

093739

**GEOPHYSICAL, GEOCHEMICAL, TRENCHING
AND PROSPECTING REPORT ON
THE WATSON PROPERTY**

**Liard 1-26 (YB78363-388), Watson 1-30 (YB78389-418), Steph 1-6
(YB84651-656), Lee 1-10 (YB77736-745), & Luck 1-10 (YB77746-755)**

Watson Lake Mining District
Watson Lake, Yukon

NTS 105A/2
60°01' N latitude, 128°38' W longitude

for KRL Resources Corp.

Work performed between March - October, 1996

R. Chow
March 5, 1997

This report has been examined by
the Geological Evaluation Unit
under Section 53 (4) Yukon Quartz
Mining Act and is allowed as
representation work in the amount
of \$ 12,000.00.

M. B. B.

for Regional Manager, Exploration and
Geological Services for Commissioner
of Yukon Territory.

YUKON ASSESSMENT REPORT
REQUIRED INFORMATION

093739

PROPERTY: WATSON

NTS MAP SHEET: 105A/2

LATITUDE: 60°01' N

LONGITUDE: 128°38' W

CLAIMS AND GRANT NUMBERS:

LIARD 1-26	YB78363 - YB78388
WATSON 1-30	YB78389 - YB78418
STEPH 1-6	YB84651 - YB84656
LEE 1-10	YB77736 - YB77745
LUCK 1-10	YB77746 - YB77755

OWNER OF PROPERTY: KRL RESOURCES CORP.

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OPERATOR: KRL RESOURCES CORP.

TYPE OF WORK: GEOPHYSICAL, GEOCHEMICAL, TRENCHING, PROSPECTING

DATES WORK WAS DONE: MARCH - OCTOBER, 1996

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CONTRACTORS - TERRAQUEST LTD., D.J. DRILLING CO. LTD.



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INTRODUCTION

Between March and October of 1996, KRL Resources Corp. carried out an exploration program on the Watson Property near the Liard Canyon, consisting of airborne and ground geophysics, soil geochemical sampling, trenching, and minor prospecting. The purpose of this program was to explore for sedex type massive sulphide mineralization. Past exploration by other owners has located a barite and a lead-zinc-silver showing on the property.

The property straddles the Yukon-B.C. border, but for the purposes of this report, only work performed on the claims within the Yukon will be reported. Discussions will however include results from both sides of the border in order to understand the broader geologic context.

Location and Access

The claims are located on both sides of the Liard River, on the north side of the Yukon - British Columbia border, about 8 air km southeast of the town of Watson Lake, YT [Figure 1]. The centre of the claim ground lies at 60°01'00" N. latitude, 128°37'45" W. longitude on mapsheet 105A/2 in the Watson Lake Mining District.

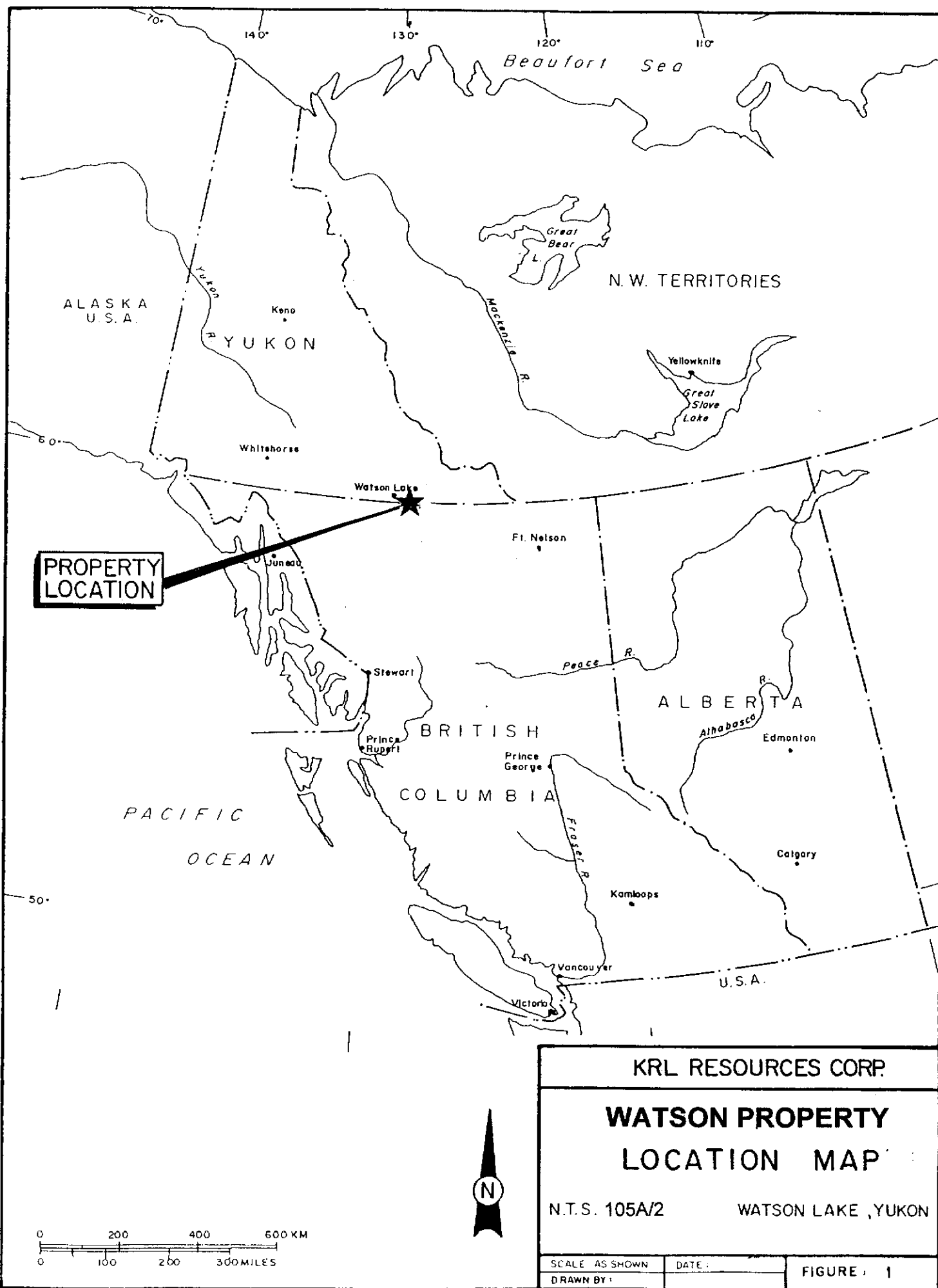
Several access options are available. Helicopter out of Watson Lake takes about 5 minutes, with 2 helipad locations on the property. Road access is available by a 4X4 road from Upper Liard along the south side of the Liard River. The Alaska Highway passes through the northeast corner of the property. The claims can also be reached by boat from Upper Liard along the Liard River, which flows southeasterly through the property.

Physiography / Climate

The claims lie within the Liard Plains, a broad, low lying and relatively flat region through which the Liard River flows. Elevations on the property range from 2000 ft. to 2400 ft. The steep walls of the Liard Canyon are exposed for a distance of 2.5 km on the east side of the property. Elsewhere, the terrain is gentle with low sand and gravel terraces flanking the river. Much of the property is covered by glacial deposits of silt, sand and gravel up to 50 m thick, producing a hummocky terrain. These deposits are classified as glaciofluvial and glaciolacustrine in origin, while the terraces adjacent the river are classified as modern alluvial terraces.

Vegetation is light to moderately dense, consisting of mainly jack pine, spruce, and poplar, and various deciduous trees. Underbrush consists of willow and labrador tea.

The climate is typical of northern continental regions, with long cold winters and short warm summers. Temperatures range from about -25° in January to +15° C in July. Total annual snowfall averages 219 cm. Exploration can be carried out from May to October.



Property Status

The Watson Property consists of 84 claims covering an area of approximately 4203 acres (1701 hectares) in the Watson Lake Mining District. The Luck and Lee claims (20 units in total) are optioned from Nu-Lite Industries Ltd. The claims are listed below in Table 1 and illustrated in Figure 2.

Table 1: Watson-Liard Claims

Claim Name	Tenure #	Record Date	Expiry Date	Claim Owner
Lee 1	YB 77736	96 Feb 26	97 Feb 26	Nu-Lite
Lee 2	YB 77737	96 Feb 26	97 Feb 26	Nu-Lite
Lee 3	YB 77738	96 Feb 26	97 Feb 26	Nu-Lite
Lee 4	YB 77739	96 Feb 26	97 Feb 26	Nu-Lite
Lee 5	YB 77740	96 Feb 26	97 Feb 26	Nu-Lite
Lee 6	YB 77741	96 Feb 26	97 Feb 26	Nu-Lite
Lee 7	YB 77742	96 Feb 26	97 Feb 26	Nu-Lite
Lee 8	YB 77743	96 Feb 26	97 Feb 26	Nu-Lite
Lee 9	YB 77744	96 Feb 26	97 Feb 26	Nu-Lite
Lee 10	YB 77745	96 Feb 26	97 Feb 26	Nu-Lite
Luck 1	YB 77746	96 Feb 26	97 Feb 26	Nu-Lite
Luck 2	YB 77747	96 Feb 26	97 Feb 26	Nu-Lite
Luck 3	YB 77748	96 Feb 26	97 Feb 26	Nu-Lite
Luck 4	YB 77749	96 Feb 26	97 Feb 26	Nu-Lite
Luck 5	YB 77750	96 Feb 26	97 Feb 26	Nu-Lite
Luck 6	YB 77751	96 Feb 26	97 Feb 26	Nu-Lite
Luck 7	YB 77752	96 Feb 26	97 Feb 26	Nu-Lite
Luck 8	YB 77753	96 Feb 26	97 Feb 26	Nu-Lite
Luck 9	YB 77754	96 Feb 26	97 Feb 26	Nu-Lite
Luck 10	YB 77755	96 Feb 26	97 Feb 26	Nu-Lite
Liard 1	YB 78363	96 Mar 03	97 Mar 04	Tim Young
Liard 2	YB 78364	96 Mar 03	97 Mar 04	Tim Young
Liard 3	YB 78365	96 Mar 03	97 Mar 04	Tim Young
Liard 4	YB 78366	96 Mar 03	97 Mar 04	Tim Young
Liard 5	YB 78367	96 Mar 03	97 Mar 04	Tim Young
Liard 6	YB 78368	96 Mar 03	97 Mar 04	Tim Young
Liard 7	YB 78369	96 Mar 03	97 Mar 04	Tim Young
Liard 8	YB 78370	96 Mar 03	97 Mar 04	Tim Young
Liard 9	YB 78371	96 Mar 03	97 Mar 04	Tim Young
Liard 10	YB 78372	96 Mar 03	97 Mar 04	Tim Young
Liard 11	YB 78373	96 Mar 03	97 Mar 04	Tim Young
Liard 12	YB 78374	96 Mar 03	97 Mar 04	Tim Young
Liard 13	YB 78375	96 Mar 03	97 Mar 04	Tim Young
Liard 14	YB 78376	96 Mar 03	97 Mar 04	Tim Young
Liard 15	YB 78377	96 Mar 03	97 Mar 04	Tim Young
Liard 16	YB 78378	96 Mar 03	97 Mar 04	Tim Young
Liard 17	YB 78379	96 Mar 03	97 Mar 04	Tim Young
Liard 18	YB 78380	96 Mar 03	97 Mar 04	Tim Young
Liard 19	YB 78381	96 Mar 03	97 Mar 04	Tim Young
Liard 20	YB 78382	96 Mar 03	97 Mar 04	Tim Young
Liard 21	YB 78383	96 Mar 03	97 Mar 04	Tim Young

Liard 22	YB 78384	96 Mar 03	97 Mar 04	Tim Young
Liard 23	YB 78385	96 Mar 03	97 Mar 04	Tim Young
Liard 24	YB 78386	96 Mar 03	97 Mar 04	Tim Young
Liard 25	YB 78387	96 Mar 03	97 Mar 04	Tim Young
Liard 26	YB 78388	96 Mar 03	97 Mar 04	Tim Young
Liard 27	YB 79253	96 Mar 07	97 Mar 08	Jim Donaldson
Liard 28	YB 79254	96 Mar 07	97 Mar 08	Jim Donaldson
Watson 1	YB 78389	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 2	YB 78390	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 3	YB 78391	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 4	YB 78392	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 5	YB 78393	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 6	YB 78394	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 7	YB 78395	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 8	YB 78396	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 9	YB 78397	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 10	YB 78398	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 11	YB 78399	96 Mar 03	97 Mar 04	Tim Young
Watson 12	YB 78400	96 Mar 03	97 Mar 04	Tim Young
Watson 13	YB 78401	96 Mar 03	97 Mar 04	Tim Young
Watson 14	YB 78402	96 Mar 03	97 Mar 04	Tim Young
Watson 15	YB 78403	96 Mar 03	97 Mar 04	Tim Young
Watson 16	YB 78404	96 Mar 03	97 Mar 04	Tim Young
Watson 17	YB 78405	96 Mar 03	97 Mar 04	Tim Young
Watson 18	YB 78406	96 Mar 03	97 Mar 04	Tim Young
Watson 19	YB 78407	96 Mar 03	97 Mar 04	Tim Young
Watson 20	YB 78408	96 Mar 03	97 Mar 04	Tim Young
Watson 21	YB 78409	96 Mar 03	97 Mar 04	Tim Young
Watson 22	YB 78410	96 Mar 03	97 Mar 04	Tim Young
Watson 23	YB 78411	96 Mar 03	97 Mar 04	Tim Young
Watson 24	YB 78412	96 Mar 03	97 Mar 04	Tim Young
Watson 25	YB 78413	96 Mar 03	97 Mar 04	Tim Young
Watson 26	YB 78414	96 Mar 03	97 Mar 04	Tim Young
Watson 27	YB 78415	96 Mar 03	97 Mar 04	Tim Young
Watson 28	YB 78416	96 Mar 03	97 Mar 04	Tim Young
Watson 29	YB 78417	96 Mar 03	97 Mar 04	Jim Donaldson
Watson 30	YB 78418	96 Mar 03	97 Mar 04	Jim Donaldson
Steph 1	YB 84651	96 Jul 02	97 Jul 02	Tim Young
Steph 2	YB 84652	96 Jul 02	97 Jul 02	Tim Young
Steph 3	YB 84653	96 Jul 02	97 Jul 02	Tim Young
Steph 4	YB 84654	96 Jul 02	97 Jul 02	Tim Young
Steph 5	YB 84655	96 Jul 02	97 Jul 02	Tim Young
Steph 6	YB 84656	96 Jul 02	97 Jul 02	Tim Young

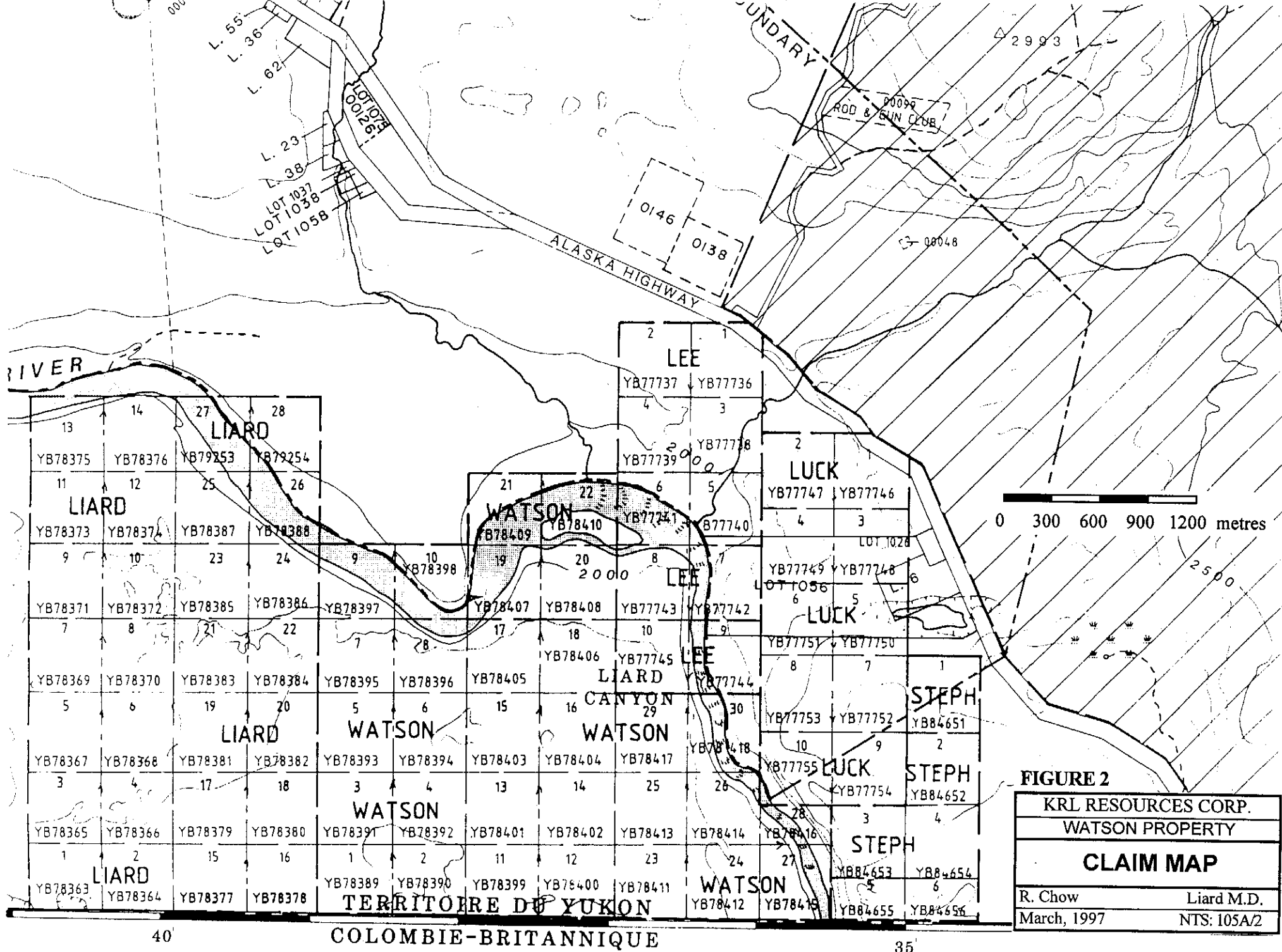


FIGURE 2

KRL RESOURCES CORP.
WATSON PROPERTY

CLAIM MAP

R. Chow
March, 1997

Liard M.D.
NTS: 105A/2

Property History

The following chronology is modified from Rainsford (1984). The earliest reference to exploration in the area was made by G.M. Dawson in 1886, who noted argentiferous galena in the lower Liard Canyon. More recent history includes:

- 1962: The Jim and Moose claims are staked by F. Lutz to cover 2 showings on the Liard River.
- 1965-75: Claims restaked several times under different names. Minor trenching in 1969, 1971 and 1973.
- 1979: The Roman 1-16 claims are staked by Jake Melynychuck and optioned to St. Joseph Exploration. Geological mapping and geochemical soil sampling is performed in the Barite Showing area.
- 1980: Logan Mines optioned the property and diamond drilled 2 holes from one set-up totaling 123.1 m at the Barite Showing. A limited EM-16 survey was performed around the Main Showing.
- 1981: Logan Mines conducted 9.2 km of soil sampling and magnetic surveying in the Barite and Main Showing areas. Detailed geological mapping and sampling of showings are also performed.
- 1984: Billiton Canada Ltd. optioned the property and carried out 65 km of grid linecutting, IP, resistivity, VLF-EM, HLEM, magnetometer and gravity surveys over a major part of the property.
- 1986: Samarkand Resources optioned the property and performed 46 km of line cutting, Genie EM (horizontal loop), VLF-EM and magnetic surveying, and geological mapping.

REGIONAL GEOLOGY AND METALLOGENY

Regional mapping by H. Gabrielse of the McDame (1963) and Watson Lake (1967) map areas have identified predominantly Proterozoic to Mississippian marine sedimentary rocks with some Jurassic to Tertiary intrusions. The geology is not well understood due to the complex tectonic history of the region and the general lack of bedrock exposure in the broad drift covered plains.

The region lies within the Omineca tectonic belt of the Canadian Cordillera, to the east of the Tintina-Northern Rocky Mountain Trench. The tectonic assemblage compilation map by Wheeler and McFeely (1991) shows 3 different assemblages in the Watson Lake area [Figure 3]:

- (1) Cassiar Terrane: Cambrian to Devonian passive continental margin sediments consisting of mainly dolomite, limestone, and shale deposited in platformal and basinal environments; includes the Kechika, Road River, Sandpile, Askin, and McDame Groups. The Cassiar Terrane is considered to be a displaced part of autochthonous North America.
- (2) Earn Group: Devonian to Mississippian fault trough clastic wedge consisting of chert pebble conglomerate, chert quartz sandstone, pebbly mudstone, shale and volcanics.
- (3) Slide Mountain Terrane: Devonian to Triassic oceanic marginal basin volcanics and sediments included in the Sylvester Group, which form a stack of fault-bounded slices emplaced eastward onto the Cassiar Terrane.

