.199	1	5.56	.071	1.58	.5	.01	10.2	1.7	.07	17	.6
405201	.7	19.6	9.9	75	<.1	20.7	11.8	504	2.47	76.4	1.3	10.2	3.6	11	.4	1.6	.8	35	.12	.063	22	22	.40	157	.030	<1	1.25	.005	.08	.8	.02	2.2	.2	<.05	4	<.5
405202	1.0	18.4	10.1	66	<.1	17.1	7.0	269	2.51	77.3	1.1	7.5	1.5	10	.2	.8	.9	41	.09	.065	17	23	.42	88	.025	<1	1.50	.005	.07	.4	.04	1.7	.2	<.05	5	.6
405203	.7	25.5	9.3	62	.1	22.2	11.1	276	2.21	222.0	1.2	5.0	2.9	21	.3	1.5	1.0	33	.15	.061	21	19	.37	126	.027	1	1.20	.006	.09	.5	.03	1.6	.2	<.05	4	.6
405204	.9	17.6	11.4	56	<.1	17.3	6.4	187	2.56	240.6	1.0	6.8	.9	13	.1	1.3	1.2	42	.10	.050	18	23	.37	140	.019	1	1.43	.006	.06	.4	.04	1.3	.2	<.05	5	.5
405205	.9	16.4	9.1	54	<.1	16.3	6.8	301	2.40	344.4	.9	9.0	.7	11	.2	1.1	1.3	39	.08	.047	15	20	.35	94	.021	<1	1.31	.006	.05	.4	.03	1.2	.2	<.05	4	<.5
405206	.7	20.0	10.4	54	<.1	16.7	8.1	355	2.33	382.8	.9	7.9	1.8	14	.1	1.1	1.7	35	.12	.044	17	20	.37	109	.024	1	1.24	.005	.06	.6	.03	1.6	.2	<.05	4	.5
405207	.9	69.3	13.0	84	.2	26.6	11.7	418	3.33	1293.9	1.6	43.6	2.9	38	.5	2.4	8.3	38	.21	.070	24	25	.46	154	.028	<1	1.82	.013	.15	.7	.03	1.8	.3	<.05	5	.9
RE 405205	.8	17.7	9.8	54	<.1	15.8	7.4	326	2.47	362.5	.9	9.0	.9	11	.1	1.1	1.3	40	.08	.050	15	21	.36	94	.022	<1	1.36	.006	.06	.3	.03	1.3	.2	<.05	4	<.5
405208	.8	48.1	14.0	66	.2	21.2	11.4	490	3.17	1600.4	1.2	52.4	1.7	27	.3	2.3	6.8	39	.21	.068	17	23	.44	159	.019	<1	1.68	.010	.08	.7	.03	1.6	.2	<.05	5	.9
405209	.5	62.0	11.9	70	.2	25.0	11.1	421	3.06	1427.2	1.3	51.8	3.0	28	.2	3.4	5.6	34	.21	.063	22	23	.45	159	.021	1	1.52	.010	.10	.8	.03	2.0	.2	<.05	5	.5
405210	.7	66.7	11.6	69	.2	27.1	13.3	393	3.21	1203.0	1.5	155.2	7.5	37	.3	8.9	4.9	31	.21	.057	28	22	.46	177	.029	<1	1.57	.009	.14	.8	.01	2.3	.3	<.05	5	.9
405211	.8	74.0	26.9	72	.3	26.4	11.2	549	3.54	1498.2	1.7	56.4	5.4	27	.5	52.5	8.1	29	.24	.078	31	24	.38	135	.015	2	1.28	.006	.15	.7	.01	3.1	.3	<.05	4	.5
405212	.6	59.2	17.0	75	.3	33.1	12.4	465	3.48	754.3	1.5	48.9	8.9	55	.2	10.8	3.7	33	.41	.066	30	30	.65	132	.023	<1	2.03	.009	.21	.4	.02	3.2	.4	<.05	6	.5
405213	.4	136.7	19.4	39	.5	42.5	24.8	574	4.38	4847.2	2.0	148.7	17.1	48	.2	8.9	20.0	20	.46	.058	58	17	.39	146	.006	1	1.23	.009	.11	.7	.01	2.8	.2	<.05	4	1.2
405214	.6	89.0	36.6	87	.4	32.4	14.2	465	3.65	1703.3	1.5	75.7	8.1	50	.9	10.2	9.6	29	.46	.064	32	23	.50	123	.015	1	1.63	.010	.15	.4	.02	2.9	.3	<.05	5	.9
405215	.6	70.8	49.9	68	.6	28.4	11.7	380	3.63	1324.6	2.1	33.6	9.1	18	.3	29.5	5.1	17	.13	.057	41	16	.30	91	.006	1	1.13	.004	.10	.2	.03	2.1	.2	<.05	3	.8
405216	.6	99.1	25.3	65	.4	37.0	13.6	556	4.35	2453.6	1.9	70.1	13.0	28	.4	37.8	8.4	14	.30	.063	47	13	.19	91	.002	2	.86	.007	.10	.2	.03	3.8	.3	<.05	2	1.4
405217	.7	100.5	28.1	61	.8	44.4	19.0	741	4.83	1948.0	2.2	66.9	16.1	38	.5	26.8	6.8	15	.38	.051	44	15	.30	71	.007	3	1.01	.021	.10	.2	.03	3.4	.2	.07	3	1.1
405218	.4	216.3	28.9	55	.7	57.1	30.9	1356	5.46	5048.6	2.2	104.2	19.1	29	.3	23.7	16.1	6	.33	.061	46	6	.12	44	.001	1	.49	.004	.08	.1	.04	3.8	.2	<.05	1	1.5
405219	.4	69.9	13.0	88	.2	50.9	22.9	570	4.37	746.4	2.7	13.3	15.7	18	.2	5.8	2.4	13	.07	.072	54	14	.30	66	.004	1	.89	.004	.08	.1	.03	1.8	.2	<.05	2	.8
405220	12.0	1399.0	4.9	51	.4	435.4	18.5	564	4.03	23.6	.3	103.5	1.4	69	.1	1.7	.3	62	1.17	.058	5	586	.81	127	.097	5	1.50	.118	.22	1.4	.23	3.8	.1	.95	4	2.9
405221	.5	127.7	14.9	45	.4	42.5	20.5	527	4.39	2071.1	1.9	63.1	23.8	50	.2	6.5	8.2	12	.49	.043	62	11	.38	96	.001	1	1.25	.008	.14	.2	.03	3.1	.3	<.05	3	.9
405222	.4	38.9	13.1	48	.3	27.6	9.5	434	3.05	490.4	.9	7.4	7.1	16	.2	2.0	2.3	28	.20	.051	37	24	.35	92	.007	1	1.58	.006	.07	.2	.03	2.9	.3	<.05	5	.6
405223	.5	75.2	24.1	74	.2	33.7	24.5	593	4.55	1070.8	1.5	24.3	14.4	48	.2	7.5	3.3	8	.29	.053	47	7	.74	140	.001	2	1.53	.006	.08	<.1	.03	3.3	.3	<.05	2	1.5
405224	.8	21.4	11.7	47	.1	21.6	7.7	302	2.43	133.3	.8	4.7	2.1	12	.1	1.6	.5	37	.11	.049	16	23	.41	143	.017	1	1.54	.006	.06	.3	.03	1.9	.3	<.05	4	.5
405225	.7	37.4	12.6	50	.1	27.6	13.9	312	2.87	573.1	.8	12.1	7.7	26	.1	2.9	4.1	32	.13	.026	22	20	.42	133	.024	2	1.24	.007	.07	.3	.02	2.2	.2	<.05	4	<.5
405226	.6	26.5	10.5	51	<.1	24.0	12.4	349	2.64	302.5	1.1	2.7	7.6	10	.2	1.9	.4	29	.09	.042	26	18	.42	97	.019	1	1.30	.004	.10	.2	.02	1.9	.3	<.05	3	.6
STANDARD DS7	20.5	105.7	68.1	399	.9	53.7	9.4	615	2.34	46.6	4.8	68.3	4.4	68	6.2	5.7	4.4	84	.90	.078	12	161	1.05	365	.120	38	.96	.073	.43	3.7	.20	2.4	4.1	.19	4	3.8

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ℓ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.4	2.1	46	<.1	5.7	4.9	577	1.93	<.5	2.7	<.5	4.1	59	<.1	<.1	<.1	40	.58	.089	5	62	.62	203	.127	1	.86	.062	.44	.1	<.01	2.0	.3	<.05	5	<.5
405227	.6	23.0	10.4	39	.1	16.1	7.5	439	2.33	466.9	.9	8.9	4.0	11	.1	3.7	2.0	25	.10	.057	18	16	.30	82	.009	1	1.13	.003	.05	.2	.03	1.3	.2	<.05	3	<.5
405228	.3	80.8	7.7	42	<.1	34.1	12.1	365	3.66	922.1	1.4	26.7	17.3	13	.1	5.8	9.1	22	.17	.053	34	27	.75	130	.008	1	1.97	.004	.25	<.1	<.01	2.5	.5	<.05	5	.5
405229	.7	51.2	24.6	102	<.1	38.6	14.9	240	4.72	475.7	2.2	4.3	14.7	10	.1	2.7	.6	19	.03	.043	43	30	.77	49	.007	<1	1.85	.003	.09	.1	.01	1.4	.2	<.05	5	1.3
405230	.6	44.5	15.0	78	<.1	33.2	18.9	361	3.66	752.1	1.6	18.9	10.6	16	.4	4.1	3.3	27	.06	.041	28	28	.56	107	.024	<1	1.52	.004	.14	.3	.03	1.8	.3	<.05	4	<.5
405231	.5	25.7	9.5	64	<.1	31.4	17.0	602	3.11	318.8	1.1	1.7	5.7	9	.1	1.8	.7	23	.06	.042	23	27	.51	111	.018	1	1.26	.004	.10	.2	.01	1.4	.2	<.05	4	<.5
RE 405231	.6	25.1	9.1	60	<.1	31.9	16.7	555	2.94	307.7	1.2	2.0	5.2	9	.2	1.7	.7	21	.06	.039	21	24	.47	102	.016	1	1.19	.003	.10	.2	.01	1.2	.1	<.05	3	.7
405232	.8	34.5	9.7	58	<.1	26.9	14.3	487	2.69	472.9	1.9	7.8	3.5	11	.2	2.1	2.3	29	.05	.042	21	21	.33	82	.016	<1	1.07	.004	.05	.4	.02	1.3	.1	<.05	3	.6
405233	.5	46.7	9.9	57	<.1	23.3	9.7	398	2.81	550.2	1.6	16.9	7.8	10	.2	2.3	3.0	24	.06	.048	27	20	.39	95	.021	1	1.31	.004	.16	.4	.02	1.9	.3	<.05	4	.7
405234	.8	31.3	8.4	61	<.1	19.5	9.8	366	2.50	315.6	1.3	9.7	2.6	11	.2	1.6	2.1	31	.07	.053	19	22	.40	91	.024	<1	1.23	.004	.07	.4	.02	1.6	.2	<.05	4	.6
405235	.9	28.4	8.5	60	<.1	19.7	7.4	213	2.46	212.4	1.2	12.2	1.7	12	.2	1.6	1.0	32	.08	.046	18	22	.37	103	.019	<1	1.09	.005	.04	.5	.02	1.6	.1	<.05	3	.7
405236	.4	47.0	8.9	45	<.1	20.8	11.6	388	2.47	590.1	1.6	4.3	11.3	23	.2	2.4	2.9	17	.05	.034	31	17	.39	190	.021	<1	1.12	.005	.10	.2	<.01	1.8	.2	<.05	3	<.5
405237	1.0	17.8	9.5	56	<.1	16.9	8.4	292	2.42	98.0	1.0	2.4	1.4	10	.2	1.1	.5	38	.06	.046	15	22	.34	102	.020	1	1.16	.004	.03	.3	.04	1.7	.1	<.05	3	.6
405238	.8	28.2	9.1	54	<.1	19.0	9.7	280	2.56	309.3	1.4	2.4	2.2	20	.2	2.1	1.1	29	.06	.048	23	19	.33	90	.016	<1	1.04	.005	.04	.3	.02	1.3	.1	<.05	3	.5
405251	1.0	32.1	10.1	53	<.1	18.3	8.3	307	2.54	731.2	1.3	12.0	3.5	13	.2	3.3	2.9	32	.08	.062	18	22	.51	104	.023	1	1.34	.005	.07	.5	.01	1.8	.3	<.05	4	<.5
405252	.7	17.2	9.4	34	.1	10.2	3.9	108	2.09	460.3	.7	8.4	.3	12	.1	2.3	2.3	30	.04	.036	14	16	.25	67	.009	2	.92	.006	.05	.3	.03	.6	.2	<.05	4	.5
405253	1.1	23.9	9.5	45	.1	16.1	7.5	218	2.45	500.6	.9	6.8	6.3	9	.2	2.3	3.1	37	.05	.032	15	20	.30	84	.019	1	1.25	.004	.05	.6	.03	1.8	.2	<.05	4	.6
405254	.9	29.9	9.3	55	.1	22.7	11.3	321	2.50	662.6	1.0	21.1	7.2	17	.2	4.3	2.9	27	.10	.051	17	17	.34	102	.016	1	1.11	.005	.07	1.0	.01	1.5	.2	<.05	2	.8
405255	.9	19.6	10.0	48	<.1	15.1	8.5	383	2.42	442.9	.7	5.9	2.8	11	.1	2.9	1.9	30	.08	.054	15	18	.31	59	.019	1	.85	.005	.08	.5	.02	1.2	.2	<.05	3	<.5
405256	.9	29.8	8.2	60	<.1	21.9	10.3	331	2.52	271.2	1.5	11.5	6.9	17	.2	2.2	1.1	29	.14	.063	19	19	.42	155	.026	1	1.06	.005	.05	.5	.02	2.3	.1	<.05	3	<.5
405257	.8	26.1	8.1	65	<.1	23.7	10.6	439	2.41	189.6	1.4	6.1	5.6	14	.3	1.4	1.1	36	.15	.073	16	22	.43	110	.035	<1	1.16	.007	.08	1.0	.03	2.6	.1	<.05	3	.5
405258	.9	15.3	12.0	58	<.1	15.9	10.0	418	2.28	167.1	.7	19.7	5.1	10	.4	1.9	.6	33	.10	.066	13	18	.27	59	.023	1	.81	.005	.05	.5	.03	1.5	.1	<.05	2	.5
405259	.6	37.3	14.4	68	.1	25.2	12.2	529	3.02	124.6	1.6	10.4	11.9	15	.2	5.3	.4	17	.07	.042	42	18	.48	98	.010	1	1.22	.004	.06	.2	.01	1.6	.1	<.05	3	<.5
405260	.7	15.5	11.9	58	<.1	15.2	10.9	512	2.45	94.3	.8	9.4	3.7	9	.2	4.6	.3	25	.10	.067	13	17	.32	47	.018	1	.99	.004	.04	.2	.02	1.4	.1	<.05	2	<.5
405261	.7	28.3	31.5	88	.3	21.0	10.7	471	2.28	83.4	2.0	13.7	4.4	10	.6	8.2	.4	30	.10	.063	14	20	.39	97	.020	1	1.40	.005	.05	.2	.05	2.3	.1	<.05	3	<.5
405262	.8	28.3	20.9	66	.2	21.5	12.2	428	2.64	119.3	1.7	14.4	4.5	8	.3	4.7	.5	30	.07	.057	17	22	.42	73	.020	1	1.40	.005	.06	.2	.05	2.4	.1	<.05	3	<.5
405263	.6	28.9	19.8	68	.2	21.4	12.1	412	2.48	110.6	1.8	13.1	4.8	9	.4	4.4	.3	30	.08	.059	16	21	.41	73	.019	1	1.40	.004	.06	.2	.04	2.3	.1	<.05	3	.5
405264	.7	14.3	26.4	54	.1	14.9	9.4	419	2.15	185.7	.8	27.3	3.8	9	.6	8.7	.4	26	.07	.049	11	17	.30	67	.015	1	1.09	.004	.04	.2	.02	1.6	.1	<.05	2	<.5
405265	.8	24.4	19.7	87	.2	23.4	11.5	440	2.48	138.6	1.4	20.5	4.3	13	.8	6.2	.4	36	.13	.070	17	24	.44	97	.030	1	1.38	.006	.06	.3	.03	2.4	.1	<.05	3	<.5
405266	1.6	20.5	47.8	61	.2	14.5	11.8	651	2.35	267.7	.9	18.8	.8	8	.3	20.1	1.5	46	.08	.052	15	26	.71	83	.020	2	1.53	.006	.06	.2	.03	1.6	.3	<.05	5	.5
405267	1.0	17.8	13.1	51	<.1	18.3	9.1	220	2.77	43.9	.9	4.6	5.8	9	.2	1.9	.3	45	.06	.023	14	26	.41	110	.027	1	1.58	.006	.07	.2	.03	2.2	.1	<.05	4	<.5
405268	.9	37.7	33.4	74	.1	36.3	18.4	666	3.23	206.1	1.4	38.0	12.4	16	.2	15.0	.3	32	.08	.028	31	27	.57	199	.024	1	1.63	.005	.18	.2	.02	2.7	.2	<.05	4	<.5
405269	2.4	74.1	20.9	95	<.1	35.2	21.1	1035	3.78	262.6	2.9	9.7	14.4	16	.6	8.7	3.7	38	.15	.043	38	33	1.17	196	.041	1	1.93	.006	.23	.2	.01	4.3	.5	<.05	5	.5
405270	.8	28.2	12.7	66	<.1	22.7	10.5	400	2.54	104.5	1.2	10.9	4.1	14	.1	4.3	.8	41	.17	.057	19	24	.65	168	.036	1	1.58	.006	.07	.3	.03	3.0	.2	<.05	4	.7
405271	.9	33.0	11.0	68	<.1	32.7	19.5	578	2.94	344.9	1.2	8.1	8.4	13	.2	1.5	.7	35	.12	.056	28	21	.44	94	.027	1	1.24	.006	.06	.4	.03	1.8	.2	<.05	3	<.5
STANDARD	20.2	106.8	68.3	401	.9	54.4	9.3	603	2.31	48.8	4.7	68.1	4.2	64	6.1	5.7	4.4	83	.85	.077	9	157	1.03	362	.106	37	.94	.070	.42	3.7	.20	2.2	4.1	.20	4	3.6

Standard is STANDARD DS7. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.1	2.3	50	<.1	6.8	4.9	588	1.96	.5	2.4	.5	4.3	56	<.1	<.1	<.1	40	.57	.106	6	60	.68	228	.129	1	1.02	.058	.49	.1	<.01	1.9	.3	<.05	5	<.5
405272	.8	64.7	14.8	64	.1	41.1	22.5	540	4.18	3669.2	1.7	19.8	9.8	26	.2	12.0	3.1	29	.09	.052	29	30	.48	263	.025	1	1.46	.005	.17	.4	.03	3.1	.4	<.05	4	1.8
405273	.8	33.8	12.2	66	<.1	30.6	12.5	385	3.26	396.5	1.0	12.1	5.2	8	.1	7.6	1.0	26	.04	.034	19	16	.23	83	.012	1	1.11	.005	.04	.2	.04	1.6	.1	<.05	3	.7
405274	.7	24.0	10.1	52	<.1	23.5	11.8	318	2.41	86.3	.7	3.4	5.4	10	.2	2.5	.4	28	.08	.038	14	18	.34	114	.022	1	1.16	.004	.06	.2	.03	1.8	.2	<.05	3	.5
405275	1.3	80.6	16.3	44	.1	21.7	7.3	167	3.77	330.5	1.3	4.8	11.4	25	.1	1.6	.8	24	.03	.033	33	14	.19	55	.011	1	1.01	.008	.07	.2	.03	1.4	.2	<.05	3	.7
405276	.7	24.5	8.2	56	<.1	25.3	11.7	429	2.33	234.9	.7	9.7	5.2	11	.2	3.6	.6	26	.11	.054	16	15	.28	100	.017	1	.93	.004	.04	.3	.02	1.6	.1	<.05	2	.5
405277	.9	150.6	14.6	68	.2	44.5	30.6	1347	3.37	1479.6	3.3	51.3	6.3	37	1.4	2.4	5.6	31	.16	.070	36	20	.37	169	.019	1	1.15	.006	.11	.5	.02	3.0	.3	<.05	4	1.2
405278	.8	37.2	11.1	55	.1	18.7	11.0	347	2.92	653.2	1.2	19.0	6.9	25	.2	4.7	2.4	25	.10	.059	24	16	.36	77	.024	1	1.04	.005	.12	.5	.02	1.5	.3	.07	3	.8
405279	.6	40.3	7.7	52	<.1	20.8	9.5	246	2.28	498.4	.9	16.7	5.7	14	.2	1.4	.9	25	.13	.067	15	16	.33	88	.022	1	1.05	.005	.07	.3	.02	1.7	.2	<.05	3	.7
405280	.6	25.2	12.1	53	<.1	23.9	10.8	344	2.34	109.5	.7	19.5	6.6	13	.3	2.2	.3	27	.11	.045	19	17	.34	171	.032	1	1.04	.004	.11	.3	.02	1.7	.1	<.05	3	<.5
405281	.8	13.5	11.6	45	<.1	13.6	7.1	284	2.30	123.0	.5	5.9	4.2	7	.4	1.6	.4	36	.06	.031	14	18	.26	65	.028	1	1.03	.005	.05	.3	.02	1.5	.1	<.05	4	.5
405282	.8	30.9	10.0	55	.1	21.8	11.2	359	2.48	197.9	1.2	11.2	5.4	13	.5	1.4	.4	35	.13	.056	20	22	.40	139	.033	19	1.26	.005	.05	.4	.02	2.4	.1	<.05	3	.6
405283	.7	35.7	10.5	58	<.1	24.0	13.4	315	2.81	678.2	1.1	16.1	6.5	22	.2	1.7	2.9	26	.14	.073	19	20	.43	101	.024	2	1.16	.009	.09	.4	.02	1.6	.2	.06	3	.6
405284	.8	31.7	10.6	50	.1	15.0	8.0	311	2.89	269.5	1.1	15.6	5.2	24	.2	2.8	1.1	29	.06	.049	22	19	.35	72	.024	1	1.07	.007	.12	.3	.01	1.2	.2	.08	4	.5
RE 405282	.8	31.4	10.3	58	.1	22.4	11.4	369	2.55	201.1	1.2	11.6	5.5	14	.5	1.3	.4	36	.13	.058	20	22	.42	146	.035	1	1.32	.006	.04	.4	.03	2.3	.2	<.05	3	.7
STANDARD	20.5	109.2	70.3	414	.9	56.0	9.6	617	2.35	49.3	4.9	69.6	4.3	67	6.4	6.0	4.6	85	.91	.080	12	161	1.05	369	.118	39	.94	.071	.45	3.9	.20	2.4	4.2	.22	5	3.8

Standard is STANDARD DS7. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A603488 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	2.5	3.3	47	<.1	4.0	4.2	528	1.80	<.5	2.9	1.6	4.3	77	<.1	<.1	.1	36	.58	.070	9	10	.58	215	.128	2	1.07	.121	.52	.1	<.01	2.2	.3	<.05	5	<.5
C115670	.5	11.9	1.3	17	<.1	8.2	2.7	63	.94	18.0	.2	.9	1.0	2	<.1	.5	.4	4	.03	.003	4	12	.17	19	.007	3	.28	.009	.08	.2	.01	.4	.1	<.05	1	<.5
C115671	5.3	29.3	218.6	10	17.5	4.0	2.1	66	.75	245.5	.7	406.9	.8	2	.4	90.0	473.9	1	.01	.002	3	10	.02	17	.002	3	.10	.008	.05	.2	.03	.3	<.1	<.05	<1	1.1
C115672	.4	10.6	2.0	1	<.1	2.3	.5	22	.48	32.7	.1	1.2	.1	1	<.1	1.5	2.6	1	.01	.003	<1	11	.01	4	<.001	1	.02	.003	<.01	.2	<.01	.1	<.1	<.05	<1	<.5
C115673	.6	7.1	1.3	1	<.1	1.4	.5	33	.40	17.4	<.1	1.5	<.1	1	<.1	.7	2.2	<1	.01	.001	<1	12	<.01	2	<.001	1	.01	.003	<.01	.1	.01	.1	<.1	<.05	<1	<.5
C115674	.4	2.9	2.1	3	<.1	1.8	.3	20	.33	42.3	<.1	.9	.5	<1	.1	.5	.3	<1	<.01	.001	1	14	<.01	16	<.001	2	.05	.003	.03	.2	<.01	.1	<.1	<.05	<1	<.5
RE C115674	.5	2.6	2.1	3	<.1	2.1	.3	21	.34	41.9	<.1	.8	.5	<1	.2	.6	.2	<1	<.01	.001	1	14	<.01	17	<.001	3	.05	.002	.03	.2	<.01	.1	<.1	<.05	<1	<.5
C115675	.3	18.5	3.1	4	<.1	2.8	1.3	53	.80	182.5	.3	<.5	1.0	11	<.1	1.3	1.0	2	<.01	.008	6	13	.06	10	.001	1	.18	.005	.05	1.3	<.01	.3	<.1	<.05	1	<.5
C115676	.3	5.9	17.7	52	.1	4.7	2.0	424	.54	27.1	.7	3.4	7.7	97	1.9	.5	.4	7	6.57	.015	16	12	.71	114	.045	3	.70	.065	.09	.7	.01	1.3	.1	<.05	2	<.5
C115677	.5	53.2	8.2	53	.2	32.1	12.9	338	2.76	26.3	1.4	3.6	11.3	79	.4	.7	.8	36	.78	.018	24	43	.62	374	.080	1	2.69	.225	.51	12.3	<.01	5.6	.6	<.05	9	1.2
C115678	.4	47.1	17.3	117	.2	27.1	11.7	331	2.37	36.8	2.0	2.8	18.0	262	1.1	.5	.5	35	2.68	.054	50	40	.41	106	.090	2	3.66	.410	.46	.4	.01	4.8	.3	<.05	10	<.5
C115679	.2	1.9	.3	1	<.1	1.1	.3	24	.29	2.0	<.1	.5	.1	1	<.1	.1	.1	<1	.01	<.001	<1	11	<.01	4	.001	<1	.03	.004	.01	.2	<.01	.1	<.1	<.05	<1	<.5
C115680	.4	2.5	.5	1	<.1	2.1	.4	28	.36	299.5	.1	4.0	.2	2	<.1	.4	.5	<1	.01	.001	2	13	.02	11	.001	1	.05	.004	.01	.1	<.01	.1	<.1	<.05	<1	<.5
C115681	.3	5.0	.4	1	<.1	1.7	.3	29	.41	67.5	<.1	5.8	.3	<1	<.1	.6	1.5	<1	<.01	.001	1	12	<.01	5	<.001	1	.02	.003	.01	.1	.01	.1	<.1	<.05	<1	<.5
C115682	.4	1.9	1.1	1	<.1	1.1	.2	19	.30	37.6	<.1	.5	<.1	<1	<.1	.5	.2	<1	<.01	<.001	<1	15	<.01	2	<.001	<1	<.01	.002	<.01	.2	<.01	<.1	<.1	<.05	<1	<.5
C115683	.7	14.4	5.9	92	<.1	18.1	12.0	649	3.76	92.3	3.6	2.3	15.5	143	.4	1.0	.5	124	1.82	.077	29	144	1.92	903	.266	2	3.79	.229	1.41	1.4	<.01	13.6	1.0	<.05	11	<.5
C115684	.5	7.2	2.1	3	<.1	1.3	.3	30	.36	30.2	.1	2.0	1.9	2	.1	1.2	.5	2	.02	.003	3	12	.02	28	.002	2	.10	.004	.06	.1	<.01	.2	<.1	<.05	<1	<.5
C115685	.3	30.7	6.6	52	<.1	16.1	9.3	212	2.64	209.8	1.5	1.6	15.4	23	.2	1.0	.9	14	.05	.024	33	21	.61	216	.018	2	1.46	.023	.34	.2	<.01	1.4	.3	.06	4	<.5
C115686	.5	81.4	1.1	1	<.1	3.5	2.4	27	.84	91.4	.1	<.5	.2	1	<.1	.5	.1	1	.02	.010	<1	12	.01	6	.001	2	.04	.002	.01	.4	<.01	.1	<.1	.23	<1	1.1
C115687	.4	8.8	1.1	9	<.1	6.4	3.1	65	.60	979.5	.2	8.8	1.7	3	.2	1.3	.3	2	.03	.014	4	16	.04	28	.002	2	.15	.004	.07	.1	<.01	.5	.1	<.05	<1	.6
C115688	.4	31.4	13.1	24	.3	3.7	1.4	102	.75	77.3	.3	2.2	9.8	4	.3	8.1	.7	2	.13	.009	17	11	.05	97	.002	4	.36	.019	.22	.1	.01	.5	.1	<.05	1	<.5
C115689	1.6	17.8	6.2	83	<.1	20.2	11.3	408	3.03	58.4	3.4	4.5	13.9	193	.2	1.0	1.0	94	1.76	.086	22	117	1.59	806	.249	2	3.91	.278	1.19	1.2	<.01	6.6	.9	<.05	10	<.5
C115690	.2	12.4	8.2	21	<.1	5.1	2.0	273	.84	54.5	.5	1.0	8.3	79	.6	1.8	.4	9	2.37	.015	14	14	.26	94	.033	3	.63	.081	.18	.3	<.01	1.3	.1	<.05	2	<.5
C115691	.3	5.3	1.1	2	<.1	1.1	.4	28	.39	129.4	.1	1.2	.5	1	.4	1.7	.2	<1	.02	.001	1	13	.01	10	.002	1	.05	.004	.02	.1	<.01	.1	<.1	<.05	<1	<.5
C115692 (pulp)	18.0	5766.7	15.0	99	1.3	365.1	19.9	793	7.62	13.0	.2	476.0	1.2	112	.4	4.6	.5	39	1.84	.089	4	474	.82	21	.002	13	.79	.051	.35	1.1	.98	3.9	.2	3.69	3	14.7
C115693	.3	6.3	9.6	14	<.1	1.7	.6	156	.36	50.3	.2	3.8	7.0	7	.4	4.4	.2	<1	.36	.009	13	11	.02	73	.001	20	.24	.003	.16	.1	<.01	.4	.1	<.05	1	<.5
C115694	1.1	14.6	8.4	105	<.1	18.4	12.7	670	3.81	73.4	3.5	1.1	15.1	167	.5	.9	.3	133	1.96	.084	24	167	2.05	939	.267	2	4.23	.259	1.59	1.1	<.01	12.5	1.1	<.05	11	<.5
C115695	1.4	6.6	.4	2	<.1	1.3	.3	40	.37	20.7	<.1	.8	.1	3	.1	.6	.1	<1	.07	.001	<1	13	.01	9	.002	<1	.03	.004	.01	.2	<.01	.1	<.1	<.05	<1	<.5
C115696	.8	30.4	3.8	6	.3	1.3	1.1	36	.91	1611.5	.3	15.9	5.8	8	1.0	4.0	.8	1	.03	.004	10	14	.03	55	.002	2	.22	.006	.14	.2	.01	.4	.1	<.05	1	.6
C115697	.3	4.2	1.3	1	<.1	1.3	.3	19	.34	61.2	<.1	1.8	.2	1	<.1	1.1	.1	<1	<.01	.001	1	13	<.01	11	<.001	2	.03	.002	.02	.2	<.01	.1	<.1	<.05	<1	<.5
C115698	.8	23.1	5.6	103	<.1	17.7	11.7	671	3.98	79.6	3.2	.6	15.3	148	.8	.7	.4	132	1.64	.083	27	159	2.02	980	.269	2	3.88	.228	1.46	1.2	<.01	13.6	1.1	<.05	11	<.5
C115699	.3	13.4	101.3	7	1.7	1.5	.4	47	.51	831.9	.3	21.7	5.8	2	.8	29.5	.4	3	.02	.008	12	11	.03	92	.002	12	.27	.007	.19	.1	.01	.3	.1	<.05	1	<.5
C115700	1.5	32.5	8.2	82	<.1	24.5	14.4	610	3.97	80.8	3.7	2.5	14.1	148	.2	1.2	.6	121	1.73	.084	22	154	2.01	805	.239	2	3.94	.233	1.25	.7	<.01	11.4	1.0	.17	11	.8
404901	.4	19.8	30.1	63	.2	7.6	3.2	182	.45	8.4	.8	.6	12.0	224	2.2	.4	.2	11	7.64	.013	19	17	.11	34	.064	6	1.40	.181	.08	.4	.01	1.1	<.1	.11	5	<.5
404902	1.0	10.0	8.2	119	<.1	17.3	11.5	702	3.56	22.7	3.9	1.5	14.5	80	.4	1.0	.3	102	1.92	.073	25	125	1.88	399	.161	2	2.85	.129	.78	.4	.01	10.0	.8	<.05	9	<.5
STANDARD DS7	20.9	112.6	70.7	413	.9	56.7	9.8	627	2.39	48.4	4.9	70.7	4.5	68	6.3	5.8	4.5	84	.93	.079	12	164	1.05	372	.123	38	.97	.073	.44	3.8	.20	2.5	4.2	.22	5	3.4

GROUP 1DX - 30 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

07-29-2006 A10:59

Data h FA ____ DATE RECEIVED: JUL 7 2006 DATE REPORT MAILED:.....

BRITISH COLUMBIA CERTIFIED ASSAYER Clarence Leong

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.3	3.4	3.0	49	<.1	4.4	4.5	539	1.93	<.5	3.0	<.5	4.6	65	<.1	<.1	.1	37	.57	.075	9	11	.61	201	.135	2	1.05	.104	.51	.2	<.01	2.1	.3	<.05	5	<.5
404903	.4	41.5	15.7	35	.5	11.8	5.1	457	1.52	73.2	.6	335.7	9.4	75	.4	2.8	50.5	6	2.62	.015	23	9	.15	71	.006	4	.54	.027	.22	.1	<.01	1.6	.1	<.05	1	.7
404904	.2	14.8	11.0	25	<.1	14.1	6.8	258	1.37	21.6	.3	5.5	8.1	39	.2	13.0	1.1	3	1.58	.009	17	6	.04	71	.002	6	.33	.028	.21	.1	<.01	1.1	.1	<.05	1	.7
404905	.8	14.3	2.3	20	<.1	7.3	3.1	152	1.23	37.1	.3	3.0	6.3	4	.1	.3	.2	9	.02	.007	8	21	.32	17	.008	2	.64	.032	.10	.2	<.01	1.0	.1	<.05	2	<.5
404906	.3	10.9	2.1	2	<.1	2.8	2.2	27	.81	5373.4	.1	185.7	.7	3	<.1	5.1	6.0	1	.02	.002	2	13	.01	27	.001	4	.08	.009	.04	.4	<.01	.2	.1	.16	<1	4.6
404907	.5	3.3	.8	1	<.1	1.6	.5	28	.32	6.8	<.1	3.0	.2	2	<.1	.5	.3	<1	.02	.001	<1	10	.01	4	.001	3	.03	.005	.01	.1	<.01	.1	<.1	<.05	<1	<.5
404908	.3	10.8	4.2	36	<.1	15.0	5.4	228	1.67	54.2	.4	2.5	9.0	5	<.1	.4	.3	14	.05	.011	12	24	.39	57	.027	1	.91	.028	.19	.2	<.01	1.5	.2	<.05	4	<.5
RE 404908	.3	10.3	4.0	34	<.1	15.7	5.1	220	1.60	53.0	.4	1.2	8.9	5	<.1	.4	.3	14	.05	.012	12	24	.39	55	.026	1	.86	.030	.19	.2	<.01	1.6	.2	<.05	3	<.5
404909	.5	11.1	2.6	4	<.1	5.4	2.2	48	.66	980.6	.1	16.2	2.7	2	<.1	1.3	2.1	1	.02	.007	4	13	.06	19	.001	2	.16	.010	.04	.2	<.01	.3	.1	<.05	<1	.7
404910	.4	21.4	2.1	5	<.1	7.4	3.4	77	.50	450.8	.2	7.0	2.2	10	.1	3.3	.4	1	.08	.032	4	11	.05	48	.001	8	.35	.009	.18	.4	<.01	.3	.1	<.05	1	<.5
404911	1.2	5.9	2.5	2	.3	1.2	.4	32	.52	188.4	.1	29.4	.9	3	<.1	1.2	.1	2	<.01	.005	2	12	.04	7	.001	1	.10	.004	.03	.3	<.01	.2	<.1	<.05	<1	.7
404912	.4	20.4	1.8	6	<.1	3.8	1.3	56	.88	957.2	.3	29.4	1.5	5	.1	4.2	2.7	4	.02	.011	3	13	.09	26	.002	2	.25	.006	.08	.5	<.01	.4	.1	<.05	1	.6
404913	.5	17.7	2.1	4	.3	2.5	.9	29	.77	142.7	.2	5.7	1.4	3	<.1	11.0	.3	2	.01	.008	4	13	.01	12	.001	4	.12	.009	.06	.5	<.01	.2	<.1	<.05	<1	.7
404914	.2	19.0	12.3	31	.2	3.3	1.5	334	.66	45.1	.1	2.0	5.7	73	2.6	3.8	1.6	2	2.82	.008	11	11	.03	32	.001	4	.19	.011	.11	.2	<.01	.5	.1	<.05	<1	<.5
404915	1.1	10.3	.9	3	<.1	7.7	2.8	43	.69	10.0	<.1	<.5	.1	1	.1	2.4	.1	2	.02	.001	<1	15	<.01	7	<.001	2	.02	.002	.01	.1	<.01	.1	<.1	.21	<1	<.5
404916	.5	7.7	.9	3	<.1	4.4	1.8	64	.53	21.0	.1	1.1	.8	20	<.1	1.8	.2	3	.53	.007	3	13	.01	5	.001	3	.06	.003	.03	.5	<.01	.2	<.1	<.05	<1	<.5
404917 (pulp)	.7	23.3	6.4	41	<.1	31.2	8.2	355	1.93	8.0	.8	6.2	4.7	67	.3	.6	.1	44	3.19	.098	16	37	.77	169	.086	3	.85	.026	.08	.2	.03	3.1	.1	<.05	3	<.5
STANDARD DS7	20.8	111.5	70.1	414	.9	55.7	9.6	634	2.42	48.1	4.9	69.9	4.4	69	6.4	6.0	4.6	85	.94	.080	13	163	1.06	382	.124	39	.97	.075	.44	3.9	.21	2.5	4.2	.23	5	3.7

Sample type: ROCK R150. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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ACME ANALYTICAL LABORATORIES LTD. (ISO 9001 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. File # A603487 Page 1

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Al Doherty

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.2	2.7	44	<.1	6.5	4.5	498	1.77	<.5	1.9	.9	3.7	53	<.1	<.1	.1	35	.44	.075	6	65	.60	183	.117	2	.95	.068	.48	.1	<.01	2.3	.4	<.05	4	<.5
404501	.8	41.1	16.4	84	.1	31.9	17.4	512	3.49	264.7	1.8	9.7	9.0	21	.2	5.1	1.4	32	.13	.068	34	27	.54	171	.033	2	1.85	.009	.30	.2	.02	2.5	.3	<.05	5	.5
404502	1.0	34.4	18.5	79	.2	24.9	13.8	512	3.47	287.5	1.7	16.4	2.3	12	.3	5.9	1.6	41	.08	.081	21	25	.40	130	.018	1	1.66	.006	.14	.4	.04	1.8	.3	<.05	5	.6
404503	.9	14.8	10.4	57	<.1	17.3	9.5	400	2.38	108.3	.7	6.3	3.9	9	.3	1.8	.7	32	.10	.054	14	18	.29	66	.025	2	.94	.004	.07	.5	.02	1.4	.1	<.05	3	<.5
404504	.7	26.1	9.9	68	<.1	26.2	10.3	283	2.68	113.0	.9	11.2	5.7	11	.2	3.3	.5	35	.10	.047	20	25	.48	132	.040	1	1.52	.005	.19	.3	.02	2.0	.2	<.05	5	<.5
RE 404504	.7	25.6	9.5	67	<.1	26.0	9.9	286	2.65	110.8	.9	4.5	5.5	11	.2	3.3	.5	34	.10	.047	21	25	.48	132	.041	1	1.56	.005	.19	.3	.02	2.0	.2	<.05	5	<.5
404505	.9	15.3	12.3	56	<.1	16.2	8.6	322	2.59	91.1	.8	3.6	1.5	9	.2	1.1	.3	40	.07	.046	13	21	.38	91	.024	1	1.30	.005	.06	.3	.02	1.4	.2	<.05	4	.6
404506	.9	31.5	11.1	64	<.1	20.8	8.8	348	2.88	229.9	1.4	5.7	1.5	16	.2	3.9	1.3	38	.08	.065	17	24	.39	142	.021	1	1.37	.007	.14	.3	.03	1.4	.2	<.05	5	.6
404507	.9	30.7	11.7	67	<.1	23.1	9.3	319	2.96	297.4	1.3	10.1	2.9	20	.2	1.6	2.1	39	.09	.062	23	27	.44	137	.029	1	1.59	.007	.18	.3	.03	1.7	.3	<.05	6	.6
404508	1.0	31.4	11.0	68	.1	23.5	8.7	282	2.68	184.2	1.3	13.1	4.6	12	.3	2.3	1.2	35	.10	.054	20	22	.39	124	.024	2	1.38	.005	.11	.8	.02	2.1	.3	<.05	4	.6
404509	1.0	26.6	10.3	69	.1	24.2	10.9	382	2.47	288.9	1.0	31.6	7.0	19	.4	5.6	1.5	35	.17	.052	19	21	.41	199	.035	2	1.30	.007	.10	1.8	.02	2.4	.1	<.05	3	.5
404510	.9	32.2	12.2	75	<.1	25.1	12.4	400	2.95	398.0	1.1	34.0	3.3	18	.4	2.9	3.4	40	.12	.050	20	25	.47	145	.030	1	1.65	.005	.16	1.3	.03	2.0	.3	<.05	5	.5
404511	.8	33.1	10.0	58	<.1	19.2	8.0	224	2.42	282.3	1.0	20.1	3.8	20	.2	1.4	3.0	33	.12	.049	21	21	.40	143	.030	1	1.40	.007	.11	.6	.02	1.8	.2	<.05	4	<.5
404512	.8	30.0	12.2	55	.1	20.4	8.0	223	2.34	340.5	1.0	16.2	2.9	23	.2	2.6	1.6	32	.15	.051	18	21	.40	151	.027	1	1.38	.008	.11	.4	.03	1.8	.2	<.05	4	.5
404513	.8	26.5	10.3	55	<.1	19.9	8.1	225	2.46	183.5	1.0	19.9	5.7	19	.2	1.3	1.4	34	.15	.052	23	22	.45	149	.038	2	1.42	.007	.13	.4	.02	2.2	.2	<.05	4	<.5
404514	.8	18.6	10.4	47	<.1	17.0	6.2	209	2.04	209.2	.7	23.0	2.9	16	.2	1.9	1.6	35	.16	.051	14	18	.33	136	.026	1	1.17	.007	.05	.4	.03	1.7	.1	<.05	4	<.5
404515	.8	25.5	7.6	53	<.1	22.4	8.8	240	2.10	84.5	.9	15.2	6.0	20	.2	.9	1.0	32	.17	.056	18	20	.40	151	.040	1	1.23	.007	.10	.4	.03	2.0	.2	<.05	3	<.5
404516	.7	30.1	8.5	61	<.1	24.2	11.6	286	2.47	197.9	1.0	16.5	6.9	20	.2	1.4	1.4	34	.15	.056	22	23	.49	173	.042	1	1.65	.006	.20	.5	.03	2.5	.3	<.05	4	.6
404517	.7	47.2	13.0	56	<.1	20.1	11.7	268	2.55	389.4	1.0	26.5	3.8	15	.3	6.8	2.4	39	.10	.046	16	21	.41	151	.023	1	1.42	.006	.08	.6	.03	2.4	.2	<.05	4	.6
404518	.7	46.1	14.0	60	<.1	21.9	10.6	277	2.46	499.4	.8	23.6	4.2	13	.6	3.1	1.9	30	.10	.046	16	20	.37	111	.019	1	1.32	.005	.08	.6	.03	1.9	.2	<.05	4	.5
404519	.7	40.5	10.9	58	<.1	24.9	11.2	354	2.58	296.2	1.0	25.2	4.8	17	.3	3.6	1.9	35	.13	.052	18	26	.45	162	.031	<1	1.49	.006	.07	.5	.02	2.5	.2	<.05	4	.5
404520 (pulp)	.7	26.0	6.6	37	<.1	33.3	8.5	372	2.02	10.3	.8	9.4	4.7	65	.3	.7	.1	46	3.27	.099	14	37	.81	174	.077	1	.85	.027	.08	.3	.04	2.9	.1	<.05	3	<.5
404521	.5	82.4	14.7	57	.2	34.1	14.8	421	3.25	620.8	1.3	51.9	13.8	28	.3	4.6	4.1	33	.19	.047	31	31	.66	218	.031	<1	2.07	.006	.18	.3	.02	3.8	.4	<.05	6	<.5
404522	.6	40.7	9.9	56	<.1	22.9	9.0	328	2.31	399.4	1.0	62.2	5.3	10	.4	17.8	1.8	25	.10	.050	21	16	.31	101	.018	<1	1.00	.004	.05	.4	.02	2.0	.1	<.05	3	.5
404523	.6	53.8	12.8	52	.1	25.0	12.3	394	2.64	536.2	1.2	55.9	9.8	11	.4	13.2	3.1	25	.09	.033	30	17	.35	190	.017	1	1.07	.004	.06	.5	.03	2.5	.2	<.05	3	<.5
404524	.5	41.3	8.9	56	<.1	24.6	10.9	284	2.69	352.0	1.3	24.7	6.5	15	.2	4.0	1.7	29	.13	.046	25	25	.52	205	.019	1	1.45	.004	.12	.2	.03	2.3	.3	<.05	4	.5
404525	.6	30.8	15.0	78	.1	30.0	15.2	1053	3.38	283.9	1.1	7.4	3.8	13	.2	2.3	6.0	48	.08	.076	20	43	.68	199	.037	<1	2.68	.006	.21	.2	.03	3.7	.4	<.05	9	.5
404526	.5	29.5	12.7	53	<.1	22.7	13.5	521	2.60	213.5	.8	5.2	5.5	9	.2	2.2	2.7	30	.08	.040	21	23	.47	90	.027	<1	1.36	.004	.14	.2	.01	2.0	.3	<.05	5	<.5
404527	1.0	18.7	12.0	52	<.1	15.6	7.0	312	2.43	98.4	.8	4.2	.5	9	.1	1.1	1.8	37	.08	.048	15	21	.34	127	.018	<1	1.30	.005	.05	.2	.02	1.1	.2	<.05	4	.5
404528	.8	21.0	10.5	63	<.1	19.4	9.5	668	2.48	143.4	.8	8.5	2.0	7	.1	1.3	1.2	35	.05	.049	16	24	.40	104	.027	1	1.48	.004	.07	.2	.03	1.7	.2	<.05	5	<.5
404529	.7	37.5	10.0	81	.8	28.7	10.5	429	2.66	564.7	3.7	8.7	1.1	14	.4	1.6	1.3	29	.13	.079	34	32	.38	107	.014	<1	1.35	.006	.08	.3	.04	1.8	.2	<.05	4	.5
404530	.9	23.7	9.7	71	<.1	19.8	9.0	368	2.41	106.6	1.2	18.9	1.8	10	.3	1.2	.6	38	.09	.062	19	23	.42	111	.025	1	1.35	.005	.06	.3	.04	1.9	.1	<.05	4	<.5
404531	1.0	23.5	9.6	64	<.1	19.3	12.3	519	2.53	103.5	1.0	18.3	2.3	9	.2	1.0	.8	40	.07	.049	19	26	.46	83	.029	1	1.48	.006	.08	.3	.03	1.8	.2	<.05	5	.5
404532	.6	42.2	11.1	83	<.1	29.4	19.1	631	2.65	284.9	1.6	6.9	8.5	16	1.2	1.7	1.8	29	.11	.052	38	21	.49	197	.032	1	1.28	.005	.14	.3	.02	2.5	.3	<.05	4	<.5
404533	.6	30.3	10.3	58	<.1	22.2	9.4	312	2.48	167.4	1.1	16.1	2.7	8	.3	1.5	1.5	31	.06	.049	26	20	.37	80	.018	1	1.19	.004	.10	.3	.03	1.3	.2	<.05	4	.5
STANDARD DS7	21.0	107.4	70.4	401	.9	55.9	9.5	623	2.37	47.3	4.9	70.4	4.4	69	6.2	5.8	4.4	86	.92	.078	12	163	1.04	372	.123	39	.96	.074	.44	3.8	.20	2.5	4.2	.21	4	3.6

GROUP 1DX - 30 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

2006-07-28 P02:38

Data L FA ____ DATE RECEIVED: JUL 7 2006 DATE REPORT MAILED:.....

