

**2001 EXPLORATION PROGRAM
on the
HYLAND RIVER PROJECT,
WATSON LAKE AREA,
YUKON TERRITORY**

60° 19' Lat, 128° 04' Long

NTS 105A-08

Watson Lake Mining District

Mineral Claims:

ZAP 1 to 20, YB93334 to YB93353
ZAP 23 to 44, YB93354 to YB93375

Scott Casselman, B.Sc., P.Geol.
Aurora Geosciences Ltd.
January, 2002

SUMMARY

In the summer of 2001 Aurora Geosciences Ltd conducted a program involving prospecting, soil sampling, trenching, stream sediment sampling and claim staking in the Hyland River area, 55 km northeast of Watson Lake, Yukon. The program targeted Selwyn Basin rocks prospective for sedimentary exhalative (SEDEX) lead-zinc-silver mineralization. The area was identified as prospective through research of the Geological Survey of Canada Regional Geochemical Survey (RGS) database, which identifies a large region of anomalous lead, zinc, cadmium, barium and silver in stream sediment samples. As well, the Yukon Minfile and assessment reports identified a number of SEDEX mineral occurrences in the area.

The program targeted an area on the southern margin of the anomalous RGS data, where previous workers identified anomalous lead, zinc, cadmium and silver in soil. Detailed soil sample surveys identified areas anomalous for the suite of SEDEX indicator elements. The anomalies occur in drainage basins at roughly the same elevation around the mountain indicating that the streams are cutting down through a mineral enriched horizon which is believed to dip gently to the west.

Trenches were dug on two of the stronger lead-in-soil anomalies to determine the source of the lead. The trenching program was not able to exposed the source of the mineralization, however, soil profiles in the trenches identified the Pb and Zn anomalies occurring in progressively lower soil horizons as the trenches continue up slope. Thus, the source of the Pb-Zn-Cd-Ba-Ag is believed to be a short distance further up slope and further trenching may expose the source.

Detailed stream sediment sampling was conducted down stream of the trenches and soil anomalies to determine the dispersion pattern to aid in follow-up on other drainages in the area.

Recommendations for future work on the property are to extend the existing trenches up slope to identify the source of the soil geochemical anomalies and to follow-up other soil geochemical anomalies on the property with detailed soil sampling and trenching. If the source of the Pb-Zn-Cd-Ba-Ag mineralization is a buried SEDEX horizon, a gravity survey across the mountain may help to define its size and location. As well, there remain numerous RGS anomalies in the region which should be followed-up with stream sediment sampling and prospecting.

Table of Contents

SUMMARY

1	INTRODUCTION	1
2	LOCATION AND ACCESS	1
3	LAND STATUS	3
4	EXPLORATION HISTORY	3
5	REGIONAL GEOLOGY	5
6	HYLAND RIVER PROSPECT GEOLOGY	6
7	2001 WORK PROGRAM	7
8	RESULTS	7
9	CONCLUSIONS AND RECOMMENDATIONS	8
10	REFERENCES	9
11	STATEMENT OF EXPENDITURES	10
12	STATEMENT OF QUALIFICATIONS	11

List of Figures

Figure 1	Property Location Map	2
Figure 2	Claim Location Map	4
Figure 3	Stream Sediment Sample and Trench Location Map	In pocket
Figure 4	Hand Trench # 1 Map	In pocket
Figure 5	Hand Trench # 2 Map	In pocket
Figure 6	2001 Soil Sample Locations	In pocket
Figure 7	Lead Soil Sample Plot	In pocket
Figure 8	Zinc Soil Sample Plot	In pocket
Figure 9	Cadmium Soil Sample Plot	In pocket
Figure 10	Silver Soil Sample Plot	In pocket

Appendices

Appendix I	Daily Log
Appendix II	Sample Descriptions
Appendix III	Geochemical Analytical Certificates
Appendix IV	Grid GPS Coordinates

1 INTRODUCTION

The Hyland River Pb-Zn-Ag Prospect is a sedimentary exhalative exploration target located 50 km northeast of Watson Lake, on the east side of the Hyland River, Yukon Territory. The prospect was identified while researching the Geological Survey of Canada Regional Geochemical Survey (RGS) data, the Yukon Minfile and assessment reports for southeastern Yukon Territory. The prospect area stood out for its highly anomalous barium, zinc, cadmium, lead and silver values in stream sediments over a sizable area (up to 15 by 40 km).

Significant Zn-Pb-Ag mineralization is known to occur in the area at the Quartz Lake (McMillan) deposit, which is located on the northeastern margin of the stream sediment geochemical anomaly. Quartz Lake hosts 1.5 million tonnes grading roughly 11% combined lead-zinc and 62 g/t silver.

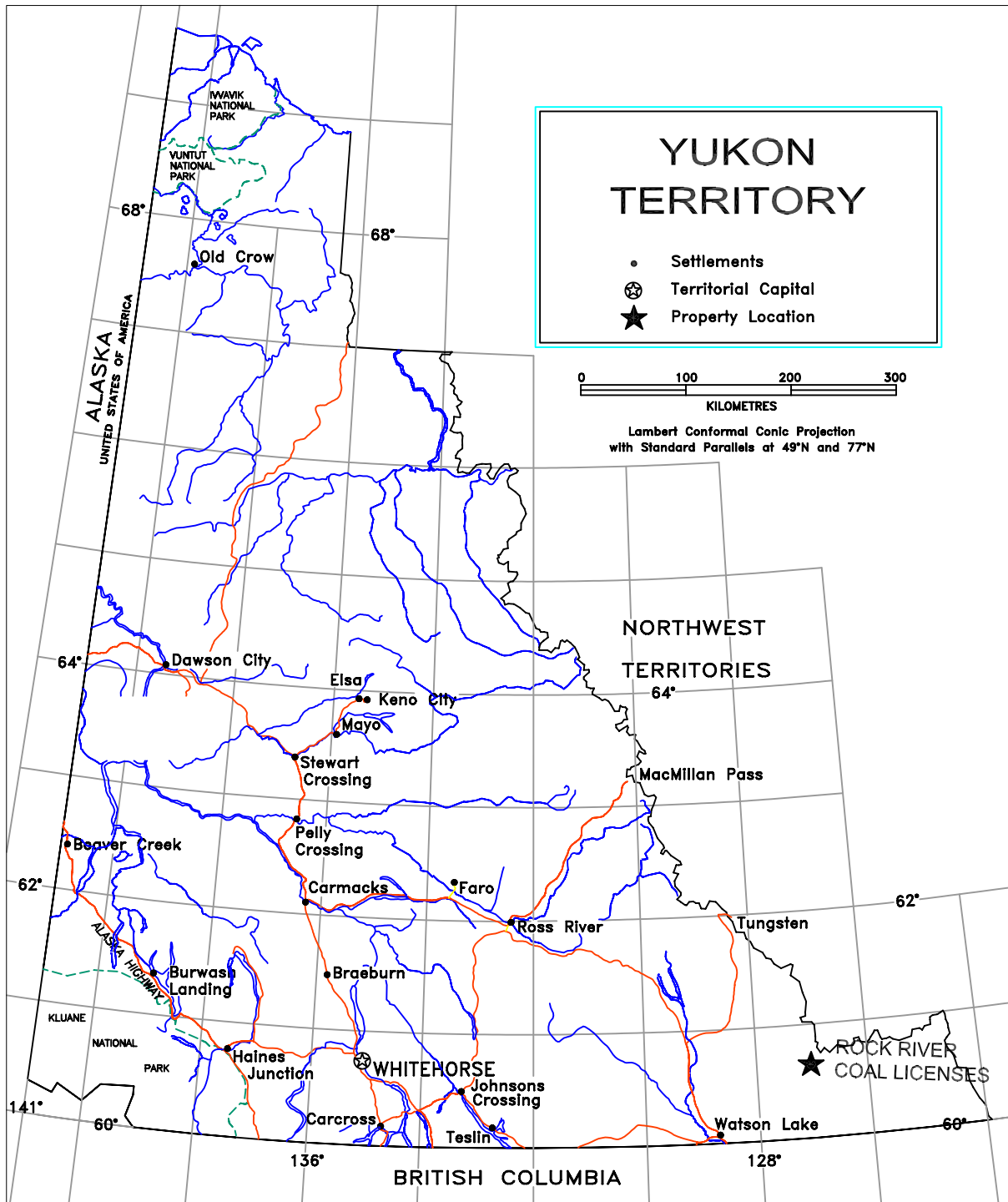
The 2001 exploration program targeted an area on the southern margin of the anomalous RGS data, where previous workers identified anomalous lead, zinc, cadmium and silver in soils and numerous anomalous rock samples (Pawliuk, 1996). The program involved following-up the soil and rock anomalies with additional soil sampling, stream sediment sampling, trenching and prospecting. As the program progressed, 42 mineral claims were staked in the core of the soil geochemical anomaly to protect the prospect.

The field work was conducted in two phases; the first phase was from July 12 to July 30 (19 days) and involved some trenching, soil sampling, prospecting and claim staking. The second phase was conducted from August 31 to September 10 (11 days) and involved trenching, stream sediment sampling and prospecting. The crew consisted of a project manager (Scott Casselman) and assistant (Peter Malacarne).

2 LOCATION AND ACCESS

The Hyland River Prospect is located 50 km northeast of the community of Watson Lake, in the Watson Lake Mining District, on NTS map sheets 105A-08 (Figure 1). The prospect is centered at 60° 19' North Latitude, 128° 04' West Longitude.

Access to the prospect for the 2001 program was by helicopter from Watson Lake. Gravel logging roads come to within 30 km of the prospect area. A winter cat trail from the Coal River Logging Road may provide access to the eastern part of the prospect area.



4763 NWT LTD	ZAP PROPERTY	
PROPERTY LOCATION	MINING DISTRICT: WATSON LAKE	
	NTS: 105A/08	SCALE 1: 6 000 000
<i>Aurora Geosciences Ltd.</i>	DRAWN BY: SGC	
	DATE: 9 Oct 03	FIGURE: 1

3 LAND STATUS

The Hyland River Prospect area has seen a fair amount of exploration activity in the past, however at present there are very few active claims. The Quartz Lake (McMillan) Deposit is still staked and owned by Noranda. Immediately to the east is the Hyland Gold Property of Archer, Cathro and Associates (1981) Ltd and Hemlo Gold Mines Ltd. The area has a large native land claim on the west side of the Hyland River, however this claim is outside of the anomalous RGS area.

During the program, 42 Quartz Claims were staked to cover the core of the prospective area. The claims were recorded in the name of Aurora Geosciences Ltd. on July 30, 2001 in Watson Lake. Claim information is as follows:

Claim Name	Grant #	Expiry Date*
ZAP 1 to 20	YB93334 to YB93353	July 30, 2002
ZAP 23 to 44	YB93354 to YB93375	July 30, 2002

* not including assessment work filed from this program.

4 EXPLORATION HISTORY

The Hyland River area has been explored intermittently since 1949. The main focus of the exploration activity has been the Quartz Lake (McMillan) Pb-Zn-Ag deposit and the Hyland Gold Deposit. Both of these properties are immediately east of the Hyland Pb-Zn-Ag Prospect area.

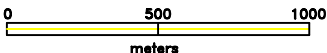
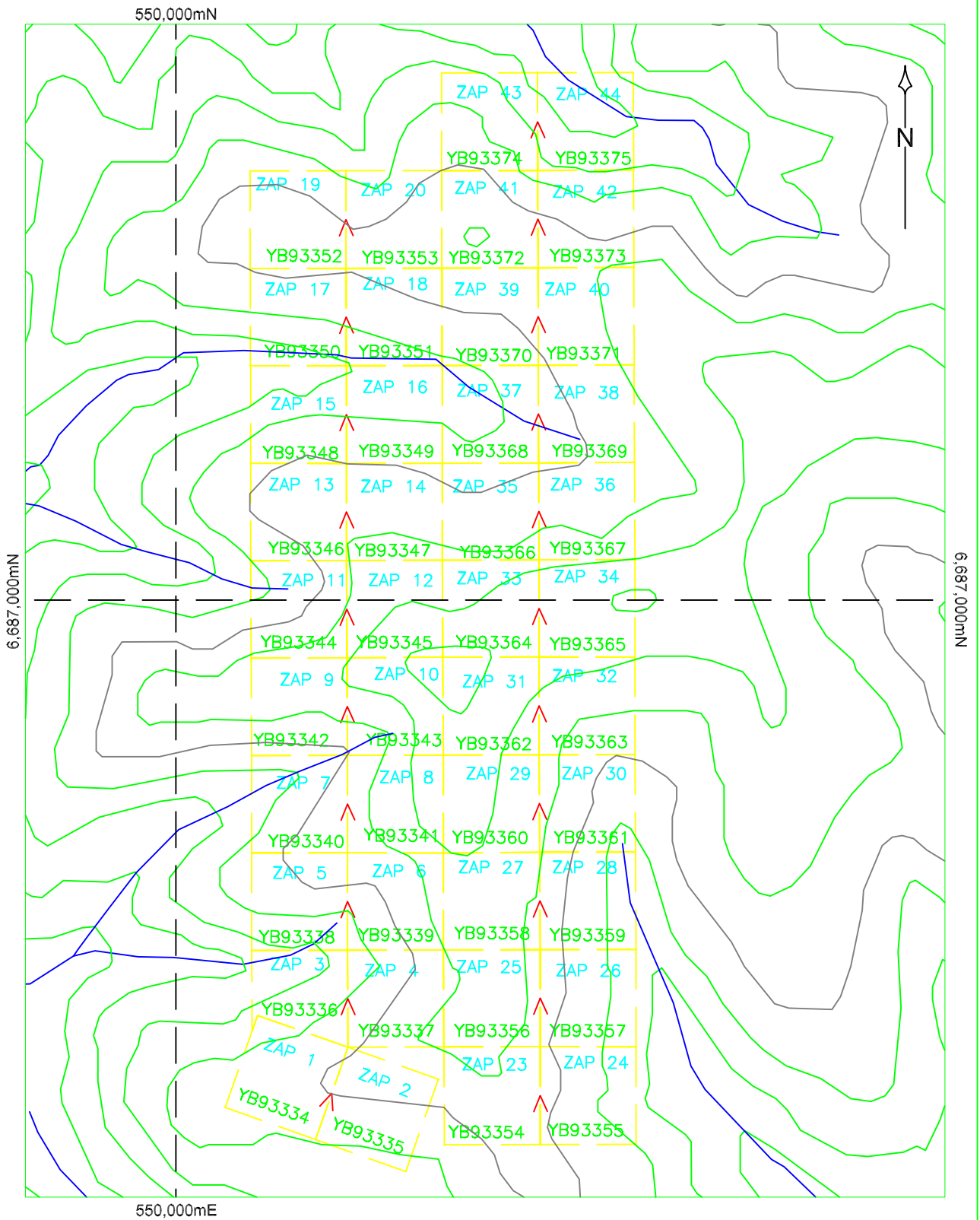
The showing at Quartz Lake (Minfile # 095D 006) was discovered in 1892 and staked in 1930. The property had been explored extensively from 1949 to 1981, during which time 16,597 m of drilling was completed in 190 holes. The drilling defined two ore zones; the McMillan deposit and the South Zone (300 m south of McMillan). The last documented work on the property was bulldozer trenching and soil sampling in 1990 and reclamation work in 1993.

The Hyland Gold Deposit (Minfile # 095D 011) is a low-grade oxide gold deposit with open-pit potential. A reserve estimate of 6.75 million tonnes grading 2.0 g/t Au has been published for the deposit, however it is based mainly on trench results. The property has undergone 5,283 m of diamond and rotary drilling in 56 holes from 1954 to 1995. Archer, Cathro complete some work on the property in 1999, however details of that work are not known.

In the area of the Hyland Pb-Zn-Ag Prospect there has been some scattered exploration activity for Pb-Zn-Ag and for gold. In 1978, prospectors found zinc-rich black shale in an unnamed creek in the northern prospect area (Minfile # 105A 027). This led to the staking of the GUM claims by Hudson Bay Exploration and Development. Hudson Bay conducted soil sample surveys on three small grids in 1978 and 1979 and some hand trenching in 1979. The soil surveys identified four anomalous areas, which received limited follow-up and the claims were later allowed to lapse.

In the center of the Prospect area is the Aurum gold occurrence (Minfile # 105A 039). The showing was originally discovered in 1973, but not staked until 1981 by Kidd Creek Mines Ltd. It hosts disseminated tetrahedrite, enargite and sphalerite in quartz-chlorite veins up to 20 cm wide which cut black silty to sandy limestone of the Hyland Group. Archer, Cathro conducted mapping and soil sampling surveys for Kidd Creek in 1982. The property was later dropped.

At the southern extent of the anomalous RGS area is the Balon Showing (Minfile # 105A 018). Render Resources Ltd staked the HY claims over the showing in 1978 and carried out mapping and soil sampling in 1979. In 1980, a joint venture between Cyprus Anvil Mining Corp and Hudson's Bay Oil and Gas optioned the HY claims and surrounded them with the SF and GS claims. The joint venture conducted mapping, line cutting, soil sampling and a magnetic survey on a large widely spaced grid in 1981. The soil sampling defined some highly anomalous Pb and Zn zones. These results were not followed-up and the claims were later allowed to lapse. In 1994, Archer, Cathro and Westmin Resources Ltd re-staked the area as the SPK claims and carried out airborne magnetic and radiometric surveys, geological mapping, line cutting, rock, soil and stream sediment sampling. This work corroborated the anomalous soil results from the Cyprus Anvil/Hudson



AURORA GEOSCIENCES LTD.		HYLAND RIVER PROJECT	
CLAIM LOCATION		MINING DISTRICT: WATSON LAKE	
		NTS: 105 A/8	SCALE 1: 250,000
Aurora Geosciences Ltd.		DRAWN BY: HDS	
		DATE: 2001.12.19	FIGURE: 2

Bay work and identified a number of anomalous barite values in rock samples throughout the area. These claims were allowed to lapse on March 16, 2000. It is in this area that Aurora focused its exploration program in 2001.

5 REGIONAL GEOLOGY

The Hyland River area in southeastern Yukon is at the southern limit of the Selwyn Basin, just north of the Kechika Basin. The southern part of the Selwyn Basin is underlain from bottom to top by: Upper Proterozoic to Cambrian Hyland Group; Upper Proterozoic to Paleozoic Gog Assemblage; Upper Cambrian Rabbitkettle Formation of the Rocky Mountain Assemblage; and Devonian to Mississippian Earn Assemblage.

The Hyland Group is divided into two formations: the lower Yusezyu Formation and the upper, Narchilla Formation. The Yusezyu Formation is up to 3,000 m thick and is dominated by coarse-grained clastic rocks with interbedded shale and minor limestone. The upper part of formation is variably calcareous and in many places is capped by a fine grained, light to dark gray limestone member.

The Narchilla Formation conformably overlies the Yusezyu Formation and has been divided into three members. The lowest member is up to 300 m thick and consists of blue-gray to green weathering slate, commonly laminated. The middle member is thin to thick bedded, fine-grained quartz sandstone and siltstone about 70 m thick. The upper member is more than 400 m thick and consists mainly of blue-gray slate, which, in its upper part, weathers to apple green. The strata of the Hyland Group can be traced southward into the northern Rocky Mountains as far as the Gataga River area.

The base of the Gog Assemblage is marked by carbonate rocks of the Risky Formation. This formation occurs a short distance below the base of the Cambrian and is tentatively correlated with the carbonate at the top of the Yusezyu Formation (Gabrielse, et. al., 1992). In the Hyland River area, the Risky Formation is overlain by the Vampire Formation, also of the Gog Assemblage. The Vampire Formation is comprised of dark gray siltstone and shale interbedded with light brown, very fine grained quartzite. Abundant slump folds suggest a slope environment.

The Rabbitkettle Formation is up to 1200 m thick and is comprised of craton-derived, dark gray and black, non-calcareous argillite, slate and phyllite, buff and gray calcareous, phyllitic limestone, phyllite and slate and minor wavy-banded silty limestone.

The capping rocks of the Selwyn Basin in southeast Yukon are of the Earn Group. They are thin bedded, laminated slate with thin to thickly interbedded fine to medium grained chert-quartz arenite and wacke, thick members of chert pebble conglomerate, black siliceous siltstone, nodular and bedded barite and rare limestone.

The rocks exhibit low-grade regional metamorphism. The strata are generally flat lying to shallowly dipping with local undulations due to gentle folding. Faulting in the area is dominated by two structures, a low angle fault on the east side of the prospect (the Green River Fault), dipping to the west, and a normal fault to the west with west side down.

Intrusive rocks in the Hyland River area occur mainly to the north and west. They are Mid Cretaceous quartz monzonite, granodiorite, quartz-diorite and syenite of the Mt Billins Batholith.

6 HYLAND RIVER PROSPECT GEOLOGY

Much of the bedrock in the area is overlain by unconsolidated glacial and glacio-alluvial deposits, which can be up to 50 m in the Hyland River valley floor. The glacial cover decreases up slope. Outcrops are scarce on mountain slopes, however on the mountain tops the cover is much thinner and outcrop is more evident. Hence, the detailed geology of the area is poorly understood. Most local mapping has been confined to canyon walls in deeply incised creek valleys and on mountain tops.

The area is underlain by Hyland Group sediments consisting of green and purplish, gray to maroon phyllite, coarse quartz and feldspar grit, shale and limestone, probably of the Narchilla Formation. These rocks have been subject to low grade regional metamorphism and have been intruded by numerous, randomly oriented, quartz feldspar porphyry dykes of probable Cretaceous age.

7 2001 WORK PROGRAM

The 2001 work program on the Hyland Prospect consisted of following-up anomalous rock and soil results from Westmin's 1995 work in the area to determine the source of the anomalies. The program was completed in 2 phases; the first phase consisted of prospecting, soil sampling, trenching at Trench #1 and staking of 42 quartz claims; the second phase consisted of prospecting, trenching at Trench #2 and stream sediment sampling.

In most instances, the follow-up of the 1995 anomalies was hampered by the inability to find old sample flags and the lack of outcrop. It was decided to follow-up the anomalies with detailed soil sampling to better define the anomaly and to allow for a more focused trenching program.

Detailed soil lines were run over four anomalous soil areas from the 1995 survey. The samples were collected at 10 or 20 m intervals. Soil sample lines are shown on Figure 6 with lines from the 1995 survey. The 2001 soil results were combined with Westmin's 1995 soil data to generate plots for lead, zinc, cadmium and silver (Figures 7 to 10).

Two trenches were dug on lead soil anomalies to determine the source of the lead in soils. The trenching involved digging a series of pits approximately 1 m wide, by 2 to 3 m long along the slope and up to 3 m deep to expose bedrock. At Trench #1, 3 pits were dug (Figure 4); at Trench #2, 4 pits were dug (Figure 5). Two rock samples were collected from the pits at Trench #1 (ZAP01-001, 002) and one sample of clayey overburden (ZAP01-003). From the pits at Trench #2 soil profile samples were collected from each of the different soil horizons (generally 4 samples per pit) and a sample of bedrock at the bottom of each pit (ZAP01-005 to ZAP01-008). Rock and trench sample descriptions are included in Appendix II.

Stream sediment samples were collected at 200 m intervals on the stream draining the area of the two trenches (Figure 3) to determine the down-stream dispersion pattern of the base and precious metals.

