GEOLOGICAL AND GEOCHEMICAL REPORT

ON THE

GODDELL/ CARBON HILL PROPERTY
(MOM, POP, BERG, STEN, TECH, MIL & MB CLAIMS)

WHITEHORSE MINING DISTRICT
YUKON TERRITORY, CANADA
NTS MAP SHEET 105D/3

Centred at Latitude: 60° 10' 45"N, Longitude: 135° 15' 00"W
Work Performed: June 28 to September 28, 1998

FOR

OMNI RESOURCES INC./ARKONA RESOURCES INC
#910 – 700 West Pender Street
Vancouver, B. C. V6C 1G8

094028

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February, 1999

This report has been examined by
the Geological Evaluation Unit
under Section 53 (4) Yukon Quartz
Mining Act and is allowed as
representation work in the amount
of $ 52,100 .

for Regional Manager, Exploration and
Geological Services for Commissioner
of Yukon Territory.

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SUMMARY

The Goddell/Carbon Hill group of claims is located approximately 60 km south of Whitehorse in the Whitehorse Mining District. Access to the property is provided via the Alaska Highway, South Klondike Highway and Annie Lake Road thence via 4-wheel drive road along the west side of Becker Creek. The Becker Creek road connects with individual drill access roads on the property.

The property is located near the eastern margin of the Coast Plutonic Complex within the Boundary Ranges of the Coast Mountain physiographic division. The claims cover a sequence of foliated Mesozoic (Cretaceous) granitoid rocks flanked by metamorphosed and unmetamorphosed sedimentary and volcanic rocks. Irregular belts of metavolcanic and metasedimentary rocks of Mesozoic, Paleozoic and Precambrian age occur as roof pendants. These plutonic rocks and associated roof pendants are locally overlain and intruded by Eocene Mount Skukum Group rhyolites.

The area drained by the upper reaches of the Wheaton River has been explored for gold and minerals since the late 1800's when prospectors passed through on their way to the interior. Prospecting and geological mapping commenced in the early part of this century and culminated in the discovery of several gold, silver and base metal occurrences. By the First World War, adits had been driven into structures on Gold Hill, Tally Ho Mountain, Mount Stevens and Carbon Hill. These areas experienced limited gold production until the mid 1920's. Sporadic base metal exploration was performed at the Goddell, Porter and Becker-Cochrane showings on Carbon Hill from about 1909 to the mid 1970's. The current gold exploration rush began in 1981 with the discovery, by AGIP Canada Ltd., of the Mount Skukum gold deposit which was brought into production in February, 1986 and produced 80,000 ounces of gold from 220,000 tons of ore.

The 1998 program on the Goddell/Carbon Hill property comprised detailed geological mapping, grid controlled and contour soil sampling and bulldozer trenching over two selected, favourable target areas designated as The Sinter Cap – Conglomerate Creek area and Antimony Creek area. The former occurs along the major Goddell-Becker-Cochrane Structure which hosts the Goddell gold deposit and Becker-Cochrane antimony deposit. These mesothermal vein type deposits are localized approximately 3.6 km apart along this fault. The east-west trending Antimony Creek zone exhibits characteristics similar to the Goddell deposit and occurs 2.1 km south of Goddell Gully. Significant barite-stibnite veins are exposed on the north side of Antimony Creek suggesting a mineralogical setting equivalent to the Goddell zone.

A total of 126 rock samples, 696 soil samples and 17 stream silt samples were collected for analysis. Drill targets and prospective areas requiring further geological and geochemical assessment have been identified in the Sinter Cap area and Antimony Creek area.

A program of detailed geological mapping and systematic sampling and prospecting, concurrent with diamond drilling, is recommended for these two target areas.

INTRODUCTION

This report discusses the exploration procedure and results of a geological and geochemical survey conducted by Omni Resources Inc. and Arkona Resources Inc. on the Goddell/Carbon Hill Group of claims located in the Wheaton River Valley south of Whitehorse. Field work was performed by a total of five company personnel plus five personnel from Caron Diamond Drilling Ltd. of Whitehorse. Company personnel were lodged at the Omni exploration camp located at the former Skukum Mines mill site near Butte Creek. Contract personnel generally commuted approximately 84 road km from Whitehorse to the job site.

The objective of the 1998 program was to evaluate the properties' economic potential though detailed geological mapping, grid controlled and contour soil sampling, prospecting and bulldozer trenching on promising targets delineated by previous exploration programs.

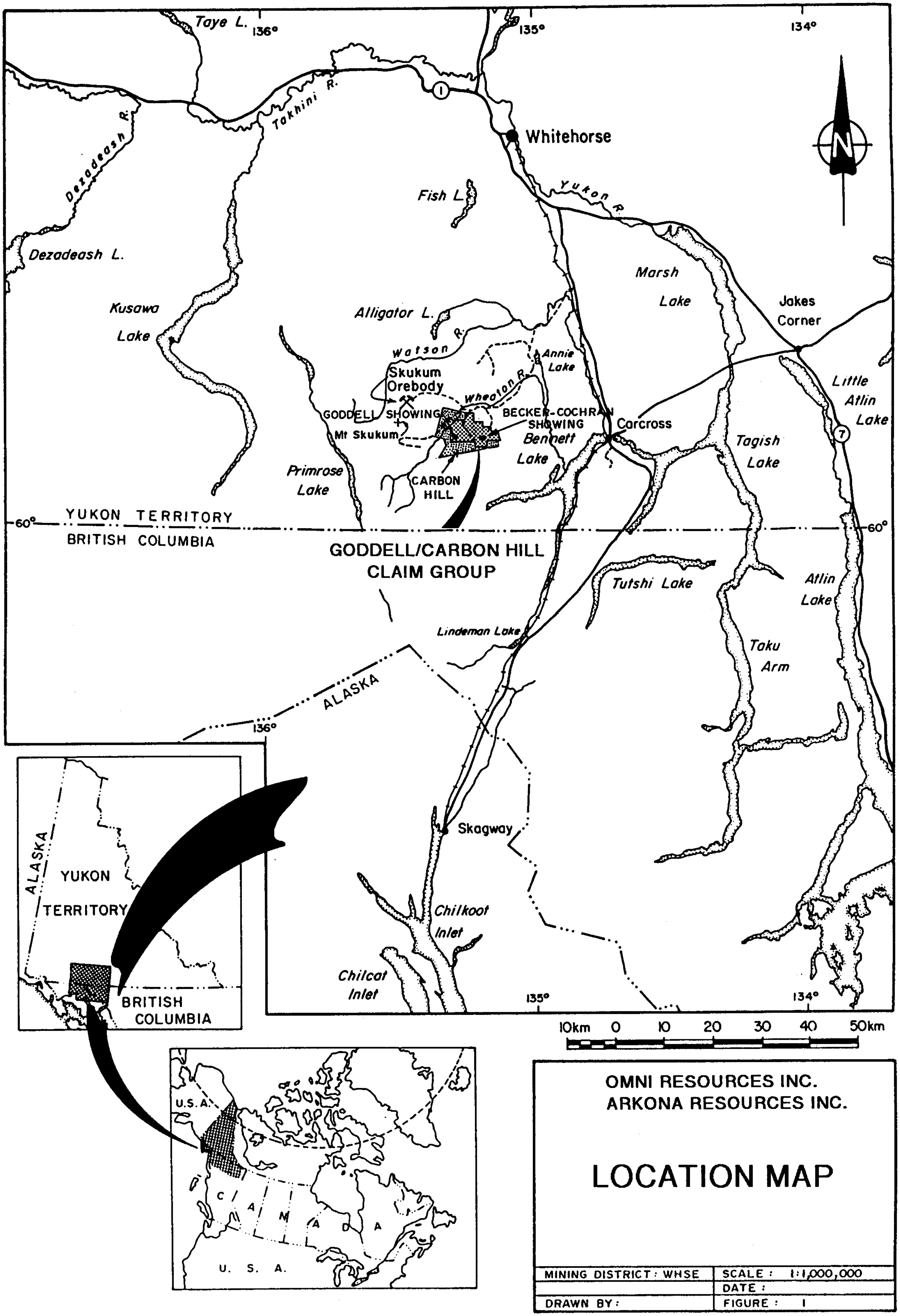
Work described in this report was performed on the following claims: POP 33, 35-38, 41-44, 62, 69, 79, 105, 106 and 110-114.

Geological and geochemical field data were initially compiled on 1:5000 scale contour maps. All final data were produced at 1:2000 scale.

A total of 126 rock grab samples, 696 soil samples and 17 stream silt samples were collected for analysis. All geochemical samples were shipped to Acme Analytical Labs of Vancouver, B. C. for 32 element ICP geochemical analysis plus gold analysis by Fire Assay with AA finish. Analytical procedures are described in APPENDIX III and analytical results are presented in APPENDICES IV, V and VI.

Location and Access

The Goddell/Carbon Hill Group of claims is located in the southwestern Yukon Territory approximately 60 air kilometers south of Whitehorse (Figure 1). The property is situated within NTS map sheet 105D/3 and centred about 60° 10' 45" N latitude and 135° 15' 00" W longitude. The claims area covers Carbon Hill, Mount Bell and plateau terrain southwest of Becker Creek, the majority of the Fenwick Creek drainage and a portion of the Wheaton River Valley between Summit Creek and Skukum Creek. The main focus of exploration activity, and the subject of this report, is the Sinter Cap and Conglomerate Creek areas, located approximately 3.0 km east of Goddell Gully, and Antimony Creek located approximately 2.0 km south of Goddell Gully. Road access to the property is provided via the Alaska Highway and South Klondike Highway to the Annie Lake Road turnoff thence via the all weather Annie Lake road to the Becker Creek road which strikes southward at the Becker Creek bridge. This 4-wheel drive road parallels the south side of Becker Creek for 12 km then trends westerly past the former Becker-Cochrane adits and crosses the top of Carbon Hill to connect with several rough drill roads in the project area. Alternatively, helicopter charter out of Whitehorse is also available.



Taye L.
136°
135°
134°
Takhini R.
Whitehorse
Dezadeash R.
Fish L.
Yukon R.
Dezadeash L.
Marsh
Lake
Kusawa
Lake
Alligator L.
Jakes
Corner
Watson R.
Annie
Lake
Skukum
Orebody
Wheaton R.
Little
Atlin
Lake
GODDELL SHOWING
BECKER-COCHRAN
SHOWING
Carcross
Mt Skukum
Bennett
Lake
Tagish
Lake
Primrose
Lake
CARBON
HILL
YUKON TERRITORY
BRITISH COLUMBIA
60°
GODDELL/CARBON HILL
CLAIM GROUP
Tutshi Lake
Atlin
Lake
Lindeman Lake
Taku
Arm
ALASKA
Skagway
Chilkoot
Inlet
Chilcat
Inlet
ALASKA
YUKON
TERRITORY
BRITISH
COLUMBIA
U.S.A.
C A N A D A
U. S. A.
10km 0 10 20 30 40 50km
OMNI RESOURCES INC.
ARKONA RESOURCES INC.
LOCATION MAP
MINING DISTRICT : WHSE
SCALE : 1:1,000,000
DATE :
DRAWN BY :
FIGURE : 1

Physiography and Climate

The Goddell/Carbon Hill Group of claims is located within the Boundary Ranges of the Coast Mountain physiographic division. Topography is moderate to rugged and, in the central portion of the claims area, is characterized by upland alpine plateaus bordered by steep scarps. The northern 25% of the property covers the broad, flat-bottomed Wheaton River Valley. Elevations on the property range from 915 metres (2,974') up to 1854 metres (6,082') above sea level.

During the Pleistocene Epoch, ice covered the entire area except the tops of the highest peaks. Glaciation has produced broad U-shaped valleys which are now occupied by underfit streams and rivers; tributaries to these streams often originate in cirque valleys. On a regional scale, outcrop exposure is relatively uncommon and low relief plateau areas are covered with felsenmeer and glacial till.

Valley bottoms are typically underlain by glaciofluvial sediments having a thickness in excess of five metres. Lower slopes above the valley floor are draped with colluvial apron sediments. Slopes above the valley floor to tree line are populated by forests of spruce, balsam fir, poplar and willow. Tree line occurs at approximately 1350 metres (4,428') and above this elevation, alpine grasses, low shrubs and a variety of mosses prevail.

Weather records indicate that seasonal precipitation is light and falls mainly as rain during the summer. Snow cover averages 1.0 to 1.5 metres during winter. The climate is continental type with warm, short summers and long, cold winters. Average summer temperatures are recorded at 25° Celsius while winter temperatures are commonly in the -30° to -40° Celsius range. Permafrost at this latitude is discontinuous but widespread. It is rarely possible to commence surface geological work before the end of June and difficult to continue past September.

Property Status and Ownership

The Goddell/Carbon Hill Group of claims, located in the Whitehorse Mining District, comprises a total of 423 two-post, unsurveyed mineral claims in seven separate claim blocks grouped into 28 groups. The POP, STEN and MB claims are 100% owned by Arkona Resources Inc. The MOM, BERG and TECH claims are owned 100% by 276 Taurus Ventures Ltd. TECH 5 and 14 were re-staked in 1997 by Omni Resources Inc. The MIL claims are 100% owned by BYG. Current claims status is shown on Yukon Quartz and Placer Sheet 105D/3 (Figure 2) and relevant claims data is tabulated in Table 1.

TABLE 1: GODDELL/CARBON HILL PROPERTY-CLAIMS STATUS

Claim Name and Numbers	No. of Claims	Grant Number	Current Expiry	New Expiry Date
MOM 1-10	10	YA81767-776	2002/12/01	2003/12/01
MOM 15-44	30	YA81781-810	2002/12/01	2003/12/01
MOM 47-60	14	YA81813-826	2002/12/01	2003/12/01
MOM 62-75	14	YA81828-841	2002/12/01	2003/12/01
MOM 76	1	YA81842	2002/12/01	2005/12/01
MOM 77	1	YA81843	2002/12/01	2003/12/01
MOM 78	1	YA81844	2002/12/01	2005/12/01
MOM 79	1	YA81845	2002/12/01	2003/12/01
MOM 80	1	YA81846	2002/12/01	2005/12/01
MOM 81	1	YA81847	2002/12/01	2003/12/01
MOM 82-89	8	YA82000-007	2002/12/01	2003/12/01
POP 1-5	5	Y75415-419	2002/12/01	2003/12/01
POP 6	1	Y75420	2002/12/01	2005/12/01
POP 7	1	Y75421	2002/12/01	2005/12/01
POP 8-14	7	Y75422-428	2002/12/01	2005/12/01
POP 15-21	7	YA81468-474	2002/12/01	2003/12/01
POP 22-24	3	YA81475-477	2004/12/01	2005/12/01
POP 25	1	YA81478	2002/12/01	2003/12/01
POP 26	1	YA81479	2004/12/01	2005/12/01
POP 27-28	2	YA81480-481	2002/12/01	2003/12/01
POP 29-30	2	YA81482-483	2004/12/01	2005/12/01
POP 31	1	YA81484	2004/12/01	2007/12/01
POP 32	1	YA81485	2004/12/01	2005/12/01
POP 33	1	YA81486	2004/12/01	2007/12/01
POP 34	1	YA81487	2004/12/01	2005/12/01
POP 35-38	4	YA81488-491	2004/12/01	2007/12/01
POP 39-41	3	YA81492-494	2002/12/01	2003/12/01
POP 42-48	7	YA81495-501	2002/12/01	2005/12/01
POP 49	1	YA81502	2002/12/01	2003/12/01
POP 50	1	YA81503	2004/12/01	2007/12/01
POP 51	1	YA81504	2004/12/01	2005/12/01
POP 52	1	YA81505	2004/12/01	2007/12/01
POP 53	1	YA81506	2004/12/01	2005/12/01
POP 54	1	YA81507	2004/12/01	2007/12/01
POP 55-58	4	YA81508-511	2004/12/01	2005/12/01
POP 59	1	YA81512	2004/12/01	2007/12/01
POP 60	1	YA81513	2004/12/01	2005/12/01
POP 61	1	YA81514	2004/12/01	2007/12/01
POP 62	1	YA81515	2004/12/01	2005/12/01
POP 63-64	2	YA81516-517	2002/12/01	2003/12/01
POP 65-67	3	YA81518-520	2006/12/01	2009/12/01
POP 68	1	YA81521	2006/12/01	2009/12/01

Claim Name and Numbers	No. of Claims	Grant Number	Current Expiry	New Expiry Date
POP 69-70	2	YA81522-523	2004/12/01	2005/12/01
POP 71-72	2	YA86194-195	2002/12/01	2003/12/01
POP 73-76	4	YA86196-199	2004/12/01	2005/12/01
POP 77	1	YA86200	2005/12/01	2008/12/01
POP 78	1	YA86201	2005/12/01	2006/12/01
POP 79	1	YA86202	2005/12/01	2008/12/01
POP 80-82	3	YA86203-205	2005/12/01	2006/12/01
POP 83-84	2	YA86206-207	2002/12/01	2003/12/01
POP 85-104	20	YA86208-227	2004/12/01	2005/12/01
POP 105-116	12	YA93384-395	2002/12/01	2005/12/01
POP 117-122	6	YA94672-677	2002/12/01	2003/12/01
POP 101Fr., 102Fr.	2	YA93378-379	2002/12/01	2005/12/01
BERG 1-12	12	YB07446-457	2002/12/01	2003/12/01
BERG 15-16	2	YB07460-461	2002/12/01	2003/12/01
BERG 21-22	2	YB07466-467	2002/12/01	2003/12/01
BERG 29-45	17	YB07474-490	2002/12/01	2003/12/01
BERG 54	1	YB07499	2002/12/01	2003/12/01
BERG 56	1	YB07501	2002/12/01	2003/12/01
BERG 58	1	YB07503	2002/12/01	2003/12/01
BERG 60	1	YB07505	2002/12/01	2003/12/01
BERG 62	1	YB07507	2002/12/01	2003/12/01
BERG 64	1	YB07509	2002/12/01	2003/12/01
BERG 66	1	YB07511	2002/12/01	2003/12/01
BERG 68	1	YB07513	2002/12/01	2003/12/01
BERG 70	1	YB07515	2002/12/01	2003/12/01
BERG 72	1	YB07517	2002/12/01	2003/12/01
BERG 74	1	YB07519	2002/12/01	2003/12/01
BERG 76	1	YB07521	2002/12/01	2003/12/01
BERG 78	1	YB07523	2002/12/01	2003/12/01
BERG 80	1	YB07525	2002/12/01	2003/12/01
BERG 82	1	YB07527	2002/12/01	2003/12/01
BERG 84	1	YB07529	2002/12/01	2003/12/01
BERG 86	1	YB07531	2002/12/01	2003/12/01
BERG 88	1	YB07533	2002/12/01	2003/12/01
BERG 90	1	YB07535	2002/12/01	2003/12/01
BERG 92	1	YB07537	2002/12/01	2003/12/01
BERG 94-95	2	YB07539-540	2002/12/01	2003/12/01
BERG 152-154	3	YB07597-599	2002/12/01	2003/12/01
BERG 156-160	5	YB07601-605	2002/12/01	2003/12/01
STEN 1-17	17	YA92922-938	2002/12/01	2003/12/01
STEN 19	1	YA92940	2002/12/01	2005/12/01
STEN 20-22	3	YA92941-943	2002/12/01	2003/12/01

STEN 23	1	YA92944	2003/12/01	2004/12/01
STEN 24-45	22	YA92945-966	2002/12/01	2003/12/01
TECH 1-4	4	YA82362-365	2002/12/01	2003/12/01
TECH 6	1	YB26465	2002/12/01	2003/12/01
TECH 7-13	7	YA82368-374	2002/12/01	2003/12/01
TECH 15-18	4	YA82376-379	2002/12/01	2003/12/01
TECH 19-21	3	YA86013-015	2002/12/01	2003/12/01
TECH 22-40	19	YA92145-163	2002/12/01	2003/12/01
MIL 1-6	6	YB67166-171	2002/12/01	2003/12/01
MIL 7	1	YB67172	2003/12/01	2004/12/01
MIL 8	1	YB67173	2002/12/01	2003/12/01
MIL 9-10	2	YB67174-175	2003/12/01	2004/12/01
MIL 11-22	12	YB67176-187	2002/12/01	2003/12/01
MIL 23	1	YB67188	2003/12/01	2004/12/01
MIL 24-69	46	YB67189-234	2002/12/01	2003/12/01
MB 1-3	3	YA94610-612	2004/12/01	2005/12/01

HISTORY OF EXPLORATION

Regional History

The area drained by the upper reaches of the Wheaton River was first explored for minerals at the turn of the century when prospectors passed through the region on their way to the interior. This stimulated geological investigations by McConnell (1906) and Cairnes (1908, 1910).

Considerable prospecting was performed in the Wheaton River area commencing in the early 1900's and culminated in the discovery of numerous gold, silver and related base metal occurrences.

In 1981, AGIP Canada Ltd. discovered gold at Mount Skukum near the headwaters of Butte Creek. The Mount Skukum gold deposit was developed with published pre-production proven reserves of 235,000 tonnes (259,000 tons) grading 20 g/t (0.58 oz/t) Au. The mine operated between February, 1986 to July, 1988 and produced approximately 80,000 ounces of gold from 220,000 tons of ore.

The Skukum Creek gold deposit, initially staked in 1922, is the largest vein gold deposit discovered to date in the Yukon. The deposit comprises two quartz-sulphide veins which were explored with several trenches, shafts and two adits by 1937. Road construction and further bulldozer trenching was completed in the mid 1960's. The property was re-staked in 1973 and explored intermittently by several owners prior to acquisition by Omni Resources Inc. in 1984. To the end of 1988, Omni completed a total of more than 24,000 metres of surface and underground diamond drilling and 2200 metres of underground development. Drill indicated and proven reserves are 867,890 tonnes grading 7.6 g/t Au and 275 g/t Ag.

Property History

A review of government Assessment Report Archives and Minfile records indicates that considerable work is recorded within the project area. Ground presently owned by Omni Resources/Arkona Resources was initially staked in the late 1800's by Frank Corwin and Thomas Rickman following the discovery of gold bearing veins on Mt. Anderson, Chieftain and Carbon Hill. The discovery of high grade gold and gold telluride bearing veins on Gold Hill resulted in a staking rush in 1906. Adits were subsequently driven into structures on Gold Hill, Tally Ho Mountain, Mount Stevens and Carbon Hill.

The Goddell stibnite veins on the northwestern facing slopes of Carbon Hill were probably among the first mineral occurrences discovered in the Wheaton River area in 1893. Charles Goddell staked the first known mineral claims about 1906 and completed trenching and a short adit on the Goddell antimony showing. The property experienced little activity during the first half of the century. Exploration activity by Prospectors Airways in 1958, Yukon Antimony Corp. in 1965 and Con Am Resources Ltd. in 1976 returned low gold values.

A short adit was driven into the Porter antimony showing in the early 1900's. The Becker-Cochrane antimony showing was worked intermittently between 1906 and 1940 and included bulldozer trenching and driving a 95 foot adit. Yukon Antimony Corp acquired the ground in 1964 and commenced extensive diamond drilling. The company collared three adits which defined a mineralized antimony bearing shear zone containing possible and probable reserves of approximately 140,000 tons of 4% antimony.

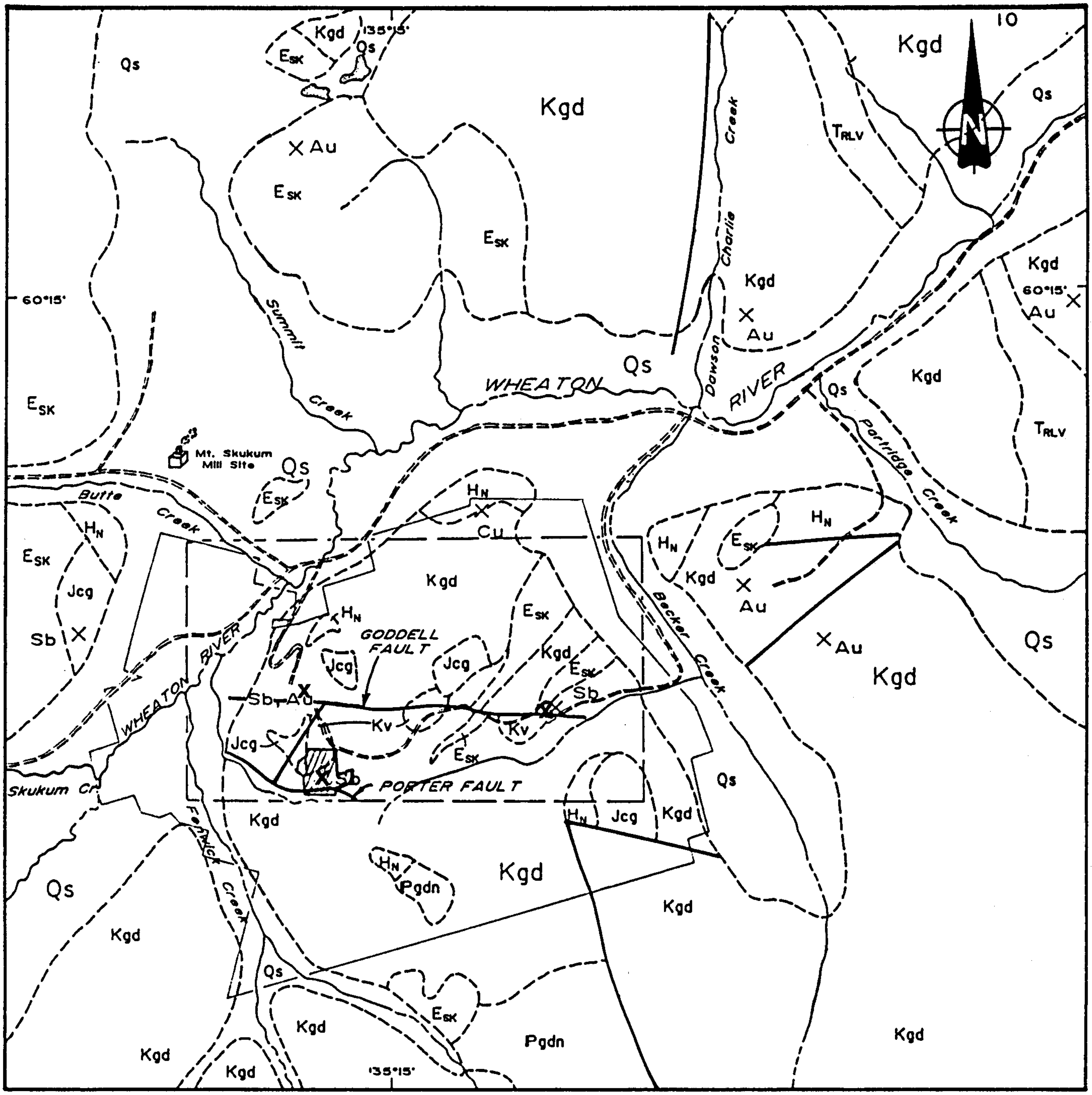
The Becker-Cochrane showing was re-staked in 1974 by E. Bergvinson as the POP 1-14 claims; these were optioned to Belmoral Mines Ltd. who subsequently dropped the option after preliminary investigations. In 1976 the ground was optioned to Con Am Resources Ltd. who conducted a 17 hole diamond drilling program on the Becker-Cochrane zone and the Porter showing. This option was eventually dropped and additional ground was acquired on Carbon Hill by Berglynn Resources (E. Bergvinson) during 1984-85. An extensive soil geochemical survey performed on the POP claim group in August, 1985 outlined five separate areas anomalous in gold and indicator elements. Additional assessment work in 1986 outlined a minimum of five separate targets which warranted further examination. These included the Goddell Gully, Horseshoe Gulch, Goldpan Gully, Becker-Cochrane area, Antimony Creek area and the Eastern Gold geochemical anomaly. Extensive surface exploration was conducted on the POP property during 1987 specifically in Goddell Gully, Horseshoe Gulch and Goldpan Gully areas. The area north of Antimony Creek and the Eastern Gold anomaly also saw limited exploration.

GEOLOGY

Regional Geology

The Goddell/Carbon Hill Property is located at the eastern margin of the Coast Plutonic Complex near the boundary with folded Mesozoic and Paleozoic volcanic and sedimentary rocks of the Whitehorse Trough (Intermontaine Belt). This portion of the Coast Plutonic Belt is composed of foliated and non-foliated Mesozoic (Cretaceous) granite, granodiorite, monzonite and quartz diorite flanked by metamorphosed and unmetamorphosed sedimentary and volcanic strata belonging to the Yukon Group, Lewes River Group, Laberge Group and Tantalus Formation. Granite, granodiorite and quartz monzonite are characteristic of the composite plutons (Figure 3).

Irregular belts of lower Mesozoic to Paleozoic, and probable Precambrian age, metasedimentary and metavolcanic rocks belonging to the Nisling Terrane and Tantalus Formation occur as roof pendants and erosional remnants in the granitic suites. These older units commonly are exposed in the eastern portion of the Wheaton River District. These lithologies are overlain and intruded by a coeval suite of Tertiary rhyolitic to andesitic flows, dykes and stocks at Mount Skukum.



L E G E N D

LITHOLOGIES

QUATERNARY

- Qs — surficial debris

EOCENE

- E_{SK} — andesite and rhyolite

CRETACEOUS

- Kgd — granodiorite
- Kv — andesite

JURASSIC

- Jcg — conglomerate

TRIASSIC

- T_{RLV} — andesite

PALEOZOIC

- Pgdn — granite and gneiss

PRECAMBRIAN

- H_N — quartzite and gneiss

SYMBOLS

- fault
- approximate lithologic contact
- road
- creek, river
- × mineral occurrence

GEOLOGICAL ASSOCIATION OF CANADA
G.L. WESA
FELLOW

NOTES – claim boundaries modified from D.I.A.N.D. claim sheets 105 D-3 & 105 D-6
– geology simplified after Doherty et al (1988)

1 km 0 1 2 3 4 5 km

SCALE IN KILOMETRES

OMNI RESOURCES INC.
ARKONA RESOURCES INC.

WHITEHORSE MINING DISTRICT – YUKON TERRITORY

REGIONAL GEOLOGY

January, 1999

NTS 105 D/3&6		SCALE 1:100,000	FIGURE: 3

After Aurum Geological Consultants

The Goddell/Carbon Hill Property is located on the eastern margin of the Paleocene-Eocene Mount Skukum Volcanic Complex, an elliptical shaped, nested cauldron collapse structure comprised of bimodal volcanism covering approximately 140 square kilometres. Lithologies representing the initial phase of volcanic activity comprise rhyolite and andesite flows, breccias, tuffs and agglomerates. The final stage of volcanic activity is represented by intrusion of rhyolite, dacite and andesite dykes along a prominent set of vertically dipping, northeast trending faults that host quartz-sulphide vein mineralization. The Mount Skukum epithermal gold-silver vein deposit is located within the cauldron and the Skukum Creek deposits are at its southern margin.

The Mount Skukum Volcanic Complex and surrounding area has been extensively faulted as a consequence of cauldera collapse. Faults, lithological attitudes and other regional structures generally trend northwest. The majority of structurally controlled mineral deposits in the area are associated with pre-existing northeast to west-northwest striking fault zones now occupied by intermediate to felsic dykes. The key structural feature of the Skukum Creek deposits is association with the Porter Creek Fault which parallels the Goddell Fault. Together, these main structures represent the major determinants controlling the emplacement of gold mineralization in the area and host all mineral deposits occurring on the company's current claim holdings.

Property Geology

Property geology is complex and locally complicated by the lack of outcrop which probably constitutes less than 10% of the total property area. Rock exposures are restricted to scarps bordering upland plateaus and local deeply dissected drainages. Table 2 illustrates the bedrock geology underlying the claims area.

The oldest exposed lithologies on the property are Hadrynian to Cambrian age foliated quartz-feldspar-biotite gneiss, biotite schist and marble belonging to the Nisling Terrane. These rocks commonly occur as roof pendants in granodiorite. Local exposures show evidence of contact metamorphism including skarnification. Irregular zones of Paleozoic to Cretaceous variably metamorphosed granitoid, volcanic and sedimentary rocks also occur as roof pendants and tectonic slices. These include unconformably overlying chert pebble conglomerate of the Jura-Cretaceous Tantalus Formation.

Leucocratic, medium grained, equigranular to porphyritic granitic rocks, classified as granodiorites and locally grading into quartz monzonite and monzonite, intrude the older metamorphic assemblages. Compositionally, hornblende generally predominates over biotite and both minerals are variably chloritized. These plutonic rocks are the most commonly exposed on the property.

Eocene volcanic rocks comprise mainly rhyolite and andesite which occur as dykes and small stocks at many locations within the property. These igneous intrusions have been emplaced along faults and local fracture systems related, in part, to collapse of the Mount Skukum Caldera Complex.

TABLE 2: Table of Formations – Goddell-Carbon Hill Area

ERA	PERIOD	FORMATION	LITHOLOGY
Cenozoic	Quaternary		Unconsolidated surficial alluvium.
	Pleistocene		Glacial and glaciofluvial deposits.
	Erosional Interval		
		SKUKUM GROUP (Mount Skukum Volcanic Complex)	Felsic to intermediate volcanic flows, breccias, ash to lapilli tuffs and related epiclastic rocks and pyroclastic flows, felsic dyke emplacement, quartz veining and mineralization.
Paleocene – Unconformity (Intrusive Contact)			
Mesozoic	Middle Cretaceous	COAST PLUTONIC COMPLEX (Mount McIntyre Plutonic Suite)	Carbon Hill Plug: recessive, granular weathering biotite-quartz monzonite and granophyric, hornblende and alkali feldspar granite.
		Mid-Cretaceous dykes, plugs	Siliceous pale green, saccharoidal rhyolite and aplite.
		(Whitehorse Plutonic Suite)	Mr. Anderson Pluton: Biotite and porphyritic hornblende granodiorite.
		Mount Nansen Group (Carbon Hill Volcanics)	Undifferentiated volcanics, andesite flows and breccias, tuffaceous andesite.
	Lower Cretaceous – Erosional Unconformity		
	Late Jurassic	Tantalus Formation	Chert pebble conglomerate, polymictic conglomerate and related siliciclastic rocks.
		Late Jurassic Volcanics	Andesite porphyry flows, breccia, epiclastic rocks.
Mesozoic	**Erosional Unconformity**		
	Early Jurassic	Alligator Quartz Monzonite	Foliated hornblende-quartz monzonite to granodiorite.
	Late Triassic	Bennett Granite	Megacrystic, potassium feldspar-hornblende granite to granodiorite to quartz monzonite.
Erosional Unconformity			
Paleozoic and Older (?)	Late Triassic to Paleozoic	Nisling Assemblage	Rusty weathering metavolcanic schists, quartzite and marble; minor black argillite.

Dykes and faults follow a predominant northeastern trend discordant with regional structures and tangential to the margin of the Mount Skukum Volcanic Complex. Other lineaments, including the 6.0 km long Goddell Fault, trend east to east-southeast. It is now believed that the Goddell and Becker-Cochrane zones are localized along this east-west trending structure.

The Goddell Shear Zone is exposed for over 1220 metres (4,000') on surface. Gold mineralization is associated with sulphides comprised of mainly stibnite with minor pyrite, sphalerite, arsenopyrite and jamesonite enclosed within a quartz-barite-calcite-clay gangue. Multiple, subparallel, sulphide bearing vein type structures are restricted to a 50-100 metre wide zone of sheared, altered and brecciated quartz monzonite which hosts narrow rhyolitic dykes and andesite dykes containing hairline pyritic fractures. The gold bearing shear zone occurs adjacent to a breccia zone, comprising quartz-feldspar porphyry, andesite dykes and quartz monzonite within a fine grained, grey groundmass, which is enclosed by two prominent quartz-feldspar porphyry dykes. Fine acicular arsenopyrite-pyrite-lithic quartz-sericite-carbonate breccias and stockwork veinlets at felsic to intermediate dyke selvages are the primary hosts of gold mineralization. In addition, intensely microfractured and argillic altered quartz monzonite wallrock, sandwiched between multiple felsic dyke structures, has returned up to 3.0 g/t gold. This altered plutonic rock is barren of visible sulphides.

The shear zone is bounded on both sides by a 25-metre wide phyllic alteration halo. The alteration zone is intense, especially within the granitoid wallrocks, and is identified by bleached, gossanous bedrock on surface. Other alteration mineral assemblages identified include carbonate, Fe-carbonate, chlorite, chalcedony and fluorite.

At the Becker-Cochrane deposit, vein type mineralization consists of irregular, massive stibnite pods with minor sphalerite, realgar and orpiment in quartz-barite-clay gangue localized along the 126° trending Becker-Cochrane Fault. Mineralization is hosted within structurally complex pre-Tertiary granodiorite, conglomerate and andesite intruded by numerous Tertiary rhyolite and andesite dykes. Exploration work to date consists of diamond drilling and underground development in three adits.

SINTER CAP – CONGLOMERATE CREEK AREA

The Sinter Cap is an exposure of white to greyish green, flow banded to layered, hydrothermally altered, siliceous "exhalative sediment" intruded along a fault cross-cutting a shear zone representing a portion of the Goddell Structure. The sinter results from near surface hydrothermal activity and the precipitate marks the location of hot spring venting. Siliceous sinter can vary from thinly bedded to totally massive due to recrystallization. Clasts, bedded features and siliceous concretions indicate an exhalative origin. Siliceous sinter represents higher temperature of formation generally considered to be more productive for gold. Bedrock underlying the Sinter Grid area comprises quartz monzonite to granodiorite, chert pebble conglomerate and rhyolitic to andesitic flows, dykes and small stocks. These lithologies have been locally extensively sheared, brecciated and hydrothermally altered. Other lithologies include minor exposures of Bennett granite, argillite and amphibolite. Approximately 180–190 metres east of the Sinter Cap, mapping has identified Tertiary rhyolite in contact with Mesozoic (Jurassic) Tantalus Formation chert pebble conglomerate along a north to northeasterly trending contact. This contact is defined by a locally well developed, intensely hydrothermally altered chalcedonic breccia which may host minor gold values. Silica (chalcedony) cemented, pale mottled grey to limonitic breccia appears to be the dominant form of breccia at embayments in the contact defined by a change to a northeast to easterly trend in the contact. This breccia is exposed along road cuts and in trenches east of the Sinter Cap.

The Goddell Structure is a major pre-Tertiary shear structure which hosts the Goddell deposit and Becker-Cochrane antimony (stibnite) occurrence. The Goddell-Becker-Cochrane Structure has a strike length greater than 6 km and measures in excess of 75 metres wide at the Goddell deposit. In Goddell Gully, wall rock is intensely sheared, brecciated and hydrothermally altered. The structure strikes 090° to 115° with a general trend of 105° azimuth. On surface, this fault appears to dip vertically to steeply south.

Secondary cross faults, which strike roughly 060° azimuth, are represented by the Sinter and Conglomerate Creek cross faults. The western extension of the Becker-Cochrane section of this regional structure is exposed in outcrop on the north bank of Conglomerate Creek at a point of intersection with the Conglomerate Creek cross fault. At this location, two 20 cm wide quartz-sulphide (tetrahedrite (?), chalcopyrite, galena, stibnite) veins, separated by a 7 metre wide rhyolite dyke, reflect a lithological association similar to that identified at the Becker-Cochrane quartz-stibnite deposit.

Approximately 270 metres to the northwest, the "Sinter Zone" follows the east-northeast trending Sinter cross fault which is exposed for 280 metres along strike and cuts across both Tertiary rhyolite and Tantalus conglomerate. Here, the Sinter Cap effectively represents a linear zone of weakness which appears dyke-like due to vertically dipping layering.

Between these two cross faults, a west-northwest trending, shallow graben-like gully is exposed on steep slope. Deep bulldozer trenching across this depression exposed a thick layer of Upper Jurassic Tantalus Formation chert-pebble conglomerate and minor glacial debris. Tantalus conglomerate also is exposed in outcrop on the south side of Conglomerate Creek. Typically, this lithology occurs at higher levels capping plutonic intrusions, however, block faulting along the Becker-Cochrane fault and Conglomerate Creek cross fault has down-dropped Tantalus conglomerates.

ANTIMONY CREEK AREA

Antimony Creek forms an arcuate shaped, westerly flowing drainage located 2.1 km south of the Goddell deposit. Antimony Creek has cut a steep, narrow, V-shaped valley on the west-central side of Carbon Hill. This valley is bounded by and underlain with an assemblage of quartz monzonite to granitic intrusions which are, in turn, intruded by numerous, roughly east-west trending andesite dykes and a major 6.0-8.0 metre wide, near vertical dipping quartz-feldspar porphyry dyke that is traceable discontinuously for over 800 metres.

Bedrock underlying steep slopes along Antimony Creek gully comprise relatively fresh to intensely sericitized Carbon Hill quartz monzonite and granite. This Cretaceous age plutonic suite also hosts the Goddell deposit and appears as recessive, orange, granular weathering, red to pink to grey biotite-quartz monzonite.

Early Jurassic Alligator quartz monzonite, composed of foliated hornblende-quartz monzonite to granodiorite, underlies the gully to the southeast and the area surrounding Carbon Hill. The Alligator quartz monzonite appears in fault contact with the Late Triassic Bennett granite at a point in the gully due south of the former Porter adit. Bennett granite appears as unaltered, pink to reddish-grey, megacrystic potassium feldspar-hornblende granite to granodiorite. In Antimony Creek, Bennett granite occurs as a fault bounded block sandwiched between Carbon Hill quartz monzonite and Alligator quartz monzonite.

Intense hydrothermal alteration, represented by sericitization, chloritization and iron carbonate alteration, affects the Carbon Hill quartz monzonites at Goddell and Antimony Creek. At Goddell, a 75 metre wide zone of intensely sericitized granite is identified. Correspondingly, at Antimony Creek, this style of alteration measures in excess of 100 metres and includes phyllic, advanced argillic and pyrophyllitic stockwork alteration.

Both Goddell and Antimony Creek exhibit extensive brecciation along a major shear zone. At Antimony Creek, quartz monzonite is iron-carbonate altered, sericitized and intensely brecciated for 10 metres on the hanging wall and foot wall margins of the 6.0-8.0 metre wide, post mineral quartz-feldspar porphyry (QFP) dyke. Wall rock brecciation is observed for approximately 475 metres in the eastern half of the approximately 850 metre long QFP dyke.

In Antimony Creek, a dyke swarm, comprised of 1.0-3.0 metre wide, east-southeast and west-northwest trending andesitic dykes, is observed on the southern cliffed slopes of the gully on the south side of the QFP dyke. Similarly, at Goddell, a bimodal suite of dykes is represented by intermediate dykes which associate with a pair of near vertical dipping QFP dykes. The Antimony Creek dykes indicate dilation of the shear zone caused by arching along Antimony Creek. This broad folding is illustrated by east-west trending quartz veins gently dipping away from the axial plane.

Significant stibnite-barite veining and underground workings occur to the north of, and above, both Antimony Creek and Goddell deposit. The largest vein discovered is the easterly trending Porter-Fleming vein located approximately 100 metres north of Antimony Creek gully. This vein has been explored with over 330 metres of underground workings.

The Antimony Creek prospect features a pyritic halo marked by a large, brightly gossanous patch exposed in outcrop and talus debris on steep north facing slopes in Antimony Creek gully. This gossan is the result of oxidation of up to 10% disseminated pyrite associated with commonly saccharoidal textured, intensely phyllic altered quartz monzonite.

Copper mineralization in the form of chalcopyrite, chalcocite and malachite occurs in outcrop and in float along Antimony Creek. Quartz monzonite float boulders containing 10-12% disseminated to coarse, patchy chalcocite, chalcopyrite, malachite and azurite occur with alluvial gravels and coarse debris at approximately the 4,600' elevation in the gully. Similarly, copper mineralized float boulders are found in coarse alluvial material at the 4,440' elevation in the drainage.

Intensely cross-fractured, sheared and quartz-carbonate altered quartz monzonite hosts 3-5% disseminated to coarse pyrite and chalcopyrite with abundant malachite, azurite and limonite staining along 0.3 metre wide shear zones at the 4,200' elevation in the gully. Quartz flooding commonly occurs within the shears at this location and bedrock locally exhibits several parallel sets of shears and fracture systems (sheeted fractures) marked by zones of foliated, pale greenish-grey quartz-sericite ± carbonate alteration. This shear zone measures approximately 50 metres wide, trends roughly 45° azimuth and likely represents the southern extension of a major dextral strike slip fault which trends north-northeast toward the Goddell deposit.