BRITISH COLUMBIA CERTIFIED ASSAYER
Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	2.1	3.0	51	<.1	7.4	4.9	536	1.88	<.5	2.1	<.5	4.1	56	<.1	<.1	<.1	36	.46	.087	7	63	.64	213	.125	2	1.02	.081	.52	.1	<.01	3.1	.4	<.05	5	<.5
404534	.9	23.3	14.4	57	<.1	17.3	6.4	213	2.37	252.0	1.0	5.8	1.2	10	.1	1.6	1.0	35	.09	.058	16	20	.37	79	.015	2	1.19	.005	.04	.3	.03	1.3	.2	<.05	4	.5
404535	.9	29.9	10.2	53	<.1	18.4	8.1	241	2.51	408.1	.9	4.7	1.0	21	.2	2.1	1.9	35	.06	.053	18	20	.33	94	.014	1	1.20	.006	.04	.4	.02	1.2	.2	<.05	4	.6
404536	.8	17.0	10.2	48	<.1	16.2	7.8	276	2.30	53.8	.7	6.0	1.3	8	.2	.9	.3	33	.05	.045	14	18	.31	71	.015	1	1.05	.004	.03	.3	.02	1.1	.1	<.05	3	.5
404537	.9	26.7	10.5	55	.1	20.7	8.6	413	2.31	192.9	.9	2.4	1.0	10	.2	1.4	.8	31	.07	.073	17	18	.34	79	.017	2	1.08	.004	.06	.2	.02	1.2	.1	<.05	4	<.5
404538	.8	37.0	9.0	52	<.1	19.0	6.6	194	2.70	600.4	1.2	5.2	1.9	25	.1	4.0	3.6	30	.07	.048	28	20	.43	99	.016	1	1.31	.006	.10	.2	.03	1.2	.4	<.05	4	.7
404539	.6	78.4	13.8	51	.2	23.4	12.4	260	3.30	2039.8	1.3	47.5	6.6	25	.2	9.4	18.1	24	.06	.040	29	18	.44	127	.015	<1	1.39	.005	.13	.3	.02	2.0	.4	.06	4	.8
404540	.6	80.9	12.9	50	.2	23.9	13.2	254	3.37	1948.5	1.3	55.1	7.8	24	.2	8.8	18.1	23	.05	.038	30	18	.46	117	.015	1	1.44	.005	.15	.3	.02	2.1	.4	<.05	4	.8
404541	.7	43.9	9.9	52	.1	21.8	11.9	354	2.72	811.0	1.1	7.6	3.9	12	.2	3.3	4.2	26	.07	.048	25	16	.34	93	.013	1	1.10	.004	.08	.3	.02	1.3	.2	<.05	3	.6
404542	1.1	49.5	16.8	70	.2	25.0	12.4	479	3.08	820.8	1.2	13.5	2.6	14	.2	23.8	5.4	29	.08	.066	24	18	.34	92	.013	1	1.14	.005	.08	.4	.02	1.5	.2	<.05	3	.7
404543	.9	38.8	9.9	69	.2	23.0	8.5	278	2.74	679.7	1.3	12.7	3.9	15	.3	2.8	3.8	36	.14	.070	22	21	.39	137	.024	1	1.13	.006	.06	.5	.03	2.2	.1	<.05	4	.6
404544	.7	55.9	10.2	63	.1	32.2	14.3	450	3.04	1497.3	1.4	28.0	7.2	14	.3	9.1	5.0	21	.10	.061	30	13	.24	116	.009	1	.76	.004	.05	.3	.02	2.0	.1	<.05	2	.9
404545	.7	62.5	70.1	83	.4	33.7	16.9	744	4.35	1627.6	2.3	32.3	5.1	25	.4	21.3	8.2	23	.36	.111	37	20	.34	118	.005	1	1.32	.006	.07	.3	.03	2.5	.2	.06	4	.9
404546	.8	36.0	13.0	71	.1	28.0	10.1	375	2.95	521.9	1.5	36.8	3.5	24	.1	3.7	2.3	37	.21	.058	26	27	.51	156	.019	1	1.58	.007	.07	.4	.02	2.6	.2	<.05	5	.5
404547	.5	64.2	89.5	60	1.3	32.1	17.2	515	3.48	2352.6	2.0	43.9	7.8	56	.9	8.7	17.6	27	.34	.058	32	21	.42	157	.030	1	1.25	.015	.14	.8	.02	2.4	.3	<.05	4	<.5
404548	.7	26.8	11.7	56	<.1	21.6	10.0	438	2.67	378.4	1.3	22.5	1.9	23	.1	2.9	1.9	35	.18	.061	20	23	.39	127	.019	1	1.37	.007	.08	.4	.03	1.7	.2	<.05	5	<.5
404549	.5	43.9	15.0	61	.1	41.5	19.1	823	3.40	423.1	1.3	23.7	11.2	35	.2	3.6	5.1	34	.30	.071	26	30	.67	250	.036	1	2.25	.016	.15	.3	.01	3.7	.3	<.05	6	<.5
404550	.6	81.2	59.3	86	.8	42.2	18.6	623	4.53	2086.1	2.6	55.0	8.5	27	.6	31.8	8.7	17	.27	.078	57	17	.27	86	.004	3	.94	.007	.09	.3	.02	3.0	.2	<.05	3	1.2
RE 404550	.6	81.1	59.8	86	.8	40.7	18.5	599	4.48	2096.9	2.6	55.3	8.9	27	.6	30.5	8.9	16	.27	.083	57	17	.28	88	.004	2	1.00	.007	.09	.2	.02	3.1	.2	<.05	3	1.2
404551	.6	73.4	16.1	67	.1	50.8	46.5	665	3.33	1054.3	1.7	21.4	13.9	21	.4	12.5	5.8	19	.19	.053	38	20	.54	84	.005	1	1.31	.004	.09	.2	.01	1.8	.3	<.05	4	<.5
404552	.8	56.3	15.6	71	.1	37.2	22.7	436	3.20	681.2	1.6	24.5	8.1	52	.3	5.3	3.9	32	.20	.074	30	23	.48	122	.018	<1	1.38	.006	.14	1.8	.03	2.1	.3	<.05	4	<.5
404553	1.0	86.6	14.3	64	.1	37.1	22.3	746	3.76	745.0	1.7	28.5	7.4	62	.3	2.9	4.1	29	.16	.088	23	22	.42	142	.022	<1	1.84	.028	.17	1.6	.02	2.2	.3	.15	5	.9
404554	.6	20.3	9.4	59	<.1	19.8	8.8	294	2.05	341.9	.9	15.4	5.2	16	.3	2.6	1.2	27	.23	.081	17	18	.33	74	.023	1	.80	.004	.05	.9	.01	1.5	.1	<.05	2	<.5
404555	.7	24.7	10.8	75	<.1	24.2	9.9	385	2.47	714.6	2.5	9.1	4.4	17	.2	3.9	1.0	31	.21	.074	20	21	.40	101	.021	1	1.23	.005	.05	.4	.01	2.3	.1	<.05	3	.5
404556	.6	28.9	21.0	93	.3	20.9	10.1	422	2.64	1035.8	2.3	18.4	2.4	23	.7	6.7	3.1	33	.34	.071	21	26	.43	120	.016	1	1.38	.008	.07	.6	.02	2.0	.2	<.05	4	.5
404557	1.0	33.4	12.6	84	.2	31.2	10.4	389	2.60	537.6	1.3	13.2	5.8	23	.6	3.4	1.7	37	.27	.091	20	23	.42	157	.033	1	1.18	.007	.10	.8	.04	2.5	.2	<.05	3	.6
404558	1.0	29.1	13.7	86	.2	26.7	10.1	410	2.59	564.8	1.4	18.9	3.9	22	.5	5.1	1.4	33	.24	.066	19	22	.42	142	.024	1	1.08	.008	.09	.6	.03	2.2	.1	<.05	3	.5
404559	.8	53.7	27.9	68	.6	19.2	8.6	284	3.49	1222.9	1.4	64.6	3.3	16	.7	15.9	7.5	29	.15	.072	26	28	.42	89	.015	<1	1.39	.007	.12	1.1	.03	1.9	.3	<.05	4	1.1
404560 (pulp)	11.4	1156.4	4.6	45	.3	496.6	17.6	495	3.64	10.0	.3	119.5	1.2	62	.1	1.8	.2	57	1.08	.056	4	607	.69	127	.093	4	1.41	.111	.21	1.5	.19	3.9	.1	.77	5	2.7
404561	1.0	37.4	13.8	57	.2	25.9	14.8	409	2.95	298.4	1.5	11.8	2.7	15	.3	5.4	1.5	32	.15	.078	26	20	.37	81	.019	1	1.19	.005	.12	.6	.02	1.4	.2	<.05	4	.5
404562	1.0	36.6	14.7	61	.7	20.3	10.3	498	2.32	470.1	1.2	20.2	.9	32	.5	5.5	2.1	34	.42	.084	19	22	.37	162	.015	1	1.20	.009	.07	.9	.04	1.1	.2	<.05	5	.7
404563	.7	16.6	9.9	50	.1	14.3	6.5	230	2.03	181.6	.8	12.1	1.3	13	.2	3.5	.8	29	.16	.058	14	18	.33	110	.016	<1	1.04	.004	.05	.7	.02	1.3	.1	<.05	3	<.5
404564	.9	29.1	12.8	45	.3	16.4	7.5	230	2.36	486.9	1.3	24.8	.8	25	.2	4.5	2.2	34	.13	.064	18	18	.31	97	.011	1	1.24	.006	.07	.5	.04	1.0	.2	<.05	5	.7
404565	1.0	34.2	15.1	58	.3	21.7	9.1	267	2.59	883.2	3.0	32.3	1.2	31	.3	8.2	2.5	31	.48	.086	24	20	.32	108	.008	2	1.26	.007	.08	.6	.04	1.1	.2	<.05	4	1.0
404566	.5	92.5	18.5	93	.4	37.1	18.4	468	4.37	2229.5	2.9	86.9	11.3	53	.7	9.7	10.2	23	.73	.065	49	19	.42	70	.005	3	1.39	.014	.11	1.8	.02	2.7	.2	<.05	5	1.1
STANDARD DS7	21.0	110.1	71.9	411	.9	56.5	9.6	628	2.40	47.9	5.0	69.8	4.4	69	6.3	5.8	4.4	86	.93	.078	12	166	1.05	370	.123	39	.96	.074	.44	3.9	.21	2.5	4.2	.21	5	3.4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 6 FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.6	1.9	2.7	48	<.1	7.2	4.9	565	1.87	<.5	1.9	<.5	4.0	51	<.1	<.1	.1	35	.44	.088	6	63	.67	211	.124	1	1.00	.057	.51	.1	<.01	2.0	.4	<.05	5	<.5
404567	.9	75.0	12.0	81	.4	25.3	14.4	559	3.30	1076.6	1.7	94.8	2.9	64	.7	7.1	9.2	33	.23	.073	27	24	.44	130	.022	1	1.84	.010	.17	4.0	.03	1.7	.3	.06	6	.8
404568	.7	35.5	9.8	63	<.1	24.7	13.7	339	2.96	428.5	1.4	41.6	8.7	15	.2	6.3	2.2	27	.12	.046	30	25	.48	190	.044	1	1.39	.005	.21	.5	.02	2.2	.4	<.05	4	.5
404569	1.0	18.6	10.0	49	<.1	14.7	7.3	255	2.82	181.5	.8	3.8	2.5	9	.1	1.4	.9	35	.06	.040	16	21	.31	59	.022	<1	1.06	.004	.05	.3	.03	1.3	.1	<.05	4	.6
404570	.9	29.2	9.7	49	<.1	19.0	8.3	260	2.53	117.6	1.0	4.5	1.5	18	.1	3.0	.9	26	.09	.051	19	19	.31	73	.011	<1	1.06	.005	.04	.3	.02	1.0	.1	<.05	4	.5
404571	1.0	41.5	11.7	59	<.1	20.3	8.5	266	3.71	333.6	1.2	10.7	6.4	13	.3	3.9	2.1	34	.08	.052	26	23	.40	75	.017	1	1.37	.008	.04	.5	.03	1.7	.1	<.05	4	.7
404572	.8	12.4	8.8	36	<.1	11.8	5.6	145	2.06	58.7	.6	2.0	.3	7	.1	.7	.3	33	.06	.045	12	18	.25	52	.015	1	1.04	.004	.03	.3	.03	.8	.1	<.05	4	.5
404573	1.1	32.8	11.8	66	<.1	41.2	39.3	848	2.72	102.9	1.1	4.3	6.6	13	.2	1.4	.3	31	.12	.064	22	21	.40	87	.019	<1	1.40	.005	.04	.2	.01	2.1	.1	<.05	4	.5
404574	.8	23.6	10.8	62	<.1	18.4	11.3	402	2.73	331.8	1.1	13.8	6.0	17	.2	1.7	2.7	34	.13	.051	21	24	.41	109	.027	<1	1.45	.007	.07	.5	.04	2.2	.2	<.05	5	<.5
404575	.4	33.2	21.9	92	.2	29.0	12.6	457	2.94	130.0	1.1	7.4	9.2	79	.9	2.8	1.8	40	.34	.054	27	40	.69	172	.060	<1	2.48	.024	.26	.5	.03	4.4	.3	<.05	7	<.5
404576	.6	32.0	13.9	84	.2	23.8	10.8	402	2.68	125.2	1.5	22.9	7.9	36	.5	2.7	1.7	46	.29	.063	23	45	.61	168	.055	<1	1.67	.018	.15	.8	.04	4.3	.3	<.05	5	<.5
404577	.5	33.3	15.6	88	.2	25.7	12.1	424	2.55	147.2	1.0	5.2	7.3	30	1.0	2.5	2.4	30	.21	.076	21	25	.49	147	.038	<1	1.67	.008	.12	1.1	.03	2.6	.2	<.05	5	<.5
404578	.8	29.7	27.7	67	.1	25.5	8.7	304	2.17	124.7	.9	17.1	3.6	18	.5	1.4	1.1	30	.20	.081	16	18	.33	129	.029	1	1.13	.008	.05	.7	.03	2.0	.1	<.05	3	.5
404579	.8	25.9	13.3	69	<.1	21.4	10.5	371	2.50	77.0	1.1	8.3	2.8	14	.2	1.1	.6	36	.15	.063	15	23	.41	153	.030	1	1.53	.007	.05	.4	.03	2.2	.1	<.05	4	.5
404580	.5	25.1	6.0	35	<.1	30.4	8.4	348	1.92	8.0	.8	5.1	4.6	66	.3	.6	.1	40	3.20	.096	15	34	.77	165	.077	1	.86	.027	.07	.2	.03	3.0	.1	<.05	3	<.5
404581	.7	46.0	19.3	76	.4	24.7	11.4	390	2.79	574.5	1.2	17.4	4.7	18	.5	3.8	3.3	31	.21	.054	21	21	.38	169	.026	1	1.29	.007	.09	.7	.04	2.1	.2	<.05	4	.6
404582	.6	27.9	20.4	67	.1	20.1	9.4	382	2.40	156.3	1.1	13.9	3.4	15	.4	2.4	.9	32	.21	.065	19	21	.36	117	.027	1	1.11	.005	.05	.8	.04	1.8	.1	<.05	3	<.5
404583	.4	48.6	67.3	136	.8	30.2	11.2	388	3.40	755.3	1.4	31.0	10.7	44	2.5	7.7	6.0	30	.41	.065	30	29	.58	151	.036	<1	1.67	.012	.24	.2	.03	3.3	.4	<.05	6	<.5
404584	.6	24.3	18.5	66	.4	25.3	11.0	495	2.93	270.6	1.2	25.2	5.1	39	.6	1.7	1.5	34	.55	.054	23	28	.47	160	.037	1	1.87	.029	.09	.4	.05	3.3	.3	<.05	6	<.5
404585	.5	25.7	17.5	65	.5	23.9	11.2	443	2.64	463.6	1.2	11.3	6.7	38	.7	2.4	1.6	27	.43	.070	21	22	.44	151	.034	<1	1.64	.034	.17	.5	.05	2.8	.3	<.05	5	<.5
404586	1.2	13.4	12.1	46	.1	15.3	8.9	305	2.58	198.4	.8	16.0	3.8	31	.2	2.1	1.4	42	.18	.054	15	24	.31	110	.044	1	1.39	.006	.05	.4	.03	2.4	.1	<.05	4	.5
404587	.5	33.7	21.7	78	.3	30.6	13.3	651	3.43	316.6	1.5	6.1	6.2	87	.4	2.9	1.6	34	1.04	.079	46	29	.63	174	.034	1	2.19	.069	.16	.3	.03	3.7	.3	<.05	7	.5
404588	.3	44.8	37.2	71	.3	42.5	18.8	641	3.41	627.9	1.5	10.5	16.6	38	.4	8.6	2.3	22	.32	.058	59	21	.56	123	.053	<1	1.50	.012	.31	.2	.02	2.9	.5	.06	5	<.5
404589	.4	44.7	16.6	102	.4	49.2	17.3	487	3.26	417.1	1.7	36.7	15.1	41	1.1	4.0	3.2	27	.40	.063	59	24	.61	142	.072	<1	1.63	.018	.29	.1	.03	3.6	.5	<.05	5	<.5
404590	.9	17.5	9.0	53	<.1	15.0	7.0	354	2.39	185.1	.8	5.9	.9	10	.2	1.3	.8	33	.07	.047	16	18	.28	73	.017	1	.99	.004	.04	.4	.02	1.1	.1	<.05	4	.5
404591	.7	21.8	12.4	59	<.1	18.3	7.6	339	2.46	306.5	1.0	8.0	1.2	13	.4	2.6	1.0	32	.16	.050	18	18	.30	135	.016	1	1.00	.004	.04	.4	.03	1.4	.1	<.05	3	<.5
404592	.6	29.2	14.3	63	.2	21.6	8.4	416	2.62	487.2	1.1	4.3	2.6	15	.3	4.9	1.7	28	.16	.051	26	19	.35	141	.016	1	1.12	.006	.05	.3	.03	1.9	.2	<.05	4	<.5
404593	.6	20.5	10.9	48	<.1	17.2	6.8	228	2.37	202.6	.9	5.6	1.4	15	.1	1.3	.6	31	.20	.048	18	17	.33	112	.017	1	1.15	.005	.05	.3	.03	1.3	.2	<.05	4	.5
404594	.6	53.8	10.0	54	.2	24.3	14.7	307	3.48	1253.9	2.1	20.7	14.2	27	.2	3.0	3.3	22	.14	.065	43	19	.54	167	.018	<1	1.38	.011	.11	.2	.02	2.1	.3	<.05	4	<.5
404595	.6	22.8	13.6	55	<.1	24.6	10.7	433	2.44	106.9	.8	16.3	6.1	19	.2	1.8	.5	27	.17	.053	25	16	.39	147	.028	2	1.15	.005	.09	.3	.02	1.7	.3	<.05	3	<.5
404596	.3	33.9	10.1	98	<.1	36.5	17.0	395	4.35	151.7	2.0	1.4	21.1	15	.1	2.2	.4	22	.05	.043	50	39	1.08	51	.008	<1	2.21	.003	.07	<.1	.01	1.7	.2	<.05	7	<.5
404597	.7	27.9	9.7	55	<.1	22.0	9.5	260	2.56	173.7	.8	2.7	5.5	12	.2	1.5	.9	26	.10	.053	20	18	.41	66	.017	2	1.18	.004	.05	.3	.02	1.6	.2	<.05	3	.6
404598	.6	23.0	7.8	48	<.1	17.0	7.3	269	1.90	517.0	.7	25.4	4.8	12	.2	2.3	2.8	22	.13	.058	15	13	.29	55	.017	2	.79	.006	.04	.3	.02	1.4	.1	<.05	2	.6
404599	1.0	26.7	10.2	53	<.1	20.0	9.1	325	2.36	271.6	.8	4.8	1.7	10	.2	1.5	1.8	33	.08	.050	18	18	.33	101	.016	2	1.22	.004	.05	.2	.03	1.5	.1	<.05	4	.7
RE 404599	.8	26.7	10.4	55	<.1	18.9	9.2	335	2.40	277.6	.8	4.0	1.7	10	.2	1.5	1.9	33	.07	.052	18	18	.34	104	.016	2	1.29	.005	.05	.3	.03	1.5	.1	<.05	4	.7
STANDARD	21.3	108.8	72.1	412	.9	56.5	9.6	633	2.41	48.0	5.0	69.2	4.4	68	6.4	5.9	4.5	87	.93	.080	13	165	1.07	373	.122	39	.97	.073	.44	4.0	.21	2.4	4.3	.20	5	3.6

Standard is STANDARD DS7. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.5	2.0	2.4	46	<.1	7.4	4.6	538	1.80	<.5	1.9	1.2	3.9	49	<.1	<.1	.1	36	.43	.087	6	61	.66	204	.123	1	.99	.059	.53	.1	<.01	2.2	.4	<.05	5	<.5
404600	.7	27.7	10.4	52	<.1	19.7	9.5	344	2.34	286.7	.8	4.6	2.2	9	.2	1.7	2.0	30	.07	.049	17	18	.34	100	.015	1	1.22	.004	.05	.3	.04	1.4	.2	<.05	3	.6
404601	.6	23.4	9.3	52	<.1	17.6	9.2	210	2.32	149.0	1.0	3.1	2.4	12	.2	1.5	.8	27	.10	.054	20	19	.40	106	.021	2	1.25	.005	.14	.4	.02	1.3	.3	<.05	4	<.5
404602	1.0	23.0	10.5	53	<.1	17.8	9.2	243	2.37	84.3	.9	6.8	3.9	12	.2	1.1	.6	31	.08	.050	16	19	.39	111	.022	1	1.37	.005	.09	.6	.03	1.7	.2	<.05	3	.7
404603	.9	19.5	9.3	55	<.1	17.3	7.9	253	2.34	59.5	1.0	5.9	2.3	9	.2	1.1	.4	35	.09	.059	15	21	.38	110	.019	1	1.33	.005	.07	.6	.03	1.7	.2	<.05	4	.6
404604	.8	20.1	9.7	57	<.1	19.7	7.5	237	2.42	97.4	1.0	5.8	2.5	11	.3	1.3	.5	34	.10	.057	17	21	.40	117	.023	2	1.37	.005	.10	.6	.03	1.6	.2	<.05	4	.6
404605	.7	33.8	9.8	62	.1	22.9	11.4	321	2.59	322.7	1.3	17.0	8.1	16	.2	5.1	2.0	30	.13	.058	24	20	.41	113	.031	1	1.21	.005	.17	1.6	.04	1.9	.2	<.05	4	.6
404606	1.1	22.4	10.9	68	<.1	18.2	9.4	327	2.68	157.0	1.2	11.2	1.2	10	.2	4.7	1.0	38	.08	.056	15	23	.40	118	.018	1	1.47	.004	.07	.6	.04	1.4	.2	<.05	4	.7
404607	.9	23.0	11.3	58	.1	20.5	9.9	315	2.43	143.7	1.1	6.2	1.8	15	.3	2.3	.8	33	.11	.062	19	19	.36	126	.020	1	1.21	.005	.08	.5	.02	1.1	.1	<.05	4	.5
404608	.7	19.6	10.2	50	<.1	17.8	9.4	274	2.21	152.1	1.0	4.6	2.7	8	.2	2.3	.5	28	.07	.047	15	17	.32	68	.018	<1	1.03	.004	.04	.3	.03	1.2	.1	<.05	3	.5
404609	.8	14.8	14.1	33	<.1	10.3	3.3	86	1.94	144.3	.7	8.4	.7	6	.2	3.7	.7	27	.04	.032	14	15	.20	42	.014	1	.88	.003	.04	.2	.03	.6	.1	<.05	3	.5
404610	.7	35.8	19.6	66	.2	23.8	9.5	337	2.56	730.7	1.7	45.6	5.4	17	.5	9.3	3.0	25	.16	.053	24	19	.39	100	.016	1	1.13	.004	.07	.9	.02	2.2	.2	<.05	3	<.5
404611	.8	29.1	13.5	71	<.1	21.4	14.5	644	2.59	764.3	1.4	25.5	1.8	22	.5	6.7	2.3	26	.23	.057	19	20	.37	103	.014	1	1.09	.007	.07	.7	.02	1.3	.2	<.05	3	.6
404612	.7	18.1	10.7	61	.2	18.6	8.4	415	2.26	850.0	1.8	9.6	1.5	22	.3	3.4	.8	28	.30	.070	16	20	.40	85	.016	1	1.17	.006	.06	.4	.04	1.3	.1	<.05	4	.7
404613	.7	24.5	12.1	65	.1	21.3	9.2	317	2.62	727.1	1.7	25.3	1.9	13	.2	5.3	2.0	30	.12	.064	18	21	.41	94	.015	1	1.36	.004	.06	.7	.03	1.4	.2	<.05	4	.6
404614	.5	51.3	18.7	74	.4	35.3	12.4	449	2.94	1105.8	4.2	17.1	3.5	46	.5	10.2	4.0	24	.44	.102	29	23	.44	116	.015	1	1.32	.010	.09	.3	.05	1.9	.3	.06	4	1.6
404615	.7	24.2	10.1	63	<.1	22.6	11.1	359	2.48	892.8	1.5	23.7	1.9	15	.2	2.5	1.8	31	.17	.077	17	23	.37	107	.019	1	1.18	.005	.06	.7	.03	1.5	.1	<.05	4	.8
404616	1.0	19.7	9.8	47	<.1	15.1	6.0	191	2.36	381.2	.8	9.8	.7	9	.2	1.5	1.1	40	.07	.043	14	20	.30	70	.021	1	.98	.004	.04	.3	.04	1.0	.1	<.05	4	.5
RE 404616	.9	18.2	9.6	45	<.1	14.7	5.5	176	2.22	364.2	.7	10.0	.7	8	.2	1.4	1.1	38	.07	.041	13	18	.29	66	.018	1	.95	.004	.04	.3	.03	1.0	.1	<.05	4	.5
404617	.8	30.6	13.3	62	.2	16.9	8.9	593	2.48	898.1	1.3	51.5	.6	27	.5	2.7	3.6	32	.49	.074	15	22	.34	109	.012	1	1.19	.008	.05	.4	.03	.8	.2	<.05	4	.6
404618	.8	48.2	34.9	72	.6	20.4	9.7	272	3.23	1438.7	2.0	65.2	4.0	15	.9	17.8	7.6	27	.09	.057	35	20	.20	74	.010	1	1.03	.006	.08	.6	.03	1.4	.2	<.05	4	1.0
404619	1.0	93.9	49.7	93	.8	34.3	16.4	444	3.97	3280.5	2.7	129.2	18.9	31	1.6	35.2	11.0	22	.37	.066	48	19	.31	182	.015	3	.93	.009	.10	1.1	.05	3.0	.2	<.05	2	1.3
404620	.7	25.8	6.3	37	<.1	33.8	8.3	371	2.02	10.6	.9	4.8	4.7	68	.3	.6	.1	46	3.32	.099	15	37	.81	172	.082	1	.90	.028	.08	.3	.03	3.1	.1	<.05	3	<.5
404621	.6	39.5	43.8	77	.6	22.3	10.4	397	2.59	743.3	1.2	21.5	5.9	23	.9	11.0	3.5	39	.25	.059	17	35	.52	188	.043	1	1.29	.011	.09	.8	.03	3.1	.2	<.05	4	.5
404622	.8	34.9	32.6	64	.4	22.9	10.4	310	2.51	652.1	.9	15.8	5.7	14	.7	5.6	3.1	35	.15	.052	18	20	.33	147	.024	1	1.38	.006	.06	.7	.03	2.2	.1	<.05	4	.5
404623	.9	58.6	35.1	91	1.2	24.2	11.1	432	3.02	1137.6	1.2	64.4	3.4	30	1.3	13.8	10.3	30	.26	.065	22	22	.39	125	.011	2	1.44	.009	.08	1.2	.04	1.9	.3	<.05	5	.7
404624	.8	34.1	14.8	64	.3	21.6	9.0	269	2.62	408.0	1.3	9.0	3.2	20	.4	1.9	3.1	39	.23	.061	17	24	.41	208	.029	<1	1.45	.009	.09	.7	.04	2.1	.2	<.05	5	.5
404625	.6	41.9	17.1	96	.3	31.1	12.4	400	3.39	270.5	1.7	26.7	9.5	30	.6	3.1	2.3	41	.40	.053	28	36	.72	216	.054	1	2.06	.032	.28	.9	.04	3.4	.4	<.05	7	<.5
404626	.6	43.0	22.0	88	.4	27.6	10.9	419	3.27	366.0	1.4	16.5	6.2	32	.4	9.0	3.2	39	.38	.052	26	32	.61	152	.039	1	1.87	.013	.16	.5	.03	3.0	.3	<.05	6	.6
404627	.6	43.7	17.5	101	.5	26.0	9.8	510	2.85	245.3	1.5	27.5	4.7	51	.7	4.5	2.7	36	.54	.075	29	29	.58	210	.025	1	1.79	.012	.09	.5	.04	3.1	.2	<.05	6	.6
404628	.5	30.5	21.1	89	.4	23.3	8.8	425	2.73	172.7	1.4	6.8	5.0	39	.7	6.0	1.7	47	.56	.066	22	46	.71	196	.039	2	1.66	.018	.10	.4	.04	4.0	.2	<.05	5	<.5
404629	.6	29.9	17.3	82	.5	26.9	10.0	548	2.78	188.7	1.5	11.3	4.8	43	.7	3.8	1.5	40	.46	.072	26	31	.48	192	.025	2	1.61	.021	.06	.7	.04	3.6	.2	<.05	5	<.5
404630	.9	23.1	15.1	71	.2	21.6	10.2	330	2.64	120.0	1.6	8.7	1.6	13	.2	3.6	1.0	44	.14	.059	18	30	.49	144	.025	2	1.62	.006	.07	.3	.04	2.3	.2	<.05	5	.5
404631	.8	24.2	25.2	85	.2	24.4	9.3	375	2.79	165.8	1.4	6.2	3.4	19	.6	6.2	1.5	44	.25	.064	21	32	.52	170	.033	2	1.55	.006	.08	.4	.03	2.9	.2	<.05	5	.5
404632	.8	23.0	20.5	84	.2	25.4	9.9	426	2.78	113.2	1.0	8.9	3.6	15	.4	5.6	.9	43	.21	.067	21	31	.53	156	.030	2	1.59	.005	.07	.4	.03	2.6	.2	<.05	5	<.5
STANDARD DS7	20.9	108.2	70.3	405	.9	55.5	9.5	625	2.38	47.3	4.9	71.1	4.3	68	6.3	5.8	4.4	86	.92	.078	11	163	1.04	371	.122	39	.95	.074	.44	3.8	.20	2.5	4.2	.20	4	3.5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
404633	.5	30.2	34.1	101	.5	30.0	11.1	514	3.16	108.2	1.2	6.8	8.0	25	1.1	19.0	.9	24	.49	.052	36	20	.34	142	.012	4	1.10	.009	.07	.2	.04	3.7	.1	<.05	3	<.5
404634	.4	20.5	46.9	100	.4	26.6	8.8	427	2.79	87.6	1.0	8.0	7.6	36	1.0	7.2	.3	25	.68	.050	27	20	.46	146	.025	1	1.23	.015	.12	.3	.03	3.1	.2	<.05	4	<.5
404635	.4	25.8	36.8	95	.4	26.9	9.2	424	2.94	108.7	.9	2.9	11.7	21	1.1	8.4	.5	23	.38	.051	40	19	.46	132	.033	2	1.26	.005	.17	.2	.04	3.2	.2	<.05	4	<.5
404636	.6	20.2	28.8	60	.3	22.2	8.5	379	2.58	51.2	.9	21.3	4.2	15	.3	4.6	.3	28	.24	.044	24	19	.37	119	.018	1	1.10	.004	.07	.3	.04	2.2	.1	<.05	3	.6
404637	.4	53.5	49.7	147	.5	72.6	41.2	1476	5.46	88.2	2.1	14.9	26.4	24	2.2	15.7	4.1	19	.56	.075	99	21	.43	117	.009	2	1.15	.005	.22	.5	.03	3.9	.3	<.05	4	.7
404638	.6	63.2	32.4	85	.2	30.2	13.0	355	3.82	140.1	1.7	22.0	20.9	11	.3	8.2	9.6	19	.04	.047	48	26	.51	94	.012	<1	1.34	.004	.27	.1	.03	1.8	.4	.09	5	1.0
404640	.7	60.5	9.9	61	.2	27.2	14.2	270	2.87	305.3	1.2	28.7	8.4	17	.4	2.0	4.7	26	.13	.066	24	19	.41	101	.024	<1	1.17	.007	.10	.4	.04	1.8	.3	<.05	3	.8
404641	.6	59.1	9.5	60	.2	27.2	13.5	263	2.82	298.3	1.1	31.2	8.6	16	.4	2.0	4.0	25	.13	.065	22	18	.39	96	.023	<1	1.11	.006	.09	.4	.02	1.7	.2	<.05	3	.7
404642	.9	37.4	10.3	48	.1	17.4	6.9	171	2.51	222.8	1.2	15.1	2.7	10	.2	2.0	2.6	27	.07	.051	21	18	.32	73	.015	<1	1.02	.005	.06	.4	.03	1.3	.2	<.05	3	.8
404643	.4	53.5	26.6	77	.1	27.5	12.6	455	3.48	258.1	1.8	23.2	9.4	18	.6	10.3	4.6	18	.23	.054	49	20	.44	89	.008	1	1.26	.005	.14	.2	.02	2.0	.3	<.05	4	.7
404644	.4	57.1	29.1	82	.3	29.2	12.4	433	3.46	260.5	1.8	28.5	13.4	21	.6	11.6	4.7	16	.38	.061	54	20	.44	77	.008	1	1.25	.005	.15	.3	.03	2.2	.3	<.05	4	.6
404645	.3	37.9	48.1	94	.3	26.8	9.4	222	3.34	232.3	1.7	15.7	13.7	26	.7	22.0	2.2	13	.52	.058	48	14	.37	63	.008	<1	1.08	.004	.11	.1	.02	1.9	.2	<.05	3	.5
404646	.4	39.3	48.2	122	.3	27.8	10.6	310	3.44	318.1	1.9	14.9	12.5	29	1.6	23.3	2.6	13	.54	.055	43	15	.36	72	.008	1	1.07	.004	.13	.1	.02	1.9	.2	<.05	3	.5
404647	.8	27.7	46.2	85	.2	20.8	15.4	679	2.95	384.0	1.6	17.6	2.2	17	1.9	7.1	1.9	27	.21	.077	30	19	.39	118	.009	1	1.33	.005	.07	.2	.02	1.2	.2	<.05	5	.5
404648	.9	25.7	9.5	64	<.1	24.0	10.5	368	2.29	23.5	.8	2.6	2.2	12	.3	1.0	.2	37	.12	.057	17	20	.40	103	.030	1	1.22	.005	.05	.3	.03	1.9	.1	<.05	4	.5
404649	.7	22.8	9.9	56	<.1	16.1	7.0	202	2.30	268.7	.9	4.6	1.0	10	.2	1.5	.6	33	.09	.054	18	18	.33	78	.018	<1	1.23	.004	.04	.2	.03	1.2	.1	<.05	4	.6
404650	.9	31.1	10.2	59	<.1	17.8	6.6	201	2.70	205.1	1.0	3.8	1.5	17	.2	2.1	.6	34	.07	.058	28	20	.39	85	.017	<1	1.33	.004	.05	.2	.02	1.2	.2	<.05	5	.5
RE 404650	.8	30.1	10.8	56	<.1	17.1	6.7	198	2.65	206.0	1.0	4.0	1.5	17	.3	2.0	.6	34	.07	.055	28	20	.39	86	.016	1	1.33	.004	.05	.2	.03	1.3	.2	<.05	4	.6
404651	1.0	31.2	10.1	63	<.1	20.4	8.8	274	2.64	127.5	1.2	2.8	1.6	13	.2	1.3	.6	34	.09	.064	22	21	.40	109	.018	<1	1.36	.005	.04	.2	.03	1.5	.1	<.05	4	.6
404652	.7	59.6	10.4	56	.1	20.9	11.3	300	3.19	455.5	1.7	3.4	6.8	17	.2	1.6	2.3	25	.08	.039	38	21	.48	141	.022	1	1.44	.009	.11	.3	.02	1.9	.4	<.05	5	<.5
404653	.7	44.4	29.9	64	.3	31.0	18.2	517	2.87	432.0	1.1	10.0	7.6	11	.3	11.7	1.1	19	.05	.031	26	11	.21	101	.010	1	.76	.003	.05	.2	.03	1.9	.1	<.05	2	<.5
404654	.5	77.9	11.7	64	.7	39.7	21.2	988	3.62	1763.6	2.1	46.3	12.1	15	.2	4.0	23.5	13	.07	.048	50	8	.12	140	.004	1	.61	.006	.06	.7	.03	2.4	.1	<.05	1	1.0
404655	.8	42.7	10.8	60	.1	24.6	10.6	450	3.06	552.5	1.2	12.1	2.1	11	.1	2.5	3.5	29	.05	.057	31	17	.26	83	.011	1	1.09	.005	.06	.4	.03	1.6	.2	<.05	3	.6
404656	.9	62.5	14.0	58	.3	22.9	9.5	276	3.25	1179.5	1.5	14.9	4.3	17	.2	7.4	8.7	26	.07	.053	34	17	.34	96	.012	1	1.12	.006	.08	.5	.02	1.6	.2	<.05	4	.7
404657	.5	131.6	20.0	63	.4	39.5	25.1	732	3.97	2906.5	1.9	33.1	13.9	26	.2	9.3	24.4	22	.20	.078	55	21	.44	211	.016	1	1.30	.009	.13	1.0	.02	2.9	.3	<.05	4	1.4
404658	.6	210.8	20.5	63	.2	39.6	23.6	1193	5.19	3657.9	2.0	61.4	13.2	23	.2	8.5	41.5	20	.18	.073	58	16	.32	132	.007	1	1.44	.010	.10	.3	.03	3.2	.3	<.05	5	1.6
404659	.8	61.5	12.0	69	.2	26.8	13.1	351	3.37	868.0	1.7	8.2	14.1	19	.1	8.2	4.9	20	.14	.056	46	15	.32	101	.024	<1	1.00	.005	.10	.2	.02	2.6	.2	<.05	3	.7
404660 (pulp)	17.3	5861.6	14.9	90	1.4	405.5	18.5	762	7.44	10.2	.2	521.7	1.3	114	.5	7.9	.5	41	1.96	.083	4	462	.80	35	.002	12	.82	.050	.37	1.1	.98	4.3	.1	3.91	3	14.7
404661	.7	70.2	16.9	69	.3	30.4	11.3	332	3.43	1044.9	1.8	14.8	7.8	21	.2	8.6	7.1	24	.12	.057	50	19	.33	115	.011	1	1.17	.006	.09	.2	.03	2.4	.2	<.05	4	.6
404662	.5	66.5	12.6	64	.2	32.9	17.9	437	4.70	476.8	3.1	7.6	22.6	23	.1	4.5	2.4	21	.26	.073	66	22	.73	75	.015	<1	1.83	.007	.18	.1	.02	2.4	.4	<.05	6	.5
404663	.6	39.6	13.4	81	<.1	30.9	12.1	378	3.21	487.2	1.9	7.8	8.9	19	.3	4.0	1.6	26	.16	.053	43	24	.61	118	.021	<1	1.66	.005	.11	.3	.02	2.2	.3	<.05	5	<.5
404664	.7	26.0	11.2	59	<.1	29.7	12.5	244	2.70	300.5	1.5	6.2	3.6	38	.2	11.7	1.3	29	.25	.095	22	20	.37	112	.024	1	1.52	.007	.09	.5	.03	1.6	.3	<.05	5	.5
404665	.4	18.1	9.6	55	<.1	17.1	6.9	104	2.82	611.7	1.0	.5	11.3	18	.1	22.3	.5	26	.41	.023	16	19	.44	93	.021	<1	1.34	.004	.22	.1	.01	1.1	.3	<.05	7	<.5
404666	.4	41.0	35.1	76	.3	37.4	15.8	298	2.94	686.6	1.9	14.8	10.3	31	.6	4.3	2.0	28	.34	.058	41	22	.55	108	.023	1	1.55	.013	.12	.3	.02	2.1	.2	<.05	5	<.5
STANDARD DS7	21.2	110.1	71.7	417	.9	56.8	9.7	635	2.43	47.7	4.9	72.9	4.4	67	6.3	5.8	4.5	86	.93	.080	12	165	1.08	369	.123	38	.98	.072	.43	4.0	.21	2.4	4.3	.20	5	3.6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	1.6	2.9	45	<.1	4.0	4.5	519	1.91	<.5	1.7	<.5	3.6	56	<.1	<.1	<.1	35	.45	.076	7	7	.61	193	.123	1	1.00	.068	.48	.1	<.01	1.8	.4	<.05	4	<.5
404667	.7	31.4	16.9	67	<.1	23.4	10.5	440	2.92	505.3	1.2	9.0	6.1	27	.7	3.9	3.4	32	.14	.055	20	22	.41	77	.023	1	1.25	.007	.09	.4	.03	1.7	.2	<.05	4	.5
404668	.4	49.2	19.1	74	.3	30.2	13.0	501	3.76	1230.8	1.7	40.7	9.4	27	.4	36.6	6.9	20	.39	.063	50	16	.33	103	.009	2	1.07	.009	.09	.4	.03	2.9	.2	<.05	3	<.5
404669	.5	61.6	26.2	82	.4	33.3	15.4	394	3.87	1408.7	2.1	40.8	12.1	69	.9	15.4	10.6	27	.40	.069	39	30	.59	140	.026	<1	1.55	.013	.25	.5	.02	3.2	.5	<.05	5	<.5
404670	.7	28.0	14.4	65	<.1	20.1	9.3	284	2.96	281.2	.8	5.1	4.3	8	.4	5.3	1.4	28	.07	.060	20	20	.35	49	.020	1	1.04	.004	.06	.3	.02	1.3	.1	<.05	3	<.5
404671	1.5	32.4	19.3	58	<.1	21.0	10.3	273	2.55	821.4	.9	15.8	5.1	14	.5	2.9	4.7	32	.12	.055	18	18	.33	87	.021	1	1.03	.005	.07	.6	.03	1.7	.2	<.05	3	.6
404672	1.2	30.8	8.1	35	.1	11.4	5.0	161	2.27	496.3	1.0	7.2	.5	10	.1	1.3	1.3	32	.05	.058	16	16	.22	52	.015	1	.87	.007	.04	.3	.04	.7	.1	<.05	3	.7
404673	.7	11.8	17.3	48	<.1	12.9	6.1	242	1.99	137.0	.6	4.5	2.8	9	.3	2.5	.7	35	.08	.041	13	21	.28	79	.025	<1	1.19	.004	.03	.3	.04	1.7	.1	<.05	4	<.5
RE 404707	1.0	21.3	9.3	61	<.1	18.0	7.5	245	2.54	119.0	1.1	10.1	1.8	12	.1	1.4	.5	43	.09	.052	17	25	.43	76	.033	<1	1.43	.005	.07	.4	.03	1.8	.2	<.05	5	.5
404674	.6	72.5	116.4	175	2.1	30.5	12.4	492	3.95	1967.6	1.5	105.6	11.4	31	5.0	29.1	15.1	34	.29	.057	39	30	.47	172	.035	1	1.56	.011	.16	.6	.05	3.4	.3	<.05	4	<.5
404675	1.8	29.9	14.1	52	.2	19.2	11.5	412	3.48	786.2	1.1	18.5	4.6	16	.4	8.1	2.2	42	.09	.045	25	20	.27	74	.035	1	1.17	.005	.13	.5	.04	1.5	.2	<.05	5	.5
404676	.7	49.0	13.2	106	<.1	47.9	12.0	409	3.98	898.5	1.2	13.0	6.5	32	.6	14.7	4.1	43	.12	.052	34	29	.81	179	.060	1	2.14	.007	.29	2.3	.03	3.2	.4	<.05	8	.5
404677	1.0	55.0	12.6	73	.1	23.2	10.4	319	3.94	1579.6	1.3	22.1	7.3	18	.6	8.7	4.7	29	.11	.042	35	19	.43	74	.028	1	1.42	.005	.15	3.4	.02	1.6	.2	<.05	5	<.5
404701	.7	17.1	7.7	52	<.1	21.5	10.0	283	2.11	35.6	.7	10.0	4.2	12	.2	1.2	.3	27	.14	.056	15	16	.32	80	.027	1	.95	.004	.06	.3	.03	1.7	.1	<.05	3	<.5
404702	.9	18.9	10.9	49	<.1	16.4	7.0	209	2.65	67.2	.9	3.6	1.2	9	.1	1.1	.5	39	.07	.053	17	22	.35	81	.022	1	1.38	.005	.06	.3	.03	1.3	.2	<.05	4	<.5
404703	.9	22.9	10.7	60	<.1	23.7	8.7	288	2.90	296.1	1.1	41.4	3.5	9	.2	8.5	1.0	31	.06	.048	25	19	.31	88	.017	2	1.24	.005	.07	.3	.03	1.7	.2	<.05	4	.5
404704	.8	21.9	9.1	54	<.1	17.2	7.4	232	2.52	382.6	.9	10.9	2.2	14	.2	2.1	1.5	39	.07	.051	19	20	.36	111	.026	1	1.37	.005	.10	1.0	.03	1.8	.3	<.05	5	.5
404705	.6	35.5	10.5	68	.1	31.7	21.0	367	2.99	378.7	1.3	21.9	9.5	21	.3	2.4	1.4	31	.12	.056	28	24	.56	225	.049	<1	1.76	.006	.32	.5	.02	2.5	.4	<.05	5	<.5
404706	.9	34.3	10.4	75	.2	28.3	11.1	282	3.00	301.0	1.5	77.9	5.2	24	.3	2.9	1.7	39	.11	.058	25	28	.56	136	.045	1	1.79	.007	.21	.6	.02	2.7	.3	<.05	5	<.5
404707	1.0	21.3	9.0	61	.1	18.5	7.7	245	2.60	121.0	1.0	110.0	1.6	13	.1	1.3	.5	44	.10	.054	18	24	.43	78	.034	1	1.48	.005	.07	.3	.03	2.0	.2	<.05	5	<.5
404708	.8	21.2	9.5	60	<.1	20.0	9.1	267	2.54	60.7	.9	8.1	4.8	11	.3	2.3	.5	33	.12	.065	19	20	.39	101	.027	2	1.32	.004	.09	.3	.03	2.4	.2	<.05	4	.5
404709	.7	21.7	17.7	71	<.1	20.3	8.4	230	2.49	78.3	1.2	7.7	4.1	12	.3	3.0	.8	30	.11	.041	28	21	.39	138	.020	2	1.29	.005	.12	.3	.02	2.4	.3	<.05	4	<.5
404710	.7	16.4	8.7	57	<.1	17.5	8.3	244	2.42	55.5	1.0	9.5	2.2	10	.1	1.9	.6	36	.09	.050	20	23	.41	120	.022	2	1.48	.005	.09	.4	.04	2.1	.2	<.05	4	.5
404711	.8	32.1	14.9	66	.1	19.1	9.7	278	2.99	274.0	1.5	40.0	3.3	22	.2	3.0	6.4	53	.13	.050	19	27	.54	196	.044	1	2.00	.008	.16	.4	.03	3.9	.3	<.05	6	.5
404712	.5	33.4	10.7	52	.1	24.8	13.3	300	2.50	379.9	1.0	22.9	6.7	25	.3	2.0	1.9	40	.12	.041	18	30	.55	218	.056	1	1.85	.009	.20	.5	.01	3.6	.3	<.05	6	<.5
404713	.5	58.3	8.6	58	<.1	33.9	27.4	386	3.26	756.3	1.6	36.3	10.3	53	.3	3.6	2.7	34	.09	.034	26	29	.52	261	.057	1	1.96	.011	.22	2.0	.02	3.6	.4	.07	6	.5
404714	.7	20.9	7.9	52	<.1	16.6	5.6	250	2.33	306.6	.7	16.7	1.2	12	.3	1.5	1.5	31	.06	.047	13	20	.33	92	.021	1	1.33	.005	.05	.8	.03	1.2	.1	<.05	5	<.5
404715	.6	33.2	9.8	55	<.1	21.8	10.7	329	2.62	437.8	1.2	33.7	4.1	17	.2	2.4	2.4	33	.08	.036	18	21	.41	129	.027	1	1.61	.007	.07	1.0	.02	2.5	.2	<.05	4	.5
404716	.6	44.0	9.7	47	.1	21.4	9.2	296	2.49	442.7	1.7	34.8	4.9	23	.2	2.8	2.2	31	.08	.033	21	21	.38	165	.028	1	1.38	.009	.08	.6	.03	2.5	.2	<.05	4	.6
404717	.7	39.2	10.2	55	.2	21.7	9.8	414	2.77	483.4	1.1	64.8	4.2	15	.3	2.7	3.3	36	.10	.051	20	26	.41	161	.034	1	1.76	.006	.06	1.1	.04	3.0	.2	<.05	5	.5
404718	.9	22.1	9.2	60	<.1	18.7	6.7	347	2.65	307.9	.9	31.9	1.2	9	.2	1.6	1.4	39	.06	.047	15	26	.38	103	.024	1	1.59	.004	.06	.4	.03	1.7	.1	<.05	5	.5
404719	.8	30.4	10.5	57	<.1	21.8	9.4	398	2.53	394.4	1.2	45.0	2.2	10	.3	2.2	2.9	36	.09	.057	18	22	.38	108	.024	1	1.39	.005	.06	.7	.03	2.2	.2	<.05	4	.5
404720 (pulp)	.6	21.6	5.8	36	<.1	31.4	8.4	369	1.98	8.1	.9	5.7	4.6	70	.3	.6	.1	47	3.40	.097	16	38	.79	170	.084	2	.83	.031	.07	.3	.03	3.3	.1	<.05	3	<.5
404721	.6	24.6	9.1	44	.1	17.5	8.2	357	2.28	380.2	.9	57.7	3.4	8	.2	3.1	2.5	27	.07	.040	17	16	.30	78	.018	1	.97	.004	.05	.5	.03	1.8	.1	<.05	3	.6
404722	.7	33.6	10.7	56	<.1	18.3	11.5	463	2.57	494.0	.8	34.4	5.6	7	.6	5.3	2.8	26	.05	.035	25	16	.30	63	.020	2	1.16	.004	.08	.5	.03	1.7	.2	<.05	3	<.5
STANDARD DS7	21.5	115.9	72.0	422	.9	56.9	9.8	618	2.39	48.1	4.9	70.7	4.4	69	6.4	6.1	4.6	86	.92	.078	12	164	1.05	378	.123	38	.97	.073	.44	3.9	.20	2.4	4.2	.21	5	3.2

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data A FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	1.7	3.4	46	<.1	3.8	4.3	514	1.94	<.5	2.1	.9	3.9	67	<.1	<.1	.1	36	.54	.074	9	7	.59	190	.127	1	1.01	.069	.48	.1	<.01	2.2	.4	<.05	5	<.5
404723	.8	39.1	28.1	63	<.1	20.3	10.1	454	2.45	418.9	1.0	25.2	4.6	9	.5	5.4	2.4	31	.07	.042	20	19	.33	100	.023	2	1.27	.004	.07	.3	.02	1.9	.1	<.05	4	<.5
404724	.9	20.3	9.4	57	<.1	17.3	6.0	234	2.39	125.5	1.0	6.3	2.3	9	.2	1.9	.6	37	.06	.037	17	23	.37	94	.022	1	1.40	.004	.06	.2	.03	1.8	.2	<.05	5	<.5
404725	.9	20.5	10.7	53	<.1	20.4	11.0	365	2.47	141.6	1.1	12.7	3.0	9	.2	1.2	.9	36	.07	.041	18	23	.41	105	.027	1	1.47	.004	.06	.3	.04	2.2	.2	<.05	4	.6
404726	.3	44.0	10.9	57	<.1	29.2	13.5	478	3.18	358.6	1.3	44.0	14.8	24	.1	2.3	1.9	25	.14	.049	42	24	.52	188	.034	1	1.95	.007	.26	.2	.01	3.4	.5	<.05	6	<.5
404727	.7	18.0	11.4	58	<.1	23.4	8.0	356	2.80	130.0	.9	12.3	1.7	15	.1	1.2	1.1	39	.09	.038	20	28	.47	148	.026	2	1.99	.005	.10	.2	.03	2.0	.2	<.05	7	<.5
404728	.6	43.9	18.8	69	.2	37.1	15.2	802	3.08	393.5	1.8	42.1	13.0	15	.6	3.0	2.5	28	.16	.075	43	20	.41	235	.031	2	1.45	.004	.16	.4	.02	3.8	.3	<.05	5	<.5
404729	1.0	30.3	9.6	72	<.1	21.3	8.2	297	2.43	75.8	1.7	4.5	3.8	11	.3	1.0	.4	38	.11	.065	22	23	.44	102	.034	1	1.44	.005	.06	.4	.04	2.8	.2	<.05	4	.6
404730	.8	27.9	10.2	67	.1	22.5	10.1	353	2.48	159.9	1.2	15.8	5.0	12	.4	1.4	1.2	33	.10	.058	27	22	.45	100	.037	1	1.41	.005	.10	.3	.01	2.2	.2	<.05	4	.5
404731	.5	39.3	12.6	127	.1	37.1	16.6	477	2.79	333.9	1.8	3.2	8.9	14	2.2	2.3	2.1	21	.14	.057	52	26	.51	128	.022	<1	1.64	.004	.17	.1	.01	1.9	.3	<.05	5	<.5
404732	.6	34.7	12.1	61	<.1	24.4	10.3	308	2.56	204.9	1.4	10.5	8.0	18	.5	1.6	1.0	24	.06	.034	39	18	.42	165	.029	1	1.40	.005	.16	.2	.02	1.8	.3	<.05	4	<.5
404733	.8	35.1	10.8	58	<.1	19.0	9.3	279	2.65	616.1	1.5	13.8	2.6	18	.2	2.6	2.0	33	.08	.056	31	21	.38	103	.018	<1	1.28	.005	.05	.3	.02	1.5	.2	<.05	4	.6
404734	.7	43.0	9.4	61	<.1	25.9	12.0	302	2.73	452.5	1.8	13.7	5.0	25	.3	2.1	1.8	34	.10	.063	47	22	.41	116	.029	<1	1.37	.006	.07	.4	.01	2.2	.2	<.05	5	.5
404735	1.1	48.1	11.7	72	<.1	27.4	10.7	329	3.14	641.9	1.7	7.9	4.3	25	.2	2.5	2.4	45	.10	.064	35	27	.47	157	.031	2	1.89	.006	.09	.3	.02	2.5	.3	<.05	6	.5
404736	1.2	41.5	9.4	79	.1	29.3	10.2	322	2.73	262.3	1.5	22.3	7.3	23	.3	1.9	1.3	43	.21	.089	27	22	.45	122	.044	1	1.24	.007	.10	.5	.03	2.4	.2	<.05	4	.5
404737	.6	35.7	8.8	55	<.1	19.7	10.1	269	2.41	325.7	1.3	8.7	6.8	13	.2	1.8	2.5	27	.09	.042	27	18	.40	151	.032	1	1.16	.004	.11	.2	.02	1.9	.2	<.05	4	.6
404738	.8	24.6	10.1	49	<.1	16.9	7.4	253	2.30	291.2	1.0	10.7	1.6	9	.2	1.8	3.6	33	.06	.042	21	18	.30	83	.015	1	1.09	.004	.07	.3	.02	1.2	.2	<.05	4	.5
404739	.4	130.0	18.6	31	.4	15.5	11.8	244	4.16	6444.9	1.9	300.5	9.6	153	.2	15.1	65.9	17	.08	.036	36	15	.30	156	.022	1	1.17	.025	.12	4.1	.02	2.0	.2	.13	4	1.7
404740	.6	30.3	8.2	56	<.1	23.6	12.4	488	2.38	600.0	1.1	24.2	7.7	12	.2	2.9	2.9	23	.08	.043	28	14	.28	64	.020	1	.84	.003	.07	.2	.02	1.4	.1	<.05	3	<.5
404741	.6	29.0	8.3	54	<.1	23.7	12.3	475	2.30	619.1	1.1	15.3	7.7	12	.2	3.0	3.0	21	.08	.043	28	13	.27	64	.018	1	.78	.003	.07	.3	.02	1.4	.1	<.05	2	.5
404742	.5	41.4	9.9	78	.1	31.3	12.3	243	3.42	675.9	1.8	8.1	11.8	12	.4	3.3	1.7	18	.09	.047	44	22	.55	80	.009	1	1.56	.003	.12	.1	.01	1.6	.2	<.05	5	<.5
404743	.4	47.1	14.3	84	.1	47.5	27.1	680	3.46	741.5	1.6	21.3	10.5	11	.4	10.1	1.2	15	.04	.043	49	11	.14	122	.003	3	.97	.006	.19	.1	.01	1.8	.2	<.05	2	<.5
404744	.6	37.3	9.2	53	<.1	24.2	16.6	289	2.90	500.7	1.3	6.5	7.4	12	.2	4.7	1.4	24	.07	.044	36	17	.35	108	.018	2	1.18	.004	.13	.2	.02	1.6	.3	<.05	4	.7
404745	.9	30.6	10.2	53	<.1	22.9	11.0	283	2.77	674.2	1.1	36.2	1.8	12	.2	5.0	2.9	37	.08	.049	27	19	.32	122	.019	2	1.32	.004	.11	.3	.03	1.4	.2	<.05	4	.8
404746	.9	27.6	11.2	49	<.1	18.5	7.0	209	2.71	823.5	1.0	17.0	2.2	10	.3	4.6	4.3	34	.07	.048	24	19	.32	89	.017	2	1.24	.004	.09	.3	.03	1.5	.3	<.05	4	.8
404747	.2	99.2	11.8	62	.2	36.2	17.3	326	4.19	1550.7	2.5	25.2	18.1	35	.4	11.9	3.4	9	.07	.046	57	10	.25	99	.003	2	1.05	.005	.18	.1	.03	1.8	.4	<.05	3	.6
404748	.5	211.6	28.5	68	.7	47.9	29.6	695	5.35	4229.8	2.3	128.3	16.8	25	.5	48.6	16.9	8	.21	.055	61	6	.08	81	.001	4	.56	.004	.13	.1	.05	3.4	.3	<.05	2	2.0
404749	.9	29.5	13.7	62	.2	17.6	6.2	198	2.43	354.1	1.2	23.1	2.8	17	.5	4.9	2.4	37	.10	.046	22	22	.40	90	.028	2	1.50	.005	.08	.9	.03	1.8	.2	<.05	5	.7
404750	1.0	32.8	13.1	69	<.1	21.8	10.6	380	2.65	295.5	1.4	28.0	4.4	13	.2	5.1	1.4	41	.12	.059	21	24	.45	135	.029	2	1.70	.006	.07	.8	.03	2.5	.2	<.05	4	.7
404751	.8	20.9	11.9	59	<.1	18.2	7.9	242	2.34	184.1	1.0	21.4	3.6	11	.3	3.1	.8	36	.11	.058	19	21	.36	78	.032	2	1.20	.005	.06	.7	.02	1.8	.1	<.05	4	.5
RE 404752	.9	19.6	10.6	61	<.1	17.7	7.9	253	2.49	231.6	1.0	17.4	3.5	16	.2	2.9	.9	40	.10	.050	22	24	.38	105	.036	2	1.52	.005	.10	.3	.04	1.8	.2	<.05	5	.6
404752	1.0	19.7	10.9	61	<.1	18.1	7.8	249	2.50	228.6	1.1	46.1	3.5	15	.2	3.1	1.1	41	.11	.050	22	23	.39	102	.037	2	1.51	.005	.11	.3	.03	1.8	.2	<.05	5	.6
404753	1.1	39.6	13.9	82	.2	25.9	10.8	336	2.76	570.5	1.4	33.8	8.8	22	.5	26.5	3.5	35	.13	.053	27	22	.43	169	.038	1	1.43	.007	.17	.7	.02	2.2	.3	<.05	4	.6
404754	.8	17.1	11.2	70	<.1	18.8	11.6	465	2.50	189.8	.9	12.4	3.3	13	.4	6.6	.7	40	.13	.059	18	22	.39	111	.034	2	1.24	.006	.08	1.0	.02	2.0	.2	<.05	4	.5
404755	1.0	15.4	8.9	51	<.1	15.9	6.8	239	2.19	130.7	.8	7.2	1.9	13	.2	1.9	.9	40	.12	.042	18	19	.31	92	.034	1	1.18	.005	.08	.5	.03	1.4	.1	<.05	5	.5
STANDARD DS7	21.3	111.5	72.3	421	.9	56.8	9.9	646	2.45	47.7	5.1	70.1	4.7	72	6.4	5.9	4.5	88	.96	.079	14	171	1.07	373	.128	38	1.01	.076	.44	4.0	.21	2.5	4.3	.21	5	3.9