All soil, stream sediment and rock samples were air dried in camp prior to shipping to Acme Analytical Labs in Vancouver for processing. The sample processing for soil and stream sediment samples consisted of further drying at the lab and sieving to -80 mesh. One gram of -80 mesh material was then analyzed for 35 elements (including gold and silver) by aqua regia digestion and Inductively Coupled Plasma emission spectroscopy (ICP). The sample processing for rock samples involved crushing to 70% at -10 mesh and pulverizing 100 gm to -230 mesh. A 1 gm sample of the pulverized material was then analyzed by aqua regia and ICP analysis as for the soil and stream sediment samples. The geochemical analytical certificates are included in Appendix III.

8 RESULTS

The detailed soil sample program corroborated the anomalous Pb-Zn-Cd and Ag zones on the property and helped define the anomalous pattern. An interesting feature of the anomalous pattern is that the highly anomalous areas occur in deeply incised creek valleys at roughly the same elevation, between 3,600 and 4,200 feet (see Figures 7 to 10). This anomalous pattern indicates two features: first, where the creeks cut through the overburden they expose a Pb, Zn, Cd, Ag-rich horizon; second, because the anomalies are occurring at roughly the same elevation around the mountain, this horizon is probably relatively flat lying.

The trenches were dug to test one of these anomalies on the west side of line 250 S. Trench #1 reached broken shaley bedrock, but failed to identify the source of the anomalous Pb-Zn-Cd-Ag in soil. Trench #2 was dug 50 m east of Trench #1. It encountered similar broken shale and also failed to identify the source of the soil anomalies. However, soil profiles from the four pits at Trench #2 identified anomalous Pb and Zn values in progressively lower soil horizons in the pits dug up slope. Thus, the source of the Pb-Zn-Cd-Ag anomaly is believed to be a short distance further up slope.

The stream sediment sampling program returned anomalous Pb-Zn-Cd-Ag-Ba results down stream of the soil anomaly on line 250 S. The anomalies for all elements, with the exception of barium, generally decrease at a fairly regular interval down stream. This pattern corroborates the source of the anomaly to be near the are of trenching.

9 CONCLUSIONS AND RECOMMENDATIONS

The soil sampling, stream sediment sampling and trenching program on the Hyland River Project confirmed the anomalous Pb-Zn-Cd-Ag-Ba values in the area and helped to better define soil anomalies from previous work. The trenches, however failed to locate the source of the anomalous Pb-Zn-Cd-Ag mineralization.

Recommendations for future work on the property are to conduct:

- 1) More detailed soil sampling across the slope in other drainages to test the theory of a mineralized horizon being cut by creeks.
- 2) Extending the trenches up slope to look for the source of the anomalous values.
- 3) A gravity survey across the mountain to determine if there is a buried SEDEX horizon, which may not be readily exposed by trenching.

Respectfully Submitted,

Scott Casselman, B.Sc., P.Geo.

10 REFERENCES

- Buchholz, J., 1968. Summary Report, Redfort Project, Fort Reliance Minerals Ltd., Yukon Assessment Report 092566.
- Crowhurst, J. J., 1969. Report on McMillan Property, Watson Lake Area, Yukon Territory, Yukon Assessment Report 092568.
- Gabrielse, H., Yorath, C. J., 1992. Geology of the Cordilleran Orogen in Canada, Geological Survey of Canada Publication, Geology of Canada no. 4.
- Geological Survey of Canada, 1968. Geology of the Coal River Map Sheet, Yukon Territory, Geological Survey of Canada, Map 11-1968.
- Geological Survey of Canada, 1966. Geology of the Watson Lake Map Sheet, Yukon Territory, Geological Survey of Canada, Map 19-1966.
- Geological Survey of Canada, 1995. Regional Stream Sediment and Water geochemical Reconnaissance Data, Southeastern Yukon, NTS 95D and 105A, Geological Survey of Canada, Open File 3293.
- Geological Survey of Canada, 1993. Regional Stream Lake Sediment and Water geochemical Reconnaissance Data, Southeastern Yukon, NTS 105A, Geological Survey of Canada, Open File 2860.
- Geological Survey of Canada, 1978. Regional Stream Sediment and Water geochemical Reconnaissance Data, Southeastern Yukon, NTS 105B, Geological Survey of Canada, Open File 1289.
- Pawliuk, D. J., 1996. 1995 Assessment Report, Spook Property. Yukon Assessment Report 093467.
- Perkins, D. A. and Mustard, J. W., 1981. Geochemical Soil Sampling and Line cutting on the SF, GS, HY Claims, Watson Lake Mining District, Yukon. Yukon Assessment Report 090893.
- Stroshein, R., 1979. Assessment Report of Geochemical Survey on GUM Claims. Yukon Assessment Report 090480.

11 STATEMENT OF EXPENDITURES

Phase 1 (costs incurred before recording of claims)

Wages	S. Casselman	6,650.00	
	P. Malacarne	2,850.00	
	B. Stirling	175.00	
Helicopter Charter (4.8 hrs @ \$ 1013.18)		4,863.27	
Camp equipment rental (19 days @ \$50/day)		950.00	
Vehicle rental (3 days @ \$75/day)		225.00	
Fuel		238.73	
Supplies		4.82	
Groceries		857.30	
Maps/Publications/Photocopies		132.21	
Communication		<u>393.45</u>	
Total Phase 1		<u>17,339.78</u>	17,339

Phase 2 (costs incurred after recording of claims)

Wages	S. Casselman (11 days @ \$350)	3,850.00	
	P. Malacarne (11 days @ \$150)	1,650.00	
Helicopter Charter (4.8 hrs @ \$ 1013.18)		1,823.73	
Camp equipment rental (11 days @ \$50/day)		550.00	
Vehicle rental (2 days @ \$75/day)		150.00	
Fuel		150.80	
Supplies		32.95	
Groceries		431.66	
Maps/Publications/Photocopies		143.74	
Communication		120.00	
Freight		171.73	
Analytical costs		2,848.55	
Expediting		40.00	
Report Writing and reproduction costs		<u>2,500.00</u>	
Total Phase 2		<u>14,463.16</u>	14,463.16
Project Total			<u>32,267.94</u>

STATEMENT OF QUALIFICATIONS

I, Scott Casselman, residing at 33 Firth Road, Whitehorse, Yukon Territory, Y1A 4R5, certify that:

- 1) I graduated from Carleton University, Ottawa, Ontario, with a Bachelor of Science Degree in Geology in 1985.
- 2) I have practised the profession of geology since graduation and that I am a currently employed by Aurora Geosciences Ltd.
- 3) I am a member of the Association of Professional Engineers and Geoscientists of British Columbia, Registration No. 20032.
- 4) I conducted the field program on the Hyland River Property described in this report.

Dated this ___th day of _____, 2002, at Whitehorse, Yukon Territory.

Scott G. Casselman, B.Sc., P.Geo.

APPENDIX I

DAILY LOG

Hyland River Project

Field Log (2001)

- Crew Project Geologist - Scott Casselman
 Field Assistant - Peter Malacarne
- July 9 Organize, prepare and pack field gear at warehouse.
- July 10 Organize maps in office, purchase food and necessary gear from Whitehorse
- July 11 Pick-up old reports from library, load gear for departure next morning.
- July 12 Travel to Watson Lake, purchase groceries, Helicopter to site and set-up camp. Clear and warm in evening.
- July 13 Sunny throughout day. Complete camp set-up in am. Organize field equip and maps and do local traverse
- July 14 Clear in am, starts raining at 2:30 pm, rains through night. Prospecting traverse west of camp to look for anomalous sample #95DPR374 from 1995 Westmin program. Locate 1995 soil survey lines (station marking generally legible), unable to locate old sample.
- July 15 Pouring rain in am, slows by 1:00 pm. Prospecting traverse on 1995 soil grid to check out anomalous soil results on Line 1000 S and 750 S. Re-establish lines by flagging and re-marking station tags. Minor outcrop observed – mainly dark gray shale with abundant quartz veining. Unable to determine cause of soil anomalies.
- July 16 Overcast in am, clearing in pm. Decide to dig test pits at site of highly anomalous Pb in soils at L250 S / 2350 W (700 ppm Pb). Dig 3 pits, Pit 1 at 7 m below sample site, pit 2 at sample site and pit 3 at approx 10 m above sample site. Encounter dark gray, fissile shale at depth of 2.0 m in pit 1 and pit 2 – no sulphides evident.
- July 17 Overcast in am, raining in pm. Continue digging on pit 3 at L250 S / 2350 W. At depth of 0.7 m encounter very hard-packed, partially frozen clay layer with shale fragments – very difficult digging. Wet clay oozes down slope and begins burying lower pits.
- July 18 Rains off and on throughout day. Continue to work on pit 3 – not much success in wet weather. Clay continues to ooze into pits 1 and 2. Decide to abort pitting and sample material that's exposed. Sample shale at bottom of pits 1 and 2, and clay at top of pit 3.
- July 19 Overcast in am, clearing through day. Lay out detailed soil sample program (10 to 20 m sample spacing) to delineate anomalies from 1995 program. Soil sample Line 2500 W from 200S to 740 S and L 2300 W from 200S to 400S.
- July 20 Clear and sunny through day. Prospect southwest of camp (L1000 S). Stake claims in SW corner of 1995 grid along old claim line. Stake ZAP 1 and 2 claims.
- July 21 Clear, sunny and very hot. Peter continues staking and prospecting along SW line. Stakes ZAP 3, 4, 5 and 6. Scott looks for claim line 914 m east of Peters line and stakes ZAP 23, 24, 25, 26.
- July 22 Clear and warm. Camp day, organize samples to send out. Helicopter in with groceries at 10:30 am, samples out. Helicopter in again at 4:30 pm for visit while in area.
- July 23 Clear and warm through day. Continue staking and prospecting to north. Peter stakes ZAP 7 to 12, Scott stakes ZAP 27 to 40. Locate a number of cut and blazed lines running roughly E-W.
- July 24 Clear in am, clouding over in pm. Finish staking – Peter does ZAP 13 to 20, Scott does ZAP 41 to 44.

- July 25 Partially overcast in am, clears through day. Write-up claim forms in am. Continue soil sampling on L 2300 W from 750 S to 600 S, L 600 S from 2300 W to 2700 W and L 2100 W from 200 S to 350 S.
- July 26 Clear in am, partially cloudy in pm. Soil sample line 2500 W from 750 S to 1200 S and L 2300 W from 750 S to 1100 S.
- July 27 Clear sunny and hot. Soil sampling in SE part of 1995 grid. Run lines 900 S and 1100 S from 800 W to 1500 W.
- July 28 Clear and sunny. Peter runs soil line 700 S from 800 W to 1500 W, Scott prospects and locates baseline and GPS coordinates for 0 W / 1000 S, 0 W / 0 N and 0 S / 1500 W.
- July 29 Overcast through day. Soil sample to northwest on lines 2100 W from 800 N to 300 N and L 2300 W from 860 N to 300 N.
- July 30 Clear and warm. Demob to Watson Lake and drive to Whitehorse for break. Ship samples for analysis. Leave camp in for return and follow-up in late August.
- July 31 to August 30 – On break
- Aug 31 Peter and Scott drive to Watson Lake and mobilize to Hyland camp. Set-up camp in evening and prepare for fieldwork next day.
- Sept 1 Clear in am, clouds over through day. Go to site of anomalous soils at L 2300 W , 240 to 270 S. Dig pits to locate source of anomaly.
- Sept 2 Partially cloudy through day. Continue digging pits at L 2300 W / 270 S. Pit 4 at 265 S, Pit 5 at 270 S. Hit bedrock in Pit 4 at 3.0 m and Pit 5 at 2.5 m.
- Sept 3 Partially cloudy and cool. Continue pitting on pits 4 and 5.
- Sept 4 Rainy in am, clears through day. Sample pits 4 and 5 with 1 rock sample each and 4 soil samples each at each different horizon. Start on Pits 6 and 7 at 275 and 280 S, respectively.
- Sept 5 Partially cloudy minor showers through day. Continue digging on pits 6 and 7.
- Sept 6 Partially cloudy, windy and cool. Prospect and survey in old grid points to coordinate old soil data with new data.
- Sept 7 Overcast and cool. Organize and pack dried samples. Generator break down in am – attempt to fix with no luck.
- Sept 8 Overcast and cool, minor rain. Finish pitting on pit 6 and 7. Sample pits with one rock sample at base of each pit and 9 soil samples of various horizons. No sulphide mineralization found in any of pits 4 through 7. Highly anomalous Pb in soils not explained.
- Sept 9 Overcast and cool with showers in afternoon. Traverse west of camp down creek to 2500 ft elevation. Stream sediment sample up creek at 200 m sample intervals (10 samples). Lots of outcrop evident at lower elevations along creek – mainly dark gray shale with qtz veins.
- Sept 10 High overcast in am with ice on standing water. Helicopter arrives at 12:30. Demob all gear to Watson Lake and drive to Whitehorse.

End of Field Program.

APPENDIX II

SAMPLE DESCRIPTIONS

Rock Sample Descriptions

Sample #	Grid N	Grid E	UTM E (NAD 27)	UTM N (NAD 27)	Comments
ZAP01-001	-250	-2350	550416	6686166	Sample from bottom of pit (3 m) in Trench #1. Fissile black shale from crumbly subcrop with grey clay beds. Has 3 cm qtz vein with minor FeOx on fractures.
ZAP01-002	-253	-2350	550416	6686163	Sample from bottom of pit in Trench #1, 3 m upslope from ZAP01-001. Fissile black shale from crumbly outcrop.
ZAP01-003	-258	-2350	550416	6686158	Sample of clayey-shaley layer (50 cm deep) from Trench #1, 3 m upslope from ZAP01-002. Grey clay soil with shale fragments (not outcrop). Hard packed clay with up to 40% dark grey to black shale fragments. Some felsic dyke fragments and quartz pebbles in clay.
ZAP01-004	-900	-840	552090.4	6686118.9	From soil sample hole. Grey sandstone/siltstone with up to 3% very fine-grained disseminated pyrrhotite. Slightly magnetic, very dense. May be slightly silicified.
ZAP01-005	-270	-2300	550467.6	6686189	Sample from bottom of pit in Trench # 2. Rubbly black shale outcrop with micaceous mineral partings. Very hard and siliceous, minor quartz veins cross cutting bedding with white clay mineral in occasional vein. Very fissile with minor FeOx on fractures. No sulphides evident. Bedding strikes 160, dips 14 west.
ZAP01-006	-265	-2300	550468	6686194	Sample from bottom of pit in Trench # 2, 5 m north of ZAP01-005. Dark grey, slightly crenulated shale with steeply dipping quartz veins striking 60 deg and dipping to south. Very platy and fissile. Much softer with very fine grained micaceous minerals and not as siliceous as ZAP01-005. Bedding strikes 220 and dips 24 to NW.
ZAP01-007	-280	-2300	550467	6686179	Sample from bottom of pit in Trench # 2, 10 m south of ZAP01-005. Dark grey, slightly crenulated shale.
ZAP01-008	-285	-2300	550467	6686174	Sample from bottom of pit in Trench # 2, 5 m south of ZAP01-007. Dark grey, slightly crenulated shale.
ZAP01-009					

Trench Sample Description

Sample #	Grid N	Grid E	UTM E (NAD 27)	UTM N (NAD 27)	Depth (m)	Comments
TR-001	-270	-2300	550467.6	6686189	20 to 50 cm	Re-sample of "B-horizon" material. Orange, sandy, bouldery clay with clasts of shale and shale with quartz veins (with FeOx) and rare, rounded cobbles of granitic rock.
TR-002	-270	-2300	550467.6	6686189	50 to 120 cm	Light grey clay layer with up to 30% clasts (5 to 60 mm) of shale, quartz and occasional granitic clast.
TR-003	-270	-2300	550467.6	6686189	120 to 190 cm	Mixed, interbedded fine shale fragment layers and clay layers. Shale layers to 7 cm thick; clay layers to 10 cm thick.
TR-004	-270	-2300	550467.6	6686189	190 to 260 cm	Tan to grey clay layer with 70% clay and 30% shale clasts (to 5 mm). Rare to no granitic clasts.
TR-005	-265	-2300	550468	6686194	20 to 50 cm	"B-horizon" material.
TR-006	-265	-2300	550468	6686194	50 to 150 cm	Grey clay layer with up to 30% clasts of shale (5 to 60 mm), quartz and occasional granitic clast.
TR-007	-265	-2300	550468	6686194	150 to 250 cm	Mixed, interbedded fine shale fragment layers and clay layers. Shale layers to 7 cm thick; clay layers to 10 cm thick.
TR-008	-265	-2300	550468	6686194	250 to 350 cm	Tan to grey clay layer with 70% clay and 30% shale clasts (to 5 mm). Rare to no granitic clasts.
TR-009	-280	-2300	550467	6686179	20 to 50 cm	"B-horizon" material.
TR-010	-280	-2300	550467	6686179	50 to 120 cm	Grey clay layer with up to 30% clasts of shale (5 to 60 mm), quartz and occasional granitic clast.
TR-011	-280	-2300	550467	6686179	120 to 190 cm	Mixed, interbedded fine shale fragment layers and clay layers. Shale layers to 7 cm thick; clay layers to 10 cm thick.
TR-012	-280	-2300	550467	6686179	190 to 240 cm	Tan to grey clay layer with 70% clay and 30% shale clasts (to 5 mm). Rare to no granitic clasts.
TR-013	-280	-2300	550467	6686179	240 to 290 cm	Predominantly shale layer with lessor clay.
TR-014	-285	-2300	550467	6686174	20 to 50 cm	"B-horizon" material.

Sample #	Grid N	Grid E	UTM E (NAD 27)	UTM N (NAD 27)	Depth (m)	Comments
TR-015	-285	-2300	550467	6686174	50 to 120 cm	Grey clay layer with up to 30% clasts (5 to 60 mm) of shale, quartz and occasional granitic clast.
TR-016	-285	-2300	550467	6686174	120 to 190 cm	Mixed, interbedded fine shale fragment layers and clay layers. Shale layers to 7 cm thick; clay layers to 10 cm thick.
TR-017	-285	-2300	550467	6686174	190 to 240 cm	Predominantly shale layer with lessor clay.

Silt Sample Location

Sample #	UTM E (NAD 27)	UTM N (NAD 27)	Elevation (ft)
SLT01-001	548768	6685320	2890
SLT01-002	548964	6685297	2948
SLT01-003	549161	6685329	2990
SLT01-004	549355	6685330	3033
SLT01-005	549501	6685447	3096
SLT01-006	549640	6685570	3162
SLT01-007	549747	6685710	3279
SLT01-008	549743	6685705	3387
SLT01-009	549990	6686004	3444
SLT01-010	550166	6686074	3528

APPENDIX III

GEOCHEMICAL ANALYTICAL CERTIFICATES

GEOCHEMICAL ANALYSIS CERTIFICATE



Aurora Geosciences Ltd. PROJECT Hyland R. File # A102662
P.O. Box 31097, 11 & 12 -, Whitehorse YT Y1A 5P7 Submitted by: Scott Casselman

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm
ZAP01-001	13.8	139	222	437	2.0	47	4	401	2.96	56	9	<2	6	173	5.5	3.3	<.5	386	.56	.274	12	91	.26	553	.089	2	1.14	.024	.27	1	<1	2.9	2	.22	5
ZAP01-002	22.8	48	61	183	1.7	16	1	88	1.24	29	10	<2	5	130	3.1	4.1	<.5	255	.33	.175	14	37	.10	1466	.079	6	.78	.015	.21	1	<1	2.0	<1	.09	3
ZAP01-003	13.6	91	136	353	1.3	46	5	486	1.63	36	9	<2	4	112	4.7	5.0	<.5	438	.55	.227	18	81	.25	1916	.077	8	1.03	.011	.19	2	<1	2.9	<1	.08	4
ZAP01-004	3.0	33	9	39	.2	36	16	145	3.29	3	<1	<2	3	153	1.2	<.5	<.5	36	1.46	.172	11	62	.26	82	.163	1	2.04	.150	.12	1	1	2.3	1	1.20	6
RE ZAP01-004	2.9	34	9	40	.2	37	17	148	3.35	3	1	<2	4	155	1.3	.5	<.5	36	1.48	.176	12	63	.27	82	.165	<1	2.07	.153	.12	1	<1	2.4	<1	1.22	6
STANDARD C3	25.8	67	33	171	5.8	35	11	796	3.39	64	23	2	20	26	24.7	14.6	22.9	80	.56	.085	18	168	.59	145	.085	17	1.81	.033	.15	14	1	4.2	3	.02	8
STANDARD G-2	1.5	3	2	42	<.1	7	4	542	1.97	<1	3	<2	4	65	<.2	<.5	<.5	40	.63	.092	7	73	.58	203	.127	<1	.93	.066	.45	2	<1	2.4	1	<.02	5

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY OPTIMA ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 10 2001 DATE REPORT MAILED: *Aug 21/01* SIGNED BY: *C.L.* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Aurora Geosciences Ltd. PROJECT Hyland R. File # A102663 Page 1