In addition, the east-west trending QFP dyke exposed along Antimony Creek is offset several metres by north trending dextral slip faults which displace sections of the dyke northward along its western extension.

1998 EXPLORATION PROGRAM

Program Logistics

Detailed geological mapping, prospecting and coincident geochemical surveys were carried out on two target areas on Carbon Hill. These included the Sinter Cap – Conglomerate Creek area and Antimony Creek area located 3.0-km east-southeast and 2.1 km south, respectively, from Goddell Gully. A 500m x 600m picketed soil grid, totaling 6.6 km of soil lines, was established over the Sinter Cap and proximal area near the headwaters of Conglomerate Creek approximately 900 metres west-northwest of the Becker-Cochrane antimony deposit and roughly on strike with the Goddell Structure. The initial "Sinter Grid" was subsequently expanded to the northeast, with the addition of a 400m x 600m grid block and a further 5.4 km of soil lines, and extended 150 metres to the west.

Following initial grid layout and coincident geological and geochemical surveys, bulldozer trenching was completed over selected anomalous targets (Figures 4, 5, 6, 7). Three NE-SW trending trenches were excavated across steep slope between the Sinter Cap and Conglomerate Creek. These trenches trend roughly perpendicular to the projected strike of the Goddell-Becker-Cochrane Structure. The objective of this work was to expose mineralization, believed to represent the western extension of the Becker-Cochrane Structure, on the northwestern side of Conglomerate Creek. The three trenches, excavated at the 5,200', 5,350' and 5,450' levels, cut across a surficial depression indicative of a graben structure possibly related to the Goddell-Becker-Cochrane Structure. Additional trenching was completed approximately 220 metres northeast of the Sinter Cap and in the northeastern portion of the grid on lines 17+50N and 18+00N. Five trenches were excavated in these designated areas. All trenches were mapped and soil and lithogeochemically sampled.

In the Antimony Creek area, preliminary geological mapping, prospecting and geochemical sampling was completed along Antimony Creek with the objective of identifying prospective drill targets. This effort proved extremely successful with the discovery of a broad area of significant hydrothermal alteration possessing many of the characteristics considered important for the formation of a Goddell-style, vein hosted precious metals deposit. Extensive road construction was accomplished in Antimony Creek valley. The former bulldozer road which terminated below the Porter adit was extended approximately 1.3 km to the west. A 1.5 km road was pushed southward from the Goddell Portal to join up with the Antimony Creek road, however, completion was precluded by impassable terrain marked by surface bedrock exposures and cliffs. Reconnaissance prospecting and rock sampling was conducted along and in the vicinity of this road.

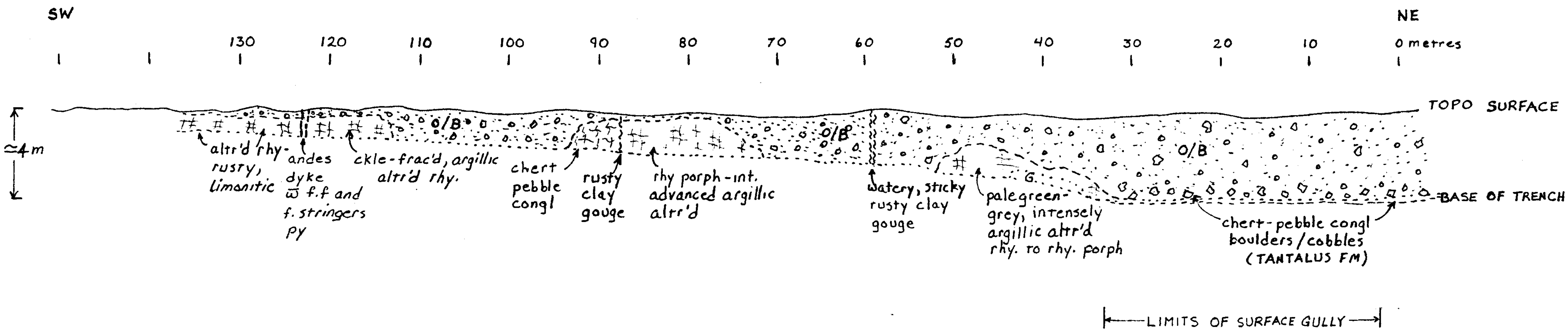


Figure 4

TRENCH #3
ELEV: 5450'
LOOKING NORTHWEST
HORIZONTAL SCALE: 1:500
VERTICAL SCALE: NOT TO SCALE
(NW EXTENSION - BECKER-COCHRANE STRUCTURE)

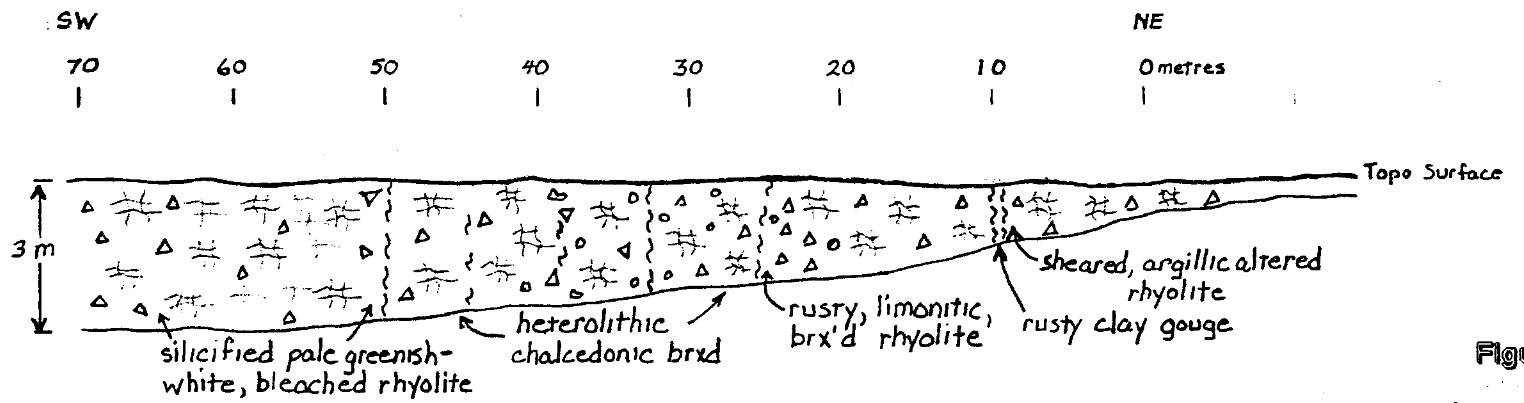


Figure 5

TRENCH 4
ELEV: 5500'
LOOKING NORTHWEST
HORIZONTAL SCALE: 1:500
VERTICAL SCALE: NOT TO SCALE
(EAST OF SINTER CAP EXHALITE)

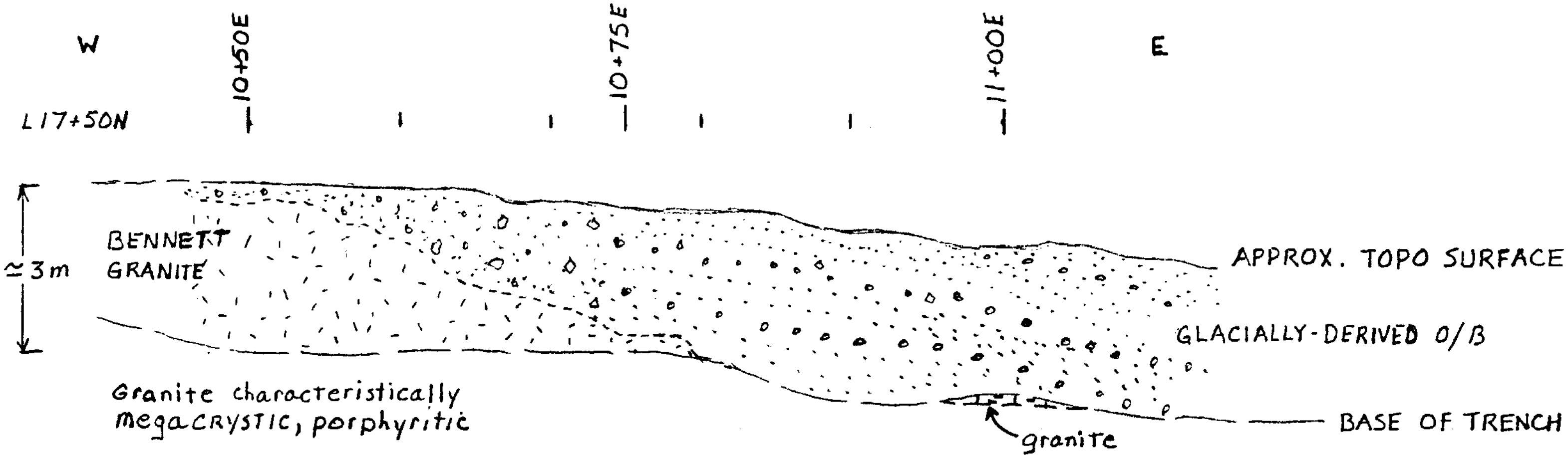


Figure 6

TRENCH #5 (Sinter Grid)
ELEV: ≃5370'
LOOKING NORTH
HORIZONTAL SCALE: 1:500
VERTICAL SCALE: NOT TO SCALE

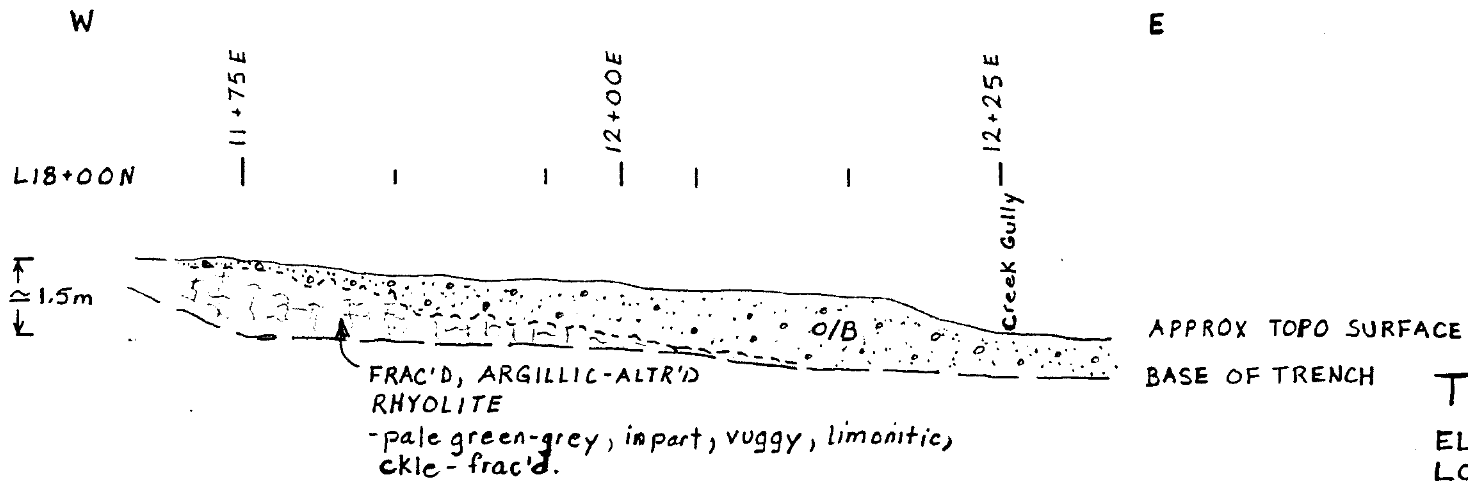


Figure 7

TRENCH #6 (Sinter Grid)
ELEV: 5300'
LOOKING NORTH
HORIZONTAL SCALE: 1:500
VERTICAL SCALE: NOT TO SCALE.

GEOCHEMISTRY

Sampling Procedure

Lithogeochemical samples were collected, concurrent with mapping and prospecting activities, from outcrop exposures exhibiting favourable characteristics such a sulphide content, gossanous weathering, alteration, shearing and deformation. Rock specimens were placed in marked plastic sample bags accompanied with a number tag for identification purposed and all sample sites were marked with a fluorescent ribbon displaying the corresponding sample code. Soil samples were collected from the Sinter Cap soil grid, contour soil lines and random locations in other parts of the project area. Samples were collected from depths of 10-30 cm using long handled mattocks and placed in marked, large gusseted kraft paper soil bags. Sample stations were correspondingly marked with coded pickets or fluorescent ribbon. Ground control for sampling was provided by altimeter, compass, GPS and hip chain, and the field crews were supplied with 1:5000 scale topo maps and air photos for plotting data. Stream silt samples were collected at regular intervals from Conglomerate Creek and these were similarly coded and plotted. During the current survey, 126 lithogeochemical samples were collected from the two target areas and in the vicinity of the Goddell-Antimony Creek road. Rock samples generally contained sulphides and were collected from areas of shearing accompanied by extensive hydrothermal alteration.

Rock, Soil and Stream Silt Geochemistry

A total of 48 rock samples, 620 soil samples and 17 stream silt samples were collected from the area enclosed by the Sinter Grid and proximal areas.

Analysis of initial soil samples documented anomalous gold values (200-883 ppb) and silver values (1035-1303 ppb) in the north-central portion of the expanded Sinter Grid at the headwaters of Horseshoe Gulch. This area is underlain by quartz monzonite and clay altered rhyolite flows. Four trenches were subsequently excavated over areas of anomalous gold-in–soil geochemistry. The highest gold value documented from these trenches is 0.126 oz./t Au (4320 ppb) recorded in TRENCH #5. Four other samples yielded strongly anomalous values for gold ranging between 285 ppb to 1345 ppb Au (TRENCH #5 and #6).

A second area of anomalous soil geochemistry occurs 300 metres northeast of the Sinter Cap. Bedrock at this location comprises intensely phyllic (chalcedonic quartz-sericite-clay ± pyrite) altered rhyolite cut by several breccia zones and limonitic shear structures. Close spaced sampling between stations 8+25E and 9+25E on lines 12+00N to 13+00N returned anomalous gold-in-talus fines values ranging up to 614 ppb Au. Analysis of soil samples collected from a single trench (TRENCH #4) excavated over this target returned anomalous values for gold (197-292 ppb) and silver (941-1528 ppb).

A new mineral occurrence, comprised of quartz vein hosted stibnite-chalcopyrite-sphalerite-malachite-azurite, was discovered and hand excavated in the north bank of Conglomerate Creek gully 300 metres southeast of the Sinter Cap. A mineralized width of 15-20 metres, exposed in outcrop along the creek, occurs on strike with the Becker-Cochrane stibnite veins 550 metres to the southeast. Although low gold values are documented from analysis of rock samples collected at this location, select grab samples yielded anomalous copper (up to 1696 ppm), lead (up to 234 ppm), Ag (up to 11.5 ppm), molybdenum (1227 ppm) and antimony (669 ppm). Two select rock grab samples (98SCER-15, 98SCERFL-16), collected from two 20 cm wide quartz-sulphide veins, returned anomalous values for copper (1.388, 1.160 ppm), antimony (0.684, 1.444 ppm) and silver (1.10, 1.65 oz/T), respectively.

Bulldozer trenching at three separate levels across a shallow surface depression southeast of Sinter Cap exposed a thick layer of talus and glacial material in excess of 10 metres thick in the middle and lower trenches. This surficial depression suggests that a graben structure has developed which subsequently has been in-filled with chert-pebble conglomerate talus debris belonging to Upper Jurassic Tantalus Formation. No mineralized outcrop or float was detected in these trenches and background values were recorded for most elements tested. The middle trench (TRENCH #2) yielded the highest gold value of 21 ppb. Elevated values for Sb, As, Hg, Ni and Co were recorded from TRENCHES #1, #2 and #3.

In the Antimony Creek area and proximal steep terrain to the north, a total of 78 lithogeochem samples and 76 soil samples were collected. Lithogeochemical and contour soil sampling was conducted concurrent with prospecting and geological mapping. Analysis of rock samples collected from outcrop along Antimony Creek returned strongly anomalous values for Ag (6.74 oz/t), Au (0.88 oz/t), Pb (2.76%, Zn (1.62%), Sb (1.61%) **(Sample 98AZBR-10)**; other samples documented elevated to strongly anomalous values for Ag (2.0-40.2 ppm), Cu (up to 0.45%), Pb (up to 0.53%), Zn (up to 1.53%), Mo (up to 0.80%), Sb (up to 1.51%) and Ba (up to 0.25%).

Contour soil samples were collected from steep gossanous slopes on the north and south sides of Antimony Creek. The majority of these samples represent talus fines collected from an area of extensive hydrothermal alteration and shearing. Analysis of soil samples yielded coincident elevated to strongly anomalous base and precious metal values: Ag (up to 1.68 oz/t), Cu (up to 1302 ppm), Pb (up to 2138 ppm), Zn (up to 2827 ppm) and rare, anomalous Sb (2150 ppm) and Hg (>1.0%).

In addition, rock samples were collected from gossans and shear zones in outcrop which was exposed during construction of the new drill access road along steep scree covered slopes on the north side of Antimony Creek. A 1.0 metre chip sample obtained across a gossanous shear zone exposed above a series of switchbacks yielded 1.09 oz/t Ag and 1001 ppm Cu with elevated Sb and Ba values.

Lithogeochemical samples were also collected from cliffs above a newly cleared 4-wheel drive road constructed at approximately the 3,300' elevation connecting the Goddell Portal and Antimony Creek road. Nine rock samples recorded coincident strongly anomalous values for Ag (10.1-175.3 ppm), Pb (0.12-1.15%), Zn (0.24-1.11%) and Cu (.05-0.50%). Two samples yielded strongly anomalous values for stibnite (3.55%, 3.95%). These anomalous values may reflect proximity to the "Empire Mine" workings; company personnel have been unsuccessful in locating these workings at this date.

This area remains highly prospective and warrants further detailed prospecting and geological mapping. The present road, although not completed to connect with the Antimony Creek drill road, provides more direct foot access to steep, rugged terrain to the east.

CONCLUSIONS

The Goddell/Carbon Hill property is underlain by Precambrian (Hadrynian) to Cretaceous metasedimentary, metavolcanic and granitoid rocks which have subsequently been intruded by Cretaceous quartz monzonite, granodiorite and related plutonic suites. These rocks are, in turn, intruded and overlain by felsic volcanic and hypabyssal lithologies related to the Eocene age Mount Skukum Volcanic Complex. Steep dipping block faults offset all units and widespread alteration, quartz-sulphide veining and associated mineralization illustrates the extensive hydrothermal regime affecting the bedrock.

Gold-silver and base metal mineralization on the property is recognized as vein-type and is structurally controlled by faults genetically related to collapse of the Mount Skukum caldera complex.

Gold and base metal bearing veins at Goddell and Becker-Cochrane deposits are classified as mesothermal in character. These veins comprise pyrite, arsenopyrite, galena and stibnite. Sphalerite, chalcopyrite, bornite and native gold is also recognized. Alteration assemblages are dominated by carbonates or silica flooding with minor pyrite. Veins examined on the property are hosted in a variety of rock types with granitic rocks being the most common.

Geological mapping, geochemical surveys and trenching during the current field season has delineated a potential drill target, measuring approximately 350 metres in length, between the Sinter Cap/Sinter Zone cross fault and the Conglomerate Creek cross fault. This linear target strikes roughly 120°-126° and may be extended several hundred metres to the northwest and southeast. This zone represents a portion of the Goddell-Becker-Cochrane Structure and, in the area bounded by the Sinter and Conglomerate Creek cross faults, may measure up to 30 metres in width as reflected in a wide, shallow graben-like surface depression. The width of this depression is encouraging as it suggests a broad, recessive weathering fault structure.

The drill target zone also includes the Conglomerate Creek base metal bearing vein showings-which are localized along strike of the Becker-Cochrane fault zone. The Conglomerate Creek vein showing occurs at exactly the same level of 1550 metres (5,080') above sea level as the Becker-Cochrane antimony deposit. At the Goddell deposit, evidence is documented showing the relationship between surface vein-type antimony showings and ore-grade gold mineralization encountered at depth.

Similarly at the Becker-Cochrane deposit, the Becker-Cochrane Structure and related cross faults are considered to be high priority exploration targets since mineralization may exhibit a vertical zonation with gold precipitating at the 1000 metre (3,300') level or deeper. In addition, structurally controlled antimony + arsenic ± gold mineralization may occur below the Sinter Cap/Sinter Zone area at the intersection of the Sinter cross fault and Goddell-Becker-Cochrane Structure.

Much of the area enclosed by the Sinter Grid, as well as peripheral areas, are covered by silica caps in the form of thick Tantalus Formation chert pebble conglomerate. These caps may act as traps for mineralization northwest of the Sinter Zone and southeast of Conglomerate Creek along the strike of the Becker-Cochrane antimony deposit. These impervious capping lithologies therefore provide a prospective setting that is favourable for development and concentration of economic precious ± base metal mineralization.

The Antimony Creek zone exhibits characteristics which suggest that a significant Goddell-style mesothermal system exists at this location. A wide, Goddell-like zone of alteration, brecciation, faulting, dyke emplacement and mineralization has been documented along an east-west trend centred on Antimony Creek.

Current geological and geophysical surveys have resulted in recognition of the following promising characteristics:

1) Multiple, parallel shear zones and fault structures.
2) Intense hydrothermal alteration as indicated by the identification of the following alteration facies: phyllic, advanced argillic and pyrophyllitic stockwork.
3) Significant width in excess of 100 metres.
4) Continuity of the system; strike length measures >800 metres along Antimony Creek.
5) Significant brecciation and fracturing of the wallrock, particularly in proximity to a major quartz-feldspar porphyry dyke.
6) Presence of andesite dykes and dyke swarms south of the QFP dyke.
7) Presence of sulphide mineralization in the form of disseminated pyrite associated with a distinct, brightly gossanous "pyritic halo" developed in intensely phyllic altered quartz monzonite, and disseminated copper mineralization (chalcocite, chalcopyrite, malachite, azurite) found in float boulders and in narrow shears, fractures and joints in altered felsic intrusions.
8) Peripheral stibnite-barite veins occur on the north slopes of Antimony Creek near the Porter-Fleming adits.

RECOMMENDATIONS

On the basis of the discussion and conclusions provided in this report, a proposed exploration program is warranted to better define the trend, dimensions, style and controlling factors of mineralization documented at currently defined target areas. It is recommended that the following exploration program be implemented:

1. Conduct a preliminary geophysical survey, possibly in the form of EM and/or IP, over the portion of the Goddell-Becker-Cochrane Structure bounded by the Sinter and Conglomerate Creek cross faults. The parameters of this survey should be discussed with the geophysical contractor.

2. Contingent upon favourable results from this survey, drill preliminary, shallow holes of approximately 100 metres into this structure to test for precious metals mineralization at depth.

3. Follow-up mapping and prospecting of the Antimony Creek fault zone eastward toward Mount Bell.

4. Drill the Antimony Creek zone from the road established on the north side of Antimony Creek to test areas of brecciation, alteration, bimodal dykes and sulphide mineralization. A 300-400 metre hole would adequately test bedrock below and adjacent to Antimony Creek. Documented evidence indicates that anomalous precious metals values may not be identified at surface due to the apparent elevation control on mineralization. Prospective drill targets would be zones of silicified quartz-wall rock breccias indicative of centres of intense hydrothermal activity.

5. Follow-up geological mapping and prospecting of selected prospective areas north and south of Antimony Creek plus the east-west trending ridge near the western limit of Antimony Creek.

6. Obtain an estimate of the cost of completing the Goddell-Antimony Creek road. Also determine all permitting requirements prerequisite for completion of this road.

Respectfully Submitted:
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ARKONA RESOURCES INC.

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Pride, M. J. and Clark, G. S. (1985): An Eocene Rb-Sr Isochron for Rhyolite Plugs, Skukum Area, Yukon Territory, C.J.E.S. Vol. 22, pp. 1747-1753.

Wheeler, J. O. (1961): Whitehorse Map Area, Yukon Territory (105D), G.S.C. Memoir 312.

STATEMENT OF QUALIFICATIONS

I, Gary L. Wesa, of #309 – 6669 Telford Avenue, in the City of Burnaby, B.C., do hereby certify that:

1. I am presently employed as Project Geologist to OMNI RESOURCES INC. and ARKONA RESOURCES INC. with offices at #910 – 700 West Pender Street, Vancouver, British Columbia.

2. I am a graduate of the University of Saskatchewan with a B.Sc. Degree in Geology (1974) and I have practiced my profession continuously since graduation.

3. I have been employed by various mining and exploration companies in Canada, U.S.A. and Brazil since 1970.

4. I am a registered Fellow, in good standing, of the Geological Association of Canada.

5. I am familiar with the geology of the Mount Skukum Volcanic Complex, Goddell/Carbon Hill and surrounding area.

6. I am the author of this report, entitled: "Geological and Geochemical Report on the Goddell/Carbon Hill Property", which is based upon researched documents, referenced in this report, and supervision of the 1998 field program.

Dated at Vancouver, British Columbia this 10 day of February, 1999.

Respectfully Submitted:
OMNI RESOURCES INC.
ARKONA RESOURCES INC.

GEOLOGICAL ASSOCIATION OF CANADA
G. L. WESA
FELLOW

Gary L. Wesa, B.Sc., F.G.A.C.

APPENDIX I

Itemized Cost Statement

Itemized Cost Statement
Goddell - Carbon Hill Project

			Totals
Caron Diamond Drilling Ltd.			
Road Construction		$ 23,527.50	
			$ 23,527.50
Project Personnel			
G. Wesa (Project Geologist)		$ 7,051.31	
T. Elliott (Senior Geologist)		$ 7,077.40	
B. Sauer (Field Assistant)		$ 9,020.43	
T. Johnson (Junior Geologist)		$ 1,146.74	
R. Michel (Field Assistant)		$ 749.42	
R. Stack (Field Assistant)		$ 1,200.00	
			$ 26,245.30
Geochemical Analysis			
Rock Samples	126 @ $23.75/Sample	$ 2,992.50	
Soil Samples	696 @ $18.00/Sample	$ 12,528.00	
Drill Core Samples	17 @ $23.75/Sample	$ 403.75	
			$ 15,924.25
Field Expenses			
Camp/Office Supplies & Tools		$ 3,073.55	
Communication/Satellite Phone		$ 1,737.89	
Equipment Rental		$ 462.84	
Freight/Shipping		$ 678.95	
Fuel (Diesel, Gasoline, Propane)		$ 6,754.18	
Groceries/Food Supplies		$ 6,071.70	
Maintenance/Repairs		$ 3,608.28	
Recording & Assessment		$ 606.74	
Roadwork		$ 535.00	
Travel/Airfair		$ 3,960.34	
			$ 27,489.47
Office Costs			
Salaries			
G. Wesa		$ 1,408.61	
T. Elliott		$ 1,564.51	
Post field, drafting, reproductions		$ 721.71	
			$ 3,694.83
Total Expenditures			**$ 96,881.35**

GEOLOGICAL ASSOCIATION OF CANADA
G.L. WESA
FELLOW

APPENDIX II

Summary of Personnel

SUMMARY OF PERSONNEL

NAME	TITLE	ADDRESS
Gary L. Wesa	Project Geologist	Burnaby, B.C.
Terence Elliott	Geologist	New Westminster, B.C.
Brian Sauer	Prospector	Whitehorse, Yukon
Trent Johnson	Geologist	Kelowna, B.C.
Rod Michel	Field Assistant	Port Coquitlam, B.C.
Ron Stack	Field Assistant	Whitehorse, Yukon

APPENDIX III

Analytical Procedure

ACME ANALYTICAL LABORATORIES LTD.
Assaying & Trace Analysis
852 E. Hastings St., Vancouver, B.C., Canada V6A 1R6
Telephone: (604) 253-3158 Fax: (604) 253-1716

METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE GROUP 1D - 30 ELEMENT ICP BY AQUA REGIA

Sample Preparation:

Soils and sediments are dried (60°C) and sieved to -80 mesh (-177 microns), rocks and drill core are crushed and pulverized to -100 mesh (-150 microns). Plant samples are dried (60°C) and pulverized or dry ashed (550°C). Moss-mat samples are dried (60°C), pounded to loosen trapped sediment then sieved to -80 mesh. At the clients request, moss mats can be ashed at 550°C then sieved to -80 mesh although this can result in the potential loss by volatilization of Hg, As, Sb, Bi and Cr. A 0.5 g split from each sample is placed in a test tube. A duplicate split is taken from 1 sample in each batch of 34 samples for monitoring precision. A sample standard is added to each batch of samples to monitor accuracy.

Sample Digestion:

Aqua Regia is a 3:1:2 mixture of ACS grade conc. HCI, conc. HNO_3 and demineralized H_2O. Aqua Regia is added to each sample and to the empty reagent blank test tube in each batch of samples. Sample solutions are heated for 1 hour in a boiling hot water bath (95°C).

Sample Analysis:

Sample solutions are aspirated into an ICP emission spectrograph (Jarrel Ash Atom Comp model 800 or 975) for the determination of 30 elements comprising: Ag, Al, As, Au, B, Ba, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sr, Th, Ti, U, V, W, Zn.

Data Evaluation:

Raw and final data from the ICP-ES undergoes a final verification by a British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

ACME ANALYTICAL LABORATORIES LTD.
Assaying & Trace Analysis
852 E. Hastings St., Vancouver, B.C., Canada V6A 1R6
Telephone: (604) 253-3158 Fax: (604) 253-1716

METHOD FOR WET GEOCHEM GOLD ANALYSIS

Sample Preparation:

Soils and sediments are dried (60°C) and sieve to -80 mesh.

Rocks and cores are crushed and pulverized to -100 mesh.

Sample Digestion

1. 10g samples in 250 ml beaker, ignite at 600°C for four hours.
2. Add 40 ml of 3:1:2 mixture $HCL:HNO_3:H_20$.
3. Cover beaker with lids.
4. Boil in hot water bath for one hour.
5. Swirl samples 2 to 3 times within the hour.
6. Cool, add 60 ml of distilled water and settle.
7. Pour 50 ml of leached solution using a graduated cylinder into 100 ml volumetric flask.
8. Add 10 ml of MIBK and 25 ml of distilled water.
9. Shake 3 to 4 minutes in shaker.
10. Add additional 25 ml of distilled water to stripe out excess iron.
11. Shake each flask 10 times.
12. Pour MIBK into container for graphite AA finished.

Acme Analytical Laboratories Ltd.
Assaying & Trace Analysis

Method and Specifications for Analytical Package
Group 1F & 1G – Ultratrace ICP Analysis

Comments

Sample Preparation

Soils and sediments are dried (60°C) and sieved to -80 mesh (-177 microns), rocks and drill core are crushed and pulverized to -100 mesh (-150 microns). Plant samples are dried (60°C) and pulverized or dry ashed (550°C). Moss-mat samples are dried (60°C), pounded to loosen trapped sediment then sieved to -80 mesh. At the clients' request moss mats can be ashed at 550°C then sieved to -80 mesh with possible loss of Hg, As, Sb, Bi and Cr by violatization. Splits of 5 g (Group 1G), 15 or 30 g (Group 1F) are weighed into test tubes or beakers. Precision is monitored by duplicate split taken from 1 sample in each batch of 34 samples. Accuracy and measurement process are monitored by reference material STD-D2 added to each batch of samples.

Sample Digestion

Aqua Regia is a 2:2:2 mixture of ACS grade conc. HCI, conc. HNO, and demineralized H_20. Aqua Regia is added to each sample and to the empty reagent blank test tube in each batch of samples. Sample solutions are heated for 1 hr in a boiling hot water bath (95°C).

Extraction

A 30 ml aliquot of the sample solution is extracted using an organic extract (Aliquat 336 and MIBK).

Sample Analysis

An aliquot of the acic sample solution is analysed by direct aspirating into an ICP emission spectrograph (Jarrel Ash AtomComp model 800 or 975) for the analysis of: Al, B, Ba, Ca, Co, Cr, Fe, K, La, Mg, Mn, Na, Ni, P, Sr, Th, Ti, U, V, W and Zn. The extracted sample solution is aspirated into an ultrasonic nebulizer equipped ICP emission spectrograph (Jarrel Ash AtomComp model 975) for the determination of of Ag, As, Bi, Cd, Cu, Ga, Mo, Pb, Sb, Se, Te and Tl. Au included in package Group 1F only, is determined by wet extraction and GFAA analysis (Group 3A). Hg is determined by cold vapour AA analysis (Group IC)

Data Evaluation

Raw and final data from the analytical undergo a final verification by a British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

Acme Analytical Laboratories Ltd.
Assaying & Trace Analysis

Methods and Specifications for Analytical Package
Group 7-15 Element Assay by ICP-Emission Spectrometry

Comments

Sample Preparation

Assaying is recommended for samples containing very high concentrations of commodity or pathfinder elements (ie. > 1%). Soils and sediments are sieved to minus 80 mesh (-177 microns). Rocks are crushed to 75% minus 10 mesh (-1.7 mm), a 250 g sub-sample is riffle splitted then pulverized to 95% minus 100 mesh (-150 microns). Reject duplicate and pulp duplicate splits are taken from one sample in every 34 to monitor sub-sampling variation due to sample inhomogeniety (reject split) and analytical precision (pulp split). Into 100 ml volumetric flasks are placed 1.000 ±0.002g splits of pulp (0.25 g / ml or 0.25 g / 250 ml weight to volume ratios may be used for very high grade samples). In each batch of 34 samples, in-house reference material STD R-1 and a blank are carried through weighing, digestion and analysis to monitor accuracy.

Sample Digestion

Into each flask is added 30 ml of Aqua Regia (2:2:2 ACS grade conc. HCI, conc. HNO_3 and demineralized H_20). Sample solutions are heated for 1 hour in a boiling water bath (95°C) then cooled for 3 hours. Dilute HCI (5%) is added to bring the volume to the 100 ml mark.

Sample Analysis

Sample solutions are aspirated into and ICP emission spectrograph (Jarrel Ash AtomComp model 800 or 975) for the determination of Ag, As, Bi, Cd, Co, Cu, Fe, Mn, Mo, Ni, Pb, Sb, lTh, U and Zn.

Data Evaluation

Raw and final data from the ICP-ES undergoes a final verification by the British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

APPENDIX IV

Rock Geochemical Lab Reports

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]3-1716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources PROJECT SKUKUM CREEK File # 9802765
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary L. Wesa

SAMPLE# (ROCK)		Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
98ACBR-01	ALUNITE	.001	.002	<.01	<.01	.01	<.001	.001	.03	9.91	<.01	<.01	<.01	<.001	<.001	<.01	<.001
98ACWR-01	CAP	.001	<.001	<.01	<.01	.02	<.001	<.001	<.01	.23	<.01	<.01	<.01	<.001	.001	<.01	<.001
98BEKJR-01	BECKER	.001	<.001	.01	.01	<.01	.001	<.001	.26	1.69	<.01	<.01	<.01	<.001	.001	<.01	.001
98DENWR-01		.007	.001	<.01	<.01	.03	<.001	<.001	.01	1.46	<.01	<.01	<.01	<.001	<.001	<.01	<.001
RE 98DENWR-01	DENERO	.007	<.001	<.01	<.01	.04	<.001	<.001	<.01	1.46	<.01	<.01	<.01	<.001	<.001	<.01	<.001
98SCER-01	SINTER	.001	<.001	<.01	<.01	.01	.001	<.001	<.01	.31	<.01	<.01	<.01	<.001	.001	<.01	.003
98SCER-02	CAP	.004	.014	<.01	.02	.01	.002	<.001	.03	16.95	.01	<.01	<.01	<.001	.004	<.01	<.001
98SCMR-01		.001	.001	<.01	.01	.02	.002	<.001	<.01	8.29	<.01	<.01	<.01	<.001	.001	<.01	<.001
STANDARD R-1/AU-1		.087	.835	1.28	2.23	2.94	.025	.025	.08	6.51	.95	.01	.01	.044	.167	.03	.099

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 10 1998 **DATE REPORT MAILED:** July 15/98 **SIGNED BY** ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME ANA[illegible]TICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]3-1716
(ISO [illegible]02 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources PROJECT SINTER CAP-CARBON HILL File # 9803020

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

SINTER CAP — Rock

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
98SCERFL-03	<.001	.001	<.01	<.01	<.01	<.001	<.001	<.01	.29	<.01	<.01	<.01	<.001	<.001	<.01	.002
98SCERFL-04	<.001	.001	<.01	<.01	<.01	<.001	<.001	<.01	.21	<.01	<.01	<.01	<.001	<.001	<.01	<.001
98SCER-05	<.001	.001	<.01	<.01	.01	<.001	<.001	<.01	.19	<.01	<.01	<.01	<.001	<.001	<.01	<.001
98SCER-06	<.001	.001	<.01	<.01	.01	<.001	<.001	<.01	.28	<.01	<.01	<.01	<.001	<.001	<.01	<.001
98SCERFL-07	<.001	<.001	<.01	<.01	.03	<.001	<.001	<.01	.18	<.01	<.01	<.01	<.001	<.001	<.01	<.001
RE 98SCERFL-07	.001	.001	<.01	<.01	.02	<.001	<.001	<.01	.18	<.01	<.01	<.01	<.001	<.001	<.01	<.001

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 23 1998 DATE REPORT MAILED: Aug 4/98 SIGNED BY C. L........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources PROJECT SINTER CAP-CARBON HILL File # 9803075
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

SINTER CAP — Rock

SAMPLE#	Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
98SCBR-01	.001	.014	.15	2.26	2.02	<.001	.001	.09	.74	<.01	<.01	<.01	.039	<.001	.01	.002
98SCBR-02	.001	.012	.63	.32	.53	<.001	.001	.10	1.88	<.01	<.01	<.01	.002	<.001	<.01	<.001
98SCBR-03	.002	.366	.04	.08	.45	<.001	.001	.10	1.74	<.01	<.01	<.01	.001	.002	<.01	<.001
98SCBR-04	.005	3.921	.44	6.12	4.40	.002	.003	.02	6.66	<.01	<.01	<.01	.055	.001	.01	.001
RE 98SCBR-04	.005	3.818	.43	5.93	4.28	.002	.003	.02	6.46	<.01	<.01	<.01	.053	.001	.01	.001
98SCBR-05	<.001	.013	<.01	.03	.03	.001	.001	.13	5.30	<.01	<.01	<.01	<.001	.001	<.01	<.001
98BONWR-01 BONANZA Rock	.001	.022	.83	.06	1.18	<.001	<.001	.04	2.38	<.01	<.01	<.01	.001	<.001	<.01	.565
STANDARD R-1/AU-1	.087	.845	1.33	2.26	3.01	.022	.025	.08	6.50	.97	.01	.01	.045	.168	.03	.098

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 27 1998 **DATE REPORT MAILED:** Aug 6/98 **SIGNED BY** C. L[illegible] ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data / FA ___

ACME ANA[illegible]TICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources Inc. PROJECT SINTER CAP/GODDELL File # 9803304
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G. Wesa

	SAMPLE#		Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
SINTER CAP	98SCERFL-10	Rock	.002	<.001	<.01	<.01	<.01	.002	<.001	<.01	.56	<.01	<.01	<.01	<.001	<.001	<.01	.013
	98SCERFL-11		.001	<.001	<.01	<.01	.01	.002	<.001	<.01	.35	<.01	<.01	<.01	<.001	<.001	<.01	.002
	98SCERFL-12		.001	<.001	<.01	<.01	<.01	.001	<.001	<.01	.33	<.01	<.01	<.01	<.001	<.001	<.01	.006
	98SCERFL-13		.002	<.001	<.01	<.01	.04	.001	<.001	<.01	.32	<.01	<.01	<.01	<.001	<.001	<.01	.018
	RE 98SCERFL-13		.002	.001	<.01	<.01	.04	<.001	<.001	<.01	.32	<.01	<.01	<.01	<.001	.001	<.01	.016

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 7 1998 **DATE REPORT MAILED:** Aug 14/98 **SIGNED BY**.......... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources Inc. PROJECT SKUKUM CREEK/GODDELL File # 9803328
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

	SAMPLE#		Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
SINTER CAP	98SCERFI-14	Rock	.001	<.001	<.01	<.01	.01	<.001	<.001	.01	.68	<.01	<.01	<.01	<.001	<.001	<.01	<.001
	98SCERFI-15		.002	.001	<.01	<.01	.12	<.001	<.001	<.01	1.34	<.01	<.01	<.01	<.001	.002	<.01	.002
	RE 98SCERFI-15		.002	.001	<.01	<.01	.14	<.001	<.001	<.01	1.35	<.01	<.01	<.01	<.001	.002	<.01	.002

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 10 1998 DATE REPORT MAILED: Aug 14/98 SIGNED BY..........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

ASSAY CERTIFICATE

Omni Resources Inc. PROJECT SKUKUM CREEK File # 9803378
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

	SAMPLE#		Mo %	Cu %	Pb %	Zn %	Ag** oz/t	Ni %	Co %	Mn %	Fe %	As %	U %	Th %	Cd %	Sb %	Bi %	Au** oz/t
ANTIMONY ZONE	98AZBR-06	Rock	.021	.138	.39	.01	1.10	<.001	<.001	.06	1.11	.01	<.01	<.01	.001	.039	.01	<.001
	98AZBR-07		<.001	.002	<.01	<.01	.02	<.001	.001	<.01	.27	<.01	<.01	<.01	<.001	.001	<.01	.001
	98AZBR-08		.006	.001	.01	<.01	.01	<.001	<.001	<.01	.50	<.01	<.01	<.01	<.001	.001	<.01	.001
	98AZER-01		<.001	.006	<.01	.01	<.01	.001	.002	.12	3.36	<.01	<.01	<.01	<.001	<.001	<.01	<.001
	98AZER-02		.001	.003	.01	<.01	.10	<.001	<.001	<.01	1.26	<.01	<.01	<.01	<.001	.001	<.01	<.001
	RE 98AZER-02		.001	.002	.01	<.01	.11	<.001	<.001	<.01	1.26	<.01	<.01	<.01	<.001	.001	<.01	<.001
SINTER CAP	98SCER-16	Rock	.005	1.388	.01	.07	1.10	.003	.001	.10	4.08	.06	<.01	<.01	.001	.684	.01	<.001
	98SCERFL-17		.013	1.160	.18	.15	1.65	.001	.001	.01	2.89	.23	<.01	<.01	.001	1.444	.01	.001
	STANDARD R-1/AU-1		.088	.837	1.30	2.29	2.97	.023	.024	.08	6.55	.94	.01	.01	.044	.166	.03	.099

1 GM SAMPLE DIGESTED IN 30 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1.A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 11 1998 **DATE REPORT MAILED:** Aug 14/98 **SIGNED BY** C. Leong ......D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL(ANTIMONY CK) File # 9803584