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.2	1.9	3.0	45	<.1	4.0	4.3	518	1.94	<.5	1.8	<.5	3.7	59	<.1	<.1	.1	35	.49	.073	8	7	.61	189	.118	1	.99	.076	.48	.1	<.01	1.9	.4	<.05	5	<.5
404756	1.0	20.9	10.4	69	<.1	20.4	10.1	363	2.50	158.8	1.0	18.7	3.8	18	.4	1.7	1.1	38	.16	.070	19	22	.38	119	.034	1	1.36	.008	.06	1.0	.02	1.9	.1	<.05	4	.6
404757	.9	23.7	9.8	52	<.1	17.0	6.7	219	2.53	151.5	.9	23.8	3.0	21	.2	1.6	2.3	38	.10	.046	16	22	.34	87	.030	2	1.29	.005	.05	2.1	.04	1.6	.1	<.05	5	.5
404758	1.0	9.1	10.4	32	<.1	8.7	3.9	147	2.01	97.7	.6	5.7	1.3	13	.2	.8	.8	41	.08	.027	14	17	.21	72	.023	1	1.01	.004	.03	.4	.03	1.1	.1	<.05	6	.5
404759	.7	13.3	9.0	44	<.1	14.3	5.7	176	2.18	35.9	.7	5.3	3.3	13	.1	.8	.2	26	.10	.046	12	17	.31	68	.021	1	1.06	.004	.03	.4	.03	1.5	.1	<.05	3	.5
404760 (pulp)	17.5	5430.4	15.3	88	1.3	335.9	17.7	745	7.10	9.0	.2	485.8	1.2	107	.5	7.0	.5	38	1.87	.081	4	396	.79	25	.002	12	.80	.047	.35	.9	.92	4.0	.2	3.60	3	13.5
404761	.7	20.2	9.2	62	<.1	22.2	7.1	205	2.29	519.3	1.3	10.8	4.1	15	.2	2.4	.4	28	.16	.062	20	20	.39	80	.024	1	1.03	.004	.07	.7	.02	1.5	.1	<.05	3	<.5
404762	.9	21.1	13.3	61	<.1	17.7	7.2	261	2.43	614.3	1.0	17.9	1.4	12	.3	5.4	1.8	30	.09	.050	19	19	.36	82	.016	1	1.14	.004	.05	.5	.02	1.1	.1	<.05	4	<.5
404763	.8	21.5	12.7	62	<.1	18.7	9.5	420	2.45	626.5	1.1	22.3	1.5	15	.2	3.1	2.0	31	.16	.053	18	20	.38	90	.018	1	1.30	.006	.06	.7	.02	1.2	.2	<.05	4	.5
404764	.9	19.6	8.5	43	<.1	14.6	4.7	156	2.02	233.2	.8	11.4	.6	10	.2	1.4	1.7	31	.07	.048	15	19	.29	65	.016	1	1.05	.005	.05	.8	.02	.8	.1	<.05	4	.5
404765	.7	27.3	9.9	56	<.1	16.3	8.6	384	2.35	844.9	1.5	15.3	1.6	14	.1	3.6	2.4	29	.12	.066	17	20	.37	98	.014	1	1.27	.005	.05	.8	.02	1.3	.2	<.05	4	.5
404766	.6	47.8	11.1	54	.1	23.1	9.7	347	2.46	804.1	1.6	29.7	6.6	18	.2	5.9	1.9	24	.21	.050	23	18	.40	85	.019	1	1.07	.006	.06	.5	.02	2.1	.1	<.05	3	.6
404767	.6	60.2	14.3	67	.5	24.0	8.1	291	3.02	1315.2	2.7	54.2	3.6	32	.4	7.1	5.3	25	.44	.089	33	20	.41	102	.009	1	1.48	.007	.07	.8	.03	2.1	.2	<.05	4	.7
404768	.5	63.2	26.6	66	.5	23.6	6.2	201	3.24	1377.7	1.4	55.8	5.4	18	.2	12.1	6.3	24	.15	.066	34	19	.37	76	.008	2	1.35	.004	.07	.2	.04	1.9	.2	<.05	4	.7
404769	.6	70.5	41.2	57	.3	25.6	11.3	427	3.82	1900.8	1.9	63.9	8.2	21	.3	30.9	6.0	15	.13	.071	45	12	.20	101	.002	3	1.03	.005	.08	.1	.02	2.3	.3	<.05	3	1.3
RE 404769	.7	68.3	39.8	52	.3	23.9	10.8	420	3.73	1845.5	1.9	42.6	8.0	22	.2	31.4	6.1	15	.13	.068	46	12	.20	105	.002	3	.97	.005	.08	.1	.03	2.3	.3	<.05	3	1.3
404770	.5	126.5	34.7	72	.8	43.5	18.2	639	4.80	3112.3	2.3	103.1	14.1	29	.6	38.4	11.4	9	.32	.061	57	8	.12	68	.001	3	.66	.005	.08	.1	.04	4.1	.2	<.05	1	1.4
404771	.7	25.5	14.9	65	.2	22.4	9.1	300	2.48	124.3	1.3	8.2	3.3	13	.3	4.0	1.0	36	.15	.062	19	27	.42	148	.028	1	1.27	.006	.07	.3	.03	2.4	.2	<.05	4	.5
404772	.6	41.1	36.6	92	.8	34.7	16.3	1056	3.76	619.8	2.2	48.8	8.5	24	1.2	30.6	3.5	25	.23	.063	31	19	.26	194	.008	2	1.08	.005	.13	.2	.03	4.6	.3	<.05	3	<.5
404773	.9	23.1	14.1	64	.2	20.9	9.0	300	2.77	166.7	1.0	11.4	3.0	14	.3	2.1	1.4	45	.12	.054	19	37	.54	164	.038	<1	1.75	.007	.10	.3	.03	2.7	.3	<.05	5	.6
404774	.6	35.6	17.9	69	.3	22.9	9.6	339	2.92	471.0	2.0	8.9	6.3	23	.2	5.3	3.1	47	.21	.064	27	47	.66	132	.043	1	1.63	.007	.12	.3	.02	3.9	.3	<.05	5	<.5
404775	.7	31.7	19.4	67	.2	22.7	12.0	357	3.09	160.5	.9	8.0	3.0	25	.5	3.6	2.5	52	.22	.103	18	20	.63	195	.046	<1	2.04	.007	.15	.3	.03	3.0	.5	<.05	7	.6
404776	.8	23.8	22.2	59	.2	22.1	10.3	302	2.77	248.3	.9	5.0	3.7	12	.3	6.4	1.6	37	.10	.053	24	24	.46	152	.027	1	1.54	.005	.11	.2	.02	2.0	.3	<.05	5	<.5
404777	.7	70.1	173.2	80	2.1	37.7	21.3	955	3.70	996.6	2.0	17.2	10.4	14	1.1	103.5	4.8	17	.11	.063	48	15	.24	172	.008	3	1.09	.004	.09	.1	.02	2.3	.4	<.05	3	.5
404778	.6	33.5	33.5	146	.3	23.2	15.8	706	3.49	510.4	1.3	3.2	10.1	26	1.7	13.9	2.5	80	.31	.072	34	108	1.20	304	.088	1	2.61	.009	.28	.2	.02	8.9	.8	<.05	8	<.5
404779	.4	29.5	19.0	71	.2	25.6	10.5	402	2.48	173.7	.9	10.0	12.8	20	1.0	4.7	.7	18	.31	.051	33	16	.42	131	.024	1	1.10	.005	.15	.1	.01	2.0	.3	<.05	3	<.5
404780 (pulp)	.6	25.2	6.1	38	<.1	32.3	8.2	369	2.01	7.9	.8	5.1	4.8	67	.4	.6	.1	44	3.31	.099	16	36	.81	169	.079	2	.86	.026	.08	.3	.02	2.9	.1	<.05	3	<.5
404781	.8	23.5	46.1	59	.2	19.5	9.3	311	2.61	61.7	1.0	4.1	2.4	14	.6	8.7	.3	31	.09	.061	25	19	.37	87	.016	1	1.23	.004	.06	.2	.02	1.3	.1	<.05	4	.6
404782	.5	35.6	25.8	100	.2	30.7	11.6	565	2.92	152.3	1.0	2.0	12.2	11	1.8	8.2	.7	25	.14	.041	46	20	.47	177	.027	1	1.42	.004	.13	.1	.02	3.2	.3	<.05	4	<.5
404783	.3	34.6	62.8	127	.3	34.9	16.7	1236	3.17	219.6	1.2	4.8	15.8	11	3.6	11.5	.8	9	.12	.042	49	8	.13	206	.005	2	.69	.003	.09	.1	.04	3.2	.2	<.05	1	<.5
404784	.3	33.5	43.1	90	.3	39.3	16.3	942	3.65	144.8	1.7	10.7	16.0	106	1.0	3.4	.4	19	3.00	.078	63	20	.69	224	.027	<1	1.61	.006	.16	.1	.03	3.6	.3	<.05	5	<.5
404785	.5	28.3	324.5	186	1.9	33.8	14.1	766	2.86	135.9	1.1	13.0	9.8	9	4.2	4.4	.3	23	.12	.036	41	19	.47	175	.029	1	1.32	.004	.10	.2	.03	2.4	.2	<.05	3	<.5
404786	.7	28.7	14.1	89	.2	25.0	9.9	458	2.74	84.8	1.2	13.9	5.0	20	.7	2.6	1.5	38	.27	.058	27	28	.47	170	.029	1	1.52	.014	.08	.5	.02	2.9	.2	<.05	5	<.5
404787	.7	23.0	15.0	63	.2	20.2	8.0	368	2.57	70.7	.9	3.7	2.4	13	.3	1.8	1.0	38	.18	.052	20	24	.41	113	.024	1	1.43	.006	.06	.3	.03	1.9	.2	<.05	4	.6
404788	.7	32.9	25.7	82	.5	24.0	10.7	709	2.98	318.3	1.1	22.4	2.6	24	1.3	3.8	7.4	42	.40	.070	30	29	.49	200	.025	2	1.69	.012	.09	.4	.03	2.4	.3	<.05	6	.7
STANDARD DS7	21.5	113.5	72.8	420	.9	57.7	9.9	632	2.44	48.3	5.0	84.1	4.5	70	6.5	6.0	4.4	88	.94	.079	13	169	1.06	370	.126	38	.97	.073	.44	4.0	.21	2.5	4.3	.23	5	3.7

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	.1	1.8	3.0	45	<.1	3.9	4.5	522	2.00	1.0	1.8	<.5	3.7	60	<.1	<.1	<.1	36	.48	.076	7	7	.61	193	.122	1	.99	.072	.49	.1	<.01	1.9	.3	<.05	5	<.5
404789	.5	40.7	24.0	84	.4	36.9	18.8	491	3.59	664.8	1.5	74.4	11.4	28	.4	5.1	11.0	26	.33	.065	55	21	.45	108	.029	1	1.24	.011	.19	.5	.03	2.7	.2	<.05	4	.5
404790	.6	39.6	38.8	84	.3	29.6	11.4	374	3.31	372.9	1.4	27.1	10.2	20	.5	10.9	6.0	28	.29	.047	45	23	.51	128	.028	1	1.42	.010	.15	.7	.02	2.8	.2	<.05	5	.5
404791	.4	60.9	21.8	85	.4	30.4	12.9	477	3.75	446.1	1.6	63.9	12.4	31	.4	5.0	9.7	32	.36	.050	44	30	.71	129	.033	<1	2.06	.017	.21	.8	.02	3.6	.3	<.05	6	.6
404792	.7	45.7	11.4	67	<.1	28.6	12.3	413	2.84	453.6	1.3	20.6	8.2	11	.2	5.0	2.4	34	.13	.059	28	27	.70	129	.028	<1	1.68	.004	.11	.6	.02	2.8	.3	<.05	5	.7
404793	.9	22.2	29.9	64	<.1	18.1	9.5	319	2.30	226.2	.9	12.0	1.8	10	.6	9.7	.4	29	.09	.058	16	17	.29	55	.018	<1	.94	.003	.04	.4	.02	1.1	.1	<.05	3	<.5
404794	.9	25.3	34.4	68	<.1	19.1	9.8	370	2.55	350.6	1.1	10.3	3.9	12	.5	18.9	.9	28	.10	.057	19	18	.31	72	.019	1	.91	.004	.07	.6	.02	1.3	.1	<.05	3	.5
404795	.8	16.1	18.0	57	<.1	17.1	10.8	372	2.33	316.4	.9	21.2	2.9	12	.3	4.9	1.6	29	.11	.060	17	17	.30	65	.022	1	.95	.004	.07	.5	.03	1.3	.1	<.05	3	<.5
404801	.9	30.0	10.7	61	.1	22.2	10.4	354	2.68	408.1	.9	6.4	1.6	12	.3	1.8	3.7	34	.07	.050	19	20	.38	100	.017	1	1.33	.005	.06	.4	.02	1.6	.2	<.05	4	.7
404802	.9	34.4	11.5	62	<.1	21.8	12.5	328	2.84	500.8	1.1	4.9	2.8	17	.3	2.3	3.4	30	.07	.047	27	20	.43	129	.018	<1	1.34	.005	.15	.2	.02	1.5	.3	<.05	4	.6
404803	.2	31.4	4.5	70	<.1	37.8	18.4	370	4.40	250.3	1.0	<.5	15.5	11	<.1	1.2	1.2	19	.11	.052	40	26	.94	153	.012	<1	2.02	.003	.13	<.1	<.01	2.6	.3	<.05	6	<.5
404804	.7	33.9	16.8	61	.1	21.7	7.3	251	2.67	351.7	1.0	30.7	2.4	11	.4	2.5	3.8	32	.07	.046	22	21	.39	126	.019	1	1.46	.005	.07	.3	.02	1.7	.3	<.05	4	.5
RE 404804	.7	34.4	17.5	60	.1	22.6	7.7	258	2.78	347.2	1.0	3.7	2.3	12	.4	2.5	3.7	32	.07	.046	21	21	.39	125	.019	<1	1.44	.005	.07	.5	.02	1.7	.3	<.05	4	<.5
404805	.8	38.8	14.5	75	.3	28.0	13.5	488	2.83	282.2	1.8	3.3	.8	22	.5	1.9	1.7	32	.14	.086	30	24	.42	150	.010	1	1.47	.006	.06	.2	.03	1.2	.2	<.05	4	.6
404806	.9	30.7	9.5	64	.2	23.3	7.9	268	2.41	151.3	1.4	5.1	6.9	19	.4	1.5	1.3	30	.15	.073	23	18	.39	89	.025	1	1.13	.006	.04	.4	.03	2.2	.1	<.05	3	.5
404807	.8	22.8	10.3	59	.1	20.5	11.7	410	2.38	34.8	1.2	3.4	3.1	11	.3	1.0	.4	34	.12	.065	18	21	.41	148	.023	1	1.29	.005	.03	.3	.05	2.8	.1	<.05	3	.8
404808	.8	38.7	44.3	96	.6	21.5	7.6	247	2.87	480.3	1.7	2.2	1.5	18	1.1	5.5	5.7	34	.07	.061	25	23	.42	101	.013	<1	1.51	.006	.06	.2	.04	1.4	.3	<.05	4	.7
404809	.8	43.4	21.2	70	.3	19.7	7.6	290	2.90	773.5	1.3	5.3	2.6	20	.6	3.3	6.3	29	.07	.056	24	20	.43	129	.016	<1	1.43	.006	.08	.3	.02	1.5	.3	<.05	4	.6
404810	.8	33.2	13.4	70	.3	22.0	9.0	324	2.43	474.3	1.1	14.7	2.9	12	.5	2.3	2.1	33	.08	.050	18	20	.37	108	.020	3	1.14	.005	.05	.4	.04	1.8	.2	<.05	3	.7
404811	.7	81.6	25.1	85	.3	30.3	17.2	470	3.35	967.4	1.6	17.1	7.0	19	1.3	6.3	6.9	20	.07	.045	45	15	.33	134	.013	<1	1.08	.004	.09	.2	.02	1.8	.3	<.05	3	.6
404812	.7	63.1	11.9	66	.2	36.7	19.0	439	3.24	537.3	1.6	17.9	8.5	18	.3	2.4	2.8	33	.09	.049	45	28	.56	175	.037	<1	1.74	.005	.20	.3	.02	2.9	.5	<.05	5	.5
404813	.7	26.7	17.9	64	<.1	20.6	9.4	373	2.56	316.4	1.0	4.2	1.9	10	.4	4.5	2.4	30	.06	.044	23	17	.29	94	.015	1	1.07	.004	.08	.3	.02	1.2	.2	<.05	3	<.5
404814	.8	26.5	11.6	59	<.1	22.4	9.2	309	2.41	177.8	.9	3.0	3.6	8	.4	2.4	1.2	27	.06	.039	21	17	.35	70	.014	<1	1.07	.004	.03	.3	.03	1.4	.1	<.05	3	<.5
404815	.8	17.4	11.9	56	<.1	18.9	7.8	275	2.40	63.1	.8	4.5	1.1	8	.2	1.1	.5	30	.07	.051	17	19	.36	73	.013	<1	1.12	.004	.04	.2	.03	1.0	.1	<.05	3	.5
404816	.9	32.9	14.3	72	.1	28.8	13.3	336	2.81	132.7	1.3	4.3	6.6	12	.4	2.0	.7	30	.11	.057	30	21	.44	84	.019	<1	1.32	.004	.05	.2	.03	1.8	.1	<.05	4	.5
404817	.7	27.6	11.2	67	<.1	28.1	16.2	333	2.91	99.1	1.1	10.8	5.8	12	.4	1.4	.6	29	.07	.049	27	22	.46	91	.017	<1	1.46	.005	.04	.3	.03	1.9	.1	<.05	4	<.5
404818	.8	27.9	9.7	66	<.1	26.0	12.8	334	2.69	80.1	1.2	6.3	7.4	14	.3	1.3	.4	28	.10	.051	27	21	.48	86	.023	<1	1.35	.005	.05	.2	.03	2.0	.1	<.05	3	.5
404819	.9	23.5	15.4	64	<.1	26.7	13.3	373	2.98	137.0	1.1	4.2	3.2	13	.2	1.7	.7	33	.08	.051	26	22	.44	123	.016	<1	1.46	.005	.07	.2	.02	1.7	.2	<.05	4	<.5
404820 (pulp)	19.4	5931.7	15.3	100	1.3	379.2	21.1	870	8.44	11.8	.2	553.0	1.3	115	.4	8.0	.3	33	2.09	.093	3	469	.90	51	.001	8	.84	.046	.35	.9	1.15	4.3	.1	4.29	3	16.3
404821	.4	28.5	17.4	61	<.1	38.1	17.8	695	3.18	135.7	1.6	2.5	15.3	19	.2	1.3	.6	22	.17	.048	55	22	.56	203	.026	<1	1.57	.008	.11	.1	.02	3.1	.2	<.05	5	<.5
404822	.6	28.2	29.1	115	.2	29.4	13.5	585	3.01	495.9	1.1	9.6	7.4	14	1.9	5.0	1.8	24	.11	.039	37	18	.39	181	.020	1	1.30	.006	.11	.1	.03	2.6	.3	<.05	4	<.5
STANDARD DS7	20.8	114.4	71.9	412	.9	56.5	9.7	618	2.39	47.4	4.9	69.5	4.4	68	6.3	5.8	4.4	86	.91	.077	12	164	1.04	363	.121	38	.94	.071	.43	3.8	.21	2.4	4.2	.21	5	3.2

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data L FA ___

ACME ANALYTICAL LABORATORIES LTD. (ISO 9002 Accredited Co.)
852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Copper Ridge Exploration Inc. PROJECT Scheelite Dome File # A605327

500 - 625 Howe St., Vancouver BC V6C 2T6 Submitted by: Greg Dawson

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm
G-1	21.8	30.3	3.2	48	.2	5.1	4.8	516	2.03	<.5	2.9	<.5	4.2	59	<.1	<.1	.1	38	.52	.076	7	11	.58	199	.129	<1	1.00	.067	.48	.2	<.01	1.9	.4	<.05	5	<.5
405012	7.2	20.6	2.4	4	.1	3.7	1.2	82	.57	181.7	.5	<.5	14.7	4	<.1	3.6	.4	1	.06	.011	21	13	.02	31	.001	2	.20	.004	.09	.4	<.01	.3	.1	<.05	<1	<.5
405013	2.1	48.3	10.6	35	.1	22.6	10.4	323	2.43	51.6	.7	4.4	7.5	110	<.1	.5	.3	36	1.31	.013	8	24	.76	185	.059	1	3.58	.193	.62	.4	<.01	5.1	.6	.36	11	.7
405014	1.2	41.2	5.8	29	.1	5.6	3.4	80	1.10	267.5	1.0	48.9	8.2	5	.5	25.6	.5	3	.03	.015	20	10	.03	38	.001	6	.32	.007	.14	.3	.01	.7	.1	<.05	1	<.5
405015	2.1	13.9	9.2	24	.7	3.2	.9	50	.90	377.4	.6	165.6	7.5	4	.7	22.2	.4	1	.02	.009	19	11	.01	27	.001	10	.18	.003	.13	.7	<.01	.8	.2	<.05	<1	<.5
405016	1.3	23.9	14.0	38	.4	5.7	3.4	122	1.47	658.0	1.1	100.7	8.4	3	.8	28.0	.1	1	.02	.009	20	9	.02	52	.001	8	.36	.004	.19	.2	<.01	.9	.2	<.05	1	<.5
405017	.4	21.4	1.1	2	.1	2.2	.4	38	.97	121.2	.1	8.6	.5	5	<.1	.8	.6	1	.01	.009	2	12	.04	5	.001	1	.09	.004	.02	.1	.01	.3	<.1	<.05	<1	<.5
405018	.4	3.5	.7	5	<.1	11.0	14.3	25	.88	7604.3	.2	36.5	.7	5	.1	21.9	1.4	<1	.01	.001	2	13	<.01	26	<.001	3	.04	.002	.02	.1	<.01	.1	<.1	.33	<1	4.6
405019	.3	4.1	.4	1	<.1	1.0	1.4	19	.39	901.3	.1	5.2	.1	1	<.1	1.4	.2	<1	<.01	.001	<1	15	<.01	8	<.001	1	.01	.002	<.01	.2	<.01	.1	<.1	<.05	<1	<.5
405020	.5	24.1	3.1	13	.3	4.7	4.0	43	1.15	2466.1	.6	21.0	3.9	11	.2	2.9	3.0	5	.11	.057	10	14	.09	54	.002	4	.37	.005	.13	.2	.01	.7	.2	<.05	1	.8
405021	.4	6.2	1.0	1	<.1	1.4	2.6	21	.44	1057.9	.1	<.5	.6	2	<.1	2.2	1.8	1	<.01	.001	2	18	<.01	9	.001	3	.03	.002	.02	.3	.01	.2	<.1	<.05	<1	<.5
405022	.3	19.1	2.0	4	<.1	8.5	4.1	25	.53	1261.0	.7	13.1	4.4	6	.1	4.8	2.5	1	.02	.008	13	15	.02	27	.001	11	.13	.005	.06	.1	<.01	.3	.1	<.05	<1	<.5
405023	.4	121.0	5.2	3	.3	14.9	43.6	19	2.21	>10000	.6	48.1	5.2	8	.3	18.4	4.0	1	.01	.007	12	10	.01	55	.001	15	.15	.005	.09	.1	<.01	.3	.2	.70	<1	4.0
405024	.6	25.7	1.2	2	<.1	6.3	60.4	29	.48	1210.4	.2	13.1	.3	2	<.1	2.0	1.2	1	<.01	.001	1	18	<.01	17	<.001	2	.04	.002	.01	.1	<.01	.1	<.1	.14	<1	.6
405025	.3	4.6	3.8	3	.3	5.2	6.9	26	1.01	7823.3	.4	55.5	1.1	7	.2	12.9	9.1	1	<.01	.002	3	17	.01	18	<.001	7	.06	.003	.03	.1	<.01	.1	<.1	.21	<1	2.3
RE 405025	.4	4.0	3.7	2	.3	5.5	7.0	26	1.02	7904.4	.4	58.1	1.1	7	.1	12.6	9.1	<1	.01	.002	4	19	.01	17	.001	8	.06	.003	.04	.1	.01	.2	<.1	.21	<1	2.0
405026	.3	47.4	6.5	21	.1	26.8	34.5	120	2.42	8121.7	1.5	16.2	10.4	95	<.1	7.9	2.6	17	.28	.021	17	27	.51	142	.013	3	1.54	.046	.25	.2	<.01	2.3	.3	.25	5	2.1
405027	.2	6.5	1.5	13	<.1	13.5	9.2	119	.93	346.8	.3	2.9	5.7	4	.1	.7	.2	10	.04	.018	4	17	.40	27	.003	1	.63	.008	.09	.1	<.01	1.6	.1	<.05	2	<.5
405028	.5	262.4	5.3	11	.5	14.9	19.9	80	7.82	>10000	2.6	32.1	10.3	46	<.1	63.4	7.9	14	.05	.012	9	19	.51	54	.010	1	1.07	.010	.14	.1	<.01	1.5	.2	2.63	4	26.9
405029	.4	44.9	7.9	34	.4	37.3	92.8	176	4.85	>10000	.8	149.6	.5	116	.1	39.4	10.0	16	.02	.009	10	12	1.07	215	.002	2	1.41	.008	.09	.1	.01	1.6	.6	.90	6	4.3
405030	.3	7.6	1.1	5	<.1	3.8	6.4	36	1.61	>10000	.2	32.3	2.0	57	.1	10.0	1.4	1	.02	.005	6	9	.07	124	.001	1	.23	.007	.08	.1	.01	.5	.1	.19	1	1.6
405031	.5	46.0	1.7	7	.2	2.6	2.2	32	1.89	>10000	.3	84.4	3.5	70	.1	17.1	4.9	4	.01	.005	16	14	.04	235	.001	3	.20	.009	.09	.1	<.01	.9	.2	.10	2	4.0
405032	.3	46.5	150.5	7	5.9	1.9	.7	30	5.23	>10000	.3	897.3	5.1	7	.7	125.2	383.7	2	.01	.018	7	9	.02	106	.003	4	.19	.003	.12	.2	.05	.8	.1	.12	1	25.3
405033	.3	173.6	222.6	17	16.6	7.9	10.7	31	12.94	>10000	.7	3049.0	6.3	24	.8	233.3	1444.6	3	<.01	.014	6	8	.02	46	.003	4	.29	.004	.12	2.5	.16	1.1	.2	3.32	1	>100
405034	.3	218.3	58.0	15	3.9	7.9	13.5	18	17.62	>10000	.6	4502.0	5.1	26	.8	233.0	1373.5	3	<.01	.012	3	7	.02	26	.003	5	.32	.003	.11	16.4	.06	1.2	.2	5.54	1	>100
405035	.3	30.8	51.0	5	3.0	19.1	30.9	23	16.52	>10000	.5	1490.0	5.2	8	.1	103.0	195.9	<1	<.01	.010	2	5	.02	38	.002	3	.20	.003	.14	1.2	.04	.5	.1	5.06	1	73.2
405036	1.4	143.8	5.2	11	.5	18.4	9.4	135	3.62	>10000	.8	301.6	6.9	20	.1	29.9	24.2	5	.02	.012	24	13	.19	68	.003	2	.55	.019	.14	.1	.01	.9	.2	.91	2	11.2
STANDARD DS7	20.6	111.5	70.5	414	.9	56.4	9.8	634	2.40	48.7	4.8	59.8	4.3	69	6.2	5.8	4.5	86	.94	.078	12	165	1.06	370	.124	38	.98	.071	.44	3.9	.20	2.5	4.1	.23	4	3.5

GROUP 1DX - 30.0 GM SAMPLE LEACHED WITH 180 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 600 ML, ANALYSED BY ICP-MS.
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

09-18-06 P12:59 OUT

Data___ FA ____ **DATE RECEIVED:** AUG 24 2006 **DATE REPORT MAILED:**.....

BRITISH COLUMBIA CERTIFIED ASSAYER Raymond Chan

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

VOLUME II

APPENDIX C - AURORA GEOSCIENCES FIELD REPORT ON THE 2006 SCHEELITE DOME GEOPHYSICAL PROGRAM

INDUCED POLARIZATION / RESISTIVITY, TOTAL MAGNETIC FIELD AND VERY LONG FREQUENCY ELECTROMAGNETIC SURVEYS AT THE SCHEELITE DOME PROPERTY, YUKON TERRITORY

for: **COPPER RIDGE EXPLORATIONS INC.**
Suite 500 - 625 Howe Street,
Vancouver, B.C.
Canada V1C 2P1

by: Dave Hildes, Ph. D., P. Geo.
and Geneviève Hétu, Tech.
Aurora Geosciences Ltd.
108 Gold Road
Whitehorse, Yukon, Y1A 2W3

Work Performed: July 6 – July 30, 2006
Location: 63° 47' N 136° 15' W
NTS: 115P/6, 115P/9 and 105M/13
Mining District: Mayo
Date: Jan 22 2007

SUMMARY

Induced polarization / resistivity, total magnetic field and very long frequency electromagnetic surveys were conducted on the Scheelite Dome Property for Copper Ridge Explorations Inc. The surveys were performed on a 22.8 km grid composed of 13 lines from 1000 m to 1900 m long.

In general the highest chargeabilities and lowest resistivities are on lines 1400E and 1600E where several distinct anomalies of 50 mV/V and 200 Ohm-m are imaged. On the western part of the grid there are several high-gradient chargeability couplets indicative of thin or small very chargeable bodies. The eastern part of the grid has broad, low amplitude (120 nT peak to trough), magnetic structures while the total magnetic field is generally featureless to the west. Several weak conductors were identified by the VLF survey.

Aurora Geosciences Ltd. was not retained to provide an interpretation of the data.

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APPENDIX I. IP / RESISTIVITY PLAN MAPS ..... Back Pocket

1.0 INTRODUCTION

Induced polarization / resistivity (IP), total magnetic field (mag) and very long frequency electromagnetic (VLF) surveys were conducted on the Scheelite Dome Property in the Toby zone for Copper Ridge Explorations Inc. 13 lines from 1000 m to 1900 m long were surveyed. The IP survey used dipole-dipole and modified pole-dipole arrays of 25 m and 50 m dipoles. Station spacing for both the mag and VLF surveys was 12.5 m. A total of 20.4 line kilometres of IP, mag and VLF were completed. 22.8 km of lines including a 2.4 km baseline was cut prior to the survey. Three different crews worked on this project; the IP crew worked 24 days, the mag / VLF crew 4 days and the line cutting crew 21 days (all include travel time).

2.0 LOCATION AND ACCESS

The Scheelite Dome property is located 25 kilometers northwest of Mayo in the central Yukon. The property falls within the Mayo Mining District on NTS map sheets 115P/16, 115P/9 and 105M/13, at latitude 63º47" north and longitude 136º15" west (Figure 1). It comprises 549 Quartz claims. The 2006 geophysical survey were done on the Toby Creek zone. Initially the line cutters accessed the grid by foot from a camp on the Highet Creek road, but during the project the camp was flown onto the grid to reduce travel time. Similarly, the IP crew was based from a camp on the grid and was equipped with an ATV to move the IP gear from line to line. The MAG / VLF crew's camp was set up by the road and the grid accessed daily by foot.

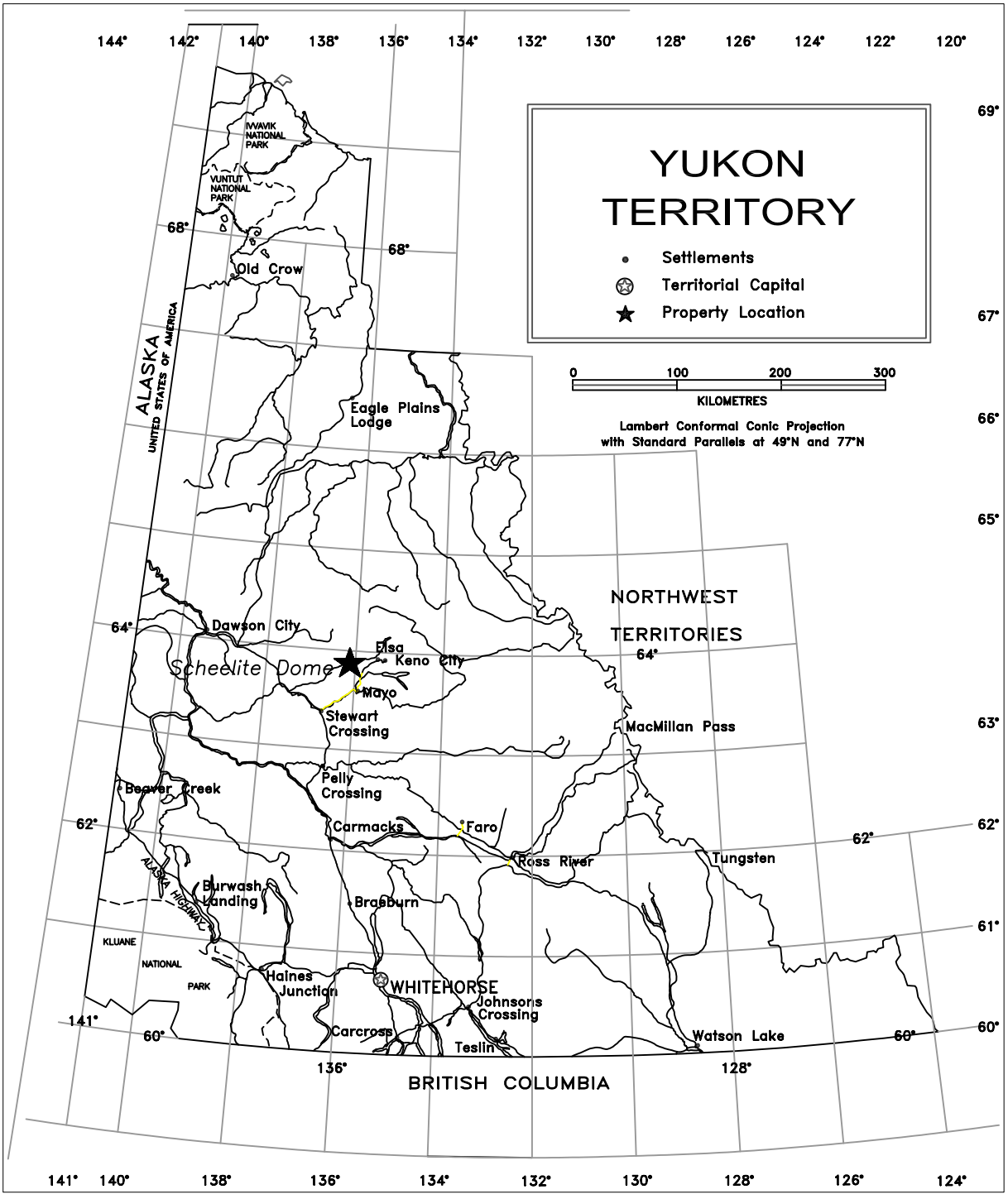
3.0 GRID

The survey grid is shown in Figure 2 (back pocket). The grid centre coordinates are 437000E, 7070000N (UTM Zone 8N, NAD27). The grid is composed of 13 wings lines from 1000 m to 1900 m long following a 2.4 km baseline. The baseline azimuth is 90º. The total length of the grid is 22.8 km including the baseline, but only the wings lines were surveyed. Grid cutting and installation was performed by Aurora Geosciences Ltd. prior to the geophysical surveys.

4.0 PERSONNEL AND EQUIPMENT

The surveys were conducted by the following personnel:

Jennifer Black	IP Crew chief /Geophysicist	From July 6 to July 30



Copper Ridge Explorations Inc.	SCHEELITE DOME PROPERTY	
PROPERTY LOCATION MAP	MINING DISTRICT: MAYO	
	SCALE 1: 6,000,000	NTS: N/A
	DATUM: N/A	DRAWN BY: DH
AURORA GEOSCIENCES LTD.	DATE: 15 Jan 2007	FIGURE: 1

Geatan Cyr	IP Technician	From July 6 to July 30
Warren Pearson	IP Helper	From July 6 to July 30
Chris Mills	IP Helper	From July 6 to July 30
Gabe Fortin	Mag / VLF Crew chief	From July 10 to July 14
Cody Woodman	Mag / VLF Helper	From July 10 to July 14
Larry Brault	Line cutting Foreman	From June 11 to July 1
Matt Olsen	Cutter	From June 11 to July 1
Warren Pearson	Brusher	From June 11 to July 1
Gordon Ruby	Brusher	From June 11 to July 1

The crew was equipped with the following instruments and general equipment:

IP Receiver	IRIS Elrec Pro
IP Transmitters	GDD Tx II - 3.6 kW Honda 5kVA gas generator
Magnetometers	Proton GSM-19T (s/n 1091111) Overhauser GSM-19 (s/n 708719)
VLF	Geonics EM-16
Other	2 Dell lap top computer (IP and mag/VLF crews) 3 1 ton trucks 1 ATV (from July 6 to July 30) 1 X 2 person summer camp + 2 X 4 person summer camp Standard line cutting equipment 1000 survey lath metal butter tags Repair tools (electrical / light mechanical) IP repair tools Globalstar satellite phones Geo-reel winders Geo-reel spools Speedy winders and spools IP wire
Software	Geosoft Oasis 6.0.1 with IP package

5.0 SURVEY AND LINE CUTTING SPECIFICATIONS

The surveys were conducted according to the following specifications:

IP SURVEY

Grid registration: All geographic coordinates are in NAD27 (Canada) coordinates projected to UTM Zone 8N. Line-ends and stations were surveyed every 500 m (nominal) with non- differential GPS to an estimated averaged accuracy of < 10 m.

IP Array: Modified pole-dipole (L0–L10) and dipole-dipole (L12–L24)

Dipole spacing: 25 m (L0–L20) and 50 m (L22 and L24).

Separations: Six dipoles read from n=1,2, …, 6.

Tx: Time domain with a 50% duty cycle, reversing polarity, 0.125 Hz

Signal sampling: 20 windows, semi-logarithmic sampling over 2 s. Sampling commences 40 ms after shutoff. Sample windows are shown in the table below:

	1	**2**	**3**	**4**	**5**	**6**	**7**	**8**	**9**	**10**
Width	40	40	40	40	40	40	40	80	80	80
Channel	**11**	**12**	**13**	**14**	**15**	**16**	**17**	**18**	**19**	**20**
Width	80	80	80	80	160	160	160	160	160	160

Parameters readings:
Mi - 20 semi-logarithmically spaced time slice channels
V_p - primary voltage
Sp - self-potential (voltage)
I - current
Rs - electrode resistance
Err - standard deviation of stacked readings

Stacks, repeats: At least 15 stacks were taken at each station. Stations that were noisy (error > 5 mV/V) had extra readings taken.

MAG SURVEY

Station spacing	12.5 m
Base station	Installed at a fixed location (438480E, 7071026N) and cycled at a five second interval throughout the survey period.
Registration	Data was registered to UTM Zone 8N, NAD27 coordinates using a non-differential GPS points averaged to an estimated accuracy of < 10 m, at line-ends and every 500 m (nominal).
Levelling	30 points in orthogonal directions surveyed daily by each operator

VLF SURVEY

Station spacing	12.5 m
Facing direction	North
VLF Transmitter	24.0 kHz, NAA Cutler, Maine, USA

LINE CUTTING

Base line azimuth	90.0º (declination 25.0º E)
Station spacing	25 m
Wing line station	Marked with flagged half length tagged pickets, with station coordinates on both the tag and picket.
Chainage	All survey stations tight chained / *NOT* slope corrected on wing lines. Base line stations slope corrected.
Line quality	1.5 m wide, cleared to ground level of all brush.

6.0 SURVEY NOTES

The survey logs in Appendix B describe detailed survey and line cutting operations including production. The line cutting crew mobilized to the property on June 11 by truck from Whitehorse and set up a camp along the road (438427E, 7071011N). On June 17,

the camp was moved by helicopter to the middle of the grid (437311E, 7069792N) to reduce daily travel time. The line cutting crew demobilized on July 1. The IP crew mobilized to the property on July 6 by truck. The same day, the gear and the crew were flown to the grid and a camp set up on the east side of the grid (437750E, 7069250N). IP production proceeded from July 7 to July 29. The IP crew demobilized back to Whitehorse on July 30. The mag / VLF crew mobilized by truck on July 10 and set up a camp along the road (438427E, 7071011N). The mag / VLF crew surveyed from July 11 to July 14 and demobilized on July 14 leaving a small amount of VLF to be finished by the IP crew.

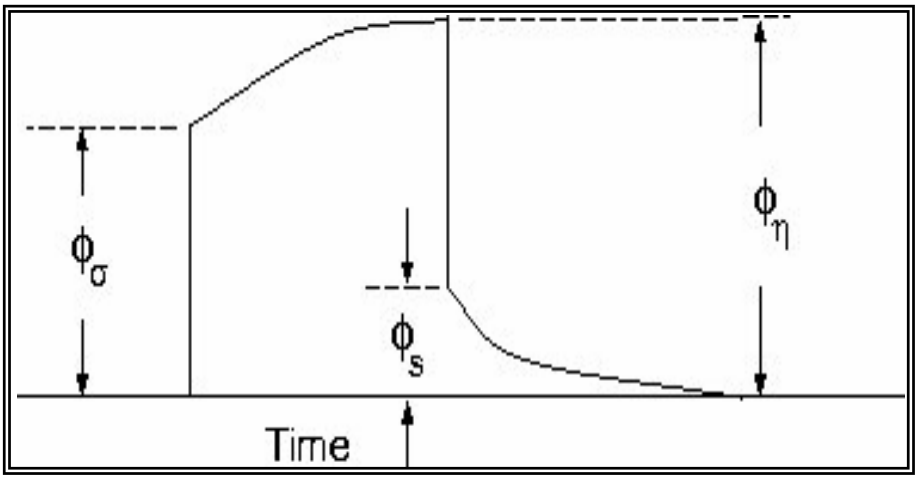
At Copper Ridge's request, the dipole spacing was changed from 50 m to 25 m after lines 2400E and 2200E were surveyed. Due to poor signal to noise ratio, the array geometry was switched from dipole-dipole to modified pole-dipole after lines 2400E – 1200E were completed. In the modified pole-dipole array geometry, one of the two current electrode remains at the start of the line while the other follows the receiver at 1 X the array distance.

7.0 IP INVERSION METHOD

The data were inverted using the DCIP2D package developed by the University of British Columbia Geophysical Inversion Facility. The inversion algorithm is described in detail by Oldenburg and Li (1994). A brief description of key features of the algorithm follows.

The IP effect can be described in macroscopic terms. If a time domain signal is put into the ground, as soon as the current is turned on, the voltage immediately rises to a level (ϕ_σ) and thereafter continues to rise to a higher level (ϕ_η). At current shutoff, the voltage immediately falls to a level (ϕ_s) and then slowly decays to zero along a curve similar to that between ϕ_σ and ϕ_η . Apparent chargeability is defined as the "extra"voltage observed:

$$\eta_a = \frac{\phi_\eta - \phi_\sigma}{\phi_\eta} = \frac{\phi_s}{\phi_\eta}$$



The observed DC potentials ϕ_σ are defined by the vector form of Ohms Law:

$$\nabla \cdot (\sigma \nabla \phi_s) = -I\delta(r - r_s)$$

where **r-r$_s$** is the vector to the measurement point, **I** is the current and **σ** is the conductivity structure of the earth - the unknown quantity in the geophysical problem. The chargeability can be modeled by replacing the conductivity by an equivalent apparent conductivity controlled by the chargeability:

$$\sigma_\eta = \sigma(1 - \eta)$$

Modeling the IP effect then involves running two conductivity models - one with **σ** and one with σ_η .

The unknown quantity is the distribution of conductivities in the earth. The software models the earth conductivity structure as a series of rectangular cells of varying size and aspect ratio. The grid is finest (most detailed) near the measurement points and much coarser at locations beside or at depth beneath the measurement points. The padding cells are necessary to avoid having edge effects appear in the model. The size and dimensions of the models in no way compensates for the basic limitations on depth of penetration and resolution inherent in the IP/resistivity survey. Thus the effective depth of penetration (0.5 to 1.0 times the maximum dipole separation) is the limit to which the models should be relied upon to accurately reflect true earth conductivities and chargeabilities.

The program calculates the potential across the finite element network using a starting model. Appropriate boundary conditions are applied when calculating the potentials across the network. These include the condition that all current flow is normal to the cell

boundaries and voltages are continuous across the boundaries. The sensitivity of the model to changing the parameters in any cell is calculated as is the misfit between the model results and the actual observed potentials / chargeabilities. The model is then adjusted using the calculated sensitivities of the response to changes in the conductivity of individual cells.

There is no unique solution or model which fits any set of IP / resistivity data. A best-fit model is one which (1) fits the data within the error of the survey and (2) invokes the minimum required degree of complexity to fit the data. For a set of **N** measurements, a global misfit can be defined as:

$$\Psi_d = \sum_{i=1}^{N} \left(W_i(r_i - r_i^{obs})\right)^2$$

where W_i is the weighting factor for the i^{th} measurement (r^{obs}) and r_i is the model response for this measurement. The weighting factor is usually the inverse of the error so that a measurement with high error has a low weighting and vice versa. In a system with random noise, the target misfit is **N**. The algorithm reduces Ψ_d by repeatedly adjusting the conductivities to improve the fit until the global misfit equals the target misfit. At this point, the model fits the data to within the error of the survey.

The second requirement of a successful solution is that the complexity of the final model be minimized. IP measurements are inherent averages, deriving resistivity and chargeabilities from large volumes of the subsurface. It is possible to over-fit data, deriving solutions which over-minimize misfit but which invoke models with detail beyond the resolving power of the measuring arrays. The problem is ill-posed and inherently ambiguous in that an infinite number of models may satisfy the global misfit equals target misfit criterion. If both a simple and complex solution can adequately replicate the field data within the bounds of measurement error, the simple solution is to be preferred.

Starting with a reference model m_0 and weighting functions for x and z (w_x, w_z), define the complexity of the model as Ψ_m where:

$$\psi_m(m, m_0) = \alpha_s \int\int w_s(x,z)(m - m_0)^2 \, dx\, dz + \int\int \left\{ \alpha_x w_x(x,z) \left(\frac{\partial(m - m_0)}{\partial x} \right)^2 + \alpha_z w_z(x,z) \left(\frac{\partial(m - m_0)}{\partial z} \right)^2 \right\} dx\, dz$$

where α_x , α_z and α_s define the relative weight of the model in x, z and fineness. Increasing any of these values increases the importance of that dimension in the final

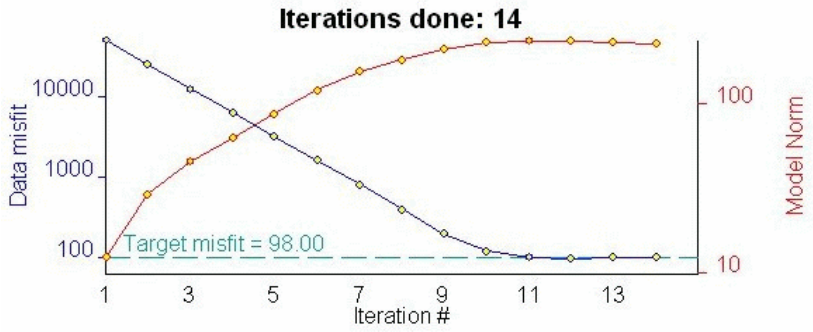
solution. For example, to weight the final solutions towards vertical structures, α_z would be weighted several times more than α_x. To force the model to generate fewer small scale structures, α_s is increased.

The final criteria for a successful solution can then be expressed as:

1. Minimize Ψ_m

2. Subject to the constraint that Ψ_d = N (or very close to it).

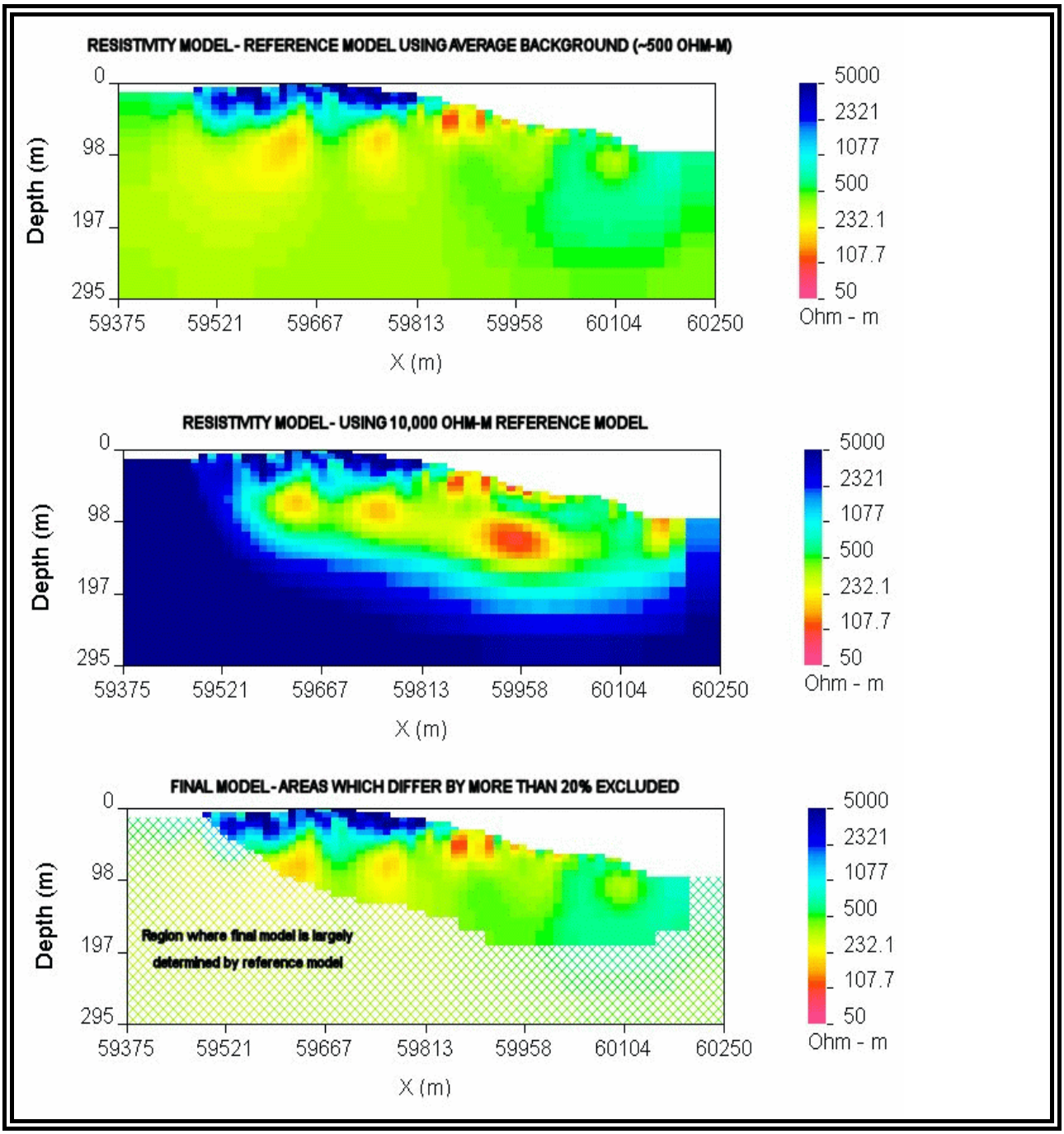
To evaluate a solution, the reader should examine not only the final values but the path the program followed to reach these values. An example of typical convergence curves is shown below:



The black line traces the value of Ψ_d with each iteration and in a good inversion, this will converge to the target misfit (N). The orange curve traces the convergence behavior of Ψ_m . This curve normally starts at a very small value because the reference model is usually set to the initial model and the initial and reference models are very simple. As the inversion proceeds, the solution model becomes increasingly complex as it is adjusted to meet the target misfit. After reaching target misfit, minor adjustments are made to reduce the complexity of the model and the Ψ_m curve stabilizes at some high value.

The field observations often have significant poorly quantified errors and the complexity of the background conductivity response may be such that it is impossible to reduce Ψ_d to N. Instead, Ψ_d can be scaled proportionately by a “chi-factor” ranging up or down from 1.0 (no scaling). Setting a large chi-factor loosens the control that goodness-of-fit exerts on the solution and generally directs the program to use very simple models which tend to smooth out the conductivities and fails to accurately model the fine details in resistivity or chargeability known to exist in the ground. Setting a chi-factor which is too low may prevent convergence to an acceptable solution. Generally, chi is left at 1.0.

A final feature of note in the inversion is the use of initial and reference conductivity and chargeability models in the inversion process. As noted above, the relation for Ψ_m requires a reference model (m_0) against which solutions are compared. This can be an actual 2D model constructed from known geology or a estimate of half space conductivity or chargeability. In addition, the modeling process will start from an initial model which has the same general form. In general, an average half space conductivity and chargeability based on the field values is the best model to start from and this is the default model for both inversions if none other is specified. This will ensure that Ψ_m converges to a value which is not too large. The initial and reference models can be used to estimate the depth of investigation. If two inversions are performed with very different reference models, there will be regions in the final models which will be the same in both inversion and peripheral regions where the final models will resemble the reference models. An example is shown below:


RESISTIVITY MODEL - REFERENCE MODEL USING AVERAGE BACKGROUND (~500 OHM-M)
Depth (m)
0
98
197
295
59375
59521
59667
59813
59958
60104
60250
X (m)
5000
2321
1077
500
232.1
107.7
50
Ohm - m
RESISTIVITY MODEL - USING 10,000 OHM-M REFERENCE MODEL
Depth (m)
0
98
197
295
59375
59521
59667
59813
59958
60104
60250
X (m)
5000
2321
1077
500
232.1
107.7
50
Ohm - m
FINAL MODEL - AREAS WHICH DIFFER BY MORE THAN 20% EXCLUDED
Depth (m)
0
98
197
295
Region where final model is largely determined by reference model
59375
59521
59667
59813
59958
60104
60250
X (m)
5000
2321
1077
500
232.1
107.7
50
Ohm - m

8.0 DATA PROCESSING

Data processing included the following steps and procedures for the total magnetic field survey:

1. Registration. Stations were interpolated from the non-differential GPS points taken at line-ends and every 500 m (nominal) to an estimated averaged accuracy of < 10 m. All coordinates are in NAD27 Zone 8N.

2. Geomagnetic variation removal. Base and rover magnetometers were synchronized to GPS time prior to each survey day. Temporal geomagnetic variation was removed by linear interpolation using the base station data. Data collected during periods in which geomagnetic variation exceeds 5 nT / 5 s were not included in the final data set; no data were rejected as being above this noise threshold.

3. Levelling. Data were levelled using 30 common points in orthogonal directions that were surveyed daily by each operator. The levelling correction for July 12 was -1.56 nT, for July 13 was -1.77 nT and for July 14 was -0.02 nT.

4. Filtering and plotting. The data were despiked using a filter width of 1 and a threshold of 50 nT. The data were gridded with a minimum curvature algorithm using a cell size of 25 m and 3 passes with a 3X3 Hanning filter were applied. The vertical magnetic gradient was calculated and also gridded with a minimum curvature algorithm using a cell size of 25 m and 3 passes with a 3X3 Hanning filter were applied. Plots are in Appendix F, found in the back pocket of this report.

5. Digital archive. The final data, digital copies of stacked total magnetic field, gridded and contoured total magnetic field and calculated vertical derivative data were written to CD-ROM (attached to this report).

The following procedures were used to prepare and invert the induced polarization and resistivity data:

1. Data review. All data were dumped daily and imported into Geosoft Oasis Montaj IP package. All readings were examined; outliers and data with relatively large errors were thrown out, the rest were averaged to produce a single reading for each station and n-separation. Where there were repeat readings, a weighted average was used to bias readings with higher stacks and lower standard deviations. The averages were calculated as follows:

$$AverageV = \left(\sum_i S_i V_i / Err_i\right) / \left(\sum_i S_i / Err_i\right)$$

$$AverageErr = \left(\sum_i S_i\right) / \left(\sum_i S_i / Err_i\right)$$

where *S* represents the number of stacks, *V* is the value to be averaged and *Err* is the standard deviation of the reading. The standard deviation of voltage measurements were taken to be equal to 1 as this value is not reported by the instrument. If the data were too noisy and were not repeatable, no final data were included in the final data set.

2. *Registration*. Station coordinates were interpolated from the non-differential GPS points taken at line-ends and every 500 m (nominal) to an estimated averaged accuracy of < 10 m. All UTM coordinates are in NAD27 Zone 8N. The topography was interpolated from a digital elevation map equivalent to NTS 1:50,000 maps.

3. *Apparent resistivity calculation.* The apparent resistivity was corrected because of the effect of the proximal stationary electrode caused by the modified pole-dipole geometry array.