P.O. Box 31097, 11 & 12 -, Whitehorse YT Y1A 5P7 Submitted by: Scott Casselman



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm
2500W 200S	11.5	204	191	2751	3.3	219	5	515	2.62	50	23	<2	2	94	45.3	4.6	.8	725	.94	.154	25	95	.54	2775	.056	5	2.00	.010	.15	1	<1	3.6	<1	.09	5
2500W 210S	22.3	66	229	378	1.0	48	4	288	2.78	47	5	<2	5	79	3.0	4.7	.5	534	.25	.154	24	45	.25	1432	.095	2	1.05	.011	.14	1	<1	2.2	<1	.13	5
2500W 220S	19.4	85	174	530	1.6	69	5	341	2.88	47	8	<2	4	89	7.9	4.2	.6	476	.38	.164	25	55	.40	3418	.097	4	1.59	.007	.16	1	<1	2.9	<1	.08	6
2500W 230S	18.9	68	146	407	.8	55	5	342	2.71	49	6	<2	4	87	3.8	4.4	.5	452	.40	.167	21	47	.36	3117	.085	3	1.29	.010	.12	1	<1	2.3	<1	.11	4
2500W 240S	19.4	54	177	311	2.0	37	2	151	1.91	31	4	<2	3	68	4.1	3.1	.5	332	.19	.101	22	35	.15	2474	.075	1	1.06	.008	.12	<1	<1	1.8	<1	.10	5
2500W 250S	23.4	87	216	405	.7	54	9	671	3.23	60	7	<2	6	99	3.2	5.6	.6	558	.30	.203	25	47	.33	1506	.099	4	1.33	.013	.15	1	<1	3.0	<1	.14	4
2500W 260S	19.4	65	276	367	.9	50	3	275	3.04	50	5	<2	5	70	1.8	4.5	.7	585	.25	.187	24	51	.29	1058	.093	2	1.25	.005	.10	1	<1	2.1	<1	.11	5
2500W 270S	15.5	55	199	353	1.2	48	4	284	2.89	41	4	<2	5	54	1.7	3.3	<.5	452	.24	.160	21	54	.33	996	.076	2	1.32	.006	.10	1	<1	2.5	<1	.08	6
2500W 280S	13.6	52	187	308	.4	41	3	210	2.27	35	3	<2	4	44	1.4	3.0	<.5	372	.15	.098	20	41	.25	871	.069	3	1.10	.007	.08	1	<1	2.5	<1	.07	5
2500W 290S	23.5	169	214	840	1.3	111	10	576	3.62	98	11	<2	7	120	5.0	5.8	.5	1083	.69	.301	24	101	.42	4176	.120	3	2.03	.012	.18	1	<1	4.5	<1	.10	6
2500W 300S	33.3	112	216	478	2.2	95	6	354	2.80	97	12	<2	8	98	3.8	8.8	<.5	1156	.37	.150	27	83	.37	2984	.170	5	1.68	.010	.17	1	<1	3.4	1	.08	6
2500W 310S	24.3	140	362	665	.9	94	10	796	3.46	76	10	<2	8	114	4.3	6.2	.6	952	.47	.262	28	88	.41	3928	.117	3	1.84	.008	.15	1	<1	4.2	<1	.08	6
2500W 320S	14.0	92	223	424	1.3	69	7	396	3.08	40	6	<2	7	69	3.3	3.5	.5	452	.26	.196	23	57	.38	1572	.084	2	1.81	.007	.11	1	<1	3.2	<1	.06	5
2500W 330S	10.5	53	183	276	1.4	45	4	253	3.20	32	4	<2	6	47	1.6	2.7	<.5	338	.18	.243	18	47	.34	1008	.058	3	1.51	.006	.10	1	<1	2.4	<1	.07	5
2500W 340S	11.7	44	154	210	.9	30	3	170	2.60	30	3	<2	5	47	1.2	2.8	<.5	246	.10	.143	20	32	.25	887	.073	<1	1.17	.007	.10	1	<1	2.1	<1	.10	5
RE 2500W 340S	12.4	45	156	209	.9	30	3	175	2.73	30	3	<2	5	48	1.5	2.8	.5	249	.09	.144	20	32	.23	912	.076	2	1.18	.006	.11	1	<1	2.2	<1	.10	5
2500W 350S	11.8	31	143	169	1.0	24	2	123	2.58	26	2	<2	5	39	.8	2.5	<.5	231	.07	.130	18	30	.18	772	.082	3	.99	.007	.10	<1	<1	1.9	<1	.10	5
2500W 360S	12.2	44	164	221	.7	34	3	197	2.74	30	3	<2	4	50	1.5	2.6	.5	253	.12	.149	20	36	.26	965	.070	2	1.23	.006	.09	1	<1	2.1	<1	.09	5
2500W 370S	16.3	82	234	276	.9	45	5	297	2.93	30	7	<2	6	76	2.4	3.0	.7	341	.21	.243	23	44	.27	2439	.067	2	1.76	.007	.11	1	<1	3.0	<1	.12	5
2500W 380S	14.8	81	215	342	1.0	53	4	315	2.83	34	5	<2	6	83	1.9	3.3	.6	301	.24	.178	22	39	.36	2122	.083	3	1.43	.008	.12	1	<1	2.6	<1	.12	4
2500W 390S	13.9	54	206	260	1.2	43	6	262	3.08	31	4	<2	7	46	1.4	3.0	.5	253	.12	.183	19	42	.36	774	.061	<1	1.77	.004	.09	1	<1	2.7	<1	.07	4
2500W 400S	14.1	28	188	142	.7	17	2	87	1.37	15	2	<2	4	35	.8	1.9	.9	175	.06	.086	16	21	.10	475	.075	3	.71	.005	.06	<1	<1	1.4	<1	.04	6
2500W 420S	7.2	22	55	108	3.1	16	4	150	2.20	12	2	<2	6	10	.9	1.0	<.5	148	.05	.134	18	34	.29	510	.035	1	1.81	.003	.05	1	<1	2.4	<1	<.02	5
2500W 440S	15.3	56	158	258	3.5	47	5	217	3.00	30	6	<2	6	37	1.3	3.2	.5	445	.11	.240	18	61	.33	982	.060	1	1.98	.005	.10	1	<1	2.9	<1	.07	5
2500W 500S	4.2	14	29	97	1.1	20	5	173	2.32	11	2	<2	7	10	.6	1.0	<.5	93	.05	.098	18	34	.34	347	.046	1	1.57	.005	.05	<1	<1	2.7	<1	<.02	5
2500W 520S	3.4	18	32	98	1.6	16	4	131	2.45	13	1	<2	6	11	.6	.9	<.5	127	.05	.125	16	36	.27	412	.034	2	1.67	.004	.05	<1	<1	2.5	<1	.03	5
2500W 540S	6.2	34	58	172	.9	31	5	192	2.42	20	2	<2	6	23	1.0	1.8	<.5	138	.08	.121	18	35	.36	635	.056	2	1.46	.006	.08	<1	<1	2.2	<1	.02	4
2500W 560S	7.8	28	86	168	.5	26	4	204	3.23	23	2	<2	6	115	1.1	1.6	<.5	193	.09	.223	19	38	.29	686	.050	<1	1.32	.006	.08	<1	<1	2.2	<1	.07	5
2500W 580S	2.9	11	26	75	2.0	10	4	120	1.62	7	1	<2	5	7	.8	<.5	<.5	67	.06	.095	19	28	.22	345	.037	<1	1.39	.004	.04	<1	<1	2.4	<1	<.02	5
2500W 600S	3.8	9	50	48	.6	8	2	84	1.42	10	1	<2	6	10	.5	.5	<.5	92	.04	.098	20	22	.13	281	.036	2	1.06	.003	.04	<1	<1	2.1	<1	<.02	6
2500W 620S	3.0	21	28	88	2.5	11	3	105	1.42	5	1	<2	4	7	.6	<.5	<.5	68	.06	.077	19	25	.23	571	.038	<1	1.43	.004	.04	<1	<1	2.1	<1	<.02	6
2500W 640S	6.1	18	73	119	.3	19	4	148	3.15	19	2	<2	6	13	.6	.8	<.5	151	.09	.235	16	35	.34	488	.030	<1	1.80	.003	.07	<1	<1	2.4	<1	.02	6
2500W 660S	6.8	39	87	208	9.2	21	5	164	2.59	14	3	<2	7	9	1.6	1.6	<.5	182	.06	.156	17	51	.35	474	.056	3	2.29	.004	.06	<1	<1	3.1	<1	<.02	6
2500W 680S	8.3	26	101	170	1.0	24	4	174	2.68	19	2	<2	5	21	.8	1.3	<.5	135	.05	.120	18	33	.31	656	.048	1	1.42	.006	.07	<1	<1	2.1	<1	.07	5
STANDARD C3	26.8	65	37	165	5.5	38	12	823	3.27	57	20	<2	21	28	22.6	14.1	24.0	78	.56	.097	18	177	.60	147	.090	20	1.81	.034	.17	14	1	4.2	1	.03	8
STANDARD G-2	1.8	3	2	47	<.1	10	5	573	1.72	1	2	<2	5	72	<.2	<.5	<.5	42	.68	.111	8	81	.63	238	.141	1	1.01	.067	.60	2	<1	2.5	<1	<.02	5

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY OPTIMA ICP-ES.
 UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
 - SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 10 2001 DATE REPORT MAILED: Aug 22/01 SIGNED BY: *C. L. Toye* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data *KA* FA



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm
2500W 700S	6.0	29	71	362	2.6	29	7	174	2.60	19	4	<2	6	13	2.7	1.2	<.5	211	.10	.184	17	40	.33	763	.055	7	2.22	.005	.06	<1	<1	2.5	<1	<.02	6
2500W 720S	5.5	23	68	172	1.5	18	4	125	2.14	13	2	<2	5	11	1.9	.7	<.5	135	.07	.121	17	31	.23	547	.037	4	1.51	.004	.05	<1	<1	2.2	<1	<.02	6
2500W 740S	3.9	19	48	257	1.8	30	7	188	2.66	14	2	<2	7	11	1.9	.7	<.5	116	.11	.165	17	44	.38	555	.059	6	2.12	.006	.06	<1	<1	2.5	<1	<.02	5
2500W 760S	3.9	22	172	239	4.3	33	3	186	1.91	16	3	<2	5	37	2.4	1.4	.5	414	.30	.265	21	64	.23	625	.051	3	1.12	.004	.06	6	<1	2.1	<1	<.03	5
2500W 780S	5.9	29	476	410	1.3	53	4	376	2.05	17	4	<2	6	35	2.5	1.7	1.3	546	.34	.239	26	70	.35	601	.049	4	1.20	.004	.08	3	<1	2.4	<1	<.02	6
2500W 800S	9.6	51	245	508	1.9	70	4	341	2.20	25	4	<2	6	51	3.1	2.8	1.3	613	.35	.269	22	78	.34	845	.061	6	1.45	.004	.07	3	<1	2.5	<1	<.02	5
2500W 820S	4.8	11	93	281	1.2	21	7	600	2.34	11	1	<2	5	14	5.6	.7	<.5	162	.16	.207	18	35	.23	364	.039	3	1.23	.005	.06	1	<1	1.8	<1	<.02	6
2500W 840S	6.7	16	89	166	2.0	19	4	195	1.48	10	2	<2	5	18	2.0	1.3	.6	196	.08	.107	19	34	.15	662	.036	3	.94	.004	.05	1	<1	1.5	<1	<.02	5
2500W 860S	8.8	33	131	407	.9	47	6	350	2.42	21	3	<2	5	37	3.2	2.3	.9	401	.21	.178	21	55	.31	1198	.065	8	1.22	.004	.08	1	<1	2.3	<1	<.02	6
2500W 880S	6.6	31	86	265	1.2	38	6	222	2.10	16	2	<2	6	22	1.4	1.5	<.5	197	.18	.112	18	40	.34	843	.043	6	1.19	.004	.06	1	<1	2.0	<1	<.02	5
2500W 900S	6.0	19	92	230	.7	28	6	169	2.35	15	1	<2	5	17	2.4	1.2	<.5	192	.13	.122	18	38	.28	835	.039	5	1.32	.005	.06	1	<1	2.1	<1	<.02	5
2500W 920S	12.4	61	226	405	.7	54	4	250	2.24	31	5	<2	6	62	3.2	3.1	.5	454	.30	.172	22	53	.29	2979	.067	2	1.41	.006	.10	1	<1	2.6	<1	<.05	5
2500W 940S	15.1	56	243	383	.7	53	3	289	2.14	36	5	<2	5	71	2.3	3.4	.5	492	.29	.158	24	53	.25	2675	.069	4	1.22	.005	.11	1	<1	2.3	<1	<.06	5
2500W 960S	9.4	25	186	220	1.4	27	3	187	1.87	21	3	<2	5	37	3.2	2.1	<.5	319	.17	.118	20	38	.16	1586	.063	3	1.03	.006	.08	<1	<1	1.9	<1	<.04	5
2500W 980S	8.9	35	231	315	3.2	35	5	290	2.20	26	3	<2	5	44	4.5	2.2	.5	359	.25	.210	21	47	.20	1760	.065	4	1.13	.006	.09	1	<1	2.4	<1	<.03	5
RE 2500W 980S	8.7	34	224	321	3.1	35	5	290	2.29	26	3	<2	5	43	4.3	2.3	.5	360	.24	.209	21	49	.20	1771	.064	3	1.17	.005	.09	1	<1	2.4	<1	<.04	5
2500W 1000S	10.2	27	220	198	1.1	22	2	107	1.79	18	3	<2	5	35	2.9	2.2	.6	360	.12	.165	19	39	.09	777	.057	3	.91	.003	.06	<1	<1	1.6	<1	<.04	5
2500W 1020S	8.6	31	205	287	2.3	28	4	195	2.46	20	3	<2	5	36	4.1	2.0	.6	407	.18	.257	19	55	.17	1175	.084	4	1.36	.007	.06	1	<1	2.3	<1	<.03	7
2500W 1040S	13.8	61	425	394	1.4	56	3	282	2.42	29	6	<2	6	71	2.8	3.4	1.0	575	.39	.476	22	71	.26	2037	.073	12	1.53	.007	.09	1	<1	2.5	<1	<.07	5
2500W 1060S	11.9	77	328	705	2.6	75	4	470	1.70	28	8	<2	1	95	14.2	3.2	.6	439	.90	.156	20	56	.22	2531	.047	6	1.08	.007	.09	1	<1	1.8	<1	<.10	4
2500W 1080S	11.1	55	111	424	.5	64	6	226	2.79	24	4	<2	6	51	2.3	3.7	<.5	296	.22	.144	19	46	.36	1348	.068	3	1.48	.008	.08	2	<1	2.2	<1	<.05	4
2500W 1100S	5.9	20	46	234	.8	27	5	200	3.76	15	2	<2	6	20	1.0	1.6	<.5	131	.08	.108	16	45	.35	386	.062	<1	1.61	.005	.07	<1	<1	2.3	<1	<.04	6
2500W 1120S	9.4	43	41	425	1.2	58	6	209	2.28	22	3	<2	6	44	1.8	3.3	<.5	176	.23	.179	18	32	.32	755	.058	4	1.04	.007	.08	<1	<1	1.9	<1	<.06	4
2500W 1140S	10.9	132	221	2942	3.4	211	5	428	2.15	32	19	<2	1	102	48.2	4.2	.7	493	1.12	.209	24	75	.64	2804	.042	3	1.45	.007	.12	<1	<1	2.4	<1	<.12	5
2500W 1160S	13.0	121	172	2345	2.1	163	6	387	1.94	32	7	<2	3	99	29.0	5.6	.6	507	.77	.220	26	63	.52	3185	.067	3	1.16	.007	.12	3	<1	2.7	<1	<.08	4
2500W 1180S	14.9	120	78	857	4.7	123	9	542	2.63	41	5	<2	1	64	7.9	4.8	<.5	553	.59	.197	29	93	1.07	2088	.031	2	1.90	.005	.14	<1	<1	2.5	<1	<.06	6
2500W 1200S	11.4	64	62	426	1.4	67	9	436	2.15	32	3	<2	2	47	3.1	4.3	<.5	342	.41	.201	26	52	.82	1080	.048	6	1.36	.004	.09	1	<1	2.3	<1	<.05	5
2300W 860N	12.3	66	215	710	1.5	74	9	541	2.54	48	5	<2	5	70	4.5	5.0	<.5	527	.38	.164	22	66	.48	1878	.090	5	1.52	.007	.12	<1	<1	3.1	<1	<.08	6
2300W 840N	11.3	84	197	764	1.3	80	9	801	2.45	46	6	<2	4	75	13.2	5.1	<.5	510	.43	.156	24	64	.43	2404	.088	3	1.36	.008	.12	<1	<1	3.3	<1	<.11	5
2300W 820N	10.7	51	143	459	.7	60	5	287	2.82	54	3	<2	4	50	2.3	4.1	.5	427	.20	.136	21	60	.48	1477	.083	6	1.66	.005	.11	<1	<1	2.9	<1	<.07	6
2300W 800N	9.2	44	121	310	.3	40	3	160	2.06	42	3	<2	3	44	1.7	4.0	.5	340	.17	.085	20	41	.26	935	.084	4	1.16	.004	.09	<1	<1	2.1	<1	<.07	6
2300W 780N	10.7	54	153	472	.9	57	7	421	2.47	44	4	<2	5	64	3.6	4.5	.5	414	.32	.122	21	53	.37	1738	.095	6	1.24	.006	.10	<1	<1	2.7	<1	<.07	5
2300W 760N	11.4	54	152	390	.8	55	5	264	2.83	61	4	<2	5	55	2.4	5.5	<.5	494	.21	.136	22	58	.38	1501	.093	2	1.38	.005	.10	<1	<1	2.7	<1	<.11	6
2300W 740N	11.5	60	141	396	.5	52	5	322	2.45	50	4	<2	4	58	2.8	5.4	<.5	476	.26	.126	24	52	.38	2086	.084	2	1.38	.007	.11	<1	<1	2.9	<1	<.08	6
STANDARD C3	26.1	65	39	171	5.6	40	13	865	3.27	59	20	<2	22	28	23.3	14.2	24.2	81	.57	.103	19	184	.61	150	.090	22	1.86	.033	.16	15	1	4.4	1	<.04	8
STANDARD G-2	1.7	3	3	45	<.1	9	5	488	1.92	1	2	<2	5	68	<.2	<.5	<.5	41	.64	.106	8	85	.61	231	.128	4	.94	.067	.49	2	<1	2.2	<1	<.02	5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm
2300W 720N	12.9	58	188	462	1.3	60	5	327	2.69	51	5	<2	5	72	2.9	6.0	.5	555	.32	.172	28	55	.52	1877	.108	7	1.53	.007	.13	<1	<1	3.2	<1	.13	6
2300W 700N	13.1	68	122	383	.8	52	6	292	2.58	55	5	<2	6	68	2.6	6.9	<.5	520	.30	.143	27	46	.40	2108	.084	3	1.42	.007	.11	<1	<1	3.2	<1	.15	5
2300W 680N	12.1	61	144	383	.6	51	6	294	2.41	53	5	<2	6	67	2.5	6.3	<.5	478	.27	.146	26	43	.41	2107	.091	5	1.26	.006	.10	<1	<1	2.9	<1	.10	5
2300W 660N	12.2	67	145	417	1.1	57	8	407	2.42	52	5	<2	5	74	4.0	6.2	<.5	471	.36	.152	27	45	.43	2401	.085	9	1.27	.007	.12	<1	<1	2.8	<1	.10	5
2300W 640N	11.9	66	142	439	1.2	58	8	422	2.54	53	5	<2	6	69	3.7	5.4	<.5	506	.33	.133	26	48	.44	2355	.088	5	1.33	.007	.12	<1	<1	3.4	<1	.09	5
2300W 620N	10.6	68	142	475	1.2	60	9	478	2.42	48	5	<2	4	65	3.5	5.0	<.5	486	.32	.121	24	51	.49	2641	.075	6	1.47	.013	.13	<1	<1	3.4	<1	.10	5
2300W 600N	13.0	90	182	563	1.2	70	11	598	3.01	59	6	<2	4	70	6.5	5.9	<.5	564	.30	.125	28	62	.59	2883	.084	2	1.73	.009	.19	<1	<1	3.9	<1	.08	6
2300W 580N	10.9	103	163	1202	1.3	108	8	348	2.58	42	8	<2	8	99	13.4	5.1	.5	558	.65	.190	29	69	.52	2343	.102	5	1.36	.010	.13	1	<1	4.5	<1	.10	5
2300W 560N	11.8	77	156	707	.7	81	7	356	2.33	60	6	<2	5	88	3.4	8.0	<.5	647	.46	.188	25	66	.36	2131	.104	6	1.25	.006	.12	<1	<1	3.5	<1	.08	5
2300W 540N	11.9	67	228	649	.4	72	9	493	2.36	54	6	<2	7	88	3.2	6.8	.5	594	.46	.185	25	62	.43	2302	.115	5	1.41	.005	.12	1	<1	3.5	<1	.05	5
2300W 520N	13.7	154	312	1314	1.5	124	7	571	2.47	63	9	<2	5	109	23.1	7.0	.5	674	.68	.194	29	70	.46	3573	.103	8	1.38	.008	.18	1	<1	4.4	<1	.09	5
2300W 500N	14.7	71	412	605	.8	64	11	937	2.75	67	6	<2	6	77	4.6	6.6	.6	576	.35	.159	25	54	.43	1930	.127	3	1.24	.009	.14	<1	<1	3.6	<1	.10	5
2300W 480N	17.8	103	130	747	1.4	82	10	491	2.75	56	9	<2	6	104	9.2	4.8	<.5	584	.41	.179	29	60	.37	2001	.101	5	1.36	.015	.15	<1	<1	3.7	<1	.17	5
2300W 460N	18.8	91	139	787	1.8	90	10	432	2.67	66	8	<2	8	108	7.1	5.5	<.5	700	.42	.173	27	59	.38	1884	.092	8	1.40	.015	.13	<1	<1	3.5	<1	.16	5
2300W 440N	12.8	36	116	307	2.8	44	5	208	3.36	47	3	<2	7	46	1.3	3.5	<.5	484	.17	.188	21	54	.36	626	.071	5	1.55	.007	.09	<1	<1	2.8	<1	.07	6
2300W 420N	14.7	36	89	277	1.1	38	4	183	2.70	41	3	<2	4	53	1.5	3.8	<.5	431	.16	.140	22	45	.27	722	.069	3	1.20	.007	.09	<1	<1	2.3	<1	.12	6
2300W 400N	9.6	32	84	238	1.0	29	4	152	2.32	33	3	<2	6	30	1.2	2.3	<.5	430	.12	.111	23	46	.23	697	.064	2	1.33	.004	.07	<1	<1	2.4	<1	.06	7
RE 2300W 400N	10.1	32	84	240	1.0	29	4	146	2.26	34	3	<2	6	30	1.3	2.4	<.5	427	.10	.107	22	46	.22	690	.059	3	1.22	.003	.07	<1	<1	2.5	<1	.03	7
2300W 380N	7.4	49	93	499	1.9	56	6	265	2.46	35	3	<2	6	35	1.3	2.5	<.5	438	.22	.130	21	59	.44	708	.048	2	1.64	.004	.07	<1	<1	2.6	<1	.05	5
2300W 360N	6.9	20	78	225	1.1	33	5	201	3.06	31	2	<2	5	17	.8	2.0	<.5	343	.10	.134	17	50	.35	345	.036	4	1.45	.004	.05	1	<1	2.4	<1	.02	5
2300W 340N	7.3	16	41	144	2.0	24	3	137	3.45	27	1	<2	5	16	.6	2.2	<.5	320	.06	.124	16	38	.22	282	.059	2	.92	.002	.05	<1	<1	1.7	<1	.02	6
2300W 320N	4.2	14	38	124	1.0	20	3	120	2.43	21	1	<2	4	14	.5	1.5	<.5	156	.07	.093	17	33	.24	223	.041	4	1.07	.003	.04	<1	<1	2.0	<1	.05	6
2300W 300N	4.0	7	67	113	1.4	11	4	227	2.99	9	1	<2	9	8	.5	.6	<.5	144	.06	.064	21	38	.23	192	.138	1	1.44	.004	.03	<1	<1	1.9	<1	.03	9
2300W 200S	18.2	62	155	316	2.2	41	3	202	2.09	29	6	<2	2	59	3.4	3.2	.6	393	.22	.134	24	49	.25	2131	.073	3	1.20	.010	.10	<1	<1	2.0	<1	.16	6
2300W 210S	21.6	43	160	206	2.2	23	1	81	1.67	24	5	<2	2	69	1.4	4.8	.6	322	.10	.086	24	35	.11	1116	.079	2	.72	.008	.12	<1	<1	1.5	<1	.16	4
2300W 220S	23.1	79	182	416	1.4	48	4	250	3.19	56	7	<2	7	117	2.3	5.3	.6	585	.31	.247	22	50	.24	1534	.095	2	1.24	.013	.14	1	<1	2.7	<1	.19	5
2300W 230S	17.1	76	195	294	1.5	35	3	193	2.11	28	7	<2	3	61	3.5	3.4	.8	446	.18	.124	24	47	.17	2006	.073	4	1.06	.007	.09	1	<1	2.4	<1	.11	5
2300W 240S	24.3	75	135	610	1.4	83	6	959	2.74	44	7	<2	5	147	4.3	3.7	4.9	930	.48	.200	25	93	.36	2345	.097	3	1.32	.008	.10	7	<1	3.0	<1	.08	7
2300W 250S	44.9	96	3181	798	1.0	95	6	982	2.63	52	8	<2	6	202	5.1	4.2	9.2	1396	.49	.248	27	104	.38	1862	.083	3	1.57	.005	.10	14	<1	2.8	<1	.09	8
2300W 260S	37.7	106	2313	917	2.8	127	6	938	2.80	54	12	<2	7	163	5.6	4.7	5.7	1423	.61	.272	37	127	.51	3104	.096	7	1.76	.007	.12	9	<1	4.1	<1	.11	7
2300W 270S	42.9	111	2556	1074	3.9	183	21	2273	3.07	56	14	<2	8	186	6.7	4.9	5.4	1349	.79	.347	36	151	.65	2525	.106	5	1.92	.009	.12	17	<1	4.5	<1	.12	7
2300W 280S	15.5	55	390	364	.5	53	4	299	3.11	49	4	<2	6	61	2.0	3.2	.9	598	.27	.232	22	71	.29	880	.081	4	1.28	.006	.09	1	<1	2.3	<1	.08	6
2300W 290S	18.9	81	366	459	1.7	67	7	353	3.46	54	7	<2	8	74	2.9	4.2	.7	632	.29	.277	24	85	.33	1489	.082	3	1.94	.007	.09	1	<1	3.2	<1	.13	6
2300W 300S	12.6	55	364	381	1.6	50	6	286	3.05	40	4	<2	6	36	1.6	2.5	.5	466	.20	.211	20	70	.35	604	.056	4	1.70	.004	.07	1	<1	2.5	<1	.09	6
STANDARD C3	25.4	63	35	158	5.4	38	12	787	3.11	55	20	<2	22	29	22.6	14.5	24.1	76	.55	.095	19	166	.59	155	.084	18	1.65	.031	.16	14	1	4.2	1	.05	8
STANDARD G-2	1.7	3	3	48	<.1	8	5	493	2.00	1	2	<2	5	75	<.2	<.5	<.5	42	.72	.111	9	78	.63	243	.135	2	.94	.066	.53	2	<1	2.8	<1	.02	6