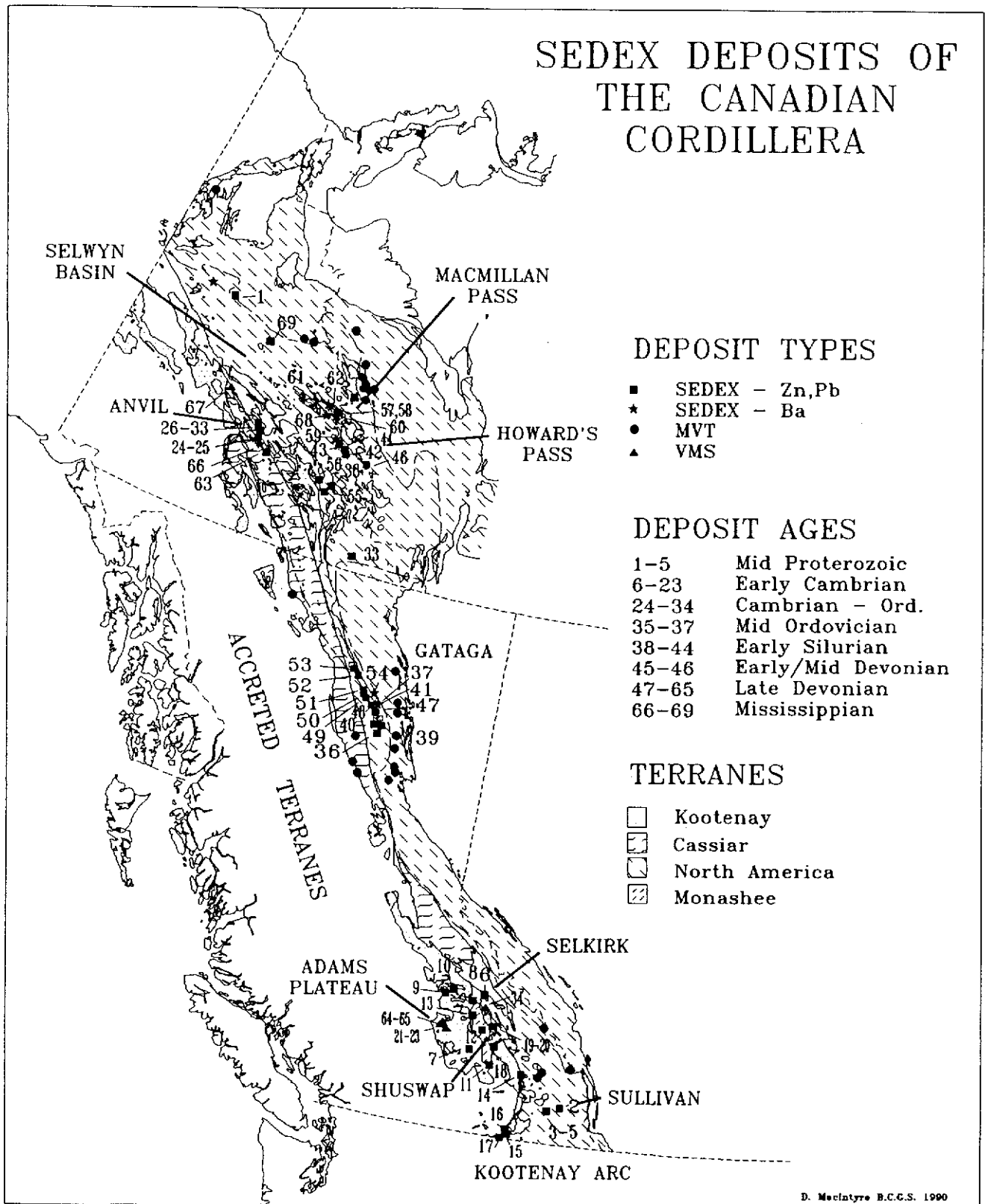
During Early Cambrian to Mid Devonian time, the continental margin of ancestral North America was comprised of a series of rift-controlled basins, of which the Selwyn Basin in the Yukon was the largest. The Cassiar Terrane is believed to be a fragment of the continental margin which moved north along the Tintina-Northern Rocky Mountain fault during Late Mesozoic to early Tertiary time. Another major rifting event during mid-Devonian to Early Mississippian produced basin sedimentation, including the Earn Group, which was deposited in local fault-bounded basins or rift troughs on the outer edge of the Selwyn Basin. The Slide Mountain Terrane in the Cassiar region is comprised of Sylvester Group oceanic marginal basin volcanics and sediments formed in Devonian to Upper Triassic time and thrust eastward onto the North American margin as a series of fault-bounded slices during Early to Mid-Jurassic.

Proterozoic and Paleozoic basinal and platformal marine sedimentary rocks are important hosts of sedimentary exhalative lead-zinc-silver deposits worldwide and within the Canadian Cordillera [Figure 4]. Some major producers include the Sullivan mine in southeast British Columbia and Faro in the Yukon. Other important occurrences include deposits of the Anvil, Howard's Pass and MacMillan Pass districts in the Yukon, and the Cirque deposit in northeast British Columbia (MacIntyre, 1991). All major sedex deposits known in the Cordillera occur in rocks of ancestral North America, hosted within intracratonic basins and miogeoclinal. The most economically important sedex deposits are found in the Selwyn and Purcell basins and in platformal sequences of the Cassiar Terrane and equivalents to the west.

The Earn Group is host to some of the largest sedex deposits including the Tom and Jason of the Macmillan Pass district and the Cirque of the Gataga district. The lower Earn is distinguished regionally by its blue weathering siliceous shale and chert and the upper Earn by mainly brown weathering shale (not highly siliceous) and common bedded chert (Gordy et al., 1982). Coarse clastics consisting of chert pebble conglomerate, quartz-chert sandstone, and conglomeratic mudstone are found in both Upper and Lower Earn groups. Bedded barite occurs within the siliceous shale facies of the lower and possibly upper Earn Group at MacMillan Pass, and sedex zinc-lead-silver-barite deposits occur within clastic facies of the lower Earn Group.

The Road River Group which underlies the Earn Group is also host to several mid-Ordovician to mid-Devonian deposits including Howard's Pass and the Aikie. Black graptolitic mudstone and chert of the Road River Group was deposited throughout the Selwyn Basin and Kechika Trough during mid to late Ordovician time in response to a major marine transgression.

SEDEX DEPOSITS OF THE CANADIAN CORDILLERA



D. MacIntyre B.C.G.S. 1990

Figure 4: Location of sedimentary exhalative deposits in the Canadian Cordillera. Numbers refer to deposits listed in Table 2. (From MacIntyre, 1991)

Table 2: Cambrian to Mississippian sedimentary exhalative deposits. (From MacIntyre, 1991)

Map No.	Terrane	Tectonic Element	Dep. Type	Deposit Name	Commodity	Million Tonnes	Zn %	Pb %	Cu %	Ag g/t	Au g/t	Host Rocks
Early Cambrian												
6	KO	Selkirk Allochthon	1B	Rift	Zn,Pb,(Cu)							Hamill or Lardeau?
7	KO	Shuswap Complex	1B	Kingfisher Creek	Zn,Ag,Pb,(Cu,F)							paragneiss
8	KO	Shuswap Complex	1B	Ruddock Creek	Zn,Pb,Ag,(F,Ba)	5	7.5	2.5				paragneiss
9	KO	Shuswap Complex	1B	CK	Pb,Zn,Ag,(Cu,Au)	.5-1	15	3				paragneiss
10	KO	Shuswap Complex	1B	Summit	Zn,Pb,Ag,Cu							paragneiss
11	MO	Monashee Complex	1B	Big Ledge	Zn	6.5	4					paragneiss
12	MO	Monashee Complex	1B	Jordan River	Zn,Pb,Ag,(Ba,F)	2.61	5.6	5.1		35		paragneiss
13	MO	Monashee Complex	1B	Cottonbelt	Pb,Zn,Ag	.8	2	6		50		paragneiss
14	KO	Kootenay Arc	1C	Duncan	Pb,Zn	2.76	3.1	3.3				Badshot limestone
15	KO	Kootenay Arc	1C	Jersey	Zn,Pb,Ag,(Cd);W	7.68 P	3.49	1.65		3.08		Reeves limestone
16	KO	Kootenay Arc	1C	HB	Zn,Pb,Ag,(Au)	6.45 P	4.1	.77		4.8	002	Reeves limestone
17	KO	Kootenay Arc	1C	Reeves-MacDonald	Zn,Pb,Ag,(Cu,Cd, Ga,Ge)	5.8 P	3.42	0.98		3.4		Reeves limestone
18	KO	Kootenay Arc	1C	Wigwam	Zn,Pb,(Au,F)	8.48	3.54	2.14				Badshot limestone
19	KO	Kootenay Arc	1C	J & L	Zn,Pb,Ag,(Au)	4.77	4.3	2.70		72	7.2	Hamill Group
20	KO	Kootenay Arc	1C	Mastodon	Zn,Pb,Ag	.029 P	9.25	0.28		6.56		Badshot limestone
21	KO	Adams Plateau	2	Mosquito King	Pb,Zn,Ag							Eagle Bay
22	KO	Adams Plateau	2	Lucky Coon	Pb,Zn,Ag							Eagle Bay
23	KO	Adams Plateau	2	Twin Mountain	Pb,Zn,Ag,(Cu,Au)							Eagle Bay
Cambrian-Ordovician												
24	CA	Cassiar Platform	1A	Sunset (Lower)	Pb,Zn,Ag							Kechika
25	CA	Cassiar Platform	1A	JA	Pb,Zn,Ag							Kechika
26	NA	Selwyn Basin	1A	Swim	Zn,Pb,Ag	4.3	4.7	3.8		42		Mt. Mye graph. phyllite
27	NA	Selwyn Basin	1A	Grum	Zn,Pb,Ag,(Cu, Ba)	30.8	4.9	3.1		49		Mt. Mye graph. phyllite
28	NA	Selwyn Basin	1A	Dy	Zn,Pb,Ag,Cu,Au, Ba	21.1	6.7	5.5	0.12	84	0.95	Mt. Mye graph. phyllite
29	NA	Selwyn Basin	1A	Vangorda	Zn,Pb,Ag,Au,(Cu, Ba)	7.1	4.3	3.4		48		Mt. Mye graph. phyllite
30	NA	Selwyn Basin	1A	Faro	Zn,Pb,Ag,(Cu,Ba)	57.6	4.7	3.4		36		Mt. Mye graph. phyllite
31	NA	Selwyn Basin	1A	SB	Cu,Zn							Mt. Mye graph. phyllite
32	NA	Selwyn Basin	1A	Sea	Cu,Zn							Mt. Mye graph. phyllite
33	NA	Selwyn Basin	1A	Mel	Zn,Pb,Ba	4.8	5.61	2.05				Mt. Mye graph. phyllite
34	KO	Selkirk Allochthon	2	Goldstream	Cu,Zn,Ag	3.175	3.123		4.49	20		Kechika limestone, shale Lardeau

Deposit Types: 1A — clastic hosted SEDEX; 1A1 — bedded barite; 1A2 — mainly feeder zone mineralization; 1B — clastic carbonate hosted SEDEX; 2 — volcanic sediment hosted; Terranes: NA — North America; KO — Kootenay; CA — Cassiar; MO — Monashee; P — tonnage based on production; other tonnage figures reserves plus production.

Table 2 (con't)

Map No.	Terrane	Tectonic Element	Dep. Type	Deposit Name	Commodity	Million Tonnes	Zn %	Pb %	Cu %	Ag g/t	Au g/t	Host Rocks
Middle Ordovician												
35	CA	Cassiar Platform	1A	JA (Upper)	Pb,Zn,Ag							Road River shale
36	NA	Kechika Trough	1A	Reb	Fe,(Zn)							Road River shale
37	NA	Kechika Trough	1A1	Aikie-Sika	Ba							Road River shale
Early Silurian												
38	NA	Selwyn Basin	1A	Maxi	Zn,Pb,(Ag)							Road River
39	NA	Kechika Trough	1B	CT	Ba,Zn,(Pb)							Road River Ist. dol.,chert
40	NA	Kechika Trough	1B	Ern	Zn,Ba							Road River Ist. dol.,chert
41	NA	Kechika Trough	1B1	Aikie-Sika	Ba							Road River Ist. dol.,chert
42	NA	Selwyn Basin	1B	Howard's Pass (XY)	Zn,Pb	125	5.4	2.1				Road River Ist. dol.,chert
43	NA	Selwyn Basin	1B	Grand (Nor)	Pb,Zn							Road River Ist. dol.,chert
44	NA	Selwyn Basin	1B	Anniv	Zn,Pb							Road River Ist. dol.,chert
Early-Middle Devonian												
45	CA	Cassiar Platform	1A	Angie	Zn,Ag							Road River shale
46	NA	Selwyn Basin	1B	Vulcan	Zn,Pb,Ba, (Ag, F, Cu)							Road River shale
Late Devonian — Mississippian												
47	NA	Kechika Trough	1A	Elf	Pb,Zn,Ag,Ba							Lower Earn ch. arg., shale
48	NA	Kechika Trough	1A	Fluke	Pb,Zn,Ag,Ba							Lower Earn ch. arg., shale
49	NA	Kechika Trough	1A	Pie	Pb,Zn,Ag,Ba							Lower Earn ch. arg., shale
50	NA	Kechika Trough	1A	Cirque	Zn,Pb,Ag,Ba	32.2	7.9	2.1		48		Lower Earn ch. arg., shale
51	NA	Kechika Trough	1A	Mount Alcock	Zn,Pb,Ag,Ba							Lower Earn ch. arg., shale
52	NA	Kechika Trough	1A	Bear	Pb,Zn,Ag,Ba		10	5.7		52		Lower Earn ch. arg., shale
53	NA	Kechika Trough	1A	Driftpile Creek	Pb,Zn,Ba							Lower Earn ch. arg., shale
54	NA	Kechika Trough	1A1	Kwadacha	Ba							Lower Earn ch. arg., shale
55	NA	Selwyn Basin	1A	Matt Berry	Pb,Zn,Ag,Sb	0.5	4.6	6.1		105		Lower Earn
56	NA	Selwyn Basin	1A	Fin	Pb,Zn,Ag							Lower Earn
57	NA	Selwyn Basin	1A	Torn (E & W)	Zn,Pb,Ag,Ba	15.7	7.0	4.6		49.1		Lower Earn
58	NA	Selwyn Basin	1A	Jason (Main,S,End)	Pb,Zn,Ag,Ba	15.5	6.6	7.1		79		Lower Earn
59	NA	Selwyn Basin	1A1	Oro	Ba							Lower Earn
60	NA	Selwyn Basin	1A1	Moose	Ba							Lower Earn
61	NA	Selwyn Basin	1A1	Cathy	Ba							Lower Earn
62	NA	Selwyn Basin	1A2	Nidd	Zn,(Pb)							Lower Earn
63	CA	Cassiar Platform	2	Clear Lake	Zn,Pb,Ag,(Ba)							Lower Earn
64	KO	Adams Plateau	2	Homestake	Ag,Zn,Pb,Cu, Ba,(Au)	1.01	4	2.5	0.6	248	0.68	Eagle Bay metavolc., phyl.
65	KO	Adams Plateau	2	Rea	Zn,Pb,Cu,Ag, Au	0.24	2.3	2.1	0.5	75	6.8	Eagle Bay metavolc., phyl.
Mississippian												
66	CA	Cassiar Platform	1A	GK, Dirck	Ba							Upper Earn turbidites
67	CA	Cassiar Platform	2	MM	Pb,Zn,Ag							Upper Earn shale, volc.
68	NA	Selwyn Basin	1A1	Tea	Ba							Upper Earn turbidites
69	NA	Selwyn Basin	2	Marg		1.92	5.19	2.72	1.97	67	1.02	Upper Earn shale, volc.

Deposit Types: 1A — clastic hosted SEDEX; 1A1 — bedded barite; 1A2 — mainly feeder zone mineralization; 1B — clastic-carbonate hosted SEDEX; 2 — volcanic sediment hosted; Terranes: NA — North America; KO — Kootenay; CA — Cassiar; MO — Monashee; Tonnages reserves plus production

PROPERTY GEOLOGY & MINERALIZATION

Bedrock exposure on the property is limited to shorelines and in the Liard Canyon, where beds of predominantly shale, argillite, slate, mudstone, and sandstone are well exposed along the steep canyon walls. Outcrops along the canyon on the BC side of the border were first mapped as Sylvester Group by Gabrielse (1963) and described as being similar to the limestone-quartzite-siltstone-slate sequence on the Alaska Highway. The same outcrop in the canyon on the adjoining mapsheet to the north was subsequently mapped by Gabrielse (1967) as Cambro-Ordovician dark grey and black, non-calcareous argillite, slate, and phyllite. Recent mapping by the B.C. Geological Survey has identified Devonian-Mississippian age Earn Group strata in the Liard Canyon and an overlying chert unit of possible Mississippian-Permian age (Ferri et al., 1997).

Previous mapping of the property geology was performed by T. Scott of Samarkand Resources in 1986, as well as detailed mapping of the Barite Showing by St. Joseph Explorations Ltd. in 1979 and the Main Showing just south of the border by Logan Mines Ltd. in 1981. Available reports on property geology are summarized from D.G. Mark (1988), V. Cukor (1981), and D. Rainsford (1984).

At the Barite Showing (also referred to as the West Showing) located in the north central part of the property [Figure 24], carbonaceous black shales with calcareous and siliceous beds, and minor carbonaceous sandstone units are present. A 2 m wide conformable barite lense and a 0.4 m wide cross-cutting barite vein are found in black shales on the south bank of the river. Isolated patches of base metal and silver mineralization is reported within the barite. As well, pyrite occurs as a bedded horizon in excess of 20 m thick within shales and in quartz-barite cemented breccia zones. On the north bank, numerous barite-quartz lenses and veins up to 20 cm wide are also found in black shales.

In the Liard Canyon, rocks are described as intercalated black shale and buff-weathering, phyllitic, grey calcareous mudstone. Half way along the canyon, mudstone with a distinctive ochre to brown weathering is present.

Further south along the river on the B.C. side of the border, in the vicinity of the Main Showing, units of phyllite, sandstone with quartzite, and black shale have been described. The showing is located on the south bank and consists of lenses of massive, very fine-grained galena and sphalerite, hosted in grey calcareous mudstones. The lenses are 20 cm wide, and exposed above the river for about 10 m in length. A typical assay from these lenses is 8.94 oz/ton Ag, 46.3% Pb, 22.6% Zn. About 100 m east, a zone of silicification at the contact between shales and quartzite contains patches of galena, sphalerite, and tetrahedrite. A channel sample across 0.6 m from this zone returned values of 9.1 oz/ton Ag, 0.2% Cu, 24.95% Pb, and 2.23% Zn. On the north shore opposite the Main Showing, a 15 m thick unit of chert and calcareous grit occur at a shale-sandstone interface. The grit contains rounded chert pebbles and elongate shale clasts in a sandy matrix. Quartz lenses and crossfractures in phyllite are mineralized with argentiferous galena, locally with tetrahedrite.

Mineralization observed elsewhere on the property include traces of galena, sphalerite, chalcopyrite and tetrahedrite, associated with narrow quartz veins and quartz stockwork. These veins generally strike east to northeast and dip steeply, or are concordant with bedding.

A zone of intense, upright folding is coincident with the Liard River canyon. These folds are described as trending south-southeast and plunging gently north. Bedding is generally steep and parallels the canyon walls. West of the canyon, beds dip gently to steeply southwest. Normal faults with minor displacements were observed, as well as some intense fracturing.

Minor intrusive rocks on the property include andesitic dykes, 1 to 5 m wide, striking sub-parallel to the shales at the west end of the Liard Canyon.

GEOPHYSICS

Airborne Survey

During March of 1996, an airborne high sensitivity magnetic and VLF-EM survey was conducted over property by Terraquest Ltd. on behalf of KRL Resources Corp. A total of 177 line km were flown with lines spaced 200 m apart. Numerous narrow north-northwest trending magnetic horizons were identified. Structures representing faults, shear zones, or tight fold axes strike predominantly at 60°, with a few younger, more continuous structures at 20°. Several conductive zones were identified from the VLF-EM data, while overall subdued responses in the central part of the survey area were interpreted to be due to overburden. Refer to Appendix A for the full report by Terraquest.

Ground Survey

Three days were spent conducting a ground geophysical survey consisting of 26.7 km of magnetometer and VLF-EM on the grid area [Figure 24]. A Scintrex IGS-2 (Integrated Geophysical System) field unit and a Scintrex MP-3 magnetic base station recorder were used to conduct the survey. The survey consisted of measurements of the total magnetic field and the induced electromagnetic field due to two VLF-EM transmitter stations. The stations are located at Cutler, Maine and Annapolis, Maryland with frequencies of 24.0 kHz and 21.4 kHz respectively. Instrument accuracies were 0.1 nT magnetically and plus-minus 0.5% of the measured vertical in-phase and out-phase secondary electromagnetic VLF fields.

Survey lines were oriented at 090°, spaced 100 m apart, with readings taken at 25 m intervals. At the end of survey day, the digitally recorded data was downloaded onto a computer and subsequently saved onto floppy diskettes.

Data Presentation

The field data was processed by Fred Syberg, Geophysicist, Vancouver, B.C. Field data was first corrected for diurnal variations in the total magnetic field and calculation of dip angles and quadrature using methods described in the IGS-2 manual published by Scintrex Ltd. A 12.5 by 12.5 metre grid was superimposed on the survey plan. A grid matrix was interpolated for each survey item by calculating weighted means at matrix nodes within the survey area and using field observations in the neighborhood of the point of interpolation. Each matrix was smoothed according to the analytical results.