4. Data formatting. The apparent chargeability, resistivity (in normalized voltage over current) and topographic data were formatted for entry into the UBC inversion program.

5. Resistivity modelling. For each line, errors in the apparent conductance were assigned to the data. There is no means of directly quantifying these errors because neither the transmitter nor receiver records the error in the current or voltage. Errors were assumed to be 0.0001 + 3% S/m. Following error assignment, the data were inverted and where high topographic relief dictated, a deep mesh was constructed. Default initial and reference models were used, based on an average of the apparent resistivity. After the default run, the data were inverted a second time using initial and reference models as detailed below under DOI model (depth of investigation). These half-space models are a much higher value (or lower) than the average in the survey area. The purpose of this second run is to generate a model with a background resistivity greatly different than the average values used in the default run. After the second run, the two models were compared and regions in the default model which showed more than the DOI cut off were replaced by a hatching pattern on the default run. In these hatched regions, the final model is not sensitive to the field data and there is no reliable subsurface information. The Chi factor was adjusted to ensure convergence and an appropriate level of structure to the model.

Resistivity inversion parameters

Line	Chi Factor	DOI model (Ohm-m)	DOI cutoff	Comment
0	2	100000	0.1	
200	1.5	100000	0.1	

400	0.5	100000	0.1	
600	1	100000	0.1	
800	1	100000	0.1	
1000	1	10	0.1	Used a low resistivity model (Rho=10).
1200	1	100000	0.3	Boulders at station 250 caused data gap.
1400	1	100000	0.3	Boulders between 275 and 400 caused data gap.
1600	1	100000	0.2	
1800	1.5	100000	0.3	
2000	1	100000	0.1	
2200	0.3	100000	0.1	50 m dipoles.
2400	0.8	100000	0.1	50 m dipoles.

5. Chargeability modelling. For each datum, the observed standard deviation of chargeability was used as a measure of error for apparent chargeability. To avoid zero errors, a minimum of 0.3 mV/V was added to each error measurement. The IP data were first inverted using default values (initial and reference model of a 0 mV/V half-space), with the same mesh as the resistivity modelling, using the default recovered resistivity model. After the first run, the data were inverted a second time using initial and reference models which incorporated background chargeabilities as detailed below under DOI model (a much higher value than the average in the survey area). The two models were then compared and regions in the default model which showed more than the DOI cut off were replaced by a hatched pattern in the final models. In these hatched regions, the final model is not sensitive to the field data and there is no reliable subsurface information. The Chi factor was adjusted to ensure convergence and an appropriate level of structure to the model.

Chargeability inversion parameters

Line	Chi Factor	DOI model (mV/V)	DOI cutoff	Comment
0	70.00	100	0.2	Poor fit of high gradient IP data.
200	17.00	100	0.2	Poor fit of negative app. chargeabilities.
400	60.00	100	0.2	Moderate fit of high gradient IP data.
600	0.30	100	0.1	
800	25.00	100	0.1	Moderate fit of high

				gradient IP data.
1000	40.00	100	0.1	Poor fit of high gradient IP data, particularly at station 200.
1200	19.00	100	0.1	Poor fit of high gradient IP data, particularly north of baseline.
1400	17.00	100	0.2	Poor fit of high gradient IP data.
1600	19.20	100		Poor fit of high gradient data south of baseline.
1800	5.50	100	0.4	Poor fit of single point extremes.
2000	0.10	100	0.4	
2200	1.21	100	0.3	Poor fit of single point extremes.
2400	0.80	100	0.2	Poor fit of single point extremes

6. Image extraction. After the modelling was complete, final images were generated with the inversion software and converted to JPEGs which appear in Appendix D.

7. Composite sections. Pseudosections of the apparent resistivity, apparent chargeability, error in chargeability and true sections of recovered models of resistivity and chargeability were prepared from the final edited data using the Geosoft Oasis Montaj IP package with logarithmic colour scales for the resisitivity sections and linear colour scales for the chargeability and error. To highlight details, colours are scaled to each line individually. Composite sections are in Appendix E, found in the back pocket of this report.

8. Stacked sections. Stacked pseudosections of the apparent resistivity and apparent chargeability and stacked models of resistivity and chargeability were produced for the entire grid. Logarithmic colour scales were used for the resisitivity sections and linear colour scales were used for the chargeability. A common colour scheme was used for all lines. Stacked composite sections are found in Appendix H.

9. *Plan view maps.* Maps of the apparent resistivity and apparent chargeability for each constant dipole separation (n = 1, 2, …, 6) for the total survey area were produced at a 1:5000 scale. Logarithmic colour scales were used for the resisitivity sections and linear colour scales were used for the chargeability. A

common colour scheme was used for all plan maps which are Appendix I, found in the back pocket of this report.

10. *Digital archive*. The final IP data, digital copies of the composite sections, stacked sections, inversion images and plan view maps were written to CD-ROM (attached to this report).

Data processing included the following steps and procedures for the VLF survey:

1. Registration. Data were entered into a spreadsheet and imported into Geosoft Oasis Montaj. GPS points were dumped from the handheld units and the coordinates for the VLF stations determined by linear interpolation between GPS points. All coordinate are in NAD27 Zone 8N.

2. *Filtering and gridding.* Despiking fliters were applied to both the inphase and quadrature with a filter length of 1 fiducial and a threshold of 10%. A 4-fiducial low-pass filter was then applied to both the despiked inphase and quadrature data and these results are shown in the stacked profiles map at a scale of 1cm = 10%. A 5-point Fraser filter (0.5, 1, 0, -1, -0.5), with a positive result corresponding to positive to negative dip moving south to north, was then applied and gridded using a minimum curvature gridding algorithm with a cell size = 25 m. 3 passes with a 3X3 Hanning filter were made on the gridded data.

3. *Plotting*. 1:5000 scale maps were made of the inphase and quadrature profiles and colour contoured Fraser filtered inphase maps and are found in Appendix G.

4. *Digital archive*. The final VLF data, digital copies of the stacked inphase and quadrature profiles and contoured Fraser filtered inphase maps were written to CD-Rom (attached to this report).

9.0 DATA PRODUCTS

The following data files are appended to the digital version of this report

Raw	Raw IRIS Elrec Pro daily dump files, exported to ASCII
	Raw Magnetometer daily dump files
	Raw VLF daily data
	Raw GPS daily dump files

Scheelite 2006 IP.gdb, Scheelite 2006 IP.xyz, Scheelite 2006 Mag.gdb, Scheelite 2006 Mag.xyz, Scheelite 2006 VLF.gdb, Scheelite 2006 VLF.xyz, Scheelite 2006 Grid.gdb, Scheelite 2006 Grid.xyz	In the Final folder, final IP, Mag, VLF and GPS data in Geosoft database and ASCII xyz format
Figure 2 – Line location map.jpg & pdf	1:5000 scale plan map of the survey area.
Inversion images	Jpgs of recovered models with convergence curves and observed and predicted data for each line.
Appendix E – Composite sections in jpg & pdf	Composite sections (scale = 1:5000) comprising pseudo sections of apparent resistivity, apparent chargeability, error in apparent chargeability and true sections of the recovered models
Appendix F – Vertical Magnetic Gradient.jpg & pdf, Total Magnetic Field.jpg & PDF	Colour contoured total magnetic field and calculated vertical gradient (scale = 1:5000).
Appendix G – Fraser filtered VLF.jpg & pdf, VLF stacked profiles.jpg & pdf	Contoured Fraser filtered inphase and stacked inphase and quadrature profiles (1:5000)
Appendix H – Stacked sections in jpg & pdf	Stacked pseudosections of apparent chargeability and apparent resistivity and stacked recovered models of resistivity and chargeability (scale 1:5000)
Appendix I – Plan view maps in jpg & pdf	Maps of the apparent resistivity and apparent chargeability for each dipole separation (n = 1, 2, …, 6) (1:5000)
Scheelite Dome 2006 geophysical Surveys.pdf	PDF of this report

10.0 RESULTS

Composite sections comprising pseudosections of apparent resistivity, apparent chargeability and error in apparent chargeability and recovered models of resistivity and chargeability are found in Appendix E. Appendix H has stacked pseudosections of apparent chargeability and apparent resistivity and stacked recovered models of

resistivity and chargeability. Maps of gridded total magnetic field and vertical magnetic gradient are in Appendix F. The total magnetic field relief over the project area is modest (140 nT maximum). Appendix G contains maps of the VLF stacked profiles and fraser filtered inphase VLF-EM data. All of the observed conductors from the VLF survey are weak conductors. Appendix I has plan view maps of apparent resistivity and apparent chargeability for each n-spacing. All the appendices are found in the back pocket of this report.

A brief description of the results follows.

Lines 0 – 600E

Lines 0 through 400 have a similar IP response: several single-slash, high-gradient apparent chargeability features within an increasing background towards L600E, culminating in a broad elevated chargeability of 20-30 mV/V with a 40 mV/V high between stations 500 and 600 on L600E. The recovered models of chargeability on lines 0-400E must be viewed with some caution as the inversion algorithm does not handle the single-slash, high-gradient apparent chargeability data well. This style of signature is typical of very thin or small (< 12.5 m with the 25 m dipoles) sheet or pod-like structures of very chargeable material, suggesting thin veins of chargeable material on lines 0-400E. There is poor correlation between the chargeability and resistivtiy on these lines. The resistivity shows a relatively conductive zone at station 300 on all four lines, broadening out at line 600E. Another region of low resistivity is seen around station 600 N from lines 0-600E, and appears to be comprised of several distinct conductors on lines 0-400E. Near surface conductive features at stations 950N on lines 400E and 200E and at station 775N on line 0E are imaged by both the VLF and DC-resistivity survey. Moderately anomalous apparent chargeabilities appear to be associated with these features. The total magnetic field response over these lines is relatively featureless.

Lines 800E – 1200E

The broad elevated chargeability at the north end of L600E continues onto L800E with more subdued values. There is again single-slash, high-gradient apparent chargeability features indicative of thin or small, very chargeable bodies on the north end of lines 800E , 1000E and 1200E. Lines 1000E and 1200E also have similar features at station 1000S. Lines 800E through 1200E have several moderate conductive zones (400 to 600 Ohm-m) which may be continuations of the conductive zones imaged on L600E. A conductor imaged at station 350N from the VLF-EM survey corresponds with a conductive, near surface anomaly seen in the recovered resistivity models. A 30 nT magnetic high, with the largest extent on L1200E extends from station 200S to 900S and is bisected by a magnetic trough at station 600S.

Lines 1400E – 2000E

Generally these lines have the lowest apparent resistivities and highest apparent

chargeabilities of the grid. They are characterized by several (ranging from 2 to 5) zones of high chargeability (up to 55 mV/V) and zones of low resistivity (down to 200 Ohm-m), generally with poor spatial correlation between the two. Most of the chargeability zones on lines 1400E through 1800E are of greater width than single-slash anomalies indicating a broader, more consistent source. On L2000E the chargeability anomaly is more modest and concentrated at the centre of the line at station 400S. VLF conductors at station 775S on lines 1200E and 1400E and at stations 675S and 575S on lines 1800E and 2000E (the conductor is absent from L1600E) have poor correlation with the DC resistivity data.

The total magnetic field high seen on lines 800E to 1200E continues at station 350S on line 1400E. In addition there is a NE-SW trending magnetic ridge from station 1150S on line 1400E to station 750S on line 2000E with a trough in the total magnetic field immediately to the NW of the ridge. Both the ridge and the trough become stronger in amplitude, 100 nT peak to trough, towards the NE.

Lines 2200E – 2400E

These lines were IP surveyed with 50 m dipoles and have therefore lower lateral resolution than lines 0E through 2000E. Several moderate high chargeability zones are imaged mostly from stations 600S to baseline 0. The resistivity is generally highest on the northern ends of the lines. The VLF conductor at station 550S on line 2200E, which is a continuation of the VLF conductor on line 1800E and 2000E is consistent with a conductor identified by the DC resisitivity survey. The NE-SW trending magnetic ridge and trough couplet continues from L2000E with the total magnetic field ridge though L2200E at station 400S and L2400E at station 300S. There is another zone of high magnetic field north of the baseline on lines 2200E and 2400E. The magnetic relief is highest in this part of the grid, becoming 140 nT peak to trough amplitude.

Aurora Geosciences Ltd. was not retained to provide an interpretation of the data.

Respectfully submitted,
AURORA GEOSCIENCES LTD.

Dave Hildes P. Geo, Ph. D.
Geophysicist

Geneviève Hétu
Technician

REFERENCES

Oldenburg, D.W. and Y. Li (1994) Inversion of induced polarization data. Geophysics Vol. 59. No. 9. pp. 1327-1341.

Sumner, J.S. (1976) Principles of Induced Polarization for Geophysical Exploration. New York: Elsevier.

Telford, W.M., L.P. Geldart and R.E. Sheriff (1990) Applied Geophysics (2nd Edition) New York: Cambridge University Pres

APPENDIX A - CERTIFICATE

I, David Henry Degast Hildes, Ph. D., with residence address in Whitehorse, Yukon Territory do hereby certify that:

1. I am a member of the Association of Professional Engineers and Geoscientists of British Columbia, license #29887

2. I am a graduate of the Queens University of Ontario with a B.Sc. (Honours) degree in Chemical Physics obtained in 1991 and a graduate of the University of British Columbia with a Ph. D. in Geophysics obtained in 2001.

3. I have been actively involved in mineral exploration since 1999 and am now employed as a geophysicist with Aurora Geosciences Ltd.

4. I am the project manager for the work described in this report.

Dated this ____ of _____, 2007 in Whitehorse, Yukon.

Respectfully Submitted,

Dave H. D. Hildes Ph. D.

APPENDIX B – SURVEY LOG

IP survey log sheet

Grid Name:	Scheelite Dome					**Datum used :**	NAD27- Canada
Crew:	Jennifer Black, Crew chief / Geophysicist Chris Mills, Helper Warren Pearson, Helper Geatan Cyr, Helper					**UTM Zone used :** **Total line-km IP :**	8N **20.40**
Date	Line	From	To	Daily line-km	**Total line-km for the grid**	**Comments**	
06-Jul-2006	n/a	n/a	n/a	**0.000**	**0.000**	Mobe into camp. No IP completed	
07-Jul-2006	2400	-1200	-400	**0.800**	**0.800**	Heavy rain in the morning. Completed some of L2400.	
08-Jul-2006	2400	-400	400	**0.800**	**1.600**	Rain in the morning and throughout day.	
09-Jul-2006	2200	-1200	400	**1.600**	**3.200**	Excellent day, completed line without any problems.	
10-Jul-2006	2000	-1300	-425	**0.875**	**4.075**	Bad radio communication halted production.	
11-Jul-2006	2000	-425	500	**0.925**	**5.000**	Moved transmitter to new site with better radio communication.	
12-Jul-2006	1800	-1300	-350	**0.950**	**5.950**	Reeled wire from previous line and completed half of line.	
13-Jul-2006	1800	-350	600	**0.950**	**6.900**	Completed line. Intense thunderstorms slowed progress	
14-Jul-2006	n/a				**6.900**	Reeled wire from 1800 and moved line to 1600 before intense thunderstorms moved in and lasted all day.	
15-Jul-2006	1600	-1300	-500	**0.800** **0.000**	**7.700**	Thunderstorms finally cleared by 8 pm and we headed out. Lost pigtail on reel. Cliffs from 725 to 675 S on line. Noisy data necessitated several readings	
16-Jul-2006	1600	-500	600	**1.100**	**8.800**	Cliff also at 475 S. Noisy data necessitated several readings.	
17-Jul-2006	1400	-1300	-200	**1.100**	**9.900**	Noisy data necessitated several readings. Radio comm. problems.	
18-Jul-2006	1400	-200	600	**0.800** **0.000**	**10.700** **10.700**	Large boulder field between 275 and 450 N prevented us from gathering data as no current could be put into the	

				0.000	**10.700**	ground and no signal was being picked up.
19-Jul-2006	1200	-1300	-200	**1.100** **0.000**	**11.800** **11.800**	Noisy data necessitated several readings. Reeled wire from previous line before getting started.
20-Jul-2006	n/a	n/a	n/a	**0.000**	**11.800**	Rain and fog prevented us from setting out for night shift. Slept & set out early following day.
21-Jul-2006	1200	-200	600	**0.800**	**12.600**	Rock field at 250N prevented readings here. Triggered on Ch3 at station 200 and Ch3 at 225 to maximize readings possible.
22-Jul-2006	1000	-1300	600	**1.900** **0.000**	**14.500** **0.000**	Open loop turned out to be a total of 6 breaks in the line and the electrodes at the start of the line were pulled out.
23-Jul-2006	800	-700	150	**0.850**	**15.350**	Shorter day to make up for extra long previous day.
24-Jul-2006	800 600	150 -500	700 0	**0.550** **0.500**	**15.900** **16.400**	Stakes 475 and 500N mixed up on line. First half of line 800 VLF done.
25-Jul-2006	600	0	1000	**1.000**	**17.400**	VLF for line 800 completed.
26-Jul-2006	400	0	1000	**1.000**	**18.400**	Part of VLF for line 400 completed.
27-Jul-2006	200	0	1000	**1.000**	**19.400**	Intense thundershower with hail and heavy rain did not clear until 4 pm, delaying progress.
28-Jul-2006	0	0	1000	**1.000**	**20.400** **0.000**	Lost radio contact with transmitter for 30 minutes. Reeled all wire along baseline and prepared load for mobe.
29-Jul-2006	n/a	n/a	n/a	**0.000**	**20.400**	Completed VLF for lines 600, 400, 200, and zero
30-Jul-2006	n/a	n/a	n/a	**0.000**	**20.400**	Mobe out of camp, no IP completed.

Mag / VLF survey log sheet

Crew: Gabe Fortin (Geologist, crew chief)
Cody Woodman (Field assistant)

Monday, July 10
Pick up groceries and fuel up in Mayo then drive to Scheelite Dome. Setup Camp at 438427 7071010. Mostly sunny and warm.

Tuesday, July 11
Locate grid. VLF for Cody and he does L2400E and L2200E. Gabe fixed Jenn's xGate the Mag on north end of L600E, all of L800E and south part of L1000E. Mostly sunny and hot, a few showers around lunch time.
Production: 3.7 km of Mag / 3.2 km of VLF

Wednesday, July 12
Cody VLF L2000E and L1800E. Gabe mags L0000E, L0200E, L0400E, South end of L600E, South end of L1200E, south end of L1400E, south end of L1600E, south end of L2000E. Sunny in AM then rain and hail at times pretty heavy.
Production: 5.9 km of Mag / 3.7 km of VLF

Thursday, July 13
Some thunder showers through the day, thunder and lightning mostly farther away. Smoke from forest fire seen on north side of mountain north of camp. Cody VLF L1400E and L1600E, Gabe mags north end of L1000E, north end of L1200E, north end of L1400E, north of L1600E, L2200E and L2400E
Production: 7.8 km of Mag / 3.8 km of VLF

Friday, July 14
Gabe mags L1800E and finished L2000E. Cody VLF south part of L1200E. Return to camp and de-mobe to Whitehorse in afternoon-evening. Some rain and thunder around noon.
Production: 3.0 km of Mag / 0.6 km of VLF

Line cutting operation log sheet

Grid:	Scheelite Dome		**Datum used:** NAD27 - Canada 8N
Crew:	Larry Brault, line cutting Foreman Matt Olsen, Cutter Warren Pearson, Brusher Gordon Ruby, Brusher		**Total line-km cutting**: 22.8
Date	Daily line-km	**Total line-km for the grid**	Comment
11-Jun-2006	0.000	0.000	Line cutters mobe into road camp.
12-Jun-2006	0.800	0.800	Finish setting up camp in morning.
13-Jun-2006	1.400	2.200	
14-Jun-2006	1.500	3.700	
15-Jun-2006	1.750	5.450	
16-Jun-2006	0.000	5.450	Rain, low cloud. Camp move postponed, finish pickets
17-Jun-2006	0.000	5.450	Light rain, move camp up to grid
18-Jun-2006	1.150	6.600	
19-Jun-2006	1.400	8.000	

20-Jun-2006	2.050	10.050	
21-Jun-2006	1.200	11.250	
22-Jun-2006	2.450	13.700	
23-Jun-2006	2.400	16.100	
24-Jun-2006	2.000	18.100	
25-Jun-2006	0.700	18.800	
26-Jun-2006	1.300	20.100	
27-Jun-2006	0.000	20.100	Rain and low cloud, no work
28-Jun-2006	0.900	21.000	
29-Jun-2006	1.400	22.400	
30-Jun-2006	0.400	22.800	
01-Jul-2006	0.000	22.800	Line cutters demobe to Whitehorse

APPENDIX C – INSTRUMENT SPECIFICATIONS

I. OVERVIEW

I.1. GENERALITIES

The ELREC Pro unit is a receiver designed for high productivity mineral exploration
It allows to measure primary voltage and decay voltage curve values, giving thus resistivity and chargeability (IP) data.
This unit is designed to be used with an *IRIS instruments* external transmitter, called VIP.

The main technical characteristics of this receiver are the following ones:
- 10 reception dipoles available to carry out some measurements with high productivity in the field
- 20 partial chargeability windows available to measure the discharge phenomena with an high accuracy.
- a 1 µV resolution on the primary voltage allowing to obtain very accurate measurements.
- a large graphic LCD display for user-friendly operating allowing to show the data in real time numerically and graphically.

The ELREC Pro unit can be also used in automatic switching mode (in that case, some additional external *Switch Plus* boxes have to be used) for intensive measurements.

I.2. DESCRIPTION

I.2.1. Front panel

All controls are located on the front panel. This one features:
- Graphic LCD (128x140 dots) made of 16 lines by 40 characters
- Eleven plugs for connecting the potential electrodes
- Plugs "+" and "-" for the external battery connection
- Three pins plug (RS232 standard port) for the serial link cable connection
- Four pins plug for internal battery charger connection
- Keyboard with 16 keys

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ANNEX 3: IP PARAMETERS AND CHARGEABILITY

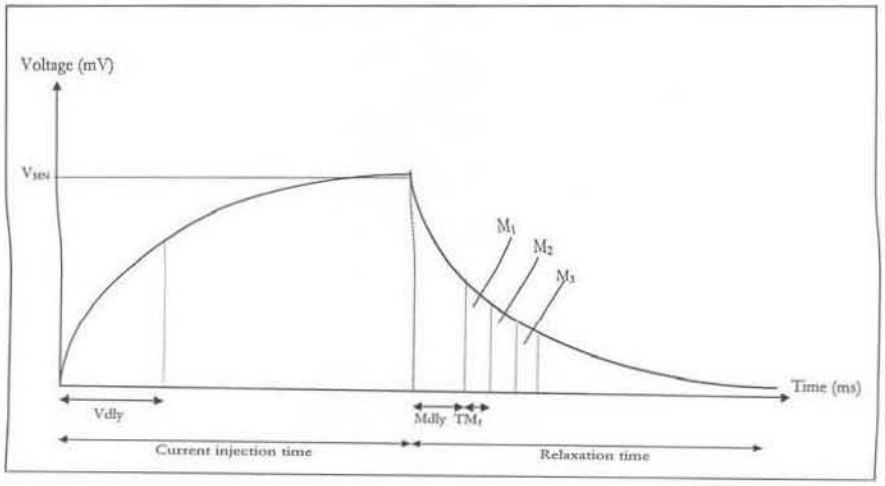
The partial chargeabilities measurements (M_i) and the average global one deduced (M_g) give some information regarding the ability of the soil to charge itself due to a current flow.
The partial chargeability of the window "i" is measured thanks to the following formula:

$$M_i = \int_{TM_i} Vdt \,/\, TM_i.V_{MN}$$

And the global chargeability is computed thanks to the following formula:

$$M_g = \sum_{i=1}^{n} (M_i.TM_i) \,/\, \sum_{i=1}^{n} TM_i \qquad \text{(n: number of IP windows)}$$

The discharge phenomena observed during the relaxation time can be described according to the following curve:



With the ELREC Pro, up to 20 IP windows can be used to define the decay curve.

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The number of IP windows available for the measurement depends on the type of IP mode and on the current injection time:

⇒ **Current injection times** available (cf. II.1.5): 500 ms - 1 s - 2 s - 4 s - 8 s

⇒ Types of **IP mode** available (cf. II.1.5): Arithmetic – Semi logarithmic – Logarithmic Cole-Cole - Programmable

For a given current injection time and IP mode, the program will choose automatically the IP parameters (Mdly, Vdly, TM_i) that will be used for the measurement.

Note:

The programmable mode is a mode where 20 fully programmable windows are available. The operator has to select the delay time (Mdly) with a minimum of 20 ms and the width of each partial window (TM_i) with a minimum of 10 ms. Vdly is automatically determined by the injection time chosen.

In the following tables, the preset TM_i values are given for each IP mode (1 means TM_1 ...):

- **Time = 500 ms**

Mode	Vdly	Mdly	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Arith.	280	60	40	40	40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Semi	280	40	40	80	160	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Log.	280	160	80	180	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cole	280	160	80	180	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

- **Time = 1000 ms**

Mode	Vdly	Mdly	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Arith.	580	120	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40
Semi	580	40	20	20	20	20	20	20	20	20	40	40	40	40	40	40	80	80	80	80	80	80
Log.	580	160	120	220	420	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cole	580	20	10	20	20	20	20	20	30	30	30	40	40	40	50	50	50	60	60	70	80	90

- **Time = 2000 ms**

Mode	Vdly	Mdly	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Arith.	1260	240	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80	80
Semi	1260	40	40	40	40	40	40	40	80	80	80	80	80	80	80	160	160	160	160	160	160	160
Log.	1260	160	120	220	420	820	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cole	1260	20	20	30	30	30	40	40	50	60	70	80	90	100	110	120	130	140	150	160	180	200

• **Time = 4000 ms**

Mode	Vdly	Mdly	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Arith.	2620	480	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160
Semi	2620	160	80	80	80	80	80	80	80	80	160	160	160	160	160	160	320	320	320	320	320	320
Log.	2620	160	120	220	420	820	1620	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cole	2620	20	40	50	60	70	80	90	100	110	120	140	160	180	200	220	250	280	320	380	450	530

• **Time = 8000 ms**

Mode	Vdly	Mdly	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
Arith.	5340	960	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320	320
Semi	5340	320	160	160	160	160	160	160	160	160	320	320	320	320	320	320	640	640	640	640	640	640
Log.	5340	160	120	220	420	820	1620	3220	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cole	5340	20	40	60	80	100	120	150	180	220	250	280	320	360	400	450	500	580	700	850	1010	1180

About the **IP values type**, note that the changing "raw (R) ⇔ normalised (N)" can be realised after the acquisition.

The normalization allows to homogenize the data that have been obtained with various injection and integration times. This is made with respect to a standard decay curve, which is the one obtained with the following parameters:

Mode: Logarithmic
Injection time: 2000 ms
Vdly: 1260 ms
Mdly: 160 ms
TM_1: 120 ms
TM_2: 220 ms
TM_3: 420 ms
TM_4: 820 ms

The coefficients to multiply, allowing to go from a type to the other one, are indicated in the following tables:

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ANNEX 7: SPECIFICATIONS

Technical:

- Input impedance: 10 Mohm
- Input overvoltage protection up to 1000V
- Automatic SP bucking with linear drift correction
- Internal calibration generator for a true calibration on request of the operator
- Internal memory: 3200 dipoles reading
- Automatic synchronization and re-synchronization process on primary voltages signals whenever needed
- Proprietary intelligent stacking process rejecting strong non-linear SP drifts
- Common mode rejection: more than 100 dB (for Rs = 0)
- Self potential (Sp) : range: -15V - +15V
  : resolution: 0.1 mV
- Ground resistance measurement range: 0.1 - 100 kohms
- Primary voltage : range: 10µV - 15V
  : resolution: 1µV
  : accuracy: typ. 0.3%
- Chargeability : resolution: 10µV/V
  : accuracy: typ. 0.6%

General:

- Dimensions: 31x21x25 cm
- Weight (with the internal battery): 9 kg
- Operating temperature range: -30°C - 70°C
- Case in fiber-glass for resisting to field shocks and vibrations

Instrumentation GDD

The Induced Polarization Transmitter

TxII-1800 and TxII-3600 Models

For Fast, High-Quality Induced Polarization Surveys in All Field Conditions

Flyers high / low resolution TxII/1 **(63 KB) /** TxII/2 **(1 MB)**

At Last, a High-Quality Affordable IP Transmitter

TxII-1800 Model, 1800 watts

Its high power, up to 10 amperes, combined with its light weight and a 21 kg/2000W Honda generator makes it particularly suitable for dipole-dipole Induced Polarization surveys.

Features

- **Protection against short circuits even at zero (0) ohms**
- **Output voltage range: 150 V to 2400 V / 14 steps**
- **Power source: 120 V, Optional: 220 V / 50/60 Hz**
- **Operates from a light backpackable standard 120 V generator**
- **Up to three years warranty**

This backpackable 1800 watts induced polarization (I.P.) transmitter works from a standard 120 V source and is well adapted to

CONTENTS

TxII-1800/TxII-3600 IP transmitter
Specifications
Purchase - Rental

rocky environments where a high output voltage of up to 2400 V is needed. Moreover, in highly conductive overburden, at 150 V, the highly efficient TxII-1800 watts transmitter is able to send a current of up to 10 amperes. By using this I.P. transmitter, you obtain fast and high-quality I.P. readings even in the most difficult conditions.

TxII-3600 Model, 3600 watts

Its high power, up to 10 amperes, combined with a Honda generator makes it particularly suitable for pole-dipole Induced Polarization surveys.

Features

- **Protection against short circuits even at zero (0) ohms**
- **Output voltage range: 150 V to 2400 V / 14 steps**
- **Power source: 220 V, 50/60 Hz**
- **Operates from a standard 220 V generator**
- **Up to three years warranty**

This 3600 watts induced polarization (I.P.) transmitter works from a standard 220 V source and is well adapted to rocky environments where a high output voltage of up to 2400 V is needed. Moreover, in highly conductive overburden, at 150 V, the highly efficient TxII-3600 watts transmitter is able to send a current of up to 10 amperes. By using this I.P. transmitter, you obtain fast and high-quality I.P. readings even in the most difficult conditions.

Specifications

General	
Size TxII-1800	21 x 34 x 39 cm
Size TxII-3600	21 x 34 x 50 cm
Weight TxII-1800	approx. 20 kg
Weight TxII-3600	approx. 35 kg

Operating temperature	-40°C to 65°C
Electrical	
Used for time-domain IP	2 sec. ON 2 sec. OFF
Time Base	1-2-4-8 sec.
Output current range	0.005 to 10 A
Output voltage range	150 to 2400 V
Power source TxII-1800	Recommended motor/generator set: Standard 120 V / 60 Hz backpackable Honda generator Suggested Models: EU1000iC, 1000 W, 13.5 kg. or EU2000iC, 2000 W, 21.0 kg.
Power Source TxII-3600	Recommended motor/generator set: Standard 220 V, 50/60 Hz Honda generator Suggested Models: EM3500XK1C, 3500 W, 62 kg or EM5000XK1C, 5000 W, 77 kg
Controls	
Power	ON/OFF
Output voltage range switch	150 V, 180 V, 350 V, 420 V, 500 V, 600 V, 700 V, 840 V, 1000 V, 1200 V, 1400 V, 1680 V, 2000 V, 2400 V
Displays	
Output current LCD	reads to ±0,001 A
Very cold weather	standard LCD heater on readout
Protection	Total protection against short circuits even at zero (0) ohms
Indicator lamps **(in case of overload)**	- High voltage ON-OFF - Output overcurrent - Generator over or undervoltage - Overheating - Logic failure - Open loop protection

Purchase and Rental Info

Interested by the TxII-1800 W IP or the TxII-3600 W IP transmitter?

It is simple. You can rent it or purchase it. The choice is yours. Here is some information you

INSTRUMENT SPECIFICATIONS

MAGNETOMETER / GRADIOMETER

Resolution:	0.01nT (gamma), magnetic field and gradient.
Accuracy:	0.2nT over operating range.
Range:	20,000 to 120,000nT.
Gradient Tolerance:	Over 10, 000nT/m
Operating Interval:	3 seconds minimum, faster optional. Readings initiated from keyboard, external trigger, or carriage return via RS-232C.
Input / Output:	6 pin weatherproof connector, RS-232C, and (optional) analog output.
Power Requirements:	12V, 200mA peak (during polarization), 30mA standby. 300mA peak in gradiometer mode.
Power Source:	Internal 12V, 2.6Ah sealed lead-acid battery standard, others optional. An External 12V power source can also be used.
Battery Charger:	**Input:** 110 VAC, 60Hz. Optional 110 / 220 VAC, 50 / 60Hz. **Output:** dual level charging.
Operating Ranges:	Temperature: - 40°C to +60°C. Battery Voltage: **10.0V minimum to 15V maximum.** Humidity: **up to 90% relative, non condensing.**
Storage Temperature:	-50°C to +65°C.
Display:	LCD: 240 X 64 pixels, OR 8 X 30 characters. Built in heater for operation below -20°C.
Dimensions:	**Console:** 223 x 69 x 240mm. **Sensor Staff:** 4 x 450mm sections. **Sensor:** 170 x 71mm dia. **Weight:** console 2.1kg, Staff 0.9kg, Sensors 1.1kg each.
VLF	
Frequency Range:	15 - 30.0 kHz plus 57.9 kHz (Alaskan station)
Parameters Measured:	Vertical in-phase and out-of-phase components as percentage of total field. 2 relative components of horizontal field. Absolute amplitude of total field.
Resolution:	0.1%.
Number of Stations:	Up to 3 at a time.
Storage:	Automatic with: time, coordinates, magnetic field / gradient, slope, EM field, frequency, in- and out-of-phase vertical, and both horizontal components for each selected station.
Terrain Slope Range:	0° - 90° (entered manually).
Sensor Dimensions:	140 x 150 x 90 mm. (5.5 x 6 x 3 inches).
Sensor Weight:	1.0 kg (2.2 lb).

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APPENDIX G
GSM-19T MAGNETOMETER/GRADIOMETER

THEORETICAL DESCRIPTION

Introduction

The GSM-19T is a portable standard proton magnetometer/gradiometer designed for handheld or base station use for geophysical, geotechnical, or archaeological exploration, long term magnetic field monitoring at Magnetic Observatories, volcanological and seismic research, etc. The GSM-19T is a secondary standard for measurement of the Earth's magnetic field, having 0.2nT resolution, and 1nT absolute accuracy over its full temperature range.

The GSM-19T is a microprocessor based instrument with storing capabilities. Large memory storage is a available (up to 2Mbytes). Synchronized operation between hand held and base station units is possible, and the corrections for diurnal variations of magnetic field are done automatically. The results of measurement are made available in serial form (RS-232-C interface) for collection by data acquisition systems, terminals or computers. Both on-line and post-operation transfer are possible.

The measurement of two magnetic fields for determination of gradient is done concurrentlly with strict control of measuring intervals. The result is a high quality gradient reading, independent of diurnal variations of maganetic field.

Optionally the addition of a VLF sensor for combined magnetometer / gradiometer-VLF measurement is available.

Magnetic Field Measurement

The magnetic field measuring process consist of the following steps:

a) Polarization: A strong DC current is passed through the sensor creating polarization of a proton-rich fluid in the sensor.

b) Pause: The pause allows the electrical transients to die off, leaving a slowly decaying proton precession signal above the noise level.

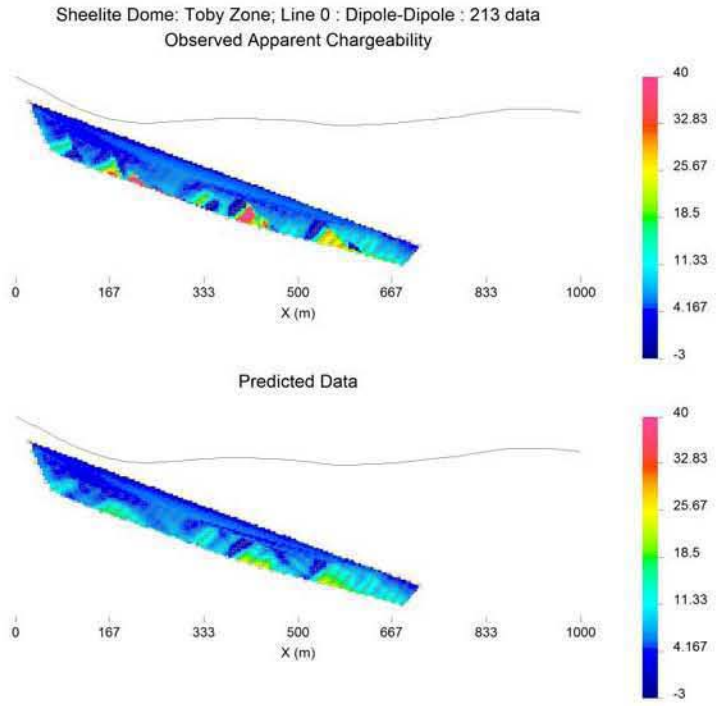
c) Counting: The proton precession frequency is measured and converted into magnetic field units.

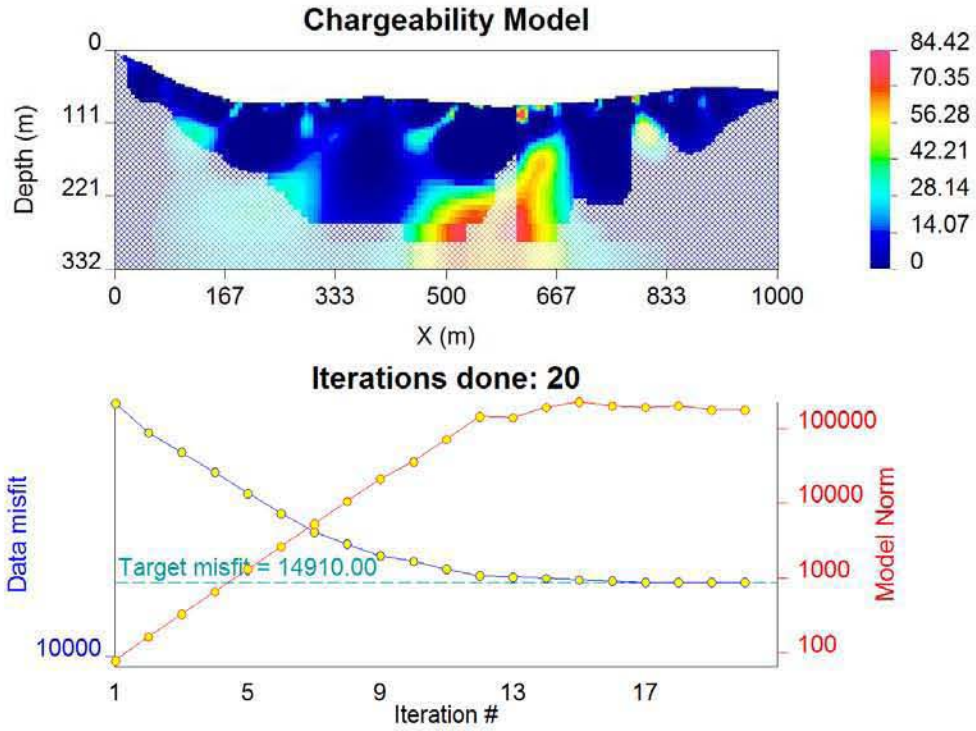
d) Storage: The results are stored in memory together with date, time and coordinates of measurement. In base station mode, only the time and total field are stored.

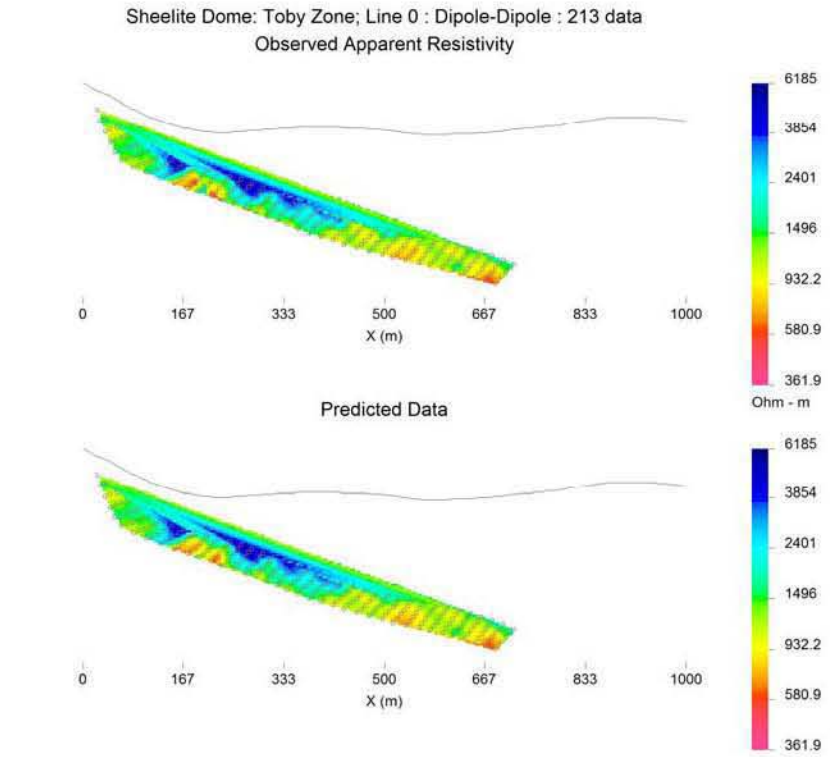
GEONICS LIMITED
VLF EM 16

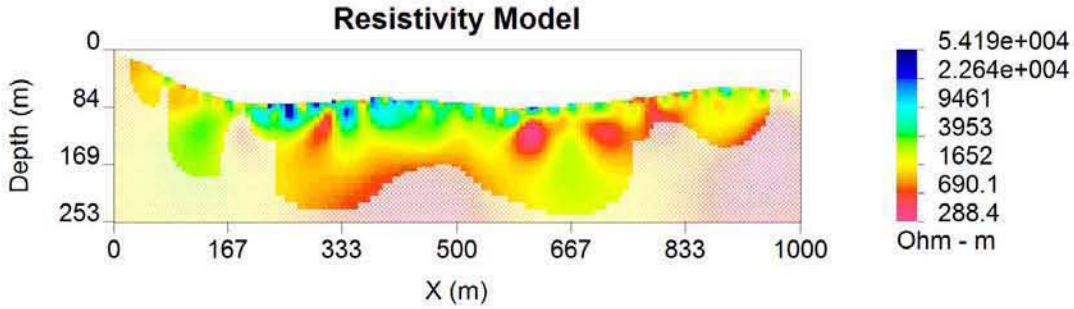
Source of Primary Field:	VLF transmitting stations
Transmitting Stations Used:	Any desired station frequency can be supplied with the instrument in the form of plug-in tuning units. Two tuning units can be plugged in at one time. A switch selects either station.
Operating Frequency Range:	About 15-25 Hz
Parameters Measured:	(1) The vertical in-phase component (tangent of the tilt angle of the polarization ellipsoid). (2) The vertical out-of-phase (quadrature) component (the short axis of the polarization ellipsoid compared to the long axis).
Method of Reading:	In-phase from a mechanical inclinometer and quadrature from a calibrated dial. Nulling by audio tone.
Scale Range:	In-phase ±150%; quadrature ±40%
Readability:	±1%
Reading Time:	10-40 seconds depending on signal strength
Operating Temperature Range:	-40 to 50° C.
Operating controls:	ON-OFF switch, battery testing push button, station selector, switch, volume control, quadrature, dial ±40%, inclinometer dial ±150%
Power Supply:	6 size AA (penlight) alkaline cells. Life about 200 hours
Dimensions:	42 x 14 x 9 cm (16 x 5.5 x 3.5 in)
Weight:	1.6 kg (3.5 lbs)
Instrument Supplied With:	Monotonic speaker, carrying case, manual of operation, 3 station selector plug-in tuning units (additional frequencies are optional), set of batteries
Shipping Weight:	4.5 kg (10 lbs.)
Name and Address of Manufacturer:	Geonics Limited 1745 Meyerside Drive/Unit 8 Mississauga, Ontario L5T 1C5

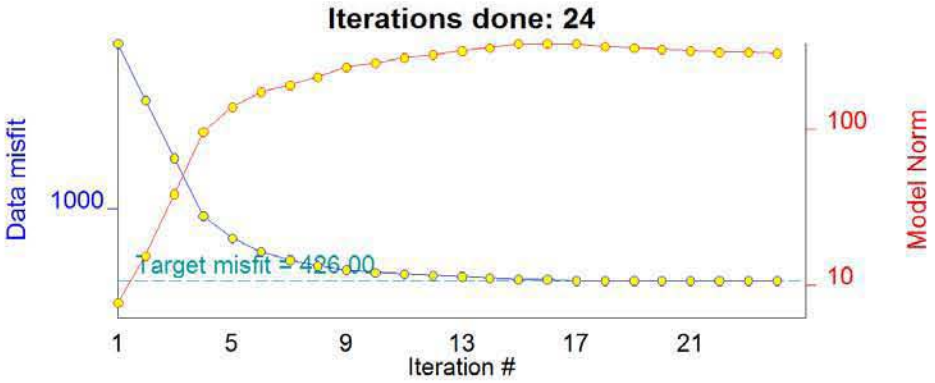
APPENDIX D – INVERSION RESULTS

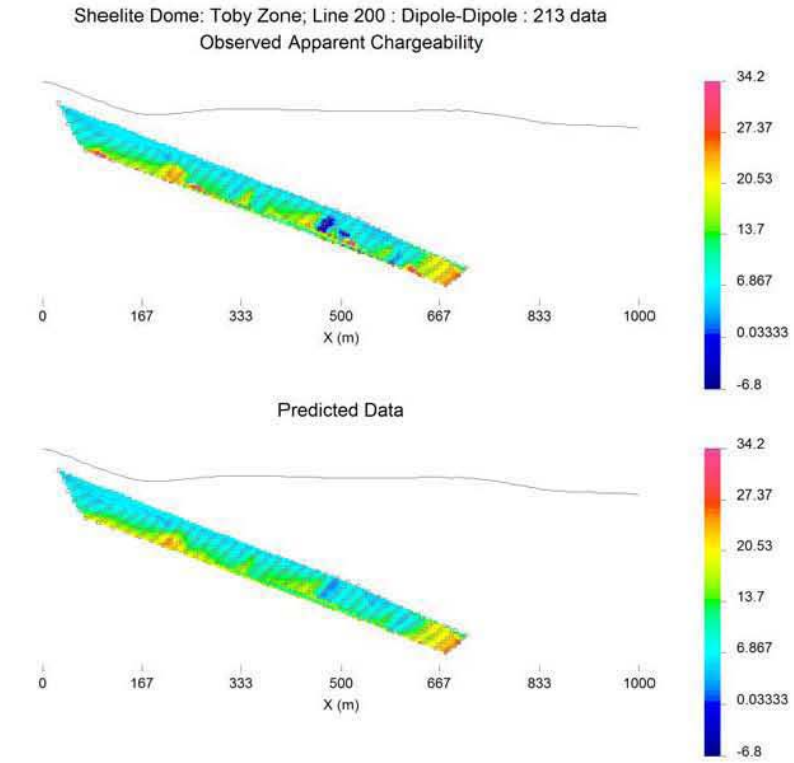


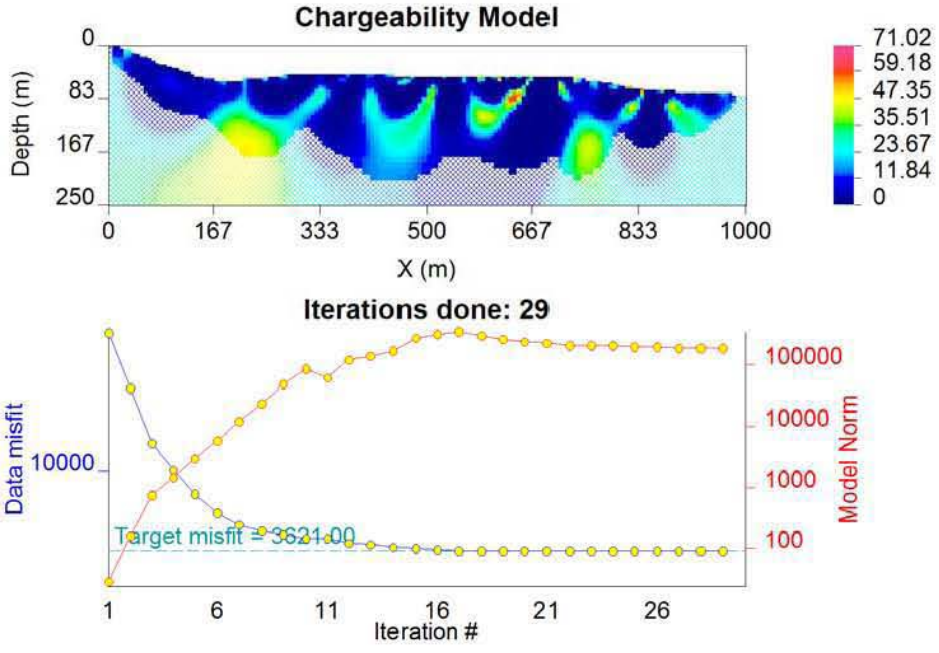


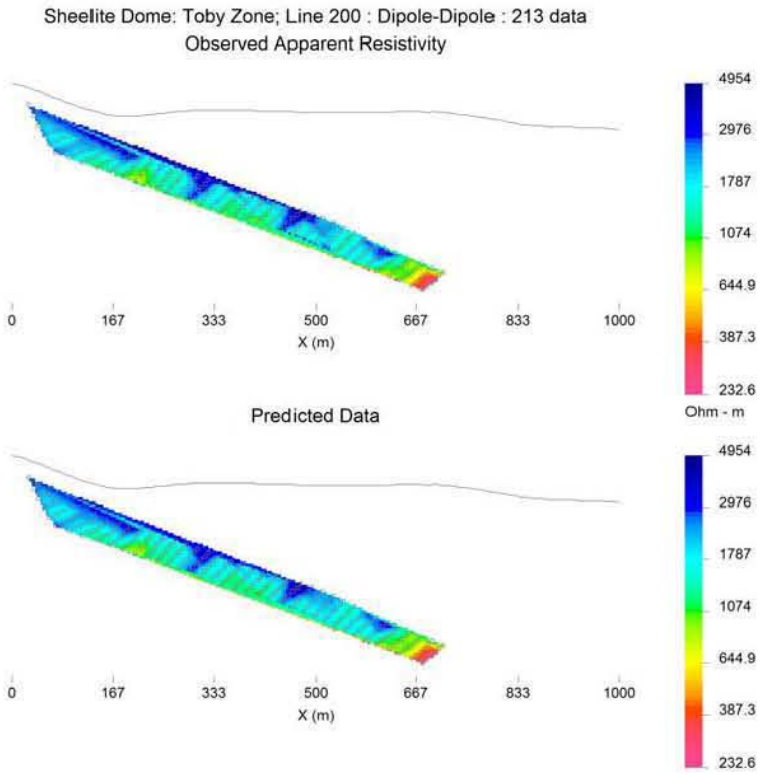

Sheelite Dome: Toby Zone; Line 0 : Dipole-Dipole : 213 data
Observed Apparent Resistivity
6185
3854
2401
1496
932.2
580.9
361.9
Ohm - m
0
167
333
500
667
833
1000
X (m)
Predicted Data
6185
3854
2401
1496
932.2
580.9
361.9
0
167
333
500
667
833
1000
X (m)

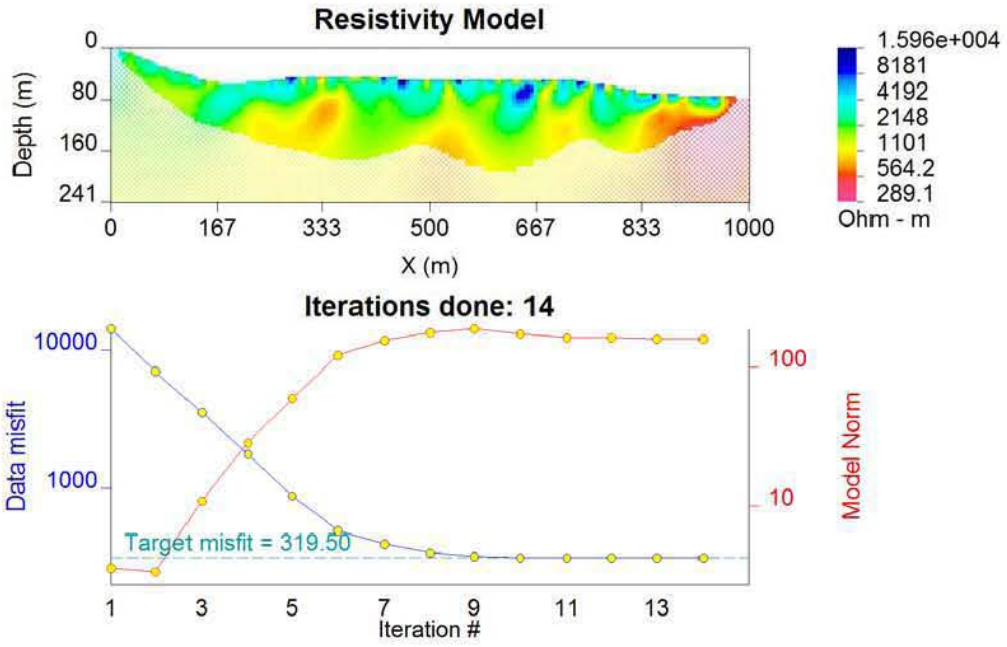

Resistivity Model
Depth (m)
0
84
169
253
0
167
333
500
667
833
1000
X (m)
5.419e+004
2.264e+004
9461
3953
1652
690.1
288.4
Ohm - m

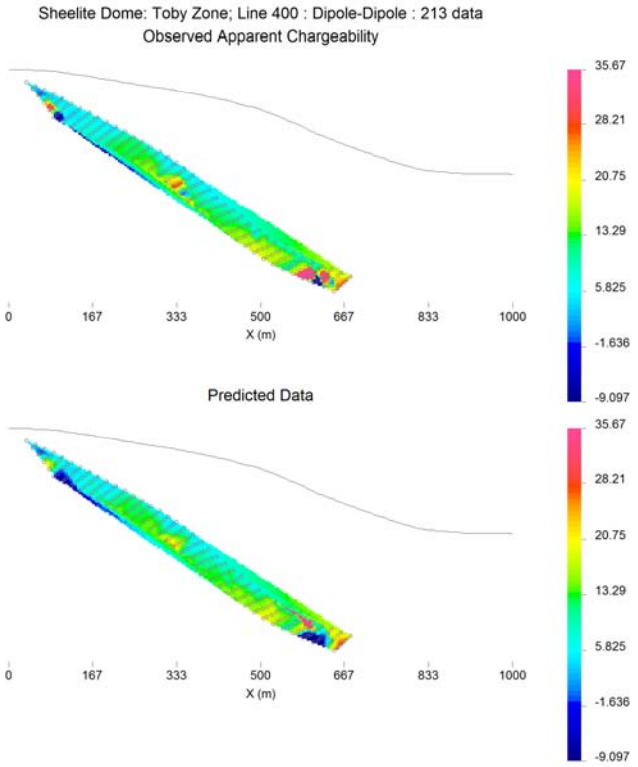

Iterations done: 24
Data misfit
1000
Target misfit = 426.00
100
10
Model Norm
1
5
9
13
17
21
Iteration #