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	
2300W 310S	20.1	79	573	509	1.8	63	3	359	3.25	51	6	<2	6	69	2.5	4.0	1.0	680	.31	.316	22	87	.24	914	.077	4	1.59	.004	.09	3	<1	1.9	<1	.11	6
2300W 320S	18.6	53	282	265	2.5	35	3	214	2.83	31	5	<2	6	61	1.5	3.8	.8	517	.16	.249	20	47	.17	1360	.080	3	1.44	.008	.11	1	<1	2.1	<1	.15	6
2300W 330S	9.2	33	119	212	2.1	34	4	233	3.06	28	3	<2	6	29	.9	2.1	.5	435	.13	.247	19	53	.29	564	.053	2	1.56	.003	.07	1	<1	2.2	<1	.05	5
2300W 340S	8.5	26	117	146	1.3	22	3	173	2.67	21	2	<2	6	24	.8	1.6	.5	277	.04	.153	17	38	.20	536	.066	2	1.25	.004	.07	1	<1	1.6	<1	.06	6
2300W 350S	15.0	60	205	289	2.3	44	4	295	2.96	33	5	<2	7	62	1.8	3.7	.6	338	.15	.219	21	46	.27	1336	.086	2	1.70	.007	.11	1	<1	2.3	<1	.11	5
2300W 360S	15.9	131	444	714	1.4	142	5	993	2.66	46	11	<2	9	106	4.9	4.5	.6	1194	.67	.225	34	144	.48	2725	.153	4	1.85	.009	.12	2	<1	4.4	<1	.11	7
2300W 370S	9.4	26	141	145	1.0	20	3	149	2.61	21	2	<2	6	28	1.1	1.6	.5	208	.07	.163	18	29	.16	650	.046	1	1.19	.005	.06	1	<1	1.5	<1	.05	6
2300W 380S	21.1	60	820	412	2.1	59	5	741	3.34	36	6	<2	7	91	2.2	3.5	2.7	549	.41	.346	20	74	.30	1348	.083	6	1.94	.007	.12	4	<1	2.6	<1	.11	6
2300W 390S	25.0	69	792	417	1.0	56	3	462	3.46	35	7	<2	7	112	2.1	3.8	1.2	571	.29	.355	20	66	.26	1759	.085	3	1.65	.008	.11	3	<1	2.3	<1	.12	6
2300W 400S	20.8	66	532	380	1.9	54	5	343	3.53	33	6	<2	7	84	2.0	3.3	1.6	481	.17	.311	21	67	.30	1600	.079	4	1.83	.007	.11	2	<1	2.5	<1	.12	5
2300W 600S	16.0	65	276	490	3.1	86	4	443	3.03	35	6	<2	6	49	2.0	3.5	1.4	863	.18	.248	21	88	.37	1603	.095	4	1.97	.005	.10	2	<1	2.6	<1	.08	7
2300W 620S	6.3	15	45	120	3.0	20	5	203	2.67	13	2	<2	6	9	.9	.9	<.5	208	.06	.119	19	40	.27	371	.054	2	1.50	.003	.04	1	<1	2.4	<1	<.02	7
2300W 640S	9.3	44	91	261	6.3	41	6	256	2.91	25	4	<2	7	19	1.4	2.1	<.5	491	.09	.145	18	60	.35	709	.065	3	2.02	.004	.07	1	<1	2.5	<1	<.02	6
2300W 660S	12.5	23	202	324	2.3	44	4	267	2.60	23	3	<2	6	22	1.8	1.8	3.4	562	.11	.136	19	53	.27	582	.069	<1	1.36	.003	.06	1	<1	2.3	<1	<.02	8
2300W 680S	6.0	17	97	184	3.2	23	4	243	2.74	15	2	<2	6	16	1.4	1.3	<.5	261	.08	.153	19	47	.27	391	.058	3	1.64	.004	.05	1	<1	2.4	<1	<.02	7
2300W 700S	4.3	16	36	117	4.6	18	3	164	2.31	12	2	<2	6	11	.5	1.2	<.5	161	.05	.153	18	43	.21	265	.033	1	1.56	.003	.04	<1	<1	1.8	<1	<.02	7
2300W 720S	4.7	35	44	284	4.5	34	7	242	2.61	17	3	<2	7	13	1.3	1.6	<.5	229	.10	.174	19	60	.35	791	.058	3	1.89	.004	.06	1	<1	3.7	<1	<.02	6
2300W 740S	6.9	22	67	124	4.0	21	3	139	2.73	18	2	<2	5	12	1.0	1.9	<.5	241	.08	.192	19	48	.21	368	.044	1	1.36	.003	.05	1	<1	2.2	<1	<.02	7
2300W 760S	8.8	64	52	329	2.9	58	7	210	2.32	27	5	<2	6	43	1.4	3.4	<.5	341	.24	.291	20	81	.31	2913	.044	3	2.26	.004	.07	1	<1	3.1	<1	<.02	5
2300W 780S	3.3	8	20	100	2.1	14	4	105	1.61	6	1	<2	5	7	.6	<.5	<.5	66	.06	.084	20	28	.22	391	.029	1	1.39	.003	.04	<1	<1	1.6	<1	<.02	5
2300W 800S	11.1	47	95	318	2.8	46	6	206	2.89	37	3	<2	7	35	2.2	4.2	.5	413	.22	.357	20	72	.33	1140	.054	3	1.94	.005	.07	1	<1	2.7	<1	.02	5
RE 2300W 800S	11.1	49	102	323	2.8	46	6	208	2.91	38	4	<2	7	36	2.3	4.3	<.5	422	.22	.363	20	70	.32	1249	.054	3	2.00	.005	.08	1	<1	2.9	<1	.02	6
2300W 820S	4.0	23	33	212	3.2	25	5	160	2.60	17	2	<2	6	12	1.6	.9	<.5	194	.10	.263	18	58	.27	1065	.039	3	2.06	.005	.05	<1	<1	2.2	<1	<.02	7
2300W 840S	17.8	48	186	403	2.8	58	5	221	2.54	34	5	<2	6	49	2.9	4.4	1.0	610	.26	.313	19	76	.26	1753	.065	3	1.90	.005	.08	4	<1	2.8	<1	.03	6
2300W 860S	25.5	120	264	501	2.2	85	5	427	1.88	38	11	<2	5	110	3.4	6.5	.9	942	.50	.275	25	86	.27	4786	.098	7	1.58	.009	.16	2	<1	3.1	1	.08	5
2300W 880S	22.2	88	539	414	1.3	62	3	372	2.44	51	7	<2	5	87	2.7	5.2	.9	781	.32	.226	25	81	.27	2248	.098	4	1.37	.005	.11	1	<1	2.8	<1	.07	6
2300W 900S	21.3	82	591	397	.8	57	3	442	2.11	49	8	<2	6	96	3.4	5.0	.9	761	.42	.245	27	78	.24	2191	.099	5	1.30	.005	.11	3	<1	2.7	<1	.07	6
2300W 920S	13.7	60	398	369	1.3	56	3	366	1.96	33	5	<2	5	83	3.7	3.5	1.0	593	.44	.257	22	69	.24	1958	.074	6	1.22	.004	.09	2	<1	2.1	<1	.05	5
2300W 940S	16.1	77	416	387	1.6	57	3	333	2.43	44	6	<2	6	78	3.5	4.0	.8	622	.33	.286	20	63	.26	1962	.074	5	1.29	.004	.10	4	<1	2.3	<1	.05	5
2300W 960S	16.6	57	256	415	1.7	62	3	254	1.78	36	5	<2	2	68	3.2	4.9	.9	601	.34	.225	25	70	.28	1619	.071	4	1.13	.004	.10	1	<1	1.7	<1	.05	5
2300W 980S	5.8	26	37	198	1.7	27	2	110	1.02	15	2	<2	<1	26	3.4	1.8	<.5	124	.20	.067	16	29	.16	534	.028	2	.59	.004	.05	<1	<1	.8	<1	.04	4
2300W 1000S	10.2	40	54	532	2.5	63	5	226	2.48	38	3	<2	5	36	2.7	3.9	<.5	325	.28	.204	19	60	.43	693	.054	3	1.30	.005	.07	1	<1	2.0	<1	.04	5
2300W 1020S	10.2	28	54	251	2.5	35	4	163	2.99	27	2	<2	5	19	1.5	3.0	<.5	379	.07	.120	17	51	.29	532	.047	1	1.47	.003	.06	<1	<1	2.0	<1	<.02	6
2300W 1040S	23.5	64	56	415	2.8	74	5	177	2.71	46	6	<2	6	47	2.2	7.4	<.5	630	.14	.233	20	81	.39	2000	.061	5	2.26	.006	.10	1	<1	2.6	1	.04	5
STANDARD C3	26.4	64	37	169	5.5	35	13	814	3.10	57	21	<2	23	27	23.5	14.1	25.0	84	.54	.099	18	182	.57	159	.089	18	1.87	.027	.16	15	1	4.1	1	.03	7
STANDARD G-2	1.6	3	2	45	<.1	9	5	569	1.80	1	2	<2	4	68	<.2	<.5	<.5	43	.58	.103	7	82	.56	230	.137	1	.92	.054	.48	2	<1	2.3	<1	.03	4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	ppm	ppm	ppm	ppm	%	ppm	
2300W 1060S	6.6	22	25	144	4.1	25	5	153	2.26	16	2	<2	4	10	1.0	2.0	<.5	158	.05	.100	16	43	.30	344	.031	1	1.59	.003	.05	<1	<1	2.0	<1	.03	4
2300W 1080S	3.0	17	16	65	4.3	13	3	97	1.98	11	1	<2	5	7	.5	1.1	<.5	93	.04	.134	19	33	.20	179	.034	1	1.29	.003	.04	<1	<1	2.2	<1	.02	5
2300W 1100S	17.7	38	27	191	5.7	38	3	136	3.36	30	3	<2	6	19	1.0	5.8	<.5	289	.09	.317	19	58	.30	427	.054	3	2.02	.002	.07	<1	<1	2.3	<1	.02	6
2100W 800N	3.2	16	59	387	.4	27	7	316	2.45	18	1	<2	3	27	4.4	1.3	<.5	145	.21	.130	17	39	.45	381	.059	3	1.39	.004	.09	<1	<1	1.9	<1	.02	6
2100W 780N	6.4	40	96	349	.7	45	6	528	1.94	23	3	<2	2	44	2.6	2.3	<.5	246	.30	.097	18	42	.39	683	.061	4	1.12	.003	.09	1	<1	2.0	<1	.05	4
2100W 760N	13.0	60	222	620	1.0	74	9	886	2.38	56	6	<2	5	85	5.1	5.1	<.5	622	.50	.182	24	73	.43	1902	.091	4	1.26	.006	.13	1	<1	3.1	<1	.10	5
2100W 740N	12.7	65	128	313	2.9	42	3	182	2.06	32	5	<2	1	46	3.4	2.9	<.5	393	.15	.111	20	47	.29	1451	.055	1	1.31	.005	.09	<1	<1	1.9	<1	.07	5
2100W 720N	13.5	41	115	248	1.1	31	3	128	1.96	34	3	<2	1	43	2.1	3.2	.5	352	.13	.097	19	37	.19	1160	.061	2	1.06	.004	.08	1	<1	1.5	<1	.08	6
2100W 700N	20.1	75	207	673	1.1	78	8	496	2.97	52	6	<2	5	93	2.9	3.5	.7	596	.29	.224	18	60	.41	1606	.082	3	1.55	.008	.13	4	<1	2.5	<1	.14	5
2100W 680N	16.2	97	249	934	1.6	113	9	838	2.68	65	7	<2	6	85	6.7	4.7	.6	820	.39	.178	23	82	.54	3515	.104	2	1.66	.007	.13	1	<1	3.6	<1	.07	6
2100W 660N	8.2	65	142	416	1.8	57	4	283	1.86	31	5	<2	3	37	3.5	2.9	<.5	449	.17	.091	23	50	.33	1222	.055	2	1.18	.008	.09	1	<1	2.9	<1	.04	4
2100W 640N	15.1	67	558	1016	1.1	153	13	2370	2.37	50	7	<2	6	93	9.9	4.0	1.1	1058	.57	.167	28	83	.69	2233	.113	6	1.49	.006	.12	3	<1	3.6	1	.07	6
2100W 620N	9.5	42	251	328	1.4	45	5	471	2.16	32	4	<2	2	31	2.9	2.3	<.5	455	.18	.123	27	52	.28	766	.051	2	1.26	.005	.07	1	<1	2.2	<1	.03	6
2100W 600N	14.2	58	605	785	.9	102	8	1138	2.75	50	5	<2	7	63	4.6	3.8	.8	789	.37	.200	22	85	.58	1153	.094	6	1.94	.005	.11	1	<1	3.2	<1	.06	7
RE 2100W 600N	14.9	60	624	812	.9	104	8	1085	2.85	50	6	<2	7	64	4.6	3.8	.7	790	.38	.212	23	85	.56	1274	.097	5	1.97	.004	.11	1	<1	3.2	<1	.05	7
2100W 580N	10.0	59	198	437	1.5	62	8	500	2.59	36	4	<2	4	41	3.9	2.6	<.5	628	.22	.168	22	65	.39	1704	.054	4	1.68	.004	.08	<1	<1	2.9	<1	.03	6
2100W 560N	24.2	89	212	662	1.4	90	15	800	3.01	51	7	<2	5	84	3.8	4.4	.5	764	.32	.181	22	71	.49	2929	.104	5	1.64	.007	.15	<1	<1	3.3	<1	.08	6
2100W 540N	13.8	59	205	428	1.5	62	11	679	2.37	51	5	<2	6	84	3.1	5.1	<.5	566	.40	.166	22	57	.41	1881	.094	3	1.19	.005	.10	2	<1	2.5	<1	.09	4
2100W 520N	10.6	57	210	726	.6	83	7	966	2.14	46	5	<2	6	84	6.1	4.5	<.5	608	.50	.168	22	73	.42	1981	.090	6	1.14	.005	.09	1	<1	3.0	<1	.08	4
2100W 500N	11.6	37	206	477	.8	54	4	381	2.34	47	4	<2	5	49	2.1	3.7	.5	611	.25	.135	22	67	.29	758	.080	2	1.29	.003	.10	<1	<1	2.6	<1	.05	6
2100W 480N	12.3	59	310	879	.8	84	7	1108	2.38	51	6	<2	5	84	5.8	5.3	<.5	782	.51	.180	25	78	.39	1781	.095	4	1.25	.006	.11	1	<1	2.9	<1	.07	5
2100W 460N	9.8	36	181	411	.7	46	4	421	2.02	37	4	<2	<1	51	2.9	4.1	.5	622	.22	.083	21	58	.25	968	.047	5	1.08	.005	.09	<1	<1	1.3	<1	.08	5
2100W 440N	11.1	55	298	632	.6	81	7	964	2.46	60	5	<2	6	81	5.6	6.3	<.5	610	.61	.150	24	78	.42	1970	.099	4	1.24	.006	.11	1	<1	3.1	<1	.07	4
2100W 420N	5.0	40	103	175	.2	22	3	333	1.33	23	2	<2	3	31	1.3	2.3	<.5	210	.17	.071	20	33	.13	487	.063	2	.84	.004	.06	<1	<1	1.2	<1	.03	5
2100W 400N	9.9	56	142	442	.7	65	11	503	2.60	55	5	<2	6	59	1.9	4.8	<.5	365	.29	.150	22	71	.33	811	.078	3	1.69	.005	.09	<1	<1	2.5	<1	.08	4
2100W 380N	7.5	29	112	465	.5	46	4	479	2.41	35	3	<2	3	46	1.4	3.0	<.5	372	.26	.140	17	54	.27	543	.065	5	1.02	.005	.06	<1	<1	1.6	<1	.05	5
2100W 360N	4.3	18	78	241	.8	31	5	300	2.31	21	2	<2	2	18	1.2	1.5	<.5	246	.13	.102	19	42	.31	377	.035	1	1.23	.002	.06	<1	<1	1.5	<1	.02	6
2100W 340N	7.8	42	266	544	1.3	69	4	462	2.76	45	4	<2	4	63	2.1	3.6	.7	498	.45	.248	18	84	.40	805	.082	5	1.35	.006	.09	1	<1	2.7	<1	.08	6
2100W 320N	3.7	18	57	131	.9	21	4	206	3.06	19	2	<2	4	10	.8	1.1	<.5	195	.07	.128	19	42	.32	258	.059	2	1.55	.003	.06	<1	<1	2.1	<1	.02	7
2100W 300N	3.0	12	67	146	.5	20	2	151	1.34	13	1	<2	4	24	.5	1.1	<.5	150	.12	.081	18	31	.22	236	.070	2	.87	.002	.05	<1	<1	1.7	<1	.02	6
2100W 200S	15.2	68	231	479	1.7	62	6	662	2.11	33	7	<2	2	69	4.2	3.3	.7	459	.42	.155	21	66	.31	2049	.057	3	1.35	.007	.10	1	<1	2.3	<1	.07	5
2100W 210S	16.9	75	405	492	1.9	68	7	830	2.65	43	5	<2	2	64	2.9	2.9	2.3	511	.31	.203	21	76	.30	1028	.055	4	1.44	.006	.09	2	<1	1.9	<1	.07	6
2100W 220S	15.8	113	225	397	4.3	52	4	346	1.83	29	10	<2	1	54	3.7	3.1	.8	431	.20	.151	25	65	.19	1761	.039	1	1.26	.008	.10	1	<1	1.6	<1	.10	5
2100W 230S	13.7	49	269	268	.9	34	3	346	1.95	31	5	<2	4	52	1.6	2.6	.9	428	.22	.150	21	55	.19	736	.070	2	1.18	.004	.08	2	<1	2.0	<1	.06	6
STANDARD C3	26.2	62	38	159	5.4	37	12	832	3.26	57	20	<2	21	28	22.4	15.0	24.0	85	.52	.095	18	184	.61	144	.093	22	1.85	.027	.17	15	1	4.1	1	.03	7
STANDARD G-2	1.6	3	2	42	<.1	9	4	571	1.84	2	2	<2	4	66	<.2	<.5	<.5	43	.57	.098	7	85	.58	220	.131	5	.91	.046	.51	2	<1	1.8	<1	<.02	4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm
2100W 240S	9.8	36	132	214	.8	33	5	262	2.20	26	3	<2	4	37	1.2	2.5	<.5	287	.22	.141	17	44	.26	729	.052	<1	1.13	.005	.06	1	<1	2.1	<1	.07	4
2100W 250S	9.3	31	137	172	.8	25	3	201	2.16	22	3	<2	3	32	1.3	2.0	<.5	274	.15	.159	15	38	.18	813	.054	2	1.06	.005	.06	1	<1	1.9	<1	.07	5
2100W 260S	7.9	28	107	130	1.1	20	2	133	1.63	18	3	<2	4	25	.6	1.7	<.5	238	.10	.087	16	34	.15	557	.045	1	1.01	.004	.05	<1	<1	1.5	<1	.04	5
2100W 270S	13.0	77	165	331	1.1	55	7	455	2.40	30	5	<2	5	55	1.5	3.3	<.5	442	.27	.154	19	54	.33	2106	.076	2	1.55	.008	.09	2	<1	3.0	<1	.06	5
2100W 280S	9.3	27	107	167	1.5	26	4	202	2.58	22	2	<2	4	28	1.1	2.1	<.5	259	.12	.144	17	41	.26	896	.058	<1	1.24	.004	.06	1	<1	1.8	<1	.06	6
2100W 290S	14.2	60	221	281	1.9	43	4	243	2.55	30	4	<2	5	59	1.5	3.4	.6	447	.20	.224	17	47	.21	1571	.067	2	1.38	.007	.09	1	<1	2.1	<1	.09	5
2100W 300S	16.5	52	235	300	1.4	45	4	309	2.79	32	4	<2	6	64	1.4	4.0	.5	494	.26	.247	19	54	.25	1556	.077	1	1.65	.009	.10	1	<1	2.8	<1	.10	5
2100W 310S	4.7	21	61	120	1.7	22	4	160	2.20	14	2	<2	4	11	.6	1.2	<.5	142	.06	.079	16	41	.28	321	.037	1	1.48	.003	.04	<1	<1	2.3	<1	.02	5
2100W 320S	10.8	40	240	269	2.1	45	4	302	2.70	34	4	<2	5	40	1.2	2.9	<.5	443	.20	.198	17	82	.27	693	.062	1	1.51	.006	.06	1	<1	2.5	<1	.07	4
2100W 330S	5.1	17	77	106	2.9	16	3	149	1.90	11	1	<2	4	12	.4	1.0	<.5	147	.07	.093	15	32	.20	371	.034	1	1.23	.003	.04	1	<1	1.9	<1	.02	5
2100W 340S	11.6	38	148	204	4.1	31	3	204	2.83	29	3	<2	5	39	.8	3.2	<.5	440	.18	.183	17	51	.25	777	.066	<1	1.55	.006	.07	1	<1	2.5	<1	.07	5
2100W 350S	10.0	56	217	271	2.8	48	3	203	2.21	29	5	<2	4	31	1.1	3.6	.7	689	.11	.173	18	65	.21	853	.061	1	1.47	.005	.06	1	<1	2.3	<1	.02	6
600S 2700W	7.1	27	100	179	1.6	26	4	183	2.54	22	2	<2	5	28	1.0	1.6	<.5	183	.07	.147	18	34	.23	636	.052	1	1.36	.005	.06	<1	<1	2.2	<1	.04	5
600S 2680W	7.4	27	90	165	1.0	25	4	202	3.13	25	2	<2	6	24	1.0	1.6	<.5	210	.07	.197	18	39	.28	608	.058	2	1.54	.005	.06	<1	<1	2.5	<1	.03	6
600S 2660W	9.8	40	120	235	2.9	36	5	225	3.09	29	2	<2	6	34	1.1	2.3	<.5	240	.08	.179	19	43	.29	862	.058	2	1.72	.005	.07	<1	<1	2.9	<1	.04	5
600S 2640W	7.8	30	81	181	1.5	33	5	223	2.68	21	2	<2	6	28	1.2	1.9	<.5	171	.07	.124	17	39	.33	774	.053	4	1.53	.004	.06	<1	<1	2.5	<1	.04	5
600S 2620W	5.6	17	35	99	3.9	17	5	186	2.91	12	1	<2	6	11	.8	.9	<.5	124	.05	.173	16	38	.26	282	.060	1	1.88	.004	.05	<1	<1	2.7	<1	.02	7
600S 2600W	9.2	21	99	106	.8	15	2	79	2.13	17	2	<2	4	23	.7	1.6	<.5	259	.05	.115	17	29	.09	670	.059	1	.93	.003	.05	<1	<1	1.6	<1	.03	6
RE 600S 2600W	8.8	21	97	102	.7	14	2	81	2.06	16	2	<2	4	23	.7	1.6	<.5	259	.05	.116	17	28	.09	660	.056	1	.91	.004	.05	<1	<1	1.5	<1	.03	6
600S 2580W	9.5	25	82	150	2.4	25	4	207	3.56	21	2	<2	5	25	1.1	2.0	<.5	268	.08	.276	16	39	.24	528	.086	2	1.16	.007	.07	1	<1	2.0	<1	.06	7
600S 2560W	5.9	23	27	109	2.1	24	4	155	1.95	13	2	<2	3	16	.8	1.0	<.5	169	.16	.116	17	31	.32	676	.023	2	1.37	.002	.04	<1	<1	2.2	<1	.02	3
600S 2540W	6.2	27	19	111	8.1	24	6	249	3.06	14	4	<2	7	9	.7	1.3	<.5	238	.10	.248	18	56	.36	560	.075	1	2.47	.004	.05	<1	<1	3.3	<1	.02	6
600S 2520W	3.1	11	17	58	2.3	10	4	108	2.20	7	1	<2	5	6	.4	.6	<.5	81	.04	.078	15	31	.24	203	.050	2	1.47	.003	.03	<1	<1	2.2	<1	.02	6
600S 2500W	7.6	32	61	189	2.9	29	6	228	2.52	16	3	<2	5	18	1.5	1.8	<.5	227	.06	.113	17	43	.29	724	.067	3	1.63	.006	.07	<1	<1	2.9	<1	.03	5
600S 2480W	10.8	32	99	181	3.3	30	5	202	3.87	23	3	<2	6	23	1.5	2.1	.6	415	.09	.321	16	57	.28	709	.065	1	1.80	.004	.07	1	<1	2.7	<1	.02	7
600S 2460W	11.1	42	84	200	2.1	33	5	190	2.68	23	3	<2	5	25	.8	2.2	<.5	299	.08	.126	17	45	.30	831	.046	2	1.52	.004	.06	<1	<1	2.6	<1	.02	5
600S 2440W	13.3	45	129	250	1.3	39	4	212	3.32	27	4	<2	6	29	1.0	2.6	.6	514	.09	.225	16	54	.27	1004	.053	1	1.56	.003	.07	1	<1	2.8	<1	.06	6
600S 2420W	8.2	31	72	195	1.6	34	6	241	2.63	16	2	<2	3	22	1.0	1.7	<.5	202	.09	.138	16	45	.33	610	.038	1	1.55	.004	.05	<1	<1	2.4	<1	.03	4
600S 2400W	12.6	42	107	231	11.3	32	5	222	2.84	25	4	<2	6	27	1.1	2.9	<.5	439	.10	.232	18	55	.30	743	.051	2	1.86	.004	.07	<1	<1	2.9	<1	.04	5
600S 2380W	6.5	13	117	105	5.6	16	4	203	3.04	13	2	<2	6	10	.7	.7	<.5	378	.11	.198	17	40	.27	342	.050	<1	1.43	.002	.04	1	<1	2.3	<1	.02	7
600S 2360W	9.0	43	92	301	6.1	44	4	339	2.52	22	5	<2	3	24	2.2	2.1	.6	612	.17	.200	22	54	.36	1551	.044	2	1.30	.003	.07	1	<1	3.0	<1	.04	5
600S 2340W	8.8	24	102	178	1.6	27	4	182	2.75	24	2	<2	4	16	.9	2.0	.5	317	.06	.134	16	44	.28	579	.041	1	1.33	.004	.06	1	<1	1.9	<1	.04	5
600S 2320W	6.8	25	95	162	2.5	24	3	146	2.37	18	2	<2	5	16	.8	1.5	.6	357	.08	.142	17	42	.24	609	.038	3	1.73	.003	.05	1	<1	2.4	<1	.02	6
700S 1500W	9.2	46	120	462	2.4	69	3	359	2.45	32	5	<2	4	77	1.5	4.5	<.5	638	.67	.394	20	95	.43	575	.072	4	1.23	.002	.07	2	<1	2.3	<1	.06	5
STANDARD C3	26.3	63	37	159	5.5	36	13	807	3.17	57	20	<2	21	27	23.4	14.1	23.8	82	.54	.096	17	168	.56	150	.087	20	1.78	.029	.16	14	1	4.3	1	.02	7
STANDARD G-2	1.4	3	2	43	.1	8	5	565	1.78	2	2	<2	3	66	<.2	<.5	<.5	43	.61	.099	7	79	.58	219	.123	<1	.87	.058	.47	2	<1	2.2	<1	.02	4