The total magnetic field was continued upward 25 metres, which means that a computational application was used to simulate the situation where the magnetic survey had been carried out at 25 metres above ground surface. Such applications tend to suppress the effects due to near-surface erratics and other non-interpretable features.

The VLF-EM dip angles were Fraser Filtered. The filter directions were from south to north along matrix columns for Cutler, and from west to east along matrix rows for Annapolis.

Results are shown in Figures 5 to 10.

Interpretation

The geophysical interpretation by F. Syberg is summarized in Figure 11. Four areas have been identified as exploration targets based on the airborne and ground magnetic and VLF-EM survey results. A strong magnetic high parallel to the canyon in the airborne survey was verified by the ground magnetic survey.

Two strong VLF-EM conductors, striking approximately north-south were identified in the north part of the grid, at line 4500N, 4800E and 4600N, 5400E. The conductors have strike lengths of at least 450 m and 225 m, and coincide with edges of areas denoted as exploration targets.

SOIL GEOCHEMISTRY

A preliminary soil geochemical survey was performed on the grid area in July of 1996. A total of 139 samples were taken at 25 m intervals, along lines spaced 200 m apart. A follow-up detailed soil sampling program, totaling 412 samples from lines spaced 50 m apart attempted to delineate a zone of anomalous gold values. Ten soil profiles were also collected along the axis of the geophysical anomaly, between lines 3250-4150N and 5550-5625E.

Methods

Samples were collected from the "B" horizon by digging a hole with a grub-hoe or round nosed shovel. Soil profiles were taken at selected sites, with samples collected at 15 cm intervals down to a depth of 1 m. The soils were placed in a kraft sample bag, and numbered with the grid coordinate location of the sample. The samples were dried before shipping to Acme Analytical Laboratories Ltd. in Vancouver, B.C. for analysis. A 30 element ICP analysis and a wet geochemical gold extraction was conducted on all soil samples. (See Appendix C for analytical methods).

The geochemical values were obtained on a floppy diskette and prepared for contouring on a computer plotter by Fred Syberg. The data was spatially analyzed spectrally, which led to a direction variable low pass filter. The filtering process suppresses chaotic attributes in the original samples, i.e. improves interpretation. The contour levels were selected on a pseudo-logarithmic scale with respect to the range of values for a specific element. This amounts to choosing contour levels of increasing interval, and results in a contour level interval which approximately increases exponentially as one passes through the original data range. Contours throughout the contour range remain spatially equidistant. (Syberg, 1993).

Results/Interpretation

The preliminary soil survey returned 11 consecutive samples with highly anomalous gold values in the range of 122 to 1421 ppb Au, representing a linear anomaly along line 3800N, between 5475-5725E. Three other isolated samples returned anomalous values of 131 to 275 ppb Au. Silver and base metal values were generally low.

Results from the subsequent detailed soil sampling are shown in Figures 12 to 23. The anomalous gold values from the first survey were unable to be reproduced, with samples from the same site returning only 1 sample with 173 ppb Au, and the other 10 samples with between

<1 to 3 ppb Au. Overall, the highest gold value obtained was 750 ppb, with several other samples between 45-395 ppb Au. An anomalous zone can be discerned adjacent to the canyon on the contour map. Similar patterns are present for Ag, Pb and Zn, although values are generally low.

The grid area is underlain by thick fluvial and glacial sediments, which are the likely source of the anomalous gold values. Surficial geology maps classify the sediments flanking the Liard River as modern alluvial terraces, composed of gravel, sand, and silt on the order of 5 to 20 m in thickness. Further west, ice contact glaciofluvial and glaciolacustrine sediments up to 50 m thick are typical. Stratigraphic studies of the Quaternary sediment record along the Liard River (Klassen, 1978) indicate a succession of fluvial sediments and till, in excess of 50 m thick, which record four major intervals of glaciation and three nonglacial intervals. Soil geochemistry in this area is therefore of limited use, as it provides no information about the underlying bedrock. Adjacent to the canyon however, trenching has revealed overburden as shallow as one metre, which lends the possibility of gold values derived from bedrock through the vegetation, producing a humus layer enriched in gold.

PROSPECTING

Minor prospecting was carried out over 2 days along the Liard Canyon and river banks. A total of 12 samples were collected [Figure 24], of mostly shales, and some quartzite and sandstone. Observed mineralization consists of mostly pyrite within shales and in quartz veins. Values in lead and silver were low, with <3 to 149 ppm Pb (avg. 30 ppm) and <.3 to 1.1 ppm Ag. A few higher values of note include 1089 ppm zinc (avg. 219 ppm) and 453 ppm copper (avg. 65 ppm). Barium reached a high of 5235 ppm, with the other samples between 1-411 ppm. Refer to Appendix B for samples descriptions.

TRENCHING

A program of backhoe trenching was performed over 7 days in October to explore the geophysical and geochemical anomalies. Five trenches had been planned over a cumulative length of 600 m, of which only 150 m were excavated due to the extensive overburden. Approximately 4 km of trail were created to provide access to the trenching sites, of which 1.7 km consisted of widening a preexisting cut line. [See Figure 24].

The details of each trench are as follows:

TR#1: This trench consists of 3 pits over a length of 375 m along the northeast trending axis of a soil gold anomaly and across a ground magnetic anomaly. The southwest pit (L3300 N, 5500 E) encountered 1.5 m of silt, underlain by 1.5 m of stratified till (sand and cobbles), and 4 m of clay. The central pit located at the base of a terrace (L3400 N, 5650 E) consisted entirely of sand to a depth of 6-7 m. At the northeast end towards the river (L3500 N, 5800 E), a 30 m long trench was excavated with bedrock was encountered at a depth of 3-4 m. Shales, phyllite with minor fine disseminated pyrite,

and quartz lenses were observed to a depth of 6 m, before the trench was quickly filled by groundwater.

TR#2: A 30 m long trench was excavated at L3800 N, 5725 E, across a magnetic high and soil gold anomaly. The east end of the trench towards the canyon reached bedrock shales at about 4 m depth, with increasing overburden to the west. Stratified unconsolidated sediments (silt to cobbles) were encountered to a depth of 6 m at the west end of the trench. This trench also filled with water.

TR#3: This trench consists of 2 pits on L4100 N at 5525 E and 5475 E, across a magnetic high. The east pit encountered a dense dark yellow brown pebbly clay sediment (permafrost?) to 5 m depth. The west pit contained glaciofluvial material with sand to cobble sized sediment and some large boulders at depth.

TR#4: This 60 m long trench at L4500 N, 5400 E, was excavated over a coincident magnetic and VLF-EM anomaly. Bedrock was encountered on the east end at under about 1 m of overburden, which gradually thickens to the west. The trench was 2-3 m deep and exposed folded phyllites and argillite with quartz lenses. Quartz-carbonate veinlets and alteration in the argillites was observed. Minor galena was noted in one quartz lense. The phyllites contained rusty laminations, but with no apparent mineralization. Chip samples, 4-5 m wide, were taken along the length of the trench in addition to several selected grab samples.

TR#5: This trench consisted of 3 pits at L4500 N, 4800 E over a coincident magnetic and VLF-EM anomaly. No bedrock was reached, with only sandy sediment to 6 m depth.

All trenches were backfilled upon examination and sampling of bedrock. Samples were analyzed at Acme Analytical Laboratories in Vancouver, which returned low values in lead, zinc, silver, and copper.

DISCUSSION / CONCLUSIONS

The 1996 exploration program on the Watson Property was successful in outlining several magnetic and VLF-EM anomalies which may represent a sulphide source and warrant further testing. The extensive glaciofluvial overburden on the property precludes the use of soil geochemistry and trenching as an exploration tool. Drill testing is recommended on 2 strong north-south striking conductors which are coincident with the edges of magnetic highs.

The regional and property geology setting is highly prospective for sedex lead-zinc-silver mineralization. The property is underlain by predominantly basinal type marine sedimentary rocks, including carbonaceous shales, argillite, mudstone, and slate which may belong to Cambro-Ordovician units of the Cassiar Terrane or Devonian Mississippian Earn Group. Both of these assemblages are hosts to numerous sedex deposits in the Cordillera including the Tom and Jason of the Macmillan Pass district and the Cirque of the Gataga district.

Two showings on the property indicate favourable depositional environments for lead-zinc mineralization. At the Barite Showing in the north part of the property, a 2 m wide barite lense is found in black shales. As well, a 20 m thick horizon of bedded pyrite is hosted in shales, and massive pyrite is found in quartz-barite cemented breccia zones. A lead-zinc occurrence at the Main Showing within the B.C. side of the property consists of 20 cm wide

lense of massive, fine grained galena and sphalerite exposed for 10 m in length within calcareous mudstones.

The airborne geophysical survey outlined narrow magnetic highs adjacent to and closely paralleling the Liard Canyon on the west and east sides of the canyon. These anomalous highs may possibly be related to pyrrhotite-bearing magnetic horizons within folded strata. Intense, upright folds are observed along the walls of the canyon. The ground survey confirmed the presence and strength of the magnetic anomaly on the west side of the canyon. A moderately strong magnetic anomaly coincides with the Barite Showing and continues across the north side of the river. Between the Barite and Main Showings, a series of northwesterly striking airborne VLF-EM conductors coincide with bedrock magnetic stratigraphy. A broad high IP-low resistivity zone from Billiton's 1984 survey was tested by Billiton with a gravity survey, and it was concluded that the anomaly represented a graphitic shale unit. The 2 north-south striking conductors detected by KRL's ground survey do not appear to be related to that zone and should be further investigated.

RECOMMENDATIONS

A program of diamond drilling is recommended to test a VLF-EM conductor and a coincident VLF-EM - magnetic high anomaly on the property. A total of 600 metres of drilling in three holes is recommended. Estimated cost of this program is as follows:

Diamond drilling: 600 metres @ \$50/metre	30,000
Helicopter support: 10 hours @ \$800/hour	8,000
Geologist + assistant, 10 days	5,000
Analyses	3,000
Travel and vehicle expenses	4,000
Room and board: 20 person days @ \$100/day	2,000
Report preparation	2,000
Total:	\$54,000

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STATEMENT OF QUALIFICATIONS

I, Rita Chow of 5615 Dumfries Street, Vancouver, British Columbia, do hereby declare that:

1. I graduated from the University of British Columbia with a B.Sc. Degree (first class standing) in Geological Sciences in May, 1995.
2. I have been employed by KRL Resources Corp. since June of 1995.
3. I am responsible for the supervision of the work described in this report.
4. This report is based on work done on the property between March and October of 1996 and on references as listed.

A handwritten signature in cursive script, appearing to read "Rita Chow", is written over a horizontal line.

Rita Chow, B.Sc.

March 5, 1997

APPENDIX A

REPORT ON A

**HIGH SENSITIVITY MAGNETIC
AND VLF-EM AIRBORNE SURVEY**

**CASH CREEK, LIARD CANYON, GARDEN CREEK,
BLIND LAKE, MCDAME CREEK, PROPERTIES**

YUKON - BRITISH COLUMBIA

for

KRL RESOURCES CORP.

by

TERRAQUEST LTD.
Toronto, Canada

June 30, 1996

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LIST OF MAPS IN JACKET (There are 5 separate survey blocks; each block has a set of the following maps with the area identified by letters A to E)

- No. A-954-1, Total Magnetic Field
- No. A-954-2, Vertical and Horizontal Magnetic Gradients
- No. A-954-3, VLF-EM
- No. A-954-4, Interpretation

1.0 INTRODUCTION

This report describes the specifications and results of an airborne geophysical survey carried out for KRL RESOURCES CORP. of 1022 - 470 Granville Street, Vancouver, BC, V6C 1V5. The survey was performed by TERRAQUEST LTD., 100-1373 Queen Victoria Avenue, Mississauga, ON, L5H 3H2, telephone (905)274-1795 and fax (905)274-3936.

The purpose of a survey of this type is to prospect directly for anomalously magnetic and or conductive areas in the earth's crust which may be caused by, or at least related to, economic minerals. Secondly, the geophysical patterns may be used indirectly for exploration by mapping the geology in detail, including the faults, shear zones, folding, alteration zones and other structures. This technique outlines structures that may control mineralization and accounts or proposes a logical, stratigraphic source for the majority of the magnetic responses.

To achieve this purpose the survey area was systematically traversed by an aircraft carrying geophysical instruments along parallel flight lines spaced at even intervals, 75 metres above the terrain surface, and aligned so as to intersect the regional geology and structure in a way to provide the optimum contour patterns of geophysical data.

2.0 SURVEY AREAS

2.1 Cash Creek (A-954A)

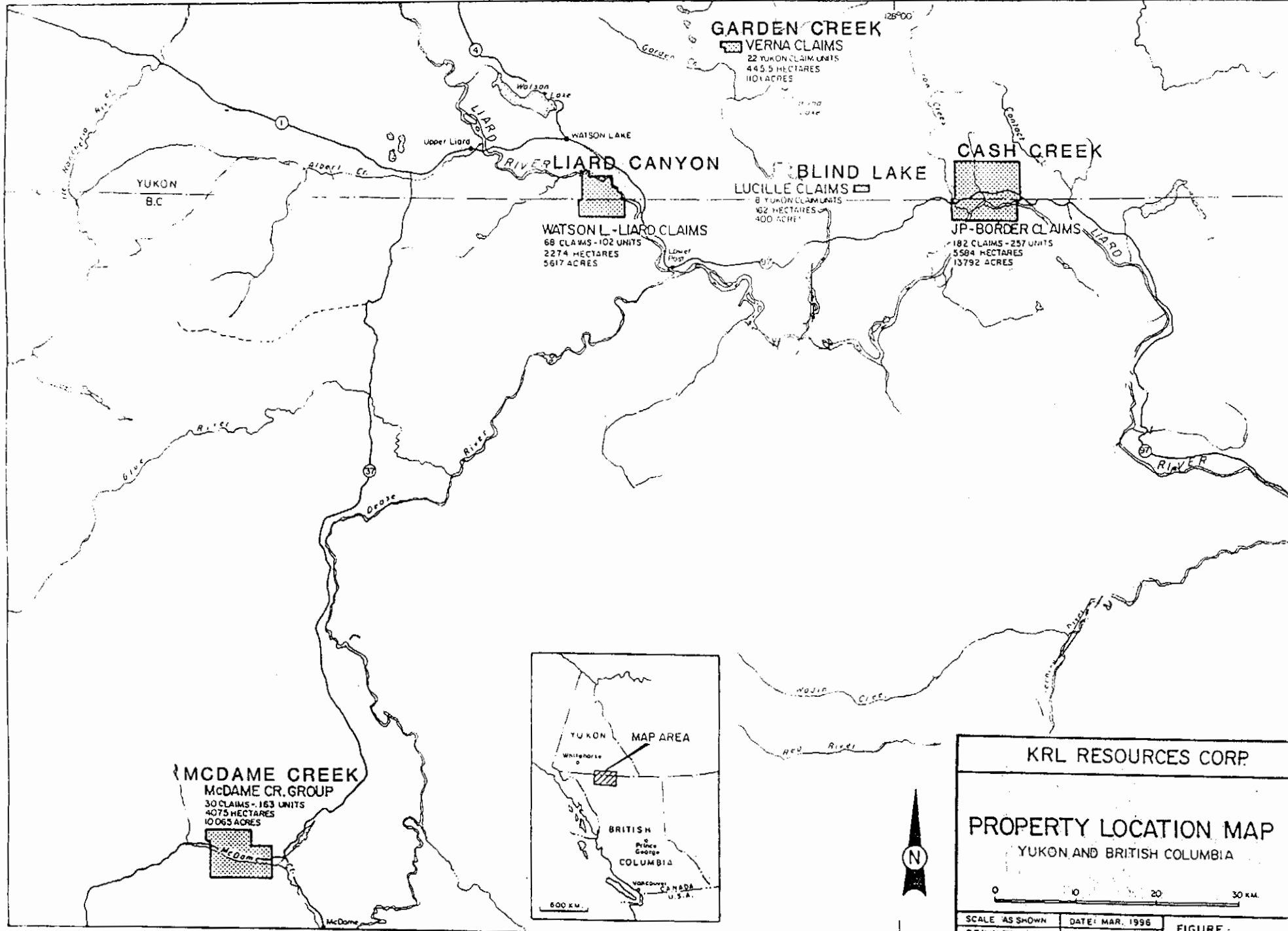
The Cash Creek block is located approximately 60 kilometres east of the town of Watson Lake, Yukon and straddles the British Columbia - Yukon border. Both the Alaska highway and the Liard River pass through the middle of the block.

The survey area is rectangular in shape and measures approximately 7 kilometres north-south and 8 kilometres east-west. The central latitude and longitude are 60 degrees north, and 127 degrees 46 minutes west. The N.T.S. references are 95D/4 and 94M/13.

2.2 Liard Canyon (A-954B)

The Liard Canyon block is located approximately 3 kilometres south of the town of Watson Lake, Yukon and straddles the Yukon - British Columbia border. The Alaska highway and the Liard River pass through the northeast quadrant of the block.

The survey area is square, with approximately 7 kilometre sides. The central latitude and longitude are 60 degrees north and 128 degrees 37 minutes west. The N.T.S. references are 105A/2 and 104P/15.