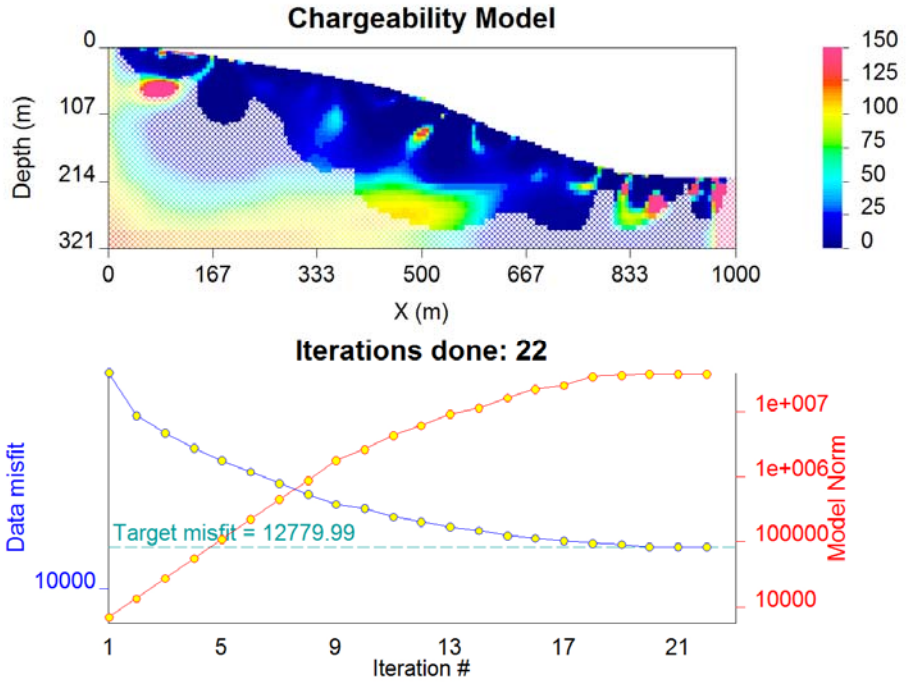

Sheelite Dome: Toby Zone; Line 200 : Dipole-Dipole : 213 data
Observed Apparent Chargeability
34.2
27.37
20.53
13.7
6.867
0.03333
-6.8
0
167
333
500
667
833
1000
X (m)
Predicted Data
34.2
27.37
20.53
13.7
6.867
0.03333
-6.8
0
167
333
500
667
833
1000
X (m)

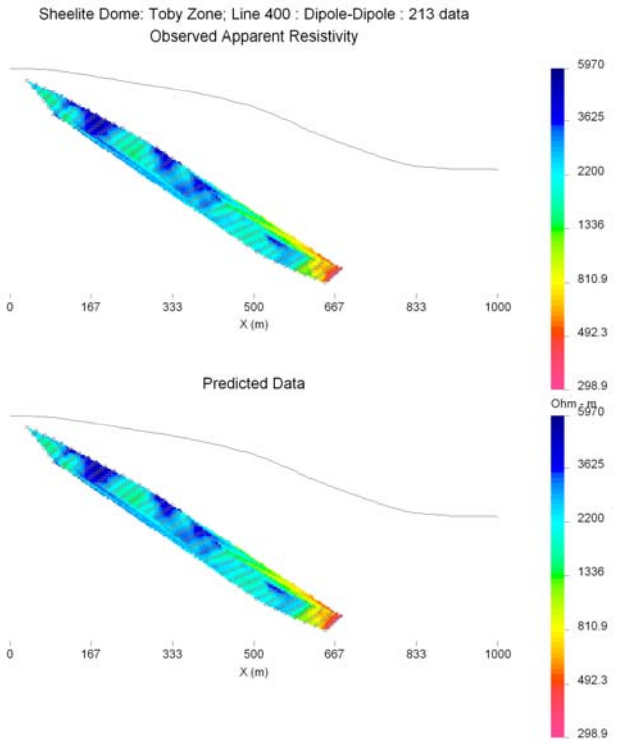

Chargeability Model
Depth (m)
0
83
167
250
0
167
333
500
667
833
1000
X (m)
71.02
59.18
47.35
35.51
23.67
11.84
0
Iterations done: 29
Data misfit
10000
Target misfit = 3621.00
100000
10000
1000
100
Model Norm
1
6
11
16
21
26
Iteration #

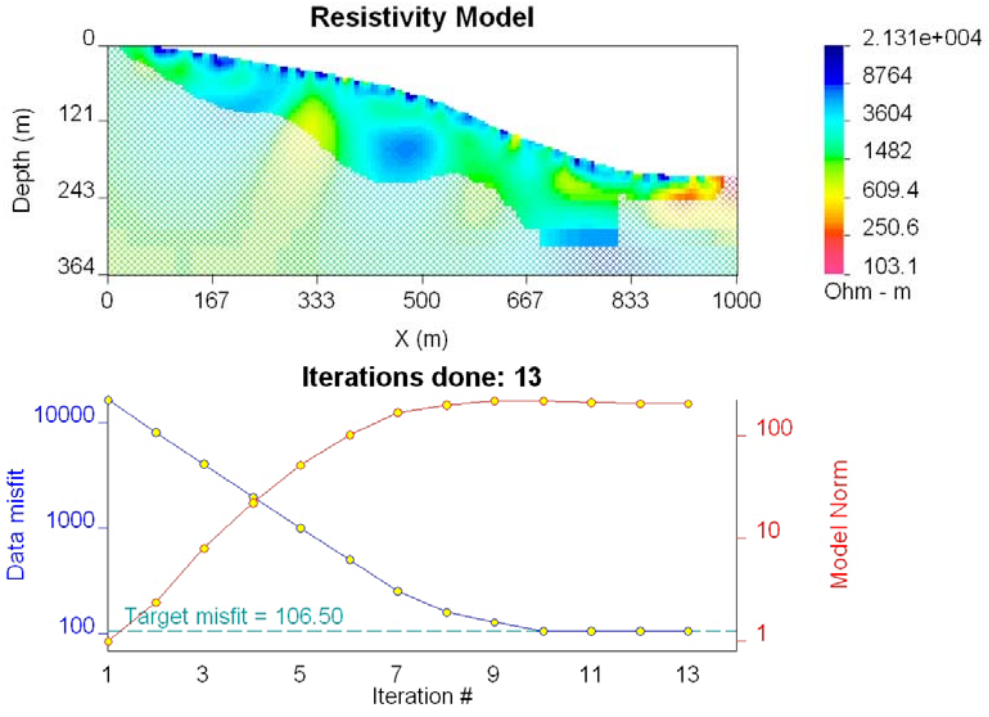

Sheelite Dome: Toby Zone; Line 200 : Dipole-Dipole : 213 data
Observed Apparent Resistivity
4954
2976
1787
1074
644.9
387.3
232.6
Ohm - m
0
167
333
500
667
833
1000
X (m)
Predicted Data
4954
2976
1787
1074
644.9
387.3
232.6
0
167
333
500
667
833
1000
X (m)

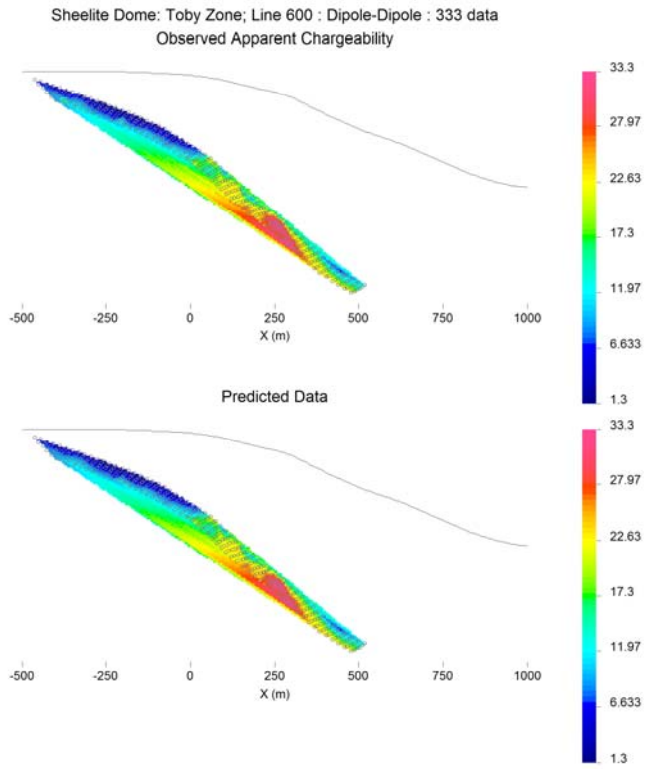

Resistivity Model
Depth (m)
0
80
160
241
0
167
333
500
667
833
1000
X (m)
1.596e+004
8181
4192
2148
1101
564.2
289.1
Ohm - m
Iterations done: 14
Data misfit
10000
1000
100
10
Model Norm
Target misfit = 319.50
1
3
5
7
9
11
13
Iteration #

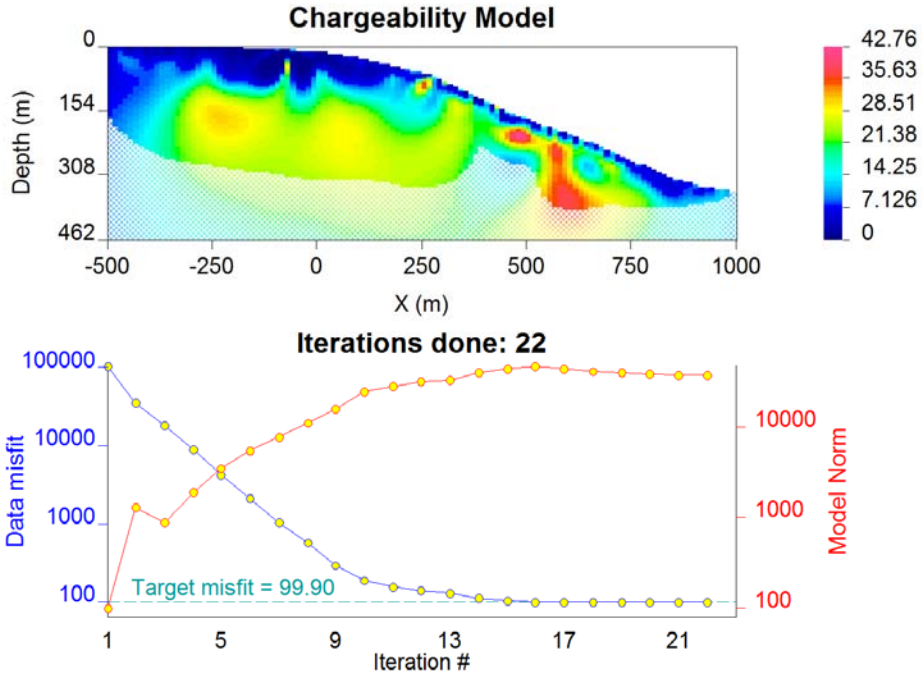

Sheelite Dome: Toby Zone; Line 400 : Dipole-Dipole : 213 data
Observed Apparent Chargeability
35.67
28.21
20.75
13.29
5.825
-1.636
-9.097
0
167
333
500
667
833
1000
X (m)
Predicted Data
35.67
28.21
20.75
13.29
5.825
-1.636
-9.097
0
167
333
500
667
833
1000
X (m)

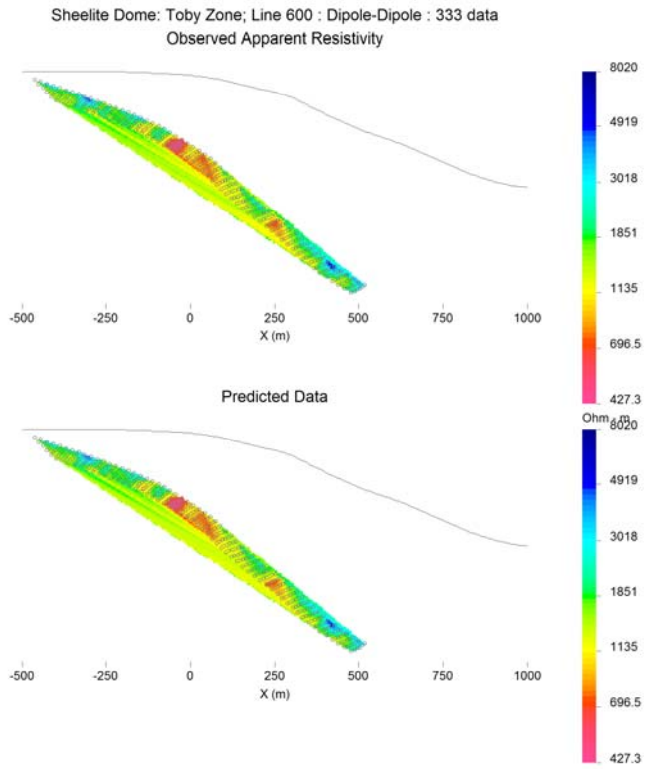

Chargeability Model
Depth (m)
0
107
214
321
0
167
333
500
667
833
1000
X (m)
150
125
100
75
50
25
0
Iterations done: 22
Data misfit
Target misfit = 12779.99
10000
1e+007
1e+006
100000
10000
Model Norm
1
5
9
13
17
21
Iteration #

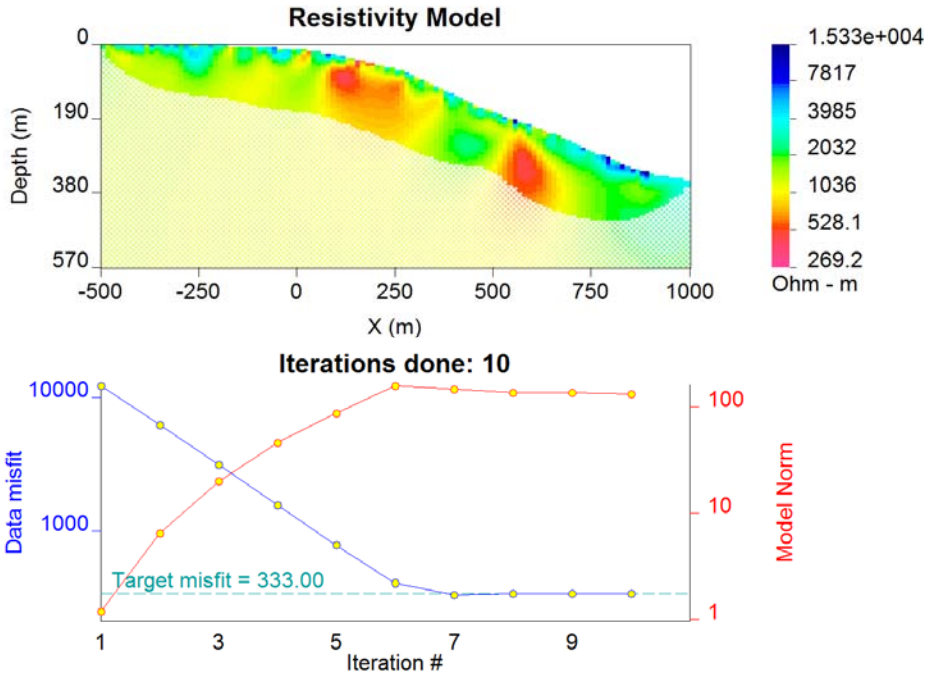

Sheelite Dome: Toby Zone; Line 400 : Dipole-Dipole : 213 data
Observed Apparent Resistivity
5970
3625
2200
1336
810.9
492.3
298.9
0
167
333
500
667
833
1000
X (m)
Predicted Data
Ohm - m
5970
3625
2200
1336
810.9
492.3
298.9
0
167
333
500
667
833
1000
X (m)

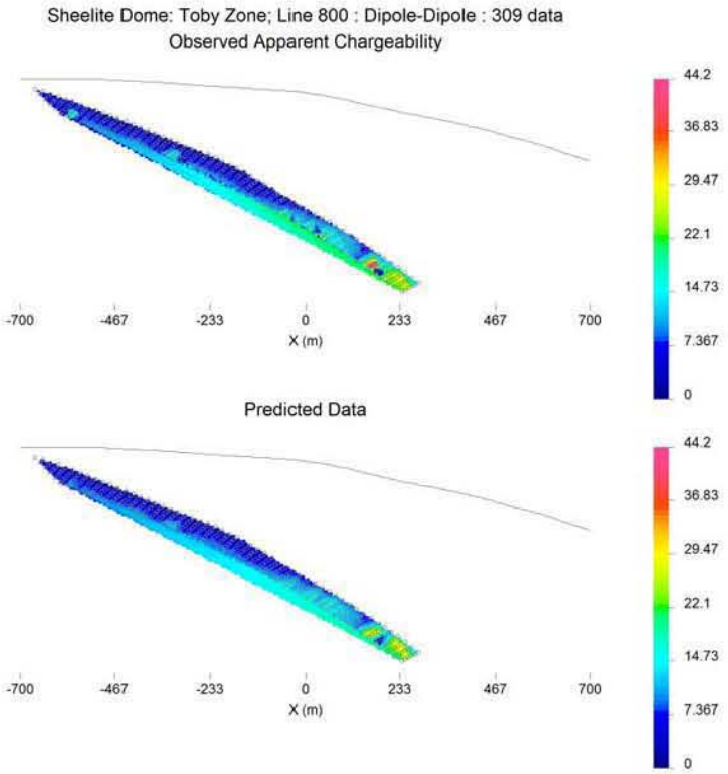

Resistivity Model
Depth (m)
0
121
243
364
0
167
333
500
667
833
1000
X (m)
2.131e+004
8764
3604
1482
609.4
250.6
103.1
Ohm - m
Iterations done: 13
Data misfit
10000
1000
100
Target misfit = 106.50
100
10
1
Model Norm
1
3
5
7
9
11
13
Iteration #

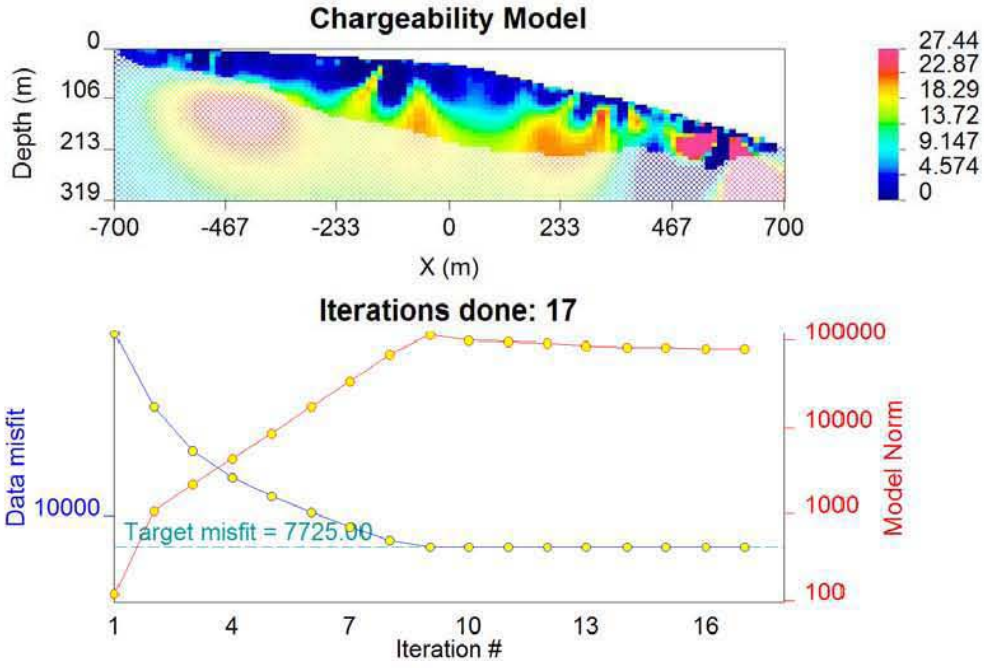

Sheelite Dome: Toby Zone; Line 600 : Dipole-Dipole : 333 data
Observed Apparent Chargeability
33.3
27.97
22.63
17.3
11.97
6.633
1.3
-500
-250
0
250
500
750
1000
X (m)
Predicted Data
33.3
27.97
22.63
17.3
11.97
6.633
1.3
-500
-250
0
250
500
750
1000
X (m)

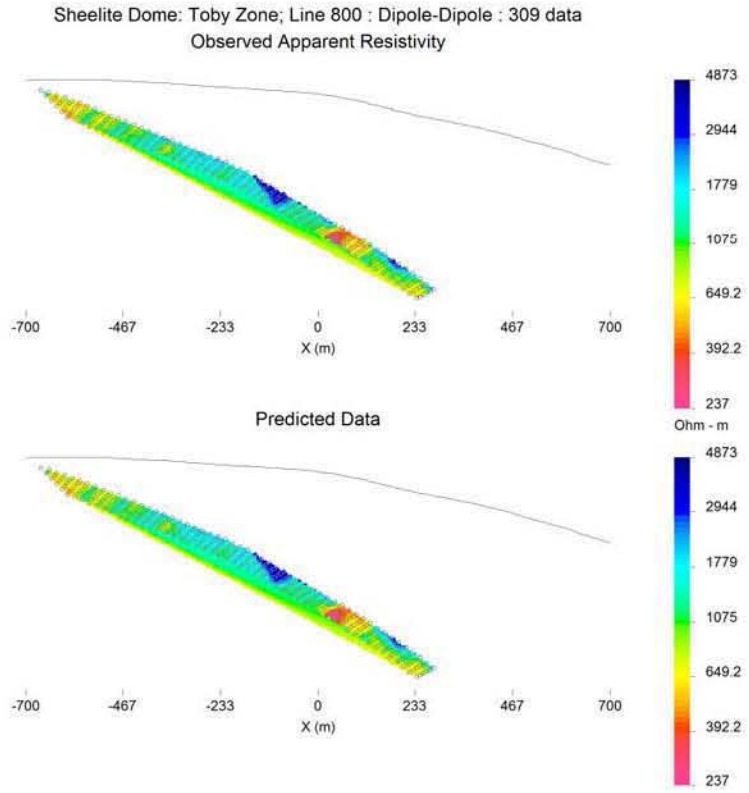

Chargeability Model
Depth (m)
0
154
308
462
-500
-250
0
250
500
750
1000
X (m)
42.76
35.63
28.51
21.38
14.25
7.126
0
Iterations done: 22
Data misfit
100000
10000
1000
100
Target misfit = 99.90
1
5
9
13
17
21
Iteration #
Model Norm
10000
1000
100

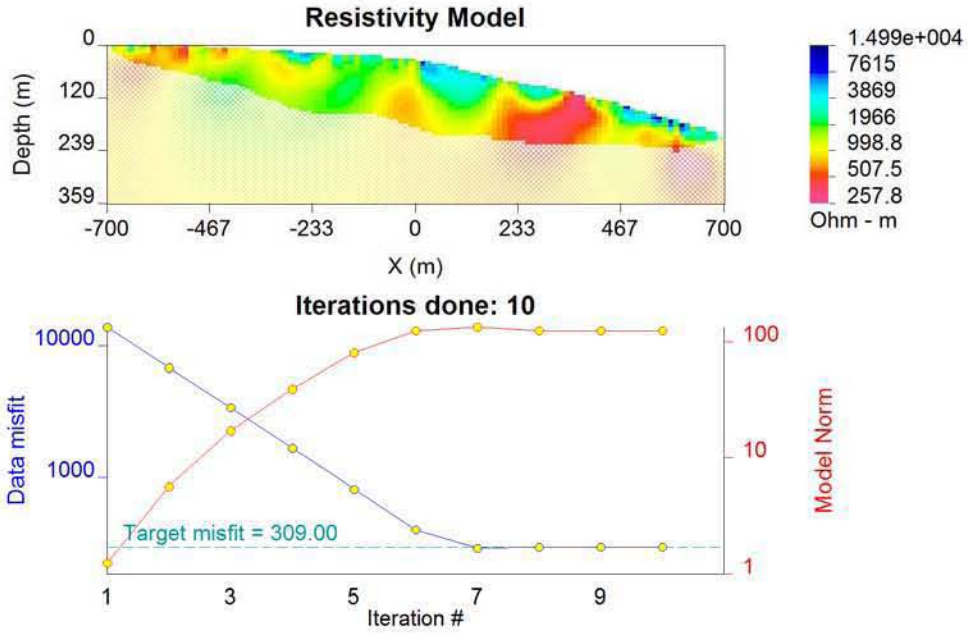

Sheelite Dome: Toby Zone; Line 600 : Dipole-Dipole : 333 data
Observed Apparent Resistivity
8020
4919
3018
1851
1135
696.5
427.3
-500
-250
0
250
500
750
1000
X (m)
Predicted Data
Ohm - m

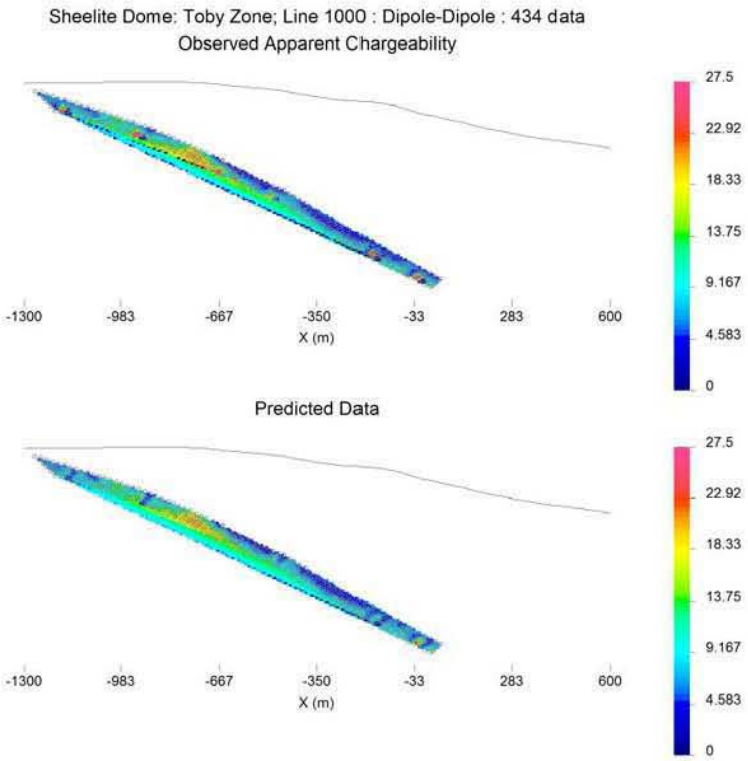

Resistivity Model
Depth (m)
0
190
380
570
-500
-250
0
250
500
750
1000
X (m)
1.533e+004
7817
3985
2032
1036
528.1
269.2
Ohm - m
Iterations done: 10
Data misfit
10000
1000
Target misfit = 333.00
Model Norm
100
10
1
1
3
5
7
9
Iteration #

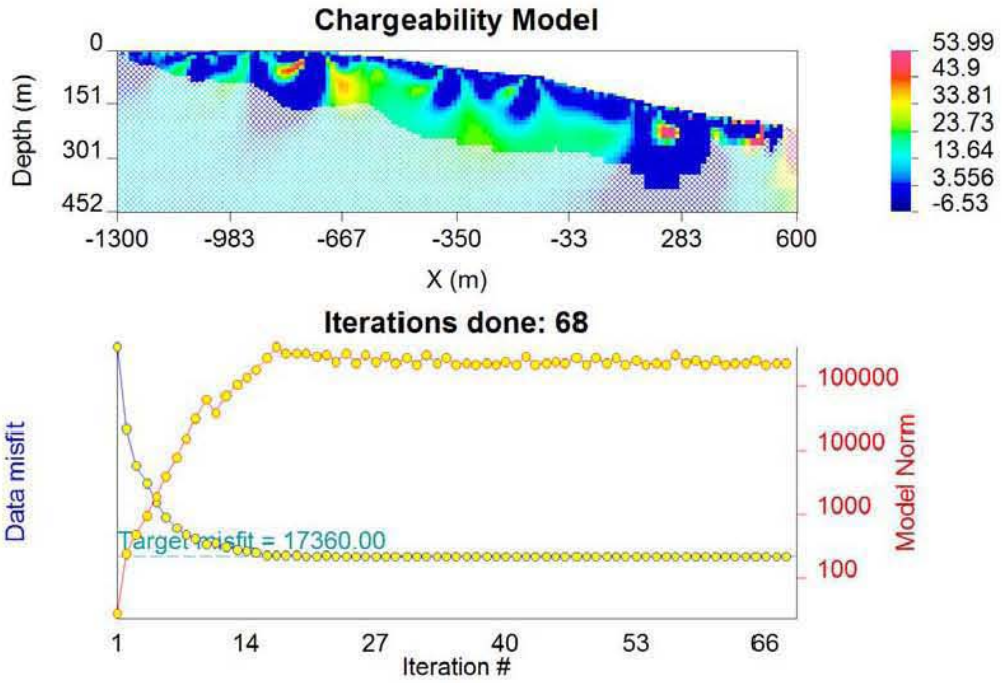

Sheelite Dome: Toby Zone; Line 800 : Dipole-Dipole : 309 data
Observed Apparent Chargeability
44.2
36.83
29.47
22.1
14.73
7.367
0
-700
-467
-233
0
233
467
700
X (m)
Predicted Data
44.2
36.83
29.47
22.1
14.73
7.367
0
-700
-467
-233
0
233
467
700
X (m)

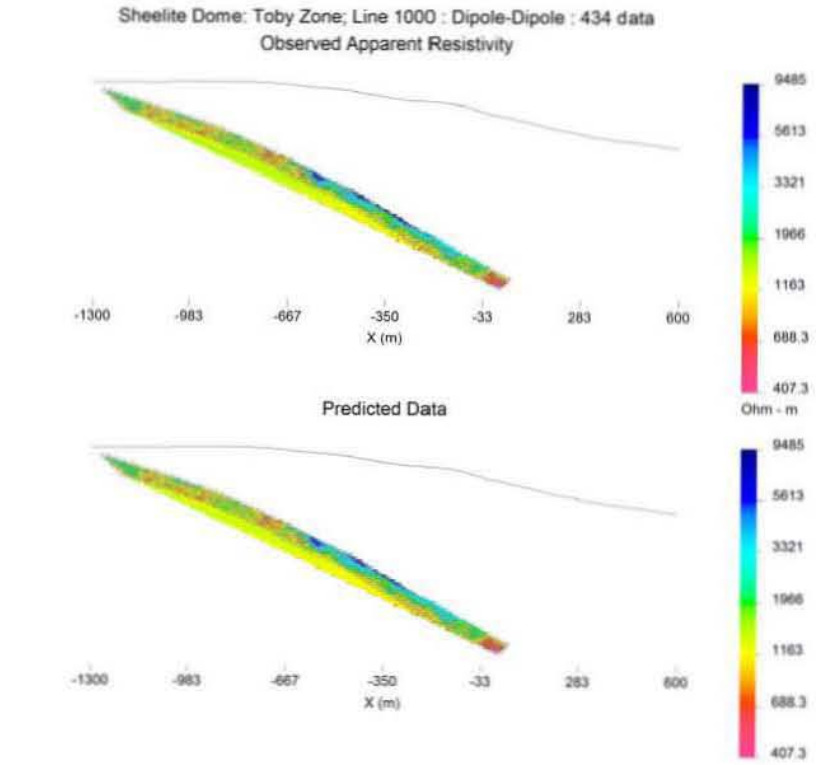

Chargeability Model
Depth (m)
0
106
213
319
-700
-467
-233
0
233
467
700
X (m)
27.44
22.87
18.29
13.72
9.147
4.574
0
Iterations done: 17
Data misfit
10000
Target misfit = 7725.00
100000
10000
1000
100
Model Norm
1
4
7
10
13
16
Iteration #

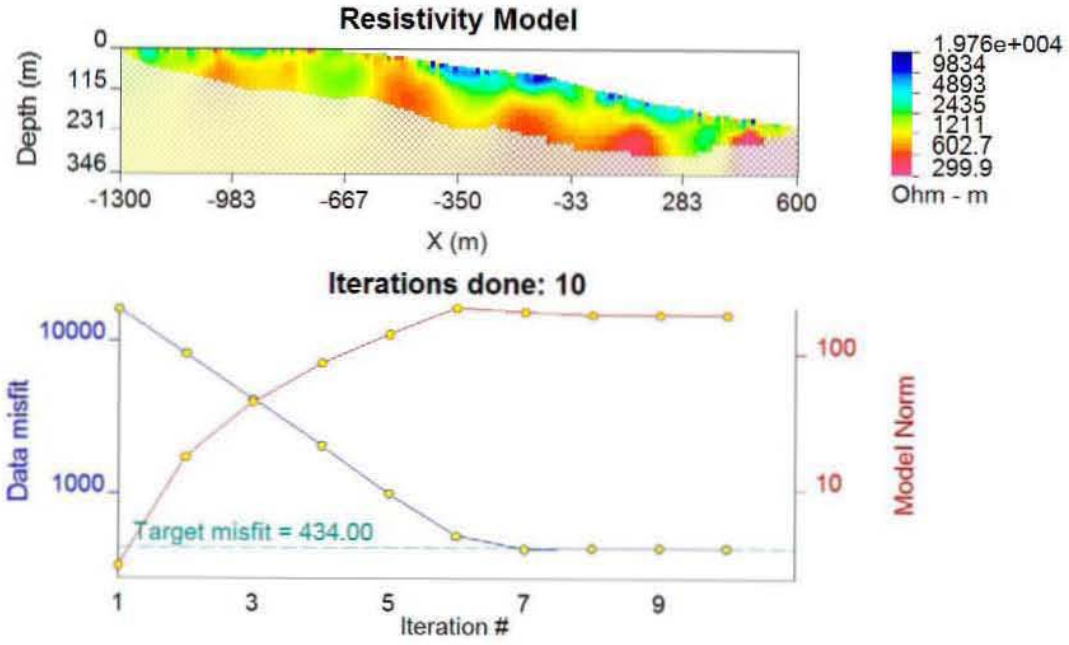

Sheelite Dome: Toby Zone; Line 800 : Dipole-Dipole : 309 data
Observed Apparent Resistivity
4873
2944
1779
1075
649.2
392.2
237
Ohm - m
-700
-467
-233
0
233
467
700
X (m)
Predicted Data
4873
2944
1779
1075
649.2
392.2
237
-700
-467
-233
0
233
467
700
X (m)

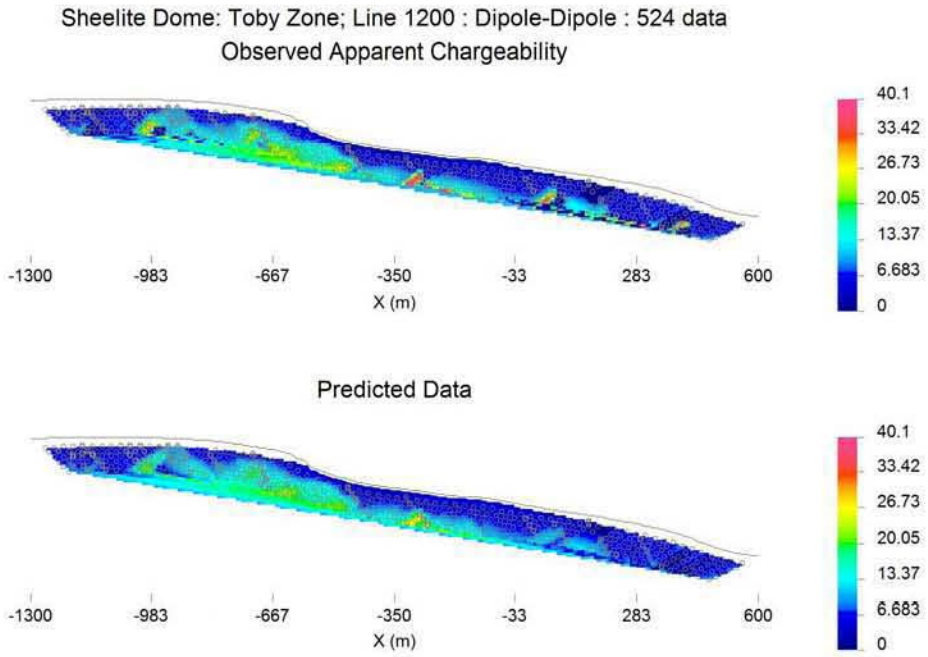

Resistivity Model
Depth (m)
0
120
239
359
-700
-467
-233
0
233
467
700
X (m)
1.499e+004
7615
3869
1966
998.8
507.5
257.8
Ohm - m
Iterations done: 10
Data misfit
10000
1000
Target misfit = 309.00
Model Norm
100
10
1
1
3
5
7
9
Iteration #

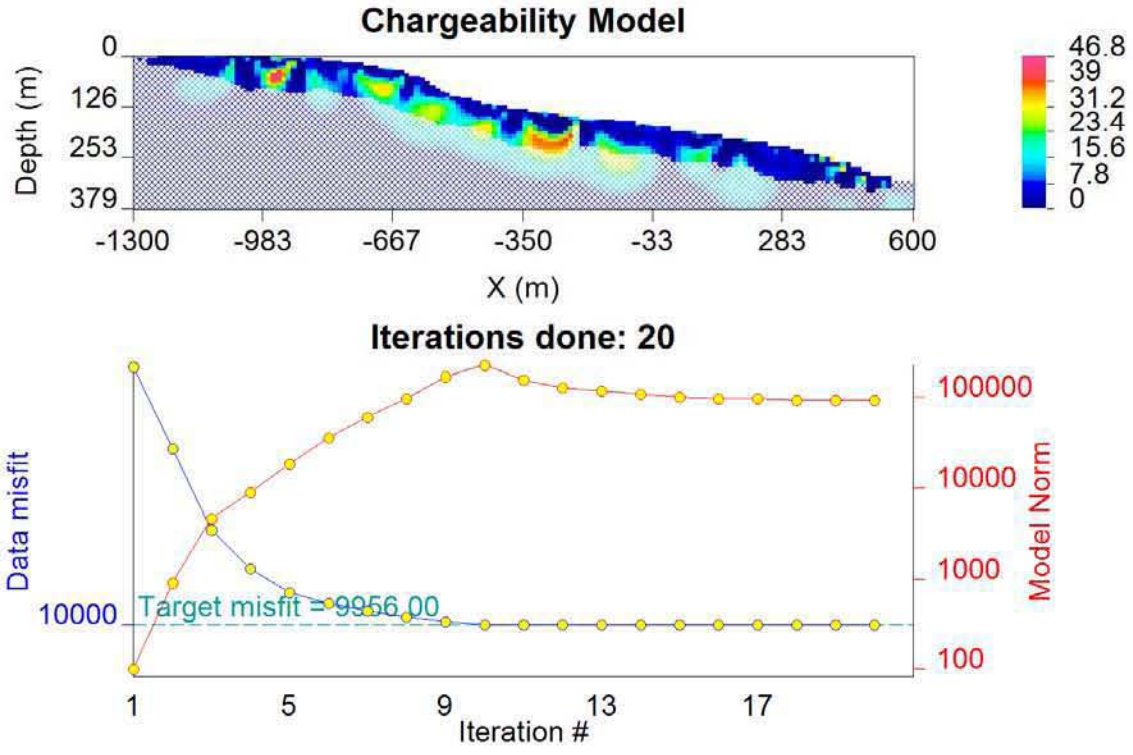

Sheelite Dome: Toby Zone; Line 1000 : Dipole-Dipole : 434 data
Observed Apparent Chargeability
27.5
22.92
18.33
13.75
9.167
4.583
0
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
27.5
22.92
18.33
13.75
9.167
4.583
0
-1300
-983
-667
-350
-33
283
600
X (m)

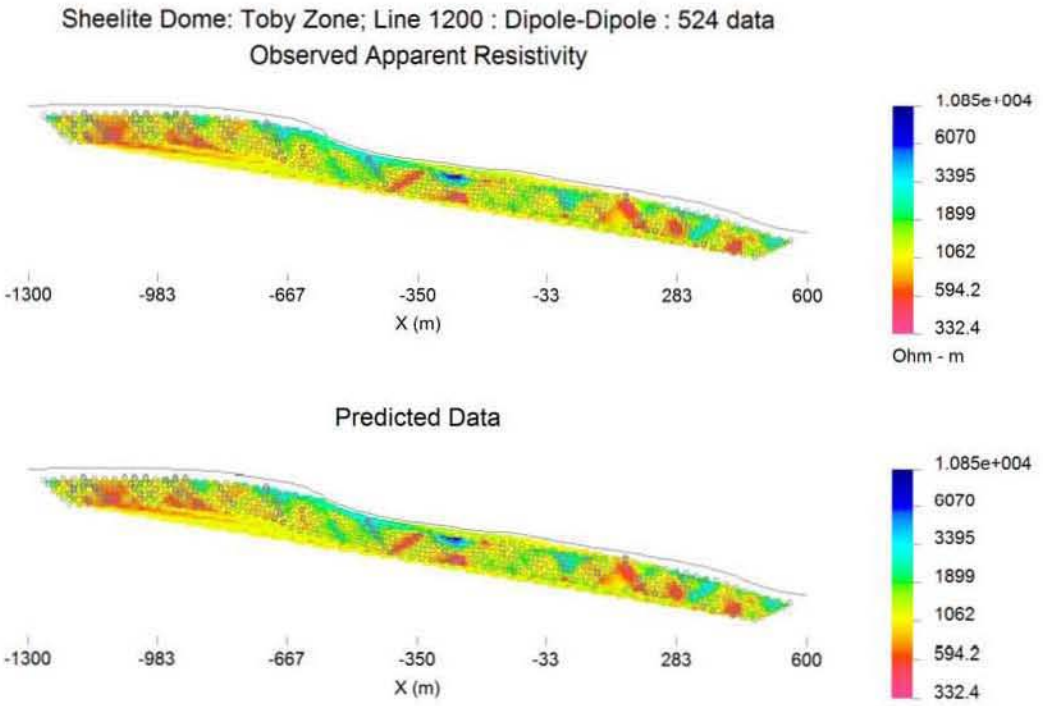

Chargeability Model
Depth (m)
0
151
301
452
-1300
-983
-667
-350
-33
283
600
X (m)
53.99
43.9
33.81
23.73
13.64
3.556
-6.53
Iterations done: 68
Data misfit
Target misfit = 17360.00
100000
10000
1000
100
Model Norm
1
14
27
40
53
66
Iteration #

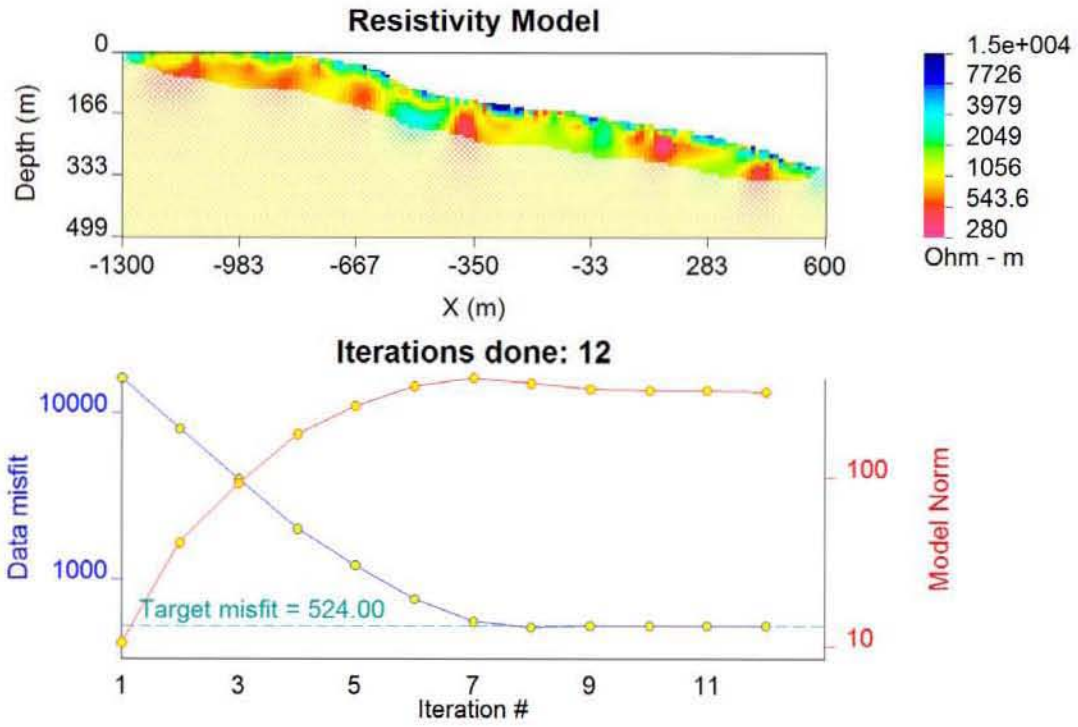

Sheelite Dome: Toby Zone; Line 1000 : Dipole-Dipole : 434 data
Observed Apparent Resistivity
9485
5613
3321
1966
1163
688.3
407.3
Ohm - m
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
9485
5613
3321
1966
1163
688.3
407.3
-1300
-983
-667
-350
-33
283
600
X (m)

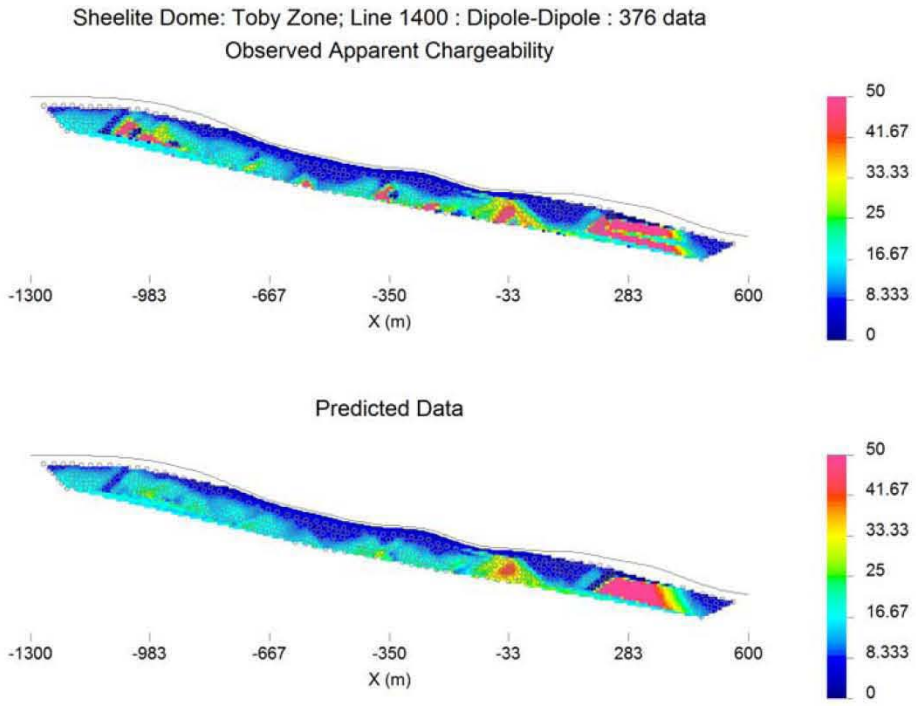

Resistivity Model
Depth (m)
0
115
231
346
-1300
-983
-667
-350
-33
283
600
X (m)
1.976e+004
9834
4893
2435
1211
602.7
299.9
Ohm - m
Iterations done: 10
Data misfit
10000
1000
Target misfit = 434.00
100
10
Model Norm
1
3
5
7
9
Iteration #

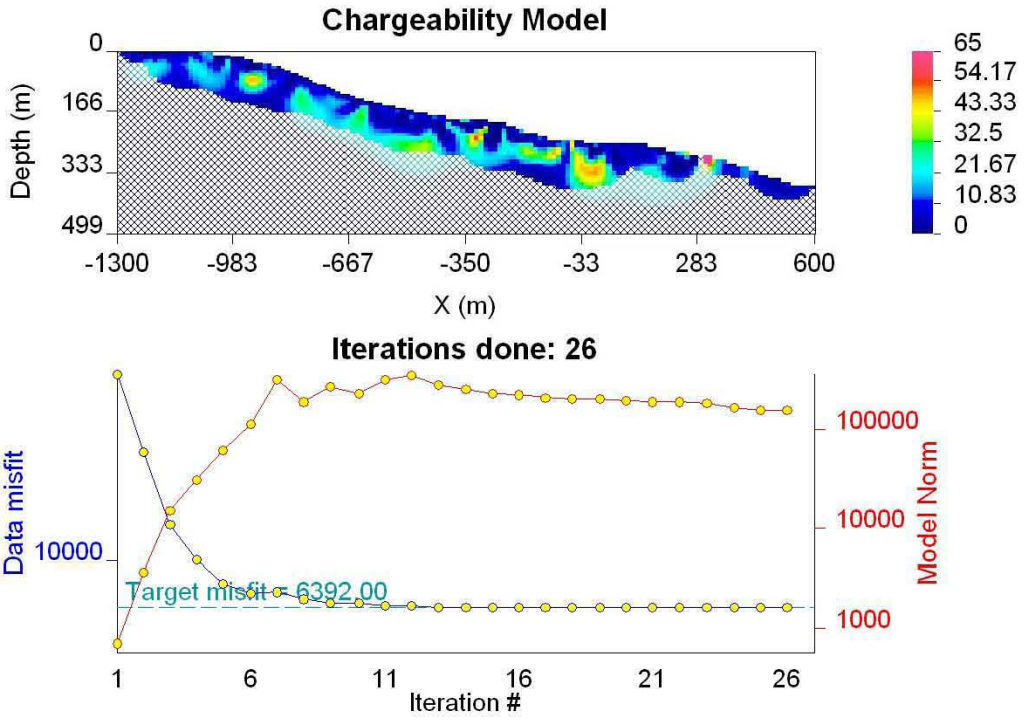

Sheelite Dome: Toby Zone; Line 1200 : Dipole-Dipole : 524 data
Observed Apparent Chargeability
40.1
33.42
26.73
20.05
13.37
6.683
0
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
40.1
33.42
26.73
20.05
13.37
6.683
0
-1300
-983
-667
-350
-33
283
600
X (m)

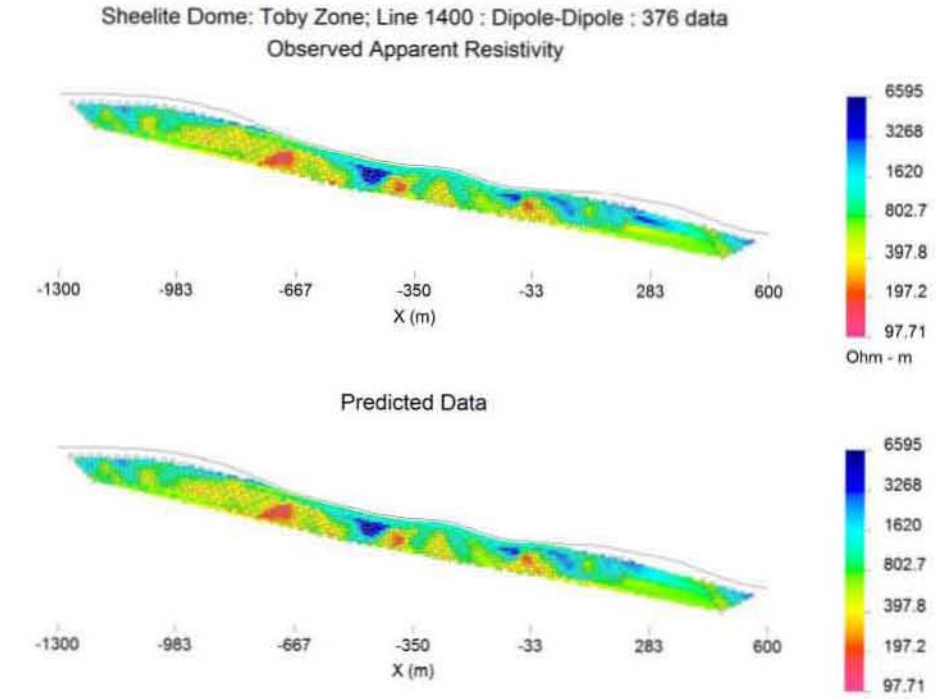

Chargeability Model
Depth (m)
0
126
253
379
-1300
-983
-667
-350
-33
283
600
X (m)
46.8
39
31.2
23.4
15.6
7.8
0
Iterations done: 20
Data misfit
10000
Target misfit = 9956.00
100000
10000
1000
100
Model Norm
1
5
9
13
17
Iteration #

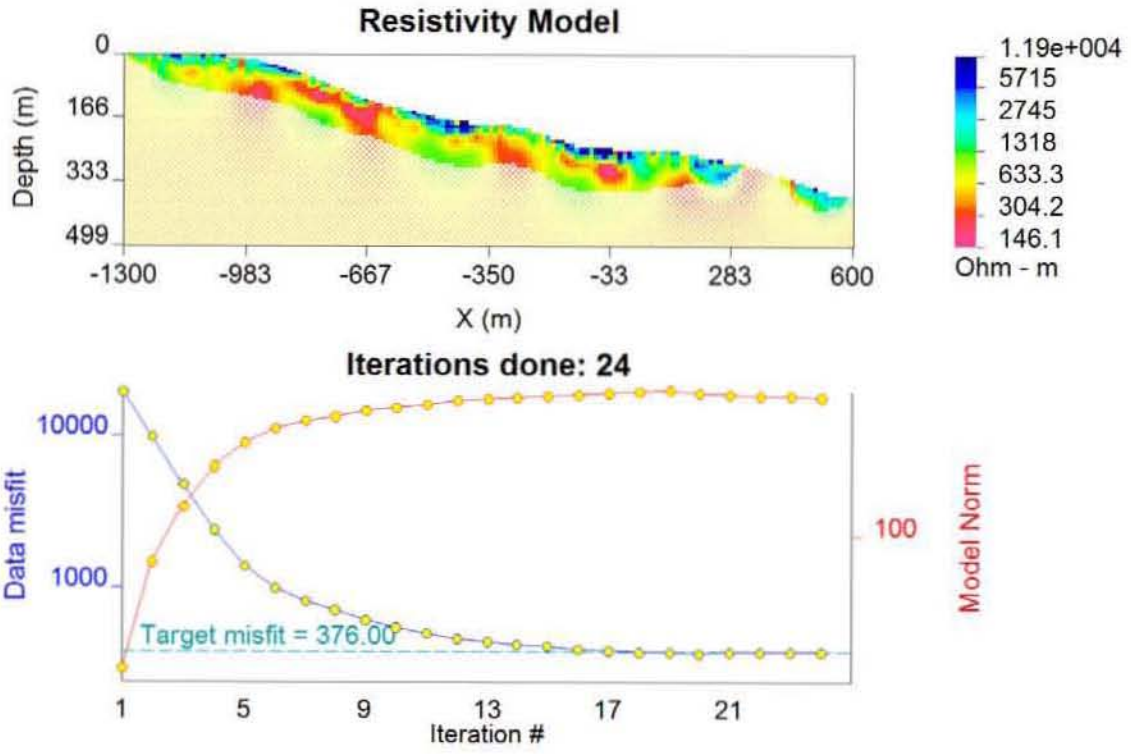

Sheelite Dome: Toby Zone; Line 1200 : Dipole-Dipole : 524 data
Observed Apparent Resistivity
1.085e+004
6070
3395
1899
1062
594.2
332.4
Ohm - m
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
1.085e+004
6070
3395
1899
1062
594.2
332.4
-1300
-983
-667
-350
-33
283
600
X (m)