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: T.M. Elliott

ANTIMONY CREEK — Rock

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** oz/t
98AZBR-01	33	822	924	432	13.0	5	2	239	.63	37	<8	<2	2	24	10.6	508	17	2	.48	.010	5	19	.20	619	<.01	<3	.13	.01	.09	9	<.001
98AZBR-02	3	147	83	860	5.7	14	1	102	.72	37	<8	<2	<2	9	18.4	15116	<3	2	.06	.003	3	16	.01	36	<.01	5	.12	.01	.09	<2	<.001
98AZBR-03	4	22	29	32	<.3	3	1	110	1.57	3	<8	<2	6	23	<.2	135	<3	4	.03	.029	10	9	.04	481	<.01	3	.40	.05	.25	3	<.001
98AZBR-04	9	19	17	18	.8	8	1	46	.94	<2	20	<2	4	7	.2	87	<3	4	.02	.014	3	11	.02	156	<.01	<3	.46	.01	.31	<2	<.001
98AZBR-05	80	37	40	40	<.3	6	4	278	10.00	5	17	<2	16	91	.2	14	3	42	.04	.085	16	62	.25	106	.01	<3	.70	.14	.20	2	<.001
98AZBR-06	7	165	72	20	.4	7	1	460	.60	2	13	<2	13	105	.2	43	<3	3	.87	.009	32	10	.05	857	<.01	<3	.33	.04	.20	<2	<.001
98AZBR-07	2	112	14	9	.4	2	1	1164	.34	3	13	<2	2	252	.2	7	<3	2	13.81	.005	3	7	.05	203	<.01	<3	.12	.01	.11	4	<.001
98AZBR-08	2	249	21	17	.8	7	2	179	.63	48	8	<2	4	60	<.2	27	<3	2	.97	.015	7	8	.39	289	<.01	<3	.27	.06	.15	<2	.002
98AZBR-09	2	2943	23	116	2.0	18	8	910	2.33	109	<8	<2	5	83	1.1	23	4	10	5.32	.035	9	11	2.00	531	<.01	<3	.49	.04	.31	3	<.001
98AZBR-10	3	953	27610	16182	230.9	12	<1	48	.44	198	60	3	<2	64	726.5	16123	<3	1	.10	.001	2	25	.02	43	<.01	<3	.05	<.01	.04	<2	.088
98AZBR-11	2	15	264	54	3.5	2	1	20	.96	2	8	<2	3	67	3.3	198	<3	2	.03	.004	7	10	.02	773	<.01	<3	.36	.01	.24	4	<.001
RE 98AZBR-11	2	15	263	53	3.6	3	1	20	.96	<2	<8	<2	3	69	3.4	199	<3	2	.03	.004	7	11	.02	804	<.01	<3	.37	.01	.24	4	<.001
98AZBR-12	26	748	2804	484	27.8	5	2	249	.64	58	<8	<2	5	56	38.6	341	37	2	.63	.010	7	20	.22	1108	<.01	3	.20	.01	.16	9	.003
98AZBR-13	9	12	123	43	1.3	9	3	94	.54	<2	<8	<2	4	86	1.5	68	<3	1	.27	.004	7	13	.03	493	<.01	<3	.22	.03	.15	<2	<.001
98AZBR-14	3	267	100	45	1.8	4	4	500	1.24	42	26	<2	9	192	.8	13	<3	2	1.60	.010	3	15	.45	1538	<.01	3	.22	.02	.18	8	<.001
STANDARD C3/AU-1	27	67	39	167	5.8	37	13	761	3.38	59	14	3	23	29	23.6	27	21	83	.55	.088	20	172	.61	151	.09	21	1.99	.04	.16	20	.097
STANDARD G-2	1	3	4	40	<.3	7	4	482	1.83	2	<8	<2	4	77	<.2	6	<3	39	.60	.085	8	73	.55	218	.12	<3	1.04	.11	.48	3	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND MASSIVE SULFIDE AND LIMTED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 21 1998 DATE REPORT MAILED: Aug 28/98 SIGNED BY C. Leong ...D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL(ANTIMONY CK) File # 9803868
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

	SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** oz/t
ANTIMONY ZONE ROCK	98AZBR-15	6	58	520	2226	11.3	12	3	449	1.05	74	29	2	6	32	52.6	8214	11	3	.12	.023	12	13	.02	170	<.01	8	.18	.01	.15	<2	.002
	98AZBR-16	<1	4	23	64	.4	10	7	1568	1.35	3	<8	<2	<2	430	1.2	67	<3	11	21.79	.022	13	12	.70	1246	<.01	3	.34	.01	.08	<2	<.001
	98AZBR-17	1	84	16	144	.5	11	17	1711	4.02	4	<8	<2	6	189	1.8	83	<3	40	7.13	.028	5	5	2.08	2487	<.01	<3	.22	.01	.16	<2	<.001
SINTER CAP ROCK	98SCBR-06	<1	32	3	80	.3	13	17	837	3.67	7	<8	<2	<2	99	.4	11	<3	145	2.58	.014	<1	54	1.85	239	.17	4	1.50	.04	.04	2	<.001
	98SCBR-07	1	118	21	79	.6	13	18	470	3.15	9	9	<2	21	75	.5	14	<3	105	.89	.086	46	7	.97	302	.12	<3	1.26	.09	.10	<2	<.001
	98SCBR-08	<1	90	9	130	.7	19	35	793	6.04	7	<8	<2	<2	46	.4	4	<3	206	1.23	.033	1	6	2.31	257	.25	<3	2.23	.12	.12	<2	<.001
	98SCBR-09	23	12	12	8	1.6	18	2	30	.99	86	9	<2	2	7	<.2	13	<3	3	.01	.003	4	26	.01	160	<.01	<3	.05	<.01	.06	<2	<.001
	98SCBR-10	7	74	9	302	1.0	118	27	1570	14.70	57	<8	<2	5	185	.3	4	<3	118	.40	.258	12	62	1.19	96	.01	<3	4.21	.01	.09	<2	<.001
	98SCBR-11	2	452	<3	352	1.3	151	58	1909	18.32	439	<8	<2	3	198	.6	<3	<3	134	1.09	.462	7	73	2.37	38	.01	<3	7.23	.01	.07	<2	<.001
	98SCBR-12	2	42	3	205	<.3	161	36	1164	7.22	23	<8	<2	4	29	.6	3	<3	134	.24	.116	19	155	4.28	97	<.01	<3	4.40	.03	.09	<2	<.001
	98SCBR-13	70	1696	102	206	6.9	14	5	683	2.02	132	<8	<2	3	55	.7	699	4	15	.55	.182	9	13	.14	1071	<.01	7	.43	.01	.22	<2	<.001
	98SCBR-14	19	1473	152	323	4.8	14	6	610	2.38	99	10	<2	5	48	1.9	351	5	6	.41	.024	11	18	.22	213	<.01	<3	.32	.01	.18	8	<.001
	98SCBR-15	1227	430	234	189	11.5	44	14	807	4.65	44	<8	<2	5	26	1.1	34	5	30	.31	.080	15	23	.38	218	<.01	<3	.71	.01	.26	<2	<.001
	98SCBR-16	5	9	10	136	<.3	28	8	935	3.45	9	<8	<2	8	32	.5	4	<3	30	.52	.090	15	21	.42	296	<.01	3	.62	.01	.36	3	<.001
	RE 98SCBR-16	4	9	8	134	<.3	27	8	923	3.40	8	<8	<2	7	31	.6	3	3	30	.52	.089	15	22	.41	295	<.01	3	.64	.01	.37	3	<.001
	98SCBR-17	12	11	82	35	1.4	6	1	47	1.38	350	<8	<2	3	17	<.2	25	<3	10	.02	.029	15	6	.03	349	<.01	6	.36	.01	.27	<2	<.001
	98SCBR-18	8	262	9	409	1.5	25	56	2981	11.83	88	<8	<2	<2	47	<.2	<3	<3	302	.92	.032	2	42	5.31	49	.19	<3	4.94	.01	.05	<2	<.001
	98SCBR-19	2	37	23	88	.4	12	7	364	3.47	12	9	<2	5	8	<.2	3	<3	21	.07	.046	16	10	.97	133	<.01	<3	1.13	.03	.20	2	<.001
	98SCBR-20	17	116	29	124	1.2	41	28	1031	6.92	37	<8	<2	<2	67	.3	5	3	60	1.22	.073	11	41	1.26	501	<.01	<3	2.10	.01	.30	2	<.001
	98SCBR-21	6	170	27	240	1.5	166	23	1578	13.87	135	<8	<2	3	8	.2	29	<3	112	.63	.336	5	109	3.40	33	.01	<3	4.42	<.01	.03	<2	.002
	STANDARD C3/AU-1	25	64	34	173	5.6	36	12	749	3.26	60	23	3	22	29	24.4	22	23	79	.53	.087	17	160	.59	150	.08	22	1.89	.04	.17	17	.102
	STANDARD G-2	1	4	4	48	<.3	8	4	511	1.99	<2	9	<2	4	73	<.2	<3	<3	41	.61	.096	7	73	.57	224	.13	9	.95	.07	.47	3	<.001

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND MASSIVE SULFIDE AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 3 1998 DATE REPORT MAILED: Sept 9/98 SIGNED BY. C. L.......D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data JV FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL/CARBON HILL File # 9803995

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

Zone / Type	SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm
Antimony Zone – Rock	98AZBR-18	2	7	40	133	<.3	4	5	700	1.48	2	<8	<2	3	82	1.9
Antimony Zone – Rock	98AZBR-19	3	577	18	69	1.6	9	9	669	2.20	7	<8	<2	10	200	.3
Antimony Zone – Rock	98AZBR-20	3	7	<3	12	<.3	4	1	139	.52	2	<8	<2	7	53	.3
Antimony Zone – Rock	98AZBR-21	3	5	11	43	<.3	9	9	821	2.16	5	<8	<2	13	174	.4
Antimony Zone – Rock	98AZBR-22	2	5	5	37	<.3	6	6	593	1.77	<2	<8	<2	12	133	<.2
Antimony Zone – Rock	98AZWR-01	6	36	11	87	.4	11	13	903	3.16	7	<8	<2	8	41	.9
Antimony Zone – Rock	98AZWR-02	2	6	14	21	<.3	4	2	159	1.66	2	<8	<2	5	35	<.2
Antimony Zone – Rock	98AZWR-03	4	291	884	54	1.7	7	4	454	1.24	79	<8	<2	<2	408	.7
Antimony Zone – Rock	98AZWR-04	5	260	431	45	2.4	4	2	297	.98	17	<8	<2	2	952	.8
Antimony Zone – Rock	98AZWR-05	3	103	82	20	.7	7	7	322	1.79	5	<8	<2	5	262	.2
Sinter Cap – Rock	98SCBR-22	28	10	23	11	.4	5	1	57	.73	13	<8	<2	<2	13	<.2
Sinter Cap – Rock	98SCBR-23	4	12	11	24	<.3	5	2	169	.92	4	<8	<2	4	23	<.2
Sinter Cap – Rock	98SCBR-24	5	29	30	29	<.3	4	1	291	.83	2	<8	<2	3	17	.3
Sinter Cap – Rock	98SCBR-25	3	3	9	32	<.3	2	<1	73	.40	2	<8	<2	11	11	.3
Sinter Cap – Rock	98SCBR-26	5	5	14	35	<.3	8	1	327	.76	11	<8	<2	12	10	.5
Sinter Cap – Rock	98SCBR-27	21	4	26	15	<.3	6	1	235	.34	7	<8	<2	15	13	<.2
Sinter Cap – Rock	98TR4-01	12	6	26	11	<.3	3	<1	22	.56	18	<8	<2	10	12	<.2
Sinter Cap – Rock	98TR4-02	8	8	25	7	.3	5	<1	16	.60	11	<8	<2	9	11	<.2
Sinter Cap – Rock	98TR4-03	7	8	11	49	<.3	5	1	203	.94	14	<8	<2	9	6	<.2
Sinter Cap – Rock	98TR4-04	6	4	16	49	<.3	9	1	79	.80	3	<8	<2	10	6	<.2
Sinter Cap – Rock	98TR4-05	10	5	4	7	.4	3	<1	18	.40	12	<8	<2	11	3	<.2
Sinter Cap – Rock	RE 98TR4-05	9	5	6	8	.4	3	<1	17	.39	11	<8	<2	11	3	<.2
Sinter Cap – Soil	98TR5A 0+03m-0+05m	3	16	13	35	<.3	5	3	677	1.20	3	<8	<2	3	18	<.2
Sinter Cap – Soil	98TR5A 0+05m-0+10m	3	6	5	39	<.3	7	2	479	1.17	<2	<8	<2	3	22	<.2
Sinter Cap – Soil	98TR5A 0+10m-0+15m	3	8	10	27	<.3	4	2	498	.87	2	<8	<2	3	15	.2
Sinter Cap – Soil	98TR5A 0+15m-0+20m	5	10	10	42	<.3	6	2	804	1.23	5	<8	<2	4	19	.2
Sinter Cap – Soil	STANDARD C3/AU-1	25	60	38	169	5.5	34	12	741	3.27	50	20	4	18	29	24.0
Sinter Cap – Soil	STANDARD G-2	2	3	5	45	<.3	8	4	525	2.06	<2	<8	<2	5	74	<.2

SAMPLE#	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** oz/t
98AZBR-18	<3	<3	2	1.80	.025	6	8	.35	350	<.01	<3	.25	.02	.17	4	<.001
98AZBR-19	20	5	17	2.65	.057	18	9	.91	1591	<.01	4	.28	.04	.20	<2	<.001
98AZBR-20	6	<3	1	.50	.004	7	18	.17	983	<.01	5	.12	.01	.08	7	<.001
98AZBR-21	3	<3	15	3.11	.062	22	10	.89	2005	<.01	3	.31	.02	.23	<2	<.001
98AZBR-22	4	<3	15	2.11	.071	27	9	.44	242	<.01	4	.34	.03	.23	3	<.001
98AZWR-01	<3	4	67	.78	.071	5	18	1.34	137	.13	<3	1.42	.06	.10	<2	<.001
98AZWR-02	<3	<3	19	.05	.025	10	12	.28	285	<.01	<3	.46	.05	.17	4	<.001
98AZWR-03	6	<3	2	1.12	.017	4	9	.34	475	<.01	4	.23	.01	.17	<2	<.001
98AZWR-04	<3	<3	2	.75	.015	4	14	.21	634	<.01	4	.20	.01	.16	5	<.001
98AZWR-05	<3	<3	2	.64	.048	9	6	.17	148	<.01	<3	.29	.01	.23	<2	<.001
98SCBR-22	4	<3	1	.02	.012	4	19	.01	126	<.01	<3	.15	<.01	.10	7	<.001
98SCBR-23	6	<3	3	.10	.026	13	5	.03	209	<.01	3	.55	.01	.27	<2	<.001
98SCBR-24	19	<3	4	.13	.036	17	9	.03	234	<.01	4	.45	.01	.29	5	<.001
98SCBR-25	<3	<3	<1	.05	.005	34	5	.01	128	<.01	<3	.35	.02	.31	<2	<.001
98SCBR-26	3	<3	3	.05	.025	24	5	.01	133	<.01	4	.36	.05	.15	<2	<.001
98SCBR-27	<3	<3	1	.03	.009	36	6	.01	145	<.01	4	.38	.01	.22	<2	<.001
98TR4-01	3	<3	1	.03	.012	22	10	.01	552	<.01	3	.28	.04	.18	4	<.001
98TR4-02	<3	<3	1	.03	.021	20	7	.01	460	<.01	3	.27	.05	.21	<2	.001
98TR4-03	3	<3	2	.06	.017	9	11	.01	134	<.01	<3	.29	.04	.16	5	<.001
98TR4-04	<3	<3	<1	.03	.002	23	8	.01	483	<.01	<3	.26	.05	.18	<2	<.001
98TR4-05	3	<3	<1	.02	.003	8	7	<.01	97	<.01	4	.31	.06	.15	3	<.001
RE 98TR4-05	3	<3	<1	.02	.004	8	7	<.01	96	<.01	<3	.31	.05	.15	3	<.001
98TR5A 0+03m-0+05m	5	<3	11	.12	.037	14	9	.15	209	<.01	<3	.73	.03	.17	4	<.001
98TR5A 0+05m-0+10m	3	<3	13	.13	.034	13	8	.20	223	<.01	<3	.74	.03	.15	<2	<.001
98TR5A 0+10m-0+15m	8	<3	6	.10	.028	13	8	.07	238	<.01	6	.54	.02	.25	5	<.001
98TR5A 0+15m-0+20m	10	<3	9	.13	.036	16	7	.13	350	<.01	<3	.69	.02	.23	2	.001
STANDARD C3/AU-1	18	23	77	.52	.091	16	159	.58	148	.09	21	1.81	.04	.15	17	.095
STANDARD G-2	<3	3	40	.62	.098	6	73	.60	234	.13	3	.95	.07	.46	3	<.001

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND MASSIVE SULFIDE AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 11 1998 DATE REPORT MAILED: Sept 16/98 SIGNED BY: C. L. D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data FA

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL/CARBON HILL File # 9804160
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G. Wesa

ANTIMONY ZONE - ROCK

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm
98AZWR-06	15	1001	328	133	34.8	6	10	780	2.05	87	<8	<2	8	195
98AZWR-07	3	37	25	36	1.0	4	6	446	1.35	4	<8	<2	9	91
98AZBR-23	1	21	12	52	<.3	66	22	825	3.64	3	<8	<2	<2	280
98AZBR-24	2	8	17	37	<.3	6	6	565	1.55	<2	<8	<2	12	104
98AZBR-25	8003	27	31	26	1.8	11	9	307	.75	11	<8	<2	27	74
98AZBR-26	20	35	94	61	1.4	8	5	523	1.46	100	<8	<2	5	53
98AZBR-27	17	5	20	44	<.3	9	7	646	1.68	3	<8	<2	10	276
98AZBR-28	5	56	4028	15308	40.2	3	1	34	.28	14	9	<2	2	19
98AZBR-29	24	13	32	68	2.4	8	5	97	1.18	431	<8	<2	4	97
98AZBR-30	331	140	5320	82	21.9	5	8	154	.59	25	<8	<2	4	411
98AZBR-31	5	9	32	16	.4	7	2	165	.49	13	<8	<2	4	104
98AZBR-32	3	12	41	52	.3	3	2	330	1.48	2	<8	<2	5	58
RE 98AZBR-32	3	14	41	52	<.3	2	2	327	1.46	<2	<8	<2	5	57
98AZBR-33	13	4457	33	51	14.3	7	3	367	1.28	40	<8	<2	<2	44
98AZBR-34	92	882	13	55	2.7	4	9	565	2.13	33	<8	<2	5	83
98AZBR-35	4	30	14	32	1.0	8	4	467	.85	3	<8	<2	2	50
98AZBR-36	5	13	30	61	.5	4	2	516	.72	3	<8	<2	3	26
98AZBR-37	4	44	47	37	25.8	7	3	98	.35	44	<8	<2	2	283
98AZBR-38	2	41	5	74	<.3	92	33	1046	4.91	<2	<8	<2	2	2179
98AZBR-39 not received	-	-	-	-	-	-	-	-	-	-	-	-	-	-
98AZBR-40	8	65	621	9908	5.8	8	2	100	.49	36	<8	<2	3	34
STANDARD C3/AU-1	25	60	37	163	5.3	32	11	738	3.15	54	20	<2	20	29
STANDARD G-2	3	4	3	38	<.3	6	4	466	1.76	<2	<8	<2	4	66

SAMPLE#	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** oz/t
98AZWR-06	2.1	268	8	8	2.27	.058	16	7	.42	1734	<.01	<3	.33	.01	.28	<2	<.001
98AZWR-07	.2	6	<3	6	1.35	.035	19	16	.23	1497	<.01	3	.23	.02	.28	6	<.001
98AZBR-23	<.2	<3	3	34	4.09	.072	8	35	2.11	933	<.01	<3	.59	.02	.33	<2	<.001
98AZBR-24	<.2	<3	<3	10	2.62	.059	23	11	.68	492	<.01	<3	.28	.02	.26	3	<.001
98AZBR-25	.4	<3	<3	4	.64	.032	28	10	.15	710	<.01	<3	.26	.03	.31	<2	<.001
98AZBR-26	.7	20	<3	7	.45	.043	6	19	.11	300	<.01	4	.24	<.01	.33	6	<.001
98AZBR-27	<.2	<3	5	16	2.70	.058	20	9	.74	1346	<.01	<3	.27	.02	.24	<2	<.001
98AZBR-28	315.1	5473	3	1	.02	.001	1	22	<.01	105	<.01	<3	.02	<.01	.08	<2	.001
98AZBR-29	1.0	30	<3	8	.19	.019	7	10	.06	234	<.01	<3	.31	.01	.42	<2	.006
98AZBR-30	2.8	141	<3	2	.05	.018	4	12	.01	926	<.01	3	.11	.01	.22	5	<.001
98AZBR-31	<.2	7	3	4	.51	.024	8	13	.08	914	<.01	<3	.15	<.01	.25	<2	<.001
98AZBR-32	.3	4	6	19	.56	.029	9	14	.20	577	.05	<3	.66	.05	.17	3	<.001
RE 98AZBR-32	.3	5	5	19	.56	.028	9	14	.20	562	.05	<3	.66	.05	.17	3	<.001
98AZBR-33	1.2	54	<3	1	.93	.005	23	15	.11	281	<.01	<3	.06	<.01	.12	<2	<.001
98AZBR-34	.5	5	4	5	1.97	.021	6	15	.49	448	<.01	<3	.20	.01	.25	5	<.001
98AZBR-35	.5	3	<3	2	1.19	.005	3	14	.17	1428	<.01	<3	.09	.01	.17	<2	<.001
98AZBR-36	.7	5	<3	2	.68	.011	7	21	.03	611	<.01	<3	.12	<.01	.20	8	<.001
98AZBR-37	.8	37	<3	1	.08	.002	1	8	<.01	1624	<.01	<3	.03	<.01	.12	<2	<.001
98AZBR-38	.8	<3	<3	102	4.88	.152	18	275	4.01	1408	.03	<3	3.05	.02	.17	<2	<.001
98AZBR-39 not received	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
98AZBR-40	255.9	59	3	2	.18	.004	2	15	.05	203	<.01	<3	.09	<.01	.17	5	.001
STANDARD C3/AU-1	22.5	16	26	74	.51	.086	18	162	.58	169	.08	19	1.83	.03	.19	14	.096
STANDARD G-2	<.2	<3	5	35	.55	.086	7	70	.54	185	.11	<3	.87	.07	.58	<2	<.001

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DATE RECEIVED: SEP 21 1998 DATE REPORT MAILED: Sept 25/98 SIGNED BY.........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

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Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL ANALYSIS CERTIFICATE

Omni Resources Inc. File # 9804279
910 - 700 W. Pender St., Vancouver BC V6C 1G8

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** oz/t
R-1-98	6	9	7	70	<.3	13	9	1185	1.65	<2	<8	<2	3	182	.9	14	6	8	3.21	.013	5	11	.14	2713	<.01	<3	.29	.01	.17	<2	<.001
R-2-98	12	14	157	26	1.7	6	4	170	.94	57	<8	<2	4	13	.2	17	<3	2	.08	.015	9	18	.01	361	<.01	<3	.17	.01	.30	7	.004
R-3-98	7	16	36	29	1.2	9	3	158	.66	22	<8	<2	5	13	<.2	8	<3	2	.17	.022	12	15	.02	377	<.01	<3	.23	<.01	.33	<2	<.001
R-4-98	3	6	149	136	.8	4	4	187	.59	8	<8	<2	3	383	2.3	12	<3	3	.24	.022	7	13	.02	1773	<.01	<3	.21	.01	.36	5	<.001
R-5-98	45	30	80	164	.7	9	7	2201	.99	13	<8	<2	2	56	3.2	23	<3	3	.04	.021	4	13	.01	1933	<.01	<3	.20	<.01	.31	<2	<.001
R-6-98	36	9	34	27	1.9	4	4	74	.44	13	<8	<2	2	56	.2	7	<3	4	.04	.007	2	16	.01	2117	<.01	<3	.21	<.01	.38	6	<.001
R-7-98	3	4	44	26	<.3	7	3	376	.85	<2	<8	<2	13	109	<.2	<3	<3	6	1.70	.024	23	9	.09	1083	<.01	<3	.42	.02	.29	<2	<.001
R-8-98	4	12	58	142	1.1	5	4	1087	1.46	3	<8	<2	13	28	.6	7	<3	7	.87	.037	24	11	.06	251	<.01	<3	.49	.03	.43	3	<.001
R-9-98	4	2	12	100	<.3	11	5	2056	1.23	4	<8	<2	12	67	1.4	3	<3	3	1.43	.010	15	13	.10	1812	<.01	<3	.19	.02	.22	<2	<.001
R-10-98	3	4	28	81	.3	7	5	1627	1.37	135	<8	<2	23	31	1.3	6	<3	5	1.44	.035	32	15	.06	496	<.01	<3	.37	.01	.40	6	<.001
R-11-98	4	6	31	113	1.5	9	5	1248	.83	600	<8	<2	8	36	1.7	9	<3	3	.62	.018	15	12	.03	1278	<.01	<3	.19	<.01	.30	<2	<.001
R-12-98	12	103	3486	8413	41.5	6	3	2084	.79	372	<8	<2	3	32	142.0	50	<3	2	.26	.012	6	19	.02	319	<.01	<3	.15	.01	.23	13	.014
R-13-98	3	2	50	86	.4	7	1	524	.91	6	<8	<2	12	80	1.1	<3	<3	3	1.17	.010	16	7	.08	83	<.01	<3	.36	.03	.42	<2	<.001
R-14-98 Rock	5	10	47	80	.4	5	3	763	1.28	9	<8	<2	9	90	1.0	7	<3	7	1.50	.021	14	9	.07	323	<.01	<3	.40	.02	.40	3	<.001
R-15-98	99	317	1146	11125	175.3	6	5	652	1.59	16	<8	<2	6	16	188.8	66	296	3	.32	.024	11	12	.04	106	<.01	<3	.22	.01	.30	3	.004
R-16-98	6	75	1281	2397	17.8	11	6	2655	2.01	158	<8	<2	<2	50	68.7	58	5	21	3.26	.052	4	25	.16	609	<.01	<3	.33	.01	.23	2	.004
R-17-98	18	248	294	135	10.1	7	2	2719	1.37	35	<8	<2	3	32	2.3	151	9	4	1.52	.009	2	15	.26	412	<.01	<3	.13	.01	.18	<2	<.001
R-18-98	194	553	11528	2472	21.8	5	3	228	.85	50	<8	<2	<2	38	58.9	312	29	2	.08	.006	1	25	.03	272	<.01	<3	.09	<.01	.18	8	.001
R-19-98	35	13	100	39	.6	10	1	80	.54	7	<8	<2	<2	5	.6	11	<3	1	.02	.008	2	16	.01	56	<.01	<3	.09	.01	.20	<2	<.001
R-20-98	5	60	3962	2454	45.4	9	4	35	.90	133	<8	<2	<2	8	53.9	35477	3	1	.02	.002	1	27	<.01	67	<.01	<3	.02	<.01	.10	<2	.007
RE R-20-98	5	61	4382	2535	46.6	11	4	41	.95	158	<8	<2	<2	9	55.4	39502	<3	1	.02	.002	1	37	<.01	88	<.01	<3	.03	<.01	.09	2	.008
R-21-98	9	4	71	66	1.5	8	1	65	.52	73	<8	<2	3	44	2.1	510	<3	1	.02	.006	7	17	.01	54	<.01	<3	.20	<.01	.36	<2	.009
R-22-98	28	4995	2286	2934	39.3	5	3	326	2.34	149	<8	<2	<2	16	38.9	445	27	2	.21	.002	3	23	.02	68	<.01	<3	.16	.01	.21	9	.005
R-23-98	9	88	169	258	1.5	8	4	381	1.40	7	<8	<2	3	21	4.8	108	<3	11	.32	.010	7	19	.06	733	<.01	<3	.20	.02	.14	2	<.001
R-24-98	4	273	2586	166	12.8	6	4	587	.85	27	<8	<2	5	49	4.1	253	<3	2	1.10	.018	11	19	.11	1273	<.01	<3	.19	.01	.30	7	<.001
R-25-98	11	11	52	153	2.7	10	3	162	.85	35	<8	<2	24	18	3.3	193	<3	1	.06	.009	15	9	.01	105	<.01	<3	.26	.01	.41	<2	.002
R-26-98	4	7	26	42	<.3	8	6	602	1.61	3	<8	<2	14	52	.6	33	<3	18	.49	.048	22	14	.17	346	<.01	<3	.66	.02	.38	2	<.001
98AZBR-39	1	21	12	84	<.3	41	26	1192	4.48	9	<8	<2	2	259	.8	24	5	59	7.65	.159	13	41	3.02	724	<.01	<3	.62	.03	.43	<2	<.001
STANDARD C3/AU-1	25	60	31	168	5.1	35	11	740	3.13	56	19	3	21	29	22.6	18	18	77	.53	.087	18	166	.57	152	.09	21	1.79	.04	.20	15	.096
STANDARD G-2	2	2	<3	46	<.3	9	6	557	2.09	<2	<8	<2	4	79	<.2	<3	<3	43	.65	.098	8	81	.61	245	.13	<3	1.03	.08	.61	2	<.001

Goddell- Antimony Creek Road

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ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
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DATE RECEIVED: SEP 28 1998 **DATE REPORT MAILED:** Oct 2/98 **SIGNED BY**.........D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

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Data FA

APPENDIX V

Soil Geochemical Lab Reports

ACME ANA[illegible]ICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]3-1716
(ISO[illegible]02 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

SINTER GRID

Omni Resources PROJECT SKUKUM CREEK File # 9802764 Page 1
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary L. Wesa

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L15+00N 5+00E	8.6	17.1	12.0	40.8	138	7	4	237	1.48	15.7	<5	2	12	.15	7.4	.3	25	.09	.044	10	14	.20	74	.02	<3	.61	.01	.03	<2	.2	178	.3	.3	2.7	9
L15+00N 5+25E	8.6	20.0	6.7	42.7	181	8	5	247	1.51	12.4	<5	2	15	.18	7.1	.3	26	.12	.052	11	13	.22	100	.02	<3	.69	.01	.05	<2	.2	154	.3	.2	2.8	8
L15+00N 5+50E	7.9	18.5	6.1	39.7	159	9	5	262	1.36	13.4	<5	2	13	.12	6.4	.2	23	.09	.046	9	12	.20	90	.02	<3	.63	.01	.04	<2	<.2	160	.3	.2	2.4	6
L15+00N 5+75E	10.2	22.6	31.6	80.0	169	9	6	933	1.98	16.7	<5	<2	14	.14	10.6	.4	30	.13	.076	12	12	.30	134	.01	<3	1.01	.01	.08	<2	.2	222	<.3	.2	3.6	4
L15+00N 6+00E	5.3	14.1	8.0	37.3	145	5	4	341	1.05	9.7	<5	<2	13	.10	4.5	.2	18	.13	.071	8	7	.17	84	.02	<3	.70	.02	.06	<2	<.2	110	<.3	<.2	2.2	4
L15+00N 6+25E	16.6	28.2	35.1	97.4	301	13	7	763	2.46	23.8	<5	2	22	.31	11.0	.6	36	.09	.106	16	21	.34	286	.01	<3	1.69	.01	.10	<2	.2	283	<.3	.2	5.1	10
L15+00N 6+50E	13.5	17.8	13.6	61.3	147	9	5	445	1.74	24.4	<5	<2	18	.20	23.8	.4	27	.05	.066	9	12	.17	157	.01	3	.80	.01	.06	<2	<.2	289	<.3	.2	3.1	3
L15+00N 6+75E	17.3	20.0	47.7	90.7	504	10	5	522	1.95	25.6	<5	2	25	.24	26.8	.6	31	.19	.092	15	14	.31	225	.01	<3	1.29	.01	.09	<2	.2	412	.3	.2	4.1	11
L15+00N 7+00E	24.0	20.6	39.8	82.7	415	11	5	450	2.15	32.9	<5	2	23	.20	35.8	.6	33	.10	.094	12	17	.24	173	.01	<3	1.25	.01	.08	<2	.3	547	<.3	.2	4.1	16
L15+00N 7+25E	20.6	20.7	38.3	63.1	361	7	4	354	1.67	20.2	<5	4	23	.12	13.7	.4	25	.10	.093	20	12	.15	235	<.01	<3	1.43	.01	.08	<2	.4	193	.3	.2	3.7	4
L15+00N 7+50E	10.4	16.8	52.7	107.6	198	6	6	1017	2.33	14.0	5	<2	17	.38	8.2	.5	37	.16	.107	15	12	.26	183	.01	<3	1.05	.01	.09	<2	.2	84	<.3	.2	3.8	5
L15+00N 7+75E	8.2	14.5	28.0	61.8	120	11	4	312	2.04	18.2	10	3	12	.44	9.5	.3	33	.11	.052	14	12	.25	108	.01	<3	1.00	.01	.05	<2	<.2	119	<.3	.2	3.2	2
L15+00N 8+00E	10.1	15.7	18.1	65.3	191	15	8	466	2.09	21.0	5	3	14	.17	8.1	.3	31	.15	.059	18	14	.24	158	.02	<3	.89	.01	.06	<2	.2	156	<.3	.2	3.0	4
L15+00N 8+25E	14.8	21.9	20.0	73.7	234	16	8	382	2.43	25.4	<5	<2	19	.15	7.1	.3	28	.08	.083	14	15	.20	200	.01	<3	1.24	.01	.07	<2	.2	190	<.3	.2	3.4	4
L15+00N 8+50E	18.1	21.1	74.0	90.9	566	17	7	528	2.55	16.3	<5	4	18	.09	11.6	.4	29	.09	.126	21	15	.21	317	<.01	<3	1.86	.01	.09	<2	.6	394	.3	.2	4.2	9
RE L15+00N 9+25E	7.1	11.9	25.2	70.8	96	8	2	249	1.47	10.6	<5	3	7	.23	7.5	.4	17	.06	.029	17	4	.13	77	.01	<3	.63	.01	.09	<2	.2	25	<.3	<.2	2.2	20
L15+00N 8+75E	11.5	17.7	63.9	91.0	288	17	20	1476	2.52	15.4	<5	5	17	.19	12.5	.4	29	.10	.088	18	14	.26	273	<.01	<3	1.44	.01	.12	<2	.9	176	.3	<.2	4.2	7
L15+00N 9+00E	8.3	17.9	102.0	122.4	379	15	11	1573	2.05	14.4	<5	3	12	.64	13.4	.5	25	.11	.091	18	9	.19	226	<.01	<3	1.00	.01	.13	<2	.2	79	<.3	.2	3.1	8
L15+00N 9+25E	7.0	12.1	30.0	69.0	104	7	2	242	1.43	12.2	<5	3	7	.26	8.3	.4	17	.06	.029	17	4	.12	79	.01	<3	.63	.01	.09	<2	.3	28	<.3	<.2	2.6	25
L15+00N 9+50E	4.5	18.9	55.6	95.4	215	10	4	453	2.29	14.0	<5	6	13	.45	5.1	.3	25	.06	.063	20	10	.29	158	<.01	<3	.95	.01	.12	<2	.2	40	.4	.3	3.5	15
L15+00N 9+75E	7.3	17.8	42.2	102.8	169	8	5	498	2.44	14.4	<5	5	11	.18	5.6	.5	28	.06	.040	18	9	.19	102	.01	<3	.87	.01	.12	<2	.2	44	<.3	.2	3.3	4
L15+00N 10+00E	2.6	7.2	19.7	242.8	130	11	7	673	1.91	10.5	<5	9	6	.42	2.2	.2	8	.15	.078	27	2	.03	161	<.01	<3	.78	<.01	.15	<2	.5	70	<.3	<.2	1.3	6
L15+00N 10+25E	41.1	13.2	43.7	86.4	339.	4	3	439	1.28	18.8	<5	3	8	.22	4.7	.2	12	.04	.052	18	5	.10	121	<.01	<3	.92	.01	.15	<2	.3	50	<.3	<.2	2.7	30
L15+00N 10+50E	3.9	28.3	25.7	84.7	145	5	4	1144	1.34	1.9	<5	5	5	.48	5.0	.3	11	.08	.050	22	3	.07	213	<.01	<3	.63	.01	.12	<2	<.2	27	<.3	<.2	1.5	4
L15+00N 10+75E	3.1	22.1	24.5	95.3	111	14	8	883	3.08	9.6	<5	4	6	.30	5.5	.3	35	.05	.134	22	18	.14	182	<.01	<3	1.46	.01	.10	<2	.5	33	<.3	<.2	3.4	7
L15+00N 11+00E	3.9	18.8	56.6	99.5	87	8	8	534	2.69	13.2	5	5	11	.27	5.0	.2	34	.14	.071	18	12	.27	106	.01	<3	1.32	.01	.08	<2	.2	55	<.3	<.2	2.9	8
L14+50N 5+00E	7.9	15.9	7.5	40.2	311	11	7	260	1.61	18.6	<5	2	12	.19	5.6	.3	29	.06	.026	8	14	.22	100	.02	<3	.80	.01	.05	<2	.2	115	<.3	.2	3.0	5
L14+50N 5+25E	8.9	16.5	5.2	36.6	130	11	4	177	1.30	16.0	7	2	14	.15	6.3	.2	24	.08	.029	8	11	.15	97	.02	<3	.52	.01	.03	<2	<.2	134	<.3	.2	2.4	7
L14+50N 5+50E	11.4	21.7	1.3	61.4	403	14	6	301	1.82	21.9	7	3	24	.22	8.2	<.6	31	.16	.064	14	16	.28	232	.02	3	1.01	.01	.08	<2	<.6	312	<.9	<.6	4.5	9
L14+50N 5+75E	7.9	23.7	12.6	56.5	250	12	6	347	1.75	21.0	6	2	19	.15	8.2	.3	30	.13	.073	13	13	.27	118	.02	<3	.93	.01	.08	<2	<.2	228	<.3	.2	2.9	8
L14+50N 6+00E	8.3	21.6	12.8	60.8	164	15	6	320	1.90	22.6	10	3	19	.16	6.7	.3	31	.12	.056	12	15	.28	121	.02	<3	.89	.01	.06	<2	<.2	172	<.3	.2	3.0	5
L14+50N 6+25E	7.8	22.2	15.3	52.6	142	11	6	333	1.69	19.3	<5	<2	15	.15	6.1	.4	29	.11	.061	12	13	.27	103	.02	<3	.99	.01	.05	<2	<.2	157	<.3	.2	3.1	6
L14+50N 6+50E	8.1	19.6	11.4	57.0	137	13	6	287	1.84	21.5	6	<2	14	.19	6.5	.3	31	.09	.060	11	15	.24	85	.02	3	.98	.01	.06	<2	.2	130	.3	.2	3.7	5
L14+50N 6+75E	26.3	23.5	17.5	49.9	433	13	6	559	2.38	49.3	5	<2	26	.13	12.3	.9	35	.06	.117	11	23	.17	317	.01	4	1.26	.01	.10	<2	.2	277	.7	.7	5.2	6
STANDARD D2/C3/AU-S	24.0	124.2	98.5	279.9	1933	30	15	1087	4.37	72.8	25	20	57	1.97	9.8	19.6	71	.72	.107	16	56	1.14	266	.12	32	2.30	.06	.71	17	2.7	1028	.3	2.2	7.1	51

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 10 1998 DATE REPORT MAILED: July 16/98 SIGNED BY.............D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data ___ FA ____

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L14+50N 7+00E	7.9	19.7	16.3	64.4	131	14	6	347	1.87	18.0	<5	4	15	.22	6.5	.3	30	.15	.077	12	16	.27	86	.02	<3	.87	.01	.07	<2	<.2	225	.4	<.2	3.1	28
L14+50N 7+25E	13.6	22.1	24.4	55.3	148	13	5	204	2.01	40.6	9	2	21	.15	6.8	.5	28	.05	.084	16	14	.21	161	.01	<3	1.15	.01	.08	<2	.2	158	.3	.2	3.9	3
L14+50N 7+50E	13.2	23.6	21.2	61.4	155	10	4	437	2.06	39.5	11	2	17	.18	8.7	.5	27	.04	.086	13	13	.17	126	.01	<3	1.01	.01	.10	<2	.3	75	.4	.2	4.3	5
L14+50N 7+75E	10.2	28.8	77.9	98.8	233	23	24	1314	2.73	22.6	<5	6	29	.17	8.2	.4	33	.06	.083	21	12	.30	279	<.01	<3	1.41	.01	.11	<2	<.2	133	<.3	<.2	3.8	4
L14+50N 8+00E	7.0	16.8	16.4	45.4	124	12	4	163	1.91	17.9	13	4	10	.18	6.1	.3	28	.07	.030	11	12	.19	68	.02	<3	.79	.01	.04	<2	<.2	77	.3	<.2	2.7	4
L14+50N 8+25E	9.6	19.9	15.1	49.0	145	12	4	217	1.86	19.9	12	<2	18	.17	6.7	.3	25	.09	.064	12	11	.15	228	.01	<3	.82	.01	.06	<2	<.2	160	.3	<.2	3.1	7
L14+50N 8+50E	14.3	29.9	27.7	74.5	693	22	9	414	2.22	26.0	<5	2	21	.25	8.8	.5	27	.08	.090	17	15	.20	260	.01	<3	1.44	.01	.10	<2	.2	462	.5	.2	4.0	10
L14+50N 8+75E	7.6	16.1	14.0	47.5	75	11	5	221	1.76	18.1	13	3	12	.16	6.6	.3	26	.07	.025	9	11	.20	100	.02	<3	.69	.01	.05	<2	<.2	102	.3	<.2	2.8	3
L14+50N 9+00E	5.4	20.6	75.3	116.0	195	8	6	734	2.56	17.8	<5	6	19	.43	13.4	.8	31	.17	.059	20	10	.38	334	<.01	4	1.32	.01	.09	<2	.3	77	<.3	.3	4.8	2
L14+50N 9+25E	6.4	14.8	70.9	107.4	<30	13	5	572	1.99	9.5	<5	7	7	.34	11.4	.5	20	.10	.041	17	6	.23	87	<.01	<3	1.09	<.01	.11	<2	<.2	48	<.3	<.2	2.9	13
L14+50N 9+50E	12.3	22.2	79.4	109.5	139	7	6	572	3.10	16.6	<5	6	15	.27	7.5	.5	15	.07	.051	22	5	.11	144	<.01	<3	.95	.01	.14	<2	.3	69	.4	.2	2.7	3
L14+50N 9+75E	3.9	6.0	19.7	49.1	364	2	1	46	.81	16.4	<5	3	3	.10	1.3	.2	4	.04	.026	14	1	.01	52	<.01	<3	.72	.01	.10	<2	<.2	24	<.3	<.2	1.5	33
L14+50N 10+00E	7.1	44.4	38.1	284.1	1043	6	6	973	2.92	7.4	5	6	11	2.19	14.9	.6	31	.23	.205	26	9	.38	339	<.01	<3	1.69	.01	.12	<2	.3	111	.4	<.2	4.8	8
L14+50N 10+25E	6.9	22.4	120.6	157.3	879	5	6	615	2.54	14.0	<5	6	13	.59	7.2	1.3	27	.09	.055	15	11	.20	134	.01	<3	1.31	.01	.10	<2	.3	147	.3	.2	3.5	6
L14+50N 10+50E	10.4	22.3	59.5	108.3	167	5	7	867	2.57	9.8	9	6	8	.27	12.4	.4	27	.12	.064	18	8	.18	141	<.01	<3	1.24	.01	.13	<2	.6	33	<.3	<.2	2.7	6
L14+50N 10+75E	5.9	18.6	42.2	89.3	182	7	5	334	2.56	25.3	<5	6	20	.43	10.3	.3	29	.11	.033	19	9	.31	136	.01	<3	1.12	.01	.12	<2	.4	69	.3	.3	4.7	2
L14+50N 11+00E	2.6	21.0	33.3	88.4	96	6	7	733	3.83	13.2	<5	3	25	.31	13.9	.3	64	.32	.088	13	17	.56	191	.01	4	1.28	.01	.16	<2	<.2	80	<.3	<.2	5.9	<1
L14+00N 5+00E	9.4	18.2	14.2	50.7	183	12	5	161	1.76	17.3	6	<2	12	.20	7.9	.4	31	.05	.029	9	13	.16	62	.02	<3	.68	.01	.04	<2	<.2	176	.3	.2	3.1	5
RE L14+00N 5+00E	10.0	18.2	15.0	50.4	182	13	5	154	1.78	19.3	18	2	13	.21	7.9	.3	32	.05	.030	9	14	.16	68	.02	<3	.70	.01	.04	<2	.2	168	.4	.2	3.3	5
L14+00N 5+25E	9.2	17.6	14.5	50.7	136	13	5	266	1.68	19.4	6	3	15	.26	7.9	.4	28	.12	.049	10	14	.20	127	.02	<3	.64	.01	.05	<2	<.2	203	.4	.2	2.6	8
L14+00N 5+50E	9.3	21.5	17.1	56.2	181	14	6	341	2.05	24.2	18	4	17	.25	8.0	.4	36	.16	.074	13	19	.32	91	.03	<3	1.08	.01	.06	<2	.2	110	.5	<.2	4.1	5
L14+00N 5+75E	10.6	20.3	21.5	63.1	272	14	6	401	1.98	25.7	8	3	22	.30	10.0	.5	31	.13	.071	13	15	.29	190	.02	<3	1.04	.01	.08	<2	.2	195	.5	.3	4.4	8
L14+00N 6+00E	8.5	23.8	24.0	52.6	241	11	5	305	1.87	21.7	12	3	19	.13	7.6	.5	31	.14	.086	13	12	.29	107	.02	<3	.98	.02	.08	<2	.2	110	.3	.2	4.0	4
L14+00N 6+25E	16.9	16.8	26.4	48.5	267	13	5	208	1.94	40.1	14	5	18	.18	16.7	.7	28	.13	.048	11	17	.20	216	.03	<3	.61	.01	.06	<2	<.2	325	.7	.4	2.7	5
L14+00N 6+50E	10.1	17.5	15.2	45.7	197	13	5	263	1.84	28.9	13	3	14	.20	8.2	.4	31	.11	.052	11	17	.23	86	.02	<3	.89	.01	.06	<2	.2	115	.5	.3	3.3	3
L14+00N 6+75E	9.0	17.2	15.2	42.4	141	11	5	261	1.61	23.5	12	<2	15	.16	7.0	.3	27	.10	.058	10	13	.20	75	.02	<3	.82	.01	.06	<2	<.2	98	.5	.2	3.4	5
L14+00N 7+00E	12.8	21.7	18.4	57.5	175	11	5	388	1.94	37.2	11	<2	22	.20	9.1	.5	26	.07	.085	9	15	.21	153	.01	<3	1.20	.01	.09	<2	.2	147	.5	.2	4.6	4
L14+00N 7+25E	11.1	18.9	17.2	52.8	147	11	5	285	1.84	41.6	9	<2	22	.33	8.9	.5	27	.09	.060	8	14	.22	213	.01	<3	.87	.01	.07	<2	.2	111	.4	.3	4.2	3
L14+00N 7+50E	9.2	28.1	84.5	92.4	261	13	14	877	3.26	25.2	10	4	13	.19	20.7	.5	41	.04	.081	17	15	.36	185	.01	<3	1.40	<.01	.09	<2	.3	117	.4	.2	4.6	14
L14+00N 7+75E	9.4	14.0	18.8	44.2	182	8	5	647	1.81	22.2	14	4	12	.12	7.9	.3	26	.04	.023	11	9	.12	98	.01	<3	.92	.01	.06	<2	.2	82	.5	.2	3.8	2
L14+00N 8+00E	24.9	32.0	55.2	94.4	502	25	8	517	2.80	45.4	8	2	35	.20	10.6	.7	25	.12	.101	23	15	.15	523	<.01	<3	1.43	.01	.13	<2	.3	612	.6	.4	4.0	13
L14+00N 8+25E	7.6	13.3	15.5	42.5	101	10	4	175	1.63	19.1	17	3	11	.15	7.2	.3	25	.06	.021	11	9	.14	75	.02	<3	.60	.01	.04	<2	<.2	63	.3	.2	2.8	4
L14+00N 8+50E	7.0	12.1	13.4	42.0	69	10	4	165	1.53	19.7	12	4	11	.16	7.5	.2	24	.07	.020	13	10	.13	67	.02	<3	.49	.01	.04	<2	<.2	87	.3	<.2	2.0	9
L14+00N 8+75E	27.5	19.9	60.3	207.5	307	9	8	1579	2.33	15.3	10	6	11	.57	10.2	.8	20	.08	.050	18	7	.12	359	<.01	<3	1.07	<.01	.12	<2	.4	151	.6	.2	2.5	5
STANDARD D2/C3/AU-S	24.6	127.9	99.1	280.6	1889	29	17	1084	4.51	73.7	25	21	57	1.90	10.1	19.7	71	.71	.109	16	56	1.12	264	.13	28	2.33	.06	.72	14	2.5	996	.5	2.2	7.5	56