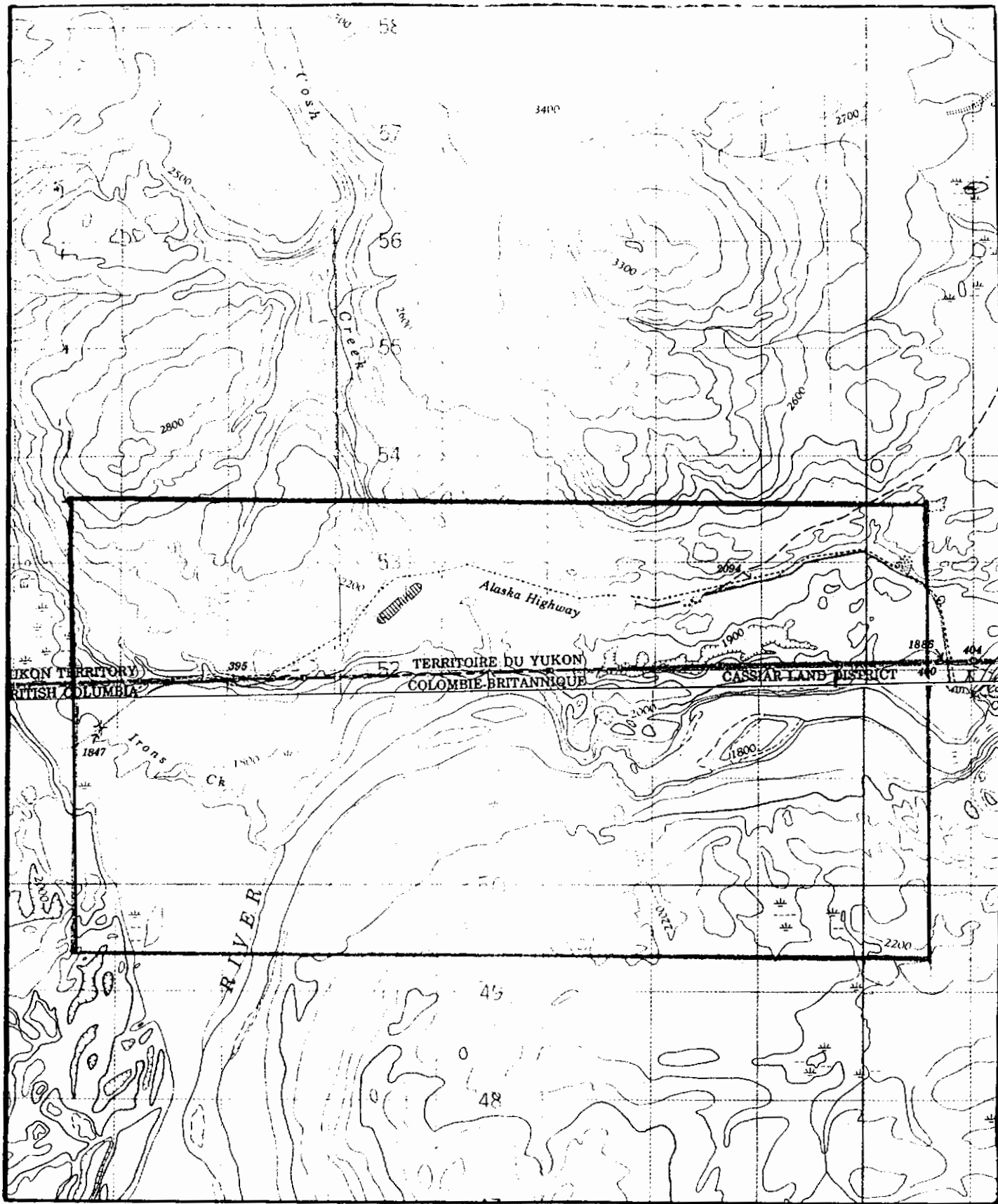


FIGURE 2a SURVEY AREA

CASH CREEK

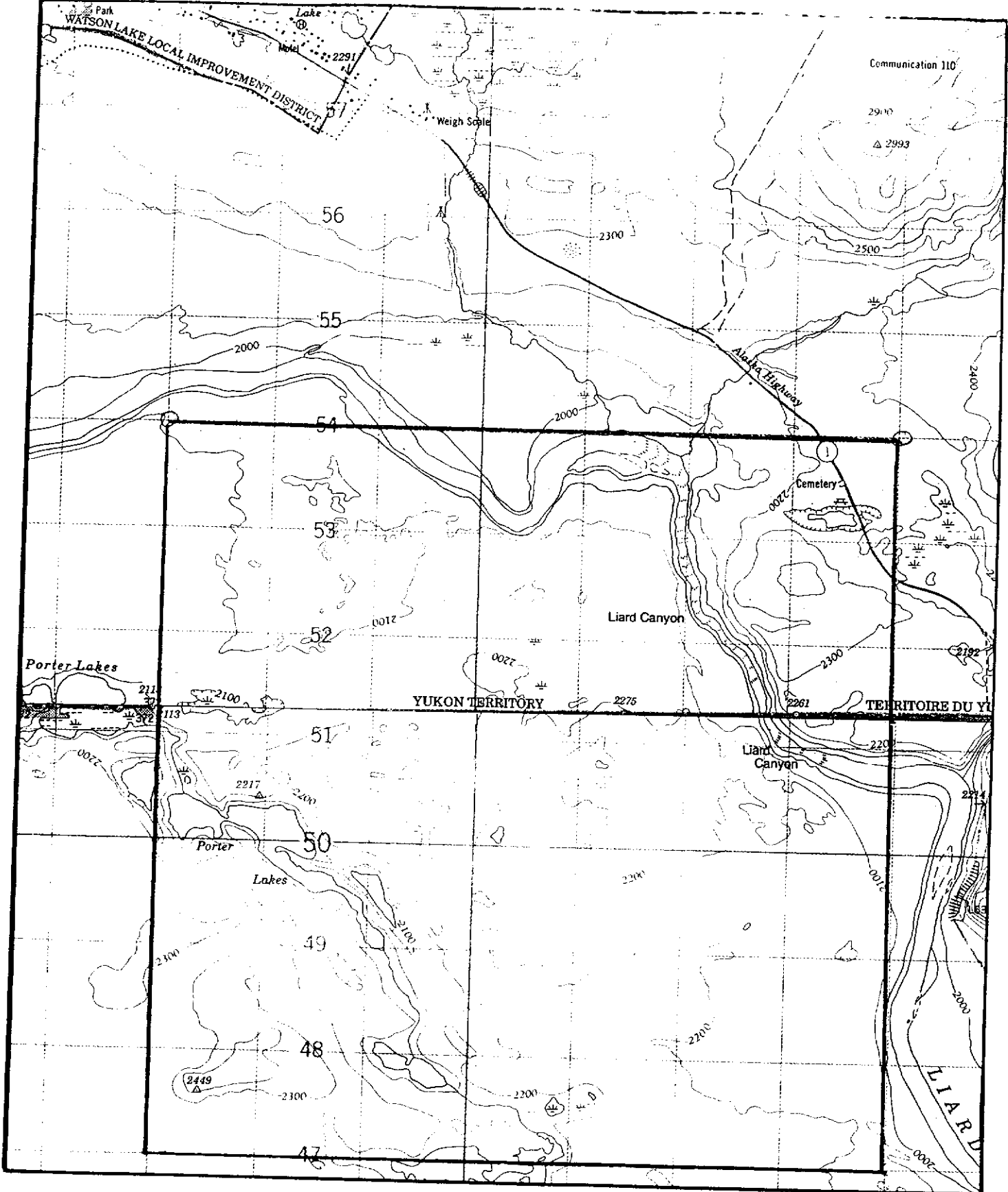


FIGURE 2b SURVEY AREA
LIARD CANYON

2.3 Garden Creek (A-954C)

The Garden Creek block is located approximately 19 kilometres northeast of the town of Watson Lake, Yukon. The Hyland River passes along the eastern edge of the block.

The survey area is rectangular measuring approximately 8 kilometres east west and 6 kilometres north south. The central latitude and longitude are 60 degrees 10 minutes north and 128 degrees 20 minutes west. The N.T.S. reference is 105A/1.

2.4 Blind Lake (A-954D)

The Blind Lake block is located approximately 34 kilometres east southeast of the town of Watson Lake, Yukon and 10 kilometres southeast of Blind Lake. The Hyland River passes along the western edge of the block and the British Columbia border along the south side.

The survey area is irregular in shape, measuring approximately 8 to 11 kilometres east west and 5.5 kilometres north south. The central latitude and longitude are 60 degrees 2 minutes north and 128 degrees 5 minutes west. The N.T.S. reference is 105A/1.

2.5 McDame Creek (A-954E)

The McDame Creek survey block is located approximately 20 kilometres east of the town of Cassiar, British Columbia. Both the McDame Creek and the Cassiar Road run east-west through the centre of the block. The abandoned town of Centreville lies in the middle of the area. The road to the town of McDame passes along the east edge of the area. The survey area is rectangular in shape measuring 5.5 km north-south and 10 km east-west. The general latitude longitude are 59 degrees 16 minutes north and 129 degrees 25 minutes west.

3.0 GEOLOGY

3.1 Cash Creek Block (A-954A)

References:

Geology and Rock & Silt Geochemistry, JP Claims, Watson Lake, Yukon. KRL Resources Corp., Aug 1995
 Geology and Rock & Silt Geochemistry, Border Claims, Liard M.D., B.C. KRL Resources Corp., Aug 1995

The Cash Creek claim group is underlain by Hadrynian or Lower Cambrian sediments and include phyllites, slate, fine grained quartz, siltstone argillite, and their calcareous equivalents. Only a few outcrops are indicated on the geological map and no correlation between outcrops has been made. Strikes and joints vary from northwest to northeast. Mineralization occurs as massive sulphide float and iron oxide cemented rubble, both located in the western part of the claim group.

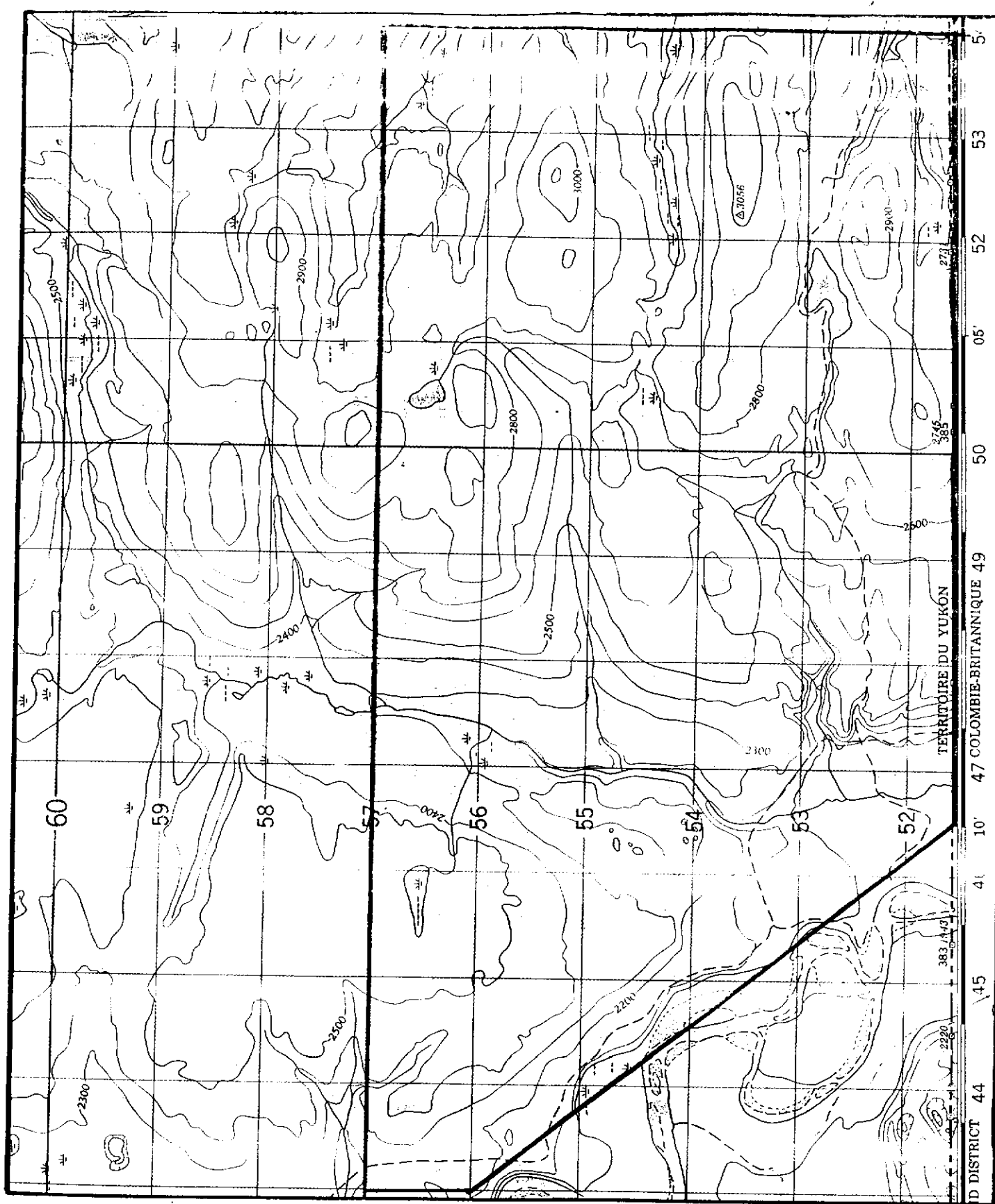


FIGURE 2d SURVEY AREA
BLIND LAKE

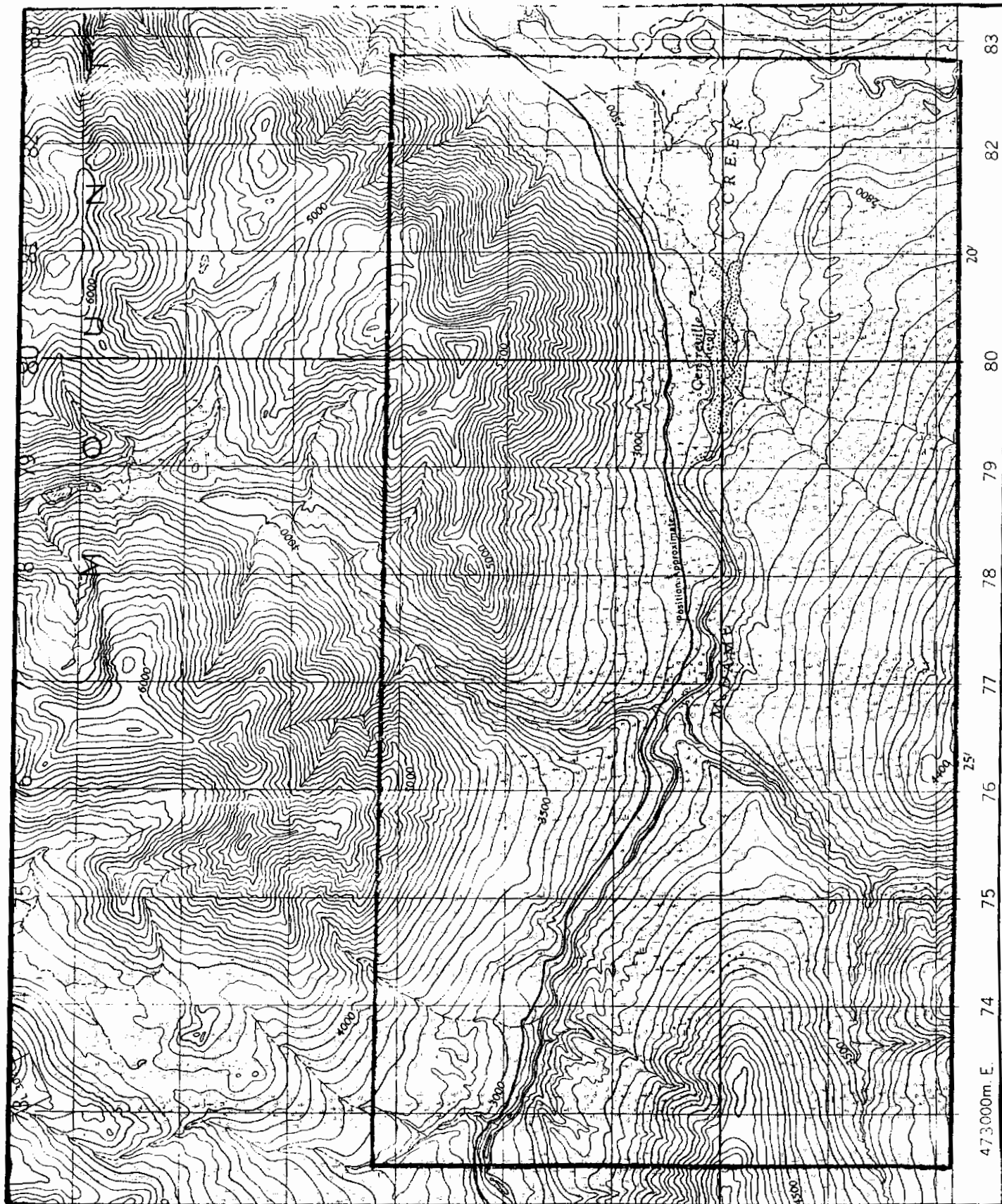


FIGURE 2e SURVEY AREA
MCDAME CREEK

3.2 Liard Canyon Block (A-954B)

References:

Geology Watson Lake, Yukon Territory, Preliminary Series, Map Sheet 105A. scale 1:253,440; Geological Survey of Canada; 1967

The Liard block is covered primarily by Quaternary overburden. A large exposure of Cambro-Ordovician rocks occurs along the Liard River in the northeast quadrant. This general rock unit contains argillite, slate, phyllite, phyllitic limestone and silty limestone. This rock unit hosts two occurrences of Pb-Zn-Ag mineralization further to the north. Beyond the survey area Mississippian clastics and limestones occupy the highlands whereas small exposures of Tertiary (?) vesicular basalt occupy the lowlands to the northwest.

3.3 Garden Creek Block (A-954C)

References:

Geology Watson Lake, Yukon Territory, Preliminary Series, Map Sheet 105A. scale 1:253,440; Geological Survey of Canada; 1967

The Garden Creek block is covered by Quaternary overburden with no mapped rock exposures. Small and remote exposures of Proterozoic sediments of Hadrynian age occur in all directions away from the block. This general rock unit contains shale, slate, feldspar-quartz pebble conglomerate, grit, quartzite, limestone, dolomite and phyllitic slate.

3.4 Blind Lake Block (A-954D)

References:

Geology Watson Lake, Yukon Territory, Preliminary Series, Map Sheet 105A. scale 1:253,440; Geological Survey of Canada; 1967

The Blind Lake Creek block is covered by Quaternary overburden with no mapped rock exposures. Small and remote exposures of Proterozoic sediments occur in all directions away from the block. This general rock unit contains shale, slate, feldspar-quartz pebble conglomerate, grit, quartzite, limestone, dolomite and phyllitic slate.

3.5 McDame Creek Block (A-954E)

References:

Regional Geology, Cassiar Map Sheet 104P

The McDame Creek survey area is mapped as having a series of clastic and calcareous sediments ranging in age from Proterozoic in the northeast quadrant through Cambrian, Ordovician, Silurian, Devonian to Lower Mississippian in the southwest corner, with a regional strike to the northwest. Regional structures trend to the northwest, north, northeast and east.

4.0 EQUIPMENT SPECIFICATIONS

4.1 AIRCRAFT

The survey was carried out using a Cessna 206 aircraft, registration C-GGLS, which carries three high sensitivity magnetometers and a VLF electromagnetic detector. It is equipped with long range tanks, outboard tanks (total 11 hours range without reserve), balloon tires, cargo door and full avionics.

The aircraft has been extensively modified to support a tail stinger, two wing tip extensions and a VLF-EM assembly. Considerable effort has been made to remove all ferruginous materials near the sensors and to ensure that the aircraft electrical system does not create any noise. With these modifications this aircraft is probably the quietest magnetic platform in the industry with a figure of merit of 9 nT uncompensated and less than 1.5 nT compensated using G.S.C. standards.

The aircraft is owned and operated by Terraquest Ltd. under full M.O.T approval and certification for specialty flying including airborne geophysical surveys. The aircraft is maintained at base of operations by a regulatory AMO facility, Leggat Aviation Inc. and in the field by a Terraquest Ltd. AME in association with an approved AMO.

4.2 AIRBORNE GEOPHYSICAL EQUIPMENT

The airborne geophysical system has three high sensitivity, cesium vapour magnetometers and a VLF-EM system. Ancillary support equipment include tri-axial fluxgate magnetometer, video camera, video recorder, radar altimeter, barometric altimeter, GPS receiver and a navigation system which includes a left/right indicator and a screen showing survey area with real time flight path. All data is collected and stored by the data acquisition system. The following provides the detailed equipment specifications.

Cesium Vapour Magnetometer (in wing tip extensions and tail stinger):

Model	CS-2
Manufacturer	Scintrex
Serial Numbers	921203, 921204, 94-03/003
Resolution	0.001 nT counting @ 0.1 per second
Sensitivity	+/- 0.005 nT
Dynamic Range	15,000 to 100,000 nT
Fourth Difference	0.02 nT

VLF-EM System (mounted in tube, projected forward of midsection of port wing):

Model	TOTEM 2A
Manufacturer	Herz Industries Ltd.
Serial Number	2805510
Primary Source	Magnetic field component radiated from two VLF radio transmitters
Parameters Measured	X, Y, Z components at two frequencies

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Serial Number	2805510
Primary Source	Magnetic field component radiated from two VLF radio transmitters
Parameters Measured	X, Y, Z components at two frequencies

Frequency Range	15.0 kHz to 24.3 kHz in 100 Hz steps
Sensitivity	130 μ V to 100 μ V at 20 kHz, 3dB down at 14 kHz and 24 kHz
Output Span	+/- 100% = +/- 1.0 V
Internal Noise	1.3 μ V rms
Output	Total Field, Quadrature; each frequency

The VLF-EM uses three orthogonal detector coils to measure (a) the total field strength of the time-varying EM field and (b) the phase between the vertical coil and both the "along line" coil (LINE) and the "cross-line" coil (ORTHO). The LINE frequency is tuned to a transmitter station that is ideally positioned at right angles to the flight lines, while the ORTHO frequency transmitter should be in line with the flight lines.

Tri-Axial Magnetic Field Sensor (for compensation, mounted in the forepart of tail stinger):

Model	MAG-03MC
Manufacturer	Bartington Instruments Ltd.
Internal Noise	at 1 Hz - 1 kHz; 0.6 nT rms
Bandwidth	0 to 1 kHz maximally flat, -12 dB/octave roll off beyond 1 kHz
Frequency Response	1 Hz - 100 Hz: +/- 0.5% 100 Hz - 500 Hz: +/- 1.5% 500 Hz - 1 kHz: +/- 5.0%
Calibration Accuracy:	+/- 0.5%
Orthogonality	+/- 0.5% worst case
Package Alignment	+/- 0.5% over full temperature range
Scaling Error	absolute: +/- 0.5% between axes: +/- 0.5%

Video Camera (camera mounted in belly of aircraft):

Model	TC2055NC (colour)
Manufacturer	RCA
Serial Number	19492
Lens	4.87 mm, auto iris - white balance

Video Recorder (mounted in rack):

Model	AG 2400 (commercial grade)
Manufacturer	Panasonic
Serial Number	C8TA00281 (plus 2 backups)

Radar Altimeter:

Model	KA-131
Manufacturer	King
Serial Number	071-1114-00
Accuracy	5% up to 2,500 feet
Calibrate Accuracy	1%
Output	Analogue for pilot; Converted to digital for data acquisition

Barometric Altimeter:

Model	LX18001AN
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Manufacturer	Sensym
Source	Coupled to aircraft barometric system

Differential GPS Receiver (antenna mounted on cabin roof):

Model	GPS Card 3951R
Manufacturer	Novatel
Antenna	Model 511
Polling	5 times per second
Accuracy	position (SA implemented) 100 metres position (no SA) 30 m velocity 0.1 knot time recovery 1pps, 100 nsec pulse width
Data Recording	all GPS raw and positional data logged by PDAS1000

Navigation Interface (mounted in rack with pilot and operator readouts):

Model	PNAV 2001
Manufacturer	Picodas Group Inc.
Data Input	Real time processing of GPS output data
Pilot Readout	Left/Right indicator
Operator Readout	Screen Modes: map, survey and line
Data Recording	All data recorded in real time by PDAS 1000 data acquisition system

Data Acquisition System (mounted in rack):

Model	PDAS 1000
Manufacturer	Picodas Group Inc.
Operating System	MS-DOS
Microprocessor	80486sx - 66 CPU
Coprocessor	Intel 80486sx
Memory	On board up to 8 MB, page interleaving, shadow RAM for BIOS, support EMS 4.0
Clock	real time, hardware implementation of MC14618 in the integrated peripherals controller
I/O slots	5 AT and 3 PC compatible slots
Display	Electro-luminescent 640x400 pixels
Graphic Display	Scrolling analog chart simulation with up to 5 windows operator selectable; freeze display capability to hold image for inspection
Recording Media	Standard 540 Mbyte hard disk with extra shock mounts; Standard 1.44 Mbyte floppy disk; Standard tape backup
Sampling	Selectable for each input type; 1, 0.5, 0.25, 0.2 or 0.1 seconds
Inputs	12 differential analog input with 16 bit resolution
Serial Ports	2 RS-232C (expandable)
Parallel Ports	Ten definable 8 bit I/O; Two definable 8 bit outputs

The PDAS 1000 also contains the magnetometer processor boards, one for each cesium vapour magnetometer:

Model	PCB
Manufacturer	Picodas Group Inc.