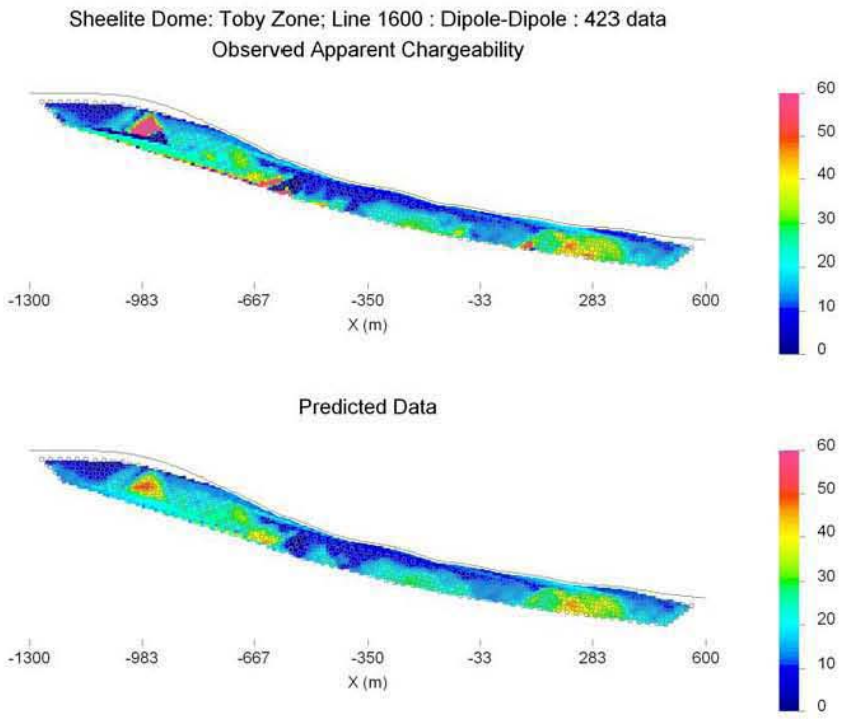

Resistivity Model
Depth (m)
0
166
333
499
-1300
-983
-667
-350
-33
283
600
X (m)
1.5e+004
7726
3979
2049
1056
543.6
280
Ohm - m
Iterations done: 12
Data misfit
10000
1000
Target misfit = 524.00
Model Norm
100
10
1
3
5
7
9
11
Iteration #

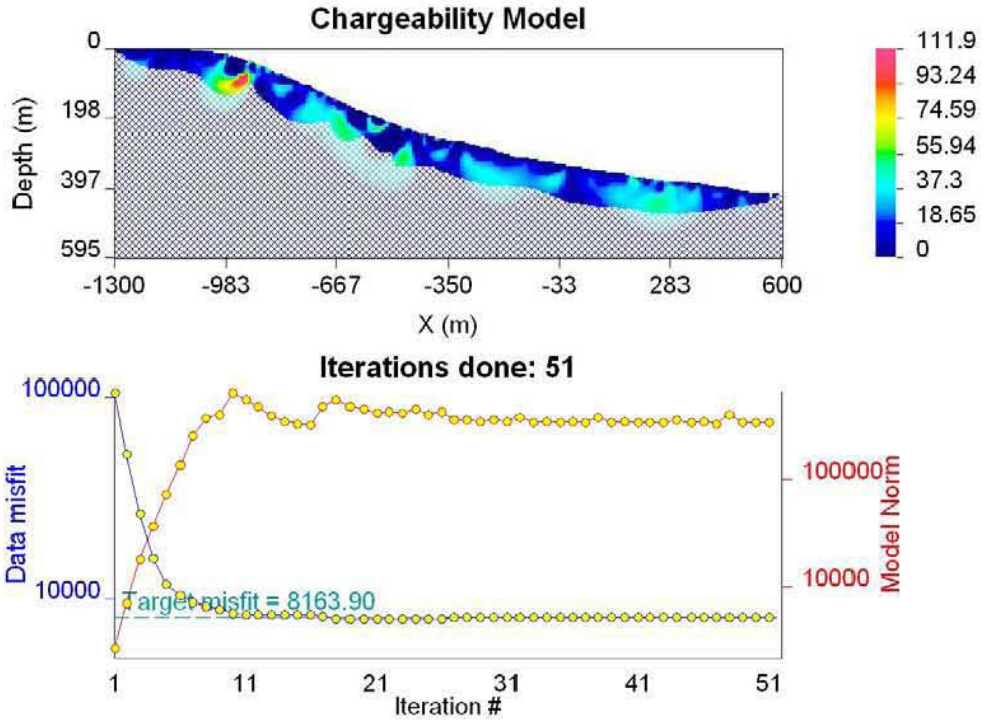

Sheelite Dome: Toby Zone; Line 1400 : Dipole-Dipole : 376 data
Observed Apparent Chargeability
50
41.67
33.33
25
16.67
8.333
0
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
50
41.67
33.33
25
16.67
8.333
0
-1300
-983
-667
-350
-33
283
600
X (m)

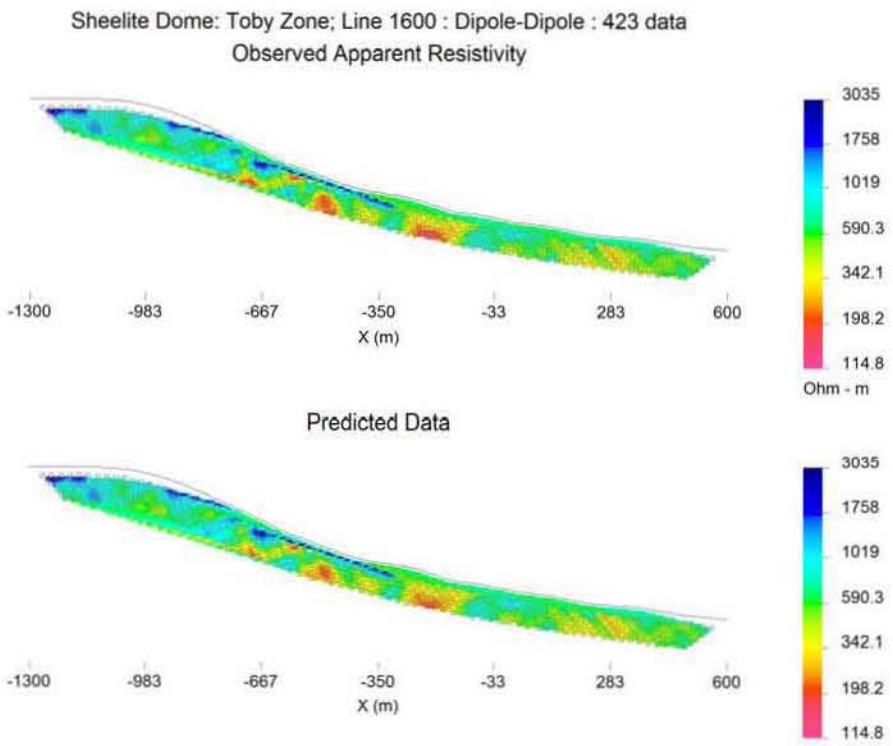

Chargeability Model
Depth (m)
0
166
333
499
-1300
-983
-667
-350
-33
283
600
X (m)
65
54.17
43.33
32.5
21.67
10.83
0
Iterations done: 26
Data misfit
10000
Target misfit = 6392.00
100000
10000
1000
Model Norm
1
6
11
16
21
26
Iteration #

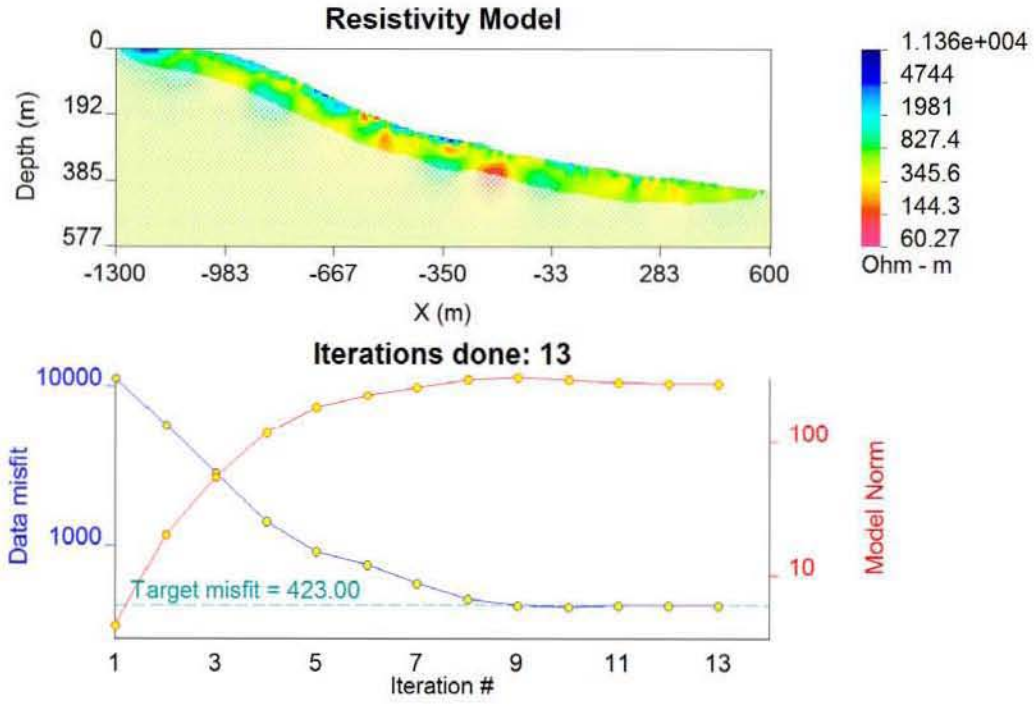

Sheelite Dome: Toby Zone; Line 1400 : Dipole-Dipole : 376 data
Observed Apparent Resistivity
6595
3268
1620
802.7
397.8
197.2
97.71
Ohm - m
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
6595
3268
1620
802.7
397.8
197.2
97.71
-1300
-983
-667
-350
-33
283
600
X (m)

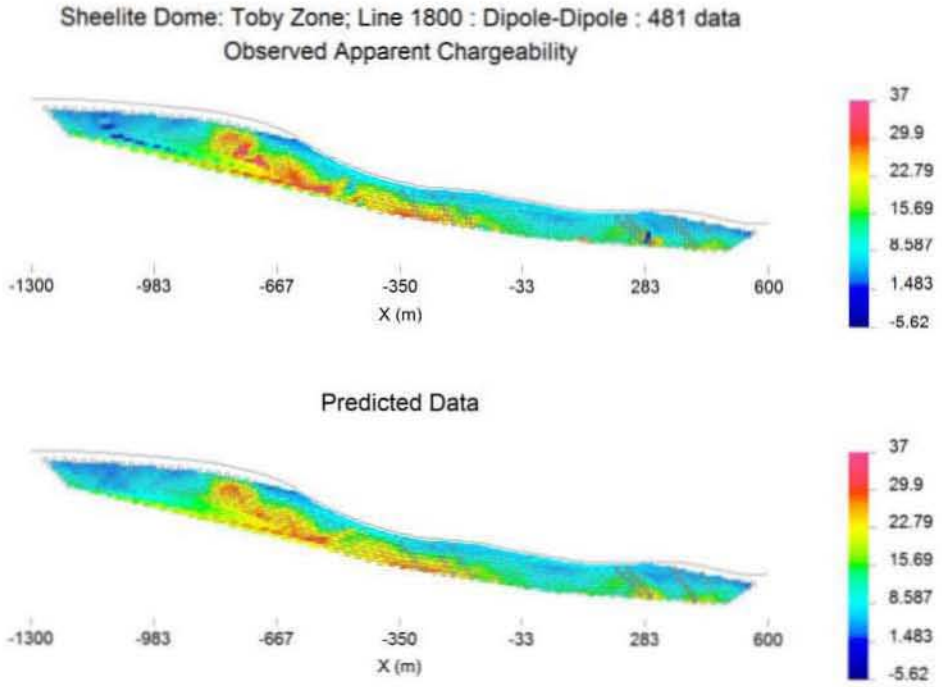

Resistivity Model
Depth (m)
0
166
333
499
-1300
-983
-667
-350
-33
283
600
X (m)
1.19e+004
5715
2745
1318
633.3
304.2
146.1
Ohm - m
Iterations done: 24
Data misfit
10000
1000
Target misfit = 376.00
100
Model Norm
1
5
9
13
17
21
Iteration #

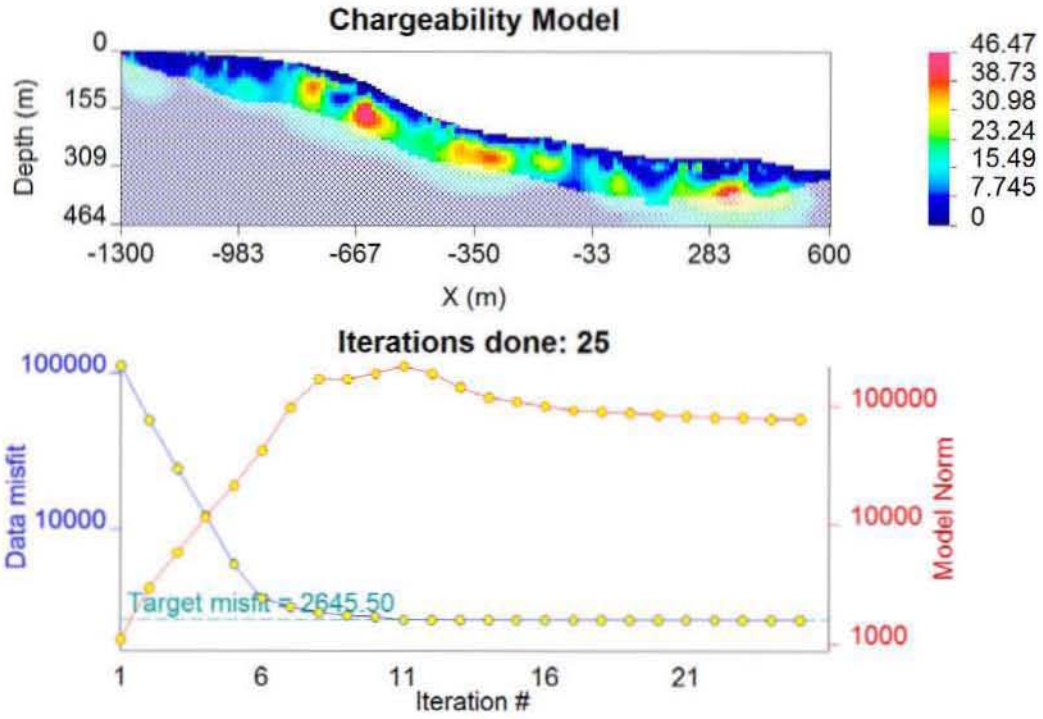

Sheelite Dome: Toby Zone; Line 1600 : Dipole-Dipole : 423 data
Observed Apparent Chargeability
60
50
40
30
20
10
0
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
60
50
40
30
20
10
0
-1300
-983
-667
-350
-33
283
600
X (m)

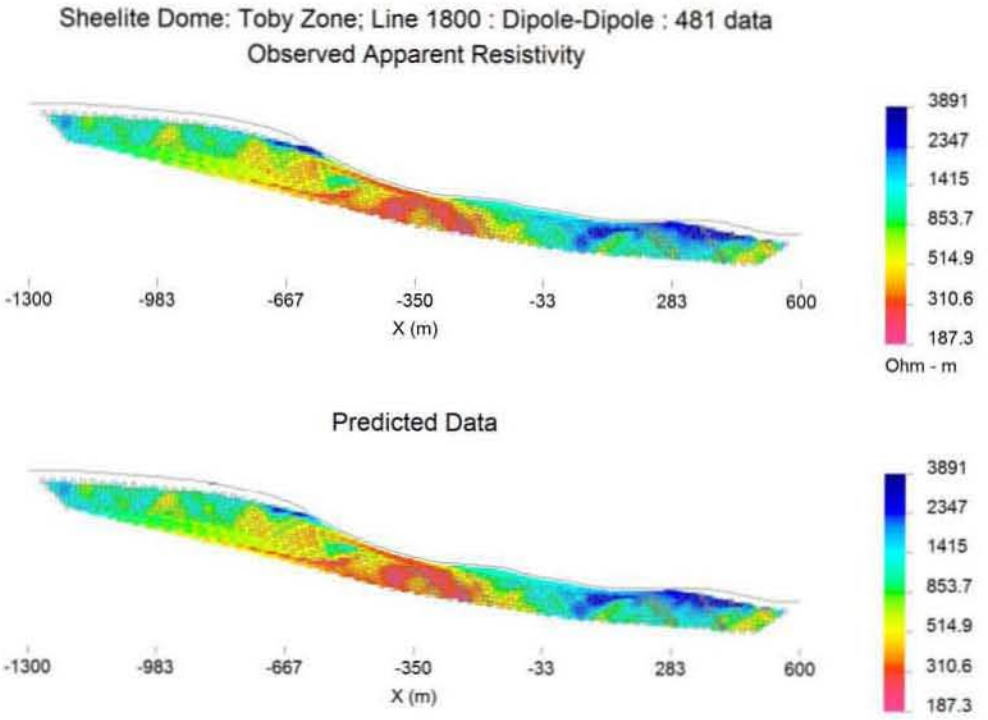

Chargeability Model
Depth (m)
0
198
397
595
-1300
-983
-667
-350
-33
283
600
X (m)
111.9
93.24
74.59
55.94
37.3
18.65
0
Iterations done: 51
Data misfit
100000
10000
Target misfit = 8163.90
Model Norm
100000
10000
1
11
21
31
41
51
Iteration #

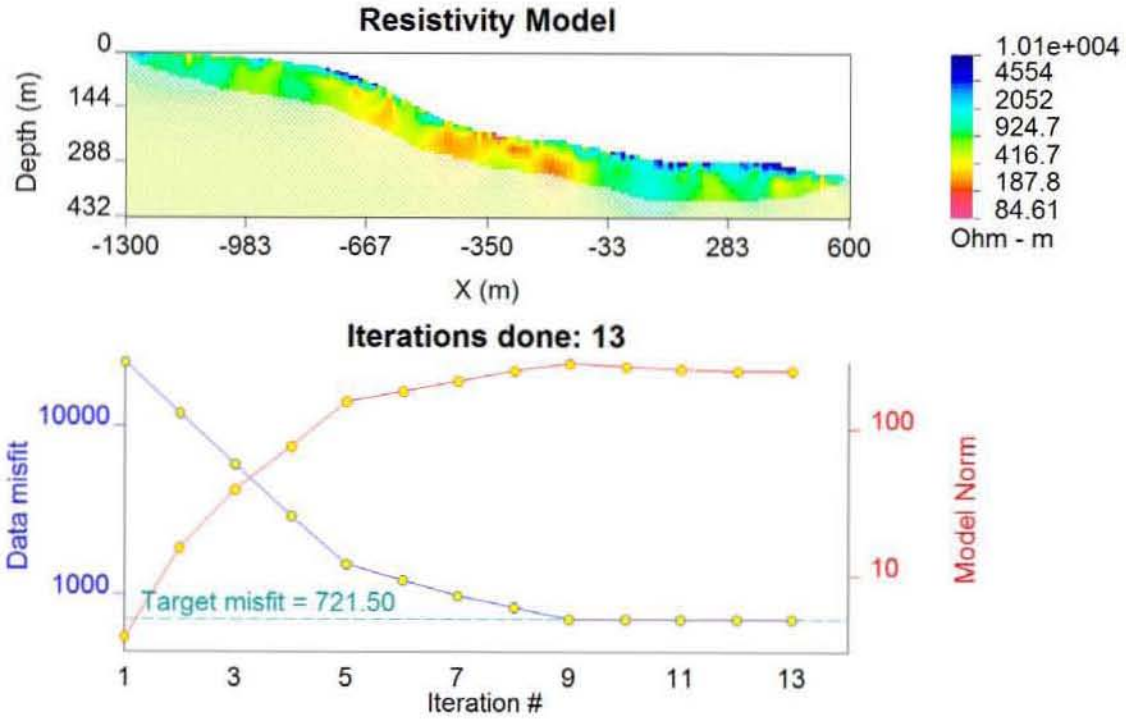

Sheelite Dome: Toby Zone; Line 1600 : Dipole-Dipole : 423 data
Observed Apparent Resistivity
3035
1758
1019
590.3
342.1
198.2
114.8
Ohm - m
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
3035
1758
1019
590.3
342.1
198.2
114.8
-1300
-983
-667
-350
-33
283
600
X (m)

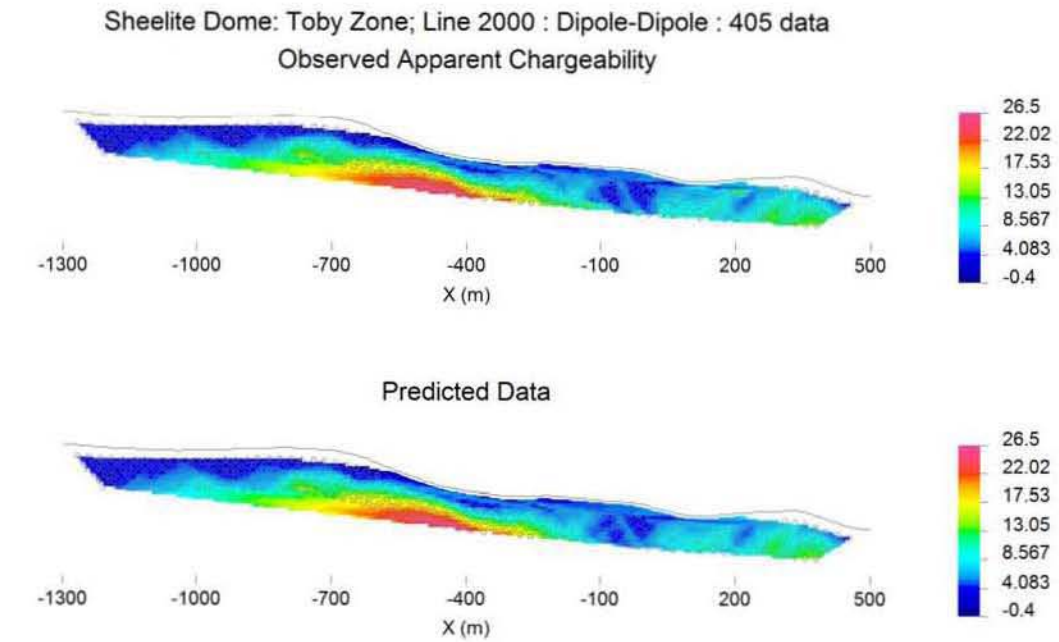

Resistivity Model
Depth (m)
0
192
385
577
-1300
-983
-667
-350
-33
283
600
X (m)
1.136e+004
4744
1981
827.4
345.6
144.3
60.27
Ohm - m
Iterations done: 13
Data misfit
10000
1000
Target misfit = 423.00
100
10
Model Norm
1
3
5
7
9
11
13
Iteration #

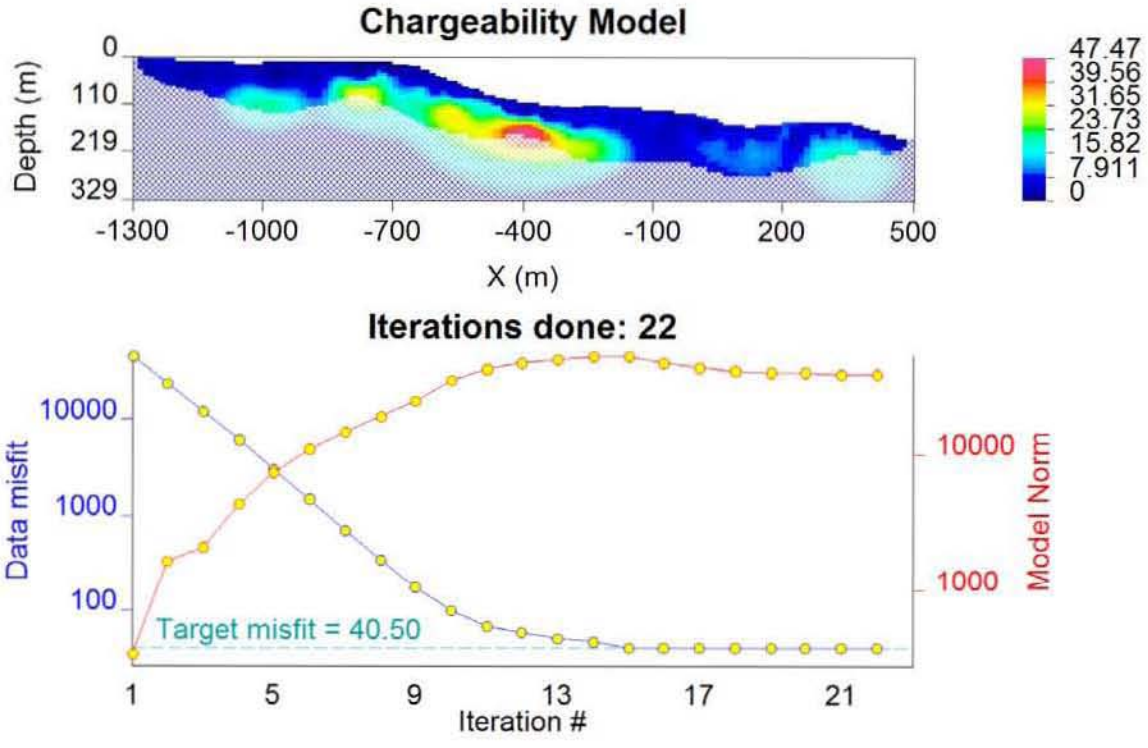

Sheelite Dome: Toby Zone; Line 1800 : Dipole-Dipole : 481 data
Observed Apparent Chargeability
37
29.9
22.79
15.69
8.587
1.483
-5.62
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
37
29.9
22.79
15.69
8.587
1.483
-5.62
-1300
-983
-667
-350
-33
283
600
X (m)

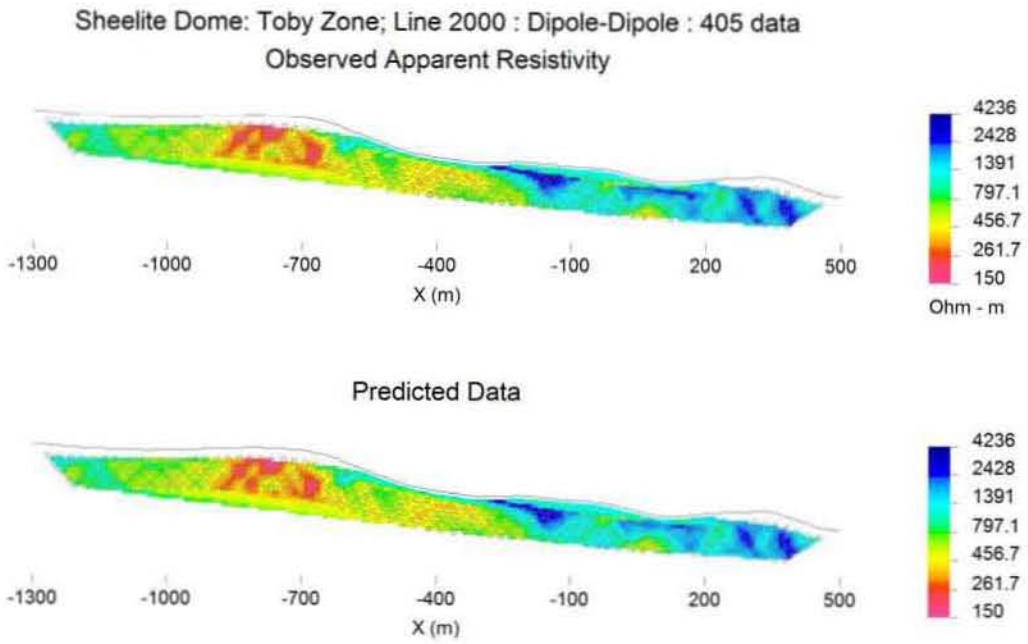

Chargeability Model
Depth (m)
0
155
309
464
46.47
38.73
30.98
23.24
15.49
7.745
0
-1300
-983
-667
-350
-33
283
600
X (m)
Iterations done: 25
Data misfit
100000
10000
Target misfit = 2645.50
Model Norm
100000
10000
1000
1
6
11
16
21
Iteration #

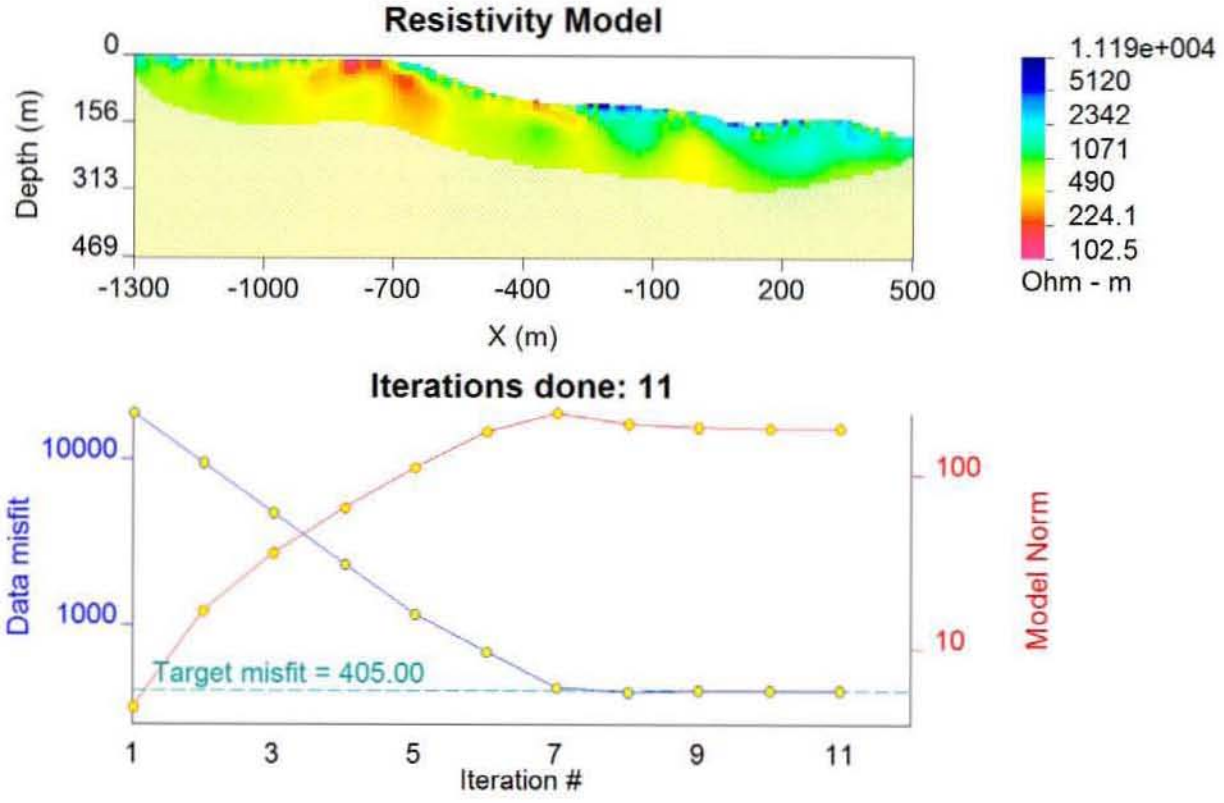

Sheelite Dome: Toby Zone; Line 1800 : Dipole-Dipole : 481 data
Observed Apparent Resistivity
3891
2347
1415
853.7
514.9
310.6
187.3
Ohm - m
-1300
-983
-667
-350
-33
283
600
X (m)
Predicted Data
3891
2347
1415
853.7
514.9
310.6
187.3
-1300
-983
-667
-350
-33
283
600
X (m)

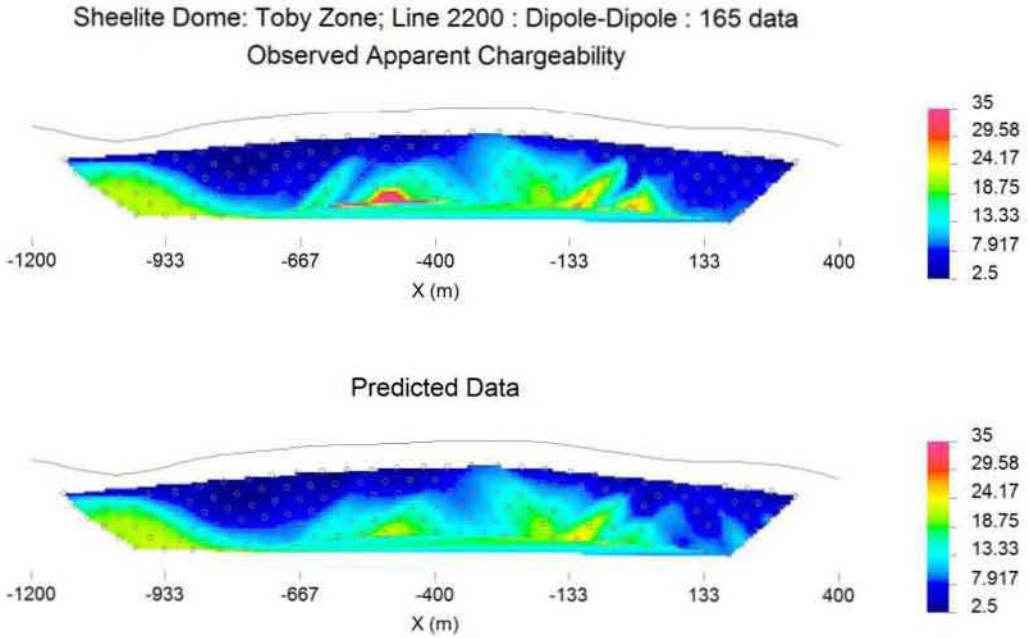

Resistivity Model
Depth (m)
0
144
288
432
-1300
-983
-667
-350
-33
283
600
X (m)
1.01e+004
4554
2052
924.7
416.7
187.8
84.61
Ohm - m
Iterations done: 13
Data misfit
10000
1000
Target misfit = 721.50
100
10
Model Norm
1
3
5
7
9
11
13
Iteration #

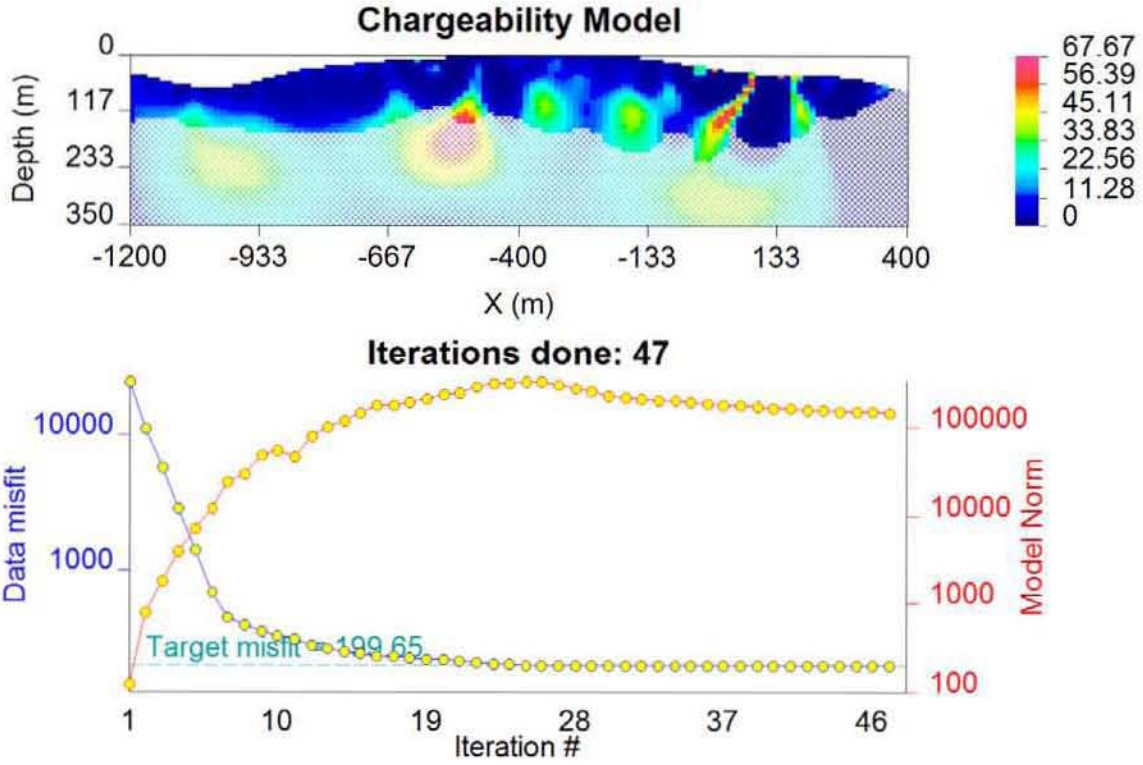

Sheelite Dome: Toby Zone; Line 2000 : Dipole-Dipole : 405 data
Observed Apparent Chargeability
26.5
22.02
17.53
13.05
8.567
4.083
-0.4
-1300
-1000
-700
-400
-100
200
500
X (m)
Predicted Data
26.5
22.02
17.53
13.05
8.567
4.083
-0.4
-1300
-1000
-700
-400
-100
200
500
X (m)

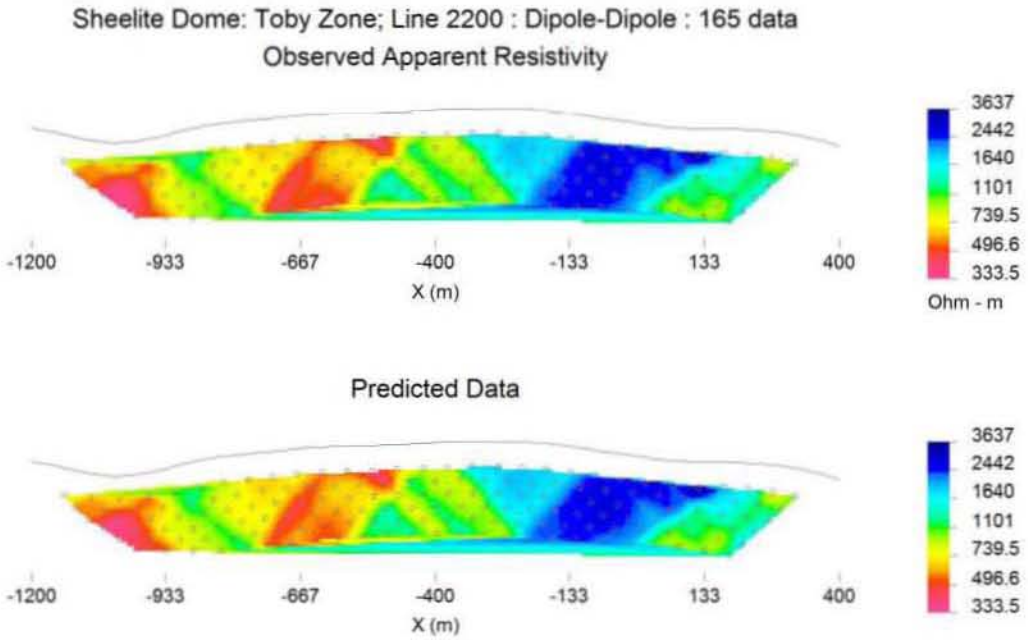

Chargeability Model
Depth (m)
0
110
219
329
47.47
39.56
31.65
23.73
15.82
7.911
0
-1300
-1000
-700
-400
-100
200
500
X (m)
Iterations done: 22
Data misfit
10000
1000
100
Target misfit = 40.50
10000
1000
Model Norm
1
5
9
13
17
21
Iteration #

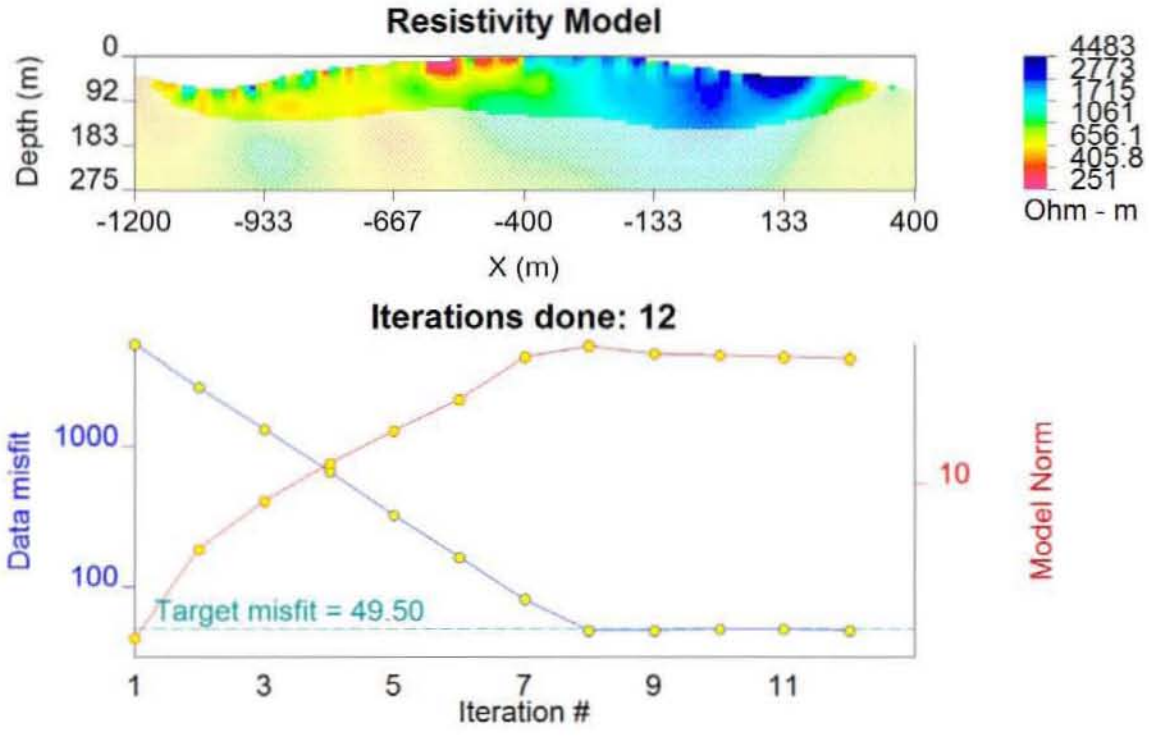

Sheelite Dome: Toby Zone; Line 2000 : Dipole-Dipole : 405 data
Observed Apparent Resistivity
4236
2428
1391
797.1
456.7
261.7
150
Ohm - m
-1300
-1000
-700
-400
-100
200
500
X (m)
Predicted Data
4236
2428
1391
797.1
456.7
261.7
150
-1300
-1000
-700
-400
-100
200
500
X (m)

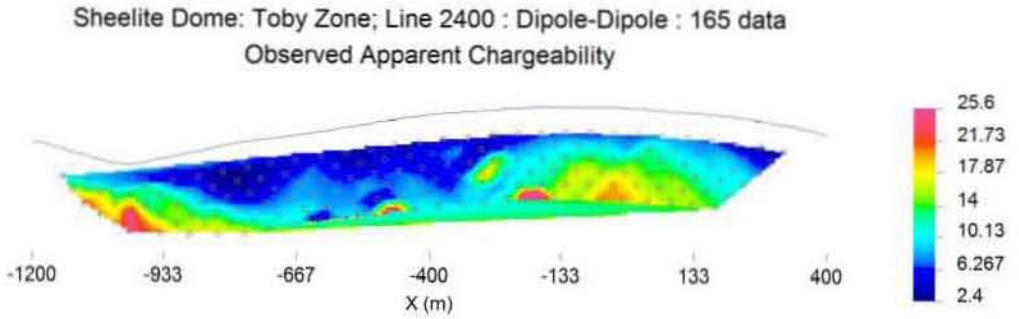

Resistivity Model
Depth (m)
0
156
313
469
-1300
-1000
-700
-400
-100
200
500
X (m)
1.119e+004
5120
2342
1071
490
224.1
102.5
Ohm - m
Iterations done: 11
Data misfit
10000
1000
Target misfit = 405.00
100
10
Model Norm
1
3
5
7
9
11
Iteration #

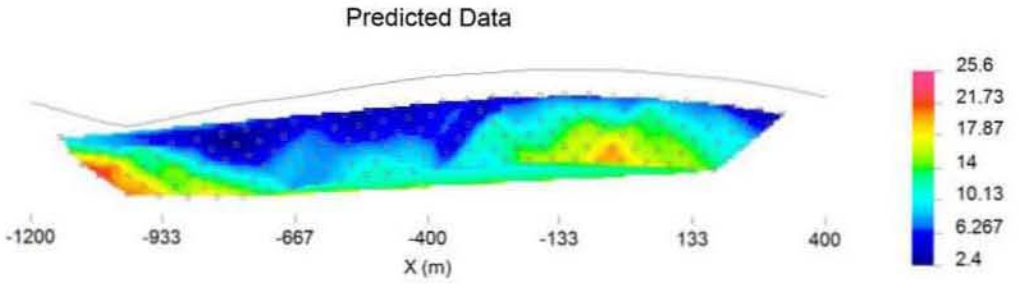

Sheelite Dome: Toby Zone; Line 2200 : Dipole-Dipole : 165 data
Observed Apparent Chargeability
35
29.58
24.17
18.75
13.33
7.917
2.5
-1200
-933
-667
-400
-133
133
400
X (m)
Predicted Data
35
29.58
24.17
18.75
13.33
7.917
2.5
-1200
-933
-667
-400
-133
133
400
X (m)

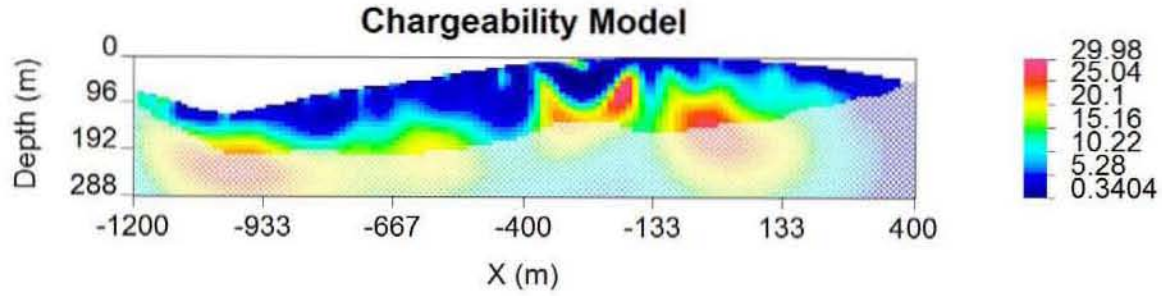

Chargeability Model
Depth (m)
0
117
233
350
-1200
-933
-667
-400
-133
133
400
X (m)
67.67
56.39
45.11
33.83
22.56
11.28
0
Iterations done: 47
Data misfit
10000
1000
Target misfit = 199.65
100000
10000
1000
100
Model Norm
1
10
19
28
37
46
Iteration #

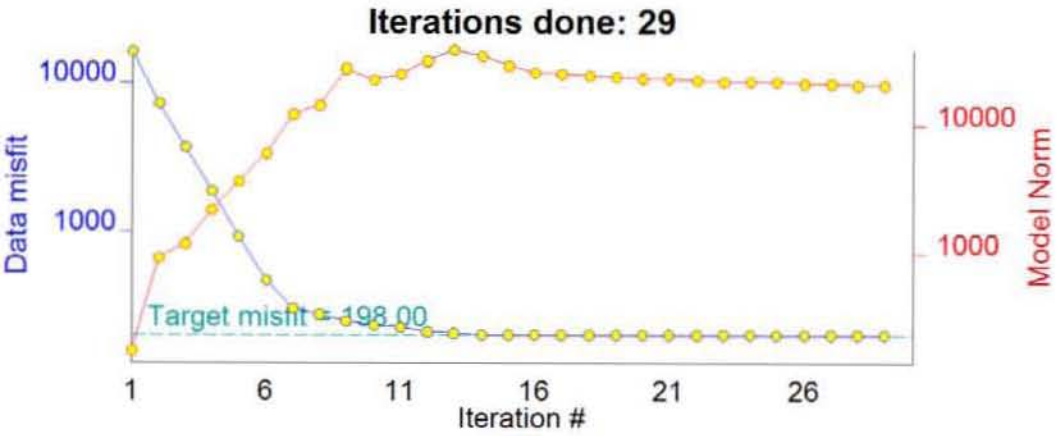

Sheelite Dome: Toby Zone; Line 2200 : Dipole-Dipole : 165 data
Observed Apparent Resistivity
3637
2442
1640
1101
739.5
496.6
333.5
Ohm - m
-1200
-933
-667
-400
-133
133
400
X (m)
Predicted Data
3637
2442
1640
1101
739.5
496.6
333.5
-1200
-933
-667
-400
-133
133
400
X (m)

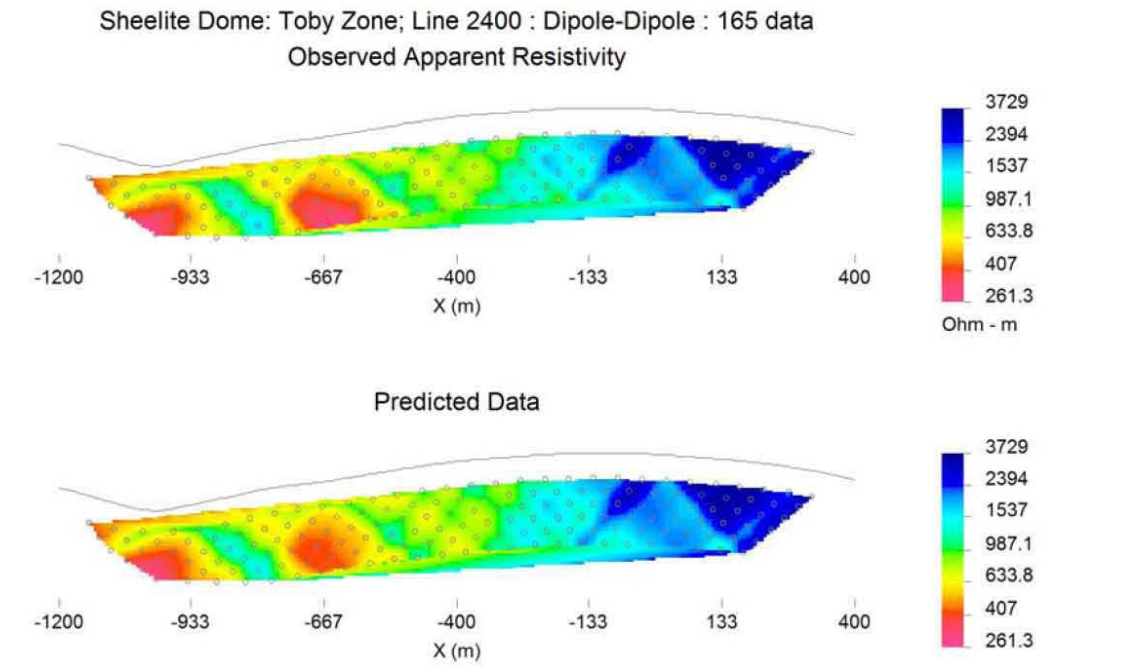

Resistivity Model
Depth (m)
0
92
183
275
-1200
-933
-667
-400
-133
133
400
X (m)
4483
2773
1715
1061
656.1
405.8
251
Ohm - m
Iterations done: 12
Data misfit
1000
100
Target misfit = 49.50
10
Model Norm
1
3
5
7
9
11
Iteration #

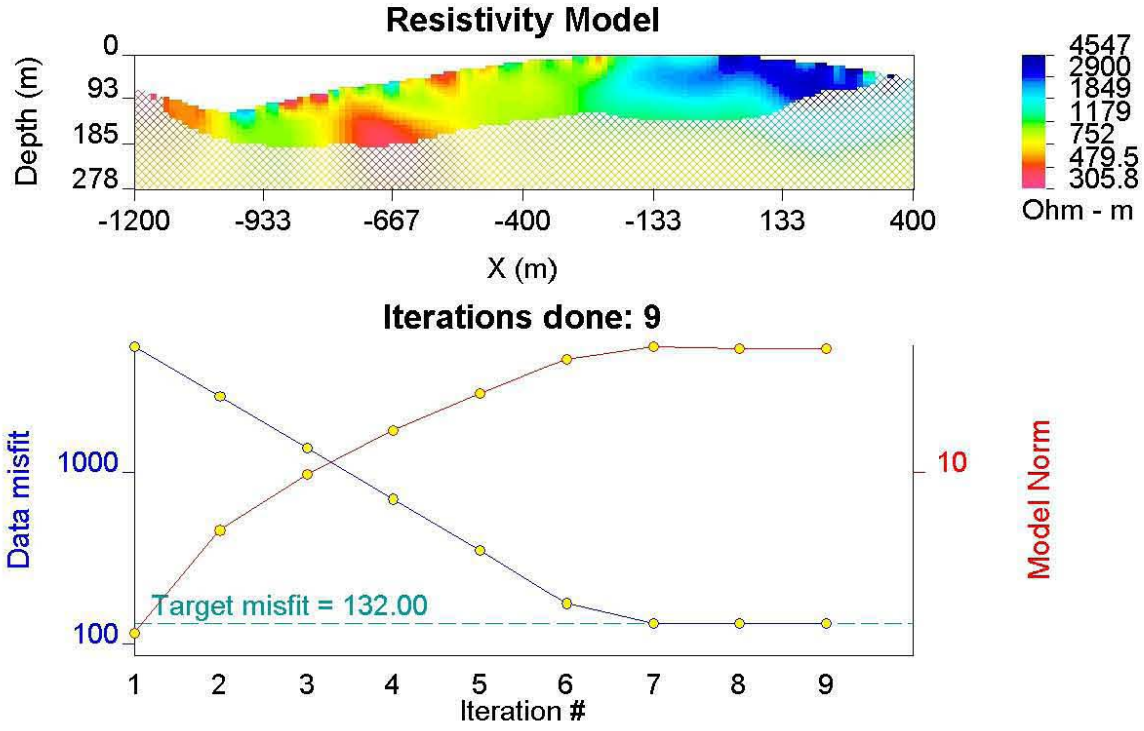

Sheelite Dome: Toby Zone; Line 2400 : Dipole-Dipole : 165 data
Observed Apparent Chargeability
25.6
21.73
17.87
14
10.13
6.267
2.4
-1200
-933
-667
-400
-133
133
400
X (m)

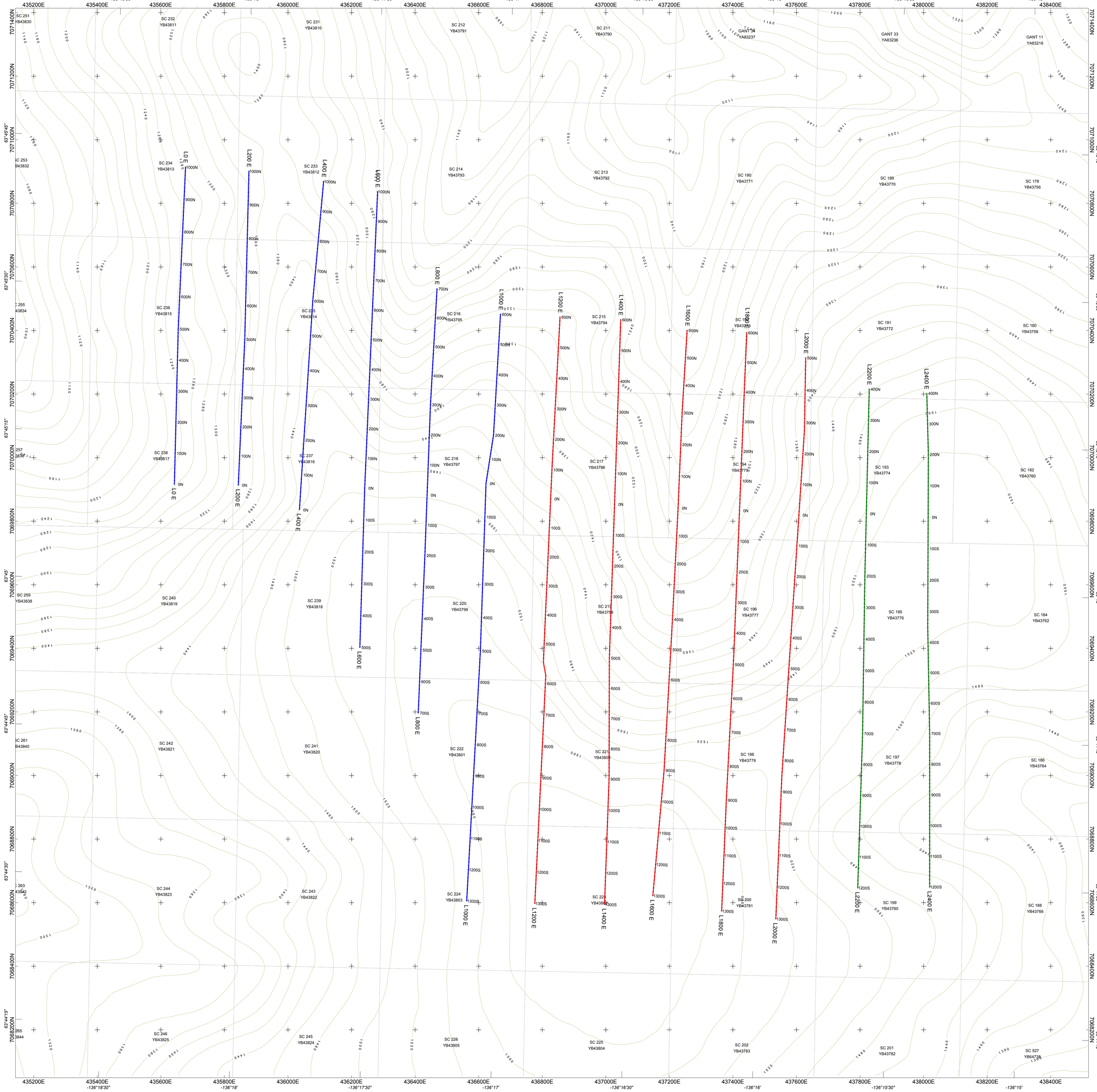

Predicted Data
25.6
21.73
17.87
14
10.13
6.267
2.4
-1200
-933
-667
-400
-133
133
400
X (m)


Chargeability Model
Depth (m)
0
96
192
288
29.98
25.04
20.1
15.16
10.22
5.28
0.3404
-1200
-933
-667
-400
-133
133
400
X (m)


Iterations done: 29
Data misfit
10000
1000
Target misfit = 198.00
10000
1000
Model Norm
1
6
11
16
21
26
Iteration #


Sheelite Dome: Toby Zone; Line 2400 : Dipole-Dipole : 165 data
Observed Apparent Resistivity
3729
2394
1537
987.1
633.8
407
261.3
Ohm - m
-1200
-933
-667
-400
-133
133
400
X (m)
Predicted Data
3729
2394
1537
987.1
633.8
407
261.3
-1200
-933
-667
-400
-133
133
400
X (m)


Resistivity Model
Depth (m)
0
93
185
278
-1200
-933
-667
-400
-133
133
400
X (m)
4547
2900
1849
1179
752
479.5
305.8
Ohm - m
Iterations done: 9
Data misfit
1000
100
Target misfit = 132.00
10
Model Norm
1
2
3
4
5
6
7
8
9
Iteration #



LEGEND

SURVEY SPECIFICATIONS

- Modified pole-dipole 25 m
- Dipole-dipole 25 m
- Dipole-dipole 50 m

Scale 1:5000

100 0 100 200 300

metres

NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.