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data / FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L14+00N 9+00E	9.5	25.2	78.7	198.7	131	18	12	748	3.16	7.5	<5	3	12	.49	17.8	.5	35	.17	.116	36	6	.10	262	<.01	<3	.99	<.01	.10	<2	.2	60	<.3	<.2	3.9	2
L14+00N 9+25E	6.8	23.4	72.8	113.6	188	4	7	675	2.84	16.0	<5	5	19	.16	4.7	.5	24	.11	.044	21	6	.19	220	<.01	<3	1.18	.01	.07	<2	.3	89	.9	.4	3.1	11
L14+00N 9+50E	10.0	20.0	75.4	72.5	522	4	4	243	2.21	43.0	<5	5	16	.17	3.4	.3	17	.05	.045	18	7	.14	85	.01	<3	.74	.01	.11	<2	<.2	248	<.3	.2	3.2	29
L14+00N 9+75E	12.9	191.3	1277.9	1122.2	1333	6	7	2196	3.40	16.9	<5	8	12	2.64	50.4	13.1	40	.40	.175	39	7	.06	617	<.01	<3	1.15	.01	.13	<2	.3	195	1.4	2.4	2.8	4
L14+00N 10+00E	22.3	24.0	57.9	170.9	465	2	3	764	1.28	12.5	<5	2	10	.85	6.3	1.2	7	.04	.024	14	1	.06	117	<.01	<3	.57	.01	.10	<2	.2	65	.3	.3	1.6	4
L14+00N 10+25E	15.8	27.9	161.4	451.3	1088	9	11	2805	3.57	21.9	<5	5	15	.97	5.7	2.7	21	.13	.066	92	8	.12	738	<.01	<3	1.13	.01	.11	<2	.2	178	.5	.2	2.7	12
L14+00N 10+50E	128.5	44.1	77.0	229.7	1218	6	6	1435	2.81	12.8	<5	2	15	1.13	25.1	2.0	31	.20	.059	19	7	.06	347	<.01	<3	.71	.01	.18	2	<.2	92	.3	.2	3.0	1
L14+00N 10+75E	13.0	19.3	37.9	143.4	166	5	3	735	1.96	8.6	<5	<2	9	.96	7.0	.5	22	.09	.090	17	8	.08	202	<.01	<3	.79	.01	.12	<2	.3	46	<.3	<.2	3.8	<1
L14+00N 11+00E	8.0	16.4	51.6	160.1	220	7	5	913	2.17	12.5	<5	<2	13	.92	5.4	.4	24	.09	.085	16	10	.18	142	.01	<3	1.08	.01	.12	<2	<.2	48	<.3	<.2	4.1	3
L13+50N 5+00E	9.0	17.4	20.3	45.0	281	16	6	226	1.85	23.4	5	2	15	.31	7.1	.3	32	.10	.036	10	12	.16	74	.02	<3	.71	.01	.04	<2	<.2	106	<.3	.2	3.3	6
L13+50N 5+25E	10.1	15.4	16.4	45.3	189	14	5	304	1.76	22.1	<5	<2	14	.21	7.1	.2	30	.05	.040	9	14	.15	69	.01	<3	.71	.01	.04	<2	<.2	124	<.3	<.2	3.4	2
L13+50N 5+50E	12.0	20.5	15.9	45.1	299	11	5	236	1.97	29.3	<5	<2	18	.24	6.5	.4	31	.05	.106	12	14	.14	99	.01	<3	.96	.01	.06	<2	<.2	130	<.3	<.2	4.8	2
L13+50N 5+75E	9.7	11.6	11.4	26.4	63	7	3	90	1.18	14.4	<5	<2	12	.13	5.8	.3	30	.05	.030	8	9	.02	78	.02	<3	.35	<.01	.04	<2	<.2	51	<.3	<.2	3.8	17
L13+50N 6+00E	8.8	13.3	13.8	35.9	115	10	4	183	1.82	21.9	5	<2	12	.15	6.6	.2	33	.06	.026	9	16	.16	74	.02	<3	.68	.01	.04	<2	<.2	92	<.3	<.2	3.5	2
RE L13+50N 6+00E	9.1	14.2	15.0	35.1	132	10	4	186	1.76	18.1	<5	<2	12	.16	7.7	.2	31	.06	.026	9	14	.16	71	.02	<3	.67	.01	.04	<2	<.2	84	<.3	.2	3.9	4
L13+50N 6+25E	7.6	14.5	11.3	34.8	150	10	4	179	1.63	19.1	<5	<2	13	.18	7.5	.2	29	.08	.032	9	15	.18	74	.02	<3	.73	.01	.04	<2	.2	121	<.3	.2	3.3	3
L13+50N 6+50E	19.0	18.4	21.1	33.6	454	10	4	252	1.68	32.6	<5	<2	44	.26	8.7	.4	23	.12	.070	10	17	.08	545	<.01	<3	.84	.01	.10	<2	.2	340	.3	.2	3.8	3
L13+50N 6+75E	9.0	12.5	12.5	33.7	172	8	3	140	1.40	20.4	<5	<2	11	.19	6.8	.2	24	.05	.031	7	13	.12	51	.01	<3	.60	.01	.03	<2	<.2	91	<.3	<.2	3.0	3
L13+50N 7+00E	9.3	14.9	16.3	42.3	148	9	4	204	1.62	22.5	<5	<2	14	.15	5.8	.3	26	.05	.055	10	14	.13	68	.01	<3	.70	.01	.06	<2	.2	85	.3	<.2	4.0	3
L13+50N 7+25E	5.0	14.3	7.6	27.9	159	6	4	169	1.27	17.2	<5	<2	13	.08	2.7	<.2	24	.08	.053	6	7	.13	76	.02	<3	.59	.02	.05	<2	<.2	114	<.3	<.2	2.9	4
L13+50N 7+50E	14.6	14.1	30.1	38.4	281	8	3	146	1.71	39.1	<5	4	18	.14	5.3	.3	21	.05	.034	17	10	.12	122	<.01	<3	.81	.01	.09	<2	<.2	104	<.3	.2	3.1	4
L13+50N 7+75E	16.9	19.7	19.5	44.2	280	11	4	245	1.80	40.1	<5	<2	25	.13	4.5	.3	24	.09	.090	16	13	.15	300	.01	<3	1.09	.01	.11	<2	1.0	257	<.3	.2	3.4	8
L13+50N 8+00E	28.8	34.4	58.4	285.5	226	72	17	1511	3.60	14.2	<5	4	11	.78	5.8	.5	23	.06	.077	33	9	.06	326	<.01	<3	1.06	.01	.11	<2	.4	227	<.3	.2	2.0	5
L13+00N 5+00E	12.8	17.9	20.0	52.2	102	16	6	269	1.84	23.5	<5	<2	16	.22	7.9	.4	28	.07	.038	10	15	.18	78	.01	<3	.74	.01	.05	<2	<.2	200	<.3	<.2	2.7	7
L13+00N 5+25E	8.4	15.3	12.6	47.8	155	14	5	232	1.69	14.8	<5	<2	13	.19	5.5	.2	27	.06	.031	9	11	.17	59	.02	<3	.65	.01	.04	<2	<.2	130	<.3	.2	2.2	3
L13+00N 5+50E	13.4	15.0	13.5	43.5	211	12	4	209	1.58	17.3	<5	<2	21	.19	6.8	.3	25	.08	.034	9	13	.14	179	.01	<3	.60	.01	.05	<2	<.2	215	<.3	<.2	2.8	72
L13+00N 5+75E	8.5	15.4	15.3	51.8	183	13	5	245	1.83	21.8	<5	<2	16	.18	5.5	.2	31	.06	.029	11	13	.17	84	.01	<3	.80	.01	.03	<2	<.2	215	<.3	.2	2.9	4
L13+00N 6+00E	8.6	13.1	14.3	45.3	142	12	4	206	1.58	18.3	<5	<2	16	.24	6.1	.2	26	.07	.024	10	14	.18	99	.02	<3	.64	.01	.03	<2	<.2	128	<.3	<.2	3.1	7
L13+00N 6+25E	11.3	15.2	13.3	45.0	184	11	4	257	1.63	19.6	<5	<2	16	.19	6.4	.3	25	.05	.045	8	14	.16	93	.01	<3	.75	.01	.05	<2	<.2	176	<.3	<.2	3.2	14
L13+00N 6+50E	8.3	13.5	11.4	45.3	179	10	5	279	1.37	20.1	8	2	11	.24	5.4	.2	19	.07	.040	9	13	.17	44	.01	<3	.57	.01	.04	<2	<.2	141	<.3	<.2	2.1	12
L13+00N 6+75E	9.2	14.2	15.0	54.2	164	11	6	355	1.56	17.4	<5	2	17	.28	7.1	.2	20	.08	.036	9	10	.18	142	.01	<3	.49	.01	.04	<2	<.2	200	<.3	<.2	2.2	10
L13+00N 7+00E	7.2	15.3	13.3	58.0	300	13	5	280	1.86	21.3	<5	2	24	.43	6.4	.3	26	.09	.028	12	16	.24	139	.01	<3	.73	.01	.07	<2	<.2	189	<.3	.2	2.4	73
L13+00N 7+25E	11.2	18.2	24.1	49.1	263	10	5	392	1.78	36.3	<5	<2	20	.15	7.8	.6	26	.06	.089	12	15	.22	133	.01	<3	1.15	.01	.08	<2	<.2	150	<.3	.2	4.4	7
L13+00N 7+50E	7.5	13.3	14.8	43.2	147	10	5	327	1.60	22.6	<5	<2	15	.15	6.5	.3	22	.09	.042	11	11	.16	90	.01	<3	.60	.01	.06	<2	.2	87	<.3	.2	2.9	9
STANDARD D2/C3/AU-S	24.5	121.4	102.3	263.8	1958	31	17	1044	4.50	72.3	26	20	57	1.91	8.4	17.3	69	.70	.107	16	56	1.10	262	.10	31	2.31	.04	.68	14	2.6	1083	.3	2.1	7.5	52

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data / FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L13+00N 7+75E	4.9	11.1	10.1	31.0	150	9	4	207	1.36	16.7	10	3	9	.15	6.4	<.2	19	.08	.027	10	8	.13	47	.02	<3	.62	.01	.04	<2	<.2	132	<.3	<.2	1.9	3
L13+00N 8+00E	10.2	16.6	36.8	48.0	235	10	4	228	1.58	22.6	<5	5	20	.26	8.0	.4	23	.15	.050	15	12	.22	203	.03	<3	.67	.01	.10	<2	<.2	254	.3	.2	2.3	7
L13+00N 8+25E	58.1	5.2	73.8	18.3	1588	1	1	40	1.54	38.2	<5	3	12	.04	17.2	1.4	4	.01	.027	13	1	.01	294	<.01	<3	.14	.01	.28	<2	.2	620	1.9	.8	1.4	11
98BEKMS-01	4.6	3.4	146.2	91.0	105	1	3	1753	2.41	25.0	<5	16	16	.54	2.8	<.2	1	.21	.007	36	1	.03	1377	<.01	<3	.42	<.01	.25	<2	.2	353	<.3	<.2	1.2	2
98BEKMS-02	5.2	61.7	49.3	61.0	231	2	6	1432	1.48	3.7	<5	7	20	.56	2.7	<.2	10	2.59	.024	35	<1	.06	344	<.01	<3	.32	<.01	.24	<2	<.2	75	<.3	<.2	1.0	1
98BEKMS-03	7.2	10.0	38.6	14.3	427	1	2	94	5.77	14.9	<5	5	59	.08	.8	.9	10	.01	.099	43	4	.02	204	<.01	<3	.61	.01	.15	<2	.2	35	1.9	.8	2.9	32
RE 98BEKMS-03	7.5	13.1	41.8	10.7	404	<1	2	96	5.35	14.4	<5	5	57	.05	.8	.9	11	.01	.099	42	2	.02	217	<.01	<3	.57	.01	.15	<2	.2	33	2.3	.8	3.2	19

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data / FA ____

ACME A[illegible]YTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(6[illegible]253-1716
(I[illegible]9002 Accredited Co.)

SINTER GRID

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Omni Resources PROJECT SKUKUM CK. File # 9802927 Page 1

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Terry Elliott

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm
L13+50N 8+25E	10.9	19.5	47.6	97.2	428	12	4	528	1.92	16.2	<5	3	17	.28	4.4
L13+50N 8+50E	11.7	18.0	45.9	68.3	336	12	4	390	1.95	19.9	<5	2	21	.29	5.6
L13+50N 8+75E	30.0	22.6	63.0	69.9	404	9	3	277	1.76	30.7	<5	4	9	.14	4.7
L13+50N 9+00E	11.3	127.6	137.5	165.7	589	14	15	1558	3.79	23.6	<5	6	9	.44	7.6
L13+50N 9+25E	11.1	85.1	196.5	105.2	746	4	3	193	2.91	74.2	<5	3	27	.12	11.2
L13+50N 9+50E	9.5	21.0	60.2	93.2	246	9	9	3391	2.55	13.2	<5	3	16	.93	3.1
L13+50N 9+75E	2.7	3.3	34.7	123.9	220	6	7	778	4.37	7.1	<5	7	9	.26	27.4
L13+50N 10+00E	8.8	53.0	87.3	135.8	657	6	6	810	3.06	11.6	<5	8	14	.46	8.0
L13+50N 10+25E	3.5	15.8	71.4	90.0	310	2	2	450	1.13	3.6	<5	6	8	.21	8.2
L13+50N 10+50E	4.3	11.5	76.2	137.6	259	6	4	2171	1.87	8.2	<5	9	12	1.85	4.0
L13+50N 10+75E	17.9	39.9	97.6	266.3	626	18	14	3124	3.60	14.6	<5	5	15	.97	8.4
L13+50N 11+00E	20.5	22.4	82.6	210.7	760	8	7	1637	2.34	10.0	5	5	9	1.31	6.5
L13+00N 8+50E	297.2	10.9	176.7	8.7	943	1	2	42	13.87	173.9	<5	24	15	.35	7.6
L13+00N 8+75E	10.2	37.0	104.7	306.2	772	21	15	2647	3.84	26.6	<5	4	26	1.17	6.0
L13+00N 9+00E	12.1	14.1	54.2	96.3	346	7	6	1253	2.05	19.9	<5	3	18	.59	3.4
L13+00N 9+25E	4.7	11.9	53.4	114.6	367	13	5	1239	2.02	8.6	6	7	15	.22	2.1
L13+00N 9+50E	10.5	45.2	135.6	173.3	398	10	10	970	3.80	23.3	5	3	29	.47	5.4
L13+00N 9+75E	8.5	55.1	118.5	143.4	304	9	10	1604	2.52	46.4	<5	3	11	.41	7.5
RE L13+00N 9+75E	8.7	51.2	111.6	134.1	341	9	10	1625	2.44	44.5	<5	4	11	.42	7.5
L13+00N 10+00E	5.5	58.8	106.1	158.8	771	13	10	1329	2.75	16.7	<5	3	23	.48	15.7
L13+00N 10+25E	7.2	30.3	80.5	138.7	558	6	6	1470	2.25	16.6	<5	6	13	.71	13.4
L13+00N 10+50E	8.9	25.9	112.9	171.8	664	11	8	1946	2.59	17.5	<5	8	18	.87	8.3
L13+00N 10+75E	6.8	25.5	103.4	124.7	176	7	7	1390	2.33	21.9	<5	<2	24	.63	9.1
L13+00N 11+00E	6.0	25.9	81.9	98.5	659	8	6	1154	1.97	17.2	<5	5	20	.54	8.2
L12+50N 5+00E	15.0	29.9	20.7	78.0	242	17	9	511	2.65	30.4	<5	2	13	.21	14.5
L12+50N 5+25E	23.8	21.1	20.6	57.9	230	17	7	356	1.96	111.2	<5	<2	18	.28	9.4
L12+50N 5+50E	72.2	43.8	66.1	103.1	1395	22	11	882	3.29	73.9	<5	2	67	.37	14.7
L12+50N 5+75E	14.7	18.6	21.0	76.7	284	16	7	313	2.17	40.0	<5	<2	23	.34	9.0
L12+50N 6+00E	9.9	14.4	17.3	54.4	147	11	5	192	1.90	30.0	<5	<2	12	.17	8.1
L12+50N 6+25E	11.0	16.6	17.1	58.5	101	11	5	226	1.94	34.4	<5	<2	13	.20	8.5
L12+50N 6+50E	12.0	17.7	17.4	57.7	138	11	5	217	1.94	28.9	<5	<2	12	.26	9.1
L12+50N 6+75E	10.1	13.2	19.4	53.3	506	11	5	254	1.96	33.3	<5	4	15	.19	7.9
L12+50N 7+00E	8.2	13.2	9.3	25.1	45	5	2	99	1.06	17.9	<5	<2	9	.08	15.7
L12+50N 7+25E	9.0	14.7	19.6	48.4	235	12	5	258	1.75	26.7	<5	3	10	.15	8.2
STANDARD D2/C3/AU-S	24.2	119.2	104.2	262.1	1704	30	17	1030	4.50	70.5	18	22	53	1.82	8.9

SAMPLE#	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L13+50N 8+25E	.3	16	.07	.063	20	5	.05	165	<.01	<3	.74	.01	.11	<2	.2	94	.3	<.2	2.1	3
L13+50N 8+50E	.3	19	.05	.111	22	6	.12	301	<.01	<3	1.18	.01	.09	<2	.3	82	.4	<.2	3.0	8
L13+50N 8+75E	.3	10	.04	.036	11	4	.03	74	<.01	<3	.67	.01	.08	<2	.3	79	<.3	<.2	1.8	9
L13+50N 9+00E	<.2	10	.05	.059	24	1	.04	463	<.01	<3	1.18	.01	.13	<2	.2	80	.7	.2	1.6	6
L13+50N 9+25E	.2	15	.03	.062	26	<1	.03	115	<.01	<3	.51	.02	.18	<2	<.2	59	.4	.3	1.5	8
L13+50N 9+50E	.3	27	.07	.062	17	8	.10	376	.01	<3	1.33	.01	.12	<2	.2	63	.3	<.2	3.2	2
L13+50N 9+75E	<.2	56	.20	.077	22	4	.05	313	<.01	<3	.87	.01	.11	2	.2	50	<.3	<.2	1.7	3
L13+50N 10+00E	.3	21	.11	.075	25	4	.10	559	<.01	<3	.98	.01	.15	<2	<.2	54	<.3	.2	1.8	2
L13+50N 10+25E	.5	10	.13	.042	18	<1	.02	517	<.01	<3	.63	<.01	.11	<2	.2	41	<.3	<.2	1.1	3
L13+50N 10+50E	.3	13	.11	.048	61	8	.14	294	.01	<3	.85	.01	.12	<2	<.2	77	<.3	<.2	2.1	7
L13+50N 10+75E	.3	30	.19	.035	59	15	.14	719	<.01	<3	.78	.01	.15	<2	.2	114	<.3	<.2	2.1	8
L13+50N 11+00E	.5	21	.08	.047	18	9	.16	281	<.01	<3	1.08	.01	.10	<2	.2	78	<.3	<.2	2.2	11
L13+00N 8+50E	<1.2	11	<.01	.108	56	<1	<.01	635	<.01	5	.43	.01	.14	<2	<1.2	367	<1.8	<1.2	7.1	20
L13+00N 8+75E	.2	36	.25	.058	70	6	.05	694	<.01	<3	.89	.01	.18	<2	<.2	129	.4	<.2	1.5	12
L13+00N 9+00E	.3	19	.18	.064	21	7	.11	345	<.01	<3	.83	.01	.13	<2	.2	47	<.3	.2	2.6	14
L13+00N 9+25E	.3	12	.12	.030	44	5	.12	140	.01	<3	.65	.01	.17	<2	<.2	71	<.3	<.2	1.8	9
L13+00N 9+50E	.5	29	.12	.086	20	8	.24	526	<.01	<3	1.06	.02	.16	<2	<.2	29	.4	.4	2.8	5
L13+00N 9+75E	.3	13	.09	.048	75	2	.07	547	<.01	<3	.71	.01	.11	<2	<.2	104	.4	<.2	1.3	14
RE L13+00N 9+75E	.3	14	.08	.045	74	2	.07	539	<.01	<3	.70	.01	.11	<2	.2	96	.4	<.2	1.5	11
L13+00N 10+00E	.5	31	.24	.066	46	10	.22	581	.01	<3	.88	.01	.16	<2	<.2	73	<.3	<.2	2.0	8
L13+00N 10+25E	.4	19	.13	.052	42	7	.14	340	<.01	<3	.63	.01	.15	<2	<.2	104	<.3	<.2	1.9	29
L13+00N 10+50E	.5	23	.20	.051	83	7	.16	628	.01	<3	.82	.01	.16	<2	<.2	79	<.3	<.2	2.1	113
L13+00N 10+75E	.4	24	.19	.090	26	6	.21	326	.01	<3	.84	.01	.19	<2	.2	193	<.3	<.2	2.4	11
L13+00N 11+00E	.5	22	.22	.036	33	8	.16	724	.01	<3	.65	.01	.13	<2	.2	240	<.3	<.2	1.7	26
L12+50N 5+00E	.3	31	.09	.050	13	14	.32	146	.01	<3	.80	.01	.03	<2	<.2	314	<.3	<.2	2.4	4
L12+50N 5+25E	.3	25	.07	.046	8	12	.17	173	.01	<3	.71	.01	.05	<2	.2	313	<.3	.2	2.4	4
L12+50N 5+50E	.8	33	.22	.164	17	18	.19	1163	<.01	<3	1.53	.01	.15	<2	.3	1025	<.3	.4	3.6	16
L12+50N 5+75E	.3	31	.08	.038	10	11	.25	175	.01	<3	.75	.01	.06	<2	<.2	221	<.3	.2	2.7	6
L12+50N 6+00E	.2	28	.04	.028	10	9	.16	68	.01	<3	.66	.01	.03	<2	<.2	163	<.3	<.2	2.5	3
L12+50N 6+25E	.2	31	.05	.036	10	6	.13	111	.01	<3	.61	.01	.04	<2	<.2	146	<.3	<.2	2.8	3
L12+50N 6+50E	.3	28	.04	.041	10	11	.15	61	.01	<3	.62	.01	.04	<2	<.2	166	<.3	<.2	2.4	28
L12+50N 6+75E	.3	25	.06	.020	12	13	.14	78	.01	<3	.73	.01	.05	<2	<.2	108	<.3	<.2	2.4	3
L12+50N 7+00E	.2	14	.03	.030	4	6	.02	68	<.01	<3	.23	<.01	.03	<2	<.2	128	.6	.2	1.6	<1
L12+50N 7+25E	.2	27	.04	.035	8	14	.20	69	.01	<3	1.16	.01	.05	<2	<.2	96	.4	.2	3.3	2
STANDARD D2/C3/AU-S	19.2	73	.69	.105	18	56	1.12	269	.13	34	2.44	.05	.70	14	2.2	904	.5	1.6	5.8	50

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 20 1998 **DATE REPORT MAILED:** July 28/98 **SIGNED BY** C.L.......D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L12+50N 7+50N	7.0	9.9	13.6	24.4	121	7	3	118	1.39	21.6	<5	<2	8	.13	6.0	.2	25	.03	.018	7	11	.10	40	.02	<3	.60	.01	.03	<2	<.2	81	<.3	.2	2.7	2
L12+50N 7+75E	2.2	2.9	31.6	24.0	97	4	3	391	.55	5.9	<5	6	4	.21	.9	<.2	2	.03	.008	27	1	.02	111	<.01	<3	.20	<.01	.11	<2	<.2	31	<.3	<.2	.6	<1
L12+50N 8+00E	9.0	7.7	65.6	103.0	355	22	5	1083	1.89	8.6	<5	<2	8	.37	2.0	.2	9	.05	.044	39	2	.10	253	<.01	<3	.85	.01	.14	<2	<.2	73	<.3	<.2	2.0	7
L12+50N 8+25E	4.7	5.2	25.9	58.2	125	11	3	867	1.07	9.8	<5	6	9	.46	1.5	<.2	5	.09	.021	81	<1	.06	572	<.01	<3	.45	.01	.17	<2	<.2	69	<.3	<.2	1.3	10
L12+50N 8+50E	11.7	13.2	93.9	94.0	957	20	8	1035	2.13	17.3	<5	8	12	.48	3.7	.4	22	.08	.032	41	13	.18	139	.01	<3	.88	.01	.11	<2	.2	138	<.3	<.2	2.3	338
L12+50N 8+75E	12.8	16.1	84.6	82.1	813	13	9	943	2.18	23.0	<5	7	15	.46	3.6	.4	20	.05	.040	31	9	.17	108	.01	<3	1.06	.01	.12	<2	.2	112	<.3	<.2	2.7	121
L12+50N 9+00E	32.1	11.2	60.7	79.7	518	8	4	332	2.28	61.9	<5	6	14	.17	4.8	.4	9	.05	.039	38	5	.06	137	<.01	3	.37	.02	.19	<2	.2	92	.5	.4	1.4	72
L12+50N 9+25E	17.9	20.5	68.1	65.7	873	7	5	403	2.15	46.9	<5	<2	17	.22	4.8	.5	17	.09	.068	35	5	.12	164	.01	<3	.73	.02	.17	<2	.2	68	.6	.3	2.1	29
L12+50N 9+50E	9.4	20.2	57.5	156.6	374	9	6	1100	2.08	22.4	<5	<2	22	3.25	4.5	.4	20	.21	.086	17	6	.09	300	.01	3	.55	.01	.16	<2	<.2	45	<.3	.2	2.6	7
L12+50N 9+75E	8.5	21.2	86.1	102.9	578	8	7	1333	2.20	27.8	<5	8	45	.92	6.0	.4	12	.30	.059	57	4	.08	506	<.01	<3	.52	.01	.25	<2	.2	102	.3	.2	1.7	7
L12+50N 10+00E	5.7	32.4	90.3	120.4	504	10	9	2151	2.56	17.8	<5	3	31	1.29	4.8	.4	19	.41	.095	42	4	.15	1311	<.01	<3	.79	.01	.18	<2	<.2	106	<.3	<.2	2.2	57
L12+50N 10+25E	5.2	36.3	89.1	105.5	378	10	9	1930	2.53	15.8	<5	3	41	1.17	5.3	.3	20	.75	.090	30	7	.15	930	<.01	<3	.95	.01	.20	<2	.2	51	<.3	<.2	2.7	6
L12+50N 10+50E	4.1	57.0	75.3	166.3	623	7	9	1638	3.18	24.9	<5	2	77	1.52	27.3	.5	35	2.30	.162	32	6	.24	775	.01	4	.87	.01	.30	<2	<.2	135	<.3	<.2	2.3	2
RE L12+50N 10+50E	4.0	55.0	77.1	167.7	602	7	9	1659	3.22	25.7	<5	2	78	1.45	27.0	.4	36	2.32	.163	32	7	.24	779	.01	4	.87	.01	.31	<2	<.2	178	<.3	<.2	2.4	4
L12+50N 10+75E	3.8	64.2	124.4	135.3	697	5	8	1645	3.26	17.5	<5	4	39	1.08	14.5	.5	45	.83	.136	34	4	.38	702	.01	<3	1.24	.01	.24	<2	.2	119	<.3	<.2	3.7	3
L12+50N 11+00E	3.2	39.0	194.6	147.9	760	7	8	1488	2.76	18.6	<5	4	30	.86	11.7	.9	38	.50	.083	61	5	.42	512	.01	<3	1.19	.01	.27	<2	<.2	93	<.3	<.2	3.2	6
L12+00N 5+00E	3.9	15.2	20.1	38.7	150	18	7	238	2.24	21.6	<5	<2	19	.26	2.8	<.2	44	.18	.104	12	26	.32	85	.02	<3	1.48	.01	.12	<2	<.2	149	<.3	<.2	4.3	6
L12+00N 5+25E N.S.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
L12+00N 5+50E	96.0	23.4	49.6	72.4	655	38	13	400	3.79	354.1	<5	<2	53	.36	38.7	1.4	29	.07	.075	9	24	.16	160	.02	<3	.72	.01	.14	<2	.6	435	<.3	.4	3.5	12
L12+00N 5+75E	42.9	22.2	36.5	77.8	646	30	11	750	2.93	263.3	<5	<2	49	.64	20.3	.7	36	.09	.079	10	22	.21	244	.02	<3	1.05	.01	.14	<2	.6	813	<.3	.2	4.0	7
L12+00N 6+00E	26.3	20.6	27.1	49.7	529	25	10	280	2.44	102.6	<5	2	23	.38	8.8	.6	32	.09	.031	11	21	.31	148	.02	<3	1.22	.01	.08	<2	.3	487	<.3	.2	3.6	12
L12+00N 6+25E	39.8	16.2	33.5	74.7	255	24	8	609	2.25	70.1	<5	<2	22	.29	7.3	.5	18	.07	.075	14	11	.10	444	<.01	4	.98	.01	.13	<2	.4	421	<.3	.2	3.3	5
L12+00N 6+50E	30.4	23.2	46.6	59.6	519	18	4	257	1.87	63.8	<5	<2	54	.15	8.2	.6	17	.13	.067	9	12	.09	721	<.01	<3	.96	.01	.15	<2	.3	615	<.3	.3	2.9	8
L12+00N 6+75E	10.6	19.0	39.7	72.5	362	18	5	210	2.21	45.6	<5	<2	21	.21	6.5	.6	27	.05	.050	12	9	.10	146	<.01	<3	.81	.01	.09	<2	<.2	250	<.3	<.2	2.7	4
L12+00N 7+00E	15.5	20.7	24.9	52.5	430	10	4	452	1.84	51.0	6	<2	18	.34	13.9	1.3	20	.08	.081	9	13	.17	90	.01	3	.79	.01	.12	<2	.2	159	<.3	.3	2.9	15
L12+00N 7+25E	11.8	10.8	17.6	10.5	210	4	1	114	.94	41.6	9	<2	7	.01	14.4	.4	7	.01	.020	3	11	.04	44	<.01	3	.28	.01	.07	<2	<.2	182	.8	.4	1.5	8
L12+00N 7+50E	13.6	10.8	16.5	11.6	198	4	1	108	.83	25.4	5	<2	12	.01	16.4	.2	8	.04	.018	4	10	.04	132	<.01	<3	.31	.01	.08	<2	<.2	108	.6	.3	1.3	3
L12+00N 7+75E	6.7	6.5	39.6	41.3	194	6	3	451	.95	9.1	<5	8	5	.76	1.9	<.2	2	.04	.014	39	1	.04	106	<.01	<3	.36	.01	.17	<2	<.2	54	<.3	<.2	.7	6
L12+00N 8+00E N.S.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
L12+00N 8+25E N.S.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
L12+00N 8+50E	9.1	12.6	150.2	168.2	235	69	11	2981	3.55	25.9	<5	12	16	.58	4.5	.2	17	.12	.038	89	9	.15	1008	.01	<3	.73	.01	.12	<2	<.2	171	<.3	<.2	2.0	11
L12+00N 8+75E N.S.	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
L12+00N 9+00E	22.1	14.8	112.8	72.2	560	21	7	843	1.74	20.2	<5	10	15	.24	5.4	.3	14	.10	.027	60	9	.13	135	.01	<3	.62	.01	.16	<2	.2	140	<.3	<.2	1.7	58
L12+00N 9+25E	14.3	18.7	78.6	60.7	599	13	10	1303	1.40	22.5	<5	4	17	.83	6.5	.3	11	.11	.042	36	7	.11	151	<.01	<3	.59	.01	.15	<2	.2	80	<.3	.2	1.9	12
STANDARD D2/C3/AU-S	20.1	114.2	98.3	263.6	1948	33	17	1031	4.53	69.8	11	21	65	1.93	8.7	19.1	73	.67	.105	18	58	1.10	255	.15	28	2.37	.05	.69	14	2.0	978	.4	1.6	6.5	55

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Data FA

ACME ANALYTICAL

Omni Resources PROJECT SKUKUM CK. FILE # 9802927

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L12+00N 9+50E	10.3	20.8	40.6	65.5	495	8	5	718	1.25	16.8	<5	2	19	1.73	4.4	<.2	9	.17	.054	34	6	.09	144	<.01	<3	.59	.01	.17	<2	<.2	56	<.3	.2	1.4	6
L12+00N 9+75E	18.8	37.3	86.2	106.5	279	15	11	783	2.90	53.7	5	5	24	.41	7.8	.3	23	.05	.065	26	10	.20	149	.01	<3	1.01	.02	.14	<2	.2	212	.9	.5	2.3	8
L12+00N 10+00E	9.4	27.5	80.3	123.6	367	11	9	1270	2.60	45.2	<5	<2	27	.95	8.0	.3	25	.17	.087	20	11	.23	362	.01	<3	.88	.02	.16	<2	<.2	248	.5	.3	2.5	4
L12+00N 10+25E	10.5	28.5	75.8	154.9	563	14	9	1546	2.77	37.7	5	5	50	1.48	6.4	.3	14	.45	.084	38	5	.13	677	<.01	<3	.73	.01	.25	<2	<.2	141	.6	.2	1.7	9
L12+00N 10+50E	5.5	26.4	65.2	162.5	1305	11	7	2606	1.89	37.0	<5	3	42	3.56	9.7	.2	16	.72	.102	53	7	.20	755	.01	<3	.83	.01	.22	<2	.2	322	<.3	<.2	2.5	3
L12+00N 10+75E	6.9	57.1	86.6	174.0	413	8	8	1683	2.72	29.8	<5	3	41	1.92	11.1	.3	24	.70	.116	23	3	.19	466	.01	<3	.87	.01	.27	<2	<.2	110	.4	.2	2.9	2
L12+00N 11+00E	4.3	42.6	212.6	202.1	1033	9	12	2306	3.33	15.3	<5	4	50	2.31	8.9	.4	34	1.07	.124	54	5	.24	980	<.01	<3	.90	.01	.27	<2	<.2	252	.6	<.2	2.3	10
STANDARD D2/C3	23.0	123.0	96.3	258.6	1980	31	16	1015	4.44	62.3	16	20	59	2.07	9.1	19.3	73	.74	.104	18	58	1.10	250	.16	24	2.36	.05	.69	13	2.3	<10	.4	1.9	6.5	48

Standard is STANDARD D2/C3/AU-S.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME AN[illegible]TICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(IS[illegible]002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

SINTER GRID

Omni Resources PROJECT SINTER CAP-CARBON HILL File # 9803019 Page 1

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L11+50N 5+00E	109.7	20.1	176.5	28.1	330	7	4	79	2.85	218.7	<5	4	39	.05	30.0	2.5	16	.02	.056	6	31	.06	236	<.01	<3	.51	<.01	.12	<2	<1	325	<1.5	<1	<2.5	29
L11+50N 5+50E	14.3	13.8	37.6	65.8	237	31	8	689	3.02	99.6	<5	7	100	.66	5.2	1.0	7	.19	.072	27	21	.03	593	<.01	<3	.52	.01	.39	<2	.6	368	.3	.3	1.6	2
L11+50N 5+75E	29.9	14.5	43.5	54.4	292	12	6	605	2.24	86.9	<5	<2	42	.42	9.0	1.0	22	.07	.079	9	18	.15	300	.01	3	.74	.01	.18	<2	.7	468	.9	.5	3.2	3
L11+50N 6+00E	20.9	13.1	22.5	43.6	297	14	6	305	2.09	72.3	<5	3	16	.23	7.4	.5	28	.07	.039	11	16	.20	123	.01	<3	.91	.01	.10	<2	.7	163	.5	.2	3.2	4
L11+50N 6+25E	25.7	7.2	62.9	17.4	191	4	2	128	.79	39.9	<5	7	8	.08	4.4	.3	9	.03	.022	16	8	.05	139	<.01	<3	.43	<.01	.20	<2	.6	74	<.3	<.2	2.4	2
L11+50N 6+50E	20.4	7.4	57.3	3.6	297	1	1	24	2.97	145.8	<5	18	25	.01	4.5	.4	5	.04	.043	30	15	.01	311	<.01	<3	.40	<.01	.64	<2	1.2	444	.3	<.2	3.6	<1
L11+50N 6+75E	20.7	10.7	50.0	9.1	203	2	1	50	1.21	63.1	<5	7	20	.02	6.5	.4	6	.02	.015	13	12	.02	332	<.01	<3	.41	<.01	.23	<2	.5	91	.4	.3	2.9	3
L11+50N 7+00E	26.5	17.9	60.8	48.3	317	13	7	1210	2.01	245.3	<5	<2	27	.19	12.4	.8	19	.03	.072	14	10	.03	261	<.01	<3	.54	.01	.19	<2	.8	215	.3	.4	2.9	3
L11+50N 7+25E	16.8	22.2	38.0	58.3	296	14	7	571	2.01	142.6	<5	3	19	.16	11.4	.6	22	.04	.070	12	9	.19	119	<.01	<3	.81	.01	.15	<2	.3	1708	.7	.3	3.1	1
L11+50N 7+50E	14.0	18.7	67.6	132.8	598	19	11	1760	1.71	51.3	<5	5	29	1.33	8.1	.4	16	.32	.070	25	6	.15	861	<.01	<3	.75	.01	.20	<2	.3	86	<.3	.2	2.8	7
L11+50N 8+25E	21.9	28.7	98.2	97.5	316	26	15	1404	2.68	67.4	<5	5	29	.48	6.4	.5	17	.11	.046	45	9	.15	307	.01	<3	.61	.02	.14	<2	.3	130	.4	.3	2.0	7
RE L11+50N 8+25E	22.1	30.1	96.7	101.0	342	26	15	1427	2.75	63.6	<5	5	29	.48	7.0	.6	18	.11	.047	46	6	.15	309	.01	<3	.63	.02	.15	<2	.2	104	.4	.4	2.0	10
L11+50N 8+50E	17.1	21.3	84.0	104.2	415	47	18	2280	2.56	47.1	<5	8	26	.77	6.5	.4	15	.14	.037	66	10	.13	447	.01	<3	.67	.01	.14	<2	<.2	82	.3	.3	2.2	6
L11+50N 8+75E	8.8	48.8	41.9	143.8	334	66	24	1384	3.79	54.5	<5	6	61	.34	4.2	.3	26	.14	.067	40	11	.06	417	<.01	<3	.70	.02	.21	<2	.2	68	<.3	<.2	1.5	4
L11+50N 9+00E	19.0	18.6	55.8	75.7	410	16	8	600	2.55	47.9	<5	6	44	.15	5.1	1.0	12	.07	.046	32	9	.05	259	<.01	<3	.34	.01	.26	<2	<.2	97	1.2	.8	1.5	6
L11+50N 9+25E	11.2	33.9	52.5	98.5	315	19	10	768	2.51	40.9	<5	7	20	.38	5.9	.4	16	.05	.058	22	7	.11	152	<.01	<3	.61	.01	.13	<2	<.2	101	.4	.4	2.0	4
L11+50N 9+50E	12.7	29.7	65.3	104.7	635	14	10	1006	2.53	40.5	<5	5	22	.34	6.9	.5	20	.08	.067	21	7	.19	211	<.01	<3	.91	.02	.15	<2	.2	121	<.3	.4	2.9	6
L11+50N 10+00E	13.0	29.0	64.1	133.0	345	25	12	1457	2.79	55.8	<5	5	21	.85	9.3	.4	24	.06	.071	23	8	.22	236	.01	<3	1.17	.02	.14	<2	<.2	188	.3	.3	2.8	9
L11+50N 10+25E	12.8	28.7	61.7	101.1	390	16	10	959	2.49	73.3	<5	6	20	.57	16.2	.5	25	.08	.051	21	10	.24	207	.01	<3	.99	.01	.12	<2	<.2	305	.3	.4	2.9	27
L11+50N 10+50E	8.2	32.5	67.6	109.1	210	15	10	823	2.77	62.0	<5	7	21	.54	20.2	.5	28	.17	.069	21	9	.28	147	.01	<3	.83	.01	.13	<2	<.2	340	<.3	.3	2.3	10
L11+50N 10+75E	9.6	33.1	82.7	152.0	359	14	11	1580	2.76	57.5	<5	4	27	1.05	18.5	.5	29	.23	.092	25	12	.32	427	.01	<3	1.03	.01	.16	<2	<.2	389	<.3	.2	3.5	5
L11+50N 11+00E	7.6	47.3	72.2	131.2	557	13	10	1827	2.54	36.1	<5	5	26	1.41	10.3	.5	24	.41	.098	42	9	.23	672	.01	<3	.84	.01	.23	<2	<.2	104	<.3	.2	2.8	10
L11+00N 5+00E	30.4	20.3	87.6	49.5	814	12	6	261	3.31	965.1	8	4	47	.30	545.1	1.9	22	.04	.063	8	15	.12	428	<.01	3	.71	.01	.27	<2	2.0	1175	1.8	.6	3.1	17
L11+00N 5+25E	58.6	41.3	62.6	54.6	403	21	8	171	6.94	289.6	<5	6	48	.10	34.0	1.6	31	.02	.101	13	28	.05	256	<.01	3	.60	.01	.26	<2	.5	1039	3.0	1.9	3.9	9
L11+00N 5+50E	18.4	16.3	29.4	92.7	312	24	10	953	3.33	46.0	<5	5	48	.33	8.4	.5	14	.16	.062	22	8	.08	424	<.01	<3	.57	.02	.21	<2	<.2	247	.3	.3	1.5	6
L11+00N 5+75E	24.3	13.0	42.7	50.2	385	12	5	194	3.44	95.6	<5	6	84	.05	12.9	1.4	14	.02	.056	11	16	.04	409	<.01	<3	.35	.01	.33	<2	.4	4431	2.8	1.0	2.4	7
L11+00N 6+00E	42.6	18.5	56.1	48.6	537	16	6	274	2.39	298.7	<5	6	58	.14	13.1	1.1	14	.07	.053	22	10	.06	463	<.01	<3	.41	.01	.32	<2	.7	420	1.0	.7	2.1	4
L11+00N 6+25E	13.7	54.8	57.6	113.5	469	32	15	1369	3.46	1431.8	<5	4	102	.19	22.2	<1	15	.21	.076	20	2	.04	641	<.01	<3	.37	.02	.28	<2	<1	1564	<1.5	<1	<2.5	9
L11+00N 6+75E	25.9	26.9	42.3	112.9	268	18	7	810	1.84	143.3	<5	7	28	.64	11.4	.3	13	.13	.041	22	6	.10	303	<.01	<3	.53	.01	.19	<2	.2	188	<.3	.2	1.5	8
L11+00N 7+00E	12.9	17.4	51.3	40.0	245	11	3	124	2.29	141.0	9	9	34	.02	7.3	.3	11	.02	.027	17	10	.02	299	<.01	<3	.51	.01	.24	<2	.3	1207	.4	.2	2.5	7
L11+00N 7+25E	10.4	8.9	23.6	25.9	213	12	3	149	1.46	102.0	5	3	11	.01	7.5	.4	7	.02	.018	9	5	.02	127	<.01	<3	.20	.01	.16	<2	<.2	441	.8	.4	1.2	3
L11+00N 7+50E	22.6	38.4	66.5	152.8	1008	27	11	600	3.42	141.8	6	3	36	.26	23.3	1.0	32	.15	.112	18	14	.23	299	<.01	<3	1.02	.01	.22	<2	<.2	123	<.3	.4	3.0	10
L11+00N 7+75E	20.9	48.9	61.7	115.2	386	33	17	903	3.92	146.9	7	4	35	.23	20.4	.5	40	.05	.091	22	15	.32	255	<.01	<3	1.38	.02	.19	<2	.2	94	.4	.6	3.8	6
L11+00N 8+00E	12.9	35.7	27.5	89.2	271	25	14	943	2.87	113.3	<5	2	28	.20	15.0	.3	37	.09	.090	13	8	.26	211	.01	<3	1.05	.01	.16	<2	<.2	203	<.3	.3	3.4	7
STANDARD D2/C3/AU-S	25.0	124.2	104.0	271.6	1795	32	17	1042	4.60	72.0	21	23	61	1.82	9.0	17.6	76	.71	.110	19	59	1.14	249	.16	29	2.47	.05	.71	14	2.7	912	.4	2.2	7.2	44