Input Range	20,000 - 100,000 nT
Resolution	0.001 nT
Bandwidth	0.7, 1 or 2 Hz
Microprocessor	TMS 9995
Firmware	8 KBit EPROM board resident
Internal Crystal	18,432 KHz
Absolute Crystal Accuracy	<0.01 %
Host Interfacing	8 KByte dual port memory
Address Selection	Within 20 bit addressing in 8 KByte software selectable steps
Input Signal	TTL, CMOS, Open collector compatible or sine wave with decoupler
Input Impedance	TTL > 1KOhm

Magnetic compensation for aircraft and heading effects is done in real time. Raw magnetic values are also stored and thus if desired, compensation with different variables can be run at a later time.

Other Boards:

Analog Processor	PCB - provides separate A/D converter for each analog input with no multiplexing; each channel is sampled at a rate of 1,000 samples per second with digital processing applied
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Power Supplies:

- 1) PC6B converter to convert the 13.75 volt aircraft power to 27.5 volts DC.
- 2) Power Distribution Unit manufactured by Picodas Group Inc. located in the instrument rack interfaces with the aircraft power and provides filtered and continuous power at 13.75 and 27.5 vDC to all rack components.
- 3) The PDAS-1000A contains a 32 volt DC cesium sensor switching power supply for the cesium vapour magnetometers in conjunction with real time magnetometer compensation; also enables interfacing the fluxgate magnetometer and the barometric altimeter; also provides clean power for radar altimeter and ancillary equipment (PC notebook, printer).

4.3 MAGNETIC BASE STATION

High sensitivity base station data is provided by an Overhauser magnetometer, data logging onto a PC 386sx notebook and time synchronization with ground GPS receiver.

Magnetic Sensor:

Model	GSM-11
Manufacturer	Gem Systems Inc.
Type	Overhauser proton precession
Sensitivity	0.01 nT at 10 readings per second
Accuracy	0.5 nT absolute

Magnetic Processor:

Model	MEP-810
Manufacturer	Urtec Inc.

Range (signal)	20,000 - 100,000 nT
Resolution (signal)	10 pT
Resolution (fdd)	1 pT
Clock Stability	2 ppm per year
Absolute accuracy correction	+/- 999x10e-6

Logging Software:

Logging software by Picodas Group Inc. version 5.02 to IBM compatible PC with RS-232 input; supports real time graphics, automatic startup, compressed data storage, selectable start/stop times, automatic disk swapping, plotting of data to screen or printer at user selected scales, and fourth digital difference and diurnal quality flags set by user.

A second, medium sense base station was available as backup with the following specifications:

Magnetometer

Model	GSM-9
Manufacturer	Gem Systems Inc.
Type	Overhauser proton precession
Range	20,000 - 100,000 nT in 23 overlapping steps
Resolution	1 nT
Accuracy	+/- 1 nT
Gradient Tolerance	up to 5,000 nT/metre
Operating Modes	manual pushbutton, cycling at 1.85 seconds, logging software controlled

Logging

Base station logging software version 5.02 by Picodas group Inc. onto NEC Multispeed laptop computer.

4.4 GPS BASE STATION

The ground GPS base station was logged onto a 486dx-66 notebook computer. Ground GPS data was collected to perform post flight differential correction to the flight path. The specifications are as follows:

Model	MX 4200D
Manufacturer	Magnavox
Serial Number	5057
Type	Continuous tracking, L1 frequency, C/A code (SPS), 6-channel (independent)
Receiver Sensitivity	-143 dBm Costas threshold
Position Update	once per second
Accuracy	position with SA implemented 100 metres, position with no SA 30 metres, velocity 0.1 knot time recovery 1 pps, 100 nsec pulse width

FID Line:1490.0W Time: 20:24:44.0 Start Fid: 1375 File: S4022720.B24

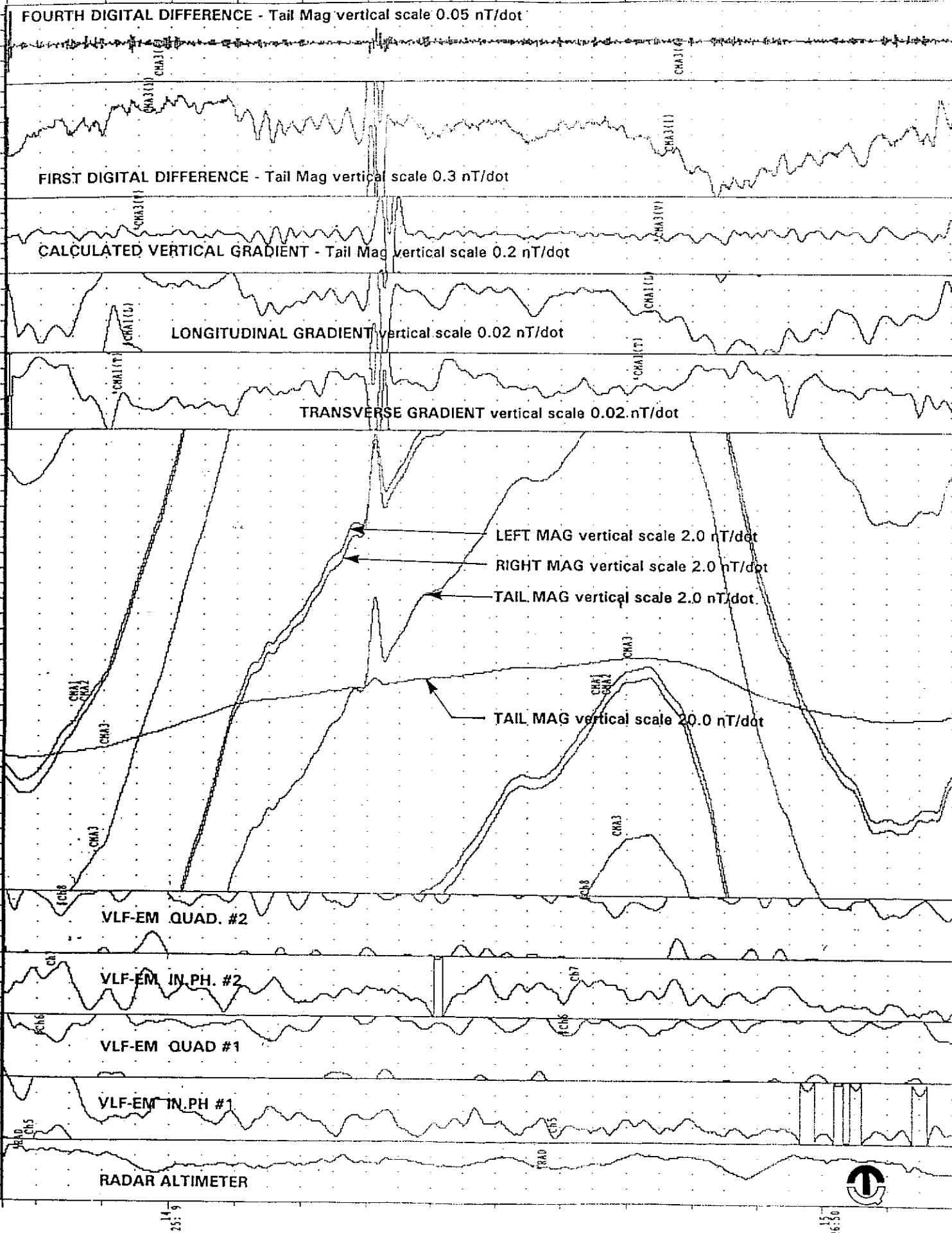


FIGURE 3. SAMPLE OF PROFILE DATA

4.5 IN-FIELD COMPUTING FACILITIES

The following equipment were supplied for infield preliminary processing including base station logging, GPS differential calculations and analogues of data on fanfold paper:

one Pentium 133-32MB PC with 2.2 GB HD, 800 MB tape drive, writable CD-ROM;
one 486DX/66 and one 386SX/25 notebooks; two dot matrix printers

5.0 SURVEY SPECIFICATIONS

5.1 LINES AND DATA

Line direction	090/270 degrees azimuth
Line interval	200 metres
Terrain clearance	75 metres (except McDame Creek Block which was flown at constant barometric elevation due to rugged terrain)
Average ground speed	60 metres/second
Data point interval:	
Magnetic	6 metres
VLF-EM	6 metres
Channel 1 (LINE)	NAA Seattle, 24.8 kHz
Channel 2 (ORTHO)	NAA Cutler, 24.0 kHz
Line kilometres	
A) Cash Creek	340 km
B) Liard Canyon	273 km
C) Garden Creek	266 km
D) Blind Lake	197 km
E) McDame Creek	<u>315 km</u>
TOTAL	1,391 km

Extensive overflight beyond the contract boundaries are included in the processed data set but have not been charged.

5.2 TOLERANCES

Line spacing: Any gaps wider than 1.5 times the line spacing and longer than 5 times the line spacing were filled in by a new line or not charged.

Terrain clearance: Portions of line which were flown above 115 metres for more than one kilometre were reflown if safety considerations were acceptable. The McDame Creek block was flown at constant barometric elevation to clear the rugged terrain.

Diurnal magnetic variation: Less than ten nanoteslas deviation from a smooth background over a period of two minutes or less as seen on the base station analogue record.

Manoeuvre noise: nil

5.3 NAVIGATION AND RECOVERY

The satellite navigation system was used to ferry to the survey site and to survey along each line using UTM coordinates. The UTM coordinates of the survey outline for navigation purposes and flight path recovery were taken from 1:50,000 scale NTS topographic maps all of which have North American Datum 1927. The Clarke 1866 ellipsoid for Canada was used with x-y-z delta shifts of +10, -158 and -187 respectively.

The accuracy is variable depending on the number and condition of the satellites, however it is generally less than twenty five metres and typically in the ten to fifteen metre range. Post flight differential correction, which corrects for satellite range errors, improves the accuracy of the flight path recovery to approximately within two to three metres.

A video camera recorded the ground image along the flight path. A video screen in the cockpit enabled the operator to monitor the accuracy of the flight path during the survey. This system also provided a backup system and verification for flight path recovery.

5.4 OPERATIONAL LOGISTICS

The main base of operations with the base station magnetometer and GPS equipment was at Watson Lake. The exact coordinates of the GPS antenna were 48 degrees 20 minutes 1.60 seconds north and 89 degrees 19 minutes and 49.53 seconds west at an elevation of 185 metres above the geoid.

The crew mobilized to Watson Lake on March 7, 1996 and finished surveying on March 26, 1996. The flights numbers were G-650 to G-665, including compensation, calibration, survey and reflights.

6.0 DATA PROCESSING

In-field processing consisted of plotting chart profiles of all the survey equipment data. This included radar altimeter; two frequencies of VLF-EM total field strength and quadrature data; all three magnetometers at detailed scale; tail mag at coarse scale; measured transverse gradient; measured longitudinal gradient; and pseudo vertical derivative, first digital difference and fourth digital difference all of the tail mag. The magnetometers are numbered as follows: left is 1, right is 2 and tail is 3.

In the office the magnetic data from the tail stinger magnetometer only was line levelled in the standard manner by tying survey lines to the tie lines. The IGRF has not been removed. The total field was gridded and micro-levelled in the Fourier domain (generally less than 1 nT corrections) to reduce any linear noise along the flight path without degrading the geological signal. The final levelled data sets were gridded and contoured at 1 nanotesla levels.

The vertical magnetic gradient was computed from the gridded and contoured total field data

using a method of transforming the data set into the frequency domain, applying a transfer function to calculate the gradient, and then transforming back into the spatial domain. The method is described by a number of authors including Grant and Fraser 1970, Grant, 1972 and Spector, 1968.

The horizontal gradient was achieved directly from the three magnetometers. The data from each sensor were levelled to each other by running a very large wavelength filter down each line and adjusting the wing tip data to the tail data. The horizontal gradient data have not been subjected to gridding and is presented on a point to point basis along each line, plotted as vectors where the magnitude is indicated by the length of the vector and the orientation of the field by the direction of the vector. The scale of the vectors is 0.05 nT/m/cm with a maximum vector length of 5 cm.

The mean and standard deviation of the VLF-EM total field and quadrature were calculated for each line. The standard deviation was used to level the total field strength to normalize for transmitter and local variability. The mean was used to level the in phase and quadrature data line to line. The data were converted from millivolts to percent and then gridded. Filtering was done along some of the lines. Final decorrugation or microleveling was done to remove any noise along the line.

All data processing, map contouring and plotting were carried out by Paterson Grant Watson of Toronto.

Grant, F. S. and Spector A., 1970: Statistical Models for Interpreting Aeromagnetic Data; *Geophysics*, Vol 35
 Grant, F. S. 1972: Review of Data Processing and Interpretation Methods in Gravity and Magnetism; *Geophy.* 37-4
 Spector, A., 1968: Spectral Analysis of Aeromagnetic maps; unpublished thesis; University of Toronto.

7.0 INTERPRETATION

7.1 GENERAL APPROACH

To satisfy the purpose of the survey as stated in the introduction, the following interpretation procedure was carried out on the magnetic data. On a local scale "geological" units were interpreted from the magnetic gradient contour patterns based on their characteristic patterns and intensities, or "signatures". The contacts are typically located along the steepest section of the gradient; therefore the vertical magnetic gradient format was used primarily to delineate stratigraphy. The total magnetic field format was used to determine the relative magnetic intensity of the interpreted unit.

The horizontal gradient vectors were used at two stages of the interpretation; first to improve the accuracy of the contact locations, and second, where possible to determine the axes of the interpreted magnetic units.

Generally, magnetic anomalies that are caused by iron deposits of ore quality are usually obvious owing to their high amplitude, often in tens of thousands of nanoteslas. Mafic to felsic metavolcanics are usually characterized by respectively strong to weak magnetic intensities. Clastic metasediments generally possess very low magnetic susceptibilities and therefore correlate with very low magnetic responses, and in some cases, the observed responses are overwhelmed by the magnetic field from the surrounding lithologies.

Alteration zones can show up as anomalously quiet areas, often adjacent to strong, circular anomalies that represent intrusives, or along an otherwise magnetically active horizon. In some cases contact metamorphic aureoles are characterized by magnetic anomalies.

Faults and shear zones were interpreted primarily from lateral displacements of otherwise linear magnetic anomalies but also from long narrow "lows". The direction of regional faulting and the topographic lineaments in the general area were taken into account when selecting the dominant fault orientations. Folding is usually seen as curved regional patterns.

The VLF-EM conductor axes have been identified and evaluated according to the Terraquest classification system (Figure 4). This system correlates the nature and orientation of the conductor axes with stratigraphic, structural and topographic features to obtain an association from which one or more possible origins may be selected. Alternate associations are indicated in parentheses.

The VLF-EM phase response has been categorized according to whether the slope/direction is normal (quadrature has negative slope at flight line), reverse (quadrature has a positive slope), or no definitive phase. The significance of the differing phase responses is not completely understood although in general reverse phase indicates either overburden as the source or a conductor with considerable depth extent, or both. Normal phase response is theoretically caused by surface conductors with limited depth extent. In some cases, a change in the orientation of the conductor appears to affect the sense of the phase response.

7.2 INTERPRETATION

The magnetic and VLF-EM data are shown in contoured format on maps located in the back pocket at a scale of 1:20,000. A qualitative interpretation map for each is also provided. The following notes are intended to supplement these maps.

CASH CREEK BLOCK (A-954A)

The total magnetic field over the Cash Creek Block has a maximum relief of only 80 nanoteslas ranging from 58,355 to 58,435 nanoteslas. The strongest widespread magnetic responses occur beyond the survey area to the west and are related to a strong regional, north-trending magnetic unit. The broad north-trending low in the total magnetic field along the western part of the claim group is probably an edge effect created by this magnetic trend.

The vertical gradient contours are capable "seeing through" the relatively uniform total field and outline numerous magnetic units across the survey area, even across the regional

FIGURE 4.

TERRAQUEST CLASSIFICATION OF VLF-EM CONDUCTOR AXES

SYMBOL	CORRELATION	ASSOCIATION: Possible Origins
A, a	Coincident with magnetic stratigraphy	Bedrock magnetic horizons: stratabound mineralogic origin or shear zone
B, b	Parallel to magnetic stratigraphy	Bedrock non-magnetic horizons: stratabound mineralogic origin or shear zone
C, c	No correlation with magnetic stratigraphy	Association not known: possible small scale stratabound mineralogic origin, fault or shear zone; overburden
D, d	Coincident with magnetic dyke	Dyke or possible fault along dyke: mineralogic or electrolytic
F, f	Crosscut magnetic units, or correlate with lineament	Fault or shear zone: mineralogic or electrolytic
OB, ob	Contours of total field conform to topographic depression	Conductive overburden, fault or shear zone: mineralogic or electrolytic
CUL, cul	Coincident with cultural sources	Electrical, telephone, pipe, fence or railway lines

NOTES:

1. Upper case symbols denote a relatively strong total field response
2. Underlined symbols denote a relatively strong quadrature response
3. Mineralogic origins include sulphides, graphite, and in fault zones, gouge
4. Electrolytic origins imply conductivity related to porosity or high moisture content
5. Symbols in parentheses represent alternative or secondary interpretation

magnetic low. It is not possible to correlate these units with the known geology since not enough geological information is available. This must be done by a prospecting or mapping program to attempt to identify these horizons; this data can be used as a guideline for fieldwork. For the purposes of this interpretation the magnetic horizons have been classified into relative units: strongly magnetic (unit 1), moderately magnetic (unit 2) and magnetic background (unit 3).

The strongest magnetic responses are most likely related to increased concentrations of iron bearing minerals such as iron sulphides. These are transitional with the moderately magnetic horizons. Note that the locally high responses at the east end of lines 250 and 260 display very large horizontal magnetic vectors, indicating that it is probably very near surface. The interpreted size and outline of this body is based on the vector data, not the contoured data.

The known mineralization occurs as massive sulphide float and iron oxide cemented rubble, neither of which can clearly be associated with a strongly magnetic horizon. However they are located along strike from the strongly magnetic horizons (unit 1) and it is suggested that these should be investigated in detail.

Two north trending dykes (unit 4) have been interpreted in the southern part of the survey.

Offsets in the magnetic horizons have been used to identify numerous structures that trend to the northeast and probably occur as two sets: 030 and 045 degrees. Many of these are coincident with topographic lineaments. A regional north-south structure probably occurs along the strong magnetic unit beyond the claim group to the west.

The VLF-EM survey has identified abundant conductor axes. Those conductor axes that are aligned with magnetically interpreted structures or that crosscut magnetic stratigraphy are interpreted to be related to faults or shear zones. This type of conductivity may be caused by minerals such as sulphides, graphite or gouge, or to an ionic effect created by water or porosity either within the structure or along the upper weathered and leached edge. Some of these may be good exploration targets and consequently those conductors that follow known mineralization trends should be investigated on the ground.

Two conductors coincide with the interpreted dykes. This conductivity may be related to structural type sources (as discussed above) or to mineralization along the dyke.

Most of the conductor axes coincide with or are parallel to magnetic stratigraphy and therefore possess increased potential for bedrock sources. These may include conductive minerals such as disseminated to massive sulphides, graphite, or conductive rock such as porous flow tops. Those that occur along the strongly magnetic horizons (unit 1) bear the greatest potential massive sulphide origins.

LIARD CANYON (A-954B)

The total magnetic field over the Liard Canyon block has a relief of 190 nT ranging from 58,145 nT to 58,335 nT, and shows a semi-regional gradient which increases relatively uniformly from the northeast corner to the southwest corner.

The calculated vertical gradient outlines numerous narrow horizons that trend to the north northwest. The only outcrop in the survey area coincides with magnetic background and therefore is not particularly useful in identifying the nature of the magnetic horizons. It is presumed that similar sedimentary rocks underlie most of the survey area and that the magnetic horizons are related to increased concentrations of iron bearing minerals or possibly even volcanic lithologies at depth. Some horizons are distinctly more magnetic and are labelled as Unit 1 on the interpretation map, and the weakly magnetic horizons as Unit 2. This helps to delineate the detailed magneto-stratigraphy of the area. The Unit 2 horizons may often be down faulted Unit 1, or Unit 1 with lower concentrations of iron bearing minerals. The decrease in total magnetic field away from the southwest corner suggests that these magnetic horizons may be at greater depth across the survey area.

The measured horizontal gradient has identified an uncommon feature located just to the west of the centre of the block. It is identified by the letter "M" on the interpretation map. It is characterized by strong attraction on the vector plots over three flight lines but does not appear to possess significant responses on the gridded and contoured total field or calculated vertical gradient. This feature must be a relatively strong, pinpoint source most likely restricted to the very near surface, possibly a cultural or boulder (?) artefact.

The measured horizontal magnetic gradient identifies axes within some of the strongly magnetic units; in some cases these may represent the near surface edge of the magnetic unit whereas the contoured vertical gradient may reflect a wider representation of the same unit at increasing depth.