GRID LOCATION MAP

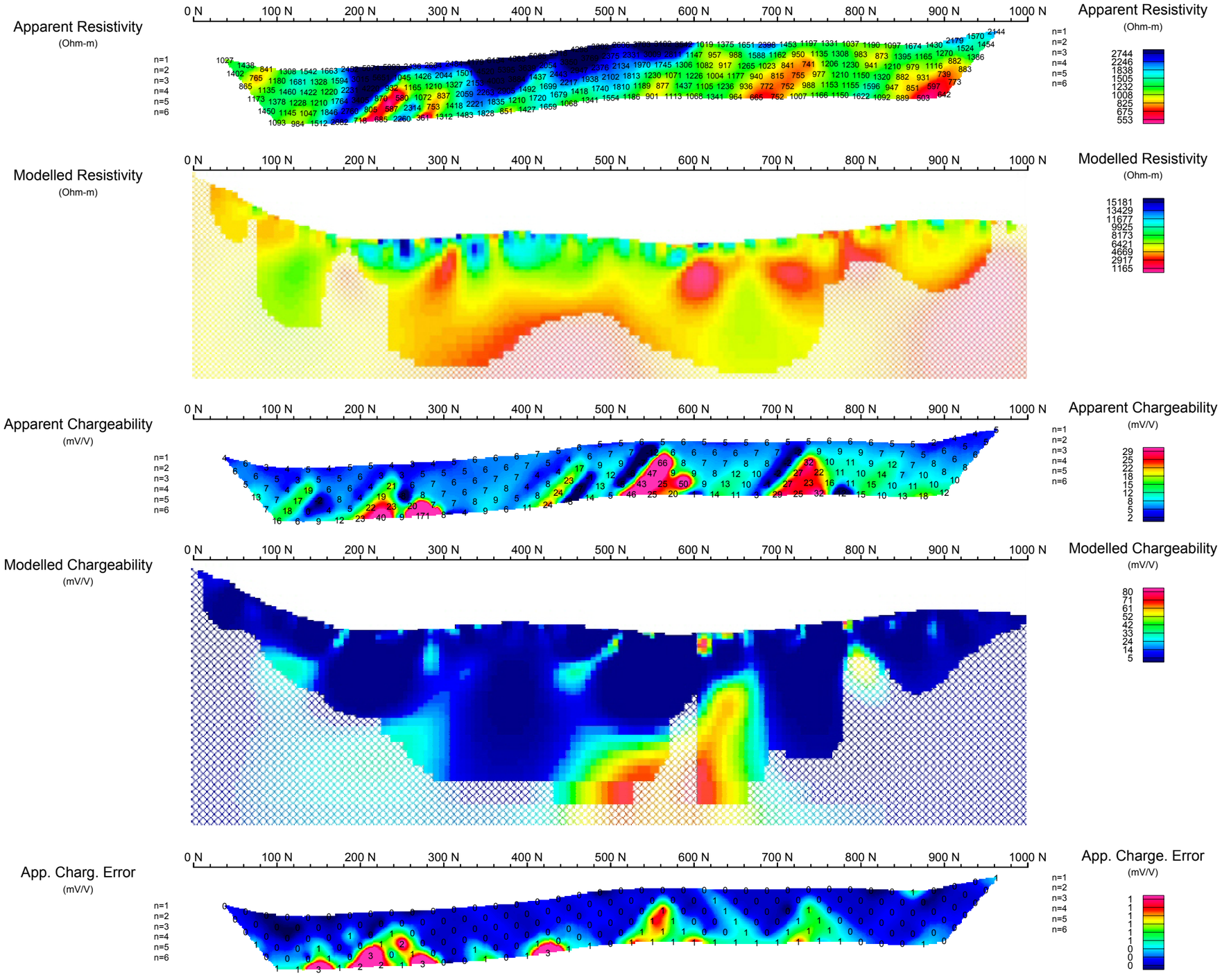
Scheelite Dome Property Toby Zone

NTS: 116 P/09 & P/16 — Mining District: Mayo

Grid: NAD 27 Canada - Zone 8 — Job: KRX-06-02-YT

Date: Jan 19, 2007 — Figure 2

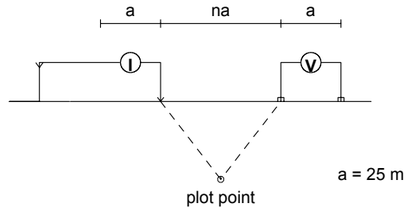
AURORA GEOSCIENCES LTD.



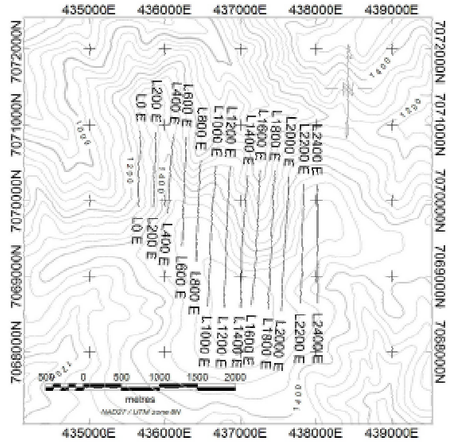
COMPOSITE SECTION PLOT

L0 E

Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 0N.



Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY

Sheelite Dome Property Toby Zone

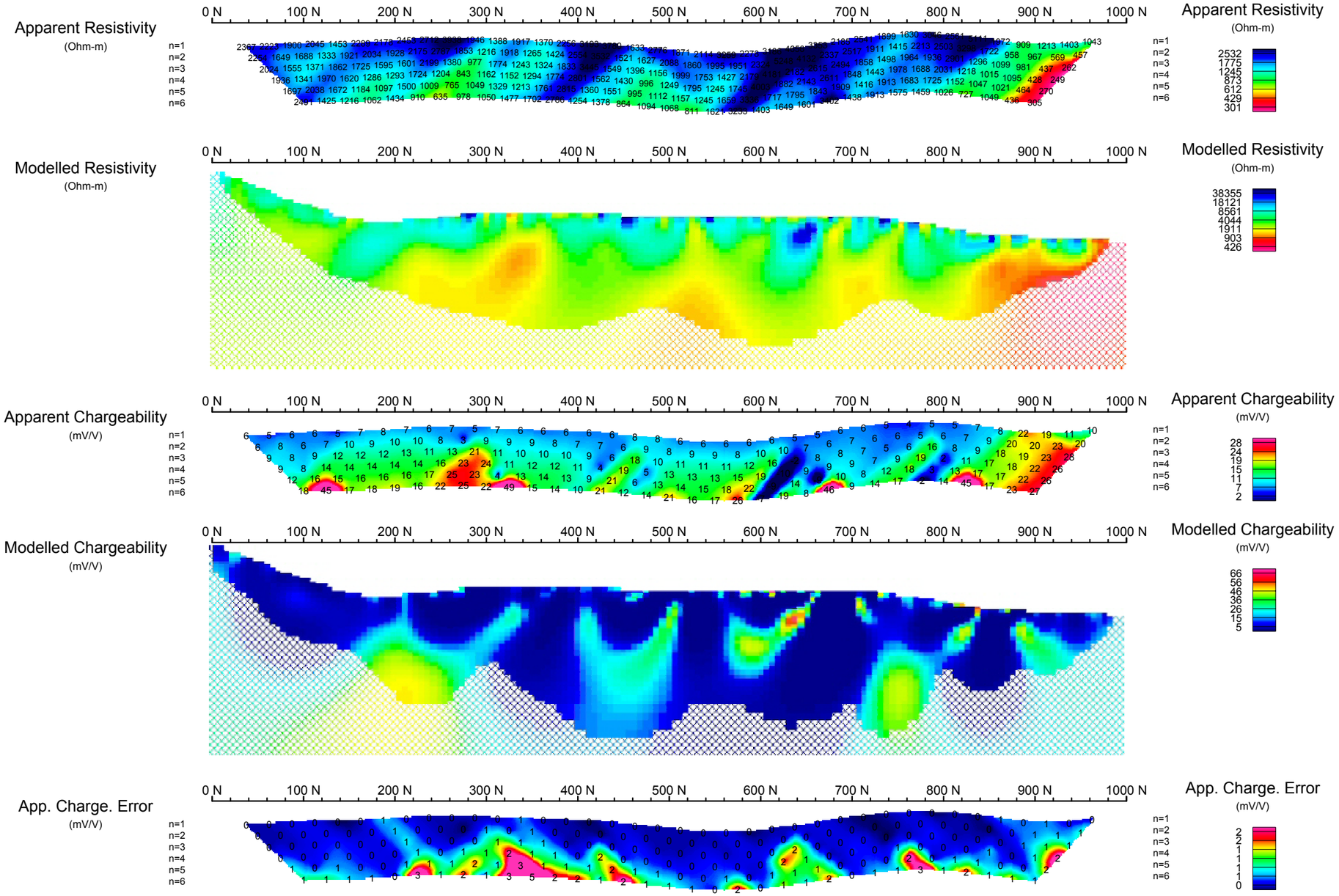
Composite Section L000E

NTS: 115 P/09 & P/16 — Mining District: Mayo

Grid: Local — Job: KRX-06-02-YT

Date: 14 Sept 06 — Appendix E

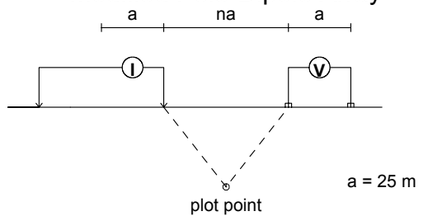
AURORA GEOSCIENCES LTD.



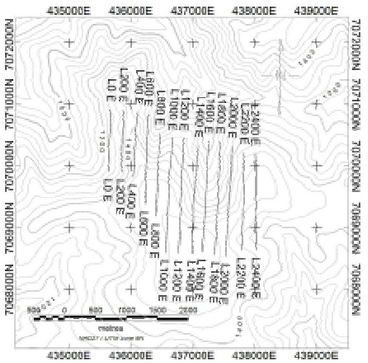
COMPOSITE SECTION PLOT

L200 E

Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 0N.



Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY

Sheelite Dome Property Toby Zone

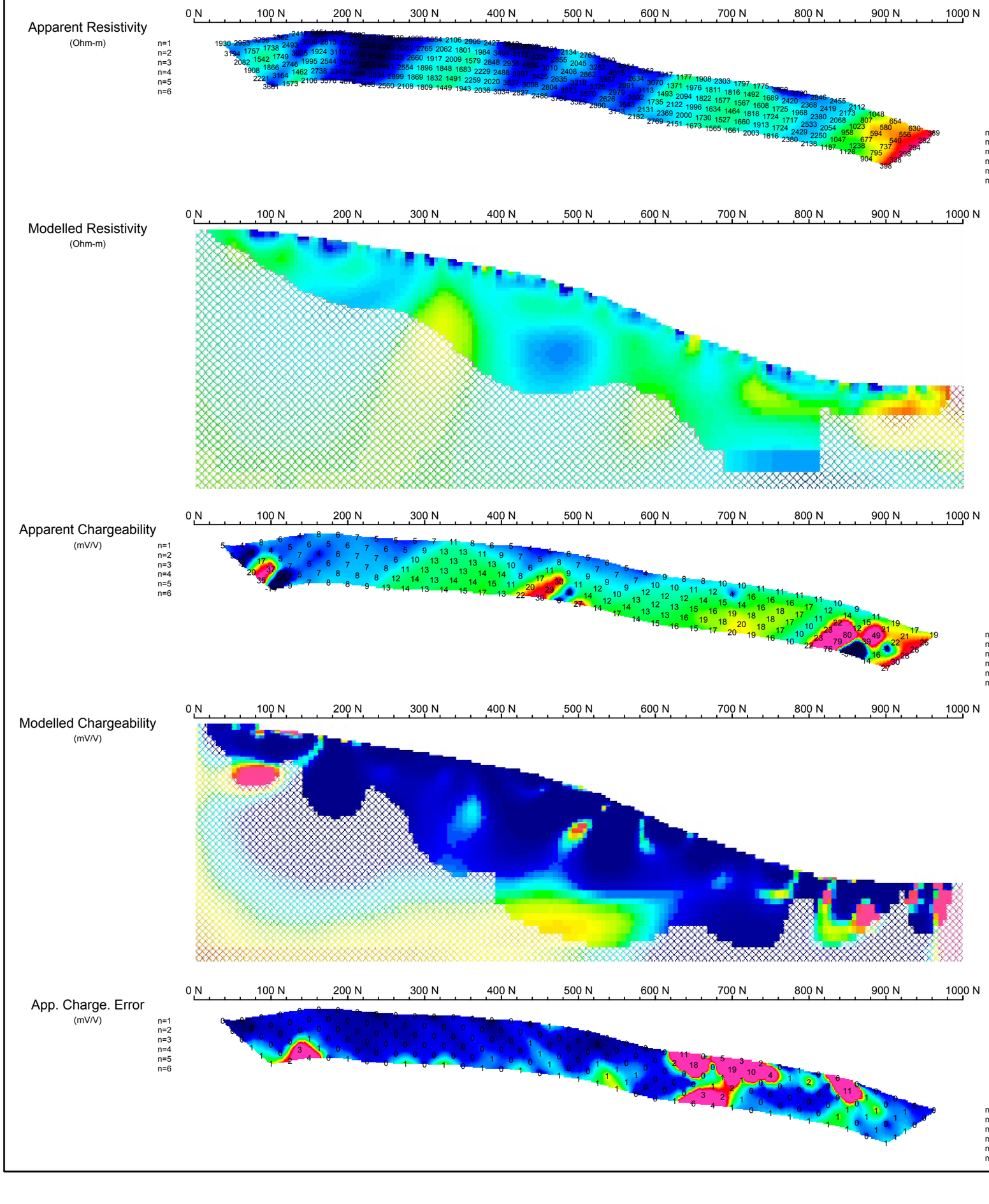
Composite Section L200E

NTS: 115 P/09 & P/16 — Mining District: Mayo

Grid: Local — Job: KRX-06-02-YT

Date: 14 Sept 06 — Appendix E

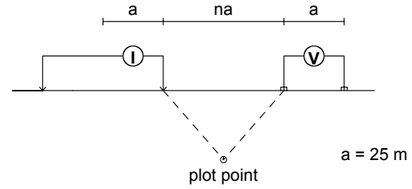
AURORA GEOSCIENCES LTD.



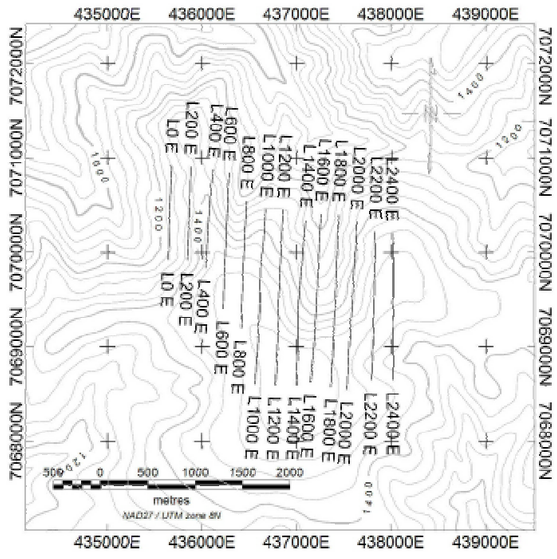
COMPOSITE SECTION PLOT

L400 E

Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 0N.



Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

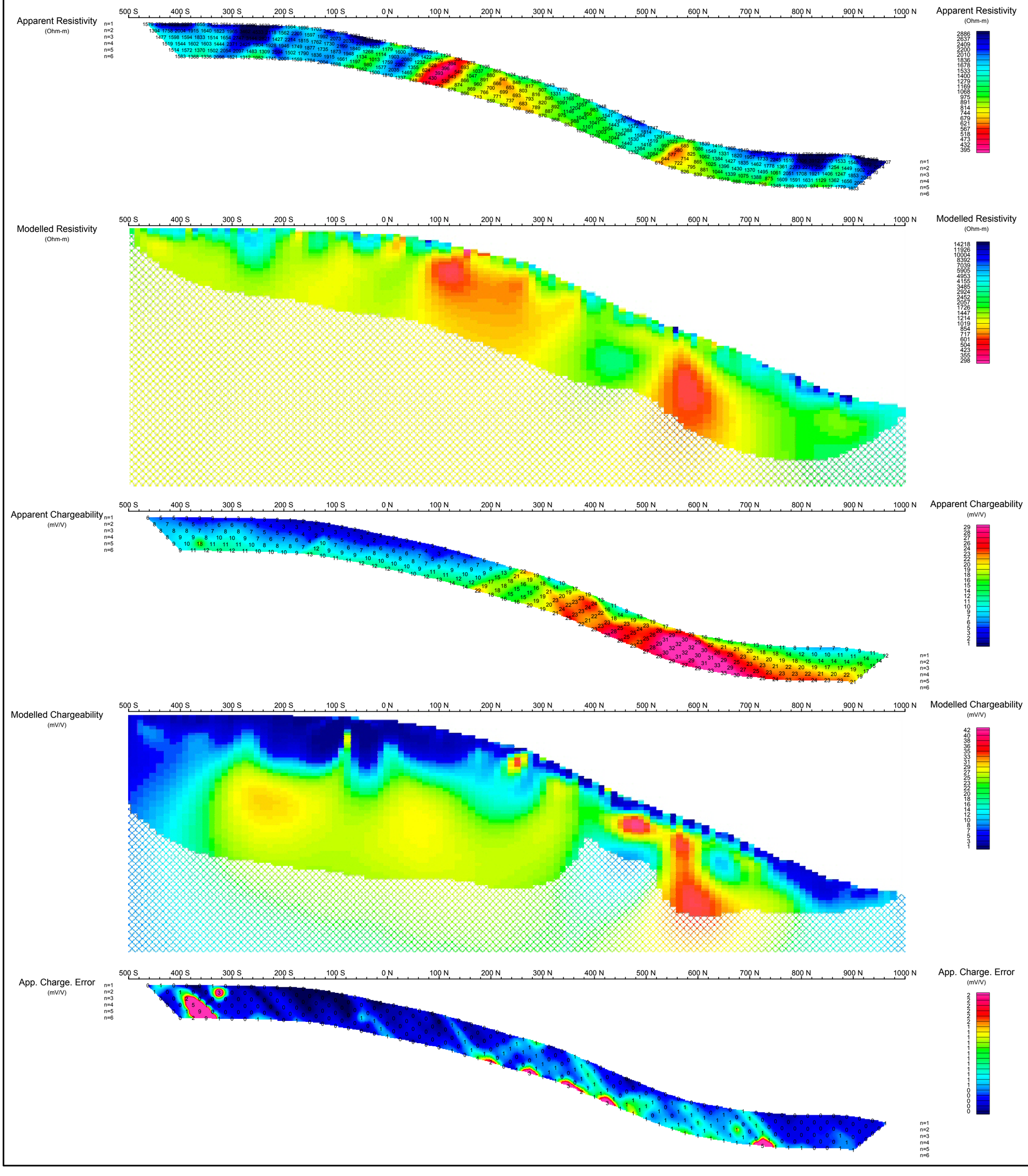
COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L400E

NTS: 115 P/09 & P/16
Grid: Local
Date: 14 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

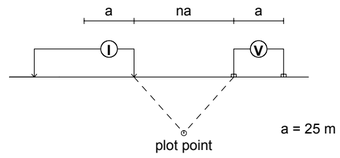
AURORA GEOSCIENCES LTD.



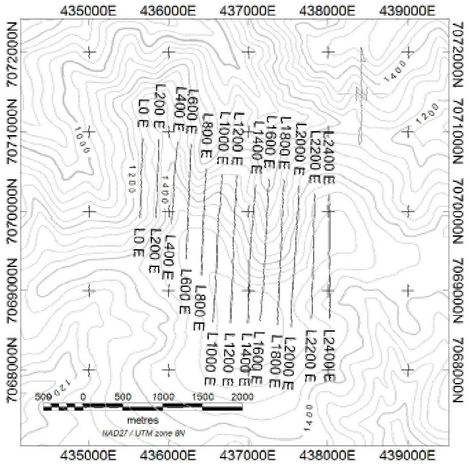
COMPOSITE SECTION PLOT

L600 E

Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 500S.



Scale 1:5000

50 0 50 100 150 200 250 300
metres

No vertical exaggeration.

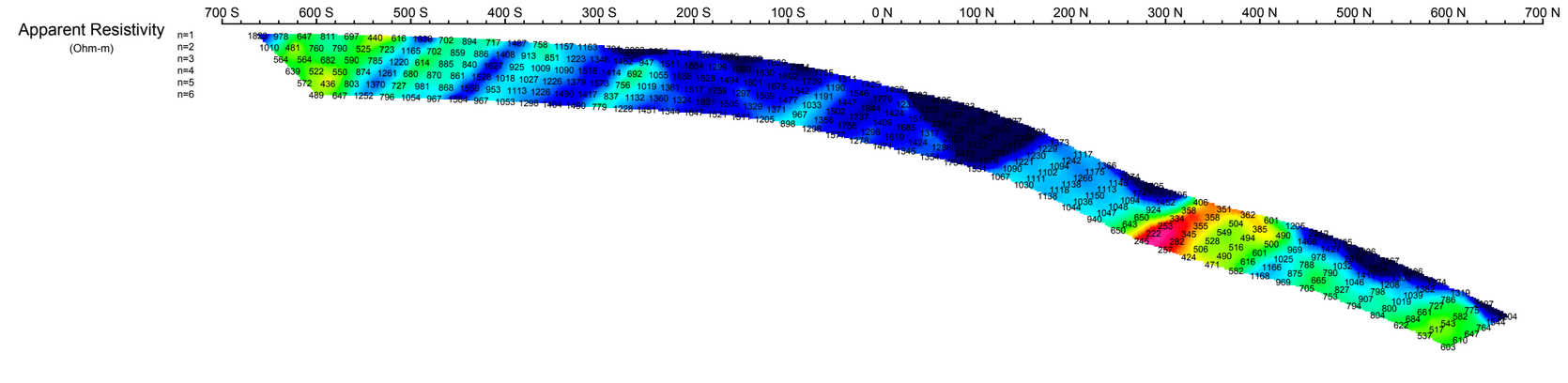
COPPER RIDGE EXPLORATIONS INC.

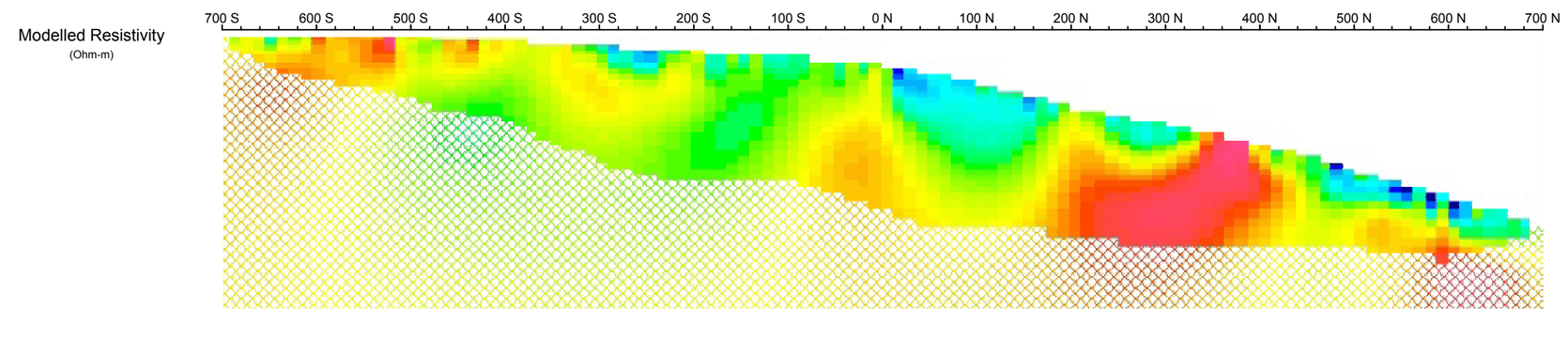
INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L600E

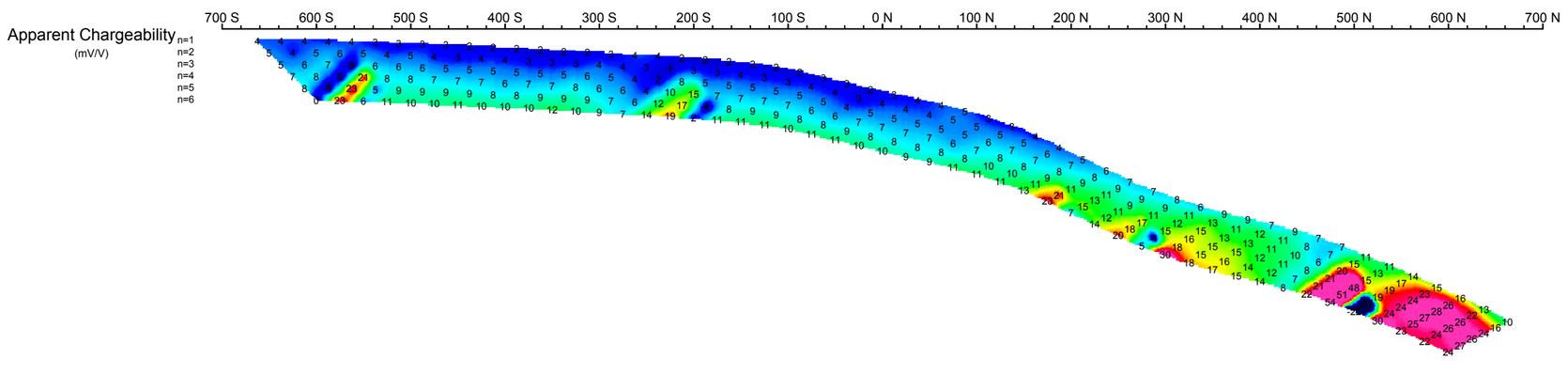
NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: Local — Job: KRX-06-02-YT
Date: 14 Sept 06 — Appendix E

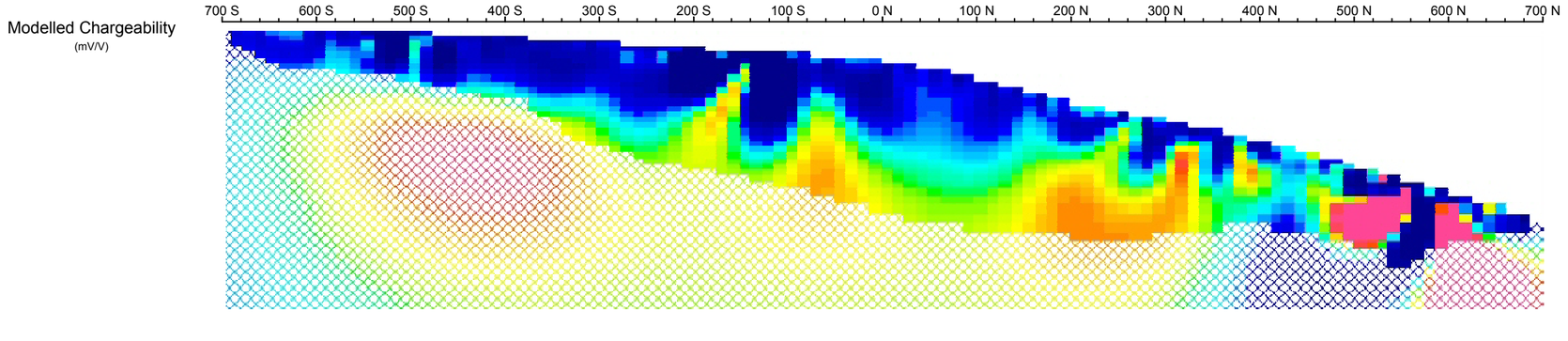
AURORA GEOSCIENCES LTD.

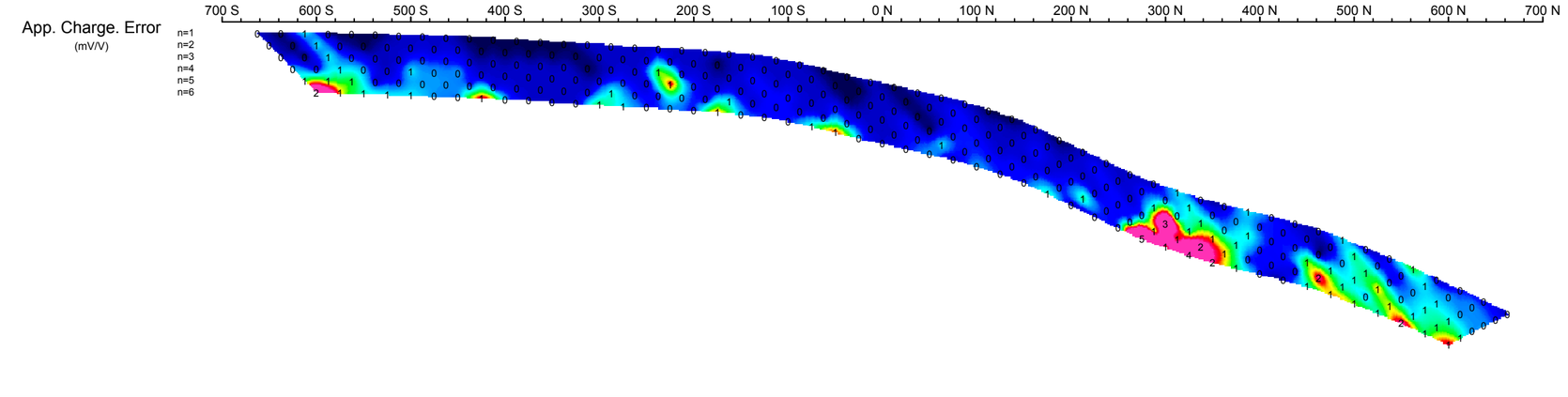
COMPOSITE SECTION PLOT
L800 E



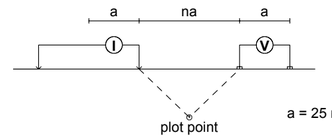




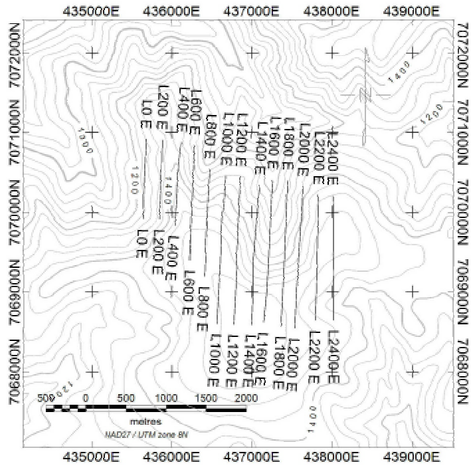




Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 700S.



Scale 1:5000

50 0 50 100 150 200 250 300
metres

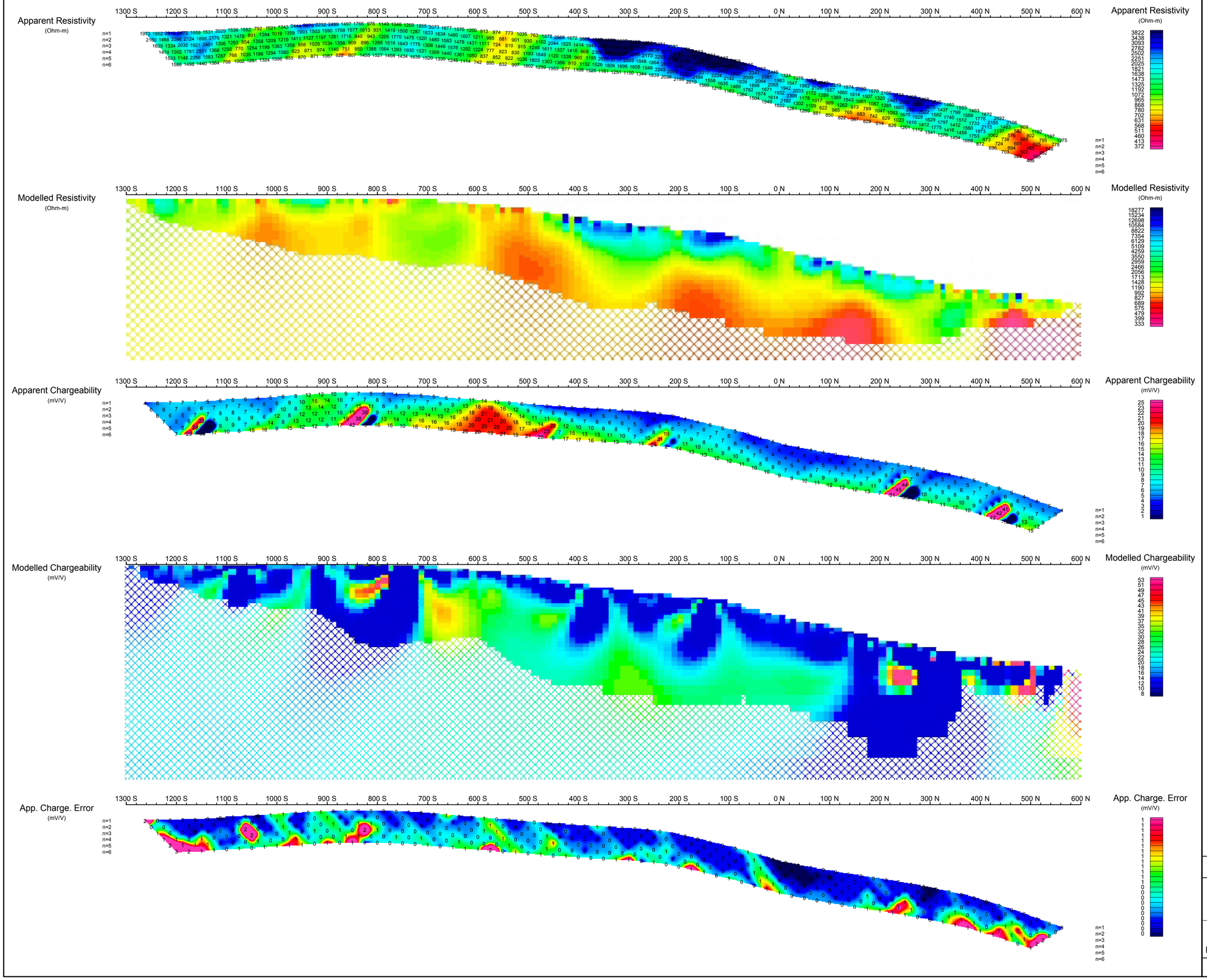
No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L800E

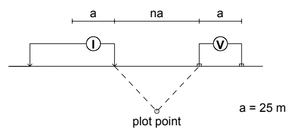
NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: Local — Job: KRX-06-02-YT
Date: 14 Sept 06 — Appendix E

AURORA GEOSCIENCES LTD.

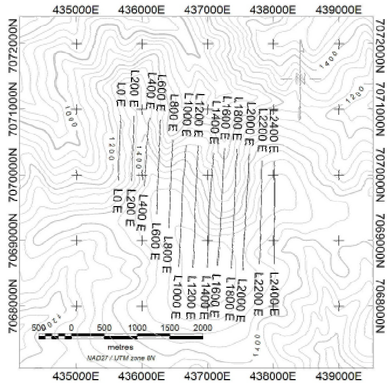


COMPOSITE SECTION PLOT
L1000 E

Modified Pole-Dipole Array



Survey moved grid north
with stationary electrode at station 1300S.



Scale 1:5000

50 0 50 100 150 200 250 300
metres

No vertical exaggeration.

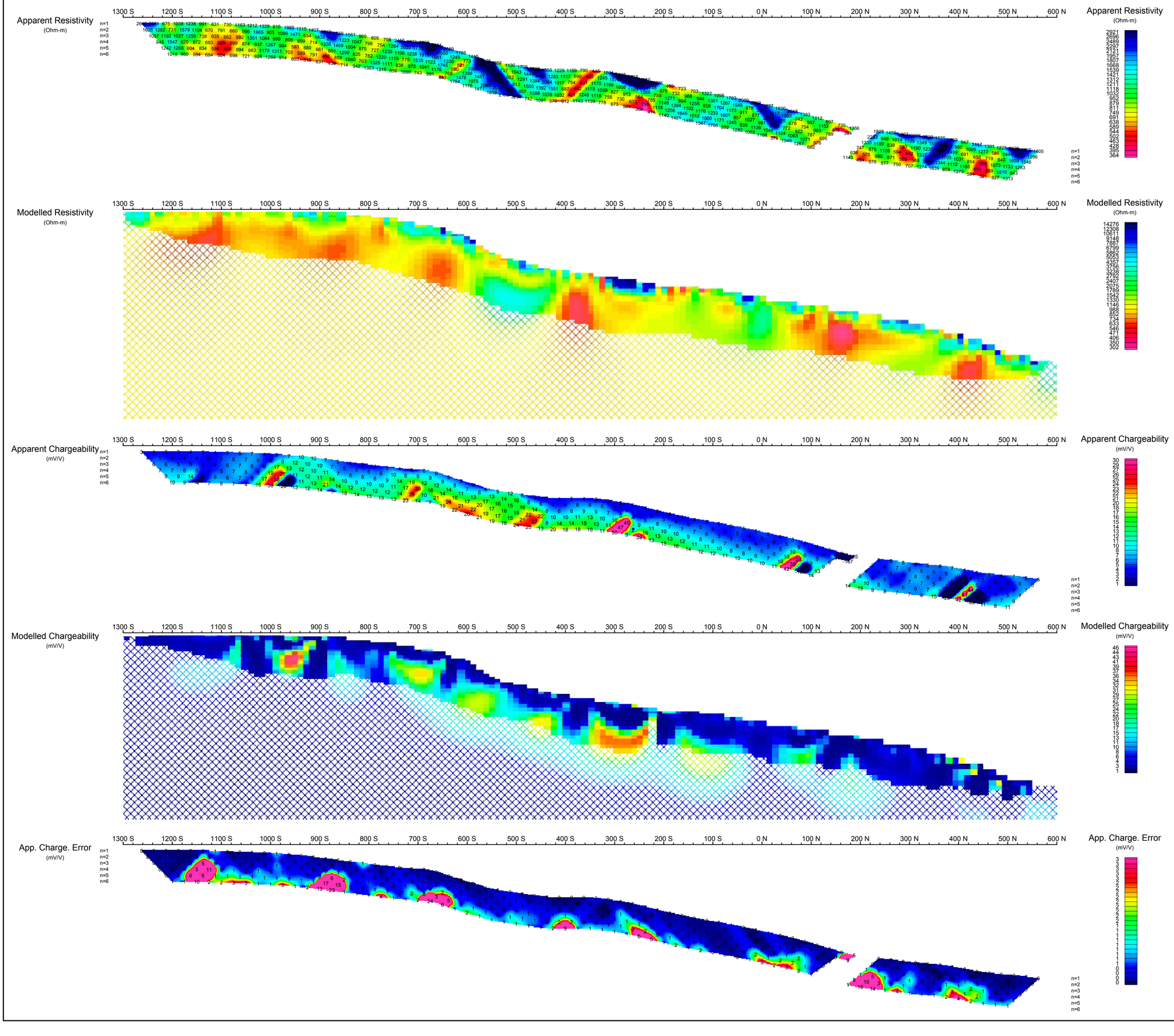
COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L1000E

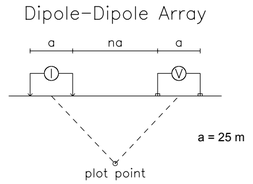
NTS: 115 P/09 & P/16
Grid: Local
Date: 14 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

AURORA GEOSCIENCES LTD.

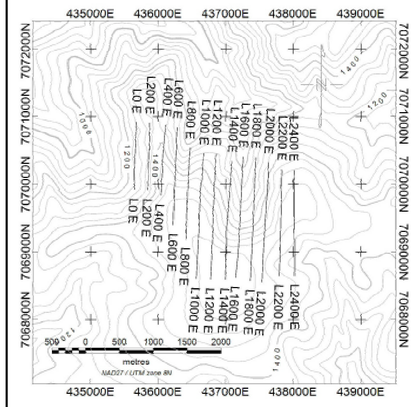


COMPOSITE SECTION PLOT
L1200 E



Survey moved grid north

with stationary electrode at station 1300S.



Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

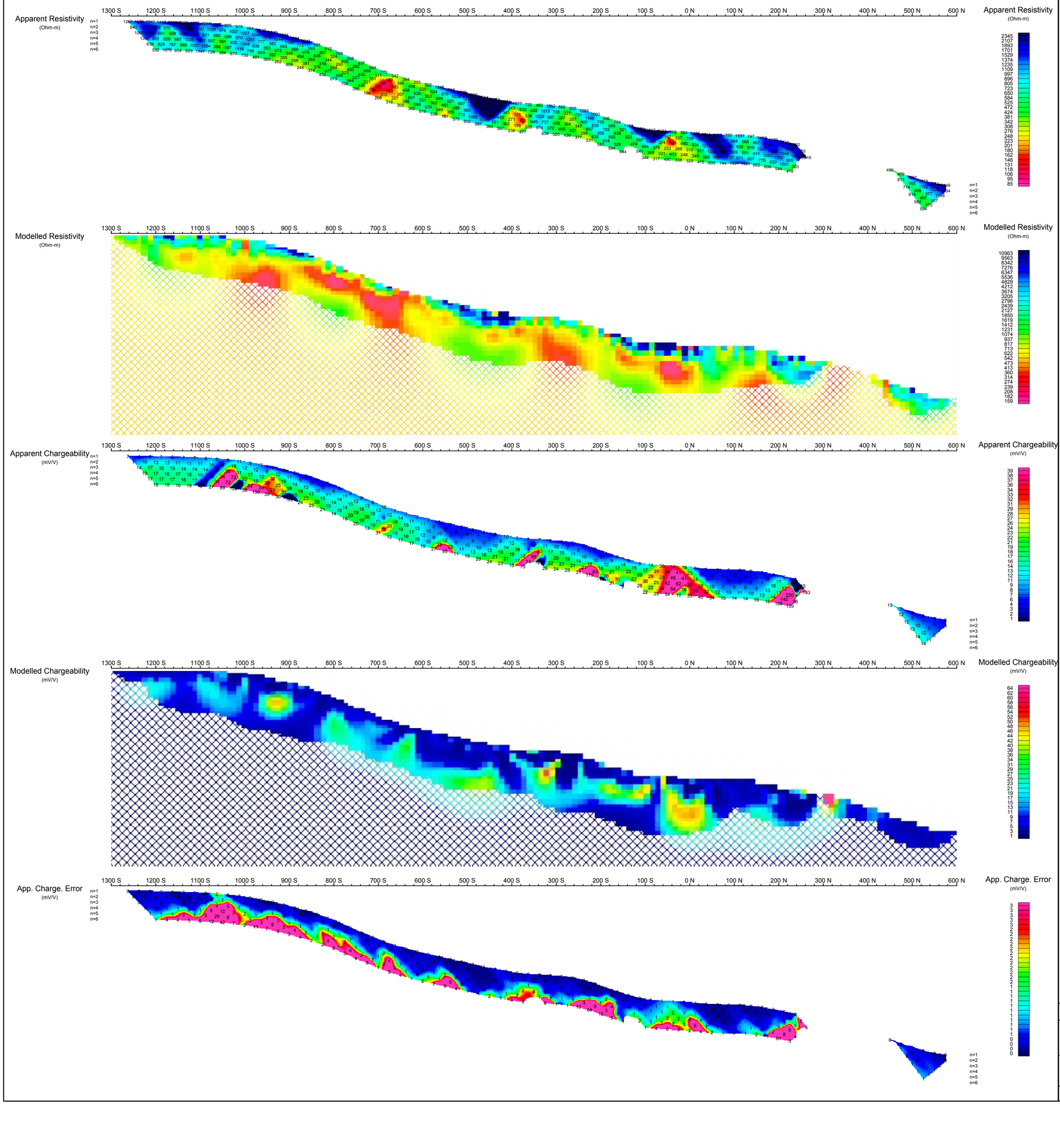
COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L1200E

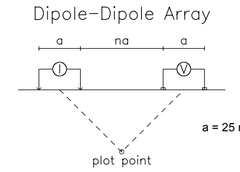
NTS: 115 P/09 & P/16
Grid: Local
Date: 10 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

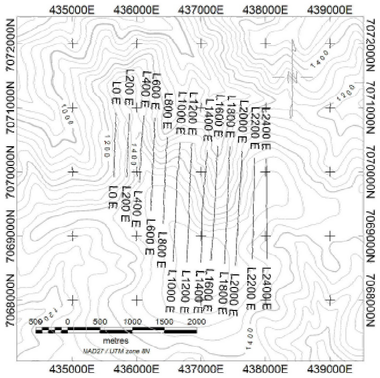
AURORA GEOSCIENCES LTD.



COMPOSITE SECTION PLOT
L1400 E



Survey moved grid north
with stationary electrode at station 1300S.



Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

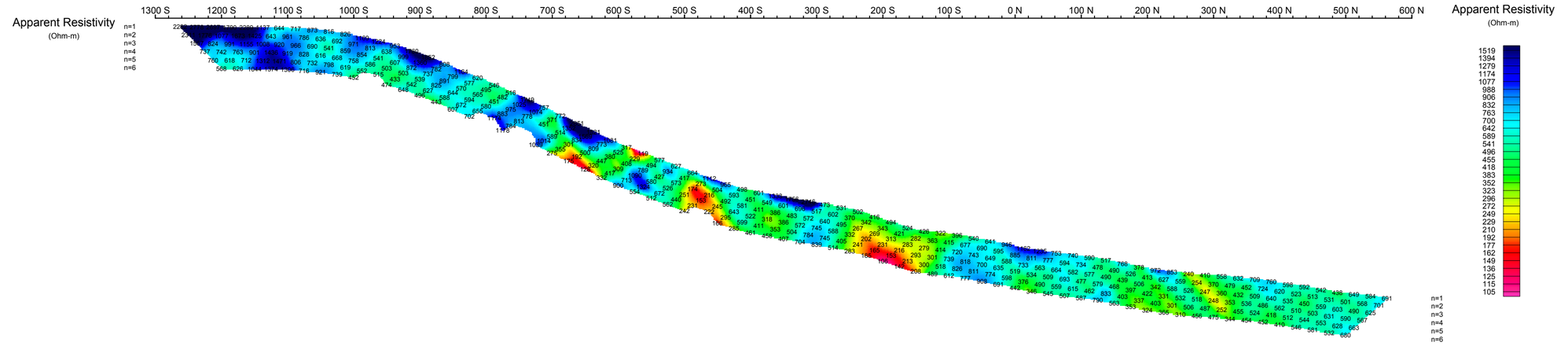
COPPER RIDGE EXPLORATIONS INC.

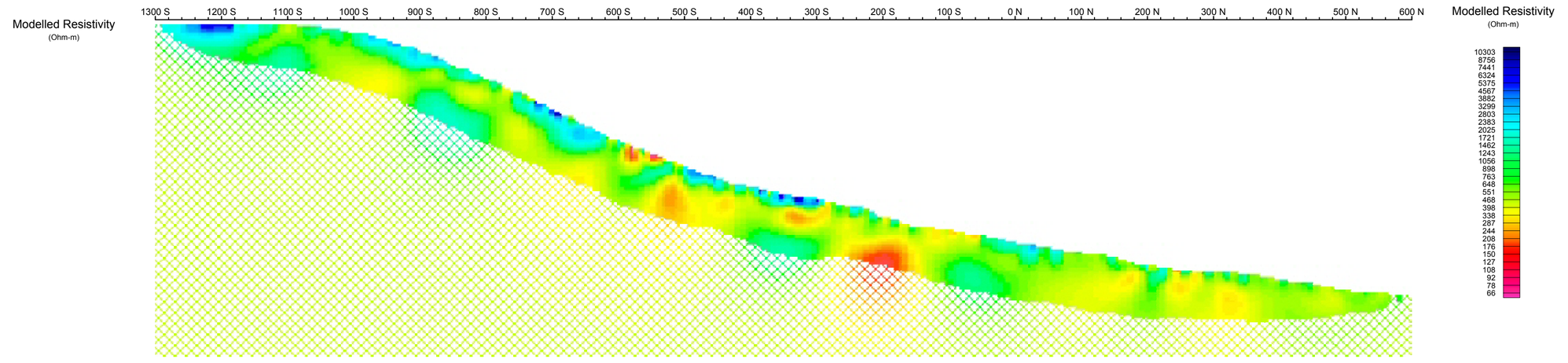
INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L1400E

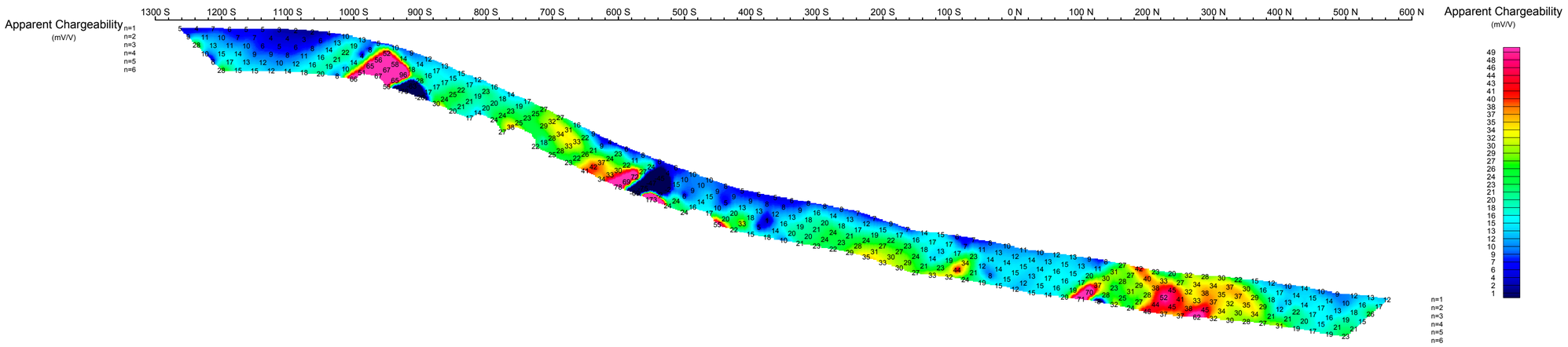
NTS: 115 P/09 & P/16
Grid: Local
Date: 13 Sept 06

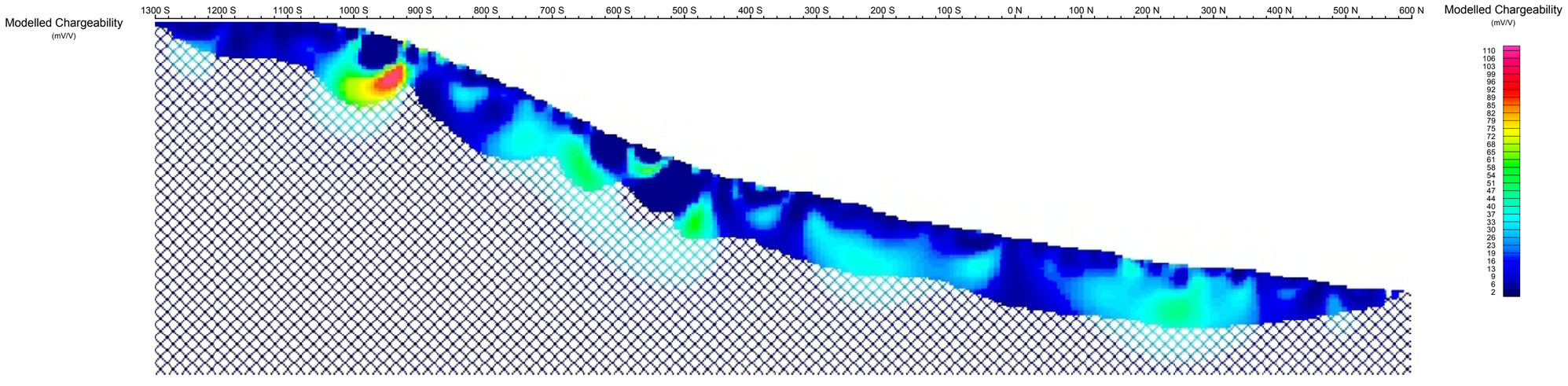
Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

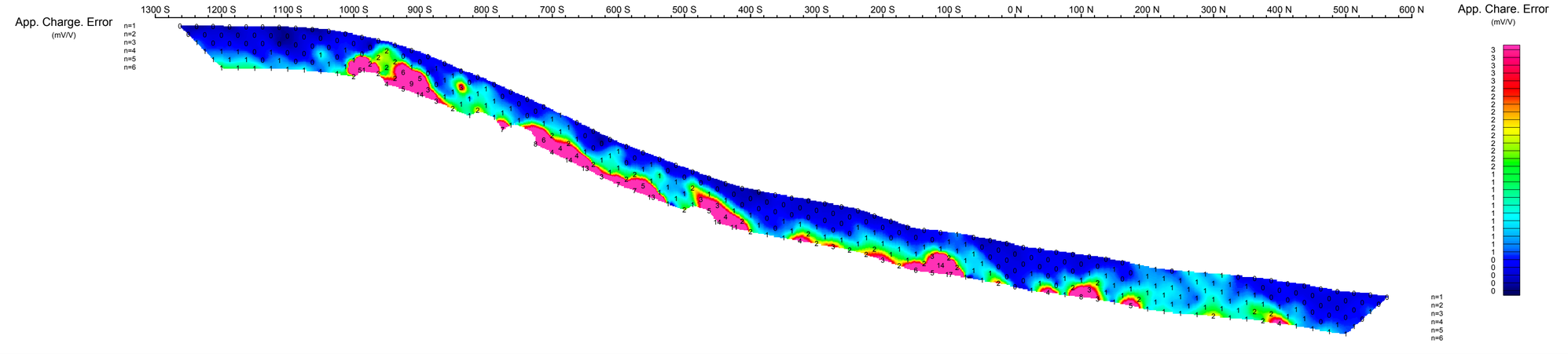
AURORA GEOSCIENCES LTD.