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 23 1998 **DATE REPORT MAILED:** Aug 6/98 **SIGNED BY**....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data FA

ACME ANALYTICAL

Omni Resources PROJECT SINTER CAP-CARBON HILL FILE # 9803019

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L11+00N 8+25E	10.7	38.4	78.5	141.1	772	20	15	1415	3.48	95.9	<5	4	34	.52	11.0	.4	32	.10	.110	24	12	.34	561	.01	<3	1.19	.02	.15	<2	<.2	249	.4	.3	3.3	3
L11+00N 8+50E	23.9	47.1	121.1	154.2	741	27	15	895	4.15	484.7	<5	5	48	.69	13.5	.7	26	.08	.078	30	7	.24	301	<.01	<3	.84	.03	.20	<2	.3	401	.8	.8	3.2	16
L11+00N 8+75E	21.2	27.6	63.2	109.4	534	22	11	997	2.41	98.7	<5	9	24	.61	6.8	.3	16	.14	.054	23	9	.17	297	<.01	<3	.66	.01	.15	<2	<.2	72	<.3	<.2	1.9	8
L11+00N 9+00E	12.6	36.0	65.4	137.1	872	29	13	1083	3.10	94.2	<5	4	72	3.24	8.9	.5	19	.60	.089	99	11	.19	949	<.01	<3	.77	.02	.23	<2	<.2	95	<.3	.7	3.4	6
L11+00N 9+25E	12.5	29.7	59.2	119.6	611	28	11	781	2.86	57.1	5	8	20	.49	6.2	.4	14	.13	.044	44	9	.17	274	<.01	<3	.70	.01	.19	<2	.2	87	.3	.2	2.3	22
L11+00N 9+75E	11.9	30.2	76.8	98.3	474	19	16	2676	2.73	79.2	<5	5	24	.61	8.3	.4	27	.07	.059	31	10	.18	280	.01	<3	1.09	.02	.13	<2	<.2	300	<.3	<.2	2.6	14
L11+00N 10+00E	9.4	27.4	55.4	98.8	611	20	10	1184	2.44	71.0	6	3	37	.63	9.7	.4	23	.17	.083	19	12	.22	556	.01	<3	1.00	.02	.13	<2	<.2	241	.3	.3	2.7	20
L11+00N 10+25E	9.6	31.7	43.4	104.5	231	24	10	732	2.54	70.5	5	5	28	.42	10.3	.4	25	.17	.050	29	13	.27	272	.01	<3	.83	.01	.15	<2	<.2	124	<.3	.2	2.3	7
L11+00N 10+50E	10.8	40.0	93.6	123.0	400	20	12	951	3.22	78.0	<5	3	27	.55	17.8	.5	37	.13	.070	21	14	.40	236	.01	<3	1.24	.01	.12	<2	<.2	305	.3	.2	3.9	13
L11+00N 10+75E	20.2	35.4	71.6	117.9	516	23	13	1136	2.67	65.6	<5	5	27	.93	14.6	.6	21	.10	.066	33	12	.18	295	.01	<3	.80	.02	.15	<2	.3	444	.6	.4	2.8	12
L11+00N 11+00E	18.6	40.3	79.5	137.3	461	24	14	1210	2.87	72.6	6	6	25	1.01	16.2	.5	24	.10	.073	28	10	.21	242	.01	<3	.79	.01	.13	<2	.2	537	.6	.3	2.4	18
L10+50N 5+00E	28.3	64.5	44.8	143.7	416	93	24	938	4.85	61.8	<5	5	65	.69	11.2	.6	39	.05	.110	17	27	.39	207	<.01	<3	1.14	.01	.12	<2	<.2	217	.8	.7	3.4	13
L10+50N 5+25E	45.0	156.3	118.5	507.1	604	116	50	5190	7.07	1490.9	<5	2	57	2.77	16.0	<1	57	.24	.115	17	7	.15	1189	<.01	<3	.61	.01	.14	<2	<1	4099	<1.5	<1	2.9	7
L10+50N 5+50E	36.0	53.7	44.8	69.7	561	29	11	309	3.56	294.1	<5	5	88	.21	31.7	.7	19	.02	.061	11	12	.05	277	<.01	<3	.70	.01	.33	<2	.7	1333	1.3	.9	2.3	12
L10+50N 5+75E	52.1	36.1	25.3	36.2	422	51	10	149	2.69	667.8	<5	3	82	.21	29.5	1.3	13	.09	.037	8	6	.03	213	<.01	<3	.21	.01	.18	<2	1.3	7047	1.5	2.4	1.3	11
L10+50N 6+00E	19.8	173.0	41.3	224.4	830	59	38	1706	8.50	173.8	<5	<2	53	1.05	9.9	.7	134	.53	.201	8	18	1.40	650	<.01	<3	2.50	.02	.27	<2	<.2	305	1.7	.9	6.4	7
L10+50N 6+25E	12.9	79.3	28.3	100.8	558	70	18	691	4.67	330.9	<5	3	87	.55	18.2	.5	45	.53	.105	11	19	.29	465	<.01	<3	.97	.01	.34	<2	.4	396	1.3	1.0	3.2	9
L10+50N 6+50E	24.7	42.1	33.3	55.2	869	60	11	294	4.50	217.5	<5	5	153	.28	36.4	1.2	20	.05	.087	24	15	.05	282	<.01	<3	.36	.02	.47	<2	.4	452	3.9	4.0	1.6	18
L10+50N 6+75E	25.7	60.4	57.4	77.5	606	61	17	496	4.11	320.3	<5	5	89	.30	648.4	.8	32	.07	.077	20	19	.16	433	<.01	<3	.72	.01	.37	<2	1.0	1146	3.7	.9	2.3	60
RE L10+50N 6+50E	24.9	41.8	30.8	55.3	873	60	11	289	4.51	216.5	<5	4	154	.26	36.3	1.2	20	.05	.087	24	16	.05	290	<.01	<3	.37	.02	.47	<2	.4	433	3.7	4.0	1.5	17
L10+50N 7+00E	24.9	57.5	34.4	96.8	521	58	14	528	4.09	195.7	<5	5	59	.75	57.3	.5	30	.16	.099	19	21	.15	458	<.01	<3	.82	.01	.32	<2	.2	312	.8	.9	1.8	8
L10+50N 7+25E	37.5	22.8	57.1	78.4	636	26	7	347	2.94	175.2	<5	12	32	.25	20.9	.5	13	.11	.043	34	5	.10	480	<.01	<3	.69	.01	.24	<2	.2	150	<.3	.4	1.9	11
L10+50N 7+50E	15.9	47.1	42.2	124.0	525	26	13	555	4.14	152.0	<5	2	34	.64	17.9	.6	45	.13	.113	19	13	.26	297	.01	<3	1.21	.01	.21	<2	.2	209	<.3	.4	4.3	4
L10+50N 7+75E	19.3	54.1	79.0	105.8	850	15	16	733	5.07	88.9	<5	5	47	.24	7.8	.7	32	.03	.113	28	9	.35	255	<.01	<3	1.40	.03	.20	<2	.2	296	1.3	.7	3.2	13
L10+50N 8+00E	14.8	48.0	78.9	196.3	700	24	16	1245	4.18	151.0	<5	2	35	.63	10.1	.6	40	.11	.125	20	10	.35	416	<.01	<3	1.35	.02	.16	<2	.2	128	.3	.4	3.8	20
L10+50N 8+25E	16.4	43.8	46.9	102.4	1184	28	14	764	3.31	121.7	<5	4	28	.39	21.2	.5	35	.06	.102	18	11	.34	218	<.01	<3	1.40	.02	.15	<2	.3	200	.4	.4	3.8	8
L10+50N 8+50E	16.0	49.2	80.3	119.4	1310	24	10	438	4.23	111.4	<5	4	36	.73	12.1	.6	42	.13	.088	26	14	.43	447	.01	<3	1.58	.02	.17	<2	.3	391	.4	.6	4.6	18
L10+50N 8+75E	12.4	40.7	74.0	136.6	942	23	14	805	3.81	142.9	<5	5	38	.89	14.4	.5	37	.20	.083	19	14	.48	344	.01	<3	1.27	.02	.17	<2	<.2	534	.4	.6	4.0	7
L10+50N 9+00E	11.4	38.9	98.4	194.3	820	18	16	1462	3.69	106.1	<5	3	66	1.58	15.4	.6	34	.45	.147	19	12	.44	601	.01	<3	1.26	.02	.23	<2	.2	366	<.3	.3	4.1	5
L10+50N 9+25E	11.8	34.0	60.5	114.6	565	21	12	955	2.99	124.8	<5	3	39	.93	23.4	.5	31	.22	.095	21	13	.33	397	.01	<3	.95	.01	.19	<2	.3	365	.3	.4	3.4	7
L10+50N 9+50E	11.6	35.9	80.8	143.9	620	18	13	1277	3.09	103.5	<5	4	40	.67	17.1	.5	31	.21	.116	18	9	.37	413	.01	<3	1.16	.02	.19	<2	.2	484	<.3	.2	3.2	5
L10+50N 9+75E	12.2	42.2	86.0	128.7	559	25	15	1034	3.44	161.3	<5	4	34	.62	25.5	.5	36	.20	.074	22	12	.43	259	.01	<3	1.11	.01	.15	<2	.2	816	.5	.2	3.1	10
L10+50N 10+00E	12.2	49.3	73.3	142.6	687	32	16	1329	3.45	129.7	<5	6	33	1.26	19.9	.6	35	.21	.084	83	12	.39	472	.01	<3	1.08	.01	.15	<2	.2	280	.6	.3	3.3	8
L10+50N 10+25E	18.0	60.2	97.4	181.5	463	36	16	960	3.37	125.2	<5	7	28	.79	18.0	.6	33	.16	.068	41	13	.32	288	.01	<3	.80	.01	.12	<2	<.2	663	.5	.3	2.0	7
STANDARD D2/C3/AU-S	23.9	122.7	102.6	265.3	1857	31	17	1039	4.52	72.3	23	23	60	1.92	9.0	17.4	73	.69	.108	18	59	1.12	245	.16	29	2.44	.05	.71	14	2.1	979	.5	1.8	6.2	55

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L10+50N 10+50E	20.7	56.8	77.5	193.1	770	88	26	5070	3.84	175.8	<5	4	42	1.75	56.6	.9	29	.24	.083	29	15	.26	590	<.01	<3	.63	.01	.16	<2	.4	1127	1.1	1.0	2.0	18
L10+50N 10+75E	16.3	132.0	292.5	428.0	1194	30	24	2375	4.90	159.1	<5	5	42	2.97	40.7	1.6	62	.39	.097	36	18	.75	420	.01	<3	1.55	.02	.14	<2	.6	1325	1.1	.9	4.5	21
L10+50N 11+00E	23.3	58.4	82.9	220.7	857	39	21	1726	4.53	175.4	<5	4	32	1.67	30.6	1.1	49	.40	.107	31	18	.51	404	<.01	<3	1.22	.01	.14	<2	.5	932	.8	.5	3.6	15
L10+00N 5+00E	76.7	125.3	173.7	291.8	807	75	15	450	4.82	138.4	<5	3	72	1.12	8.5	2.2	31	.04	.100	16	27	.06	244	<.01	<3	.44	.01	.19	<2	.7	647	.7	1.3	1.2	18
L10+00N 5+25E	54.0	62.2	108.4	182.6	558	46	18	925	3.69	114.6	<5	4	32	.62	6.4	1.2	23	.06	.093	23	12	.17	210	.01	<3	.86	.01	.16	<2	.4	191	.7	.5	2.1	28
L10+00N 5+50E	55.5	29.2	75.4	121.7	1184	19	9	609	2.51	173.4	<5	5	25	.41	6.7	1.2	18	.09	.081	23	6	.16	236	.01	<3	.81	.02	.15	<2	.2	71	.4	.4	1.9	80
L10+00N 5+75E	47.1	39.9	122.5	160.4	1511	26	11	713	3.15	459.3	<5	6	24	.34	8.3	.5	23	.06	.078	31	10	.21	139	.01	<3	.94	.01	.16	<2	.3	73	.6	<.2	1.9	230
L10+00N 6+00E	47.1	129.9	83.6	224.4	1167	81	52	2848	6.84	135.3	<5	6	59	1.99	9.5	1.4	68	.57	.167	22	19	.58	545	<.01	<3	1.22	.01	.30	<2	.4	100	.5	1.3	4.2	66
L10+00N 6+25E	27.4	55.9	75.1	208.7	373	51	25	1238	4.99	71.3	<5	6	21	1.40	5.4	.5	36	.14	.058	44	10	.33	401	<.01	<3	.93	.01	.15	<2	.3	79	.5	<.2	2.4	11
L10+00N 6+50E	21.1	47.2	53.1	135.1	758	38	17	834	4.10	90.9	<5	3	43	.47	6.1	.8	36	.07	.121	23	17	.32	287	<.01	<3	1.21	.02	.20	<2	.2	53	1.3	1.0	3.0	40
L10+00N 6+75E	25.8	59.4	50.8	106.6	504	45	15	445	2.99	83.0	<5	7	18	.28	6.0	.3	29	.08	.069	26	17	.14	236	<.01	<3	1.04	.01	.14	<2	.3	90	.5	.2	1.9	224
L10+00N 7+00E	20.4	37.1	79.6	122.1	807	27	10	398	3.34	50.0	<5	3	24	.59	5.9	.6	24	.07	.078	16	15	.19	159	.01	<3	.93	.01	.18	<2	.3	67	.4	.4	3.0	31
L10+00N 7+25E	22.6	31.7	61.8	66.8	622	17	6	267	2.40	72.3	<5	7	21	.17	5.1	.2	16	.03	.069	26	9	.11	138	<.01	<3	.89	.02	.18	<2	.3	44	.6	.3	2.1	68
L10+00N 7+50E	23.7	61.3	37.6	156.8	525	72	27	1153	5.35	215.7	<5	3	59	.65	34.9	.5	44	.27	.124	20	20	.38	280	<.01	<3	1.14	.01	.23	<2	.5	264	1.2	.9	4.0	9
L10+00N 7+75E	27.5	41.3	53.9	87.3	407	36	21	2143	3.75	111.3	<5	3	64	.50	46.1	.5	35	.20	.128	24	19	.19	637	<.01	<3	1.18	.02	.30	<2	.5	663	1.2	.6	3.1	10
L10+00N 8+00E	21.2	99.5	28.4	178.7	434	55	29	1591	7.27	107.8	<5	3	45	.58	22.1	.3	102	.11	.177	22	33	.77	429	<.01	<3	1.90	.01	.28	<2	.3	59	.7	.8	5.3	5
RE L10+00N 8+00E	20.3	99.7	28.2	177.0	441	56	28	1559	7.26	107.1	<5	3	44	.61	21.3	.4	101	.11	.176	21	32	.76	415	<.01	<3	1.83	.01	.27	<2	.2	59	.8	.8	5.1	27
L10+00N 8+25E	24.6	73.3	51.9	143.2	509	40	21	1354	5.02	79.5	<5	2	31	.53	16.2	.7	61	.04	.135	21	24	.44	253	<.01	<3	1.62	.01	.18	<2	.3	82	.9	.8	5.4	13
L10+00N 8+50E	17.9	66.2	69.2	195.1	750	31	24	2069	4.73	113.2	8	3	51	1.51	11.3	.6	51	.34	.157	23	19	.45	722	.01	3	1.34	.02	.30	<2	.4	141	.8	.5	4.5	10
L10+00N 8+75E	14.6	49.0	85.0	148.8	865	21	18	988	3.96	102.9	<5	<2	30	.61	14.9	.6	38	.08	.106	23	15	.40	216	.01	<3	1.38	.02	.13	<2	.6	701	.9	.6	4.1	25
L10+00N 9+00E	14.0	50.6	92.3	116.6	1711	20	14	698	4.44	95.5	<5	3	39	.29	11.2	.5	42	.11	.118	20	18	.45	323	.01	<3	1.48	.02	.16	<2	.5	389	1.2	.6	4.4	12
L10+00N 9+25E	30.7	89.0	107.5	334.3	819	86	36	2261	5.06	231.9	5	6	31	2.02	26.7	.8	31	.13	.090	36	17	.24	341	<.01	<3	1.09	.01	.14	<2	.7	688	1.6	.9	2.6	49
L10+00N 9+50E	26.7	64.8	119.1	175.3	1136	29	18	1131	4.07	87.5	<5	3	55	.67	21.5	1.6	33	.15	.128	30	13	.27	416	<.01	<3	1.22	.02	.17	<2	.9	457	2.1	.9	2.9	9
L10+00N 9+75E	15.0	65.4	106.6	196.5	883	25	18	1020	4.46	636.9	<5	6	46	.94	200.9	1.2	36	.25	.094	31	13	.39	446	.01	<3	.97	.02	.15	<2	1.7	13071	1.9	1.0	3.1	6
L10+00N 10+00E	16.7	76.1	91.4	168.1	742	31	23	1525	5.04	919.7	<5	4	49	.96	147.5	.9	43	.30	.104	27	12	.36	574	<.01	<3	.99	.02	.17	<2	2.2	10806	1.7	.7	2.7	11
L10+00N 10+25E	16.0	76.1	91.0	179.4	956	30	21	1306	4.96	726.8	<5	4	42	1.09	141.0	1.1	50	.33	.103	28	14	.41	279	<.01	<3	1.05	.02	.14	<2	1.4	11880	1.4	.8	2.4	11
L10+00N 10+50E	30.0	52.2	77.4	146.8	990	38	16	951	3.94	2650.3	<5	3	54	.62	682.5	1.3	32	.28	.091	18	18	.21	589	<.01	<3	1.20	.01	.16	<2	2.1	49073	2.1	<1	<2.5	17
L10+00N 10+75E	15.5	86.0	149.2	211.0	1091	22	29	2228	5.64	347.7	<5	4	61	1.51	76.2	.9	69	.46	.106	30	16	.95	253	.01	<3	2.12	.03	.14	<2	.9	3326	.3	.5	6.1	13
L10+00N 11+00E	14.8	46.1	81.9	137.7	859	21	24	1819	4.46	321.3	<5	3	52	.76	98.3	.7	55	.41	.110	24	14	.61	365	.01	<3	1.92	.02	.15	<2	1.1	2989	<.3	.4	5.1	12
98SCES-01	44.5	10.2	23.4	18.3	327	8	3	81	8.00	105.5	<5	2	30	.05	31.3	.4	12	.04	.023	7	19	.01	211	<.01	3	.20	.01	.25	<2	.5	1821	1.4	2.5	2.1	6
STANDARD D2/C3/AU-S	23.3	122.7	102.2	266.2	1837	31	17	1032	4.51	72.3	21	21	59	1.80	9.3	17.1	74	.69	.107	18	59	1.11	241	.16	29	2.39	.05	.70	14	2.3	896	.7	2.3	6.4	52

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data___ FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

SINTER GRID

Omni Resources Inc. PROJECT SINTER CAP/GODDELL File # 9803303 Page 1

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G. Wesa

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L19+00N 8+00E	4.7	10.6	28.8	76.8	120	5	4	1148	1.89	6.6	<5	<2	18	.97	22.7	.2	27	.19	.054	17	9	.15	353	.01	<3	.58	.01	.10	2	<.2	24	<.3	<.2	2.8	2
L19+00N 8+25E	2.9	10.2	28.1	50.1	91	8	5	507	1.76	8.5	<5	4	11	.23	10.5	<.2	26	.16	.055	15	12	.26	128	.02	<3	.79	.01	.07	<2	<.2	43	<.3	<.2	2.9	2
L19+00N 8+50E	4.4	13.6	28.6	76.2	232	7	4	524	1.73	11.5	13	2	15	.51	8.6	.2	24	.16	.075	17	10	.20	231	.01	<3	.86	.01	.13	2	<.2	46	<.3	<.2	4.2	7
L19+00N 8+75E	6.0	10.3	36.2	56.1	137	9	5	393	1.89	14.6	<5	5	10	.36	7.0	<.2	27	.13	.055	16	15	.23	83	.01	<3	1.13	.01	.07	<2	<.2	50	<.3	<.2	3.4	19
L19+00N 9+00E	10.0	27.8	112.7	71.6	264	7	7	1098	1.98	17.2	7	<2	11	.55	8.8	.2	22	.10	.061	25	13	.17	533	.01	<3	.82	.01	.13	<2	<.2	80	<.3	<.2	2.8	200
L19+00N 9+25E	6.4	17.3	67.0	67.8	197	6	7	1571	1.67	15.3	<5	3	13	.63	5.8	<.2	18	.11	.058	26	5	.13	451	.01	<3	.71	.01	.10	<2	<.2	75	<.3	<.2	2.4	6
L19+00N 9+50E	4.3	12.8	52.3	79.9	175	6	5	636	1.80	12.3	<5	<2	20	.33	6.9	.4	19	.17	.091	16	8	.18	356	<.01	<3	.91	.01	.12	<2	<.2	48	<.3	<.2	2.8	3
L19+00N 9+75E	3.4	11.2	24.4	48.4	93	6	4	352	1.54	9.1	<5	4	9	.34	7.9	<.2	24	.12	.048	17	10	.19	89	.01	<3	.75	.01	.06	<2	<.2	33	<.3	<.2	2.9	5
L19+00N 10+00E	3.7	9.9	28.7	51.5	91	6	6	433	1.76	11.4	<5	4	9	.41	7.3	<.2	27	.10	.039	17	11	.18	69	.01	<3	.82	.01	.08	<2	<.2	33	<.3	<.2	2.7	6
L19+00N 10+25E	4.0	11.7	23.5	51.0	164	6	4	414	1.48	14.1	5	<2	9	.37	6.0	<.2	23	.11	.062	14	8	.18	85	.01	<3	.80	.01	.07	<2	<.2	81	<.3	<.2	2.7	5
L19+00N 10+50E	3.2	13.2	20.1	63.8	222	5	4	399	1.54	12.7	<5	<2	11	.29	4.5	<.2	28	.13	.067	18	10	.17	147	.01	<3	.83	.01	.08	<2	<.2	50	<.3	<.2	2.6	59
L19+00N 10+75E	4.1	12.3	29.7	63.5	63	9	5	461	1.90	15.1	<5	4	14	.41	7.6	.2	30	.20	.056	22	11	.24	105	.02	<3	.75	.01	.09	<2	<.2	70	<.3	<.2	2.6	4
L19+00N 11+00E	3.7	13.7	27.5	59.0	44	7	6	823	1.86	14.3	<5	4	7	.42	6.9	<.2	24	.13	.056	23	10	.13	179	.01	<3	.56	.01	.07	<2	<.2	35	<.3	<.2	1.9	3
RE L19+00N 11+00E	3.7	14.1	29.5	58.9	52	8	7	831	1.89	11.1	6	4	7	.43	7.1	<.2	24	.13	.057	24	7	.13	181	.01	<3	.56	.01	.08	<2	.2	39	<.3	<.2	2.0	3
L19+00N 11+25E	4.0	10.9	28.9	64.0	75	7	4	434	1.67	13.8	6	3	9	.28	4.5	.2	22	.10	.040	22	8	.19	122	<.01	<3	.90	.01	.08	<2	<.2	56	<.3	<.2	1.9	8
L19+00N 11+50E	5.9	12.2	25.0	107.1	105	8	7	949	2.81	13.4	<5	15	13	.51	6.3	.3	30	.21	.084	47	12	.14	227	.02	<3	.61	.01	.09	<2	<.2	95	<.3	<.2	1.9	5
L19+00N 11+75E	3.6	10.2	32.6	64.2	120	7	4	341	1.88	16.1	<5	4	9	.28	10.1	.2	26	.08	.033	17	12	.19	81	.01	<3	1.06	.01	.08	<2	<.2	65	<.3	<.2	2.8	19
L19+00N 12+00E	3.3	10.3	18.6	63.3	78	7	4	412	1.58	16.1	<5	4	7	.16	5.1	<.2	24	.09	.048	13	11	.25	55	.01	<3	.82	.01	.08	<2	<.2	44	<.3	<.2	2.7	4
L19+00N 12+25E	8.8	31.1	65.7	85.5	130	8	7	1393	2.04	11.5	<5	8	19	.83	10.1	.4	25	.25	.066	35	5	.23	590	<.01	<3	.84	.01	.14	2	<.2	69	<.3	<.2	2.8	37
L19+00N 12+50E	2.7	13.5	38.5	66.3	144	6	7	749	2.28	12.3	<5	6	14	.21	11.1	.3	24	.19	.088	22	10	.17	107	<.01	<3	1.19	.01	.13	<2	<.2	74	<.3	<.2	2.4	3
L19+00N 12+75E	2.3	11.6	56.0	78.6	173	8	9	892	2.62	13.8	7	6	14	.34	16.3	.3	35	.25	.106	19	11	.34	148	<.01	<3	1.73	.01	.13	<2	.3	143	<.3	<.2	4.7	4
L19+00N 13+00E	7.7	14.6	25.9	73.3	76	6	5	974	2.16	18.4	<5	2	14	.37	11.9	.2	28	.10	.049	24	3	.13	139	<.01	<3	1.11	.01	.09	<2	<.2	223	<.3	<.2	3.2	3
L19+00N 13+25E	6.2	17.7	29.4	82.6	80	11	6	584	2.00	23.3	<5	6	9	.45	9.7	.2	26	.06	.039	22	12	.23	104	.01	<3	1.03	.01	.12	<2	.2	151	<.3	<.2	3.2	4
L19+00N 13+50E	7.0	15.6	19.9	73.8	58	8	4	264	2.03	28.9	<5	<2	7	.30	9.5	.2	23	.04	.044	20	8	.18	107	<.01	<3	.87	.01	.09	<2	.2	198	<.3	<.2	2.8	4
L19+00N 13+75E	4.7	15.9	31.4	73.1	68	10	6	678	1.98	25.3	<5	<2	8	.49	9.5	.2	29	.03	.049	19	11	.16	160	.01	<3	1.14	.01	.07	<2	.2	137	<.3	<.2	3.5	3
L19+00N 14+00E	5.9	12.0	40.0	69.1	203	6	3	405	1.53	31.5	<5	2	6	.32	6.5	.3	11	.04	.041	35	5	.09	230	<.01	<3	1.10	.01	.12	<2	.2	128	<.3	<.2	3.4	10
L18+50N 8+00E	6.3	12.8	20.7	48.8	137	5	3	152	1.47	12.6	10	3	13	.23	6.8	.2	22	.13	.026	11	8	.12	93	.01	<3	.53	.01	.09	<2	<.2	<10	<.3	<.2	3.9	2
L18+50N 8+25E	4.1	14.4	35.1	74.3	151	9	4	596	1.59	13.6	18	2	14	.44	7.5	.2	20	.17	.060	19	7	.18	238	.01	<3	.98	.01	.13	<2	<.2	36	<.3	<.2	3.2	4
L18+50N 8+50E	3.0	12.9	22.7	46.9	100	7	5	565	1.71	16.0	<5	3	12	.26	7.3	.2	24	.16	.049	21	10	.15	197	.01	<3	.71	.01	.08	<2	<.2	30	<.3	<.2	2.0	4
L18+50N 8+75E	2.4	11.2	20.8	59.0	86	8	6	715	1.87	12.2	<5	3	16	.42	5.9	<.2	25	.21	.074	26	11	.21	354	.02	<3	.76	.01	.09	<2	<.2	28	<.3	<.2	1.9	3
L18+50N 9+00E	3.1	7.8	20.3	38.6	57	6	4	247	1.73	16.5	<5	4	9	.29	6.0	.2	28	.06	.025	17	13	.16	81	.01	<3	1.00	.01	.06	<2	<.2	30	<.3	<.2	2.8	3
L18+50N 9+25E	2.7	6.8	17.4	45.3	46	7	5	347	1.68	16.2	<5	4	9	.23	5.5	<.2	26	.13	.048	17	11	.20	79	.01	<3	.85	.01	.06	<2	<.2	41	<.3	<.2	2.0	6
L18+50N 9+50E	2.7	8.0	18.3	45.8	61	6	4	358	1.51	10.8	11	2	10	.31	6.2	<.2	23	.14	.052	18	14	.20	90	.02	<3	.76	.01	.07	<2	.2	19	<.3	<.2	2.2	11
L18+50N 9+75E	2.6	8.5	19.3	41.0	57	6	4	573	1.38	7.8	<5	3	12	.25	5.6	<.2	22	.17	.057	15	8	.19	120	.02	<3	.59	.01	.06	<2	<.2	30	<.3	<.2	2.0	3
STANDARD D2/C3/AU-S	23.3	118.6	100.9	260.9	1971	31	18	1040	4.56	67.3	15	20	61	2.00	8.7	17.9	74	.70	.106	19	57	1.13	231	.12	29	2.46	.05	.69	13	2.1	1006	.4	1.9	6.8	44

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 7 1998 **DATE REPORT MAILED:** Aug 17/98 **SIGNED BY** .... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data / FA ____

Omni Resources Inc. PROJECT SINTER CAP/GODDELL FILE # 9803303 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L18+50N 10+00E	2.9	7.8	27.1	43.0	53	6	4	343	1.47	7.6	<5	4	9	.32	6.4	.2	22	.15	.062	15	11	.18	62	.01	<3	.60	.01	.06	<2	<.2	44	<.3	<.2	2.3	1
L18+50N 10+25E	3.2	8.7	27.8	43.6	95	6	4	266	1.60	8.6	<5	4	8	.34	6.5	.2	24	.10	.043	14	10	.16	75	.01	<3	.84	.01	.06	<2	<.2	37	<.3	<.2	3.0	1
L18+50N 10+50E	4.8	10.1	34.8	79.9	184	7	5	555	1.70	11.6	<5	2	14	.71	6.4	.3	25	.17	.073	18	13	.18	191	.01	<3	.80	.01	.08	<2	<.2	66	<.3	<.2	3.0	3
L18+50N 10+75E	5.1	12.8	35.7	93.8	230	7	4	461	1.70	13.7	<5	3	13	.39	5.8	.3	22	.13	.058	25	9	.22	185	.01	<3	1.01	.01	.09	<2	.2	69	<.3	<.2	3.3	3
L18+50N 11+00E	5.1	10.4	43.1	68.9	240	7	5	620	1.67	16.2	<5	4	8	.68	8.3	.3	25	.12	.054	17	9	.18	67	.01	<3	.69	.01	.08	<2	.2	38	.3	<.2	3.1	120
RE L18+50N 11+00E	3.9	9.5	33.1	65.9	109	7	5	594	1.59	13.3	<5	5	7	.47	5.9	.2	23	.11	.053	16	13	.17	64	.01	<3	.64	.01	.07	<2	<.2	67	<.3	<.2	2.2	5
L18+50N 11+25E	4.8	9.1	36.4	74.4	140	6	4	744	1.48	14.4	<5	2	11	.58	5.2	.2	18	.12	.054	23	7	.15	164	.01	<3	.77	.01	.11	<2	<.2	52	<.3	<.2	2.4	12
L18+50N 11+50E	5.4	11.7	36.7	78.7	290	7	4	483	1.59	11.0	<5	2	17	.61	6.9	.3	21	.17	.064	26	8	.20	307	.01	<3	.91	.01	.09	<2	.2	74	<.3	<.2	2.8	6
L18+50N 11+75E	4.0	12.5	39.4	89.0	94	10	6	573	2.00	10.3	<5	4	10	.46	7.5	.3	31	.07	.034	16	15	.31	81	.01	<3	1.29	.01	.09	<2	.2	35	<.3	<.2	4.0	2
L18+50N 12+00E	3.8	11.0	30.9	59.1	55	9	5	493	1.67	11.4	<5	4	10	.47	6.9	.2	25	.12	.046	16	14	.25	90	.02	<3	.72	.01	.08	<2	<.2	65	<.3	<.2	2.9	3
L18+50N 12+25E	2.7	16.6	22.6	65.4	34	7	6	550	1.80	10.8	5	9	15	.30	7.5	<.2	26	.16	.042	26	9	.23	181	.01	<3	.76	.01	.08	<2	<.2	59	<.3	<.2	2.4	1
L18+50N 12+50E	3.3	9.5	34.0	62.5	39	7	5	368	2.20	12.3	<5	5	12	.33	12.4	.4	29	.16	.070	16	10	.25	90	<.01	<3	1.20	.01	.11	<2	<.2	51	<.3	<.2	4.4	<1
L18+50N 12+75E	2.7	14.2	45.1	83.0	87	8	8	688	2.50	9.9	<5	6	15	.32	14.2	.4	31	.23	.094	23	10	.27	171	<.01	<3	1.38	.01	.13	<2	.2	103	<.3	<.2	4.4	1
L18+50N 13+00E	3.8	29.8	51.7	110.3	190	7	8	818	2.92	11.4	<5	2	20	.50	22.4	.5	38	.25	.140	18	6	.37	255	<.01	<3	1.82	.01	.14	2	.3	367	<.3	<.2	5.3	1
L18+50N 13+25E	7.3	11.2	32.5	61.5	70	6	3	480	1.54	16.1	6	4	7	.36	7.2	.3	13	.04	.030	36	6	.09	89	<.01	<3	.99	.01	.10	<2	.2	112	<.3	<.2	2.8	3
L18+50N 13+50E	8.6	15.4	71.6	114.5	95	9	8	1481	2.56	22.4	<5	4	12	.62	9.1	.5	32	.07	.042	18	10	.25	199	.01	<3	1.42	.01	.09	<2	.2	93	<.3	<.2	5.1	11
L18+50N 13+75E	4.6	8.3	36.2	66.3	81	6	2	649	1.33	30.4	<5	7	7	.51	5.9	.3	7	.06	.020	49	3	.04	193	<.01	<3	.41	.01	.09	<2	<.2	112	<.3	<.2	1.3	28
L18+50N 14+00E	3.1	12.8	27.3	78.3	47	6	4	476	1.80	10.5	7	8	4	.39	4.0	.2	15	.02	.029	27	6	.02	137	<.01	<3	1.05	.01	.11	<2	.2	160	<.3	<.2	2.2	15
L18+00N 8+00E	6.7	12.1	38.4	85.8	228	8	5	454	1.68	15.2	<5	3	20	.43	7.0	.3	19	.27	.072	22	12	.20	385	<.01	<3	1.00	.01	.13	<2	<.2	56	<.3	<.2	3.0	1
L18+00N 8+25E	12.4	9.4	63.0	99.9	237	6	5	580	2.16	15.1	<5	5	25	.32	5.4	.5	24	.38	.070	24	10	.22	777	<.01	<3	1.46	.01	.11	<2	.3	61	<.3	<.2	3.8	2
L18+00N 8+50E	3.4	6.4	24.4	56.1	52	6	3	255	1.30	10.3	<5	3	9	.34	5.2	<.2	21	.10	.028	16	8	.21	78	.01	<3	.73	.01	.05	<2	<.2	29	<.3	<.2	2.4	18
L18+00N 8+75E	8.8	14.1	31.2	97.7	146	8	4	361	1.93	16.1	<5	<2	20	.58	6.6	.4	21	.16	.063	22	8	.13	363	<.01	<3	.71	.01	.12	<2	<.2	38	<.3	<.2	3.0	2
L18+00N 9+00E	2.8	7.2	23.5	45.1	50	5	4	512	1.44	9.8	<5	6	12	.29	8.3	.2	19	.19	.067	21	9	.15	133	.01	<3	.58	.01	.08	<2	<.2	31	<.3	<.2	2.0	<1
L18+00N 9+25E	3.2	8.5	29.8	54.6	98	6	4	503	1.54	10.5	<5	4	10	.42	7.8	.2	23	.17	.066	15	9	.19	61	.02	<3	.56	.01	.08	<2	<.2	32	<.3	<.2	2.3	160
L18+00N 9+50E	5.3	14.1	38.4	85.6	52	9	5	519	1.91	14.3	<5	4	14	.65	8.8	.3	28	.20	.077	20	12	.20	129	.02	<3	.65	.01	.07	<2	.2	58	<.3	<.2	2.6	2
L18+00N 9+75E	5.2	12.3	33.2	83.9	120	8	5	473	1.71	12.8	<5	<2	8	.39	6.8	.2	24	.09	.055	16	13	.20	115	.01	<3	.95	.01	.08	<2	<.2	39	<.3	<.2	3.1	1
L18+00N 10+00E	4.5	15.8	35.7	85.3	197	8	5	558	1.73	12.1	6	3	14	.51	6.0	.3	25	.16	.078	21	13	.24	186	.01	<3	1.01	.01	.11	<2	<.2	69	<.3	<.2	3.3	3
L18+00N 10+25E	4.3	47.7	28.2	83.9	396	11	5	596	1.77	7.6	<5	4	13	.48	4.5	<.2	18	.20	.069	20	10	.14	138	.01	<3	.56	.01	.10	68	<.2	28	<.3	<.2	1.7	2
L18+00N 10+50E	3.2	10.3	18.3	53.8	83	5	4	374	1.76	9.0	<5	3	10	.24	5.5	<.2	25	.08	.044	17	11	.17	145	.01	<3	1.08	.01	.07	<2	.2	33	<.3	<.2	3.4	<1
L18+00N 10+75E	2.6	16.3	26.0	67.6	161	5	3	642	1.79	7.0	<5	3	16	.54	23.9	<.2	19	.19	.095	21	6	.14	222	<.01	<3	1.61	.01	.08	<2	<.2	124	<.3	<.2	4.3	3
L18+00N 11+00E	3.2	12.3	34.4	62.1	61	8	6	529	1.96	13.8	<5	6	6	.29	7.1	<.2	28	.11	.065	17	12	.20	110	.01	<3	1.37	.01	.09	<2	<.2	35	<.3	<.2	3.1	<1
L18+00N 11+25E	11.5	16.6	50.1	71.6	677	6	3	209	2.23	22.9	5	5	11	.24	7.4	1.2	23	.05	.030	18	8	.16	79	<.01	<3	.91	.01	.10	<2	.2	55	<.3	<.2	3.6	15
L18+00N 11+50E	7.3	11.3	47.6	60.6	162	6	3	483	1.54	13.5	<5	4	8	.39	6.0	.3	15	.05	.032	23	5	.11	104	<.01	<3	.68	.01	.10	<2	<.2	72	<.3	<.2	2.4	27
L18+00N 11+75E	4.0	7.0	21.5	25.4	297	4	1	168	.76	6.5	7	3	2	.20	4.3	<.2	8	.01	.014	11	3	.04	38	<.01	<3	.48	<.01	.06	<2	<.2	38	<.3	<.2	1.7	338
STANDARD D2/C3/AU-S	22.6	117.8	103.5	261.6	1744	31	17	1012	4.51	69.1	22	21	61	1.83	7.3	17.4	73	.70	.106	18	56	1.12	246	.13	28	2.41	.05	.70	13	1.9	1059	.3	1.6	6.2	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L18+00N 12+00E	5.0	9.1	29.6	62.1	257	9	4	481	1.48	15.3	<5	<2	11	.44	6.8	<.2	17	.10	.047	16	7	.11	192	<.01	<3	.62	.01	.10	<2	<.2	64	<.3	<.2	2.1	466
L18+00N 12+25E	5.0	13.5	39.0	107.0	274	11	4	853	1.78	22.2	7	6	13	.63	4.8	.2	14	.10	.035	33	5	.07	199	<.01	<3	.86	.01	.14	<2	.2	77	<.3	<.2	2.4	208
L18+00N 12+50E	5.1	11.8	31.3	78.9	202	8	5	649	2.21	25.0	<5	<2	14	.50	11.7	.3	33	.13	.069	17	10	.28	181	.01	<3	1.08	.01	.11	<2	<.2	43	<.3	<.2	4.5	1
L18+00N 12+75E	18.1	14.8	45.1	90.4	175	15	6	1679	2.15	72.1	8	9	9	1.36	5.2	.2	7	.06	.029	47	5	.01	430	<.01	<3	.44	.01	.12	<2	<.2	113	<.3	<.2	1.5	51
L18+00N 13+00E	33.2	10.1	83.7	177.5	365	27	6	6907	2.34	173.5	<5	8	15	2.08	8.6	.4	3	.06	.026	46	4	.02	2033	<.01	<3	.51	.01	.13	<2	.3	136	<.3	<.2	1.8	20
L18+00N 13+25E	12.7	8.9	60.0	70.9	184	6	2	1907	1.38	76.7	<5	6	5	1.16	7.2	.2	4	.02	.025	65	4	.01	404	<.01	<3	.31	.01	.09	<2	.2	64	<.3	<.2	1.3	74
L18+00N 13+50E	7.8	13.8	68.9	78.4	120	6	7	606	2.36	27.6	<5	4	12	.47	9.9	.4	27	.12	.052	15	11	.28	95	.01	<3	1.28	.01	.09	<2	<.2	192	<.3	<.2	3.4	1
L18+00N 13+75E	7.8	20.2	57.5	76.7	98	8	6	660	2.19	25.1	<5	4	8	.48	10.6	.4	28	.06	.051	25	11	.20	125	.01	<3	1.31	.01	.10	<2	.3	73	<.3	<.2	3.3	7
L18+00N 14+00E	4.6	22.7	63.1	87.4	277	7	7	873	2.34	16.3	<5	<2	14	.45	6.7	.5	34	.11	.063	21	11	.36	309	.01	<3	1.39	.01	.10	<2	.2	179	<.3	<.2	4.3	3
L17+50N 8+00E	11.3	15.2	72.1	86.8	269	8	25	1323	1.82	15.3	<5	5	27	.38	9.7	.4	17	.33	.091	60	7	.15	1178	<.01	<3	1.42	.01	.11	<2	.4	71	.3	<.2	3.3	2
RE L17+50N 9+00E	4.6	9.1	34.1	67.2	75	6	4	346	1.65	12.7	6	5	10	.38	6.2	.2	23	.12	.045	22	12	.17	82	.01	<3	.57	.01	.06	<2	<.2	35	<.3	<.2	2.1	3
L17+50N 8+25E	5.4	8.2	35.3	91.4	109	6	4	383	1.39	14.4	<5	3	11	.48	7.7	.2	17	.13	.036	17	5	.20	268	<.01	<3	.71	.01	.06	<2	<.2	89	<.3	<.2	2.4	<1
L17+50N 8+50E	6.1	12.0	25.8	87.4	43	6	4	970	1.68	11.6	<5	<2	16	.56	6.6	.2	28	.12	.046	28	9	.13	546	.01	<3	.71	.01	.12	<2	<.2	37	<.3	<.2	3.0	2
L17+50N 8+75E	5.7	12.7	39.1	89.9	150	8	5	461	1.74	11.9	<5	<2	10	.57	5.9	.3	25	.10	.069	14	13	.19	98	.01	<3	.96	.01	.08	<2	<.2	54	<.3	<.2	3.3	4
L17+50N 9+00E	5.0	10.2	35.5	69.2	86	6	4	348	1.69	13.9	<5	5	10	.43	7.0	.2	24	.13	.046	23	10	.17	84	.02	<3	.60	.01	.06	<2	<.2	108	<.3	<.2	2.5	16
L17+50N 9+25E	4.4	8.7	29.1	56.5	85	6	4	362	1.49	13.4	<5	4	11	.31	5.8	.2	22	.11	.037	22	11	.19	92	.01	<3	.78	.01	.08	<2	<.2	41	<.3	<.2	2.8	2
L17+50N 9+50E	4.8	11.6	33.8	80.2	119	8	5	469	1.93	15.7	6	4	9	.41	7.8	.3	28	.13	.063	14	13	.27	68	.01	<3	.96	.01	.08	<2	<.2	70	<.3	<.2	3.1	<1
L17+50N 9+75E	6.3	9.0	30.8	59.5	159	7	4	320	1.69	13.7	6	3	14	.24	6.2	.3	28	.19	.066	19	13	.28	134	.01	<3	1.04	.01	.06	<2	.2	227	<.3	<.2	3.9	2
L17+50N 10+00E	8.6	12.8	36.7	78.5	155	8	6	1602	1.93	13.7	<5	4	17	.53	5.3	.3	28	.12	.037	34	12	.16	202	.01	<3	1.31	.01	.12	<2	.2	85	.3	<.2	4.0	1
L17+50N 10+25E	7.5	10.6	30.3	57.0	226	6	4	287	1.64	18.3	<5	<2	17	.39	6.0	.3	20	.14	.057	23	8	.10	182	<.01	<3	.79	.01	.10	<2	<.2	264	<.3	<.2	2.9	10
L17+50N 10+50E	18.5	10.2	31.6	60.3	1060	7	4	245	1.70	25.5	<5	5	8	.16	5.6	.2	21	.07	.029	15	11	.16	57	<.01	<3	.79	.01	.10	<2	.2	36	<.3	<.2	3.1	883
L17+50N 10+75E	20.0	9.5	52.7	75.5	1303	7	3	192	2.19	30.3	<5	3	7	.19	5.5	.3	23	.06	.050	17	7	.13	66	<.01	<3	.86	.01	.11	<2	.2	65	<.3	<.2	3.3	566
L17+50N 11+00E	18.3	10.5	39.7	71.7	1035	6	4	277	1.86	25.0	<5	3	6	.31	6.8	.5	21	.07	.047	17	10	.15	80	<.01	<3	.84	.01	.11	<2	.3	52	<.3	<.2	2.8	335
L17+50N 11+25E	2.9	9.7	19.3	53.0	145	6	4	714	1.52	10.0	<5	4	13	.32	8.8	<.2	15	.16	.057	28	4	.13	205	<.01	<3	.79	.01	.15	<2	<.2	112	<.3	<.2	2.5	5
L17+50N 11+50E	14.8	14.5	68.0	89.3	467	6	3	268	2.14	29.0	<5	3	12	.23	5.9	.3	11	.05	.052	23	2	.08	98	<.01	<3	.76	.01	.13	<2	.2	67	.3	.2	2.1	24
L17+50N 11+75E	6.3	21.3	40.2	116.5	203	13	4	992	1.82	39.5	9	8	7	.92	4.6	.3	8	.07	.023	33	3	.02	307	<.01	<3	.59	.01	.15	<2	<.2	89	<.3	.2	1.6	45
L17+50N 12+00E	4.7	13.7	31.9	110.2	115	10	2	673	1.63	32.7	6	8	13	.76	3.9	.2	8	.08	.025	44	2	.04	181	<.01	<3	.64	.01	.15	<2	<.2	80	<.3	<.2	1.7	14
L17+50N 12+25E	3.5	12.5	22.0	131.0	45	17	4	901	1.96	16.8	<5	5	7	.77	2.4	<.2	12	.04	.028	35	3	.02	185	<.01	<3	.79	.01	.13	<2	<.2	59	<.3	<.2	2.1	1
L17+50N 12+50E	3.3	8.1	28.7	85.8	96	4	2	438	1.37	33.2	<5	<2	5	.53	2.8	<.2	6	.03	.044	30	7	.07	98	<.01	<3	.78	.01	.10	<2	.2	35	<.3	<.2	2.0	8
L17+50N 12+75E	3.9	15.5	19.3	77.6	114	5	4	416	2.17	9.9	<5	2	10	.28	4.8	.2	27	.08	.145	20	7	.10	142	<.01	<3	1.31	.01	.09	<2	.2	32	.3	<.2	3.3	1
L17+50N 13+00E	3.5	14.5	37.3	87.7	135	6	6	555	2.29	13.1	<5	3	12	.40	11.7	.4	29	.09	.063	19	8	.23	211	<.01	<3	1.24	.01	.11	<2	<.2	68	<.3	<.2	4.5	1
L17+50N 13+25E	4.0	22.1	58.0	96.0	94	9	9	774	2.85	23.3	<5	4	15	.51	14.9	.3	37	.19	.082	20	14	.38	172	<.01	<3	1.59	.01	.10	<2	.2	334	<.3	<.2	4.8	1
L17+50N 13+50E	11.8	9.9	36.7	57.9	110	5	6	450	2.20	16.7	<5	2	9	.25	11.6	.3	22	.07	.050	18	3	.16	165	<.01	<3	1.25	.01	.07	<2	.3	175	<.3	<.2	3.3	1
L17+50N 13+75E	4.1	13.7	37.2	69.6	100	6	5	399	2.14	17.7	<5	3	10	.43	9.2	.3	28	.11	.047	15	9	.30	144	<.01	<3	1.32	.01	.07	<2	<.2	126	<.3	<.2	4.3	1
STANDARD D2/C3/AU-S	22.8	118.0	102.7	263.8	1840	31	18	1026	4.62	72.9	24	21	62	1.82	8.3	17.4	74	.71	.109	19	60	1.15	251	.12	33	2.49	.05	.71	12	2.2	978	.3	1.9	6.7	49