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	ppm	ppm	ppm	ppm	ppm	%	ppm
700S 1480W	4.6	19	54	193	1.7	28	4 243	2.47	16	2	<2	4 21	.9	1.5	<.5	180	.15	.213	17	45	.26	242	.039	3	1.17	.003	.05	1	<1	1.7	<1	.05	5		
700S 1460W	6.2	29	92	303	2.6	42	4 287	2.45	22	3	<2	4 32	2.0	2.7	<.5	322	.23	.235	18	60	.30	455	.048	2	1.52	.004	.06	1	<1	2.0	<1	.03	5		
700S 1440W	6.5	36	95	370	1.7	54	4 275	2.68	27	3	<2	5 47	1.2	3.1	<.5	408	.37	.322	19	72	.38	551	.056	3	1.38	.003	.07	1	<1	2.3	<1	.04	5		
700S 1420W	7.1	44	163	412	5.6	59	4 335	2.20	28	4	<2	5 53	1.3	3.9	<.5	406	.43	.279	18	79	.34	525	.054	3	1.54	.003	.06	2	<1	2.2	<1	.04	4		
700S 1400W	4.0	25	66	248	8.5	31	5 310	2.88	24	3	<2	7 21	2.0	1.7	<.5	341	.24	.368	17	70	.29	294	.059	2	1.57	.004	.06	1	<1	2.2	<1	<.02	6		
700S 1380W	4.1	19	59	183	2.2	27	4 203	2.20	14	2	<2	5 15	.9	1.4	<.5	165	.11	.129	19	46	.29	314	.047	1	1.36	.003	.06	<1	<1	2.1	<1	<.02	5		
700S 1360W	2.2	9	42	100	2.6	12	2 121	1.59	7	1	<2	4 10	.7	.6	<.5	106	.06	.084	17	33	.17	233	.032	1	1.35	.003	.04	<1	<1	1.8	<1	<.02	5		
700S 1340W	1.7	8	49	59	1.1	7	1 54	.68	5	1	<2	3 10	.4	.5	<.5	92	.05	.056	19	21	.09	228	.032	1	.82	.002	.03	<1	<1	1.1	<1	<.02	4		
700S 1320W	5.0	27	70	219	2.0	34	4 228	2.35	15	2	<2	5 17	1.0	1.5	<.5	217	.11	.142	18	56	.36	367	.058	2	1.61	.003	.07	<1	<1	1.9	<1	<.02	5		
700S 1300W	10.5	83	176	534	1.3	83	5 357	2.29	33	4	<2	6 63	1.6	4.3	<.5	530	.46	.234	22	89	.58	1091	.088	4	1.45	.006	.10	1	<1	2.4	<1	.03	5		
700S 1280W	7.6	48	123	387	1.7	55	5 369	2.91	27	3	<2	6 29	1.2	2.7	<.5	463	.22	.194	20	80	.60	627	.074	3	1.78	.005	.10	1	<1	2.6	<1	<.02	6		
700S 1260W	7.6	40	138	342	1.8	48	4 297	2.53	32	3	<2	6 39	1.1	3.2	<.5	326	.30	.184	17	57	.58	594	.099	5	1.35	.006	.10	1	<1	2.3	<1	.05	4		
700S 1240W	5.2	38	80	291	1.1	40	5 302	2.35	19	2	<2	5 22	.9	1.7	<.5	268	.22	.135	20	58	.53	504	.054	4	1.53	.004	.08	1	<1	2.5	<1	.02	5		
700S 1220W	9.3	40	152	281	.5	44	3 224	1.74	23	3	<2	4 40	1.0	3.5	<.5	405	.24	.124	21	57	.37	585	.089	3	.91	.003	.08	1	<1	2.0	<1	.03	5		
700S 1200W	9.8	46	158	346	1.2	54	3 261	1.98	24	3	<2	3 52	1.5	3.8	<.5	418	.36	.207	20	59	.43	774	.075	4	1.10	.004	.10	1	<1	1.9	<1	.05	5		
RE 700S 1200W	9.0	45	146	346	1.1	51	3 256	1.95	24	3	<2	3 53	1.4	3.7	<.5	426	.38	.205	20	60	.44	772	.076	2	1.10	.004	.10	1	<1	1.9	<1	.03	5		
700S 1180W	10.6	59	201	435	1.0	63	3 325	2.10	32	4	<2	5 73	1.9	4.5	<.5	533	.56	.254	22	76	.58	1085	.083	6	1.28	.005	.10	1	<1	2.1	<1	.06	5		
700S 1160W	10.3	59	190	375	1.5	56	3 278	1.79	29	4	<2	3 73	1.7	4.5	<.5	486	.53	.231	22	67	.44	1088	.075	7	1.10	.004	.10	1	<1	2.0	<1	.03	4		
700S 1140W	9.6	64	175	420	2.1	61	3 324	1.74	26	4	<2	1 62	3.6	4.2	<.5	444	.42	.147	22	67	.43	2616	.067	5	1.11	.004	.11	1	<1	2.0	<1	.05	4		
700S 1120W	9.4	86	175	520	2.5	74	4 340	1.76	25	5	<2	1 65	6.0	3.6	.5	460	.58	.143	23	80	.64	2860	.070	3	1.28	.008	.14	1	<1	2.0	<1	.04	5		
700S 1100W	8.6	71	187	457	.8	62	4 444	1.68	24	5	<2	1 67	3.1	3.5	<.5	502	.47	.183	23	76	.60	1932	.067	3	1.26	.007	.12	1	<1	2.2	<1	.05	5		
700S 1080W	9.1	53	189	371	1.3	54	3 329	1.39	24	4	<2	3 83	2.2	4.0	<.5	452	.66	.219	21	63	.43	2072	.077	8	.93	.006	.12	1	<1	2.1	<1	.05	4		
700S 1060W	12.2	89	248	509	1.2	75	7 721	1.83	34	6	<2	5 97	3.9	5.7	<.5	557	.71	.264	24	67	.49	2608	.092	5	1.03	.005	.13	1	<1	2.7	<1	.06	3		
700S 1040W	11.2	82	251	510	.9	73	6 593	1.71	32	6	<2	5 98	3.9	4.7	<.5	562	.72	.253	24	73	.59	2736	.090	5	1.06	.006	.13	1	<1	2.8	<1	.07	4		
700S 1020W	11.3	73	233	406	1.1	60	6 627	1.49	30	5	<2	4 94	3.6	5.1	<.5	488	.68	.250	23	58	.38	2499	.075	7	.86	.005	.10	1	<1	2.2	<1	.05	3		
700S 1000W	10.4	83	290	504	1.5	68	6 696	1.70	30	5	<2	4 104	5.7	4.8	<.5	499	.89	.280	22	65	.47	2891	.070	8	.95	.006	.13	1	<1	2.8	<1	.05	3		
700S 980W	7.2	75	168	609	1.8	65	6 534	1.89	25	6	<2	2 73	6.7	2.8	<.5	427	.86	.166	20	73	.70	2027	.055	4	1.34	.007	.13	1	<1	2.5	<1	.07	4		
700S 960W	6.5	58	173	416	.6	55	9 678	1.98	23	4	<2	3 66	4.1	2.7	<.5	267	.62	.155	19	54	.67	1642	.075	5	1.33	.006	.14	2	<1	2.7	<1	.05	4		
700S 940W	3.8	62	145	531	1.4	59	6 460	2.06	19	7	<2	2 72	5.5	1.9	<.5	214	.99	.158	19	62	.69	1086	.071	4	1.50	.008	.13	<1	<1	2.6	<1	.08	5		
700S 920W	3.3	47	99	367	1.4	48	6 408	1.85	18	6	<2	2 65	4.1	1.4	<.5	175	.86	.141	17	51	.60	917	.064	4	1.43	.009	.12	<1	<1	2.3	<1	.07	5		
700S 900W	4.0	35	97	332	2.7	43	6 275	2.05	16	2	<2	2 46	2.3	1.3	<.5	171	.52	.083	16	51	.59	729	.072	4	1.69	.009	.11	<1	<1	2.1	<1	.05	6		
700S 880W	4.4	31	105	271	1.3	35	8 581	2.09	19	2	<2	1 37	1.5	1.3	<.5	197	.34	.116	18	47	.53	585	.056	2	1.32	.004	.09	1	<1	1.8	<1	.04	4		
700S 860W	3.7	44	131	470	1.3	55	8 558	2.50	23	4	<2	2 62	2.6	1.3	<.5	210	.69	.135	19	61	.78	973	.083	5	1.96	.009	.14	<1	<1	3.0	<1	.06	6		
700S 840W	2.9	31	98	265	.7	36	6 466	1.91	17	2	<2	2 47	2.4	1.2	<.5	158	.57	.113	18	43	.53	656	.072	3	1.24	.007	.09	<1	<1	2.1	<1	.04	4		
STANDARD C3	27.3	66	38	165	5.6	35	12 795	3.41	58	21	<2	23 28	22.5	14.2	25.1	83	.55	.099	18	183	.56	154	.092	18	1.81	.031	.18	14	1	4.2	1	.04	7		
STANDARD G-2	1.5	3	2	44	<.1	9	5 549	1.94	1	3	<2	5 69	<.2	<.5	<.5	43	.61	.101	8	87	.59	234	.130	4	.92	.058	.50	2	<1	2.3	<1	<.02	4		