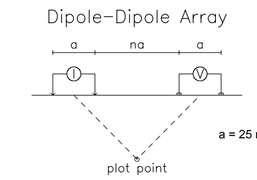


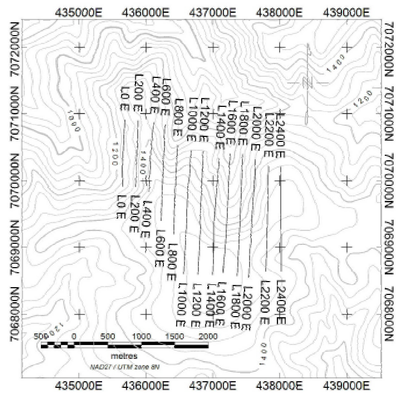






COMPOSITE SECTION PLOT
L1600 E





Scale 1:5000

50 0 50 100 150 200 250 300

metres

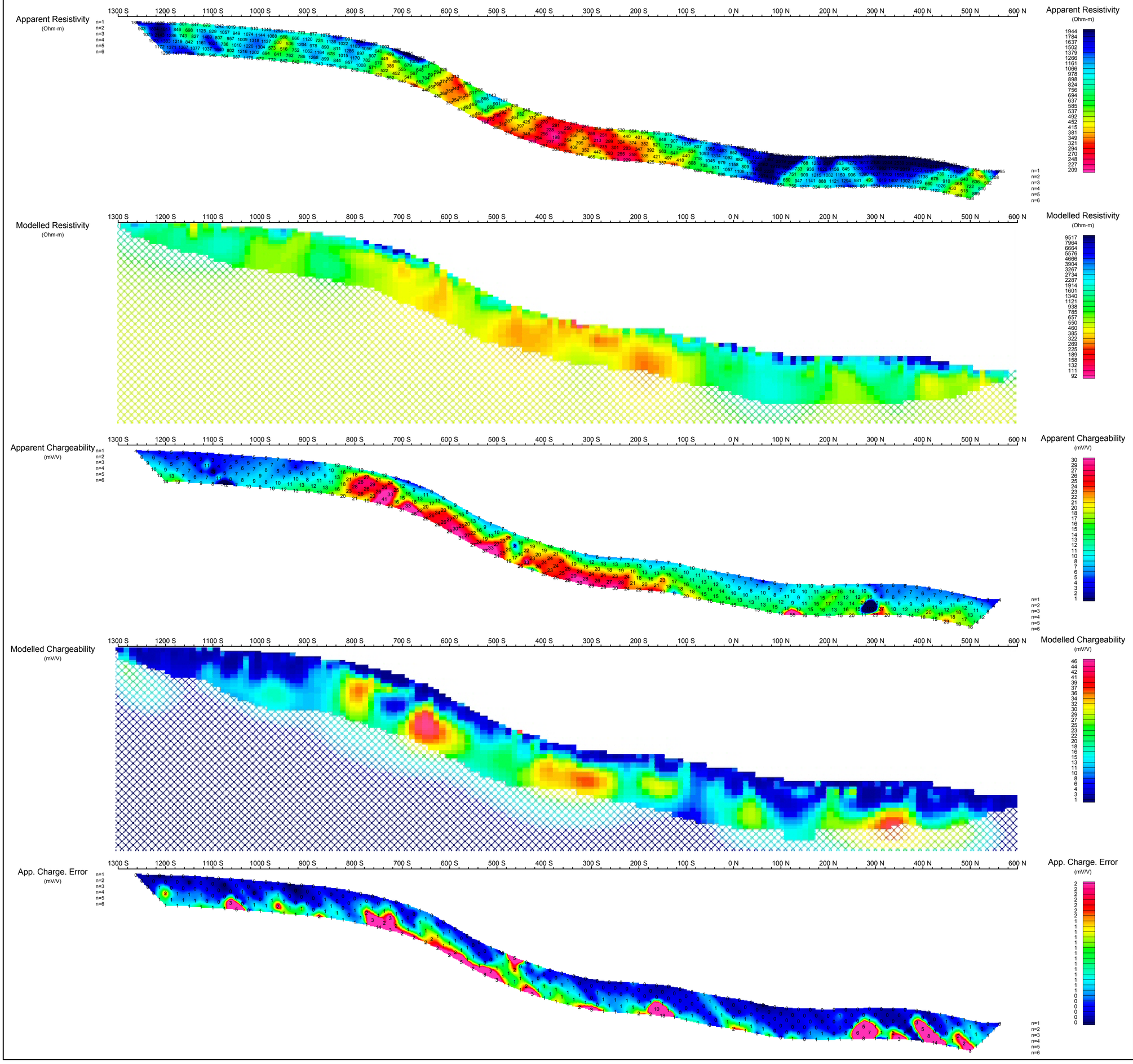
No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

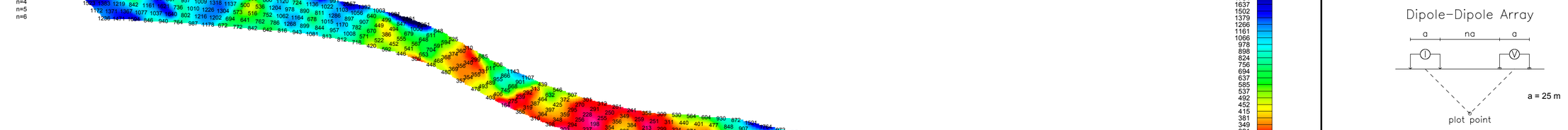
INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L1600E

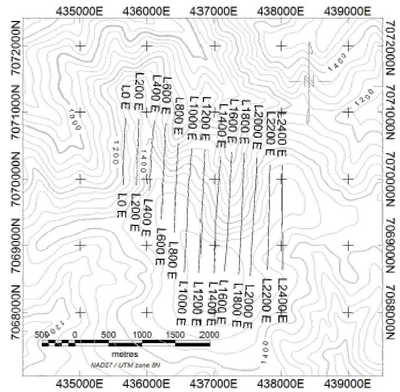
NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: Local — Job: KRX-06-02-YT
Date: 13 Sept 06 — Appendix E

AURORA GEOSCIENCES LTD.



COMPOSITE SECTION PLOT
L1800 E





Scale 1:5000

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metres

No vertical exaggeration.

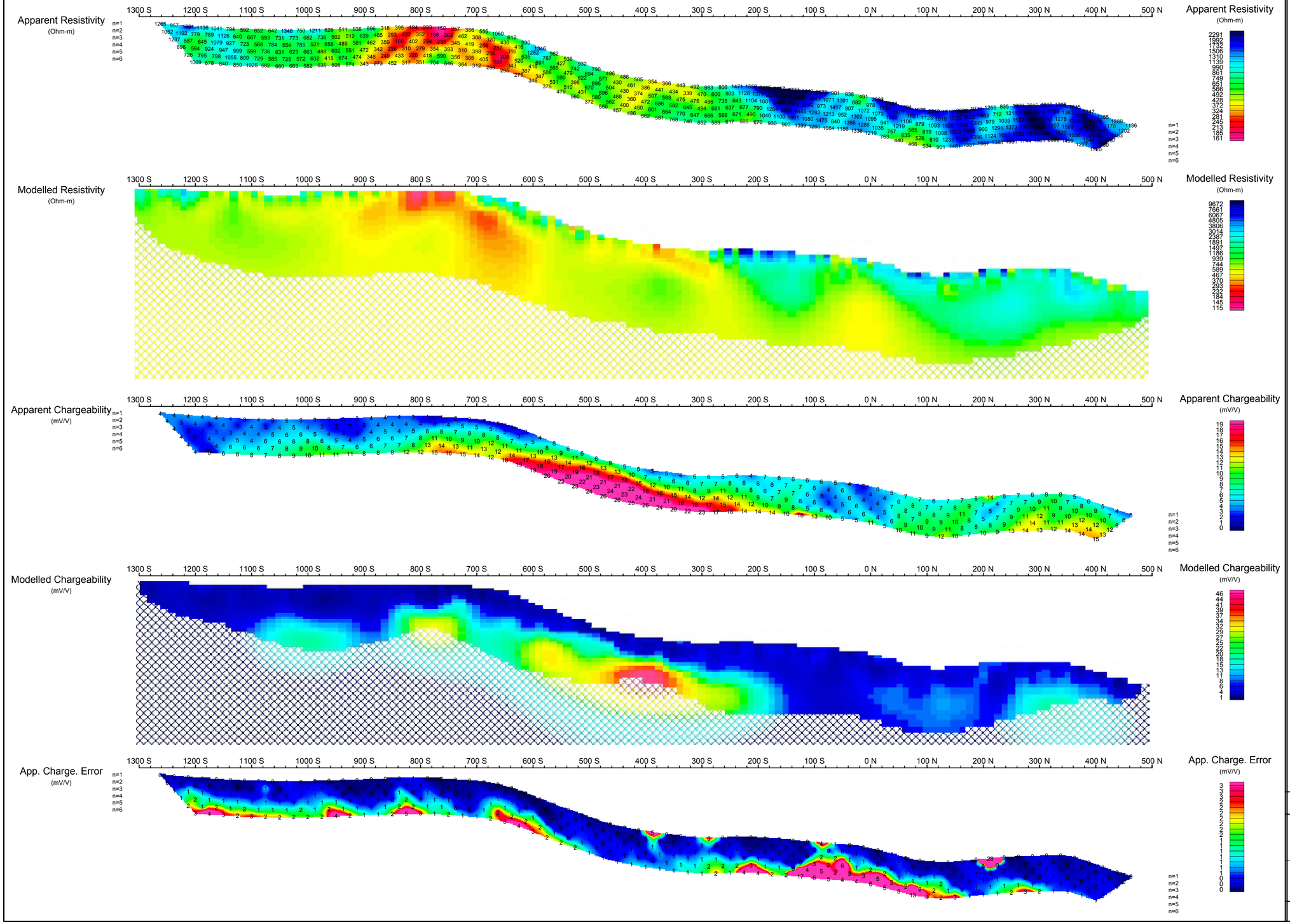
COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L1800E

NTS: 115 P/09 & P/16
Grid: Local
Date: 10 Sept 06

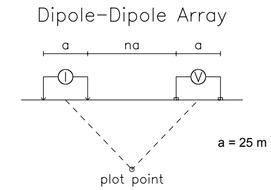
Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

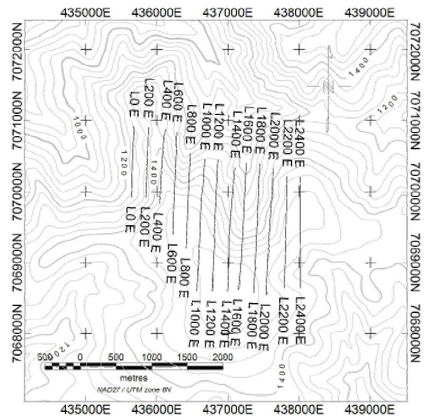
AURORA GEOSCIENCES LTD.



COMPOSITE SECTION PLOT

L2000 E





Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

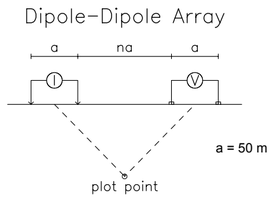
INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L2000E

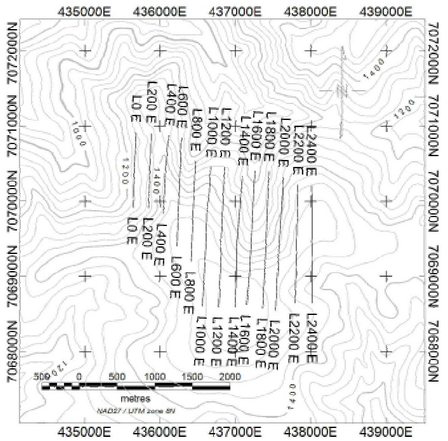
NTS: 115 P/09 & P/16
Grid: Local
Date: 10 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

AURORA GEOSCIENCES LTD.

COMPOSITE SECTION PLOT
L2200 E





Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L2200E

NTS: 115 P/09 & P/16
Grid: Local
Date: 10 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

AURORA GEOSCIENCES LTD.

Apparent Resistivity (Ohm-m)

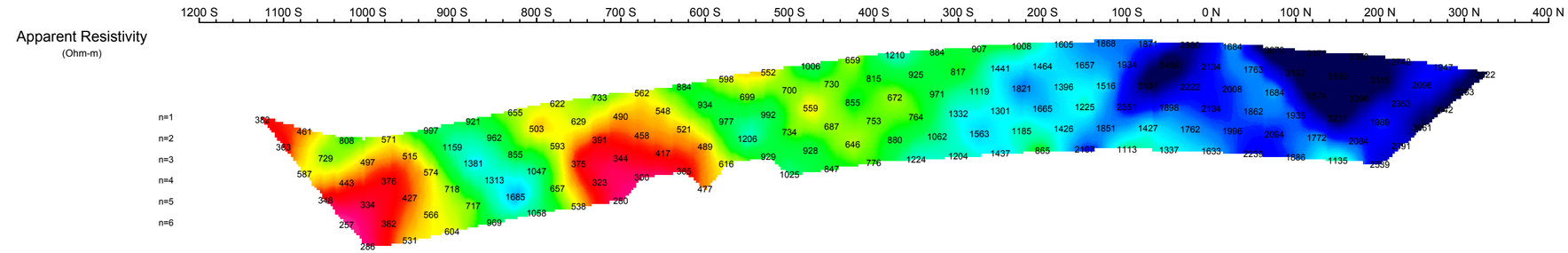
Modelled Resistivity (Ohm-m)

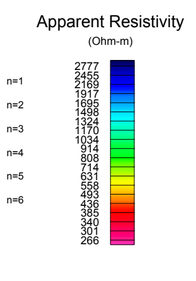
Apparent Chargeability (mV/V)

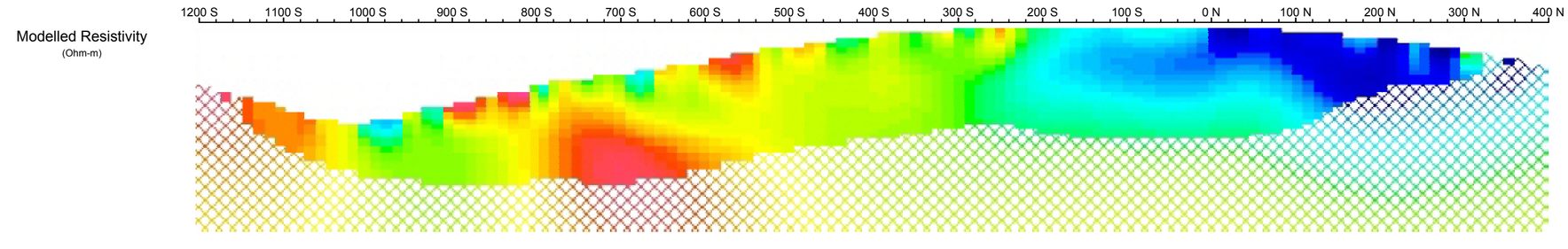
Modelled Chargeability (mV/V)

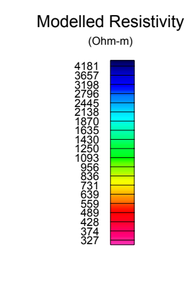
App. Charge. Error (mV/V)

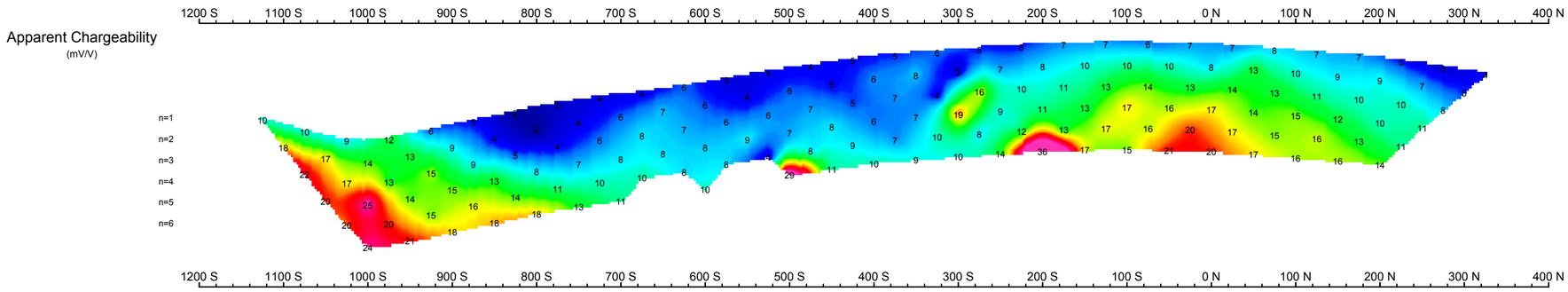
COMPOSITE SECTION PLOT
L2400 E

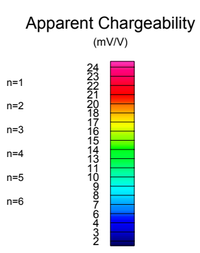


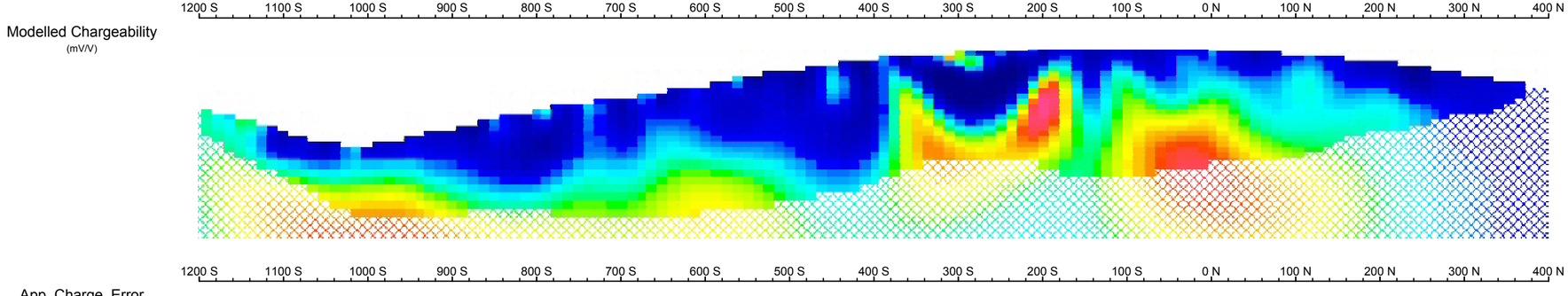


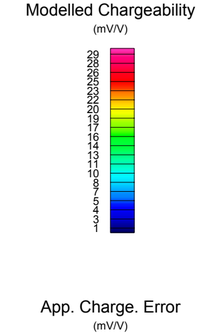


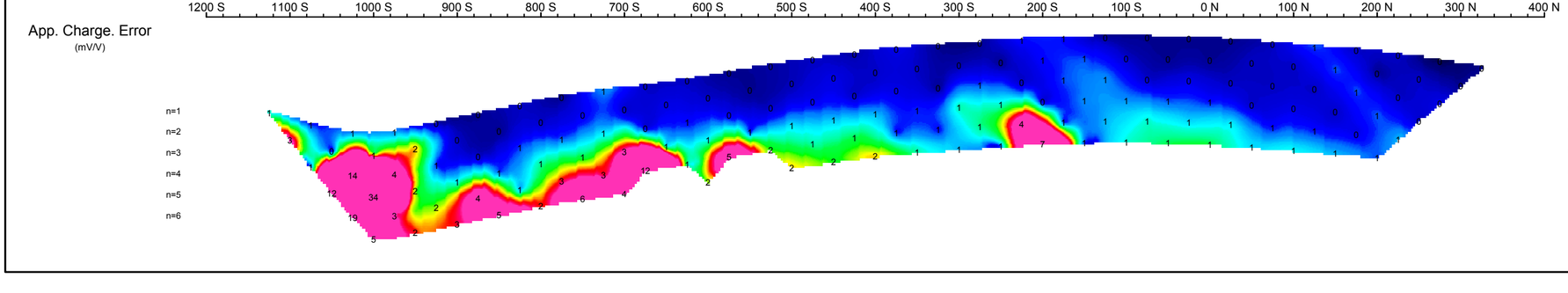


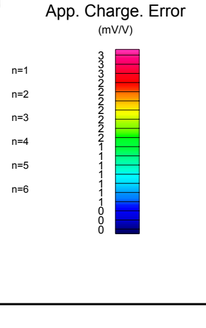


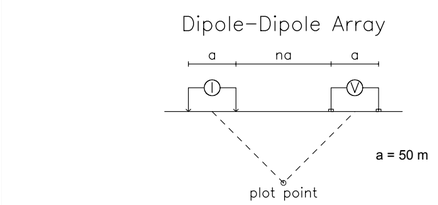


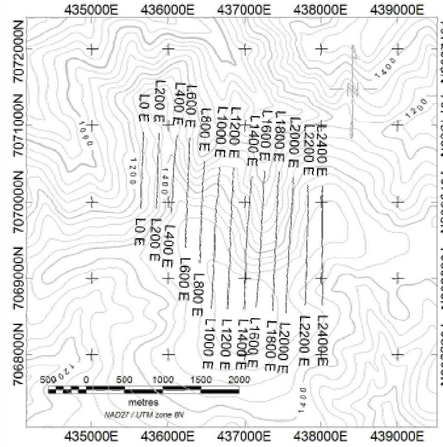












Scale 1:5000

50 0 50 100 150 200 250 300

metres

No vertical exaggeration.

COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
Sheelite Dome Property Toby Zone
Composite Section L2400E

NTS: 115 P/09 & P/16
Grid: Local
Date: 10 Sept 06

Mining District: Mayo
Job: KRX-06-02-YT
Appendix E

AURORA GEOSCIENCES LTD.

LEGEND

TOTAL FIELD MAGNETICS

CONTOUR INTERVALS (nT)

5

20

100

REFERENCE FIELD : 57,000 nT
INSTRUMENT : GEM GSM-19T (GPS)
GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m
FILTER : DESPIKED, WIDTH: 1, THRESHOLD: 50 nT
GRID HANNING FILTER : 3 PASSES
DATA FILE : Scheelite Dome 2006 Mag.gdb
OPERATOR : GF
STATION SEPARATION : 12.5 m
LINE-KM SURVEYED THIS SHEET : 19.9 km
DATES SURVEYED : July 11-14, 2006

57057
57054
57052
57049
57046
57043
57040
57037
57035
57032
57029
57026
57023
57021
57018
57015
57012
57009
57006
57004
57001
56998
56995
56992
56989
56987
56984
56981
56978
56975
56973
56970
56967
56964
56961
56958
56956
56953

Total Magnetic Field
(nT)

Scale 1:5000

100 0 100 200 300

metres

NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.

SCHEELITE DOME PROPERTY, TOBY ZONE
TOTAL MAGNETIC FIELD
COLOUR CONTOURED MAP

Loc: Yukon Territory
NTS Sheet: 115P/09 & 115P/16
Proj: UTM Zone 8N
Job: KRX-06-03-YT

Date: Aug 07, 2006
Mining District: Mayo
Datum: NAD27 (Yukon)
Drawn by: DH
Appendix F

AURORA GEOSCIENCES LTD.

LEGEND

VERTICAL MAGNETIC GRADIENT

CONTOUR INTERVALS (nT/m)

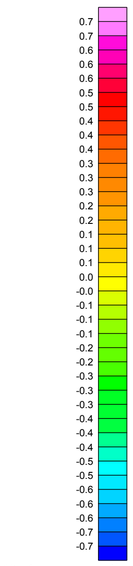
0.1

0.5

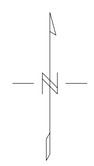
2.5

REFERENCE FIELD : 57,000 nT
INSTRUMENT : GEM GSM-19T (GPS)
GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m
FILTER : DESPIKED, WIDTH: 1, THRESHOLD: 50 nT
GRID HANNING FILTER : 3 PASSES
DATA FILE : Scheelite Dome 2006 Mag.gdb
OPERATOR : GF
STATION SEPARATION : 12.5 m
LINE-KM SURVEYED THIS SHEET : 19.9 km
DATES SURVEYED : July 11-14, 2006



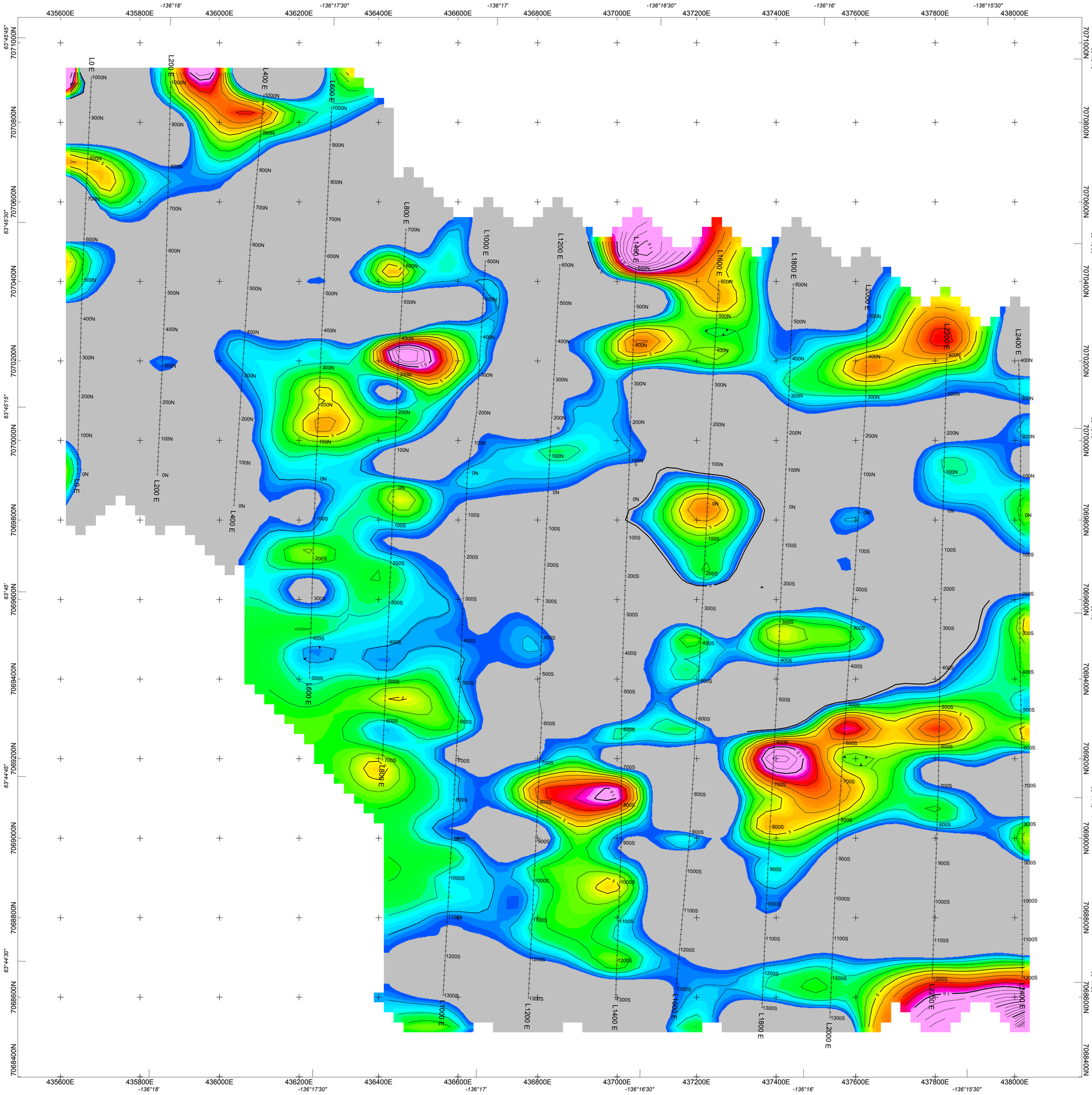
Vertical Magnetic Gradient
(nT/m)



Scale 1:5000

100 0 100 200 300
metres
NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.	
SCHEELITE DOME PROPERTY, TOBY ZONE **CALCULATED VERTICAL DERIVATIVE** **COLOUR CONTOURED MAP**	
Loc: Yukon Territory NTS Sheet: 115P/09 & 115P/16 Proj: UTM Zone 8N Job: KRX-06-03-YT	Date: Aug 07, 2006 Mining District: Mayo Datum: NAD27 (Yukon) Drawn by: DH Appendix F
AURORA GEOSCIENCES LTD.	



9.7
9.5
9.2
9.0
8.7
8.5
8.2
7.9
7.7
7.4
7.2
6.9
6.7
6.4
6.2
5.9
5.6
5.4
5.1
4.9
4.6
4.4
4.1
3.8
3.6
3.3
3.1
2.8
2.6
2.3
2.1
1.8
1.5
1.3
1.0
0.8
0.5
0.3

Fraser Filtered InPhase VLF
(%)

LEGEND

FRASER FILTERED INPHASE

CONTOUR INTERVALS (%)

1

5

10

VLF STATION : 24.0 kHz Cutler, Maine, USA
INSTRUMENT : GEONICS EM-16
GRIDDING ALGORITHM : MINIMUM CURVATURE
GRID HANNING FILTER : 3 PASSES
GRID CELL SIZE : 25 m
DATA FILE : Scheelite 2006 VLF.xyz
STATION SEPARATION : 12.5m
LINE-KM SURVEYED THIS SHEET : 19.7 km
DATES SURVEYED : July 10 - 29, 2006
FACING DIRECTION : Grid North
DESPIKING FILTER : width=1 fid, threshold=10%
LOWPASS FILTER : width=4 fids
FRASER FILTER : 5 point (.5,1,0,-1,-.5)

NAA Cutler (083)

Scale 1:5000

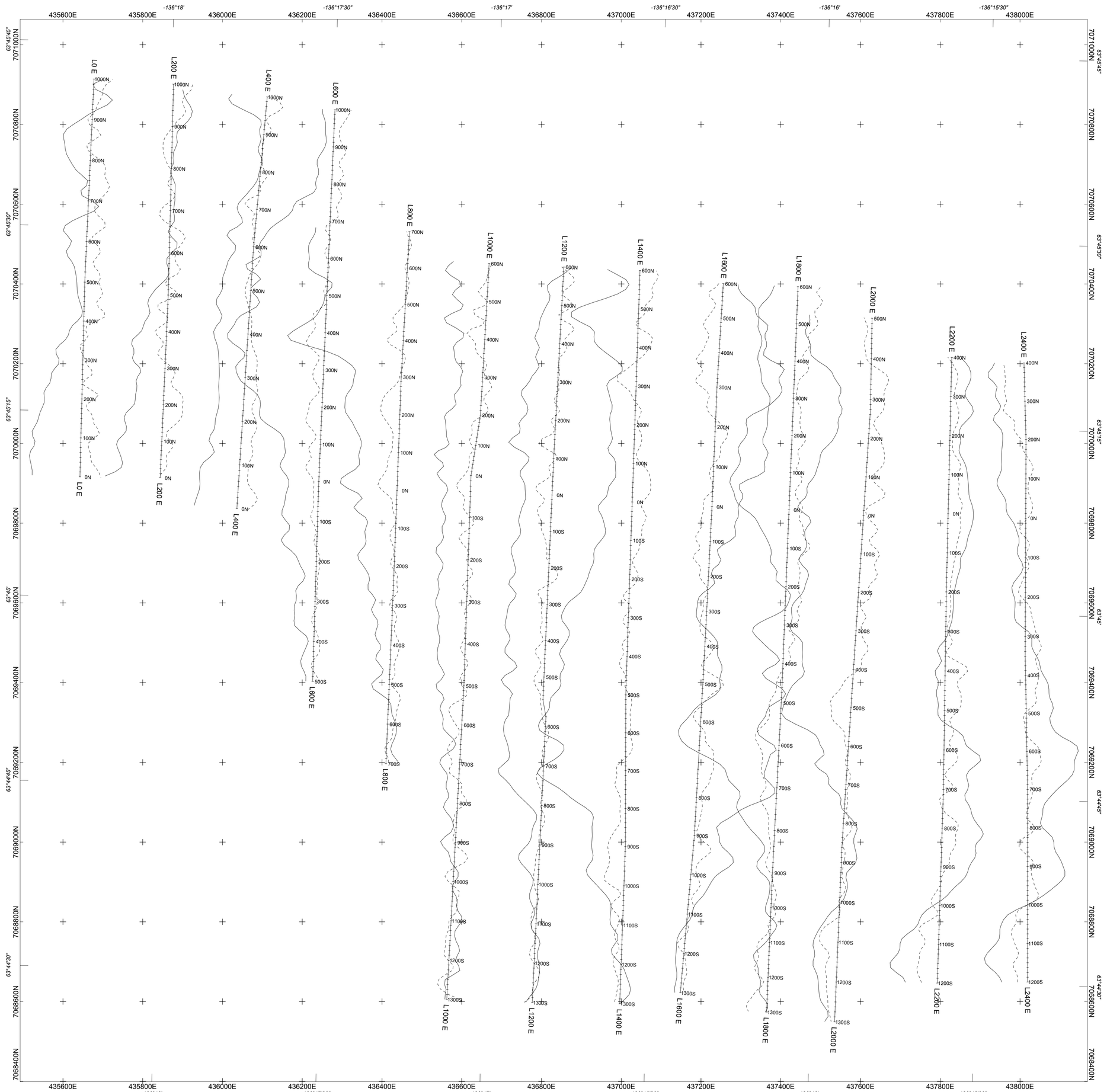
100 0 100 200 300
metres
NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.

SCHEELITE DOME PROPERTY, TOBY ZONE
VLF-EM SURVEY
CONTOURED FRASER FILTERED INPHASE
APPENDIX G

Mayo Mining District, Yukon Territory
NTS: 115P/09 & 115P/16 Date: Jan 16, 2007
Datum: NAD27 (Yukon) Proj: UTM Zone 8N
Job: KRX-06-02-YT Drawn by: DH

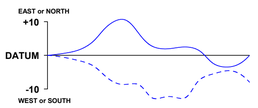
AURORA GEOSCIENCES LTD.



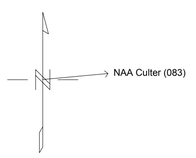
LEGEND
STACKED VLF-EM PROFILES

VLF STATION : 24.0 kHz Cutler, Maine, USA
INSTRUMENT : GEONICS EM-16
PROFILE SCALE : 1 cm = 10%

IN PHASE :
QUADRATURE :



IN-PHASE DATUM : 0%
QUADRATURE DATUM : 0%
DATA FILE : Scheelite 2006 VLF.xyz
STATION SEPARATION : 12.5m
LINE-KM SURVEYED THIS SHEET : 19.7 km
DATES SURVEYED : July 10 - 29, 2006
FACING DIRECTION : Grid North
DESPIKING FILTER : width=1 fid, threshold=10%
LOWPASS FILTER : width=4 fids



Scale 1:5000

100 0 100 200 300
metres
NAD27 / UTM zone 8N

COPPER RIDGE EXPLORATIONS INC.

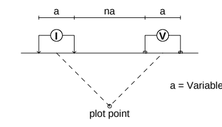
SCHEELITE DOME PROPERTY, TOBY ZONE
VLF-EM SURVEY
STACKED INPHASE AND QUADRATURE PROFILES
APPENDIX G

Mayo Mining District, Yukon Territory
NTS: 115P/09 & 115P/16 **Date: Jan 16, 2007**
Datum: NAD27 (Yukon) **Proj: UTM Zone 8N**
Job: KRX-06-02-YT **Drawn by: DH**

AURORA GEOSCIENCES LTD.

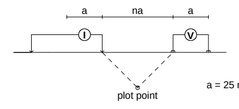
STACKED PSEUDOSECTIONS MAP
APPARENT CHARGEABILITY

Dipole-Dipole Array



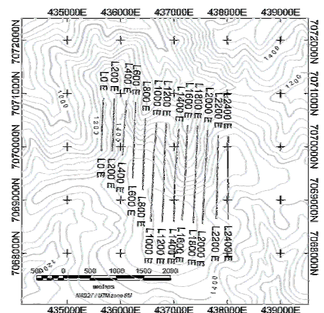
50 m dipole-dipole for lines 2400E & 2200E.
25 m dipole-dipole for lines 2000E through 1200E.

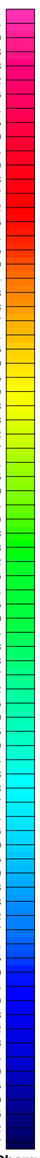
Modified Pole-Dipole Array



Modified pole-dipole used for lines 1000E through 0E.
Survey moved grid north with stationary electrode at south end of each line.

Major Contour Interval: 10 mV/V
Minor Contour Interval: 2 mV/V
Receiver: Iris ElrecPro
Transmitter: GDD Tx-II 3.6kW
Data File: Scheelite Dome IP Final.gdb
Line-km surveyed this sheet: 20.4 km





Apparent Chargeability
(mV/V)

Scale 1:5000

50 0 50 100 150 200 250
metres

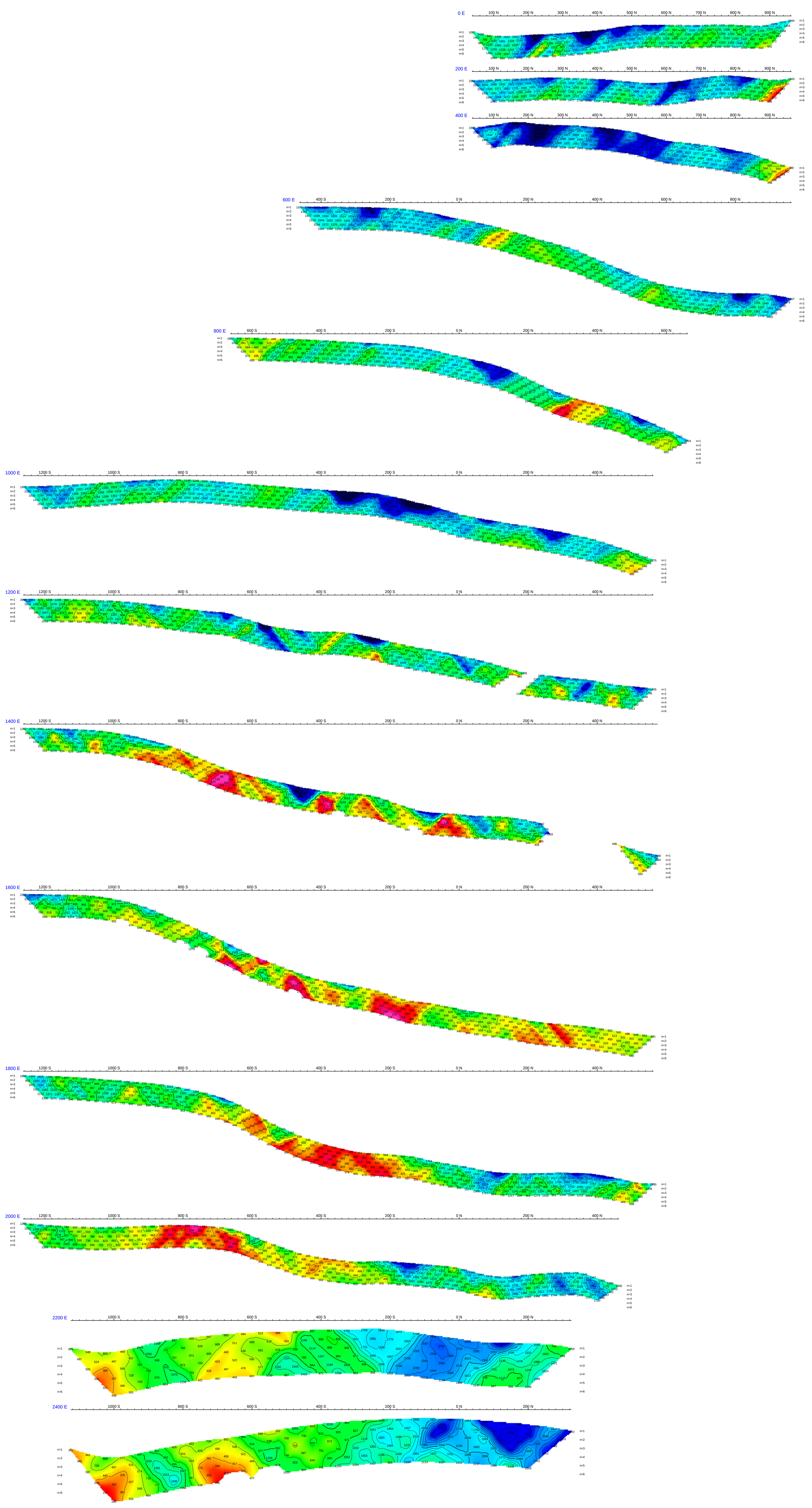
COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
SCHEELITE DOME PROPERTY, TOBY ZONE
STACKED APP. CHARGEABILITY

Yukon Territory, Canada
NTS: 115P/09 & 115P/16
Date: Aug 07, 2006

Mayo Mining District
Appendix H
JOB: KRX-06-02-YT

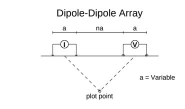
AURORA GEOSCIENCES LTD.



STACKED PSEUDOSECTIONS MAP

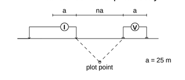
APPARENT RESISTIVITY

Dipole-Dipole Array



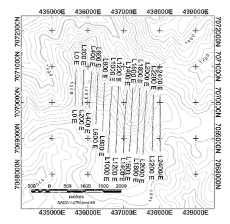
50 m dipole-dipole for lines 2400E & 2200E.
25 m dipole-dipole for lines 2000E through 1200E.

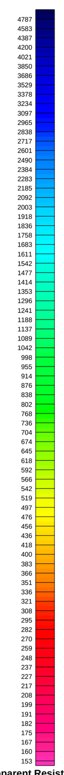
Modified Pole-Dipole Array



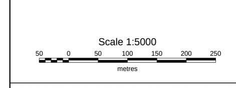
Modified pole-dipole used for lines 1000E through 0E.
Survey moved grid north with stationary electrode at south end of each line.

Major Contour Interval: 1000 Ohm*m
Minor Contour Interval: 200 Ohm*m
Receiver: Iris ElrecPro
Transmitter: GDD Tx-II 3.6kW
Data File: Scheelite Dome IP Final.gdb
Line-km surveyed this sheet: 20.4 km





Apparent Resistivity
(Ohm-m)



COPPER RIDGE EXPLORATIONS INC.

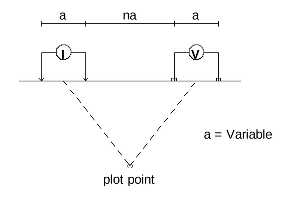
INDUCED POLARIZATION SURVEY
SCHEELITE DOME PROPERTY, TOBY ZONE
STACKED APP. RESISTIVITY
Appendix H

Yukon Territory, Canada	Mayo Mining District
NTS: 115P/09 & 115P/16	Grid: Local
Date: Aug 07, 2006	JOB: KRX-06-02-YT

AURORA GEOSCIENCES LTD.

STACKED MODELLED CHARGEABILITY SECTIONS

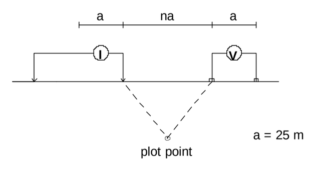
Dipole-Dipole Array



50 m dipole-dipole for lines 2400E & 2200E.

25 m dipole-dipole for lines 2000E through 1200E.

Modified Pole-Dipole Array



Modified pole-dipole used for lines 1000E through 0E.

Survey moved grid north with stationary electrode at south end of each line.

Major Contour Interval: 1000 Ohm*m

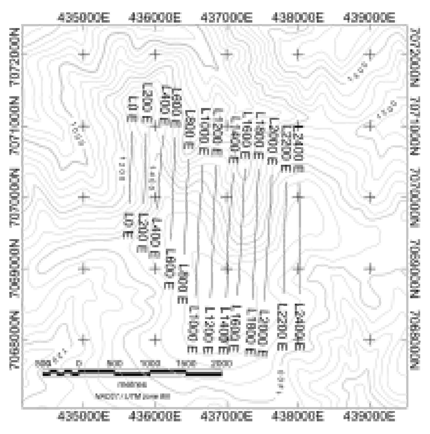
Minor Contour Interval: 200 Ohm*m

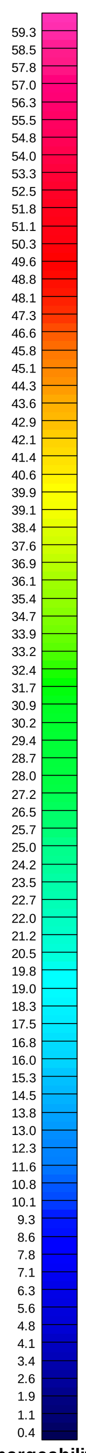
Receiver: Iris ElrecPro

Transmitter: GDD Tx-II 3.6kW

Data File: Scheelite Dome IP Final.gdb

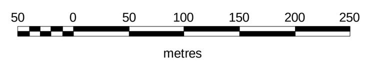
Line-km surveyed this sheet: 20.4 km





Chargeability
(mV/V)

Scale 1:5000



COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY

SCHEELITE DOME PROPERTY, TOBY ZONE

STACKED CHARGEABILITY MODELS

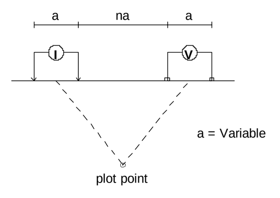
NTS: 115 P/09 & 115 P/16
Grid: Local
Date: Aug 10, 2006

Mining District: Mayo
Job: KRX-06-02-YT
Appendix H

AURORA GEOSCIENCES LTD.

STACKED MODELLED RESISTIVITY SECTIONS

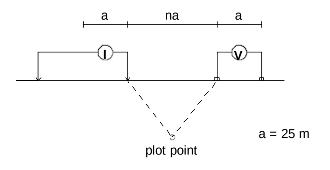
Dipole-Dipole Array



50 m dipole-dipole for lines 2400E & 2200E.

25 m dipole-dipole for lines 2000E through 1200E.

Modified Pole-Dipole Array



Modified pole-dipole used for lines 1000E through 0E.

Survey moved grid north with stationary electrode at south end of each line.

Major Contour Interval: 1000 Ohm*m

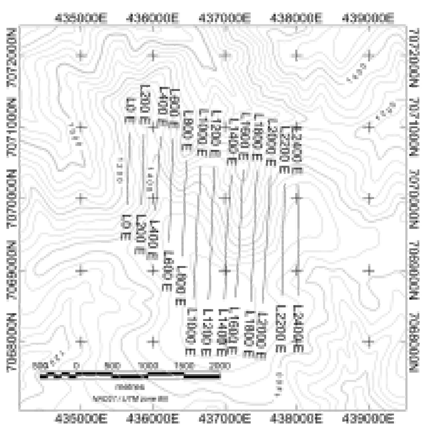
Minor Contour Interval: 200 Ohm*m

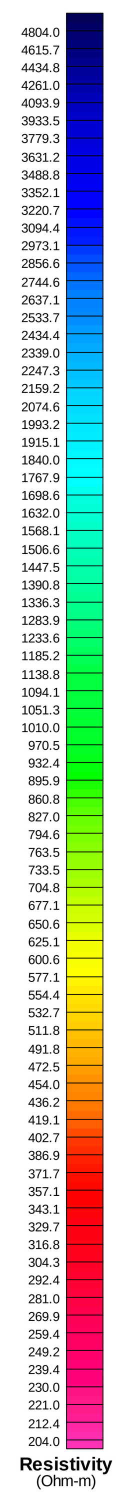
Receiver: Iris ElrecPro

Transmitter: GDD Tx-II 3.6kW

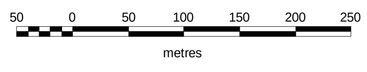
Data File: Scheelite Dome IP Final.gdb

Line-km surveyed this sheet: 20.4 km





Scale 1:5000



COPPER RIDGE EXPLORATIONS INC.

INDUCED POLARIZATION SURVEY
SCHEELITE DOME PROPERTY, TOBY ZONE
STACKED RESISTIVITY MODELS

NTS: 115 P/09 & 115 P/16
Grid: Local
Date: Aug 10, 2006

Mining District: Mayo
Job: KRX-06-02-YT
Appendix H

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 1

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm/m)

250

500

1000

INSTRUMENT : ELREC PRO / GDD 3.6kW TX II

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

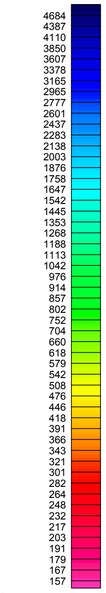
DATA FILE : IPDataPlanView. gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATES SURVEYED: July 6th - July 30th, 2006



Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300

metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVIY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 1

NTS: 115 P/09 — Mining District: Mayo

Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT

Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 2

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm m)

250

500

1000

INSTRUMENT : ELREC PRO / GDD 3.6kW Tx II

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

DATA FILE : IPDataPlanView. gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

4684
4387
4110
3850
3607
3378
3165
2965
2777
2601
2437
2283
2138
2003
1876
1758
1647
1542
1445
1353
1268
1188
1113
1042
976
914
857
802
752
704
660
618
579
542
508
476
446
418
391
366
343
321
301
282
264
248
232
217
203
191
179
167
157

Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 2

NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

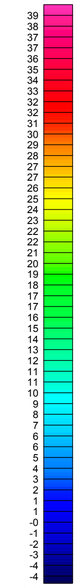
DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006



Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 3

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm m)

250

500

1000

INSTRUMENT : ELREC PRO / GDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

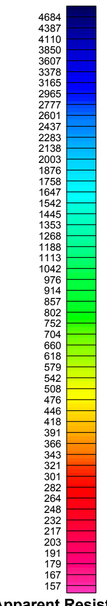
DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006



Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 3

NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

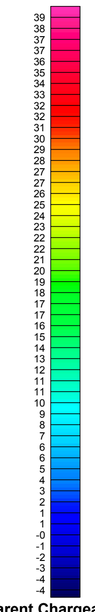
DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006



Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 4

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm m)

250

500

1000

INSTRUMENT : ELREC PRO GDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

DATA FILE : IPDataPlanView. gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

4684
4387
4110
3850
3607
3378
3165
2965
2777
2601
2437
2283
2138
2003
1876
1758
1647
1542
1445
1353
1268
1188
1113
1042
976
914
857
802
752
704
660
618
579
542
508
476
446
418
391
366
343
321
301
282
264
248
232
217
203
191
179
167
157

Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 4

NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 5

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm m)

250

500

1000

INSTRUMENT : ELREC PRO GDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

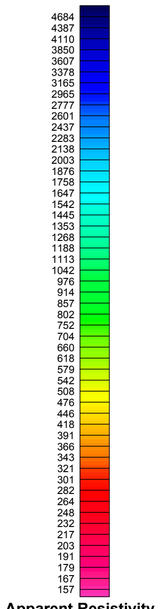
DATA FILE : IPDataPlanView. gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006



Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300

metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVIY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 5

NTS: 115 P/09 — Mining District: Mayo

Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT

Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

AVERAGE IP

CONTOUR INTERVALS (mV/V)

5

10

25

INSTRUMENT : ELREC PROGDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 2 PASSES

DATA FILE : IPDataPlanView.gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006

Apparent Chargeability
(mV/V)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT CHARGEABILITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 6

NTS: 116 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.

LEGEND

APPARENT RESISTIVITY

CONTOUR INTERVALS (Ohm m)

250

500

1000

INSTRUMENT : ELREC PRO GDD 3.6kW TxII

GRIDDING ALGORITHM : MINIMUM CURVATURE

GRID CELL SIZE : 25 m

GRID HANNING FILTER : 3 PASSES

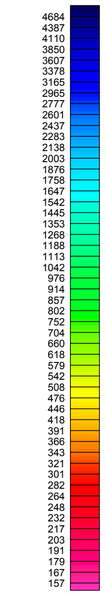
DATA FILE : IPDataPlanView. gdb

OPERATOR : JB

STATION SEPARATION : 25m & 50m

LINE-KM SURVEYED THIS SHEET : 20.4 km

DATE SURVEYED: July 6th - July 30th, 2006



Apparent Resistivity
(Ohm-m)

Scale 1:5000

100 0 100 200 300
metres

COPPER RIDGE EXPLORATIONS INC.

APPARENT RESISTIVITY PLAN MAP
Scheelite Dome Property Toby Zone
Dipole N Spacing = 6

NTS: 115 P/09 & P/16 — Mining District: Mayo
Grid: NAD 27 Canada Mean - Zone 8 — Job: KRX-06-02-YT
Date: 22 Jan 07 — Appendix I

AURORA GEOSCIENCES LTD.