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L17+50N 14+00E	3.5	21.3	63.3	97.1	192	7	7	730	2.02	9.8	<5	<2	14	.36	5.8	.3	31	.15	.105	18	10	.38	178	.01	<3	1.54	.01	.09	<2	<.2	239	<.3	<.2	3.8	1
L17+00N 8+00E	4.4	15.4	36.3	86.4	32	10	6	639	2.01	13.6	<5	5	13	.39	8.6	.2	32	.19	.066	21	15	.29	115	.02	<3	.94	.01	.07	<2	<.2	62	<.3	<.2	3.0	2
L17+00N 8+25E	4.3	13.0	35.4	78.6	58	8	5	519	1.86	12.3	<5	3	10	.31	8.7	.2	28	.16	.064	19	13	.28	112	.01	<3	.97	.01	.07	<2	<.2	38	<.3	<.2	3.0	1
L17+00N 8+50E	5.3	14.8	43.7	91.8	76	8	5	435	2.02	12.1	<5	4	13	.24	10.3	.3	33	.22	.080	23	12	.30	101	.01	<3	1.04	.01	.08	<2	.2	69	<.3	<.2	3.4	1
L17+00N 8+75E	5.7	12.7	38.5	60.5	42	8	5	387	1.69	16.3	<5	<2	12	.24	7.4	.2	27	.17	.074	17	10	.25	100	.01	<3	.87	.01	.08	<2	<.2	62	<.3	<.2	3.3	17
L17+00N 9+00E	4.0	11.5	32.1	62.9	51	8	5	445	1.76	10.8	5	4	14	.37	7.6	.2	28	.21	.066	21	11	.24	117	.02	<3	.76	.01	.08	<2	<.2	45	<.3	<.2	2.7	4
L17+00N 9+25E	4.8	12.7	35.6	69.5	104	9	5	453	1.93	12.4	<5	3	15	.29	7.9	.2	31	.20	.064	21	16	.29	132	.02	<3	.99	.01	.09	<2	.2	78	<.3	<.2	3.5	2
L17+00N 9+50E	6.2	14.1	30.9	81.0	112	10	6	453	1.96	12.7	<5	2	20	.24	10.2	.2	30	.27	.078	18	10	.30	143	.01	<3	.95	.01	.09	<2	<.2	67	<.3	<.2	3.4	2
L17+00N 9+75E	7.1	12.6	31.4	84.5	239	10	5	408	1.93	13.8	<5	2	16	.29	6.8	.3	29	.13	.093	27	13	.27	201	<.01	<3	1.52	.01	.08	<2	.3	64	<.3	<.2	4.0	19
L17+00N 10+00E	3.8	14.5	31.3	82.8	69	11	7	803	1.96	9.6	<5	<2	10	.33	5.4	.2	29	.14	.114	15	16	.31	80	.01	<3	1.52	.01	.07	<2	<.2	19	.3	<.2	4.3	2
L17+00N 10+25E	3.8	10.4	23.6	43.4	134	6	4	211	1.50	10.7	6	3	8	.20	5.7	.2	26	.09	.033	11	13	.19	67	.01	<3	.98	.01	.05	<2	<.2	32	<.3	<.2	3.3	2
L17+00N 10+50E	4.5	13.4	31.4	62.7	62	7	5	438	2.00	13.0	<5	3	10	.22	9.6	.2	30	.09	.037	20	13	.24	73	.01	<3	.99	.01	.09	<2	<.2	67	<.3	<.2	3.3	37
L17+00N 10+75E	8.8	15.7	46.1	96.2	274	11	6	793	1.96	13.4	7	4	10	.59	11.9	.3	23	.10	.072	28	10	.15	338	<.01	<3	1.32	<.01	.11	<2	.2	64	<.3	<.2	3.4	420
L17+00N 11+00E	7.1	70.2	38.1	74.4	95	5	6	2686	2.01	6.4	<5	6	24	.85	6.9	<.2	21	.36	.099	31	6	.20	613	<.01	<3	.87	.01	.14	<2	.2	40	<.3	<.2	3.0	19
L17+00N 11+25E	5.5	12.1	83.4	97.1	198	6	4	573	1.77	19.7	<5	3	8	.49	9.4	.5	15	.12	.054	23	4	.17	102	<.01	<3	.93	.01	.11	<2	<.2	36	<.3	<.2	2.4	26
L17+00N 11+50E	7.2	15.2	76.6	88.3	304	7	6	1303	2.06	19.8	5	3	14	.89	8.9	.4	29	.08	.039	16	11	.20	131	.01	<3	1.14	.01	.11	<2	.2	109	<.3	<.2	4.3	4
L17+00N 11+75E	10.2	21.0	73.8	63.8	137	6	4	680	1.43	30.3	<5	4	5	.78	5.7	.3	3	.04	.025	27	4	.02	149	<.01	<3	.35	.01	.10	<2	<.2	26	<.3	.2	1.2	17
RE L17+00N 11+75E	9.5	18.9	71.9	61.5	159	5	4	655	1.38	30.4	6	4	5	.74	5.4	.3	3	.04	.024	27	4	.02	143	<.01	<3	.34	.01	.10	<2	<.2	32	.3	.2	1.2	52
L17+00N 12+00E	4.6	32.4	24.4	91.4	70	4	4	357	2.36	12.7	<5	3	7	.38	9.4	.2	22	.04	.034	26	6	.07	82	<.01	<3	.89	.01	.12	<2	<.2	25	<.3	<.2	3.4	6
L17+00N 12+25E	1.4	62.1	40.8	67.1	47	3	4	1602	2.30	4.4	<5	5	24	.35	7.9	<.2	26	.38	.098	31	5	.29	414	<.01	<3	.97	.01	.20	<2	<.2	20	<.3	<.2	3.0	3
L17+00N 12+50E	3.8	21.1	48.5	81.0	196	9	6	830	3.05	11.5	8	2	21	.61	6.4	.3	49	.19	.076	28	16	.34	577	.01	<3	2.11	.01	.08	<2	.2	42	<.3	<.2	7.6	2
L17+00N 12+75E	.3	3.7	11.1	55.8	38	2	4	1297	1.90	2.3	<5	2	8	.17	1.8	<.2	8	.26	.053	21	2	.04	875	<.01	<3	1.00	<.01	.13	<2	<.2	<10	<.3	<.2	1.7	2
L17+00N 13+00E	1.2	7.9	23.0	61.3	<30	8	7	579	2.76	7.8	<5	7	13	.24	22.8	<.2	41	.18	.073	17	18	.46	190	<.01	<3	1.93	.01	.09	<2	.2	39	<.3	<.2	5.4	1
L17+00N 13+25E	42.9	2.2	264.4	7.2	1654	1	1	8	2.57	18.0	<5	5	76	.06	6.6	6.2	3	.03	.039	16	2	.01	340	<.01	<3	.26	.03	.47	<2	<.2	97	.5	.2	1.4	7
L17+00N 13+50E	2.9	17.2	32.5	96.4	177	9	11	801	3.57	10.4	<5	3	16	.27	25.8	.2	55	.18	.061	19	17	.62	263	<.01	<3	1.79	.01	.10	<2	<.2	149	<.3	<.2	5.9	<1
L17+00N 13+75E	6.0	15.4	37.8	79.6	137	7	6	558	2.54	18.4	<5	2	18	.50	12.6	.5	36	.07	.024	17	13	.34	122	.01	<3	1.24	.01	.11	<2	<.2	163	<.3	<.2	4.7	2
L17+00N 14+00E	3.8	36.5	74.0	116.0	45	10	11	740	3.20	20.5	<5	8	14	.43	9.8	.6	49	.16	.048	20	16	.66	335	.01	<3	2.43	.01	.13	<2	.2	137	<.3	<.2	6.2	2
L16+50N 8+00E	5.7	13.2	45.7	72.6	181	9	8	2041	2.01	15.0	<5	3	11	.81	8.2	.3	30	.11	.046	16	13	.18	132	.01	<3	1.08	.01	.10	<2	<.2	80	.3	<.2	3.5	2
L16+50N 8+25E	3.6	7.6	33.7	48.5	96	4	4	344	1.33	17.6	<5	6	18	.23	4.0	.3	16	.57	.116	29	9	.09	135	<.01	<3	.92	.01	.23	<2	<.2	37	<.3	<.2	2.6	3
L16+50N 8+50E	5.4	11.8	26.9	75.0	171	12	5	397	1.83	11.9	7	3	23	.18	8.1	.2	24	.22	.028	13	11	.33	407	<.01	<3	.95	.01	.08	<2	<.2	82	<.3	<.2	3.0	1
L16+50N 8+75E	7.5	14.2	29.9	75.4	81	13	6	458	2.02	17.6	<5	<2	13	.27	12.5	.3	31	.12	.046	15	15	.31	100	.01	<3	.97	.01	.06	<2	<.2	110	<.3	<.2	3.3	2
L16+50N 9+00E	6.1	13.9	32.2	62.7	76	10	5	366	1.81	14.0	<5	3	11	.21	9.5	.2	26	.11	.043	19	13	.21	93	.01	<3	.82	.01	.07	<2	<.2	53	<.3	<.2	2.9	2
L16+50N 9+25E	5.0	11.8	26.0	53.3	51	9	5	384	1.65	11.1	<5	4	13	.22	9.5	.2	26	.18	.060	19	13	.19	99	.02	<3	.56	.01	.06	<2	<.2	82	<.3	<.2	2.1	8
L16+50N 9+50E	7.8	11.3	24.0	57.4	133	8	4	269	1.68	12.5	5	<2	14	.16	8.6	.2	25	.10	.030	14	11	.23	186	.01	<3	.82	.01	.07	<2	<.2	120	<.3	<.2	3.0	1
STANDARD D2/C3/AU-S	23.8	121.4	103.0	264.0	1857	31	18	988	4.53	68.9	18	20	59	1.93	8.8	15.9	73	.71	.107	18	55	1.12	265	.11	31	2.44	.05	.70	14	2.1	933	.5	1.8	6.6	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Data ___ FA ____

ACME ANALYTICAL

Omni Resources Inc. PROJECT SINTER CAP/GODDELL FILE # 9803303 Page 5

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L16+50N 9+75E	8.6	14.1	35.9	68.5	148	8	6	428	1.89	15.3	7	4	13	.30	14.3	.3	23	.12	.043	19	9	.15	99	.01	<3	.74	.01	.09	<2	.2	96	<.3	<.2	2.4	3
L16+50N 10+00E	7.7	11.7	31.1	60.4	98	9	5	321	1.91	13.4	<5	4	10	.28	17.4	.2	27	.13	.055	15	9	.22	89	.01	<3	.76	.01	.07	<2	<.2	57	<.3	<.2	3.1	5
L16+50N 10+25E	4.7	13.1	28.7	60.9	95	8	6	680	1.85	10.1	<5	3	6	.36	10.8	.2	21	.07	.052	24	8	.14	123	.01	<3	.81	.01	.08	<2	.2	59	<.3	<.2	2.4	45
L16+50N 10+50E	4.6	11.3	28.2	55.5	79	10	6	567	1.77	9.9	<5	5	12	.35	9.3	.2	26	.20	.070	17	10	.22	140	.02	<3	.62	.01	.06	<2	<.2	63	<.3	<.2	2.6	2
L16+50N 10+75E	8.4	10.1	38.7	51.3	238	8	4	411	1.18	11.3	<5	2	5	.30	5.0	.2	16	.06	.038	14	4	.12	62	.01	<3	.56	<.01	.05	<2	.2	29	<.3	<.2	2.3	124
L16+50N 11+00E	5.4	5.9	48.0	45.8	135	7	1	267	.93	27.7	<5	11	5	.22	2.5	<.2	4	.04	.012	32	3	.04	62	<.01	<3	.47	<.01	.15	<2	.2	28	<.3	<.2	1.5	11
L16+50N 11+25E	9.5	8.7	42.0	59.5	190	7	3	434	1.16	17.2	<5	2	6	.44	4.6	<.2	12	.06	.024	27	3	.07	101	<.01	<3	.45	<.01	.07	<2	.2	33	<.3	<.2	1.7	40
L16+50N 11+50E	13.2	37.9	341.0	132.7	340	10	6	1199	1.81	21.3	<5	4	14	.71	11.7	.7	8	.15	.048	41	3	.04	403	<.01	<3	.86	.01	.17	<2	.3	59	<.3	.2	1.8	6
L16+50N 11+75E	3.7	7.6	23.3	73.7	50	3	1	125	1.54	12.7	<5	3	4	.36	4.4	.2	5	.03	.020	27	4	.02	118	<.01	<3	.65	.01	.12	<2	.2	19	<.3	<.2	1.7	2
L16+50N 12+00E	4.1	18.7	60.1	95.4	200	4	5	676	2.24	13.5	6	3	16	.40	9.1	.3	19	.16	.109	34	2	.11	330	<.01	<3	1.07	.01	.15	3	.2	161	<.3	<.2	2.7	7
L16+50N 12+25E	3.8	13.6	67.0	74.1	70	5	6	662	2.23	18.8	<5	4	8	.32	21.9	.4	25	.14	.054	19	7	.25	123	<.01	<3	.97	.01	.11	2	<.2	30	<.3	<.2	3.2	<1
L16+50N 12+50E	1.7	17.0	28.7	75.9	51	9	9	771	3.06	15.3	<5	4	21	.19	33.5	.2	48	.22	.045	17	16	.71	319	<.01	<3	2.03	.01	.07	<2	.2	252	<.3	<.2	6.7	2
RE L16+50N 12+50E	1.6	18.5	27.9	79.8	35	9	9	805	3.23	16.8	<5	4	23	.16	34.9	.2	51	.24	.047	18	13	.75	334	<.01	<3	2.18	.01	.08	<2	.2	225	<.3	<.2	6.9	1
L16+50N 12+75E	2.8	13.7	39.3	68.5	106	7	5	401	2.67	17.1	<5	4	13	.31	12.2	.3	36	.12	.043	17	11	.33	125	<.01	<3	1.63	.01	.09	<2	.3	60	<.3	<.2	6.1	1
L16+50N 13+00E	2.6	13.9	41.9	82.3	49	9	8	585	2.77	21.0	<5	2	13	.32	9.3	.2	43	.19	.074	14	11	.44	172	<.01	<3	1.80	.01	.09	<2	.2	70	<.3	<.2	5.0	1
L16+50N 13+25E	2.4	15.9	46.2	87.8	74	10	9	614	2.70	19.3	<5	4	12	.25	8.4	.3	40	.19	.082	15	14	.48	102	<.01	<3	2.18	.01	.10	<2	<.2	111	<.3	<.2	4.7	1
L16+50N 13+50E	4.5	15.7	48.3	83.3	114	9	6	467	2.50	16.8	9	2	13	.30	7.7	.4	36	.13	.084	14	14	.33	151	.01	<3	1.70	.01	.10	<2	.2	103	<.3	<.2	5.8	3
L16+50N 13+75E	4.3	19.7	55.1	83.1	469	9	8	508	2.78	26.2	<5	3	21	.49	8.4	.3	38	.19	.042	14	12	.39	217	.01	<3	1.52	.01	.10	<2	<.2	131	<.3	<.2	4.8	1
L16+50N 14+00E	4.6	22.2	63.0	91.5	360	9	7	491	2.68	22.5	<5	4	14	.50	7.4	.5	37	.11	.036	14	13	.39	161	.01	<3	1.62	.01	.10	<2	<.2	130	<.3	<.2	4.8	1
L16+00N 8+00E	4.3	10.9	52.9	125.2	99	8	9	576	2.19	14.9	<5	6	6	.46	4.5	.5	23	.18	.095	21	8	.19	88	<.01	<3	1.33	.01	.11	<2	.2	43	<.3	<.2	3.0	3
L16+00N 8+25E	4.8	12.6	22.6	60.5	93	9	6	513	1.92	17.7	<5	2	11	.26	6.5	.2	31	.15	.066	15	13	.25	86	.02	<3	.80	.01	.06	<2	<.2	64	<.3	<.2	2.9	14
L16+00N 8+50E	8.8	11.7	43.0	108.4	349	13	10	914	2.30	12.7	<5	3	25	.11	8.4	.5	27	.25	.063	37	9	.32	576	<.01	<3	1.31	.01	.10	<2	.2	86	<.3	<.2	3.9	2
L16+00N 8+75E	7.6	10.9	35.9	61.6	144	10	6	583	1.67	11.4	<5	3	15	.09	9.3	.3	26	.19	.065	22	8	.25	105	.01	<3	.90	.01	.08	<2	<.2	77	<.3	<.2	3.3	5
L16+00N 9+00E	7.7	10.2	31.7	65.0	207	7	3	439	1.64	7.8	<5	<2	15	.15	7.0	.3	25	.13	.056	15	6	.17	123	.01	<3	.80	.01	.07	<2	<.2	48	<.3	<.2	3.0	5
L16+00N 9+25E	10.8	19.0	42.7	78.3	236	11	5	484	1.89	21.9	<5	<2	17	.45	10.4	.4	20	.12	.084	17	9	.13	189	<.01	<3	.97	.01	.09	<2	.2	67	<.3	<.2	3.5	2
L16+00N 9+50E	10.3	16.5	55.6	81.0	271	12	9	863	2.20	18.2	<5	2	11	.44	9.0	.3	27	.11	.068	14	14	.20	111	<.01	<3	1.01	.01	.08	<2	<.2	85	<.3	<.2	3.2	2
L16+00N 9+75E	6.4	10.3	32.8	57.4	58	9	4	442	1.38	9.3	5	3	6	.30	4.9	.2	16	.05	.026	18	8	.10	86	<.01	<3	.60	.01	.10	<2	<.2	40	<.3	<.2	2.1	4
L16+00N 10+00E	4.1	9.7	29.1	47.7	66	11	4	376	1.21	9.7	<5	3	6	.15	4.0	<.2	16	.06	.027	13	3	.14	69	.01	<3	.63	.01	.09	<2	<.2	31	<.3	<.2	2.1	2
L16+00N 10+25E	6.5	15.4	52.9	71.1	183	12	7	1218	1.60	10.3	<5	3	6	.73	3.5	.3	15	.08	.055	31	3	.05	168	<.01	<3	.64	.01	.15	<2	<.2	61	<.3	<.2	1.3	4
L16+00N 10+50E	7.9	12.0	25.3	65.6	114	10	3	263	1.66	16.5	<5	<2	7	.20	4.6	.2	23	.05	.035	19	6	.11	83	.01	<3	.91	.01	.08	<2	<.2	36	<.3	<.2	2.7	4
L16+00N 10+75E	10.2	9.9	57.1	97.6	139	7	1	516	1.60	31.8	<5	5	3	.33	3.2	<.2	3	.03	.027	93	<1	.02	91	<.01	<3	.43	<.01	.10	<2	<.2	33	<.3	<.2	1.1	11
L16+00N 11+00E	10.1	4.4	51.1	50.6	78	3	1	319	.82	24.9	<5	10	4	.20	2.8	<.2	1	.04	.013	36	<1	.01	89	<.01	<3	.36	<.01	.13	<2	<.2	30	<.3	<.2	.9	5
L16+00N 11+25E	6.2	17.4	35.6	130.2	177	8	5	1049	2.20	13.6	<5	<2	8	.35	5.4	.3	19	.06	.108	20	2	.14	175	<.01	<3	.97	.01	.10	<2	<.2	51	<.3	<.2	2.3	2
L16+00N 11+50E	7.2	14.7	105.9	110.9	202	5	6	680	2.23	24.9	<5	2	10	.33	8.2	.5	21	.12	.090	20	5	.21	158	<.01	<3	1.22	.01	.11	<2	<.2	47	<.3	<.2	3.0	8
STANDARD D2/C3/AU-S	22.9	121.5	105.9	268.1	1922	32	18	1038	4.60	73.0	19	21	59	1.92	8.6	17.3	74	.71	.108	18	56	1.14	279	.12	31	2.41	.05	.71	14	2.0	920	.3	1.8	6.7	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L16+00N 11+75E	5.8	12.4	77.7	105.1	84	5	6	680	2.04	24.2	<5	2	12	.47	10.3	.4	26	.11	.040	15	7	.29	158	<.01	<3	1.18	.01	.09	<2	.3	135	<.3	<.2	2.9	6
L16+00N 12+00E	5.4	12.2	49.5	95.4	214	5	5	448	1.83	28.8	<5	<2	12	.80	9.0	.5	16	.10	.088	17	5	.18	127	<.01	<3	1.06	.01	.10	<2	.4	347	<.3	.2	2.9	<1
L16+00N 12+25E	.6	2.5	18.2	4.3	82	<1	<1	29	1.01	7.0	<5	3	12	.08	1.3	<.2	2	.02	.027	23	<1	.01	168	<.01	<3	.35	.01	.21	<2	.2	<10	<.3	<.2	.8	<1
L16+00N 12+50E	1.5	4.5	35.7	12.7	93	2	3	240	1.96	24.4	<5	<2	25	.06	3.4	<.2	4	.06	.026	8	<1	.02	657	<.01	<3	.49	<.01	.16	<2	.2	50	<.3	<.2	1.1	<1
L16+00N 12+75E	2.1	12.1	39.9	79.6	48	5	7	855	3.19	21.6	<5	4	10	.14	22.2	<.2	39	.12	.055	18	8	.41	162	<.01	<3	1.96	.01	.15	<2	.2	45	<.3	<.2	4.2	<1
L16+00N 13+00E	4.3	18.8	70.9	97.5	270	6	7	1066	2.32	24.1	<5	<2	17	.78	9.4	.4	29	.15	.081	17	8	.23	325	.01	<3	1.29	.01	.17	<2	.2	127	<.3	<.2	3.4	3
L16+00N 13+25E	2.9	19.3	55.7	84.7	177	8	11	2339	2.77	18.3	<5	2	17	.51	12.2	.2	38	.17	.111	28	12	.25	527	<.01	<3	1.63	.01	.17	<2	.2	110	<.3	<.2	4.4	3
L16+00N 13+50E	2.2	20.2	55.7	99.9	126	11	10	946	2.98	17.2	<5	3	17	.27	8.4	.3	45	.16	.086	20	12	.50	313	<.01	<3	1.97	.01	.16	<2	.2	107	<.3	<.2	4.4	1
L16+00N 13+75E	2.6	18.1	52.0	79.5	182	10	9	801	2.55	20.5	<5	<2	21	.36	10.4	.2	37	.25	.092	14	13	.45	154	.01	<3	1.45	.01	.18	<2	.2	56	<.3	<.2	4.3	1
L16+00N 14+00E	1.1	11.9	49.5	50.0	141	5	4	685	1.50	9.7	8	2	38	.22	5.4	.2	18	.43	.045	18	5	.29	399	<.01	<3	1.30	.01	.11	<2	.2	138	<.3	<.2	3.1	1
RE L16+00N 14+00E	1.2	12.2	46.6	48.6	147	4	4	687	1.43	11.1	7	<2	36	.22	5.6	.2	18	.42	.045	18	4	.28	400	<.01	<3	1.23	.01	.10	<2	.2	124	<.3	<.2	3.0	1
L15+50N 8+00E	11.1	15.5	27.5	77.3	109	10	4	401	2.28	15.2	<5	2	18	.11	10.8	.3	31	.13	.099	28	10	.12	354	<.01	<3	1.49	.01	.06	<2	.3	115	<.3	<.2	3.1	1
L15+50N 8+25E	12.7	14.8	45.3	87.4	423	14	9	961	2.28	12.2	<5	<2	25	.23	11.2	.3	27	.24	.079	32	8	.18	372	<.01	<3	1.04	.01	.09	<2	.2	173	<.3	<.2	3.2	8
L15+50N 8+50E	8.5	12.4	37.5	104.3	165	10	5	591	2.29	13.0	<5	<2	31	.16	11.2	.4	26	.27	.076	19	7	.19	452	<.01	<3	1.13	.01	.09	<2	.4	45	<.3	<.2	3.5	2
L15+50N 8+75E	7.4	14.5	36.5	89.3	47	12	7	568	2.27	20.6	<5	4	11	.62	12.6	.3	34	.13	.062	15	10	.29	76	.01	<3	1.11	.01	.06	<2	.2	78	<.3	<.2	3.3	1
L15+50N 9+00E	6.6	12.1	40.8	55.3	71	9	5	421	1.92	12.6	<5	4	11	.25	13.5	.3	29	.14	.050	20	8	.20	87	.01	<3	.66	.01	.05	<2	.2	41	<.3	<.2	2.8	10
L15+50N 9+25E	5.7	11.7	29.2	61.0	74	12	6	346	2.03	19.9	<5	3	8	.23	8.0	.3	30	.09	.038	14	9	.25	62	.01	<3	1.01	.01	.06	<2	.2	43	<.3	<.2	2.8	12
L15+50N 9+50E	7.6	13.3	63.8	124.7	105	14	10	667	2.37	8.3	<5	5	7	.35	4.4	.6	25	.10	.061	14	8	.20	79	.01	<3	1.18	.01	.09	<2	.3	39	<.3	<.2	3.4	5
L15+50N 9+75E	40.1	30.0	88.5	135.1	798	11	5	570	2.28	12.5	<5	3	5	.40	5.1	.9	11	.06	.104	17	4	.07	103	<.01	<3	.84	.01	.11	<2	.2	89	.3	.3	2.4	7
L15+50N 10+00E	6.1	13.9	50.4	69.1	204	16	8	569	1.74	12.9	<5	3	7	.36	5.7	.3	21	.08	.042	15	8	.18	71	.01	<3	.78	.01	.06	<2	<.2	50	<.3	<.2	1.9	2
L15+50N 10+25E	25.6	10.6	56.7	74.5	212	8	3	536	1.46	17.9	<5	5	7	.37	6.9	.2	12	.06	.024	36	5	.06	106	.01	<3	.41	<.01	.12	<2	.2	32	<.3	<.2	1.6	60
L15+50N 10+50E	5.1	13.3	44.6	77.3	124	8	5	397	2.21	13.0	<5	4	5	.38	10.2	.3	21	.04	.023	23	9	.16	99	<.01	<3	.94	.01	.11	<2	.3	24	<.3	<.2	2.5	6
L15+50N 10+75E	5.2	19.1	42.4	117.8	217	10	4	671	2.20	14.4	<5	3	7	.25	5.3	.4	14	.05	.062	56	6	.11	214	<.01	<3	1.29	.01	.18	<2	.2	42	<.3	<.2	2.6	4
L15+50N 11+00E	3.1	18.5	55.6	82.7	60	6	8	725	2.36	19.5	<5	9	20	.23	8.3	.2	17	.08	.063	19	3	.25	88	<.01	<3	1.17	<.01	.14	<2	.3	27	<.3	<.2	2.3	2
L15+50N 11+25E	27.8	52.2	171.7	335.0	974	13	19	2287	2.34	30.6	<5	6	7	1.67	19.4	1.4	13	.18	.133	23	2	.10	372	<.01	<3	.85	<.01	.15	<2	2.0	52	<.3	.2	2.4	5
L15+50N 11+50E	5.6	20.2	133.6	294.5	1196	6	6	753	2.62	20.4	<5	3	21	.85	13.8	2.0	32	.40	.119	26	11	.26	692	<.01	<3	1.14	.01	.16	<2	.3	246	.3	.2	3.4	3
L15+50N 11+75E	5.3	13.1	52.1	94.2	83	5	5	545	2.27	19.1	<5	4	7	.30	10.5	.4	28	.05	.017	23	9	.30	91	<.01	<3	1.21	.01	.09	<2	.2	39	<.3	<.2	3.0	2
L15+50N 12+00E	4.8	12.6	68.6	60.3	168	4	4	313	1.69	48.9	<5	<2	14	.22	12.1	.3	17	.05	.019	15	5	.15	166	<.01	<3	.60	.01	.14	<2	.2	198	<.3	<.2	2.2	2
L15+50N 12+25E	4.5	11.8	76.7	91.7	277	5	5	592	2.05	20.7	<5	3	11	.31	9.7	.5	28	.10	.020	18	7	.35	303	<.01	<3	1.09	.01	.10	<2	<.2	47	<.3	<.2	3.0	1
L15+50N 12+50E	6.0	23.1	142.7	165.6	905	8	6	697	2.78	57.0	<5	2	16	1.21	12.2	.7	35	.13	.066	14	10	.33	219	.01	<3	1.31	.01	.17	<2	.2	225	.3	<.2	4.3	<1
L15+50N 12+75E	4.6	23.7	78.5	111.5	352	8	8	1492	2.60	33.2	<5	<2	18	.80	12.4	.3	29	.07	.083	18	11	.20	557	<.01	<3	1.28	.01	.19	<2	.2	73	.3	<.2	3.5	1
L15+50N 13+00E	3.5	20.1	38.7	131.1	295	8	7	1648	2.91	19.3	<5	<2	27	1.35	13.5	.3	34	.23	.110	19	11	.26	548	<.01	<3	1.17	.01	.24	2	.2	39	<.3	.2	3.9	1
L15+50N 13+25E	5.1	20.5	62.5	184.3	229	9	11	4520	2.37	18.3	<5	<2	27	2.42	6.6	.3	25	.30	.125	23	8	.24	861	.01	<3	1.12	.01	.27	<2	<.2	60	<.3	<.2	3.3	<1
L15+50N 13+50E	4.4	27.5	73.2	143.7	386	13	12	1835	3.01	31.1	<5	4	29	2.07	10.1	.4	42	.38	.111	26	16	.47	541	.01	<3	1.45	.01	.28	<2	.2	63	.3	<.2	4.8	<1
STANDARD D2/C3/AU-S	23.5	118.8	104.1	263.7	1908	31	17	1032	4.56	73.9	26	20	59	1.92	8.8	17.3	72	.70	.108	18	57	1.11	278	.12	29	2.40	.05	.71	13	2.1	929	.4	1.9	6.4	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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Data___ FA ____

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L15+50N 13+75E	3.2	25.8	91.1	164.5	235	11	13	1818	3.15	14.8	<5	5	33	2.23	12.2	.4	45	.55	.125	28	14	.49	589	.01	<3	1.64	.01	.30	<2	.2	107	<.3	<.2	4.6	<1
L15+50N 14+00E	2.9	24.9	83.9	132.7	259	9	10	1303	2.67	14.2	<5	2	25	1.51	12.0	.4	40	.35	.091	23	13	.43	526	.01	<3	1.36	.01	.24	2	.3	100	<.3	<.2	4.1	2
L15+00N 3+50E	6.5	13.9	13.5	36.7	70	12	6	275	1.67	13.0	<5	2	13	.26	6.6	.2	30	.13	.051	11	16	.23	75	.03	<3	.72	.01	.04	<2	.2	97	.3	<.2	2.2	2
L15+00N 3+75E	8.6	15.9	12.2	36.9	138	10	5	247	1.67	18.6	<5	<2	13	.21	7.8	.2	28	.11	.050	10	15	.20	66	.03	<3	.67	.01	.05	<2	<.2	135	.3	.2	2.2	1
L15+00N 4+00E	9.6	17.3	19.8	45.0	227	11	6	296	1.76	32.1	6	2	17	.20	9.3	.5	30	.12	.056	11	18	.25	108	.02	<3	.79	.01	.06	<2	.3	143	.4	.3	2.4	3
L15+00N 4+25E	8.5	20.5	20.6	49.5	211	10	7	479	1.87	37.8	9	2	18	.32	9.5	.3	30	.16	.068	13	14	.25	176	.02	<3	.74	.01	.07	<2	.2	192	.3	.2	2.3	7
L15+00N 4+50E	8.8	27.1	36.8	64.1	404	11	7	453	1.97	25.9	11	2	19	.32	9.2	.4	29	.14	.080	16	16	.26	182	.01	<3	.85	.01	.10	<2	.3	215	.5	.2	2.6	7
L15+00N 4+75E	8.7	17.1	18.2	47.7	148	10	5	372	1.69	19.2	8	<2	15	.23	8.4	.3	26	.11	.053	11	14	.22	126	.02	<3	.65	.01	.06	<2	.3	131	.3	.2	2.0	2
L14+50N 3+50E	6.0	15.7	16.9	49.1	106	13	7	332	1.94	15.3	<5	<2	13	.32	6.9	.3	36	.14	.054	15	16	.30	87	.03	<3	.89	.01	.04	<2	<.2	206	<.3	<.2	2.5	4
L14+50N 3+75E	8.6	14.1	14.8	33.6	94	10	5	179	1.63	20.3	<5	2	10	.16	7.8	.2	29	.08	.030	10	16	.16	49	.03	<3	.63	.01	.03	<2	.2	116	.3	.2	2.3	3
L14+50N 4+00E	11.7	15.0	16.3	30.0	167	8	4	152	1.71	24.8	8	<2	11	.15	9.1	.4	30	.06	.021	11	13	.13	84	.02	<3	.62	.01	.03	<2	.3	136	.4	.3	2.4	1
L14+50N 4+25E	9.3	16.0	15.5	40.9	116	10	5	213	1.61	17.4	8	2	13	.19	8.6	.3	26	.11	.041	10	11	.20	76	.02	<3	.56	.01	.04	<2	.2	176	.4	.2	1.8	2
L14+50N 4+50E	7.8	12.9	10.5	26.9	32	7	3	169	1.33	14.6	6	<2	8	.11	7.5	.2	22	.04	.028	7	14	.13	47	.01	<3	.43	.01	.03	<2	<.2	133	.3	.2	1.6	1
L14+50N 4+75E	10.4	27.0	29.5	61.7	360	13	6	328	2.22	31.9	<5	2	23	.17	8.8	.5	35	.14	.080	15	20	.35	119	.02	<3	1.22	.02	.11	<2	.3	163	.5	.2	3.3	1
L14+00N 3+50E	13.0	17.8	14.6	43.6	121	12	6	253	1.78	18.6	<5	<2	13	.21	8.0	.3	30	.08	.033	12	15	.22	61	.03	<3	.71	.01	.04	<2	.2	161	.3	.2	2.1	1
L14+00N 3+75E	12.4	18.1	14.7	35.2	123	8	4	195	1.60	23.3	5	<2	13	.23	9.7	.3	25	.06	.033	7	15	.17	51	.02	<3	.61	.01	.04	<2	.2	115	.4	.2	2.5	2
RE L14+00N 3+75E	12.3	17.5	13.1	34.2	72	9	4	189	1.58	20.6	<5	<2	12	.18	9.7	.3	24	.05	.034	7	13	.17	50	.01	<3	.60	.01	.04	<2	.2	122	.4	.2	2.3	2
L14+00N 4+00E	11.8	17.1	10.5	31.9	63	9	4	197	1.72	20.6	<5	2	14	.14	8.4	.3	28	.11	.035	12	19	.19	62	.03	<3	.61	.01	.04	<2	.2	146	.3	.2	1.9	2
L14+00N 4+25E	9.2	13.5	10.3	26.6	80	8	3	128	1.41	20.1	<5	<2	11	.12	7.5	.2	25	.05	.033	8	13	.14	57	.01	<3	.56	.01	.03	<2	.2	105	.3	.2	2.1	2
L14+00N 4+50E	7.9	12.6	9.0	37.9	71	10	5	200	1.51	19.4	<5	<2	13	.12	5.9	<.2	27	.08	.034	9	13	.19	67	.03	<3	.65	.01	.04	<2	<.2	101	<.3	<.2	1.8	2
L14+00N 4+75E	9.2	12.9	11.9	39.1	82	10	5	250	1.48	22.8	5	<2	17	.13	5.8	.3	27	.08	.038	8	15	.18	129	.01	<3	.67	.01	.04	<2	<.2	86	<.3	<.2	2.1	<1
L13+50N 3+50E	13.1	19.8	19.9	54.5	115	16	7	288	2.15	32.2	<5	4	25	.27	10.2	.3	37	.20	.071	18	24	.26	69	.05	<3	.81	.01	.06	<2	.2	302	<.3	<.2	2.6	9
L13+50N 3+75E	8.3	16.5	14.7	47.7	72	14	6	279	1.78	26.0	<5	2	20	.26	7.5	.2	30	.17	.063	11	22	.24	87	.04	<3	.62	.01	.05	<2	<.2	257	<.3	<.2	1.9	1
L13+50N 4+00E	16.7	19.3	32.1	47.3	195	13	5	261	2.03	33.6	6	<2	19	.25	9.4	.6	34	.05	.059	9	18	.19	120	.01	<3	.85	.01	.06	<2	.2	142	.3	.2	3.5	1
L13+50N 4+25E	10.0	14.7	21.0	41.6	93	12	5	207	1.51	18.9	<5	<2	14	.20	6.1	.3	25	.08	.036	7	13	.22	73	.02	<3	.68	.01	.05	<2	.2	95	<.3	.2	1.9	1
L13+50N 4+50E	8.3	12.7	14.8	37.8	79	11	5	202	1.67	20.6	<5	<2	13	.17	6.3	.3	30	.08	.026	12	18	.20	59	.03	<3	.62	.01	.04	<2	<.2	103	<.3	<.2	1.8	3
L13+50N 4+75E	9.8	14.3	18.1	42.3	105	13	5	193	1.76	26.2	<5	<2	15	.18	7.2	.3	31	.07	.028	11	15	.16	56	.02	<3	.68	.01	.04	<2	.2	158	<.3	<.2	2.2	4
L13+00N 3+50E	12.0	15.2	12.6	42.9	97	13	6	269	1.87	27.3	<5	<2	14	.20	6.8	.2	32	.12	.049	11	17	.27	72	.03	<3	.88	.01	.05	<2	<.2	115	<.3	<.2	2.9	1
L13+00N 3+75E	16.2	18.6	14.9	46.1	89	15	7	317	2.09	34.9	9	2	14	.19	7.8	.3	33	.12	.052	12	20	.30	76	.03	<3	.89	.01	.05	<2	<.2	241	<.3	<.2	2.7	5
L13+00N 4+00E	12.5	15.9	13.4	40.9	104	14	6	243	1.74	29.6	<5	<2	11	.21	7.7	.2	28	.09	.040	10	15	.23	63	.02	<3	.73	.01	.04	<2	<.2	150	<.3	<.2	2.4	2
L13+00N 4+25E	13.8	17.0	15.3	52.4	65	17	5	231	1.90	28.2	<5	3	16	.28	8.6	.3	30	.09	.040	14	16	.17	66	.02	<3	.60	.01	.05	<2	.2	271	<.3	<.2	2.2	<1
L13+00N 4+50E	17.8	20.2	16.8	65.7	117	19	7	329	2.33	36.1	<5	<2	16	.22	7.2	.3	36	.05	.051	10	17	.21	98	.01	<3	.91	.01	.07	<2	.2	147	<.3	<.2	3.0	<1
L13+00N 4+75E	10.5	15.5	18.5	47.1	112	15	6	237	1.82	24.5	<5	<2	14	.21	6.7	.2	31	.07	.033	12	16	.20	55	.02	<3	.74	.01	.05	<2	<.2	169	<.3	<.2	2.0	2
L12+50N 3+50E	7.8	21.9	20.1	53.9	126	11	6	307	2.05	24.2	<5	<2	12	.31	8.5	.3	28	.09	.079	13	15	.33	86	.01	<3	1.11	.01	.05	<2	.2	216	.3	<.2	3.1	1
STANDARD D2/C3/A	21.9	117.4	96.4	259.9	1908	31	17	997	4.51	67.9	19	19	61	1.96	8.9	19.7	73	.69	.105	18	55	1.11	232	.12	28	2.39	.05	.69	13	2.1	980	.5	2.1	6.5	51