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	
700S 820W	3.0	35	80	243	.6	38	6	325	1.79	17	2	<2	4	54	1.5	1.4	<.5	123	.56	.118	18	39	.66	800	.101	2	1.50	.011	.13	1	<1	2.8	<1	.07	4
700S 800W	3.2	36	80	258	.7	35	5	305	1.73	13	2	<2	2	48	2.2	1.2	<.5	135	.49	.113	19	39	.60	886	.079	3	1.50	.007	.12	1	<1	2.3	<1	.07	5
900S 1500W	6.8	43	135	378	2.9	53	3	240	2.46	24	3	<2	5	39	1.4	2.6	<.5	366	.24	.249	19	63	.55	699	.062	2	1.63	.003	.06	1	<1	2.2	<1	.02	5
900S 1480W	7.4	34	77	258	1.7	40	4	210	2.31	20	3	<2	5	28	.9	2.6	<.5	276	.16	.197	18	54	.45	451	.049	3	1.48	.003	.06	1	<1	2.1	<1	.03	5
900S 1460W	4.0	18	49	155	1.5	20	3	139	1.80	13	2	<2	5	14	.7	1.2	<.5	198	.09	.154	18	38	.23	349	.042	2	1.20	.003	.04	1	<1	1.9	<1	.02	5
900S 1440W	7.3	30	81	283	1.7	41	4	229	2.35	20	2	<2	5	27	1.1	2.4	<.5	271	.17	.190	20	49	.48	528	.057	2	1.54	.003	.06	1	<1	2.5	<1	.02	5
900S 1420W	3.9	22	46	232	3.9	26	5	171	2.63	18	2	<2	4	13	1.9	1.4	<.5	209	.11	.219	17	44	.37	416	.048	1	1.52	.003	.06	<1	<1	2.3	<1	.02	5
900S 1400W	5.6	24	67	174	1.2	25	2	111	1.48	14	2	<2	3	21	.9	1.7	<.5	240	.14	.185	19	41	.24	595	.051	1	1.10	.003	.06	1	<1	1.6	<1	.02	5
900S 1380W	5.7	37	83	226	5.2	32	5	237	2.04	19	3	<2	4	23	1.8	1.8	<.5	249	.14	.167	19	42	.31	824	.043	2	1.32	.004	.07	1	<1	2.1	<1	.03	5
900S 1360W	5.5	21	95	153	2.2	20	2	100	1.45	14	2	<2	3	22	1.1	1.4	<.5	245	.12	.124	20	35	.22	647	.046	1	1.03	.003	.06	<1	<1	1.6	<1	.02	5
900S 1340W	10.6	54	233	313	.7	48	2	186	1.58	27	4	<2	4	61	1.7	3.9	<.5	498	.34	.207	22	60	.36	1283	.076	3	1.17	.003	.09	1	<1	2.2	<1	.03	4
900S 1320W	9.2	48	143	330	2.1	45	3	207	1.73	20	3	<2	3	37	1.5	2.8	<.5	412	.17	.126	21	57	.45	937	.071	3	1.34	.003	.10	1	<1	2.0	<1	.02	6
900S 1300W	10.9	65	205	412	2.6	67	4	287	2.05	36	5	<2	6	66	2.1	4.5	<.5	604	.47	.294	24	76	.62	1367	.076	4	1.60	.003	.13	1	<1	2.7	<1	.03	5
RE 900S 1300W	11.3	66	210	416	2.6	68	4	278	2.14	36	5	<2	5	69	2.2	4.4	<.5	592	.43	.279	23	77	.61	1352	.076	4	1.52	.004	.13	1	<1	2.7	<1	.02	5
900S 1280W	14.0	94	250	430	1.6	74	4	548	1.57	38	7	<2	4	116	3.3	6.5	.5	728	.64	.287	25	74	.48	2831	.080	5	1.09	.005	.16	1	<1	2.7	<1	.05	4
900S 1260W	11.4	66	220	369	2.2	59	3	279	1.59	26	5	<2	1	64	2.8	4.6	.5	586	.37	.202	23	81	.48	1711	.059	5	1.25	.003	.14	<1	<1	1.7	<1	.03	5
900S 1240W	11.9	82	203	483	1.6	75	4	461	1.83	36	6	<2	3	87	3.1	4.8	<.5	615	.54	.270	25	77	.69	1960	.082	5	1.44	.005	.16	1	<1	2.6	<1	.04	5
900S 1220W	11.8	75	215	387	1.5	58	3	187	1.97	34	6	<2	4	63	2.6	4.5	.5	489	.39	.326	22	62	.41	1843	.062	2	1.47	.004	.11	2	<1	2.9	<1	.03	5
900S 1200W	8.9	69	137	248	1.9	40	2	109	1.30	19	5	<2	<1	45	3.2	3.6	<.5	321	.17	.142	18	46	.21	1590	.025	2	.89	.008	.07	<1	<1	.7	<1	.04	3
900S 1180W	10.6	47	131	329	1.3	51	3	197	2.34	27	3	<2	3	54	2.2	4.3	<.5	409	.32	.302	20	54	.44	1056	.059	3	1.28	.004	.09	1	<1	2.0	<1	.04	5
900S 1160W	13.0	76	137	435	1.2	70	7	608	1.67	47	5	<2	4	104	3.5	6.3	<.5	552	.58	.274	24	72	.66	2082	.090	6	1.25	.006	.16	1	<1	2.5	<1	.05	3
900S 1140W	12.1	53	235	314	.7	49	2	186	1.58	28	5	<2	2	91	2.0	5.1	<.5	504	.50	.307	22	60	.32	1496	.065	3	1.07	.004	.11	1	<1	1.8	<1	.05	4
900S 1100W	8.1	96	85	538	5.6	80	8	371	2.96	28	5	<2	8	29	3.1	3.3	<.5	425	.23	.208	22	74	.71	1208	.086	3	2.15	.006	.13	1	<1	3.6	<1	.02	7
900S 1080W	4.7	17	66	98	.9	13	1	50	.71	8	2	<2	<1	22	.8	1.4	.5	150	.08	.061	20	26	.10	524	.042	1	.61	.002	.06	<1	<1	.8	<1	.03	4
900S 1060W	11.2	83	247	439	2.2	67	3	285	1.46	27	6	<2	2	91	2.7	4.4	<.5	505	.53	.252	23	63	.49	2161	.070	3	1.11	.005	.12	1	<1	2.3	<1	.06	4
900S 1040W	11.8	81	266	541	1.7	74	7	743	1.71	31	6	<2	3	114	4.1	4.9	<.5	528	.65	.263	24	64	.55	2578	.073	5	1.17	.006	.13	1	<1	2.5	<1	.04	4
900S 1020W	4.2	52	60	213	2.2	40	4	153	1.82	14	3	<2	1	35	1.1	1.1	<.5	141	.21	.134	16	42	.84	756	.046	2	2.05	.006	.12	<1	<1	1.5	<1	.06	6
900S 1000W	3.4	73	115	313	.9	65	15	598	2.26	15	2	<2	4	43	1.2	.6	.6	131	.34	.145	15	48	1.36	565	.109	2	2.78	.004	.20	1	<1	3.0	<1	.04	9
900S 980W	4.4	99	217	421	.8	71	29	1078	2.86	17	3	<2	6	48	2.0	.6	.9	134	.41	.153	18	51	1.65	636	.126	2	3.18	.006	.38	1	<1	4.3	1	.05	9
900S 960W	3.4	52	60	233	.4	42	11	454	2.10	13	2	<2	5	36	1.1	1.2	<.5	116	.24	.096	19	38	.91	597	.096	3	1.87	.006	.14	<1	<1	2.6	<1	.04	6
900S 940W	4.1	41	52	199	.3	40	6	258	2.18	13	2	<2	4	37	.9	1.4	<.5	133	.22	.109	20	41	.62	548	.085	3	1.61	.007	.11	<1	<1	2.2	<1	.06	5
900S 920W	3.4	76	150	323	.3	56	14	721	2.69	14	2	<2	7	42	1.2	.9	.5	131	.31	.126	19	45	1.38	533	.129	3	2.39	.007	.25	1	<1	3.3	1	.06	8
900S 900W	6.4	123	94	328	.7	55	13	671	2.88	20	5	<2	6	149	1.5	1.2	.5	241	1.17	.629	18	52	1.34	741	.087	2	2.56	.007	.31	1	<1	3.8	1	.09	8
900S 880W	5.4	40	60	194	.7	32	6	262	2.91	19	2	<2	3	36	1.0	1.6	<.5	141	.13	.113	19	42	.56	557	.070	3	1.62	.008	.13	<1	<1	2.0	<1	.09	5
STANDARD C3	26.7	63	41	161	5.5	35	12	800	3.27	57	21	<2	21	30	22.0	13.3	24.1	83	.53	.094	19	165	.62	165	.091	16	1.79	.028	.18	14	1	4.3	1	.02	7
STANDARD G-2	1.7	3	2	45	<.1	9	4	565	1.97	1	2	<2	4	78	<.2	<.5	<.5	44	.63	.102	8	82	.65	263	.134	1	1.02	.062	.52	2	<1	2.6	<1	.02	5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm
900S 860W	3.2	20	32	75	1.0	16	3	74	2.01	10	2	<2	2	30	1.7	.8	<.5	68	.07	.094	16	27	.16	348	.066	1	.84	.008	.07	<1	<1	1.2	<1	.09	5
900S 840W	6.2	50	35	164	1.2	40	7	221	5.68	21	5	<2	8	146	9.6	1.2	<.5	110	.12	.210	18	61	.39	955	.160	1	2.26	.036	.16	<1	<1	2.5	<1	.29	7
900S 820W	5.6	35	79	153	.4	30	6	233	3.23	25	3	<2	5	65	1.0	1.9	<.5	131	.17	.157	19	39	.31	480	.103	1	1.17	.015	.12	1	<1	1.8	<1	.16	4
900S 800W	6.3	35	118	285	1.3	46	6	211	2.84	22	3	<2	6	47	1.5	1.9	.8	146	.24	.165	19	45	.49	480	.083	2	1.53	.010	.09	<1	<1	1.9	<1	.08	5
1100S 1500W	5.8	24	26	179	4.2	22	4	122	2.44	13	2	<2	4	14	1.2	2.0	<.5	148	.07	.179	18	46	.24	392	.042	1	1.54	.004	.05	<1	<1	2.4	<1	.02	6
1100S 1480W	6.0	24	35	144	3.9	24	4	114	2.52	18	3	<2	5	17	.9	2.3	<.5	249	.11	.278	18	48	.25	403	.045	2	1.40	.004	.05	1	<1	2.0	<1	.02	6
1100S 1460W	10.5	105	124	608	1.7	90	5	406	2.13	34	6	<2	5	59	3.2	4.2	<.5	628	.38	.183	24	105	.66	2191	.086	2	1.41	.006	.11	1	<1	2.6	<1	.02	6
1100S 1440W	20.9	113	158	478	3.1	80	5	211	1.83	47	7	<2	5	128	2.4	9.5	<.5	471	.58	.333	23	64	.32	2647	.084	4	1.05	.009	.15	1	<1	1.9	<1	.08	3
1100S 1420W	13.2	41	90	296	1.6	47	3	147	2.24	29	3	<2	5	47	1.1	4.9	<.5	383	.25	.314	19	58	.37	1013	.070	1	1.20	.005	.09	1	<1	1.9	<1	.04	6
1100S 1400W	16.2	111	479	455	1.0	76	3	421	1.55	39	9	<2	6	147	3.7	6.4	.5	831	.86	.430	27	92	.38	1745	.082	6	1.05	.005	.11	2	<1	2.4	<1	.04	4
1100S 1380W	19.0	108	269	626	2.6	100	5	423	2.31	45	8	<2	5	100	2.7	6.8	<.5	796	.52	.329	25	106	.62	1869	.089	3	1.51	.006	.15	1	<1	2.8	<1	.05	6
1100S 1360W	16.6	95	324	587	1.7	96	4	340	2.04	37	7	<2	4	83	3.1	5.9	.5	795	.49	.303	26	111	.61	1983	.090	5	1.47	.006	.15	1	<1	2.7	1	.04	6
1100S 1340W	16.0	116	409	586	1.9	93	7	1025	1.66	41	8	<2	5	123	5.1	7.3	.5	805	.68	.317	27	88	.55	2739	.086	5	1.13	.005	.14	2	<1	2.7	<1	.03	4
1100S 1320W	8.6	37	70	268	2.9	37	5	228	3.13	26	3	<2	6	34	2.1	3.2	<.5	338	.22	.448	19	54	.32	1276	.050	2	1.50	.005	.07	1	<1	2.0	<1	.03	6
1100S 1300W	10.5	34	58	274	1.6	38	4	176	2.58	32	3	<2	5	33	2.4	3.8	<.5	322	.19	.311	18	50	.37	831	.065	3	1.23	.005	.08	1	<1	1.8	<1	.02	6
1100S 1280W	15.7	46	78	268	2.1	49	3	126	2.09	36	4	<2	4	61	1.5	5.6	<.5	387	.36	.293	20	53	.39	1075	.070	4	1.15	.005	.08	1	<1	1.7	<1	.04	5
1100S 1260W	9.1	34	45	222	2.6	38	5	169	2.77	27	2	<2	6	28	1.3	3.4	<.5	240	.19	.230	20	51	.43	536	.048	1	1.57	.003	.08	1	<1	2.0	<1	.02	5
1100S 1240W	11.2	44	62	249	2.5	46	5	179	2.99	33	2	<2	5	30	1.3	4.2	<.5	270	.14	.192	19	45	.49	475	.053	3	1.23	.004	.07	1	<1	1.8	<1	.02	5
1100S 1220W	13.1	79	74	464	2.8	78	10	368	2.16	38	4	<2	5	63	3.4	5.5	<.5	318	.40	.213	22	51	.64	1858	.068	4	1.26	.006	.11	1	<1	2.0	<1	.05	4
1100S 1200W	12.5	66	119	441	1.6	67	5	265	1.96	36	4	<2	4	67	2.4	4.9	<.5	360	.43	.217	20	57	.70	1584	.071	3	1.28	.004	.12	1	<1	1.9	<1	.05	5
RE 1100S 1200W	12.2	65	117	438	1.6	68	5	261	2.08	37	4	<2	4	68	2.2	5.1	<.5	352	.44	.233	20	55	.71	1599	.068	4	1.32	.005	.11	1	<1	2.0	<1	.05	5
1100S 1180W	9.5	47	68	262	2.3	44	3	138	1.76	27	3	<2	1	46	2.3	3.7	<.5	245	.33	.144	19	41	.42	1351	.044	2	1.02	.005	.08	1	<1	1.2	<1	.03	4
1100S 1160W	11.1	59	99	322	1.8	49	6	328	1.85	32	3	<2	3	44	1.8	4.4	<.5	333	.24	.169	21	49	.53	1346	.059	2	1.17	.005	.11	1	<1	1.7	<1	.03	5
1100S 1140W	11.5	50	124	274	1.7	46	3	195	1.46	27	3	<2	3	72	1.8	5.1	<.5	305	.44	.228	21	44	.43	1568	.061	3	.85	.005	.10	1	<1	1.5	<1	.05	3
1100S 1120W	10.9	87	153	640	1.9	89	5	336	2.00	32	6	<2	4	114	6.0	5.0	<.5	441	.80	.248	21	78	.73	2448	.073	3	1.35	.009	.16	1	<1	2.7	<1	.07	5
1100S 1100W	13.7	127	169	664	2.6	96	6	532	2.17	39	7	<2	2	88	5.7	5.4	.5	582	.48	.232	25	87	.82	3221	.066	4	1.65	.007	.17	1	<1	2.7	<1	.05	6
1100S 1080W	3.7	47	108	342	.5	50	18	588	2.93	13	3	<2	6	51	1.8	1.3	1.0	113	.22	.118	19	42	.49	395	.100	2	1.50	.010	.09	1	<1	2.2	<1	.07	5
1100S 1060W	4.2	46	75	264	1.8	35	5	212	2.19	12	2	<2	1	32	1.9	1.4	.6	134	.17	.059	17	42	.43	381	.055	1	1.45	.005	.08	<1	<1	1.4	<1	.05	7
1100S 1040W	4.6	41	100	386	1.3	50	7	263	2.52	15	2	<2	2	28	1.4	1.7	.5	135	.20	.105	18	47	.70	414	.057	2	1.74	.004	.09	1	<1	2.2	<1	.03	6
1100S 1020W	3.9	22	88	298	1.0	31	6	246	2.98	17	1	<2	4	19	1.7	1.7	.5	128	.14	.125	16	41	.54	252	.065	1	1.54	.004	.07	1	<1	1.9	<1	.03	6
1100S 1000W	3.4	22	80	258	1.1	27	4	203	2.50	12	1	<2	3	21	1.5	1.2	.6	129	.13	.079	17	36	.40	285	.088	2	1.33	.004	.07	1	<1	1.7	<1	.03	7
1100S 980W	1.9	17	59	284	.6	25	5	218	2.28	8	1	<2	2	15	1.3	.8	<.5	84	.15	.109	15	34	.56	189	.046	2	1.43	.003	.06	1	<1	1.6	<1	.02	6
1100S 960W	1.1	12	43	171	1.7	12	3	98	1.29	3	1	<2	1	11	2.0	<.5	<.5	53	.10	.043	16	21	.23	244	.044	2	1.03	.004	.04	<1	<1	1.4	<1	.02	5
1100S 940W	2.1	18	84	336	1.5	28	6	244	2.90	12	1	<2	5	16	1.9	.9	<.5	96	.17	.098	15	39	.57	193	.060	2	1.61	.004	.08	1	<1	1.9	<1	.02	6
STANDARD C3	26.8	65	37	165	5.4	38	13	815	3.23	58	21	<2	21	28	22.2	13.6	24.7	85	.54	.099	18	173	.62	145	.092	18	1.81	.033	.17	15	1	4.0	1	.03	8
STANDARD G-2	1.6	3	2	47	<.1	9	5	556	1.99	1	2	<2	5	72	<.2	<.5	<.5	46	.61	.107	8	81	.59	226	.131	2	.92	.074	.53	2	<1	2.1	<1	.02	5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm
1100S 920W	1.4	12	45	216	1.3	16	3	154	1.42	6	1	<2	3	15	2.1	<.5	<.5	62	.14	.041	15	26	.29	186	.059	3	1.07	.004	.07	1	<1	1.8	<1	.03	5
1100S 900W	3.4	25	121	370	.4	34	4	218	2.20	15	1	<2	4	21	2.2	1.2	.7	161	.21	.087	16	42	.47	240	.056	4	1.27	.003	.07	1	<1	2.2	<1	.02	5
1100S 880W	3.7	36	111	648	1.2	47	5	261	2.53	18	2	<2	2	26	2.3	1.6	.6	215	.26	.134	16	45	.53	256	.048	1	1.54	.003	.07	1	<1	2.2	<1	.03	5
1100S 860W	4.4	31	116	358	.3	42	4	244	1.94	17	1	<2	2	23	1.1	1.6	.7	163	.19	.078	13	40	.56	270	.063	5	1.28	.003	.07	1	<1	1.8	<1	.03	5
1100S 840W	3.2	24	88	305	.7	33	5	232	2.05	15	1	<2	3	23	1.3	1.3	.6	124	.20	.096	16	37	.52	208	.056	1	1.24	.002	.08	<1	<1	2.0	<1	.05	6
1100S 820W	1.5	11	45	169	1.1	17	4	168	1.60	7	1	<2	5	12	.7	<.5	<.5	76	.14	.043	17	27	.41	166	.052	1	1.27	.003	.05	<1	<1	2.2	<1	.03	6
1100S 800W	2.2	18	48	246	1.1	28	4	194	1.76	10	1	<2	3	19	1.3	.8	<.5	103	.21	.071	16	33	.48	236	.041	2	1.30	.003	.08	<1	<1	2.3	<1	.06	6
RE 1100S 800W	2.3	18	52	242	1.0	27	4	197	1.77	10	1	<2	3	18	1.2	.8	<.5	102	.21	.069	16	33	.46	239	.040	2	1.25	.002	.07	<1	<1	2.1	<1	.04	5
STANDARD C3	26.7	63	37	158	5.4	34	12	782	3.07	58	20	<2	21	27	22.7	14.9	23.3	84	.57	.101	17	189	.58	142	.094	20	1.80	.029	.18	17	1	4.5	1	.03	8
STANDARD G-2	1.8	3	3	48	<.1	9	5	614	2.04	<1	2	<2	5	74	<.2	<.5	<.5	44	.70	.112	8	.90	.62	234	.145	3	.98	.053	.56	5	<1	2.7	<1	<.02	5

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

GEOCHEMICAL ANALYSIS CERTIFICATE



Aurora Geosciences Ltd. PROJECT Hyland R. File # A103175

P.O. Box 31097, 11 & 12 -, Whitehorse YT Y1A 5P7 Submitted by: Scott Casselman

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	
SI	.4	4	<2	2	<.1	1	<1	6	.02	1	<1	<2	<1	4	<.2	<.5	<.5	<1	.14	.001	<1	2<.01	8<.001	<1	.02	.062	.01	<1	<1	.2	<1<.02	<1			
ZAP01-005	22.4	71	35	231	1.0	24	1	97	.78	10	6	<2	2	56	3.4	2.6	<.5	503	.20	.086	6	43	.07	2707	.060	4	.55	.009	.15	1	<1	1.5	<1	.02	2
ZAP01-006	19.3	49	28	254	.6	26	1	133	.86	13	8	<2	5	69	2.7	1.0	<.5	363	.22	.101	10	37	.10	2083	.053	4	.59	.010	.17	2	<1	1.7	<1	.03	3
ZAP01-007	8.1	23	92	120	.1	25	<1	903	.64	13	2	<2	<1	55	.5	1.1	<.5	90	.38	.131	3	44	.04	491	.012	122	.27	.005	.02	3	<1	.7	<1<.02	<1	
ZAP01-008	25.8	69	109	109	1.5	24	1	275	.79	8	12	<2	2	493	11.0	3.0	<.5	691	3.02	1.473	15	47	.16	3138	.052	10	.83	.010	.21	4	<1	2.5	<1	.04	4
ZAP01-009	41.4	108	250	193	1.2	32	1	239	.82	7	7	<2	2	33	2.9	2.5	<.5	661	.15	.073	6	32	.13	1550	.049	3	.47	.006	.10	1	<1	1.9	<1<.02	3	
RE ZAP01-009	40.8	106	251	197	1.1	34	1	241	.85	7	7	<2	1	32	2.9	2.5	<.5	675	.15	.071	6	33	.13	1482	.047	4	.45	.006	.10	1	<1	1.9	<1	.02	3
STANDARD DS3	8.8	113	30	153	.3	35	11	786	3.04	28	6	<2	4	27	5.2	5.3	5.2	73	.51	.090	15	177	.55	158	.091	3	1.68	.028	.16	3	<1	3.9	1	.02	6

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
 UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
 - SAMPLE TYPE: ROCK R150 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 17 2001 DATE REPORT MAILED: *Sept 26/01* SIGNED BY: *C.L.* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE



Aurora Geosciences Ltd. PROJECT Hyland R. File # A103176

P.O. Box 31097, 11 & 12 -, Whitehorse YT Y1A 5P7 Submitted by: Scott Casselman

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	
SLT01-001	9.4	64	87	1727	.8	107	10	576	2.45	39	4	<2	5	84	20.2	3.1	<.5	207	.67	.164	21	35	.61	2048	.040	5	1.06	.006	.12	<1	<1	2.6	<1	.08	4
SLT01-002	10.4	65	112	1727	.8	104	9	537	2.47	39	4	<2	5	87	19.4	3.1	<.5	243	.61	.176	21	40	.59	2106	.047	4	1.18	.006	.12	<1	<1	2.6	<1	.06	4
SLT01-003	10.9	70	136	1785	1.0	110	6	326	2.02	30	5	<2	4	83	17.8	3.0	<.5	272	.62	.156	20	43	.44	2042	.050	3	1.05	.006	.11	1	<1	2.5	<1	.07	4
SLT01-004	9.8	80	135	2105	1.1	126	8	473	2.30	39	6	<2	4	86	26.4	3.2	<.5	285	.65	.165	20	46	.49	2260	.049	5	1.20	.007	.12	<1	<1	2.6	<1	.08	4
SLT01-005	11.4	84	179	2042	1.4	129	6	417	2.10	33	7	<2	4	94	23.4	3.1	<.5	332	.69	.172	21	49	.49	2276	.057	4	1.13	.007	.12	<1	<1	2.6	<1	.08	4
RE SLT01-005	11.7	86	148	2157	1.3	137	6	443	2.21	34	7	<2	4	96	24.1	3.3	<.5	336	.73	.174	21	52	.47	2344	.057	3	1.20	.008	.13	2	<1	2.6	<1	.08	4
SLT01-006	12.8	119	216	3016	1.5	165	7	485	2.54	47	11	<2	4	92	35.3	3.5	.6	401	.73	.152	19	61	.47	2308	.074	3	1.41	.008	.14	1	<1	3.5	<1	.09	5
SLT01-007	11.6	117	270	3155	1.5	174	6	521	2.44	45	12	<2	3	102	36.0	3.3	.6	461	.79	.155	19	66	.48	2155	.067	4	1.38	.008	.15	2	<1	3.4	<1	.09	5
SLT01-008	15.0	109	250	2740	1.3	172	9	818	2.40	49	12	<2	4	104	34.0	3.4	.5	525	.76	.197	17	64	.47	2206	.077	4	1.32	.009	.17	4	<1	3.0	<1	.09	5
SLT01-009	19.2	146	417	2890	1.7	182	7	734	2.49	51	13	<2	3	101	36.4	3.4	.7	578	.84	.199	20	75	.52	2172	.074	4	1.51	.010	.17	8	<1	3.6	<1	.09	5
SLT01-010	11.8	215	225	4325	2.3	268	6	599	2.43	48	14	<2	2	115	55.7	3.5	.7	592	1.10	.153	20	101	.55	1942	.066	5	1.64	.011	.16	<1	<1	3.8	<1	.09	6
STANDARD DS3	9.2	121	34	150	.3	36	12	813	2.99	29	5	<2	4	27	5.4	5.4	5.2	72	.50	.090	16	184	.55	158	.089	3	1.65	.028	.15	3	<1	3.5	1	.03	6
STANDARD G-1	1.1	2	6	37	<.1	4	3	442	1.55	1	3	<2	5	60	<.2	<.5	<.5	31	.48	.090	7	12	.45	200	.110	3	.72	.057	.37	2	<1	1.8	<1	<.02	4

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
 UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
 - SAMPLE TYPE: SILT SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 17 2001 DATE REPORT MAILED: *Sept 28/01* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Aurora Geosciences Ltd. PROJECT Hyland R. File # A103177

P.O. Box 31097, 11 & 12 St., Whitehorse YT Y1A 5P7 Submitted by: Scott Casselman



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	ppm	ppm	ppm	ppm	%	ppm	
SI	1.0	2	2	36	<.1	4	3	439	1.60	1	3	<2	6	65	<.2	<.5	<.5	30	.48	.096	8	12	.43	205	.119	2	.74	.062	.38	2	<1	2.1	<1	<.02	4
TR-001	42.0	120	1939	1023	2.0	133	18	1746	2.56	58	14	<2	7	149	5.6	4.4	5.2	1174	.57	.284	27	114	.52	2390	.102	4	1.60	.010	.13	10	<1	3.3	<1	.06	6
TR-002	48.7	152	1916	1069	2.4	135	16	1517	2.47	61	16	<2	7	144	6.1	4.8	4.2	1222	.59	.265	27	107	.57	2770	.132	2	1.57	.010	.16	7	<1	4.3	1	.07	6
TR-003	37.9	170	510	885	2.6	120	13	1199	2.95	86	22	<2	9	185	10.9	8.6	1.8	1295	.75	.242	30	97	.43	1612	.173	8	1.68	.020	.27	3	<1	6.2	1	.11	7
TR-004	31.2	151	295	705	1.7	86	7	650	3.07	61	15	<2	9	121	9.0	8.6	1.1	847	.37	.183	23	64	.37	303	.148	4	1.26	.026	.27	1	<1	4.2	1	.31	5
TR-005	32.4	103	1892	967	1.7	126	14	1473	2.73	56	11	<2	7	141	4.8	4.1	4.2	1167	.63	.324	26	123	.55	2142	.103	5	1.61	.009	.12	11	<1	3.5	<1	.08	6
TR-006	24.6	145	323	684	1.5	85	8	775	2.63	55	13	<2	8	133	7.5	6.3	1.0	752	.43	.198	24	59	.33	1174	.121	3	1.14	.013	.17	1	<1	4.2	<1	.14	5
TR-007	35.5	151	223	789	1.6	76	6	501	3.53	60	13	<2	9	115	8.4	8.9	1.0	634	.34	.194	21	48	.31	277	.145	3	1.16	.025	.28	1	<1	3.9	1	.36	5
TR-008	30.1	168	301	834	1.8	87	9	632	3.35	61	13	<2	9	126	9.9	8.1	.8	649	.36	.200	23	53	.35	449	.138	2	1.37	.022	.25	1	<1	3.8	1	.26	5
RE TR-008	29.3	169	305	843	1.7	86	9	633	3.28	60	14	<2	10	124	9.9	7.9	.8	644	.36	.193	23	52	.35	425	.138	5	1.33	.022	.25	1	<1	3.8	1	.26	5
TR-009	14.4	60	277	372	.7	48	5	302	2.87	49	5	<2	6	58	2.0	2.5	.5	473	.26	.239	19	66	.30	1087	.068	2	1.46	.006	.09	1	<1	2.5	<1	.08	6
TR-010	50.6	117	2663	956	1.8	129	16	1825	2.83	52	9	<2	7	99	7.1	3.2	8.5	1159	.43	.236	25	102	.49	1676	.088	2	1.67	.007	.11	9	<1	3.6	<1	.06	7
TR-011	32.7	153	2312	1944	1.2	388	34	3481	2.91	82	23	<2	11	227	13.9	5.8	8.6	2333	1.51	.272	47	202	.97	4401	.204	7	2.58	.009	.21	14	<1	7.0	1	.04	7
TR-012	39.9	214	1008	1471	1.2	245	21	2259	3.41	99	27	<2	10	193	16.2	6.6	3.1	2164	1.32	.255	41	160	.89	3563	.234	5	2.60	.014	.27	8	<1	8.2	1	.07	11
TR-013	15.8	83	366	504	1.5	63	6	399	2.62	53	7	<2	6	75	2.6	3.0	.7	576	.33	.235	20	69	.27	1304	.072	5	1.52	.007	.09	1	<1	2.6	<1	.09	6
TR-014	11.3	90	210	476	1.7	63	7	455	2.51	35	8	<2	7	47	3.4	2.1	.5	386	.25	.162	22	62	.37	1239	.080	4	1.55	.006	.09	1	<1	3.7	<1	.04	6
TR-015	7.6	55	114	260	1.8	38	6	337	2.42	22	4	<2	7	21	2.8	1.1	<.5	212	.14	.103	21	43	.35	1031	.072	2	1.31	.006	.07	<1	<1	3.4	<1	<.02	6
TR-016	81.1	217	5108	1637	1.4	224	28	3836	3.22	78	15	<2	8	135	15.3	5.3	7.8	2040	.72	.267	35	130	.69	2793	.111	4	2.19	.008	.13	37	<1	5.2	<1	.07	8
TR-017	40.0	155	2419	1987	1.1	389	22	3129	2.94	78	28	<2	13	231	15.2	6.6	7.9	2771	1.88	.226	57	189	1.01	4754	.228	7	3.07	.011	.31	9	<1	8.7	1	.06	12
STANDARD DS3	8.8	113	35	153	.3	35	11	786	3.04	28	6	<2	4	27	5.2	5.3	5.2	73	.51	.090	15	177	.55	158	.091	3	1.68	.028	.16	3	<1	3.9	1	.02	6

GROUP 1DX - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP-ES.
UPPER LIMITS - AG, AU, HG, W = 100 PPM; MO, CO, CD, SB, BI, TH, U & B = 2,000 PPM; CU, PB, ZN, NI, MN, AS, V, LA, CR = 10,000 PPM.
- SAMPLE TYPE: SOIL SS80 60C Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 17 2001 DATE REPORT MAILED: *Sept 26/01* SIGNED BY: *C. Toy* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