Numerous structures have been interpreted and may represent variably either faults, shear zones or even tight fold axes. Most of these strike at about 60 degrees and a few at 20 degrees. The latter appear to be more continuous and hence younger.

The VLF-EM data have identified numerous conductive zones. The conductor axes have been interpreted and classified according to their magnetic, structural and topographic relationships. Of particular economic interest are those conductors that coincide with the magnetic horizons; these may originate from higher concentrations of sulphides and therefore represent good ground targets. Note that the overall VLF-EM responses in the central part of the survey area are subdued; this is interpreted to be masking by overburden and not necessarily decreased conductivity. The strong magnetic response next to Unit M has better conductivity away from the centre of the strongest magnetism. This may represent either increased overburden or possibly facies changes along the magnetic horizon, possibly representing changes in the portions of sulphide and iron bearing minerals.

Variations in the total magnetic field suggest that the magnetic horizon near Unit M may be similar if not related to the strongly magnetic horizons to the southwest. If the subdued VLF-

EM responses do represent increased overburden, then it might be easier to identify the source of the magnetism and conductivity along the horizons to the southwest.

GARDEN CREEK (A-954C)

The total magnetic field has a very low relief of approximately 35 nT ranging from 58,265 nT to 58,300 nT with the strongest responses located along the eastern boundary. Both the total field and the vertical magnetic gradient show north trending stratigraphy.

The magnetic components of the interpreted units are assumed to be caused by higher concentrations of magnetic minerals within the sediments such as finely disseminated iron particles. For purposes of this interpretation, these units have been identified as Unit 1 magnetic, Unit 2 weakly magnetic, and Unit 3 background. Based on the nature of the gradients, the strongest responses to the east may possibly be related to a metamorphic effect or upthrust block faulting, although it is difficult to identify such regional features at this scale.

Numerous weak to relatively strong VLF-EM conductor axes trend to the north-northwest. The strongest lie in the centre of the survey area across the higher ground and correlate with the weakly magnetic stratigraphic units. These possess the greatest potential for sulphide type mineralization.

Numerous structures have been interpreted most of which trend to the northeast and a few, presumably younger, to the north-northeast. North trending structures would be difficult to resolve since they would be parallel to the magnetic fabric.

BLIND LAKE (A-954D)

The total magnetic field has a relief of 190 nT ranging from 58,215 nT to 58,405 nT and forms an overall north trending fabric. The detail provided by the vertical magnetic gradient shows an overall northwest fabric.

Because there are no outcrops with which to correlate the magnetic responses, the magnetic stratigraphy has been subdivided into magnetic (Unit 1), weakly magnetic (Unit 2) and magnetic background (Unit 3) horizons. Unit 1 most likely represents sediments with higher concentrations of magnetic minerals, or possibly even volcanics or dykes if they exist the area. Unit 3 represents sediments with the lowest concentration magnetic minerals. To some degree changes in magnetic amplitude along strike may be related to block faulting. Some of the magnetic horizons have magnetic axes that are defined by the measured, horizontal gradient. The horizontal gradients have also been used to improve the resolution of the contacts and structures.

The large low-magnetic zone in the north centre of the survey block appears to truncate many of the magnetic horizons. Very little detail was able to be interpreted from the vertical gradient in this area. It is suggested that this may be related to alteration or leaching that has altered or removed the magnetic minerals.

Numerous northeast trending structures have been interpreted from offsets in the magnetic horizons. These features may be faults, shear zones or even tight folds. Any north to northwest trending structures would be difficult to identify as they would be parallel to the magnetic fabric.

The VLF-EM data show many conductive zones most of which correlate with or are parallel to the magnetic fabric. These represent the best targets for sulphide mineralization, particularly if they also correlate with magnetic axes as defined by the horizontal gradient. Those conductors that trend to the north and northeast are interpreted to have structural sources.

MCDAME CREEK BLOCK (A954E)

The McDame Creek survey has the largest range in total magnetic field values, 155 nT from 58,070 nT to 58,225 nT, despite the fact that it was flown with a much higher mean terrain clearance. The strongest responses lie in the northwest quadrant with an overall northwest strike and the lowest responses lie along the eastern edge.

The magnetic patterns have been correlated with the regional geology as much as possible. Most of the units possess similar magnetic signatures and thus they are shown together on the interpretation map. Unit 4 correlates with strong magnetic values in the northwest corner; this has been the basis for interpolating this unit across the survey area to the east side where it appears to correlate with unit 4 just beyond the survey area. Where it is overlain by other rocks, the magnetic pattern of this unit would be characterized by slightly weaker values and less distinct contacts as shown on the vertical magnetic gradient.

It is suspected that parts of unit 3 may possess slightly elevated magnetic signatures; this is shown on the east side of the survey area.

Unit 8 in the southwest quadrant correlates with weak total field values and weak and moderate responses on the vertical gradient. The latter has been identified as unit 8m, a magnetic unit within unit 8 which is probably related to narrow horizons of metamorphosed volcanic rocks.

The strong responses, both total field and vertical gradient, immediately west of the survey area correlate well with unit 9, serpentinite.

Most of the magnetically interpreted structures trend to the northeast; two trend to the north and one trends to the northwest. There is a bias against the identification of structures that are parallel to the dominant magnetic trend.

Structures identified from the VLF-EM data strike to the northwest, north, northeast and east.

The VLF-EM survey has identified several strong conductors in the northern central part of the survey block. All of these either coincide with magnetic units or are at least parallel to the dominant magnetic fabric, and therefore possess potential for bedrock, stratiform origins. Of

the two strong conductors in the southwest quadrant, one coincides with the serpentinite and the other is parallel to an 8m unit horizon.

8.0 SUMMARY

An airborne high sensitivity magnetic and VLF-EM survey has been carried out at 75 metre mean terrain clearance (except for McDame Block), and 200 metre line intervals and with data sample stations at 6 metres along the lines. Ties lines were spaced at 3 kilometres or less. A base magnetic station recorded the diurnal activity throughout the survey and a base GPS station was used to correct range errors in the GPS flight path recovery. Recorded data included three magnetometers configured in the horizontal plane and VLF-EM. The data have been processed, gridded and plotted as contours of total magnetic field, vectors of measured horizontal gradient, contours of calculated vertical magnetic gradient and contours VLF-EM total field strength with profiles of the quadrature plotted along the flight lines. All maps are at a scale of 1:20,000.

The magnetic patterns show a very low magnetic relief over all areas. The vertical and horizontal gradient data are able to provide sufficient detail to interpret magneto-stratigraphic units that where available have been correlated with known geology. Where no correlation was possible the magneto-stratigraphy has been interpreted into units of relative magnetic intensities.

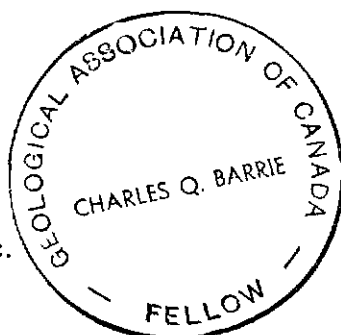
Numerous structures have been interpreted from both magnetic and VLF-EM data; in order of abundance these are north-east with a few to the northwest, north and east. The degree to which these structures are observed depends primarily upon the orientation of the magnetic unit; the higher the angle of intersection the more likely it is to be observed.

The VLF-EM data shows numerous conductive trends. The conductors have been classified according to their overall nature, strength, orientation and their topographic, structural and lithological associations in order to determine their potential origin. The origins have been interpreted as structural and stratigraphic, either coincident with or parallel to magneto-stratigraphic units. Those that correlate with known mineralization or magneto-stratigraphic units should be investigated on the ground using IP or EM methods.

TERRAQUEST LTD.



Charles Q. Barrie, M.Sc.



APPENDIX I**PERSONNEL**

Field:	Operator Pilot/AME	Sean Luck Neville Ribeiro
Office:	Manager/Interpretation Processing	Charles Q. Barrie Paterson Grant Watson

APPENDIX B

Trench and Rock Sample Descriptions

SAMPLE #	LOCATION	WIDTH(m) OR GRAB	DESCRIPTION	ASSAYS (ppm)					
				Au (ppb)	Ag	Cu	Pb	Zn	As
BR-01	Road along border	grab	Boulder of light grey-brown silicified.	1	<0.3	43	19	72	4
YLC-01	Liard Canyon	grab	Quartz in altered sedimentary rock.	6	0.5	43	109	156	50
YLC-02				4	1.3	129	620	291	66
TR1-01	1st trench, SW pit (3300N, 5500E)	grab	Grey, soft semi-consolidated clay beds at 5 m depth.	2	<0.3	27	13	87	6
TR1-02	1st trench, NE pit (3500N, 5800E)	grab	Dark grey to black shales, phyllites at 4 m depth. Contains minor fine dissemin. pyrite and quartz lenses.	7		16		18	5
TR1-03				1		27		19	4
TR1-04				<1		8		13	4
TR2-01	2nd trench (3800N, 5725E)	grab	Dark grey to black shales, phyllites at 5 m depth, east end of trench.	<1		17		65	12
TR3-01	3rd trench (4100N, 5525E)	grab	Dk. yellow-brown pebbly clay, semi-indurated (permafrost?)	5	<0.3	39	15	91	6
TR3-02	30 m west of TR3-01	grab	Quartzite boulders.	1		4		1	<2
TR3-03		grab	Siliceous (cherty?) bedded boulders.	2		79		26	43
TR4-01	4th trench (4500N, 5400E)	grab	Quartz lens hosted in phyllites.	2		18		19	13
TR4-02		grab	Phyllites with rusty laminations.	1		25		15	18
TR4-03		grab	Quartz pod, rusty fractured; contains minor galena.	1		7		16	<2
TR4-04		grab	Folded phyllites with v. soft, fine-gr. dk. orange-red mineral along fractures and between bedding.	<1		26		12	9
TR4-05		grab	Rusty, silicified argillites cut by abundant quartz-carbonate veinlets.	<1		4		28	23
TR4-06		grab	Sim. to TR4-05; some graphite.	<1		6		31	6
TR4-07	4th trench (4500N, 5400E)	4.5	Rusty phyllites, siliceous and quartz veined argillites, quartz lenses.	<1	<0.3	11	6	18	8
TR4-08		4.5		<1	<0.3	20	<3	27	15
TR4-09		4.5		<1	<0.3	21	4	28	9
TR4-10		4.5		<1	<0.3	18	5	45	7
TR4-11		4.5		<1	<0.3	24	8	166	10
TR4-12		4.5		2	0.5	94	30	130	15
TR4-13		4.5		1	0.3	46	27	79	14
TR4-14		4.5		2	0.5	64	22	48	14
TR4-15		4.5		9	0.6	132	17	31	13
TR4-16		4.5		9	0.5	124	18	25	11
TR4-17		4.5		8	0.6	136	20	26	11
TR4-18		4.5		7	<0.3	101	18	42	11

SAMPLE #	LOCATION	WIDTH(m) OR GRAB	DESCRIPTION	ASSAYS (ppm)					
				Au (ppb)	Ag	Cu	Pb	Zn	As
TR4-19		4.5		1	<0.3	28	14	59	8
WDS#1	Liard River	grab	Quartz vein, 10 m wide at base of anticline; pyrite 5%; strong alteration.	5	<0.3	33	<3	70	13
WDS#2	Liard River	grab	Dark grey-black graphitic shale at base of anticline; weakly altered; no mineralization.	9	0.3	8	16	6	6
WDS#3	Liard River	grab	Grey shale; strong alteration, silicified; pyrite 1%.	2	0.5	63	32	327	18
WDS#4	Liard River	grab	Sandstone; no mineralization. Dyke, 1 m wide, highly deformed.	1	<0.3	12	9	1089	2
WDS#5	Liard River, near Barite Showing	grab	Limestone, argillite, 2% barite, 1% chalcopryrite from 5 m wide bed.	<1	0.3	453	17	636	14
WDS#6	Liard River	grab	Quartzite; no mineralization.	1	<0.3	27	3	28	<2
WDS#7	Liard Canyon	grab	Black, carbonaceous shale, strongly oxidized; 0.5 m wide massive sulphide bed, 25% pyrite.						
WDS#8	Liard Canyon	grab	Black, carbonaceous shale, strong alteration; pyrite-pyrrhotite-quartz stringers cut across bedding.	5	<0.3	14	15	20	12
WDS#9	Liard Canyon	grab	Grey shale, oxidized; no mineralization.	10	<0.3	21	16	82	5
WDS#10	Liard Canyon	grab	Grey shale, oxidized; no mineralization.	4	<0.3	18	9	38	8
WDS#11	Liard Canyon	grab	Grey shale with quartz stringers; dyke, strong alteration; pyrite 10%.	2	<0.3	23	7	105	13
WDS#12	Liard Canyon	grab	Black, carbonaceous shale, interbedding alteration, quartz stringers.	15	0.8	100	66	968	58
WDS#13	Liard Canyon, near Main Showing	grab	Quartz vein sample taken in a cavern; strong alteration, 4% pyrite, 1% galena. Hosted in black carbonaceous shale.	11	<0.3	20	31	59	39
WDS#14	Liard Canyon, near Main Showing	grab	Massive pyrite in quartz vein; strong alteration, deformed.	60	3.3	89	32	76	75
WDS#15	Liard Canyon, near Main Showing	grab	Sandstone-limestone; 10% pyrite.	15	<0.3	36	10	37	6
WDS#16	Liard Canyon, near Main Showing	grab	Massive pyrite in carbonaceous shale host.	3	4.5	23	26	10	<2
WDS#17	Liard River	grab	Massive pyrite bed, 1 m wide. Light grey shale host.	1	1.1	45	149	3	25
WDS#18	Liard Canyon, near Main Showing	grab	Calcareous sandstone/limestone; 5% pyrite, barite, chalcopryrite, fine-grained.	23	3.9	32	36	21	301

APPENDIX C



GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-2458
1022 - 470 Granville St., Vancouver BC V6C 1V5

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WDS #1	1	33	<3	70	<.3	78	25	929	4.53	13	<5	<2	<2	342	.2	<2	<2	12	9.67	.067	5	18	4.60	102<.01	5	.26	.01	.11	2	5	
WDS #2	4	8	16	6	.3	4	1	10	.31	6	<5	<2	5	28	<.2	5	<2	16	.26	.003	5	6	.06	411<.01	8	.41	.01	.24	<2	9	
WDS #3	9	63	32	327	.5	58	6	71	1.68	18	<5	<2	5	110	4.6	8	3	59	1.18	.115	6	12	.23	75<.01	10	.64	.01	.25	<2	2	
WDS #4	2	12	9	1089	<.3	58	23	1304	9.83	2	<5	<2	8	46	3.5	<2	<2	129	1.03	.372	61	4	.33	83<.01	5	1.28	<.01	.01	<2	1	
WDS #5	3	453	17	636	.3	61	13	83	2.16	14	<5	<2	4	165	2.4	3	2	9	.47	.154	10	15	.14	90<.01	5	1.63	.02	.13	<2	<1	
WDS #6	3	27	3	28	<.3	26	7	88	1.17	<2	<5	<2	<2	44	.3	<2	<2	5	.15	.034	6	14	.06	5235<.01	3	1.06	.01	.05	2	1	
YS #1	2	17	24	35	.5	4	1	81	.49	4	<5	<2	<2	3	<.2	<2	28	2	.01	.001	<1	17	.01	204<.01	<3	.05	.01	.02	8	3	
YS #2	3	11	38	120	.7	11	1	238	.86	53	<5	<2	<2	9	5.6	<2	35	3	1.02	<.001	1	10	.12	70<.01	3	.18	.01	.07	3	5	
YS #3	1	19	8	92	<.3	44	14	392	2.68	<2	<5	<2	3	9	<.2	<2	<2	83	.40	.048	7	130	1.75	203 .25	<3	1.50	.08	1.18	2	4	
YS #4	15	37	1997	61	80.8	13	1	61	.51	30	<5	<2	<2	3	1.1	<2	4763	1	.03	.001	<1	50	.01	20<.01	3	.04	<.01	.02	7	43	
CANOL TD-001	8	122	699	120	25.5	17	392	35	26.85	99999	<5	<2	3	9	<.2	48	2350	4	10.49	<.001	<1	50	.01	37<.01	2148	.27	.28	.13	7	5240	
CANOL TD-002	3	641	153	379	9.0	10	2	117	.71	940	<5	<2	2	5	4.6	<2	72	2	.18	.031	1	10	.04	30<.01	3	.21	.01	.15	<2	51	
CANOL TD-003	6	117	2799	80	45.9	9	223	109	37.09	99999	<5	<2	3	11	<.2	84	1127	1	7.37	<.001	<1	24	<.01	27<.01	1357	.18	.17	.09	<2	2740	
CANOL TD-004	1	35	<3	409	.3	413	46	1423	6.32	279	<5	<2	6	11	<.2	<2	5	105	2.93	.015	14	1056	10.67	1232 .30	4	4.86	.12	5.58	<2	26	
KID TD-006	<1	4503	14950	13099	132.6	28	70	1637	9.68	5803	<5	<2	3	58	370.7	9	322	9	4.25	.061	8	23	.08	16 .07	5	.41	.01	.02	<2	54	
KID TD-007	<1	7733	13014	23185	135.1	41	84	963	14.84	2779	<5	<2	3	26	514.1	<2	307	7	1.97	.042	8	19	.04	17 .08	7	.17	<.01	<.01	<2	32	
RE KID TD-007	<1	7590	12832	22969	131.6	42	84	950	14.44	2759	<5	<2	3	25	507.9	<2	302	6	1.92	.042	8	23	.03	17 .07	10	.16	<.01	.01	2	24	
VIKING #1	2	56	125	150	1.4	17	3	302	1.81	206	<5	<2	2	41	2.2	4	5	7	.64	.194	3	27	.24	17 .02	3	.37	.03	.04	5	9	
VIKING #5	<1	164	448	841	3.0	37	11	1299	4.74	18	<5	<2	7	174	15.1	<2	7	54	3.99	.038	14	45	.86	26 .26	5	3.71	.24	.35	<2	2	
VIKING #6	1	22	32	317	<.3	13	4	496	1.26	40	<5	<2	3	920	7.4	<2	<2	24	30.29	<.001	8	23	.29	14 .10	4	1.82	.14	.14	<2	7	
SY #1	3	9	13	154	<.3	23	5	713	1.53	38	<5	<2	2	316	.3	4	2	18	6.31	.025	1	11	.25	79<.01	4	.20	.01	.10	<2	6	
SY #2	2	58	41	417	3.3	40	5	281	1.55	62	<5	<2	2	47	2.7	24	2	10	1.03	.067	1	20	.04	54<.01	3	.16	.01	.05	4	12	
SY #3	2	19	20	43	.5	13	2	30	1.62	40	<5	<2	<2	14	<.2	2	<2	14	.10	.020	8	14	.06	275<.01	9	.50	.01	.26	<2	3	
SY #4	2	22	10	54	<.3	10	2	416	1.51	23	<5	<2	2	798	.5	2	3	12	24.18	.087	7	11	1.68	564<.01	6	.19	.01	.08	4	4	
SY #6	3	32	11	82	<.3	29	8	348	2.37	2	<5	<2	6	210	.5	<2	<2	34	6.85	.068	24	26	1.06	468<.01	7	1.33	.01	.25	<2	5	
SY #7	2	9	9	50	<.3	14	6	1385	1.67	13	<5	<2	2	642	.2	<2	<2	18	21.50	.124	20	32	.52	652<.01	4	.60	.01	.09	2	1	
PD #1	10	10949	18	233	92.1	19	21	3075	2.94	42	<5	<2	<2	142	4.2	7	<2	23	5.53	<.001	1	10	1.71	112<.01	8	.23	.03	.13	<2	2	
HWY #1	2	40	8	14	.4	7	<1	45	1.37	19	<5	<2	3	44	.3	2	<2	17	.24	.037	3	24	.02	163<.01	3	.25	<.01	.07	5	4	
STANDARD C2/AU-R	21	62	44	147	6.6	77	38	1207	4.01	44	22	9	38	53	20.5	16	21	75	.54	.102	42	69	1.06	213 .08	32	2.00	.06	.15	13	473	