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ____

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Tl	Hg	Se	Te	Ga	Au+
	ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppb	ppm	ppm	ppm	ppb
L12+50N 3+75E	19.0	38.2	37.2	127.3	278	19	11	585	2.87	26.8	<5	4	19	.45	14.8	.4	34	.12	.066	23	13	.30	104	.02	<3	.94	.01	.05	<2	.3	440	.6	.2	3.3	2
L12+50N 4+00E	18.6	25.6	20.0	79.3	170	14	7	323	2.30	31.3	<5	<2	20	.31	10.8	.4	31	.08	.071	14	10	.21	159	.01	<3	.78	.01	.06	<2	.2	191	.5	<.2	3.2	2
L12+50N 4+25E	13.7	19.1	12.3	52.2	77	10	6	293	1.55	20.1	<5	4	13	.21	8.5	<.2	21	.09	.035	14	7	.18	87	.02	<3	.50	.01	.03	<2	.2	293	.4	<.2	2.1	2
L12+50N 4+50E	14.3	15.0	9.8	45.9	90	9	4	187	1.51	23.0	<5	<2	11	.11	6.6	<.2	24	.04	.027	9	8	.16	40	.01	<3	.62	.01	.03	<2	<.2	84	.3	<.2	2.1	1
L12+50N 4+75E	21.9	22.7	15.5	64.8	140	14	7	264	1.72	33.5	<5	4	14	.38	10.6	.2	23	.10	.041	10	7	.16	89	.02	<3	.49	.01	.04	<2	<.2	214	.4	.2	2.1	2
L12+00N 3+50E	15.4	13.0	7.5	35.4	57	12	5	186	1.40	82.6	<5	<2	13	.09	5.8	.2	24	.05	.021	8	9	.17	65	.02	<3	.60	.01	.05	<2	.2	245	<.3	<.2	1.5	2
L12+00N 3+75E	10.6	24.0	12.7	55.9	79	15	8	355	2.34	45.3	<5	<2	11	.11	13.9	<.2	33	.06	.034	12	11	.33	64	.01	<3	.86	.01	.04	<2	<.2	278	.3	<.2	2.7	3
L12+00N 4+00E	11.3	24.6	17.4	55.5	137	12	6	303	2.05	25.0	<5	3	13	.09	11.1	.3	29	.09	.045	18	11	.37	89	.01	<3	.89	.01	.04	<2	<.2	262	.3	<.2	2.6	2
L12+00N 4+25E	7.1	30.8	17.0	70.8	52	16	8	404	2.29	36.7	<5	2	12	.20	17.2	.2	36	.08	.051	13	15	.45	172	.01	<3	.93	.01	.05	<2	<.2	454	<.3	<.2	3.4	3
L12+00N 4+50E	12.1	26.4	20.7	72.4	198	17	7	365	2.47	80.8	<5	<2	32	.24	12.3	.6	33	.14	.166	20	14	.27	761	<.01	<3	1.47	.01	.10	<2	.2	882	<.3	<.2	2.5	3
L12+00N 4+75E	6.2	19.5	14.2	51.7	69	18	7	333	2.00	39.7	6	<2	16	.22	7.8	.2	35	.08	.081	13	19	.22	92	.01	<3	1.28	.01	.05	<2	.2	159	.4	<.2	3.2	1
L11+50N 3+50E	9.1	20.5	20.8	52.0	52	20	7	315	2.11	36.7	<5	2	15	.18	9.4	.2	33	.10	.047	12	21	.31	140	.02	<3	.75	.01	.04	<2	<.2	214	.4	.2	2.2	2
L11+50N 3+75E	8.3	26.7	18.0	65.0	99	32	10	402	2.40	45.5	<5	2	17	.21	9.9	.2	38	.09	.052	13	24	.37	118	.01	<3	1.14	.01	.05	<2	.2	235	.5	.2	3.1	1
L11+50N 4+00E	11.8	22.7	19.2	63.5	132	26	10	601	2.10	206.9	<5	4	21	.25	15.2	.3	24	.09	.041	12	12	.19	292	.01	<3	.61	.01	.07	<2	.2	1075	.3	.2	2.0	2
L11+50N 4+25E	20.0	22.6	21.7	71.6	248	17	8	437	2.36	199.2	<5	3	33	.34	30.4	.5	24	.13	.064	15	12	.21	298	.01	<3	.78	.01	.09	<2	.3	1926	.6	.3	2.6	3
L11+50N 4+75E	68.0	22.6	99.7	51.1	575	11	6	170	2.81	296.8	<5	3	34	.37	23.4	1.8	23	.06	.065	9	19	.14	161	.01	<3	.60	.01	.08	<2	.4	1202	1.1	.6	2.4	20
L11+00N 3+50E	20.5	20.9	80.0	59.5	185	18	7	307	2.19	34.3	<5	5	19	.35	9.4	.4	34	.13	.050	14	19	.31	97	.03	<3	.89	.01	.06	<2	<.2	198	.4	.3	2.7	3
L11+00N 3+75E	14.4	22.8	58.2	61.0	190	19	8	308	2.21	29.9	<5	4	16	.40	9.0	.4	36	.12	.052	15	23	.32	105	.02	<3	.99	.01	.05	<2	.2	149	.6	.4	3.5	5
L11+00N 4+00E	12.4	25.1	33.4	53.8	157	26	7	291	2.23	54.7	<5	<2	30	.24	8.6	.4	33	.08	.036	11	17	.27	109	.02	<3	.80	.01	.08	<2	.2	138	<.3	.3	3.0	13
L11+00N 4+25E	12.2	59.4	19.3	109.8	276	190	53	2569	5.53	54.2	<5	2	30	.88	18.1	<.2	57	.18	.103	16	23	.13	943	<.01	<3	.63	.01	.10	<2	.4	2371	.3	<.2	1.7	35
RE L11+00N 4+25E	11.7	58.8	18.1	106.7	264	186	52	2506	5.40	55.7	<5	2	30	.88	18.5	<.2	56	.17	.102	16	23	.13	899	<.01	<3	.63	.01	.10	<2	.4	2332	.3	<.2	1.5	23
L11+00N 4+50E	10.1	23.4	19.4	57.1	280	28	8	424	2.12	43.6	<5	<2	26	.23	8.6	.3	26	.10	.098	13	13	.17	283	<.01	<3	.76	.01	.08	<2	.2	228	.3	.2	2.6	3
L11+00N 4+75E	47.0	63.4	62.4	229.2	620	35	21	993	4.86	287.9	<5	2	50	1.19	35.1	1.6	33	.09	.122	8	8	.04	534	<.01	<3	.69	.01	.18	<2	.6	4664	1.4	.9	1.8	9
L10+50N 3+50E	10.3	22.3	25.9	69.2	269	16	6	270	1.95	22.4	<5	<2	16	.61	6.9	.6	31	.08	.090	11	18	.23	119	.01	<3	1.08	.01	.05	<2	.3	135	.4	<.2	3.4	3
L10+50N 3+75E	10.1	20.0	13.1	59.1	53	17	7	305	2.09	26.9	<5	2	19	.22	5.5	<.2	35	.10	.039	16	21	.31	88	.03	<3	.97	.01	.05	<2	<.2	107	<.3	<.2	1.9	2
L10+50N 4+00E	27.8	20.9	31.8	70.0	175	19	6	213	2.30	67.6	<5	2	41	.42	8.8	.4	34	.07	.037	13	18	.24	105	.02	<3	.79	.01	.06	<2	<.2	134	.4	.4	3.2	4
L10+50N 4+25E	30.4	27.7	39.8	42.8	515	13	5	257	2.50	58.2	<5	4	31	.20	26.0	1.5	20	.06	.048	18	17	.12	111	.01	<3	.55	.01	.11	<2	.2	226	1.5	1.6	3.1	6
L10+50N 4+50E	50.6	36.1	78.6	71.0	774	18	9	532	2.71	79.3	<5	4	58	.20	17.1	1.0	32	.09	.087	18	21	.26	171	.01	<3	.92	.02	.12	<2	<1	273	<1.5	<1	4.5	23
L10+50N 4+75E	78.3	79.8	56.9	104.7	986	62	16	632	4.43	79.3	<5	5	80	.53	19.1	1.1	32	.07	.103	19	26	.16	270	.01	<3	.76	.01	.13	<2	<1	260	<1.5	1.3	4.2	28
L10+00N 3+50E	21.1	22.6	42.4	52.9	183	18	7	266	2.15	55.3	<5	4	22	.19	10.3	.4	33	.12	.051	16	24	.24	82	.03	<3	.83	.01	.07	<2	.2	126	<.3	.3	2.3	13
L10+00N 3+75E	15.9	30.9	43.7	86.0	475	24	9	337	2.06	40.4	<5	2	18	.98	8.2	.5	33	.10	.034	12	19	.23	84	.02	<3	.82	.01	.07	<2	.2	119	.3	.2	3.1	3
L10+00N 4+00E	27.1	42.5	66.7	128.1	589	27	10	459	2.30	54.5	<5	2	22	1.04	12.5	.8	36	.08	.032	14	22	.25	140	.02	<3	.94	.01	.07	<2	.2	231	.3	.3	3.1	5
L10+00N 4+25E	20.9	52.7	52.1	124.8	305	28	8	342	2.29	60.4	<5	<2	23	.96	13.4	.5	35	.09	.052	12	22	.25	114	.01	<3	1.03	.01	.05	<2	.3	178	.3	.3	2.9	5
L10+00N 4+50E	21.2	36.3	95.2	272.1	441	69	28	1630	2.70	48.7	<5	5	25	2.78	11.1	.5	18	.17	.058	19	10	.15	508	.01	<3	.58	.01	.09	<2	.3	419	<.3	.3	1.8	6
L10+00N 4+75E	21.8	70.1	99.2	201.8	461	53	13	699	2.52	47.2	<5	<2	24	1.56	13.2	.5	32	.08	.072	14	17	.22	144	.01	<3	1.00	.01	.07	<2	.2	278	.3	.2	2.5	4
STANDARD D2/C3/AU-S	22.9	120.1	98.1	261.6	1897	30	18	1008	4.51	71.8	18	22	61	1.92	10.2	17.6	71	.71	.105	18	51	1.10	271	.11	27	2.31	.05	.68	14	1.9	961	.3	1.7	6.4	44

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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ACME ANA[illegible]TICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

SINTER GRID

Omni Resources Inc. PROJECT SKUKUM CREEK/GODDELL File # 9803326 Page 1
910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L15+00N 11+25E	2.8	14.4	57.1	94.7	98	7	6	460	2.47	14.7	<5	4	5	.15	7.4	.4	28	.09	.045	16	10	.28	107	<.01	<3	1.03	<.01	.09	<2	.2	46	<.3	<.2	3.3	2
L15+00N 11+50E	4.3	11.7	41.2	109.7	93	3	4	953	2.01	9.1	<5	<2	18	.44	11.9	.4	27	.28	.055	18	4	.19	501	<.01	<3	.88	.01	.14	<2	<.2	46	<.3	<.2	3.4	1
L15+00N 11+75E	5.4	20.0	77.6	113.2	211	7	6	516	2.91	18.3	<5	2	23	.72	6.6	.3	31	.20	.079	15	12	.31	150	.01	<3	1.08	.01	.13	<2	<.2	176	.3	<.2	4.1	1
L15+00N 12+00E	6.5	21.3	123.9	147.3	370	6	6	709	2.91	19.0	<5	<2	24	1.21	9.6	1.4	32	.16	.101	19	11	.27	286	<.01	<3	1.13	.01	.15	<2	<.2	47	.3	.2	4.3	1
L15+00N 12+25E	5.4	23.7	90.3	115.9	237	9	7	611	2.72	47.2	<5	<2	19	.63	11.4	.4	30	.10	.078	16	14	.36	96	.01	<3	1.13	.01	.11	<2	.3	364	<.3	.2	4.0	2
L15+00N 12+50E	6.7	11.5	58.6	122.1	192	6	6	2006	1.91	11.8	<5	<2	16	1.39	9.2	.5	29	.15	.054	12	8	.19	366	.01	<3	.70	.01	.16	<2	<.2	39	<.3	<.2	3.6	1
L15+00N 12+75E	5.4	19.7	90.5	145.5	267	10	8	1291	2.53	24.1	<5	2	18	1.17	8.8	.5	34	.23	.089	17	13	.37	329	.01	<3	1.21	.01	.25	<2	<.2	49	<.3	<.2	4.9	5
L15+00N 13+00E	5.2	23.2	86.5	119.6	495	12	10	1308	2.60	24.2	<5	5	27	1.29	8.8	.5	34	.42	.068	21	14	.39	374	.01	<3	1.21	.01	.26	<2	.2	74	<.3	.2	4.5	2
L15+00N 13+25E	4.9	22.0	95.0	213.3	246	11	11	2174	2.67	18.4	<5	2	32	3.42	7.2	.4	38	.44	.105	16	17	.39	540	.01	<3	1.30	.01	.29	<2	.2	53	<.3	<.2	5.2	3
L15+00N 13+50E	5.7	21.0	68.1	138.9	246	11	9	1443	2.73	23.8	<5	<2	24	1.27	7.3	.4	36	.20	.099	18	14	.39	325	.01	<3	1.25	.01	.22	<2	.2	60	<.3	.2	4.7	4
L15+00N 13+75E	4.0	18.3	60.5	134.3	158	11	10	1556	2.58	21.2	<5	<2	25	1.32	7.8	.3	37	.29	.116	17	16	.42	296	.01	<3	1.40	.01	.17	<2	.2	59	<.3	<.2	4.9	2
L15+00N 14+00E	3.9	26.0	77.8	150.3	306	10	11	1618	2.50	19.0	<5	3	38	3.32	10.6	.4	34	.64	.098	20	15	.44	491	.01	<3	1.11	.01	.24	<2	.2	152	<.3	.2	4.6	1
L13+00N 8+37.5E	19.0	11.1	41.4	66.8	399	7	4	775	1.19	21.9	<5	<2	10	.55	3.4	.4	12	.08	.043	17	3	.10	147	.01	<3	.59	.01	.15	<2	.2	62	<.3	<.2	2.6	7
L13+00N 8+62.5E	24.2	19.2	68.1	96.1	982	9	6	829	2.16	34.6	<5	<2	23	.69	5.4	.7	13	.10	.076	23	8	.08	350	<.01	<3	.78	.01	.22	<2	.2	89	.4	.4	3.1	52
L13+00N 8+87.5E	12.1	13.2	42.4	62.1	522	8	3	252	1.75	36.2	<5	2	13	.14	4.4	.3	14	.06	.023	29	4	.06	114	<.01	<3	.52	.01	.08	<2	<.2	56	.3	<.2	1.7	5
RE L13+00N 8+87.5E	12.4	13.1	42.7	61.3	463	8	3	247	1.73	36.3	<5	2	13	.13	4.4	.3	14	.06	.022	29	2	.06	113	<.01	<3	.51	.01	.08	<2	<.2	36	<.3	<.2	1.7	4
L13+00N 9+12.5E	4.3	24.3	44.2	116.3	338	9	7	793	2.28	21.4	<5	2	9	.28	4.9	.3	18	.09	.049	23	7	.06	531	<.01	<3	.78	<.01	.12	<2	<.2	71	.3	<.2	1.9	4
L12+87.5N 8+25E	20.6	9.9	63.9	111.2	956	9	4	1278	1.67	19.9	<5	2	12	1.03	3.4	.7	12	.11	.045	19	7	.11	492	<.01	<3	.79	.01	.20	<2	.2	86	<.3	.2	2.8	7
L12+87.5N 8+37.5E	11.7	8.3	50.2	78.1	356	7	3	1001	1.38	18.6	<5	4	9	.61	2.9	.3	9	.05	.033	22	7	.09	297	<.01	<3	.63	.01	.13	<2	<.2	52	<.3	.2	1.9	4
L12+87.5N 8+50E	13.4	3.2	25.7	44.6	524	4	1	476	.79	18.7	5	9	4	.28	1.8	.2	2	.03	.009	28	<1	.02	98	<.01	<3	.29	.01	.23	<2	.2	42	.3	.3	.9	49
L12+87.5N 8+62.5E	37.1	16.8	68.8	71.0	1046	9	6	672	2.06	47.0	6	4	14	.38	6.2	.6	10	.04	.046	33	8	.06	215	<.01	<3	.58	.01	.17	<2	.2	78	.6	.6	2.2	182
L12+87.5N 8+87.5E	8.9	10.5	43.0	91.8	258	8	6	818	1.48	24.4	<5	4	6	.75	2.9	.2	7	.05	.033	20	3	.04	90	<.01	<3	.46	.01	.15	<2	.2	58	<.3	<.2	1.3	11
L12+87.5N 9+00E	11.4	15.9	87.7	164.7	400	11	8	2162	2.28	22.3	<5	3	16	2.12	3.4	.3	17	.15	.050	67	10	.13	311	.01	<3	.75	.01	.14	<2	.2	90	<.3	<.2	2.4	19
L12+87.5N 9+12.5E	10.1	20.1	58.6	145.3	461	8	8	2563	2.26	28.1	<5	<2	16	1.46	4.5	.7	23	.10	.056	17	9	.14	383	.01	<3	.83	.01	.14	<2	.2	51	<.3	.2	3.4	30
L12+87.5N 9+25E	8.5	18.7	64.9	108.9	630	10	7	1588	2.38	19.3	<5	<2	17	.48	3.7	.7	21	.13	.073	26	8	.14	381	.01	<3	1.00	.01	.14	<2	.2	76	<.3	.2	3.5	62
L12+75N 8+25E	6.8	2.8	101.8	158.8	186	57	5	195	3.26	25.1	<5	8	8	.24	1.5	.5	1	.07	.019	44	1	.02	214	<.01	<3	.44	<.01	.20	<2	.2	48	<.3	<.2	1.3	12
L12+75N 8+62.5E	28.8	12.5	80.6	113.3	773	11	6	1285	1.78	26.2	<5	9	12	1.09	3.0	.3	8	.06	.024	60	6	.09	217	<.01	<3	.53	.01	.17	<2	.4	60	<.3	.2	1.8	36
L12+75N 8+75E	13.1	12.4	87.6	120.2	890	13	7	1187	1.94	33.3	<5	11	12	1.84	3.3	.2	14	.07	.037	59	9	.14	171	.01	<3	.86	.01	.17	<2	.2	77	<.3	.2	2.4	207
L12+75N 8+87.5E	22.1	20.0	64.0	63.0	1312	8	4	352	2.26	55.7	<5	6	18	.47	4.8	1.1	14	.08	.071	65	5	.09	282	<.01	<3	.81	.02	.18	<2	.2	40	.5	.8	2.4	229
L12+75N 9+00E	11.6	10.8	90.8	69.3	933	3	2	109	2.17	47.9	5	4	27	.17	3.7	.4	5	.02	.047	46	1	.03	175	<.01	<3	.35	.03	.25	<2	<.2	111	2.1	.3	1.3	27
L12+75N 9+12.5E	13.2	7.2	46.2	49.2	472	4	3	474	1.12	15.6	<5	3	8	.34	2.0	.2	7	.07	.020	41	5	.07	125	<.01	<3	.46	.01	.12	<2	.2	33	<.3	<.2	1.5	11
L12+75N 9+25E	9.1	18.4	85.2	143.6	483	11	9	1705	2.46	26.8	5	9	15	1.53	3.8	.4	14	.16	.039	34	7	.10	330	<.01	<3	.63	.01	.17	<2	.2	67	<.3	<.2	1.8	11
L12+62.5N 8+50E	8.0	12.5	85.8	127.0	341	26	7	2319	2.42	21.7	<5	6	16	2.04	3.0	.2	20	.06	.043	42	11	.18	386	.01	<3	.93	.01	.10	<2	.2	83	<.3	.2	2.9	6
L12+62.5N 8+75E	6.8	4.3	87.6	77.5	248	13	3	2151	.96	14.4	<5	8	5	1.60	1.5	<.2	3	.04	.015	44	1	.03	368	<.01	<3	.38	.01	.16	<2	.3	43	<.3	<.2	1.0	8
L12+62.5N 9+12.5E	23.3	16.6	130.3	66.3	1298	3	2	107	2.72	59.3	<5	5	24	.31	4.1	.8	6	.03	.070	79	3	.02	300	<.01	<3	.43	.05	.33	<2	<.2	122	.9	.5	1.3	57
STANDARD D2/C3/AU-S	25.0	121.6	103.0	266.2	1871	31	18	1039	4.64	71.1	18	20	62	1.92	9.3	17.4	74	.72	.107	19	57	1.16	275	.12	26	2.41	.05	.71	13	1.9	904	.4	1.7	6.3	50

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 10 1998 **DATE REPORT MAILED:** Aug 14/98 **SIGNED BY** [signature] D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data L FA ____

ACME ANALYTICAL

Omni Resources Inc. PROJECT SKUKUM CREEK/GODDELL FILE # 9803326

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
L12+62.5N 9+25E	15.8	20.8	63.8	74.6	565	6	5	381	2.18	42.1	<5	6	18	.33	3.9	.3	12	.07	.040	34	6	.12	146	<.01	<3	.73	.01	.16	<2	<.2	71	.3	.2	2.1	11
L12+50N 8+62.5E	17.0	13.2	85.9	82.4	1031	11	6	881	1.79	32.8	<5	8	14	.23	4.3	.3	14	.07	.033	48	8	.13	162	.01	3	.66	.01	.14	<2	.2	105	<.3	<.2	2.4	614
L12+50N 8+87.5E	13.8	18.1	70.8	84.0	496	13	8	896	2.38	26.3	6	3	23	.44	3.9	.5	23	.10	.056	29	13	.19	170	.01	<3	.92	.01	.13	<2	.2	85	<.3	.2	2.9	92
L12+50N 9+12.5E	454.4	12.5	69.3	29.7	433	4	2	141	4.26	92.4	<5	9	15	<.06	8.1	5.3	12	.01	.044	43	7	.05	178	<.01	<3	.56	.03	.34	<2	<1.2	54	<1.8	1.5	3.9	36
L12+37.5N 8+25E	5.4	6.6	32.1	72.7	249	10	4	1037	1.30	16.3	<5	7	9	.31	2.0	<.2	8	.06	.028	39	3	.08	449	<.01	<3	.52	.01	.16	<2	<.2	56	<.3	<.2	1.7	14
L12+37.5N 8+62.5E	10.9	11.2	49.0	72.5	532	10	4	748	1.30	14.5	<5	6	11	.40	4.3	.3	8	.08	.028	52	8	.07	153	<.01	3	.48	.01	.14	<2	.2	108	<.3	<.2	1.7	184
L12+37.5N 8+75E	42.7	19.4	52.6	13.9	555	3	1	102	2.65	78.9	<5	8	41	.05	3.2	.3	7	.03	.060	57	17	.02	321	<.01	<3	.47	.03	.44	<2	.2	175	<.3	<.2	1.4	11
RE L12+37.5N 8+87.5E	20.1	12.7	58.5	31.2	273	6	3	248	1.42	30.2	<5	6	19	.10	4.2	.2	11	.05	.031	24	10	.08	141	<.01	3	.51	.01	.18	<2	<.2	39	<.3	.2	1.6	26
L12+37.5N 8+87.5E	21.4	13.8	51.3	32.7	325	7	3	260	1.53	30.5	<5	6	20	.12	4.5	.3	12	.05	.033	25	12	.08	152	<.01	<3	.53	.01	.19	<2	.2	41	<.3	.2	1.6	17
L12+37.5N 9+00E	23.3	16.3	55.6	49.3	302	8	4	339	1.34	32.1	<5	7	15	.12	5.0	.3	9	.05	.027	33	8	.08	108	<.01	3	.54	.01	.15	<2	<.2	56	<.3	.2	1.6	32
L12+37.5N 9+12.5E	30.2	16.9	55.5	61.6	294	9	5	454	1.93	37.9	<5	2	19	.14	5.8	.4	15	.03	.042	27	13	.11	131	.01	<3	.69	.01	.16	<2	<.2	86	.3	.3	2.2	31
L12+37.5N 9+25E	61.1	17.6	60.0	65.6	591	7	4	437	2.39	42.0	<5	3	22	.57	4.5	.7	13	.05	.047	33	5	.08	248	<.01	<3	.64	.02	.20	<2	.4	38	.4	.8	1.5	15
STANDARD D2/C3/AU-S	22.7	118.5	100.6	258.0	1896	30	17	1018	4.47	63.0	22	21	61	1.92	9.4	17.6	70	.70	.105	18	56	1.09	271	.11	30	2.29	.05	.69	14	2.3	940	.6	2.3	7.0	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data 4 FA ____

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL/CARBON HILL File # 9803996

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

SINTER CAP SOIL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm
98SCBS-33	7.3	11.8	53.4	63.2	143	4	4	760	1.35	7.0	<5	10	11	.59	4.2	.2
98SCBS-34	7.3	12.6	49.9	72.5	206	6	4	594	1.57	10.4	<5	7	12	.43	5.9	.3
98SCBS-35	5.4	10.6	51.6	52.3	173	3	2	787	1.08	8.6	<5	11	10	.83	4.6	.3
98SCBS-36	5.6	7.3	55.7	46.9	477	5	2	689	.91	7.3	<5	10	7	.60	3.0	.2
98SCBS-37	9.6	12.7	64.0	65.9	195	12	4	778	1.51	14.6	<5	14	11	.81	4.5	.3
RE 98SCBS-37	9.7	13.6	74.1	67.1	178	10	4	798	1.53	11.0	6	14	12	.74	4.8	.3
STANDARD D2/	23.3	118.7	95.8	265.8	1878	30	18	1044	4.21	74.5	23	20	62	2.00	7.8	20.9

SAMPLE#	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
98SCBS-33	10	.09	.029	35	3	.08	182	<.01	<3	.65	.01	.27	<2	.5	105	.4	<.2	1.7	10
98SCBS-34	13	.09	.044	26	5	.11	133	<.01	<3	.62	.01	.23	<2	.6	44	.6	<.2	1.6	25
98SCBS-35	7	.09	.027	47	2	.05	192	<.01	<3	.42	.01	.25	<2	.3	58	.3	.2	1.1	40
98SCBS-36	5	.06	.019	39	1	.03	156	<.01	<3	.32	.01	.23	<2	.4	54	.4	<.2	.9	798
98SCBS-37	5	.09	.026	58	1	.02	219	<.01	<3	.52	.01	.27	<2	.3	97	<.3	.2	1.2	78
RE 98SCBS-37	6	.10	.026	59	2	.03	235	<.01	3	.57	.01	.45	<2	.7	75	.6	<.2	1.5	68
STANDARD D2/	70	.71	.106	17	54	1.10	257	.13	27	2.28	.07	.64	12	2.2	913	.4	2.3	7.4	49

Standard is STANDARD D2/C3/AU-S.

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 11 1998 **DATE REPORT MAILED:** Sept 17/98 **SIGNED BY**.......... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data __ FA __

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT SKUKUM CREEK File # 9803377 Page 1

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

ANTIMONY ZONE - CONTOUR SOILS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
98AZBS-30	.6	39.8	2138.2	2827.0	57800	9	10	851	1.84	25.3	<5	10	171	202.55	2149.6	2.5	13	1.73	.087	28	6	.43	631	<.01	<3	.27	.01	.16	<2	.9	99999	1.2	8.6	<2	129
98AZBS-31	2.5	10.1	39.1	65.3	997	10	15	1087	2.88	20.3	<5	13	124	1.45	18.5	.2	24	2.61	.078	31	9	.32	1049	<.01	3	.51	.01	.22	<2	.3	2014	<.3	<.2	.6	2
98AZBS-32	3.5	12.1	18.5	52.3	1081	10	15	1171	2.54	9.6	<5	15	157	.52	13.1	.2	25	2.85	.068	29	9	.46	905	<.01	<3	.76	.01	.29	<2	.2	510	<.3	<.2	1.1	1
98AZBS-33	1.9	7.3	18.1	51.0	396	8	12	1011	2.29	13.1	<5	15	121	.54	11.5	<.2	21	1.91	.079	38	6	.27	851	<.01	<3	.45	.01	.19	<2	<.2	293	<.3	<.2	<.5	3
98AZBS-34	1.2	8.0	18.8	39.3	253	11	13	896	1.91	8.8	<5	17	180	.46	9.8	<.2	17	4.10	.064	33	9	.46	849	<.01	<3	.54	.01	.22	<2	<.2	381	<.3	<.2	<.5	<1
98AZBS-35	2.2	10.2	18.7	51.3	986	12	15	1056	2.60	11.7	<5	16	224	.50	10.7	.2	20	3.03	.074	32	6	.49	1168	<.01	<3	.48	.01	.22	<2	.2	532	<.3	<.2	.6	1
98AZBS-36	1.4	7.7	15.4	40.9	339	9	13	1083	2.03	4.8	<5	16	452	.38	9.2	<.2	16	3.47	.063	30	6	.24	1064	<.01	<3	.46	.01	.19	<2	<.2	426	<.3	<.2	<.5	<1
98AZBS-37	2.7	12.5	22.1	57.6	615	16	17	1508	2.72	25.1	<5	9	109	.50	11.8	<.2	21	1.68	.081	30	9	.25	1054	<.01	<3	.50	<.01	.19	<2	.3	711	<.3	<.2	1.1	16
98AZBS-38	3.1	13.1	31.6	60.9	385	10	15	1462	2.76	12.5	<5	12	55	.59	8.2	.2	27	.63	.102	38	11	.17	1149	<.01	<3	.77	.01	.19	<2	<.2	313	<.3	<.2	2.2	<1
98AZBS-39	3.1	10.0	21.3	58.8	182	7	5	469	2.34	11.0	<5	5	34	.29	8.0	.2	27	.35	.157	27	10	.11	1316	<.01	<3	1.09	.01	.12	<2	.4	239	<.3	<.2	2.6	<1
98AZBS-40	2.8	15.9	44.6	72.7	488	16	19	1698	2.99	16.0	5	5	81	.65	11.4	.3	29	1.05	.099	31	13	.31	1025	<.01	<3	.88	.01	.23	<2	<.2	558	<.3	<.2	2.5	2
98AZBS-41	2.8	16.8	38.7	68.1	356	17	17	1664	3.07	10.1	<5	5	81	.67	7.5	.2	25	1.29	.124	36	17	.27	1490	<.01	<3	.76	.01	.25	<2	.2	196	<.3	<.2	2.1	<1
98AZBS-42	2.6	11.7	40.7	55.6	283	5	6	701	1.67	6.4	<5	15	77	.32	5.3	.4	12	1.24	.055	59	4	.16	1198	<.01	<3	.51	.01	.24	<2	.2	319	<.3	<.2	1.2	<1
98AZBS-43	2.0	10.8	37.0	45.8	289	9	11	1064	1.92	5.7	<5	8	53	.38	4.5	.3	18	.95	.059	39	6	.15	1151	<.01	<3	.70	.01	.21	<2	<.2	171	<.3	<.2	1.5	1
98AZBS-44	10.0	10.1	223.2	146.3	1473	10	16	1753	2.74	4.7	<5	13	45	1.25	4.5	1.6	22	.88	.066	42	6	.14	1289	<.01	3	.80	.01	.18	<2	<.2	186	<.3	.2	2.1	1
98AZBS-45	5.2	10.7	58.7	67.0	244	9	8	717	2.65	6.1	<5	8	33	.34	4.2	.4	32	.45	.099	36	14	.25	832	<.01	<3	1.17	.01	.13	<2	.2	113	<.3	<.2	3.0	<1
RE 98AZBS-45	5.6	11.4	60.8	68.5	275	9	8	736	2.74	7.0	7	9	33	.35	4.4	.4	32	.47	.102	37	15	.26	856	<.01	<3	1.18	.01	.13	<2	<.2	124	<.3	.2	3.0	<1
98AZBS-46	7.3	27.9	101.1	92.5	1479	14	14	1243	3.43	7.5	<5	3	72	.67	12.1	1.1	35	.95	.095	35	10	.34	1285	<.01	3	.71	.01	.17	<2	<.2	408	<.3	<.2	1.9	1
98AZBS-47	3.8	12.9	37.9	64.9	299	13	14	1274	2.86	6.0	<5	9	64	.50	5.8	.3	30	1.48	.079	38	14	.29	1166	<.01	<3	1.05	.01	.25	<2	.2	104	<.3	<.2	3.1	<1
98AZBS-48	4.2	12.6	42.8	64.5	239	9	13	1414	2.69	6.4	5	3	22	.48	7.2	.3	29	.18	.092	26	10	.15	556	<.01	<3	.96	.01	.13	<2	<.2	138	<.3	<.2	2.3	1
98AZBS-49	5.4	20.8	24.4	52.0	185	3	6	276	5.19	24.4	<5	6	99	.04	10.5	1.6	35	.02	.135	18	3	.19	428	<.01	<3	.95	.06	.19	<2	.2	82	2.4	.4	3.4	9
98AZBS-50	13.0	25.9	128.8	166.1	1332	14	18	1695	3.64	8.7	<5	20	67	1.49	3.5	1.5	24	1.38	.088	40	11	.21	947	<.01	<3	.78	.01	.20	<2	<.2	91	.6	.2	1.8	6
98AZBS-51	15.6	14.4	125.8	115.8	2096	12	15	1802	2.97	6.1	<5	12	29	.92	7.1	2.9	26	.31	.072	41	12	.17	1038	<.01	<3	.83	.01	.17	<2	<.2	243	<.3	.2	2.1	<1
98AZBS-52	5.2	12.5	35.2	79.4	227	10	10	968	2.36	5.8	6	8	48	.54	7.0	.3	26	.30	.072	32	11	.19	730	<.01	<3	.81	.01	.17	<2	<.2	206	<.3	<.2	2.2	1
98AZBS-53	2.4	10.1	26.7	48.7	203	7	9	767	2.14	7.0	<5	8	37	.27	6.3	.3	24	.34	.048	27	13	.18	334	<.01	<3	.69	.01	.15	<2	<.2	340	<.3	<.2	2.0	2
98AZBS-54	2.1	16.9	26.7	70.2	277	24	14	1140	3.08	7.1	<5	9	57	.64	7.7	<.2	30	.67	.089	30	25	.39	1030	<.01	3	.74	.01	.19	<2	<.2	339	<.3	<.2	2.2	2
98AZBS-55	2.7	15.8	39.7	75.3	310	15	17	1692	2.97	8.5	<5	9	50	.99	8.5	.3	30	.57	.089	39	13	.25	1254	<.01	3	.87	.01	.26	<2	<.2	299	<.3	<.2	2.3	1
98AZBS-56	4.1	15.4	34.9	97.0	273	10	9	1236	2.49	9.2	<5	4	68	.81	7.9	.3	25	.75	.184	31	10	.23	1033	<.01	4	1.10	.01	.17	<2	<.2	247	<.3	<.2	3.3	1
98AZBS-57	2.4	12.1	34.4	89.9	142	10	11	1019	2.63	7.3	<5	5	33	.63	8.6	.3	32	.32	.089	24	13	.26	556	<.01	<3	.87	.01	.14	<2	<.2	378	<.3	<.2	2.3	2
98AZBS-58	4.1	13.4	41.8	66.6	249	7	14	1245	2.63	9.0	<5	8	46	.37	8.6	.3	30	.34	.068	30	9	.18	1080	<.01	<3	1.07	.01	.16	<2	<.2	178	<.3	<.2	3.1	81
98AZBS-59	2.4	14.5	37.9	94.7	533	12	14	1423	2.89	9.3	<5	11	71	1.11	13.2	.3	30	1.05	.079	38	6	.19	1412	<.01	<3	.83	.01	.20	<2	<.2	376	<.3	<.2	2.5	4
98AZBS-60	2.2	12.1	31.0	62.1	341	10	12	1182	2.25	7.5	<5	8	85	.62	7.9	.2	25	1.27	.077	32	7	.19	1209	<.01	<3	.74	.01	.25	<2	<.2	434	<.3	<.2	1.9	2
98AZBS-61	2.0	9.7	28.3	63.6	136	9	14	1303	2.59	3.9	<5	17	170	.37	6.3	.2	28	1.90	.073	39	4	.16	1204	<.01	<3	.61	.01	.20	<2	<.2	169	<.3	<.2	1.7	3
98AZBS-62	1.9	9.5	23.6	59.5	103	8	12	1164	2.42	3.4	<5	21	175	.31	6.4	<.2	26	1.83	.065	34	5	.14	1149	<.01	<3	.50	.01	.19	<2	.2	105	<.3	<.2	1.1	3
STANDARD D2/C3/AU-S	23.2	116.9	98.4	258.3	1888	30	17	1002	4.46	68.1	17	20	61	1.92	9.2	17.5	70	.71	.104	17	57	1.09	248	.11	30	2.30	.04	.68	13	2.0	905	.4	2.0	6.5	43

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 11 1998 **DATE REPORT MAILED:** Aug 14/98 **SIGNED BY** C.L. ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only. Data FA

Omni Resources Inc. PROJECT SKUKUM CREEK FILE # 9803377

ACME ANALYTICAL

ANTIMONY ZONE – CONTOUR SOILS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au* ppb
98AZBS-63	2.8	9.3	35.3	61.0	314	6	11	988	2.01	3.1	<5	20	373	.90	5.7	.7	20	3.03	.058	32	3	.19	1013	<.01	3	.56	.01	.22	<2	<.2	350	<.3	<.2	1.1	3
98AZBS-64	4.1	14.1	45.8	69.1	590	8	12	1037	2.35	8.2	<5	22	146	.83	9.2	.6	26	1.75	.064	34	8	.28	1018	<.01	<3	.67	.01	.23	<2	<.2	291	<.3	<.2	1.3	5
98AZBS-65	1.8	48.6	63.4	61.4	452	7	12	1003	2.38	16.8	<5	18	121	.84	10.5	.4	23	1.51	.065	37	3	.25	1058	<.01	<3	.55	.01	.21	<2	<.2	1235	<.3	<.2	1.1	1
98AZBS-66	2.5	14.6	30.6	65.7	399	12	15	1209	2.78	20.8	<5	18	154	.62	10.0	.3	26	1.84	.073	33	9	.33	1227	<.01	<3	.65	.01	.25	<2	.2	442	<.3	<.2	1.1	3
98AZBS-67	1.6	5.1	17.9	35.7	87	3	6	640	1.55	8.7	<5	19	192	.51	6.2	.2	10	2.45	.045	38	3	.14	827	<.01	<3	.43	<.01	.20	<2	<.2	936	<.3	<.2	.7	<1
98AZBS-68	3.7	13.7	72.2	66.2	478	5	9	898	2.12	6.3	<5	22	126	1.05	8.3	.6	17	1.68	.056	36	4	.18	1182	<.01	<3	.55	.01	.24	<2	<.2	287	<.3	<.2	.7	1
98AZBS-69	1.9	21.6	155.4	81.4	768	6	10	914	2.10	6.3	<5	18	101	1.31	7.3	.7	18	1.66	.059	32	4	.21	1020	<.01	<3	.54	.01	.22	<2	<.2	362	<.3	<.2	1.0	9
98AZBS-70	2.0	14.6	36.0	70.8	404	8	11	961	2.43	12.4	<5	17	118	.64	12.9	.2	20	1.93	.074	33	6	.27	885	<.01	3	.50	.01	.21	<2	<.2	239	<.3	<.2	.8	4
RE 98AZBS-67	1.4	4.7	16.2	34.5	77	3	6	623	1.50	8.8	<5	19	184	.46	5.9	.2	10	2.38	.043	37	2	.13	815	<.01	<3	.41	<.01	.19	<2	<.2	912	<.3	<.2	.6	2
98AZBS-71	2.3	17.3	37.5	75.5	1094	11	12	1007	2.93	13.2	<5	13	86	.78	11.9	.3	25	1.49	.070	34	9	.27	1010	<.01	3	.53	.01	.21	<2	<.2	546	<.3	<.2	1.0	2
98AZBS-72	2.1	20.5	247.9	88.8	3336	12	12	982	3.03	20.2	<5	12	85	1.17	21.7	.2	26	1.27	.067	35	9	.30	1028	<.01	<3	.69	.01	.21	<2	<.2	1090	<.3	<.2	1.4	4
STANDARD D2/	24.2	124.2	105.7	267.4	1853	31	17	1022	4.57	73.5	18	21	60	1.92	9.3	17.4	73	.72	.107	18	54	1.16	243	.13	27	2.44	.05	.70	15	1.8	927	.5	1.8	6.3	45

Standard is STANDARD D2/C3/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ___ FA ___

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Omni Resources Inc. PROJECT GODDELL(ANTIMONY CK) File # 9803867 Page 1