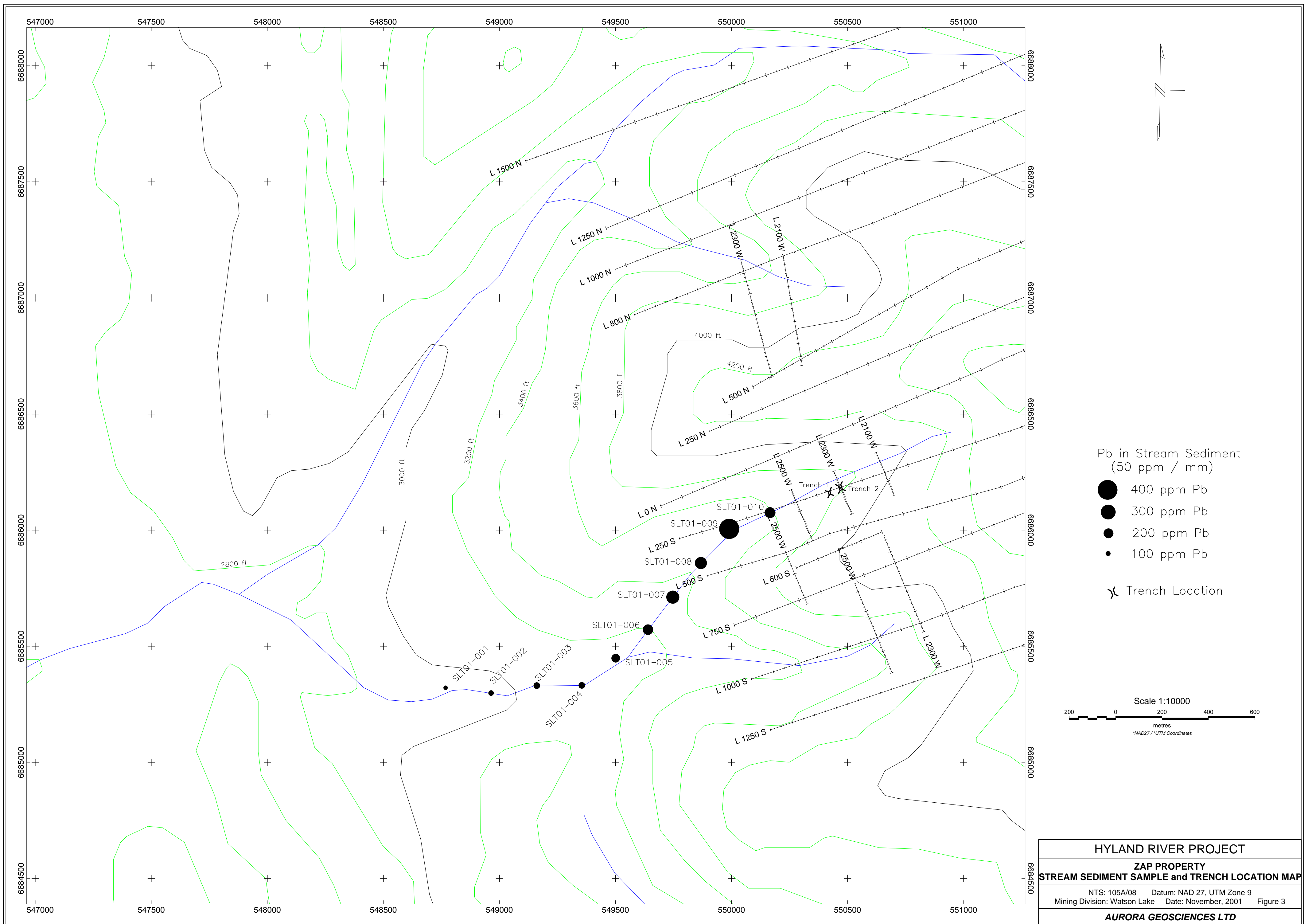
APPENDIX IV

GRID GPS COORDINATES

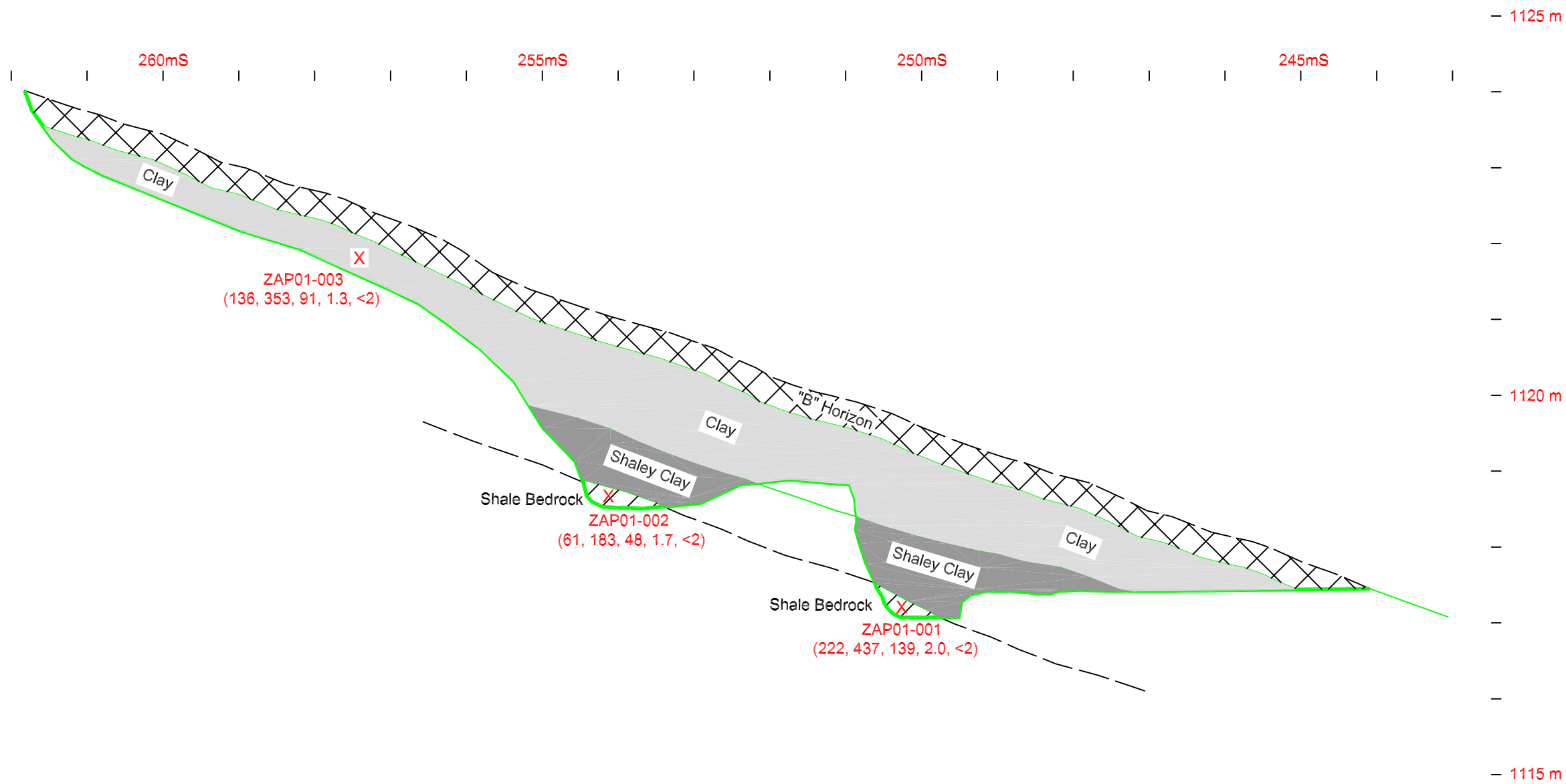
2001 GPS SURVEY POINTS

Property Grid		GPS reading (UTM - NAD 27)		Comments
Northing	Easting	Easting	Northing	
1500	0	551989	6688615	
1500	-1400	550620	6688127	in dense trees (on cut line bearing 70 deg.)
1250	-1650	550707	6687818	
1000	0	552156	6688155	
800	0	552236	6687959	
800	-1450	550851	6687423	
800	-1700	550608	6687322	
800	-2100	550222	6687181	
800	-2300	550035	6687108	
500	0	552330	6687699	
500	-1500	550977	6687125	
300	-2300	550174	6686659	
0	0	552485	6687283	
0	-1400	551166	6686735	
0	-1500	551076	6686690	
-200	-2500	550257	6686174	
-250	-1500	551250	6686444	
-250	-2450	550318	6686134	
-250	-2750	550016	6686035	
-440	-2500	550369	6685959	coincides with 1995 grid point L500S/2380W
-500	-1600	551160	6686185	
-500	-2300	550423	6685985	
-500	-2500	550234	6685903	
-740	-2500	550319	6685704	2001 grid survey point
-750	-1650	551269	6686077	
-750	-3000	550012	6685591	elev = 3460'
-900	-800	552127	6686128	
-900	-1040	551826	6685822	
-900	-1500	551487	6685969	
-1000	0	552912	6686320	
-1000	-800	552159	6686030	
-1000	-1750	551220	6685754	
-1000	-2200	550818	6685601	
-1000	-2550	550513	6685500	
-1100	-800	552193	6685932	

Note. negative Property Grid Northing numbers are South and negative Easting numbers are West

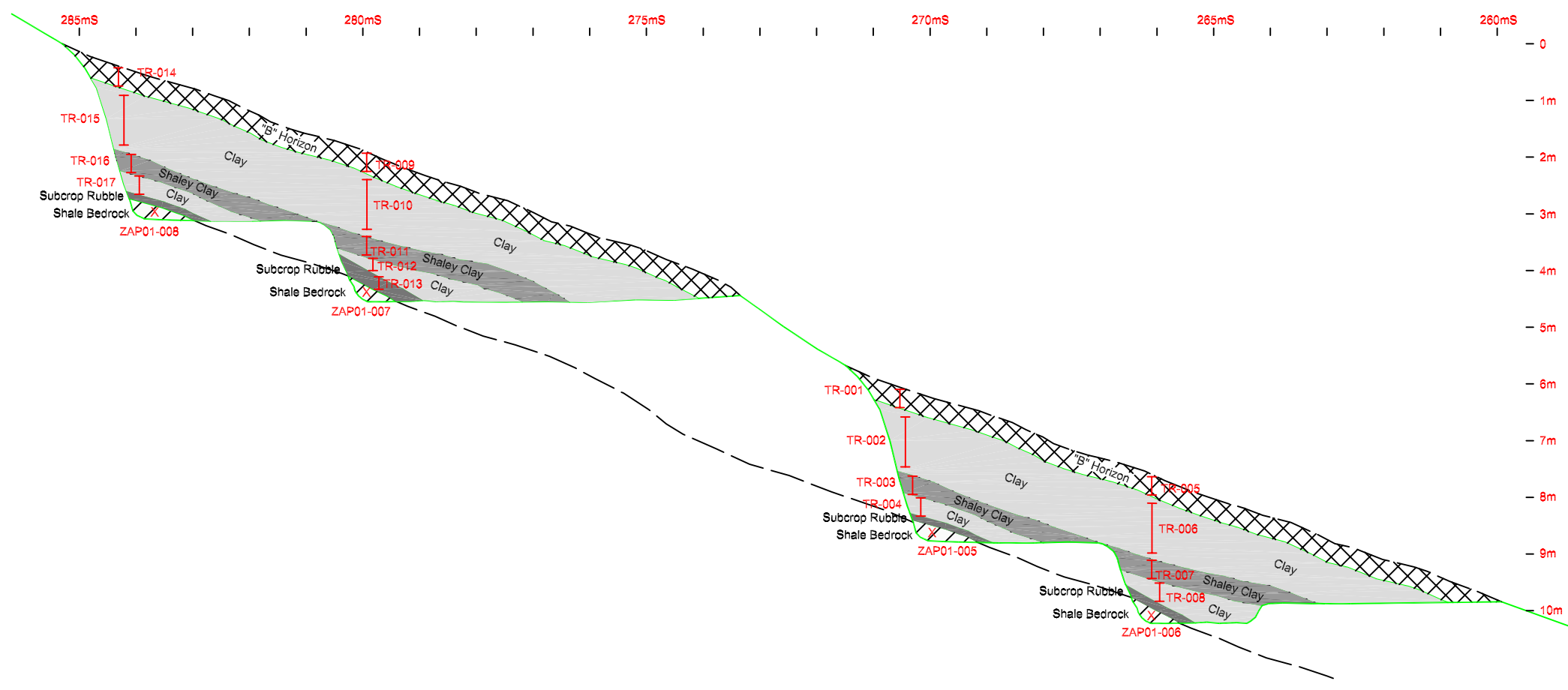


HYLAND RIVER PROJECT
ZAP PROPERTY
STREAM SEDIMENT SAMPLE and TRENCH LOCATION MAP
 NTS: 105A/08 Datum: NAD 27, UTM Zone 9
 Mining Division: Watson Lake Date: November, 2001 Figure 3
AURORA GEOSCIENCES LTD

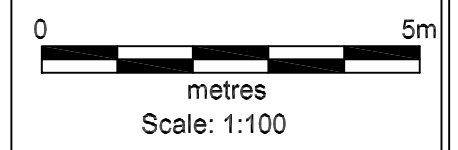


X Sample Number
(Pb ppm, Zn ppm, Cu ppm, Ag ppm, Au ppb)

HYLAND RIVER PROSPECT	
HAND TRENCH #1 L 250 S / 2350 W	
NTS: 105 A/8	FIGURE 4.
Mining District: Watson Lake	
Job: AGL-28-YT	Date: 15 Dec 01
AURORA GEOSCIENCES LTD.	



Sample #	Pb ppm	Zn ppm	Cu ppm	Ag ppm	Au ppb
TR-001	1939	1023	120	2.0	<2
TR-002	1916	1069	152	2.4	<2
TR-003	510	885	170	2.6	<2
TR-004	295	705	151	1.7	<2
TR-005	1892	967	103	1.7	<2
TR-006	323	684	145	1.5	<2
TR-007	223	789	151	1.6	<2
TR-008	301	834	168	1.8	<2
TR-009	277	372	60	0.7	<2
TR-010	2663	956	117	1.8	<2
TR-011	2312	1944	153	1.2	<2
TR-012	1008	1471	214	1.2	<2
TR-013	366	504	83	1.5	<2
TR-014	210	476	90	1.7	<2
TR-015	114	260	55	1.8	<2
TR-016	5108	1637	217	1.4	<2
TR-017	2419	1987	155	1.1	<2



**HYLAND RIVER
PROSPECT**

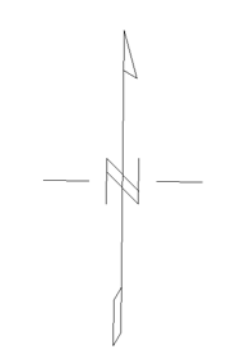
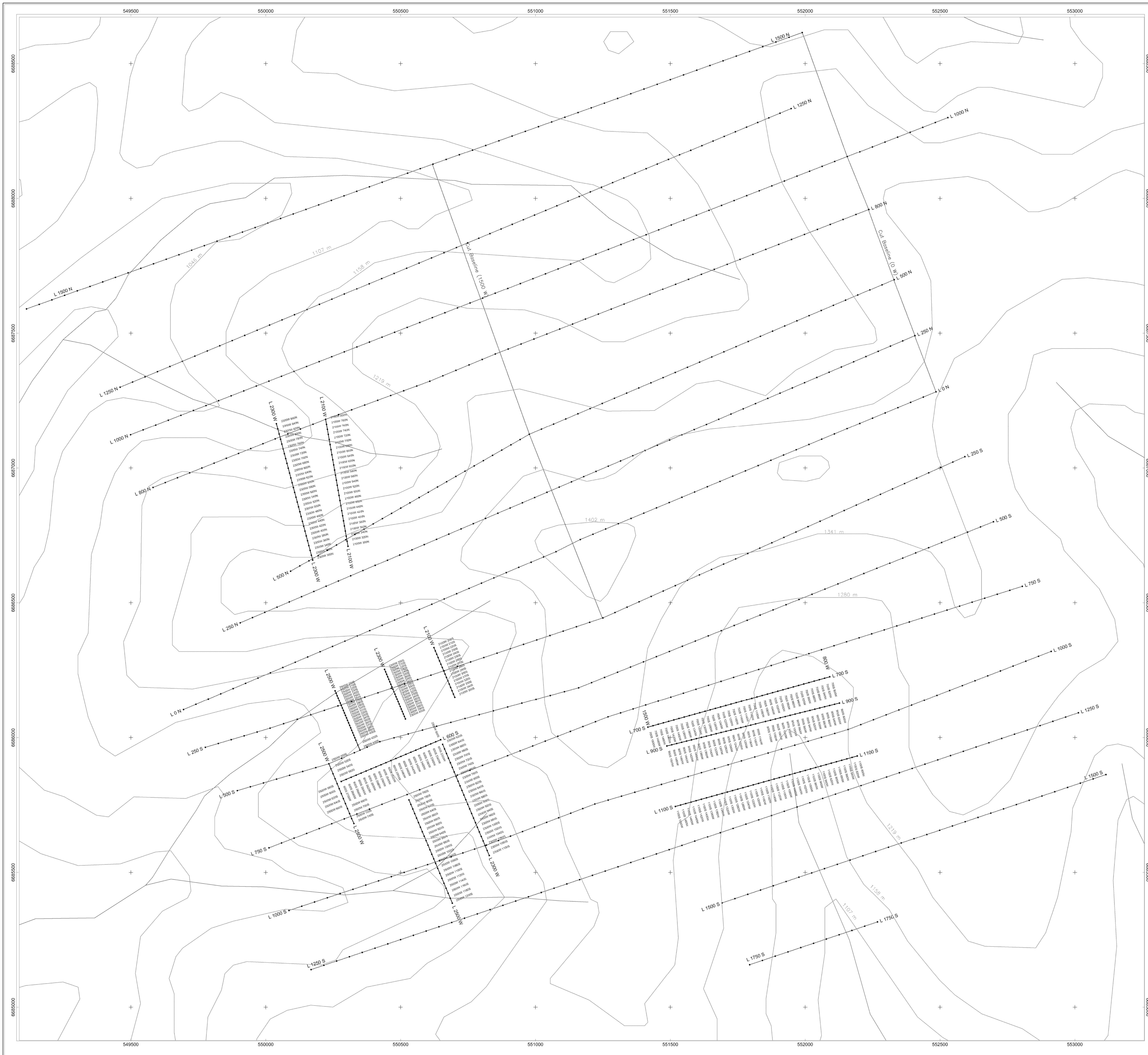
**HAND TRENCH #2
LINE 2300 W**

NTS: 105 A/8 FIGURE 5.

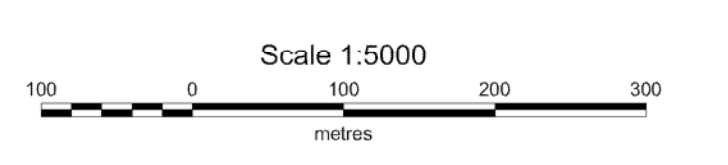
Mining District: Watson Lake

Job: AGL-28-YT Date: 15 Dec 01

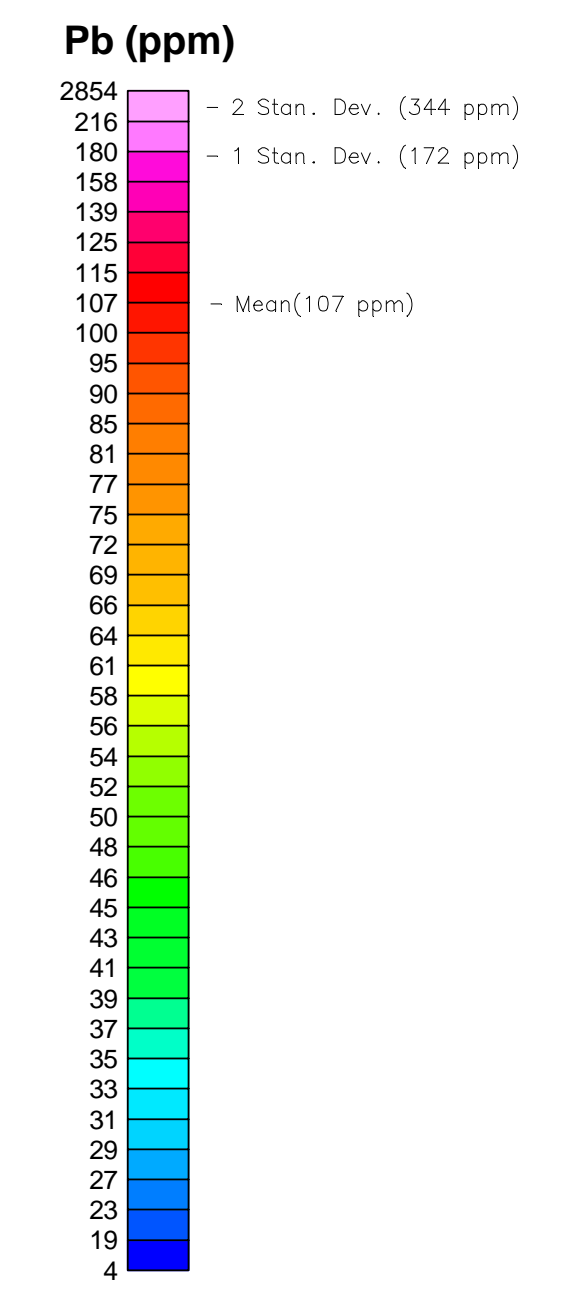
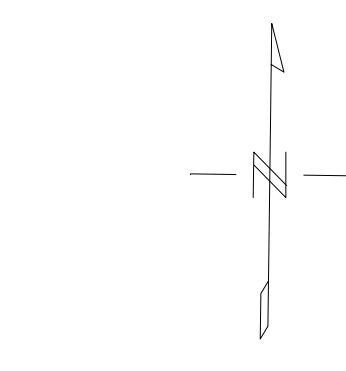
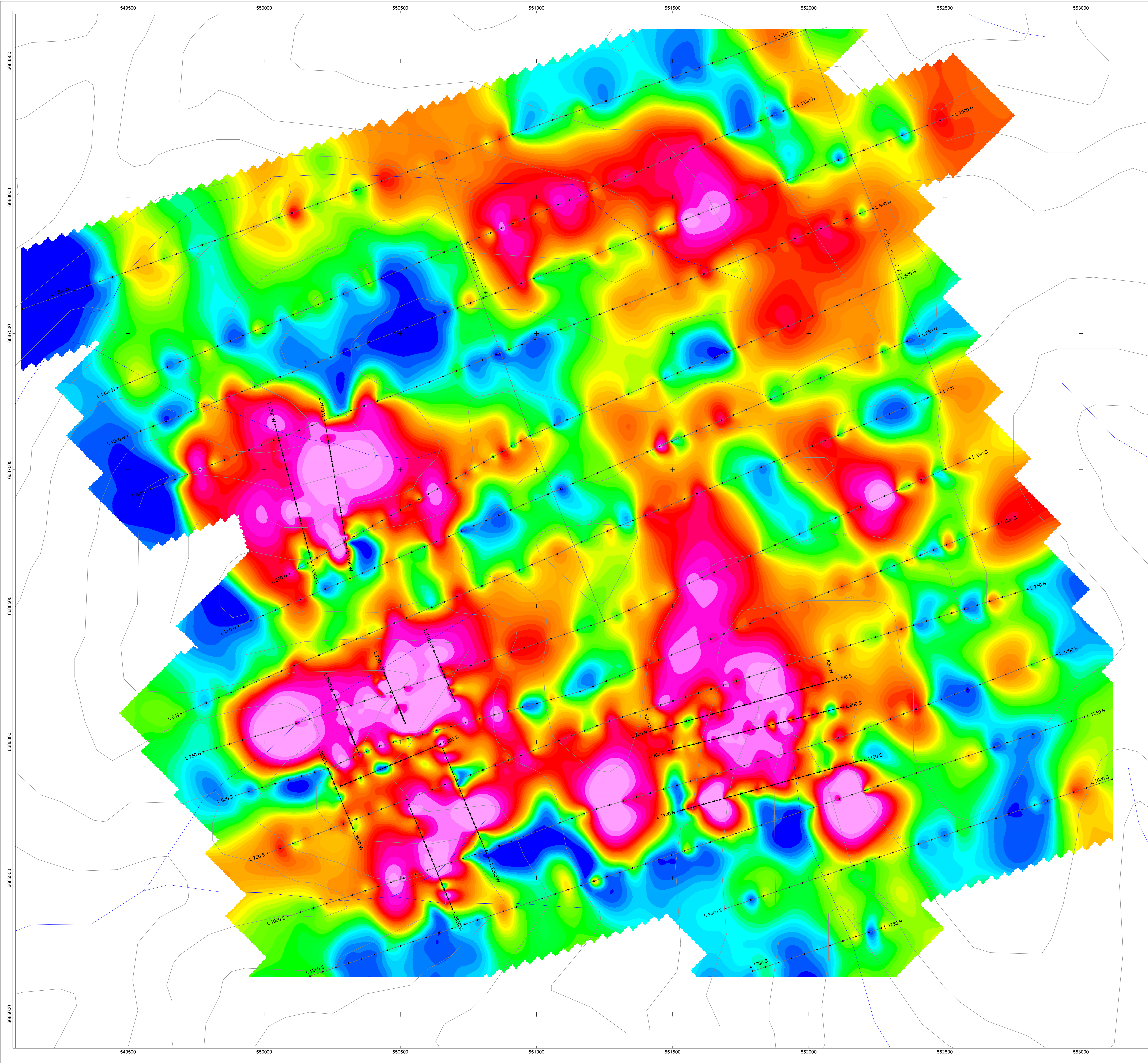
AURORA GEOSCIENCES LTD.