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: G.L. Wesa

ANTIMONY ZONE - CONTOUR SOILS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
98AZBS-01	6.2	13.9	155.9	233.6	1359	8	17	2038	3.05	1.9	<5	25	95	2.23	2.8	2.3	18	4.31	.076	45	4	.21	952	<.01	<3	.56	.01	.20	<2	.2	192	<.3	<.2	1.0	15
98AZBS-02	8.0	15.2	37.0	77.1	254	14	14	1150	2.48	7.9	<5	10	40	.64	4.8	.3	27	.54	.073	35	8	.16	647	<.01	<3	.52	.01	.15	<2	<.2	282	<.3	<.2	1.5	3
98AZBS-03	1.9	18.4	26.9	75.7	284	34	26	2055	4.02	6.5	<5	10	47	.39	5.3	.2	31	.39	.091	42	14	.13	1289	<.01	<3	.63	<.01	.17	<2	<.2	613	<.3	<.2	1.4	4
98AZBS-04	3.7	18.1	35.5	82.4	198	14	14	1253	2.69	12.4	<5	8	37	.83	5.6	.4	28	.28	.095	31	13	.20	851	<.01	<3	.86	.01	.20	<2	.2	260	<.3	<.2	2.7	10
98AZBS-05	4.5	15.6	36.3	82.8	88	10	16	1788	2.73	10.3	<5	8	48	.37	5.9	.4	30	.45	.102	26	11	.22	812	.01	<3	.78	.01	.20	<2	<.2	207	<.3	<.2	2.5	1
98AZBS-06	2.8	13.9	33.2	66.9	240	11	14	1277	2.54	12.2	<5	11	44	.39	6.1	.3	27	.50	.066	36	10	.19	868	<.01	<3	.78	.01	.21	<2	.2	433	<.3	<.2	2.1	2
98AZBS-07	2.9	20.2	89.7	119.8	530	16	14	1332	3.16	9.5	<5	12	58	1.05	5.1	.6	27	.89	.094	37	14	.24	1472	<.01	<3	.74	.01	.22	<2	.3	214	<.3	<.2	2.5	3
98AZBS-08	2.3	13.0	47.6	80.6	282	12	12	1126	2.46	6.2	<5	9	123	.51	3.1	.2	22	1.83	.084	36	9	.27	1221	<.01	3	.69	.01	.27	<2	.2	129	<.3	<.2	2.2	3
98AZBS-09	7.3	17.3	54.8	79.2	424	17	15	1241	2.97	6.4	<5	9	55	.77	3.4	.4	30	.68	.064	32	11	.23	1187	<.01	<3	.66	<.01	.21	<2	<.2	235	<.3	<.2	1.8	4
98AZBS-10	9.0	20.7	80.5	77.5	812	13	13	1170	2.65	7.3	7	3	114	.64	3.8	.8	25	1.45	.149	40	11	.25	1280	<.01	<3	.96	.01	.19	<2	<.2	266	<.3	<.2	2.2	8
98AZBS-11	19.7	12.4	44.0	64.5	264	9	9	613	2.42	10.2	<5	13	28	.30	3.9	.7	24	.26	.045	31	9	.18	453	<.01	<3	.66	<.01	.17	<2	.3	176	<.3	<.2	2.1	11
98AZBS-12	5.6	10.6	32.7	69.2	267	7	5	596	2.24	7.4	<5	4	18	.43	4.0	.4	24	.13	.137	24	10	.11	454	<.01	<3	.90	<.01	.09	<2	<.2	216	<.3	<.2	2.4	3
98AZBS-13	5.0	23.7	79.9	87.9	993	10	14	1227	2.79	5.4	<5	12	35	.60	5.3	1.1	31	.63	.084	32	8	.24	608	.01	<3	.58	.01	.14	<2	<.2	401	<.3	<.2	1.9	5
98AZBS-14	6.0	16.3	50.3	77.5	427	11	13	1258	2.68	9.0	<5	9	34	.58	4.9	.6	29	.38	.085	33	11	.21	775	<.01	<3	.83	.01	.16	<2	.2	240	<.3	<.2	2.4	8
98AZBS-15	8.5	20.6	42.1	46.5	218	8	8	290	3.93	17.9	<5	9	110	.13	3.7	1.9	32	.12	.130	19	16	.19	449	<.01	<3	.80	.02	.19	<2	.2	58	3.4	<.2	4.0	12
98AZBS-16	30.4	46.3	99.5	259.8	639	11	16	1516	3.76	8.7	<5	9	43	1.92	2.8	2.4	21	.19	.078	21	7	.32	578	.01	<3	.93	.03	.22	<2	.3	110	1.5	<.2	2.4	5
98AZBS-17	23.8	40.3	93.9	190.4	575	9	14	1546	4.34	10.2	<5	9	66	1.24	3.3	2.1	20	.98	.079	19	5	.32	399	<.01	<3	.74	.05	.37	<2	.4	108	1.9	<.2	2.5	5
98AZBS-18	64.9	48.1	112.2	172.2	497	10	13	872	4.70	8.6	<5	13	43	.92	4.7	1.4	24	.06	.105	18	7	.28	331	<.01	<3	1.02	.03	.28	<2	.5	125	2.1	<.2	2.4	6
98AZBS-19	43.2	126.2	209.1	702.4	1731	30	55	6920	7.07	19.0	<5	14	69	5.48	4.6	4.3	52	.49	.081	58	28	1.07	351	<.01	<3	1.65	.02	.28	<2	.4	1091	2.6	<.2	5.8	12
98AZBS-20	95.7	68.1	143.4	230.0	905	8	17	2142	4.95	9.5	<5	14	39	1.72	2.2	4.1	15	.20	.098	25	6	.25	363	<.01	<3	.76	.02	.25	<2	.6	88	1.6	<.2	2.2	6
RE 98AZBS-18	62.6	46.0	110.5	165.3	457	9	13	847	4.55	6.8	<5	12	40	.82	3.7	1.3	23	.06	.101	17	7	.27	248	<.01	<3	.91	.03	.26	<2	.5	129	1.9	<.2	1.8	6
98AZBS-21	38.4	43.2	155.8	188.4	505	9	22	3747	5.10	7.5	<5	18	21	1.31	1.3	1.9	15	.09	.090	24	5	.35	317	<.01	<3	.97	.01	.16	<2	.2	126	2.1	<.2	3.3	4
98AZBS-22	32.1	54.0	170.6	188.1	924	7	10	1953	2.87	4.9	<5	10	31	3.15	2.1	3.6	21	.37	.057	29	7	.37	626	<.01	<3	.78	.01	.17	<2	.2	61	.9	<.2	2.9	3
98AZBS-23	297.4	333.8	1665.8	2522.3	9516	6	15	670	9.03	14.5	<5	8	41	26.47	5.5	25.2	20	.21	.071	10	12	.12	580	<.01	<3	.79	.01	.27	<2	<2	13430	6.6	<2	<5	7
98AZBS-24	55.7	146.9	122.2	123.0	1366	8	11	726	15.00	7.8	<5	10	271	.63	.5	4.2	71	.32	.100	34	57	.59	190	.01	<3	1.02	.12	1.16	<2	.7	110	8.4	.4	12.2	5
98AZBS-25	73.5	219.1	155.8	145.6	1100	9	13	1394	5.29	10.9	<5	5	108	1.27	4.8	2.2	20	.48	.062	14	6	.22	370	<.01	<3	.81	.04	.40	<2	.4	181	.8	<.2	3.0	5
98AZBS-26	24.3	350.0	96.9	205.9	658	12	15	511	4.60	10.7	8	5	522	2.48	1.0	1.8	8	.38	.218	9	1	.04	358	<.01	<3	.65	.04	.52	<2	.2	103	1.1	.5	1.0	13
98AZBS-27	7.8	1301.7	208.1	112.0	1965	28	21	1321	3.60	223.8	<5	9	165	.74	25.8	1.9	9	6.41	.040	10	5	.52	222	<.01	<3	.43	.01	.20	<2	<.2	564	.9	1.1	.7	13
98AZBS-28	33.4	153.7	140.0	151.2	1893	10	16	1935	3.80	16.4	<5	12	115	1.10	2.7	4.2	26	1.91	.080	31	9	.43	701	<.01	<3	.88	.01	.26	<2	.2	131	.7	<.2	2.3	8
98AZBS-29	12.6	61.4	53.7	90.5	746	20	14	1695	4.54	12.5	<5	13	507	.39	2.3	2.1	63	3.52	.069	39	33	.71	980	<.01	<3	1.13	.01	.25	<2	.2	79	<.3	<.2	3.3	3
98AZBS-73	37.1	88.6	107.5	198.6	1177	8	13	1695	3.13	5.4	<5	7	84	1.62	1.7	3.8	25	.59	.070	23	8	.36	412	.01	<3	1.22	.02	.17	<2	.3	92	.6	<.2	3.7	6
98AZBS-74	108.4	161.2	309.8	191.2	5170	4	5	792	6.39	<.5	<5	10	275	.61	1.5	11.9	21	.39	.110	22	4	.35	150	<.01	<3	.70	.07	.81	<2	.6	240	1.8	<.2	2.5	2
98AZBS-75	17.5	40.7	72.3	137.5	573	8	15	991	3.61	5.9	<5	7	79	.62	1.8	1.5	43	.38	.080	19	12	.65	298	.03	<3	1.38	.02	.15	<2	.2	74	1.2	<.2	3.9	5
98AZBS-76	34.7	34.4	91.7	184.9	455	10	17	1707	3.89	6.3	<5	11	37	1.41	1.5	1.3	17	.18	.089	27	7	.22	446	<.01	<3	.88	.02	.20	<2	.3	77	1.7	<.2	2.5	6
STANDARD D2/C3/AU-S	23.0	120.5	102.3	299.7	1886	31	17	1020	4.21	73.0	20	19	61	1.92	7.9	20.3	73	.71	.107	16	53	1.11	252	.14	25	2.31	.06	.69	14	2.0	884	.5	1.7	6.1	53

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: SEP 3 1998 **DATE REPORT MAILED:** Sept 11/98 **SIGNED BY** ....D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

Data ✓ FA ____

ACME ANALYTICAL

Omni Resources Inc. PROJECT GODDELL FILE # 9803867 Page 2

SINTER CAP - TRENCH SOILS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
98SCBS-01	16.2	48.3	82.0	142.0	552	36	18	904	3.98	327.1	<5	8	33	.45	26.8	.5	37	.09	.055	26	14	.39	262	.01	<3	1.01	.01	.15	<2	.6	1262	.8	.4	3.2	8
98SCBS-02	21.3	88.6	74.7	175.1	533	60	29	1269	5.46	330.9	<5	6	43	.68	20.4	.6	61	.13	.089	29	20	.56	287	.01	<3	1.35	.02	.19	<2	.4	451	1.4	.6	3.8	8
98SCBS-03	16.9	62.9	102.8	173.2	879	37	23	949	4.16	212.4	<5	4	40	.74	24.6	.7	40	.14	.096	23	13	.44	313	.01	<3	1.21	.02	.14	<2	.3	1032	1.2	.5	3.1	11
98SCBS-04	18.2	58.1	129.0	165.4	1068	27	18	950	4.17	146.6	<5	4	41	.81	17.0	.8	37	.09	.114	23	13	.43	367	.01	<3	1.41	.02	.15	<2	.3	914	1.0	.6	3.9	12
98SCBS-05	20.5	71.1	56.1	149.8	893	49	20	613	4.51	274.2	<5	8	30	.58	20.4	.6	45	.08	.091	23	18	.39	293	.01	<3	.97	.01	.14	<2	.3	621	1.2	.6	3.0	9
98SCBS-06	12.6	41.1	100.7	144.1	914	16	15	931	3.82	71.2	<5	3	41	.67	8.4	.6	32	.15	.108	23	10	.34	340	.01	<3	1.05	.02	.16	<2	.2	112	.8	.5	3.5	7
98SCBS-07	15.1	57.5	97.1	155.9	703	30	22	1134	4.48	110.3	<5	5	41	.68	9.2	.6	39	.10	.098	27	11	.46	395	.01	<3	1.32	.02	.18	<2	.2	255	1.0	.6	3.3	8
98SCBS-08	19.8	60.7	67.3	149.7	545	53	26	1019	4.09	198.6	<5	5	42	.84	29.8	1.4	38	.08	.101	23	14	.34	414	.01	<3	1.26	.02	.18	<2	.3	320	1.3	.6	3.5	9
98SCBS-09	35.6	44.0	68.6	86.4	416	29	12	382	3.04	239.8	<5	12	38	.36	13.0	.7	25	.09	.052	30	14	.20	586	.01	<3	1.00	.01	.21	<2	.4	322	1.0	.4	3.0	21
98SCBS-10	22.4	53.8	113.7	152.1	936	29	17	797	4.53	165.5	<5	6	37	.59	11.5	.8	35	.05	.079	40	11	.31	253	.01	<3	1.17	.02	.17	<2	.3	219	1.2	.6	3.3	9
98SCBS-11	21.6	17.1	34.1	71.0	428	12	7	497	2.03	71.2	<5	<2	27	.38	8.8	.5	24	.11	.060	14	10	.11	337	.01	<3	.56	.01	.14	<2	<.2	97	.5	.2	2.6	4
98SCBS-12	12.7	25.0	26.8	81.6	459	30	12	727	2.38	130.5	<5	4	22	.51	16.2	.4	30	.08	.053	15	14	.21	144	.02	<3	.80	.01	.10	<2	.2	570	.7	.3	2.6	7
RE 98SCBS-12	11.8	22.7	26.3	74.8	429	27	11	667	2.20	120.2	<5	5	20	.47	14.7	.4	28	.07	.049	14	13	.19	132	.02	<3	.73	.01	.10	<2	.2	576	.7	.3	2.3	7
98SCBS-13	13.4	37.4	58.7	119.6	550	16	18	732	4.70	89.8	<5	5	47	.32	8.6	.8	30	.02	.121	25	9	.32	257	<.01	<3	1.56	.02	.15	<2	<.2	141	1.4	.5	3.4	9
98SCBS-14	14.2	30.9	38.8	80.8	441	27	12	393	3.24	133.8	<5	4	28	.28	18.0	.6	32	.04	.064	19	15	.29	204	.01	<3	1.10	.01	.14	<2	.2	2549	1.0	.3	3.2	10
98SCBS-15	18.6	21.6	28.7	52.8	271	26	7	188	2.23	202.5	<5	4	23	.17	20.4	.5	25	.03	.043	15	13	.16	240	.01	<3	.73	.01	.13	<2	.3	783	.9	.3	2.2	7
98SCBS-16	2.8	9.6	28.9	73.0	150	4	4	1206	1.86	4.4	<5	7	23	1.30	11.6	<.2	17	.30	.088	39	3	.26	441	<.01	<3	1.07	.01	.13	2	.2	82	<.3	<.2	3.5	5
98SCBS-17	12.4	14.4	45.8	98.3	624	9	6	385	2.27	16.5	<5	6	12	.52	4.4	.4	26	.09	.068	19	11	.27	141	.01	<3	1.34	.01	.11	<2	.2	69	<.3	<.2	3.6	285
98SCBS-18	21.5	10.7	55.1	92.9	1071	6	5	505	2.08	23.2	<5	7	8	.25	5.2	.3	18	.06	.049	18	6	.13	76	<.01	<3	.81	.01	.10	2	<.2	35	<.3	<.2	2.1	1345
98SCBS-19	55.3	9.9	54.1	92.0	1201	7	6	907	2.03	35.5	<5	11	7	.78	5.5	.6	16	.11	.058	25	6	.16	218	<.01	<3	.64	.01	.13	<2	.3	39	<.3	<.2	2.1	694
98SCBS-20	44.7	9.7	52.6	81.5	2534	6	5	797	1.88	32.2	<5	10	7	.55	5.2	.4	13	.07	.046	25	4	.10	167	<.01	<3	.65	<.01	.13	<2	.3	100	<.3	<.2	2.0	4320
98SCBS-21	14.2	16.2	55.2	114.8	191	16	7	979	2.38	23.2	<5	11	15	.83	6.5	.3	18	.07	.031	41	6	.11	288	.01	<3	.87	<.01	.11	<2	.2	194	<.3	<.2	2.4	30
98SCBS-22	5.7	10.4	38.4	63.0	178	10	4	478	1.68	12.4	<5	7	12	.51	6.3	.2	18	.07	.023	24	5	.09	155	<.01	<3	.78	<.01	.10	<2	<.2	112	<.3	<.2	2.1	43
98SCBS-23	6.2	14.0	49.8	83.4	252	13	5	791	1.83	13.7	<5	9	11	.74	6.8	.3	19	.08	.027	29	5	.12	253	.01	<3	.68	<.01	.13	<2	<.2	115	<.3	<.2	2.1	45
98SCBS-24	6.2	11.8	43.7	77.6	163	11	6	702	1.67	16.1	<5	8	22	.70	8.5	.3	17	.16	.028	31	4	.10	242	.01	<3	.81	<.01	.11	<2	.2	1200	<.3	<.2	2.6	43
98SCBS-25	9.6	10.2	45.4	79.1	596	10	3	661	1.66	17.9	<5	7	16	.58	4.8	.3	7	.11	.025	40	1	.04	233	<.01	<3	.64	<.01	.14	<2	<.2	133	<.3	<.2	1.5	712
98SCBS-26	7.6	8.3	47.2	79.2	113	4	4	963	1.69	7.9	<5	6	11	.75	1.9	<.2	5	.12	.037	42	1	.05	164	<.01	<3	.42	.01	.15	<2	<.2	84	<.3	<.2	1.1	4
98SCBS-27	3.4	17.1	43.0	110.7	447	9	10	1402	3.51	10.6	<5	9	19	.47	1.6	.4	32	.17	.091	41	4	.06	1062	<.01	<3	.82	<.01	.14	<2	<.2	78	.5	.4	2.0	9
98SCBS-28	13.0	24.4	93.3	234.9	662	26	18	2340	2.93	30.9	<5	5	16	1.80	5.1	.4	16	.09	.045	54	6	.12	379	.01	<3	.71	.01	.12	<2	<.2	131	.4	.2	2.2	31
98SCBS-29	8.6	70.6	227.0	1298.2	752	80	95	10876	4.05	39.4	<5	10	25	7.00	10.4	.3	14	.20	.076	72	6	.05	909	<.01	<3	.69	.01	.21	<2	<.2	288	.8	.2	.9	11
98SCBS-30	28.5	24.4	116.5	123.6	1321	6	3	142	4.44	70.3	<5	12	32	.43	4.4	1.2	7	.09	.098	49	<1	.02	258	<.01	<3	.37	.04	.57	<2	<.2	277	1.8	.6	1.5	197
98SCBS-31	51.1	22.1	93.2	103.8	1528	10	9	863	2.83	64.1	<5	7	25	.55	8.0	1.2	11	.05	.057	40	4	.05	369	<.01	<3	.54	.01	.23	<2	<.2	152	1.4	1.0	2.1	200
98SCBS-32	31.1	21.0	127.3	109.5	941	14	6	551	2.41	31.4	<5	13	16	.58	4.2	.7	11	.10	.032	91	6	.08	278	.01	<3	.41	.01	.12	<2	<.2	104	.4	.2	1.4	292
98SCBS-33	20.8	16.9	148.3	110.2	781	13	7	818	2.33	44.4	<5	16	12	.79	3.4	.4	8	.08	.026	75	4	.06	282	.01	<3	.40	.01	.16	<2	<.2	111	.5	<.2	1.4	100
STANDARD D2/C3/AU-S	23.5	120.8	98.4	301.3	1884	30	17	1020	4.25	71.0	20	19	61	2.12	9.7	20.4	73	.71	.104	16	55	1.12	254	.14	26	2.36	.06	.69	14	2.0	894	.8	1.7	6.0	56

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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APPENDIX VI

Stream Silt Geochemical Lab Reports

ACME AN[illegible]ICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]-1716
(ISO 9002 Accredited Co.)

GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

Omni Resources PROJECT SINTER CAP-CARBON HILL File # 9803074

910 - 700 W. Pender St., Vancouver BC V6C 1G8 Submitted by: Gary Wesa

SINTER CAP — STREAM SILTS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
98SCBW-01	8.7	30.9	132.1	178.5	359	16	10	1212	2.47	52.1	<5	6	29	1.48	24.4	.5	24	.39	.104	24	3	.29	275	<.01	<3	.61	.01	.13	<2	<.2	1234	<.3	<.2	2.2	1
98SCBW-02	8.6	32.6	115.1	190.6	337	20	10	1302	2.46	46.7	<5	6	24	1.71	14.4	.7	22	.35	.082	24	7	.30	263	<.01	<3	.63	.01	.14	<2	.3	602	.3	<.2	2.4	4
98SCBW-03	9.2	28.4	112.8	170.4	355	16	9	1128	2.20	37.0	<5	5	22	1.60	15.3	.5	22	.35	.088	21	3	.27	265	<.01	<3	.57	.01	.13	<2	<.2	401	<.3	<.2	2.2	1
98SCBW-04	9.6	28.5	99.3	184.1	432	20	10	1287	2.41	37.6	<5	5	27	1.86	12.8	.6	22	.49	.075	22	10	.32	274	<.01	<3	.65	.01	.14	<2	.3	294	.3	<.2	2.9	1
98SCBW-05	12.3	34.9	149.4	229.1	519	24	12	1572	2.56	41.5	5	6	29	2.44	15.1	.7	21	.49	.078	26	5	.28	322	<.01	3	.65	.01	.17	<2	.2	379	<.3	<.2	2.2	7
98SCBW-06	10.5	38.6	194.3	263.7	514	28	11	1405	2.28	36.9	<5	5	29	2.69	20.3	.7	18	.42	.069	26	5	.26	272	<.01	<3	.61	.01	.17	<2	.3	464	.4	<.2	1.9	1
98SCBW-07	8.8	41.4	250.7	252.8	527	24	10	1161	2.10	43.2	<5	6	28	2.85	26.0	.6	17	.40	.067	24	5	.27	228	<.01	<3	.65	.01	.16	2	.6	665	.3	.2	3.0	1
98SCBW-08	15.9	71.2	175.8	376.5	718	56	19	1745	3.13	87.3	<5	5	40	5.04	24.5	.9	27	.42	.085	34	10	.34	261	<.01	<3	.86	.01	.18	<2	.2	720	.6	<.2	2.7	48
98SCBW-09	22.4	88.0	131.1	517.1	886	111	34	2734	4.23	158.9	6	5	44	6.67	25.0	1.2	35	.35	.090	35	15	.41	299	<.01	<3	.95	.01	.18	<2	.3	1043	1.0	.3	3.0	10
98SCBW-10	26.7	100.5	113.5	612.5	939	143	38	2808	4.80	198.1	<5	5	48	7.86	25.7	1.4	37	.28	.095	38	15	.43	303	<.01	<3	.99	.01	.18	<2	.3	1758	1.1	.7	2.7	10
98SCBW-11	28.4	113.6	125.7	442.3	1276	100	31	1700	4.53	195.9	6	5	67	5.14	33.5	1.5	38	.52	.107	52	18	.42	263	<.01	4	1.02	.02	.18	<2	.4	1053	2.7	.6	2.7	15
RE 98SCBW-11	26.9	104.4	119.7	416.8	1166	95	29	1604	4.34	187.3	<5	3	64	4.66	30.2	1.4	35	.49	.104	49	14	.41	251	<.01	<3	.98	.02	.18	<2	.4	1662	2.4	.6	2.8	14
98SCBW-12	29.1	141.2	166.1	477.5	909	106	41	2861	4.43	95.4	<5	5	49	6.23	10.6	1.2	34	.27	.095	50	19	.45	332	<.01	3	1.23	.02	.19	<2	.2	514	.7	.4	2.9	11
98SCBW-13	32.6	123.0	222.5	415.9	1036	77	32	2200	4.79	84.8	<5	5	49	4.12	10.4	1.6	33	.22	.102	46	15	.36	292	<.01	<3	1.12	.02	.19	<2	.3	310	.9	.7	2.8	15
98SCBW-14	33.3	125.6	112.0	876.2	1346	117	40	3488	3.90	116.3	<5	3	55	10.57	21.0	.9	26	.30	.098	71	11	.27	305	<.01	3	1.14	.02	.22	<2	.5	914	1.1	.5	2.5	27
98SCBW-15	26.4	102.0	87.8	597.7	1134	81	28	1532	3.16	128.2	<5	2	47	6.25	19.9	1.3	22	.34	.086	74	11	.23	268	<.01	<3	.99	.01	.16	<2	.4	986	.4	.4	2.6	23
98SCBW-16	27.5	470.1	129.5	2164.7	1329	199	64	3626	3.75	222.5	<5	3	56	24.23	32.9	1.3	23	.30	.078	36	13	.19	248	<.01	3	1.76	.01	.19	<2	.7	2073	<.3	<.2	3.1	13
98SCBW-17	25.2	64.9	59.5	662.8	613	172	23	1679	3.46	218.4	<5	3	46	5.77	44.8	1.2	21	.24	.075	15	15	.17	167	<.01	3	.69	.01	.15	<2	.5	1928	.5	.7	2.3	9
STANDARD D2/C3/AU-S	23.8	122.8	104.9	269.8	1661	32	17	1015	4.56	70.7	20	21	60	1.68	9.3	17.4	76	.71	.107	19	61	1.14	248	.15	31	2.41	.05	.77	14	2.2	1006	.3	1.7	6.8	56

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 300 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQUAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.
- SAMPLE TYPE: SILT AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 27 1998 DATE REPORT MAILED: July 31/98 SIGNED BY. C. L[illegible] .D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

All results are considered the confidential property of the client. Acme assumes the liabilities for actual cost of the analysis only.

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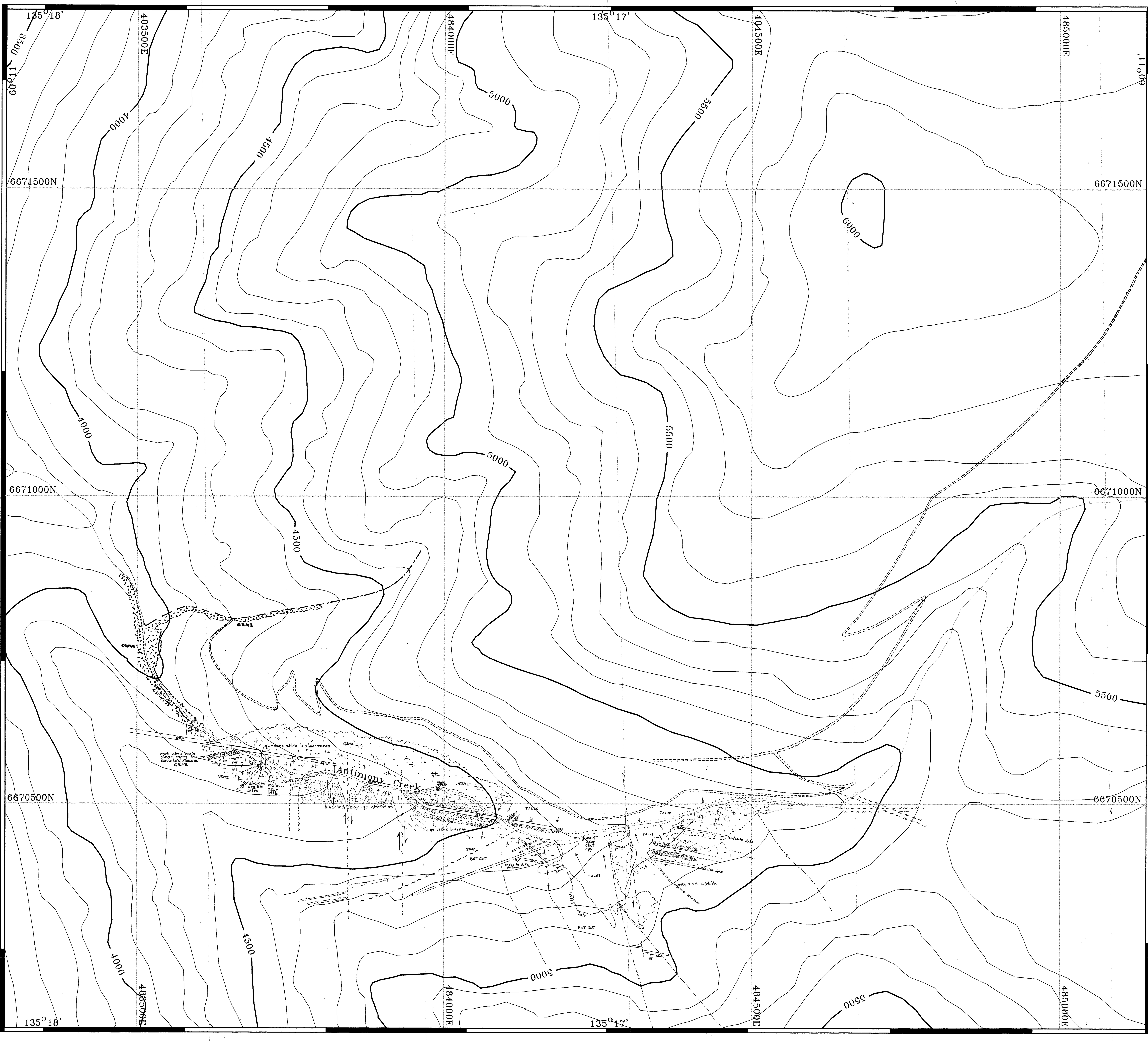

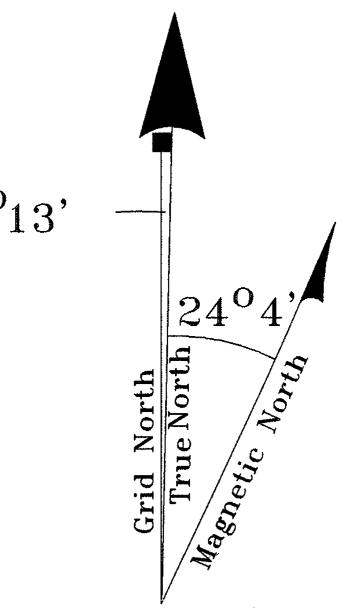

Contour Interval 100 feet

Scale 1 : 2000

0 metres 200

OMNI RESOURCES LTD.

ANTIMONY CREEK PROPERTY

GEOLOGY by G. Wesa

(NTS 105 D/3)

NAD 1927

LEGEND

- Outcrop boundary
- Geological contact (defined, approx., assumed)
- Fault
- Fault with direction of displacement shown by arrows
- Strike and dip of contacts or jointing (64°)
- Breccia
- Major contour
- Minor contour
- Road

INTRUSIVE HOST ROCKS

TERTIARY

- QFP Quartz feldspar porphyry
- AND Andesite

CRETACEOUS

- QZMZ Quartz monzonite

LATE TRIASSIC

- BNT GNT Bennett granite

094028

DwG 6

MAP 5

AMEROK GEOSCIENCES LTD.

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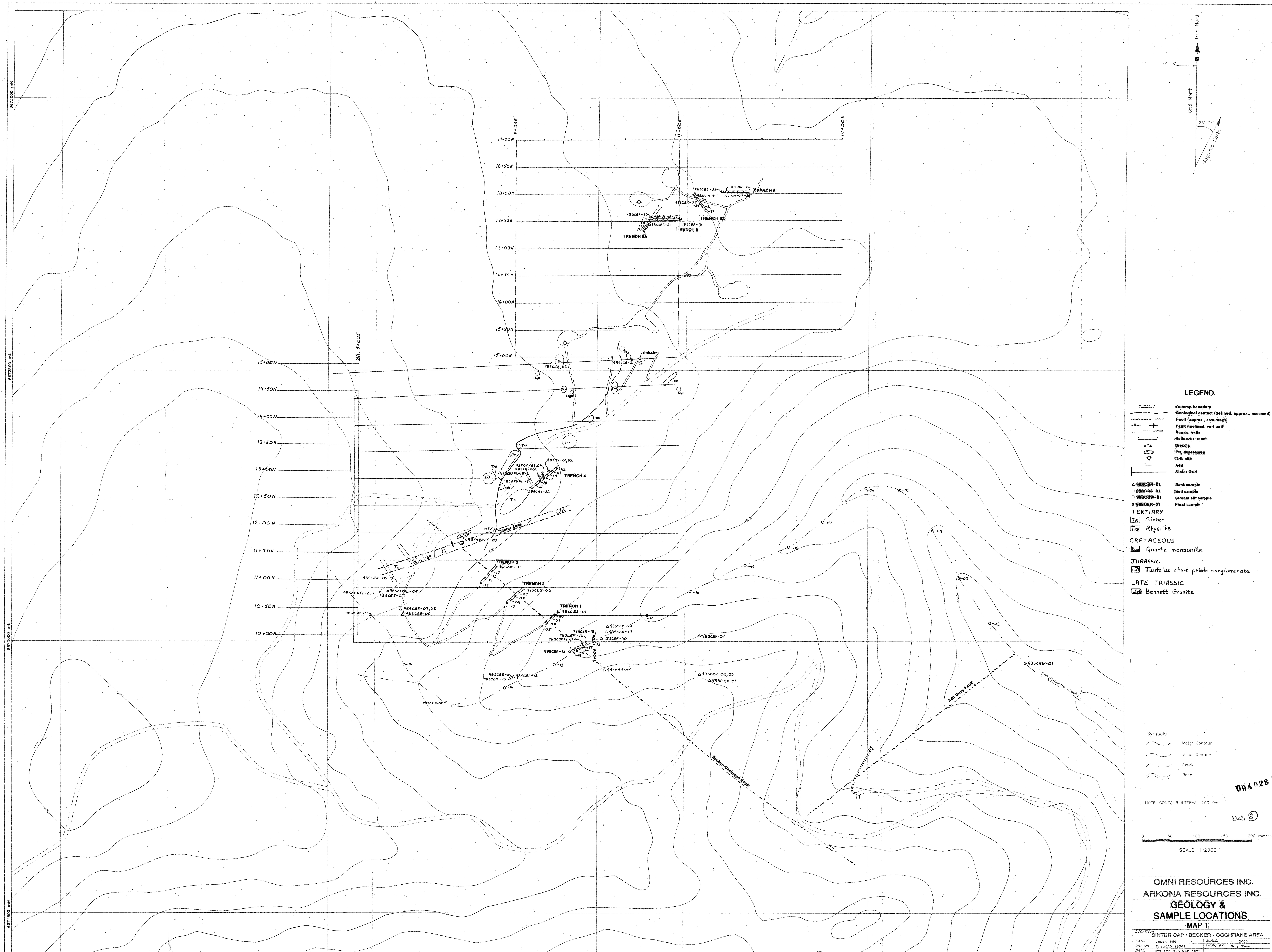

OMNI RESOURCES INC.
ARKONA RESOURCES INC.

GEOLOGY & SAMPLE LOCATIONS

MAP 1

LOCATION:	SINTER CAP / BECKER - COCHRANE AREA		
DATE:	January 1999	SCALE:	1 : 2000
DRAWN:	TerraCAD 98369	WORK BY:	Gary Wesa
DATA:	NTS 105 D/3 NAD 1927		

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OMNI RESOURCES INC.
ARKONA RESOURCES INC.
SOIL GEOCHEMISTRY
SINTER GRID
MAP 2
SINTER CAP / BECKER - COCHRANE AREA
SCALE: 1:2000
NOTE: CONTOUR INTERVAL 100 feet
DWG 3
094028
LEGEND
18 Gold in ppb.
687 Silver in ppb.
Symbols
Major Contour
Minor Contour
Creek
Road
True North
Grid North
Magnetic North
0° 13'
26° 24'
0 50 100 150 200 metres
1900N
1800N
1700N
1600N
1500N
1400N
1300N
1200N
1100N
1000N
BASELINE 500E
TIE LINE 800E
TIE LINE 1100E
1400E
Conglomerate Creek
6673000 mN
6672500 mN
6672000 mN
6671500 mN
486500 mE
487000 mE
487500 mE
488000 mE
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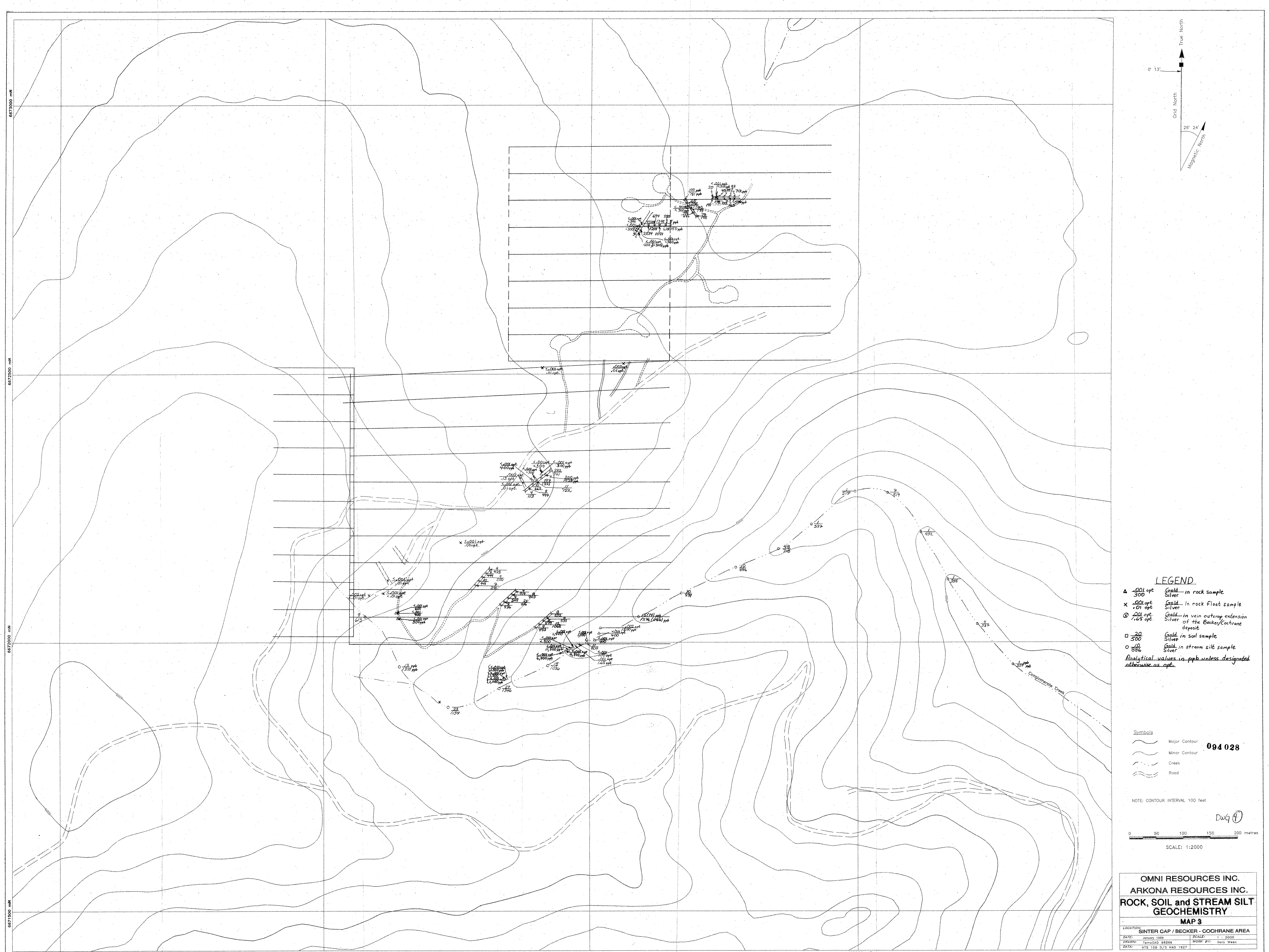

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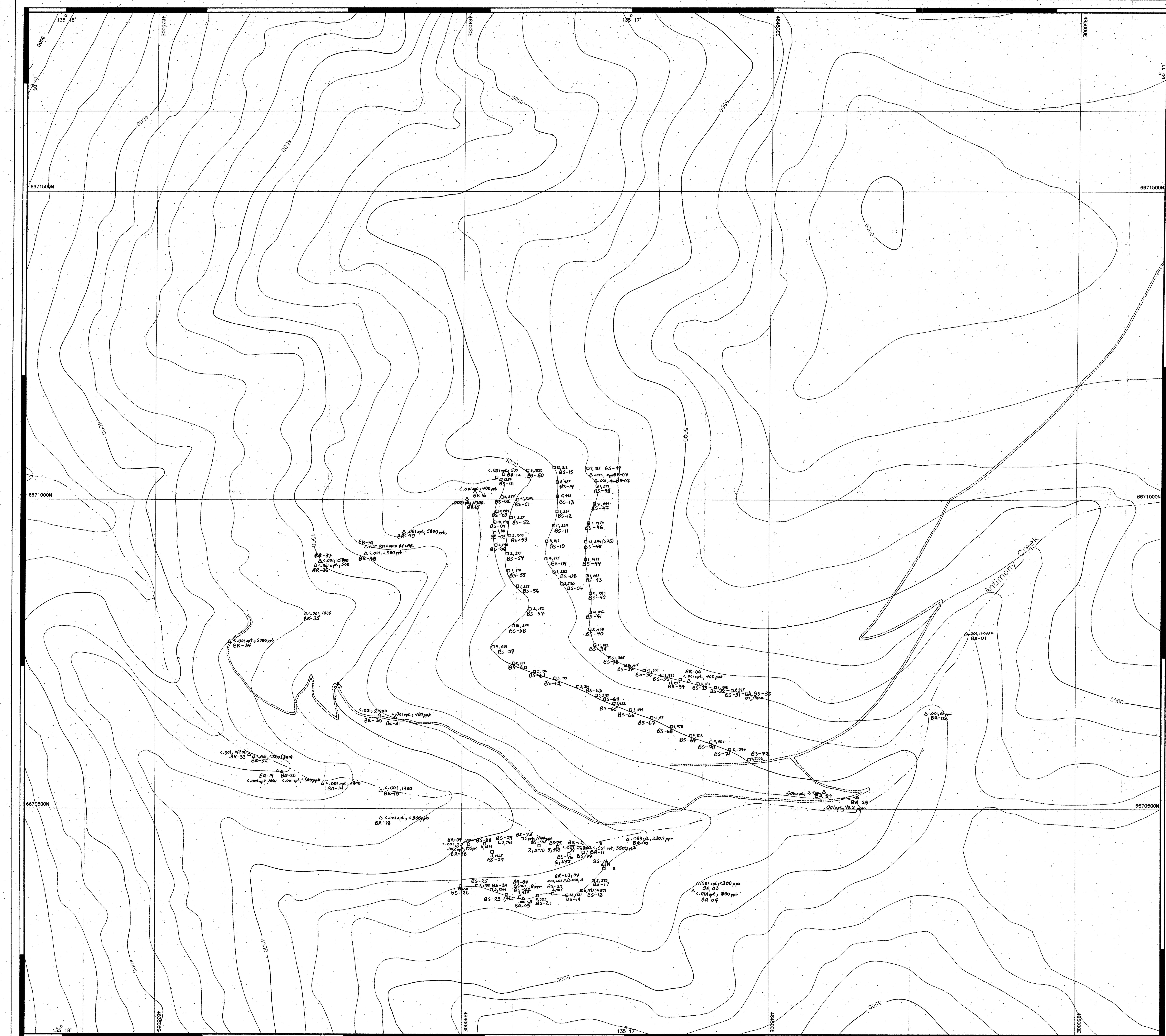

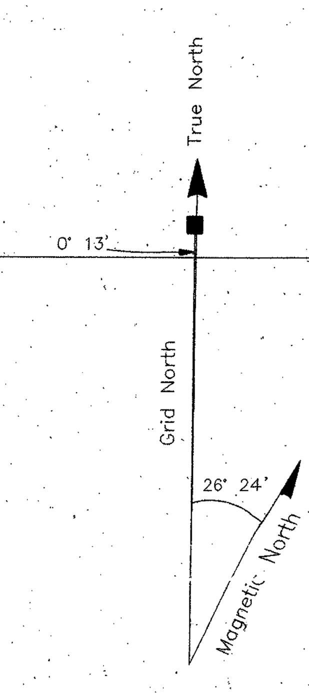

LEGEND

△ .001, 300 Gold in opt., Silver in ppb. in ROCK unless otherwise noted

□ 5, 267 Gold in ppb., Silver in ppb in SOIL or TALUS FINES unless otherwise noted

Symbols

Major Contour

Minor Contour

Creek

094028

NOTE: CONTOUR INTERVAL 100 feet

0 50 100 150 200 metres

SCALE: 1:2000

Dwg (5)

OMNI RESOURCES INC. ARKONA RESOURCES INC.			
SAMPLE LOCATIONS WITH ROCK AND SOIL or TALUS FINES GEOCHEMISTRY			
MAP 4			
LOCATION: ANTIMONY CREEK AREA			
DATE:	January 1999	SCALE:	1 : 2000
DRAWN:	TerraCAD 98369-2	WORK BY:	Gary Wesa
DATA:	NTS 105 D/3 NAD 1927		

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105D-3
QUARTZ & PLACER
LATITUDE 60 00 60 15
LONGITUDE 135 00 135 30
ISSUED UNDER THE AUTHORITY OF THE MINISTER
OF
INDIAN AFFAIRS AND NORTHERN DEVELOPMENT
SCALE 1:31,680
METRES
FEET
N
MAGNETIC NORTH
N29 35 E
20'
135 15'
10'
Summit Creek
Wheaton
Fenwick
Carbon Hill
MT. BELL
MOUNT ANDERSON
Johnson Hill
Dawson Cr
MIL
POP
STEN
DG
MOM
BERG
TECH
BANK
RIDGE
NICK
MTA
ORDER
TAS
CW
CHIEF
GLEE
OMNI RESOURCES INC.
ARKONA RESOURCES INC.
VANCOUVER, BRITISH COLUMBIA
GODDELL/CARBON HILL PROJECT
CLAIM MAP
FIGURE 2
NTS Ref: 105D/3
REVISIONS
Work by: G. WESA
Work by:
Drawn by:
Drawn by:
Date: JANUARY, 1999
Date:
Scale:
G.L. WESA
GEOLOGICAL ASSOCIATION OF CANADA
FELLOW
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