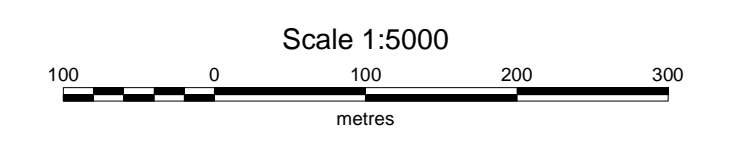
 1995 Soil Sample Grid
 2001 Soil Sample Grid



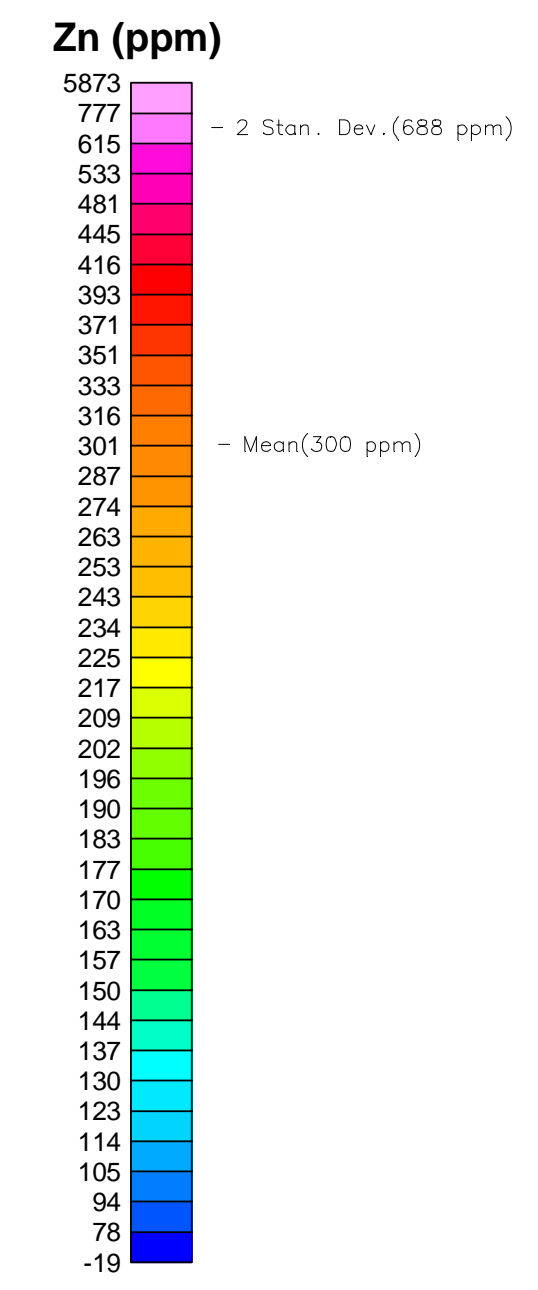
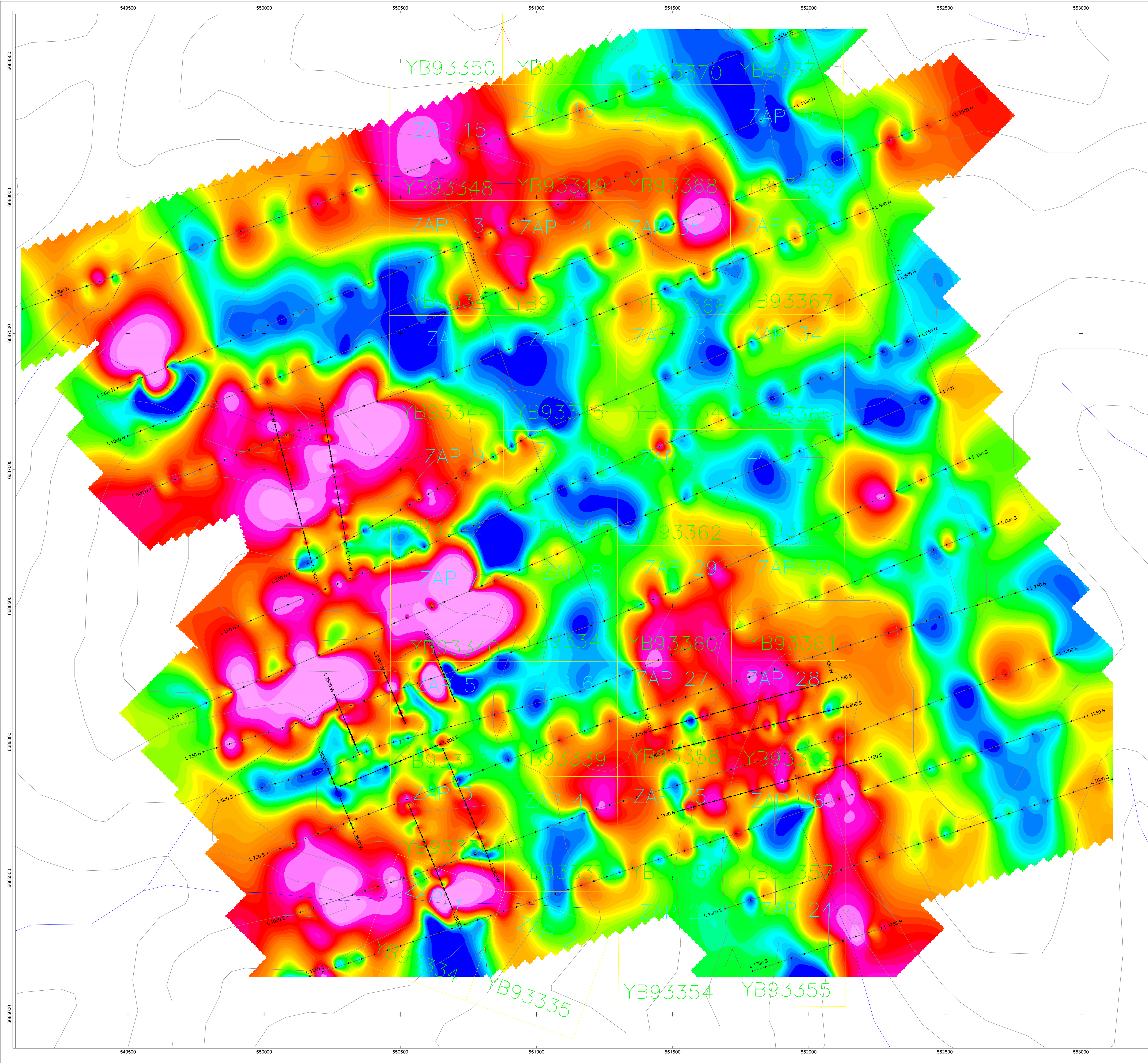
4763 NWT Ltd
 ZAP PROPERTY
 2001 SOIL SAMPLE LOCATIONS
 NTS: 105A-08 Datum: NAD 27, UTM Zone 9
 Mining Division, Watson Lake Date: December, 2001
AURORA GEOSCIENCES LTD



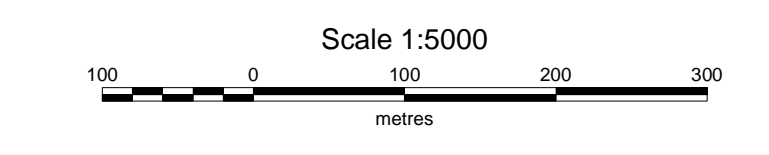
1995 Soil Sample Grid
 2001 Soil Sample Grid



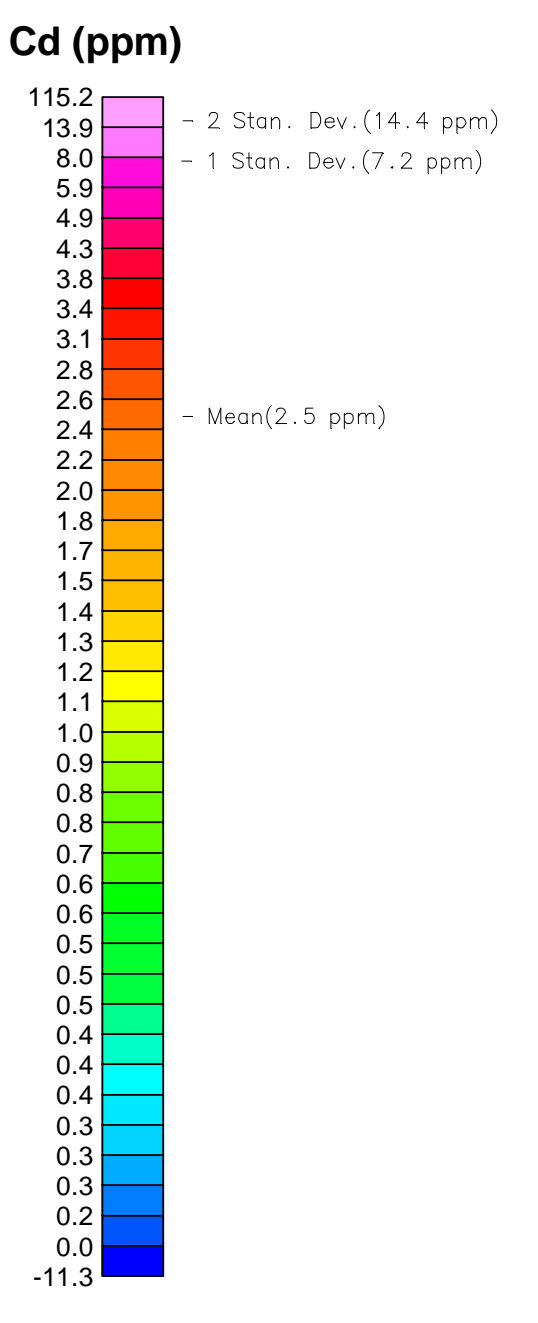
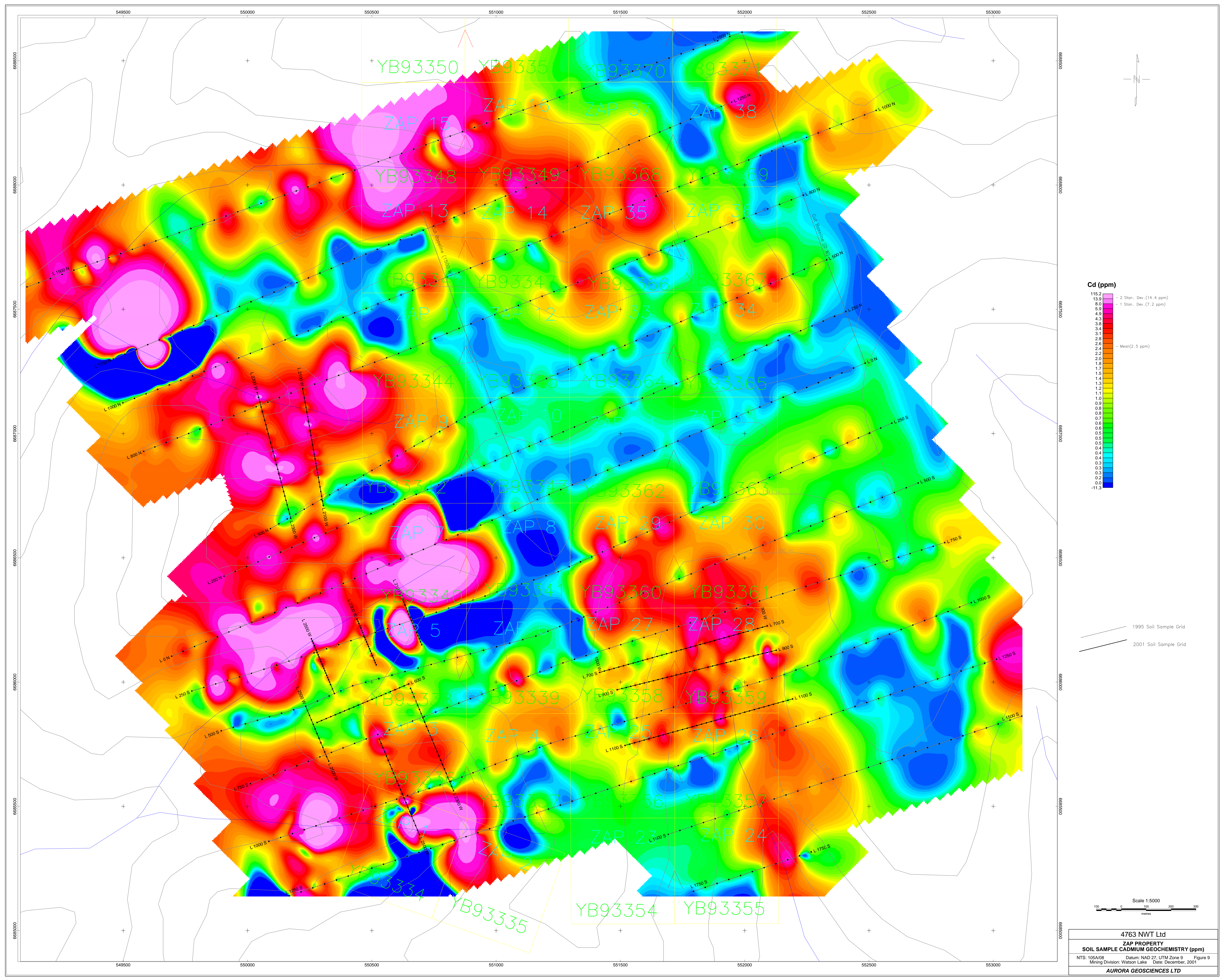
4763 NWT Ltd
ZAP PROPERTY
SOIL SAMPLE LEAD GEOCHEMISTRY (ppm)
 NTS: 105A/08 Datum: NAD 27, UTM Zone 9 Figure 7
 Mining Division: Watson Lake Date: December, 2001
AURORA GEOSCIENCES LTD



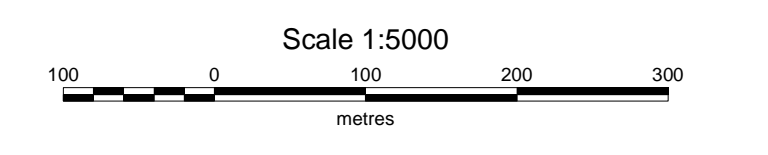
1995 Soil Sample Grid
 2001 Soil Sample Grid

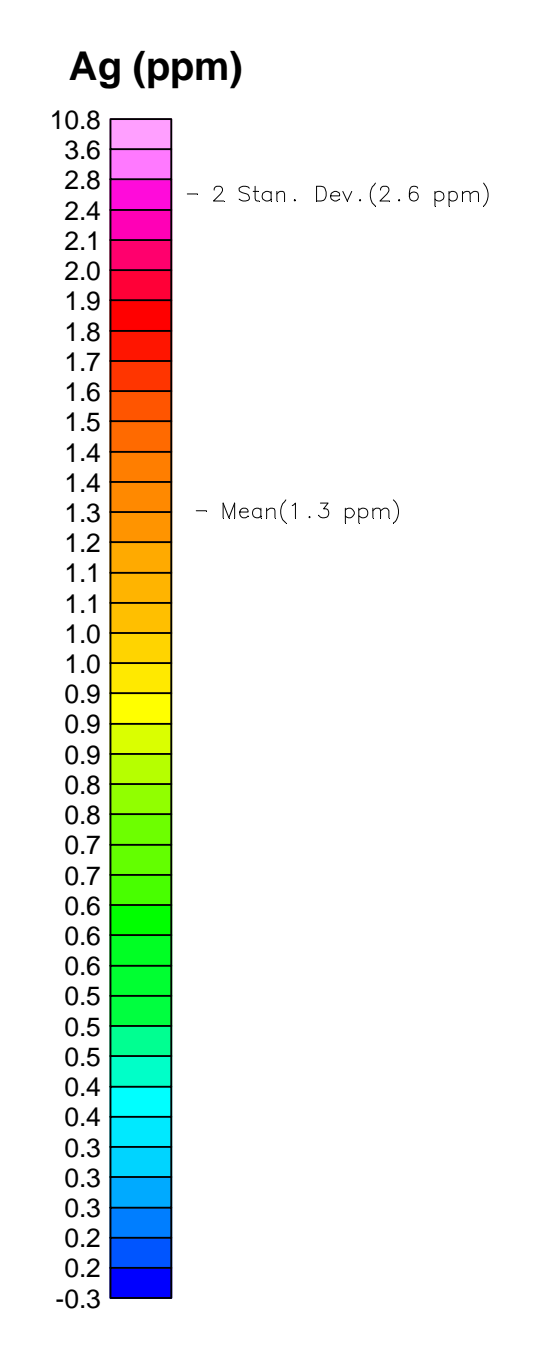
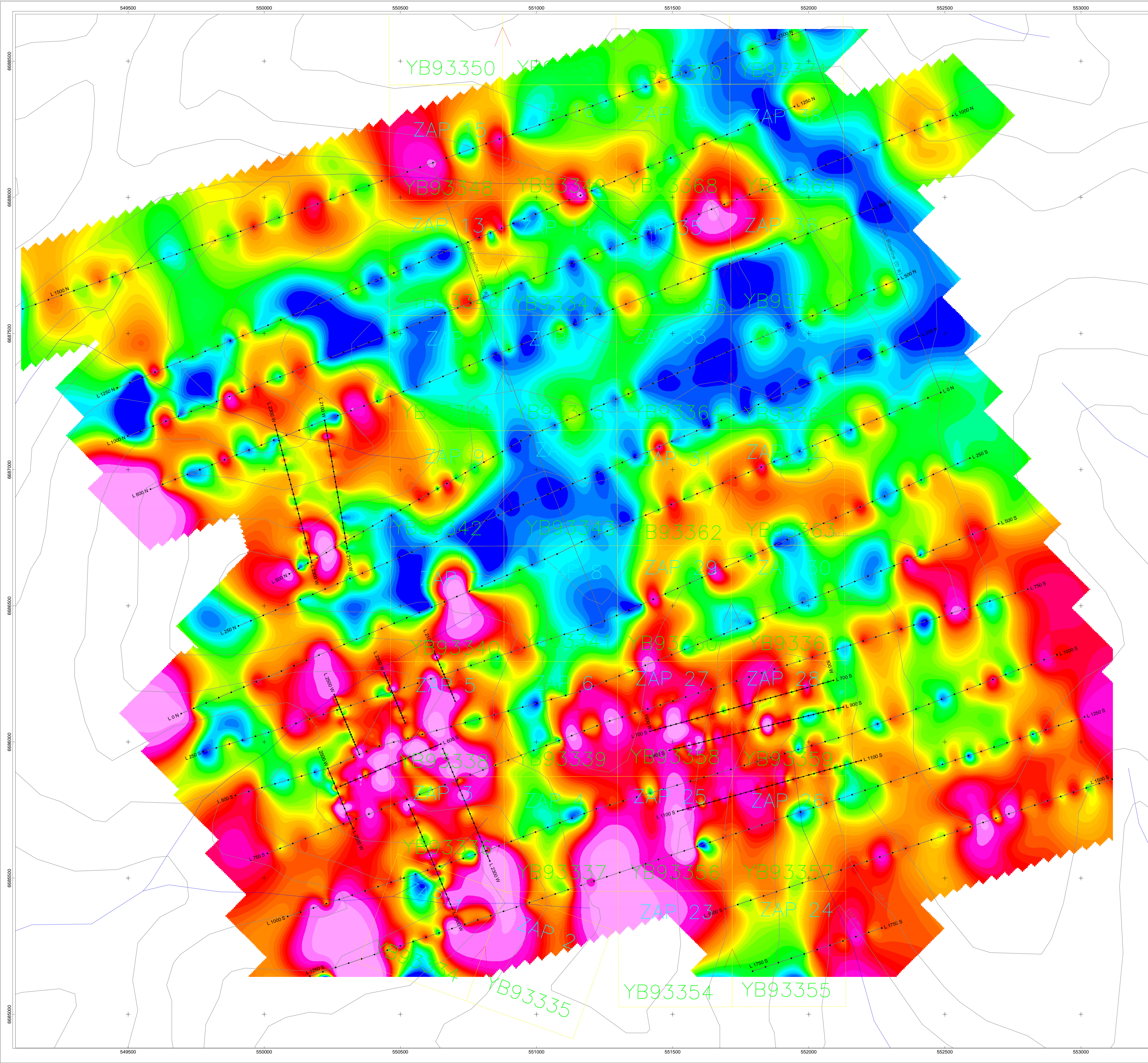


4763 NWT Ltd	
ZAP PROPERTY	
SOIL SAMPLE ZINC GEOCHEMISTRY (ppm)	
NTS: 105A/08	Datum: NAD 27, UTM Zone 9
Mining Division: Watson Lake	Date: December, 2001
AURORA GEOSCIENCES LTD	

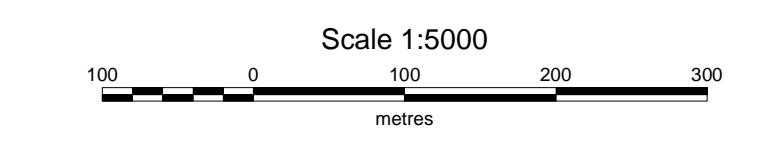


1995 Soil Sample Grid
 2001 Soil Sample Grid





1995 Soil Sample Grid
 2001 Soil Sample Grid



4763 NWT Ltd
ZAP PROPERTY
SOIL SAMPLE SILVER GEOCHEMISTRY (ppm)
 NTS: 105A/08 Datum: NAD 27, UTM Zone 9 Figure 10
 Mining Division: Watson Lake Date: December, 2001
AURORA GEOSCIENCES LTD