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUN 26 1996

DATE REPORT MAILED: July 4/96

SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
LL

GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-2614

1022 - 470 Granville St., Vancouver BC V6C 1V5

AA
LL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WDS #8	<1	14	15	20	<.3	22	12	720	3.74	12	<5	<2	7	153	<.2	2	<2	5	10.06	.021	2	4	3.10	36<.01	3	.28	.03	.16	<2	5	
WDS #9	<1	21	16	82	<.3	25	14	501	3.90	5	<5	<2	11	89	.3	11	<2	6	12.08	.022	1	4	.41	152<.01	<3	.33	.03	.17	<2	10	
WDS #10	<1	18	9	38	<.3	35	11	544	3.51	8	<5	<2	11	202	<.2	2	5	4	14.34	.027	19	8	.86	43<.01	4	.61	.02	.14	<2	4	
WDS #11	<1	23	7	105	<.3	53	13	286	3.71	13	<5	<2	7	207	<.2	<2	<2	6	7.65	.015	5	13	1.31	41<.01	<3	.76	.03	.14	<2	2	
WDS #12	14	100	66	968	.8	82	25	1403	2.47	58	<5	<2	3	150	11.1	28	2	18	2.16	.030	8	15	.96	150<.01	6	.28	.01	.13	<2	15	
WDS #13	2	20	31	59	<.3	8	1	68	.97	39	<5	<2	<2	58	<.2	11	<2	3	.34	.015	1	16	.07	185<.01	3	.11	.01	.05	6	11	
WDS #14	5	89	32	76	3.3	46	<1	53	14.23	75	<5	<2	3	18	.9	24	<2	11	.08	.003	1	17	.05	7<.01	<3	.30	.01	.14	3	60	
WDS #15	2	36	10	37	<.3	30	6	417	2.52	6	<5	<2	3	142	<.2	9	<2	10	.59	.049	14	15	.50	56<.01	4	.47<.01	.25	<2	15		
RE WDS #15	2	37	10	37	<.3	29	6	421	2.53	7	<5	<2	3	143	<.2	10	<2	10	.59	.047	14	15	.50	62<.01	5	.47<.01	.25	<2	20		
WDS #16	<1	23	26	10	4.5	16	<1	39	15.03	<2	<5	<2	<2	8	<.2	<2	<2	4	.04<.001	<1	10	.01	1<.01	<3	.10	.01	.05	4	3		
WDS #17	<1	45	149	3	1.1	23	1	16	14.79	25	<5	<2	2	5	<.2	4	<2	4	.01<.001	<1	21	<.01	1<.01	<3	.07<.01	.04	<2	1			
WDS #18	5	32	36	21	3.9	16	<1	60	5.21	301	<5	<2	<2	100	<.2	27	2	11	.45	.263	1	19	.10	20<.01	<3	.30	.01	.14	<2	23	
STANDARD C2/AU-R	19	57	42	139	6.2	71	36	1160	3.88	44	18	7	34	52	20.1	16	23	72	.52	.095	41	64	1.00	209	.09	30	2.04	.07	.15	10	458

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB

- SAMPLE TYPE: ROCK AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 4 1996

DATE REPORT MAILED:

July 13/96

SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-3036

1022 - 470 Granville St., Vancouver BC V6C 1V5



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** oz/t
JP #31	1	44	<3	11	<.3	7	2	417	.83	<2	<5	<2	<2	3	<.2	<2	<2	5	.04	.021	4	14	.04	25	<.01	<3	.14	.01	.02	7	<5	<1	<.001
JP #32	<1	26	14	67	<.3	25	10	354	2.97	<2	<5	<2	11	185	.2	<2	<2	12	4.90	.049	49	28	1.47	139	<.01	4	2.07	.01	.24	<2	<5	<1	<.001
JP #33	7	65	40	118	.6	57	28	87	8.55	11	<5	<2	3	16	<.2	<2	<2	92	.34	.121	12	28	2.18	18	.01	<3	2.96	.01	.31	<2	<5	<1	<.001
JP #34	3	116	8	76	<.3	25	8	359	3.28	21	<5	<2	2	199	.6	2	<2	22	2.92	.068	6	10	1.01	178	<.01	6	.44	.01	.16	<2	<5	<1	<.001
WDS #18	<1	18	5	115	<.3	36	15	226	4.85	<2	<5	<2	8	11	<.2	<2	<2	26	.14	.028	27	49	2.76	79	<.01	5	3.74	.02	.17	<2	<5	1	<.001
WDS #19	<1	33	11	75	<.3	30	17	392	3.40	<2	<5	<2	7	102	<.2	<2	<2	15	3.10	.022	36	31	1.70	79	<.01	<3	2.50	.01	.16	<2	<5	1	.003
RE WDS #19	<1	37	9	78	<.3	32	17	411	3.57	3	<5	<2	7	106	<.2	<2	<2	15	3.27	.023	37	32	1.79	86	<.01	<3	2.61	.02	.17	<2	<5	1	.003
96 JCR #01	4	1269	<3	37	1.0	<1	68	353	12.72	563	10	<5	5	18	.5	24	295	100	.67	.121	7	7	1.47	18	.05	<3	1.84	.03	.15	<2	<5	<1	.027
96 JCR #02	9	2304	14	197	3.9	38	2	106	7.45	166	<5	<2	<2	5	3.6	<2	105	20	.13	.004	1	19	.20	6	<.01	<3	.29	<.01	.03	6	<5	<1	.010
AMCM #01	<1	4570	22003	74641	25.4	7	<1	4259	31.98	62	<5	<2	4	4	552.7	<2	56	16	.27	.010	4	15	.69	<1	.01	<3	1.00	<.01	.01	526	<5	<1	.001
STANDARD C2/AU-1	21	61	38	129	6.8	75	34	1198	4.08	44	21	8	35	55	20.6	14	19	74	.55	.102	43	66	1.02	200	.09	27	2.08	.07	.15	10	<5	2	.096

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB

- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 22 1996

DATE REPORT MAILED:

Aug 5/96

SIGNED BY: C. Leong

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

AA
LL

GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-2707 Page 1

1022 - 470 Granville St., Vancouver BC V6C 1V5

AA
LL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L4800N 5200E	<1	11	8	55	<.3	27	10	225	2.71	6	<5	<2	6	17	<.2	<2	<2	40	.24	.041	18	34	.55	170	.10	4	1.51	.01	.07	<2	2
L4800N 5225E	<1	8	6	37	<.3	28	7	180	2.39	4	<5	<2	7	17	<.2	<2	<2	36	.26	.027	22	32	.48	171	.08	3	1.22	.02	.04	<2	2
L4800N 5250E	1	9	6	46	<.3	26	9	163	2.55	<2	<5	<2	5	10	.3	<2	<2	41	.13	.019	15	34	.41	148	.09	3	1.47	.01	.05	<2	1
L4800N 5275E	<1	6	7	50	<.3	19	8	163	2.29	<2	<5	<2	4	12	.2	<2	3	37	.19	.015	12	27	.35	182	.08	3	1.15	.01	.04	<2	1
L4800N 5300E	<1	11	12	62	<.3	35	8	166	2.64	<2	<5	<2	6	16	<.2	<2	<2	36	.21	.009	18	29	.49	143	.08	<3	1.51	.02	.03	<2	4
RE L4800N 5300E	<1	11	8	62	<.3	37	9	166	2.63	<2	<5	<2	6	15	.2	2	<2	36	.21	.009	18	29	.48	145	.08	3	1.49	.02	.03	<2	2
L4800N 5325E	<1	6	5	27	<.3	26	14	158	2.26	9	<5	<2	3	20	.2	<2	2	17	.32	.013	12	12	.16	143	.01	<3	.92	.01	.05	<2	6
L4800N 5350E	<1	6	12	56	<.3	25	8	150	2.62	<2	<5	<2	4	14	<.2	3	<2	45	.19	.004	14	31	.42	130	.10	<3	1.63	.01	.02	<2	2
L4800N 5375E	1	3	11	61	<.3	15	6	129	2.27	<2	<5	<2	4	12	.2	<2	<2	46	.19	.009	15	26	.36	161	.08	<3	1.25	.01	.03	<2	<1
L4800N 5400E	<1	6	11	48	<.3	26	8	185	2.47	2	<5	<2	5	24	.2	<2	<2	39	.36	.018	17	32	.52	188	.09	<3	1.44	.02	.03	2	<1
L4800N 5425E	1	6	7	47	<.3	26	9	203	2.71	5	<5	<2	5	15	.2	<2	2	45	.26	.015	16	30	.51	207	.09	4	1.60	.02	.03	<2	<1
L4800N 5450E	2	48	14	33	<.3	34	15	66	3.31	2	<5	<2	5	12	<.2	3	<2	19	.21	.040	4	10	.18	205	<.01	<3	.88	.01	.05	<2	9
L4800N 5475E	5	44	43	116	<.3	47	35	182	5.68	2	<5	<2	9	16	<.2	<2	<2	18	.27	.024	43	20	.62	138	<.01	<3	1.31	.01	.04	<2	1
L4800N 5500E	<1	14	6	60	<.3	26	13	156	3.22	<2	<5	<2	6	12	<.2	<2	<2	37	.13	.017	24	32	.76	76	.03	5	2.07	.01	.03	<2	<1
L4800N 5550E	<1	8	7	74	<.3	30	9	87	3.62	<2	<5	<2	9	14	<.2	<2	<2	23	.29	.008	38	31	1.19	99	<.01	<3	2.27	.01	.03	2	<1
L4800N 5575E	1	7	3	66	<.3	24	15	416	3.93	<2	<5	<2	5	24	.4	<2	<2	86	.36	.060	17	31	.85	153	.20	<3	1.85	.02	.07	<2	<1
L4800N 5600E	<1	28	10	51	<.3	20	11	227	2.14	<2	<5	<2	5	32	.4	<2	<2	18	2.54	.026	15	18	.69	87	.01	<3	1.25	.01	.04	<2	1
L4600N 4600E	<1	3	8	37	<.3	9	5	103	1.91	<2	<5	<2	3	11	<.2	<2	3	40	.17	.007	12	22	.26	76	.10	3	.88	.01	.05	<2	<1
L4600N 4625E	<1	7	7	45	<.3	13	5	184	2.22	3	<5	<2	5	13	.2	<2	<2	37	.22	.047	15	26	.34	95	.10	3	.96	.01	.09	<2	1
L4600N 4650E	<1	5	5	49	<.3	15	5	167	2.06	<2	<5	<2	4	16	<.2	<2	<2	36	.29	.020	13	25	.35	163	.08	<3	1.19	.01	.05	<2	1
L4600N 4675E	<1	8	6	48	<.3	19	6	185	2.42	4	<5	<2	5	14	<.2	<2	<2	41	.21	.020	15	31	.38	148	.10	4	1.22	.02	.07	<2	4
L4600N 4700E	1	8	5	49	<.3	20	8	183	2.72	3	<5	<2	5	14	.2	<2	6	49	.23	.052	16	33	.41	198	.11	5	1.46	.02	.06	<2	<1
L4600N 4725E	<1	6	10	55	<.3	20	7	252	2.51	2	<5	<2	5	15	<.2	<2	4	43	.20	.052	16	29	.37	126	.10	4	1.26	.02	.08	<2	<1
L4600N 4750E	<1	9	12	83	<.3	24	10	275	2.67	<2	<5	<2	6	14	.2	2	<2	42	.23	.088	17	31	.53	169	.10	<3	1.42	.02	.09	<2	<1
L4600N 4775E	<1	11	10	48	<.3	34	11	256	2.84	7	<5	<2	6	17	<.2	<2	<2	46	.29	.128	15	37	.63	145	.12	<3	1.27	.02	.10	<2	2
L4600N 4800E	<1	11	7	48	<.3	36	12	272	2.84	6	<5	<2	5	20	<.2	<2	<2	43	.34	.093	16	36	.76	125	.12	<3	1.27	.02	.08	2	1
L4600N 4825E	<1	4	6	33	<.3	5	1	83	1.75	<2	<5	<2	2	7	.2	<2	2	37	.09	.035	14	21	.14	37	.09	<3	.82	.02	.04	2	<1
L4600N 4850E	1	10	5	55	<.3	26	9	206	3.18	11	<5	<2	6	12	<.2	<2	2	53	.18	.098	16	39	.45	146	.11	<3	1.70	.01	.07	2	3
L4600N 4875E	<1	9	10	51	<.3	25	8	192	2.88	6	<5	<2	6	12	<.2	<2	<2	49	.16	.098	15	38	.43	114	.11	<3	1.55	.02	.08	<2	1
L4600N 4900E	<1	9	6	44	<.3	25	8	182	2.69	6	<5	<2	7	16	<.2	2	2	44	.21	.030	15	40	.46	132	.11	<3	1.47	.02	.07	<2	1
L4600N 4925E	<1	6	10	40	<.3	16	4	131	2.26	5	<5	<2	5	11	<.2	<2	4	42	.14	.029	16	28	.32	109	.10	<3	1.28	.01	.04	<2	3
L4600N 4950E	1	8	6	58	<.3	23	9	177	2.87	6	<5	<2	6	12	<.2	<2	<2	51	.14	.069	15	38	.40	131	.11	3	1.69	.01	.07	<2	<1
L4600N 4975E	<1	14	11	50	<.3	31	9	261	2.50	6	<5	<2	8	18	<.2	<2	4	39	.29	.061	20	31	.62	120	.10	5	1.28	.02	.10	<2	11
L4600N 5000E	<1	8	8	42	<.3	27	6	214	2.51	8	<5	<2	5	12	<.2	<2	<2	40	.22	.087	14	28	.46	87	.10	4	1.10	.02	.06	<2	1
L4600N 5025E	<1	13	8	53	<.3	24	7	260	2.23	6	<5	<2	6	21	<.2	<2	<2	39	.30	.046	20	32	.55	132	.12	6	1.12	.02	.07	<2	1
STANDARD C2/AU-S	21	60	35	144	6.5	73	36	1213	4.00	44	19	8	36	54	21.5	19	22	73	.53	.094	43	62	1.01	201	.08	33	2.04	.06	.15	12	54

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 8 1996 DATE REPORT MAILED:

SIGNED BY.....D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

July 20/96



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L4600N 5050E	<1	14	4	48	<.3	22	6	185	2.21	5	<5	<2	6	19	<.2	<2	<2	39	.30	.040	19	32	.46	125	.12	3	1.26	.02	.08	<2	1
L4600N 5075E	<1	8	3	44	<.3	19	5	141	1.99	<2	<5	<2	6	15	<.2	<2	4	35	.24	.034	16	29	.39	94	.11	3	1.05	.02	.07	<2	2
L4600N 5100E	1	9	3	42	<.3	22	7	196	2.17	<2	<5	<2	6	17	<.2	2	<2	37	.26	.038	18	32	.44	112	.11	<3	1.18	.01	.07	<2	1
L4600N 5125E	1	11	10	60	<.3	32	13	199	2.92	8	<5	<2	7	13	<.2	<2	<2	46	.17	.040	15	40	.46	110	.12	<3	1.67	.02	.08	<2	2
L4600N 5150E	<1	10	3	38	<.3	29	9	238	2.21	4	<5	<2	7	15	.2	<2	3	36	.24	.054	16	29	.50	101	.10	<3	1.12	.02	.07	<2	2
L4600N 5175E	<1	3	6	34	<.3	13	4	94	1.83	4	<5	<2	4	11	<.2	<2	4	35	.15	.016	14	22	.23	72	.09	<3	1.02	.01	.05	<2	<1
L4600N 5200E	<1	6	<3	42	<.3	22	7	185	2.02	3	<5	<2	6	18	<.2	<2	3	34	.32	.037	17	27	.39	136	.10	<3	1.08	.02	.06	<2	<1
L4600N 5225E	<1	7	4	37	<.3	18	5	156	2.06	<2	<5	<2	6	19	<.2	<2	4	37	.32	.038	20	28	.38	150	.09	<3	1.18	.02	.04	<2	<1
L4600N 5250E	1	10	<3	44	<.3	17	9	97	2.22	<2	<5	<2	3	20	<.2	<2	2	12	.44	.014	8	7	.13	57	<.01	4	.61	.01	.04	<2	1
L4600N 5275E	<1	14	<3	10	<.3	16	9	695	.50	<2	8	<2	<2	232	.7	<2	3	7	5.78	.100	5	6	.58	480	.01	5	.50	.03	.03	<2	1
L4600N 5300E	<1	13	7	35	<.3	24	7	278	2.01	4	<5	<2	3	60	<.2	2	5	30	1.19	.065	17	26	.57	208	.07	<3	.96	.02	.05	<2	2
L4600N 5325E	1	24	6	43	<.3	32	14	284	2.45	<2	<5	<2	<2	144	<.2	<2	<2	21	3.09	.066	15	21	.65	310	.03	<3	1.40	.02	.04	<2	1
L4600N 5350E	<1	8	8	45	<.3	25	10	191	2.73	2	<5	<2	5	21	<.2	<2	2	42	.39	.007	16	31	.42	168	.08	<3	1.56	.02	.04	2	1
L4600N 5375E	1	5	5	45	<.3	21	9	168	2.44	2	<5	<2	5	14	<.2	<2	6	46	.21	.012	17	30	.35	161	.09	4	1.53	.01	.03	<2	<1
L4600N 5400E	1	21	10	50	<.3	28	8	170	2.50	2	<5	<2	5	18	<.2	<2	<2	39	.29	.047	17	31	.44	172	.09	<3	1.44	.02	.04	<2	2
L4600N 5425E	1	10	11	105	<.3	18	12	1170	2.00	<2	<5	<2	3	21	.3	<2	<2	37	.45	.054	13	23	.30	271	.07	<3	1.09	.02	.05	<2	1
L4600N 5450E	1	37	8	87	<.3	34	9	256	3.07	<2	<5	<2	4	40	.6	<2	<2	28	.81	.073	10	26	.95	267	.03	<3	1.91	.02	.05	<2	1
L4600N 5475E	2	12	11	130	<.3	22	9	103	2.89	23	<5	<2	3	9	<.2	9	<2	40	.13	.020	10	11	.24	73	.01	<3	.82	.01	.04	<2	2
L4600N 5500E	1	13	6	73	<.3	18	15	645	1.76	<2	<5	<2	3	28	<.2	<2	<2	24	.63	.030	17	17	.29	148	.01	4	1.48	.01	.05	<2	<1
L4600N 5525E	<1	45	12	101	<.3	23	21	1048	3.02	6	<5	<2	5	46	.2	3	<2	15	1.34	.047	11	15	.42	172	<.01	3	1.23	.01	.06	<2	<1
L4600N 5550E	1	13	<3	57	<.3	7	2	233	.42	<2	<5	<2	<2	117	.8	<2	<2	3	3.98	.107	3	3	.57	131	<.01	7	.30	.01	.05	<2	<1
L4600N 5575E	<1	6	7	80	<.3	10	9	474	2.88	<2	<5	<2	6	15	.2	<2	<2	16	.33	.072	27	10	.14	200	<.01	<3	.99	.01	.07	<2	<1
L4400N 4600E	<1	8	<3	48	<.3	26	9	197	2.79	6	<5	<2	6	15	.5	<2	<2	51	.18	.024	15	40	.40	188	.11	3	1.64	.01	.04	<2	9
L4400N 4625E	1	9	7	52	<.3	25	10	230	2.85	3	<5	<2	7	14	.3	2	<2	50	.18	.026	17	41	.46	171	.12	<3	1.71	.01	.05	<2	<1
RE L4400N 4625E	1	10	<3	49	<.3	23	9	215	2.75	3	<5	<2	7	14	<.2	<2	4	48	.18	.025	17	40	.44	162	.11	<3	1.64	.01	.05	<2	<1
L4400N 4650E	1	6	7	50	<.3	25	11	283	2.71	3	<5	<2	5	12	<.2	3	<2	50	.18	.059	14	36	.33	174	.11	<3	1.48	.01	.05	<2	<1
L4400N 4675E	1	11	5	51	<.3	26	12	353	2.86	2	<5	<2	7	21	<.2	<2	3	52	.32	.033	20	42	.48	275	.13	<3	1.67	.02	.05	<2	<1
L4400N 4700E	<1	12	<3	46	<.3	37	11	291	2.97	<2	<5	<2	7	22	.4	<2	4	55	.36	.063	20	48	.63	241	.14	<3	1.67	.02	.05	<2	<1
L4400N 4725E	1	8	4	75	<.3	31	13	470	2.70	2	<5	<2	4	14	<.2	<2	<2	50	.20	.054	13	37	.45	303	.09	<3	1.55	.02	.05	<2	1
L4400N 4750E	1	12	6	48	<.3	28	10	373	2.55	<2	<5	<2	6	18	<.2	<2	3	47	.27	.029	18	38	.44	265	.10	<3	1.47	.02	.04	<2	<1
L4400N 4775E	<1	8	11	58	<.3	36	11	283	2.90	3	<5	<2	5	15	<.2	<2	3	50	.23	.071	14	44	.55	278	.11	<3	1.66	.01	.06	<2	<1
L4400N 4800E	1	19	6	43	<.3	39	11	417	2.54	6	<5	<2	7	31	<.2	2	<2	38	.58	.080	22	34	.81	185	.12	<3	1.02	.04	.04	<2	1
L4400N 4825E	<1	11	8	53	<.3	33	13	226	3.13	4	<5	<2	7	17	.3	4	<2	57	.22	.031	17	47	.48	249	.13	<3	1.89	.01	.05	<2	1
L4400N 4850E	1	13	6	44	<.3	33	12	275	2.99	<2	<5	<2	8	20	<.2	<2	2	55	.34	.052	19	51	.58	232	.13	<3	1.65	.02	.05	<2	1
L4400N 4875E	1	8	5	52	<.3	23	9	198	2.80	3	<5	<2	4	13	<.2	3	<2	52	.22	.054	16	37	.38	179	.11	3	1.57	.01	.06	<2	1
STANDARD C2/AU-S	19	55	41	131	6.4	71	36	1126	3.81	45	20	8	33	51	19.0	17	23	69	.55	.088	39	65	.96	199	.08	27	1.93	.06	.14	11	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L4400N 4900E	<1	18	5	41	<.3	32	11	352	2.55	7	<5	<2	7	25	.4	3	4	37	.40	.066	22	34	.69	173	.10	<3	1.07	.03	.04	<2	1
L4400N 4925E	<1	12	7	50	<.3	38	13	293	2.84	5	<5	<2	6	19	.2	<2	3	49	.31	.102	16	42	.70	204	.13	<3	1.54	.02	.06	<2	1
L4400N 4950E	<1	19	4	44	<.3	40	11	465	2.94	5	<5	<2	8	32	<.2	<2	<2	51	.52	.085	27	47	.79	251	.15	<3	1.38	.03	.05	<2	1
L4400N 4975E	<1	10	3	55	<.3	29	10	222	2.95	<2	<5	<2	7	15	<.2	<2	4	53	.20	.058	19	46	.47	199	.11	4	1.66	.01	.05	<2	<1
L4400N 5000E	<1	12	5	58	<.3	39	14	254	3.22	<2	<5	<2	7	15	.4	4	4	59	.19	.043	20	50	.51	308	.12	<3	2.02	.02	.06	<2	1
L4400N 5025E	<1	8	3	38	<.3	25	7	180	2.47	<2	<5	<2	4	11	<.2	<2	<2	46	.17	.062	13	35	.35	150	.09	<3	1.25	.01	.05	<2	1
L4400N 5050E	<1	14	6	45	<.3	40	13	323	2.81	<2	<5	<2	7	18	.2	<2	3	48	.29	.047	14	44	.63	243	.13	<3	1.63	.02	.07	<2	<1
L4400N 5075E	<1	11	3	45	<.3	32	10	198	3.09	<2	<5	<2	7	14	.2	<2	5	58	.19	.062	18	46	.44	190	.12	<3	1.77	.01	.06	2	1
L4400N 5100E	1	10	3	59	<.3	25	10	237	2.89	2	<5	<2	6	12	<.2	<2	<2	55	.19	.088	19	39	.43	190	.11	3	1.63	.01	.05	2	246
L4400N 5125E	1	13	6	52	<.3	39	13	278	3.21	<2	<5	<2	8	18	.2	<2	<2	57	.25	.051	17	52	.58	226	.13	<3	1.81	.01	.06	2	11
L4400N 5150E	<1	10	<3	37	<.3	22	8	333	2.55	2	<5	<2	6	13	<.2	2	3	47	.16	.046	16	35	.35	154	.09	4	1.48	.01	.04	<2	3
L4400N 5175E	1	8	4	49	<.3	20	7	195	2.79	<2	<5	<2	5	16	<.2	<2	<2	52	.20	.018	16	38	.43	166	.12	<3	1.65	.02	.05	<2	3
L4400N 5200E	<1	12	4	43	<.3	24	7	189	2.43	<2	<5	<2	5	20	.2	<2	<2	42	.30	.040	18	33	.46	189	.11	<3	1.33	.02	.04	2	1
L4400N 5225E	<1	9	5	48	<.3	28	11	266	2.92	3	<5	<2	7	18	<.2	<2	<2	54	.23	.048	19	46	.51	173	.14	<3	1.59	.02	.06	<2	2
L4400N 5250E	1	9	5	49	<.3	31	10	309	2.70	<2	<5	<2	6	18	.3	<2	5	49	.25	.043	14	39	.50	166	.13	5	1.47	.02	.06	<2	1
L4400N 5275E	<1	14	3	42	<.3	36	11	400	2.86	3	<5	<2	8	26	<.2	<2	<2	49	.38	.061	23	45	.58	197	.14	<3	1.47	.03	.06	<2	1
L4400N 5300E	<1	9	5	45	<.3	22	8	252	2.51	<2	<5	<2	6	17	.2	2	3	46	.23	.035	16	36	.43	172	.12	<3	1.43	.02	.05	<2	<1
L4400N 5325E	1	10	3	44	<.3	28	10	273	2.65	6	<5	<2	6	18	<.2	2	2	48	.26	.038	20	42	.47	198	.12	<3	1.46	.01	.04	<2	1
L4400N 5350E	<1	11	9	43	<.3	25	9	280	2.58	2	<5	<2	6	22	<.2	<2	<2	43	.34	.054	21	37	.47	193	.11	<3	1.35	.02	.04	<2	2
L4400N 5375E	<1	10	6	42	<.3	27	10	238	2.64	3	<5	<2	6	28	<.2	<2	<2	44	.44	.058	22	37	.53	250	.12	3	1.33	.03	.04	<2	1
L4400N 5400E	<1	13	5	46	<.3	28	9	240	2.65	4	<5	<2	7	19	<.2	<2	4	45	.28	.048	23	42	.50	186	.12	<3	1.42	.02	.06	<2	1
L4400N 5425E	<1	14	<3	43	<.3	34	10	318	2.99	<2	<5	<2	8	21	<.2	<2	2	54	.29	.037	24	50	.55	216	.15	<3	1.60	.02	.06	<2	1
L4400N 5450E	<1	9	7	32	<.3	18	5	156	1.73	2	<5	<2	7	14	<.2	2	3	25	.20	.020	28	24	.35	150	.06	<3	.91	.01	.06	<2	3
L4400N 5475E	<1	8	14	53	<.3	24	10	220	2.72	3	<5	<2	6	17	.2	<2	2	50	.22	.026	20	41	.45	184	.13	<3	1.57	.02	.05	<2	1
RE L4400N 5475E	<1	10	9	51	<.3	24	8	207	2.59	2	<5	<2	6	16	<.2	<2	4	48	.21	.026	18	39	.42	170	.12	<3	1.45	.02	.05	<2	1
L4400N 5500E	1	15	5	46	<.3	43	14	421	3.01	6	<5	<2	7	25	.8	3	2	49	.39	.069	22	45	.74	230	.14	<3	1.58	.03	.07	<2	1
L4400N 5525E	1	9	8	41	<.3	23	8	221	2.29	3	<5	<2	6	16	.5	<2	<2	37	.25	.034	20	32	.46	162	.10	<3	1.10	.02	.05	<2	1
L4400N 5550E	<1	10	<3	49	<.3	26	9	307	2.67	5	<5	<2	6	21	.2	<2	3	45	.31	.047	19	38	.53	206	.13	<3	1.41	.02	.06	<2	3
L3800N 5300E	1	13	7	44	<.3	36	10	243	2.83	2	<5	<2	6	18	.4	<2	<2	50	.28	.038	14	43	.55	248	.12	<3	1.76	.02	.06	<2	<1
L3800N 5325E	1	11	9	68	<.3	39	12	305	3.22	4	<5	<2	5	14	<.2	<2	2	56	.20	.091	18	44	.52	315	.11	<3	1.96	.01	.06	<2	1
L3800N 5350E	<1	11	5	57	<.3	32	12	219	3.30	3	<5	<2	6	16	<.2	<2	<2	62	.18	.058	16	54	.47	247	.15	<3	2.04	.01	.07	<2	4
L3800N 5375E	1	11	<3	51	<.3	31	10	214	3.13	6	<5	<2	7	14	<.2	2	<2	55	.15	.053	16	46	.45	176	.12	<3	1.90	.01	.06	2	1
L3800N 5400E	<1	5	6	29	<.3	16	5	169	1.70	<2	<5	<2	4	17	<.2	<2	<2	26	.30	.040	16	24	.44	216	.07	<3	.80	.01	.04	2	<1
L3800N 5425E	1	8	6	55	<.3	21	9	168	3.06	3	<5	<2	6	14	.3	<2	<2	61	.15	.048	17	45	.40	160	.12	<3	1.87	.01	.05	<2	9
L3800N 5450E	1	7	5	35	<.3	24	6	155	2.18	4	<5	<2	5	10	<.2	<2	<2	36	.15	.039	15	34	.44	84	.08	<3	.98	.01	.04	<2	<1
STANDARD C2/AU-S	20	58	36	138	6.5	70	37	1176	3.98	44	19	8	35	53	20.9	18	23	72	.53	.090	41	66	.98	197	.08	30	2.01	.06	.14	11	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3800N 5475E	1	7	8	40	<.3	22	8	160	2.23	3	<5	<2	5	15	.3	<2	<2	42	.22	.018	18	33	.40	180	.09	4	1.35	.01	.04	2	349
RE L3800N 5475E	1	7	9	40	<.3	22	7	159	2.26	4	<5	<2	5	15	<.2	<2	<2	42	.23	.018	17	34	.41	186	.09	4	1.38	.01	.04	2	382
L3800N 5500E	<1	8	11	48	.3	25	8	189	2.57	4	<5	2	6	18	<.2	2	2	48	.28	.021	15	38	.44	165	.12	5	1.49	.02	.05	2	546
L3800N 5525E	<1	13	8	42	.4	28	7	194	2.23	6	<5	2	6	23	<.2	<2	2	34	.47	.063	21	33	.47	178	.08	3	.99	.03	.04	2	527
L3800N 5550E	<1	7	7	46	.3	19	6	187	2.26	2	<5	<2	5	22	.5	2	<2	36	.40	.034	19	29	.41	249	.08	3	1.21	.02	.04	<2	759
L3800N 5575E	<1	7	9	45	.3	19	5	134	2.15	2	<5	<2	5	21	<.2	<2	<2	36	.37	.037	18	28	.40	222	.08	<3	1.22	.02	.05	<2	1074
L3800N 5600E	<1	6	7	62	<.3	18	8	343	2.22	<2	<5	<2	4	16	<.2	2	2	42	.28	.017	16	30	.38	188	.10	3	1.30	.02	.06	<2	368
L3800N 5625E	<1	7	7	52	<.3	19	6	174	2.49	7	<5	<2	4	17	<.2	<2	<2	46	.26	.029	14	32	.42	141	.11	<3	1.40	.02	.07	<2	147
L3800N 5650E	<1	6	8	105	.3	22	10	728	2.42	5	<5	<2	3	17	<.2	<2	3	42	.40	.095	13	30	.34	466	.07	5	1.54	.02	.09	<2	1421
L3800N 5675E	1	10	11	227	<.3	41	12	385	3.56	6	<5	<2	3	20	1.2	2	2	64	.33	.101	14	42	.52	655	.15	4	2.40	.02	.10	<2	138
L3800N 5700E	1	5	11	110	<.3	14	7	547	2.48	2	<5	<2	4	12	.9	<2	<2	49	.20	.074	17	27	.26	268	.09	<3	1.10	.01	.06	<2	122
L3800N 5725E	1	8	10	66	<.3	16	6	246	2.82	4	<5	<2	5	10	.2	<2	4	56	.16	.016	21	33	.32	128	.10	<3	1.22	.02	.06	2	149
L3800N 5750E	<1	19	4	25	<.3	10	1	168	.50	<2	8	<2	<2	294	.5	2	<2	2	28.43	.018	1	15	.39	415	<.01	8	.08	.01	.01	<2	19
L3500N 5300E	<1	10	11	68	<.3	44	10	464	2.69	4	<5	<2	5	14	.2	<2	5	47	.38	.075	16	44	.62	196	.09	4	1.44	.02	.06	<2	22
L3500N 5325E	<1	13	8	65	<.3	39	10	260	3.25	6	<5	<2	7	16	<.2	<2	<2	58	.23	.076	19	55	.52	346	.14	<3	2.08	.02	.07	<2	14
L3500N 5350E	<1	10	6	97	<.3	31	11	601	2.73	3	<5	<2	5	11	<.2	<2	<2	49	.19	.101	15	40	.40	192	.10	<3	1.87	.01	.06	<2	19
L3500N 5375E	<1	10	6	96	<.3	41	12	369	3.25	3	<5	<2	5	14	.3	<2	<2	57	.26	.137	17	47	.59	252	.12	4	2.14	.01	.07	<2	8
L3500N 5400E	<1	7	6	61	<.3	25	9	309	2.59	<2	<5	<2	4	14	<.2	<2	<2	49	.20	.057	15	39	.43	187	.11	<3	1.61	.01	.05	<2	19
L3500N 5425E	<1	10	4	51	<.3	28	8	238	2.73	5	<5	<2	4	15	<.2	<2	<2	51	.20	.046	15	43	.41	224	.11	5	1.65	.02	.05	<2	11
L3500N 5450E	1	11	8	64	<.3	49	11	247	3.22	4	<5	<2	5	15	<.2	<2	<2	58	.25	.082	16	51	.63	252	.11	<3	1.94	.02	.06	2	12
L3500N 5475E	1	10	5	59	<.3	42	9	247	3.00	4	<5	<2	5	17	<.2	<2	<2	55	.29	.085	16	48	.52	262	.11	3	1.85	.02	.08	<2	7
L3500N 5500E	1	8	10	79	<.3	25	10	283	2.94	3	<5	<2	5	17	<.2	<2	<2	57	.23	.051	16	40	.45	229	.12	<3	1.93	.01	.05	2	11
L3500N 5525E	<1	9	6	55	<.3	28	9	192	2.84	3	<5	<2	4	15	.4	<2	<2	52	.26	.044	14	41	.44	153	.12	<3	1.71	.02	.07	<2	11
L3500N 5550E	1	5	10	67	<.3	28	9	439	2.58	2	<5	<2	3	14	<.2	2	2	46	.27	.093	14	35	.38	195	.09	4	1.44	.02	.06	<2	22
L3500N 5575E	1	7	8	74	<.3	33	10	258	3.31	5	<5	<2	4	14	.3	2	<2	61	.25	.154	15	43	.52	258	.10	4	1.88	.01	.06	<2	10
L3500N 5600E	1	5	8	77	<.3	31	9	497	2.68	2	<5	<2	5	17	<.2	<2	<2	53	.32	.040	16	38	.44	405	.09	3	1.53	.02	.06	2	275
L3500N 5625E	<1	6	8	97	<.3	37	8	532	2.50	<2	<5	<2	3	15	<.2	<2	3	46	.32	.083	14	40	.46	300	.10	<3	1.55	.02	.07	<2	18
L3500N 5650E	1	7	5	57	<.3	23	8	259	2.68	5	<5	<2	4	14	<.2	<2	2	49	.23	.027	14	37	.41	171	.11	<3	1.37	.02	.08	2	19
L3500N 5675E	<1	7	6	41	<.3	34	9	313	2.37	3	<5	<2	5	15	<.2	<2	<2	32	.32	.076	16	26	.71	72	.08	<3	.86	.02	.11	2	10
L3500N 5700E	1	8	9	55	<.3	33	12	194	2.96	5	<5	<2	5	11	<.2	<2	<2	50	.20	.070	16	38	.49	154	.09	3	1.57	.02	.05	2	10
L3500N 5725E	1	6	10	64	<.3	19	8	195	2.99	4	<5	<2	5	12	<.2	<2	5	56	.20	.075	17	33	.36	147	.09	<3	1.41	.01	.06	<2	21
L3500N 5750E	1	7	14	71	<.3	23	8	274	3.03	3	<5	<2	3	12	<.2	<2	<2	56	.21	.043	16	36	.45	270	.10	<3	1.77	.01	.05	2	26
L3500N 5775E	1	6	8	61	<.3	16	7	633	2.36	3	<5	<2	4	14	<.2	<2	<2	40	.27	.074	15	25	.34	260	.08	4	1.15	.01	.07	2	20
L3500N 5800E	1	5	7	58	<.3	18	7	169	2.50	3	<5	<2	4	12	<.2	<2	2	45	.20	.032	17	29	.33	132	.09	<3	1.29	.01	.05	2	13
L3500N 5825E	1	5	6	62	<.3	17	6	165	2.11	<2	<5	<2	4	13	.2	<2	<2	34	.27	.024	14	22	.31	170	.06	<3	1.03	.01	.07	<2	131
STANDARD C2/AU-S	20	58	37	140	6.3	71	33	1162	3.85	39	19	7	34	52	20.2	16	21	70	.55	.085	40	65	.97	202	.08	29	2.01	.07	.14	11	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3500N 5850E	1	16	13	76	<.3	17	6	248	1.39	2	10	<2	<2	104	.7	<2	<2	18	3.33	.036	7	17	.40	418	.03	9	.76	.01	.05	<2	24
L3500N 5875E	1	15	9	19	<.3	12	4	173	.64	3	11	<2	<2	123	.7	<2	<2	6	4.26	.044	3	6	.27	405	.01	8	.28	.02	.01	<2	70
~~L3500N 5900E~~	1	17	11	25	<.3	15	6	224	.98	6	21	<2	<2	156	.9	2	<2	8	5.22	.056	3	8	.34	517	.01	9	.33	.01	.02	<2	26
L2600E 350N	1	7	9	64	<.3	19	6	225	1.95	2	<5	<2	3	12	.2	<2	<2	37	.17	.027	12	23	.25	242	.04	3	.83	.01	.07	2	27
L2600E 300N	1	9	7	94	<.3	24	10	289	2.20	5	<5	<2	3	16	.2	<2	2	45	.28	.018	13	23	.28	297	.04	5	1.01	.01	.09	<2	6
L2600E 250N	1	11	12	98	<.3	23	9	371	2.22	5	<5	<2	3	14	.2	<2	3	42	.24	.053	14	24	.28	278	.04	<3	.99	.01	.11	<2	6
L2900E 1400N	1	4	9	241	.3	14	8	843	1.69	2	<5	<2	2	12	.6	<2	3	37	.20	.093	11	20	.20	627	.04	<3	.98	.01	.07	<2	13
L2900E 1350N	1	8	7	80	<.3	21	7	223	2.17	8	<5	<2	4	13	.2	<2	4	40	.20	.025	15	26	.38	257	.07	<3	.98	.01	.09	<2	7
L2900E 1300N	1	7	9	66	<.3	19	5	171	2.07	2	<5	<2	4	13	<.2	<2	<2	36	.18	.021	14	26	.37	183	.05	<3	.96	.01	.09	<2	8
L2900E 1250N	<1	7	11	192	<.3	23	8	320	2.23	2	<5	<2	4	17	.4	<2	<2	43	.29	.075	15	28	.37	325	.05	5	1.21	.01	.14	<2	6
RE L2900E 1250N	1	6	8	182	<.3	24	7	301	2.11	<2	<5	<2	3	16	.3	<2	<2	40	.27	.070	14	27	.34	308	.05	<3	1.16	.01	.13	<2	8
L2900E 1200N	1	12	10	121	<.3	18	6	621	1.55	<2	<5	<2	<2	18	.3	<2	<2	31	.22	.057	9	16	.18	505	.03	3	.89	.02	.07	<2	19
L2900E 1150N	1	11	11	112	<.3	27	9	218	2.69	6	<5	<2	4	16	.5	<2	<2	57	.22	.049	16	35	.40	427	.06	5	1.50	.01	.06	2	5
L2900E 1100N	1	10	13	83	<.3	19	7	278	2.00	2	<5	<2	3	14	.2	<2	<2	48	.20	.037	12	24	.27	366	.02	<3	1.06	.01	.06	<2	16
L2900E 1050N	1	31	11	109	<.3	36	9	355	2.69	8	<5	<2	4	17	<.2	<2	4	50	.24	.054	14	33	.39	421	.02	4	1.02	.01	.08	<2	29
L2900E 1000N	1	17	11	127	<.3	27	8	490	2.14	5	<5	<2	3	12	.7	<2	3	52	.17	.046	14	25	.26	471	.03	<3	1.27	.01	.05	2	4
L2900E 950N	1	9	6	81	<.3	8	5	311	1.79	<2	<5	<2	<2	8	.3	<2	<2	45	.08	.039	10	17	.10	183	.03	<3	.65	.01	.06	<2	9
L2900E 900N	1	7	5	67	<.3	9	5	219	1.82	2	<5	<2	<2	11	.7	<2	2	47	.15	.037	11	17	.15	230	.02	<3	.66	.01	.06	<2	5
L2900E 850N	1	10	10	136	<.3	22	9	329	2.42	6	<5	<2	5	16	.2	<2	<2	49	.25	.031	16	29	.34	343	.06	<3	1.20	.02	.06	2	6
L2900E 800N	1	9	12	58	<.3	22	8	269	2.26	6	<5	<2	4	12	<.2	<2	<2	40	.20	.040	15	29	.36	175	.05	<3	1.02	.01	.07	<2	8
L2900E 750N	1	6	10	89	<.3	16	9	443	2.02	2	<5	<2	2	12	.2	<2	<2	46	.19	.037	12	22	.23	281	.04	<3	1.02	.01	.06	<2	10
L2900E 700N	1	7	7	82	<.3	18	7	323	2.01	3	<5	<2	3	13	<.2	<2	2	41	.19	.039	12	24	.29	254	.06	<3	1.05	.01	.06	2	7
L2900E 650N	1	5	7	63	<.3	13	6	194	1.97	<2	<5	<2	3	13	.2	<2	4	42	.18	.030	12	21	.24	210	.04	3	.92	.01	.08	<2	6
L2900E 600N	1	5	8	57	<.3	11	5	176	1.76	3	<5	<2	2	10	.3	<2	<2	44	.14	.013	12	19	.17	225	.03	<3	.73	.01	.05	2	7
L2900E 550N	1	9	7	41	<.3	17	5	124	1.73	7	<5	<2	2	9	<.2	<2	<2	34	.14	.016	11	22	.25	200	.02	3	.85	.01	.05	2	8
L2900E 500N	1	7	7	42	<.3	16	5	135	1.97	6	<5	<2	3	8	<.2	<2	<2	40	.14	.012	14	23	.27	189	.04	3	.89	.01	.04	2	7
L2900E 450N	1	6	5	52	<.3	14	5	174	1.84	4	<5	<2	2	10	<.2	<2	<2	38	.16	.025	12	22	.23	213	.04	3	.85	.01	.04	<2	3
L2900E 400N	1	8	6	54	<.3	21	6	200	1.86	4	<5	<2	3	13	<.2	2	<2	33	.20	.026	14	25	.27	190	.04	5	.69	.01	.07	<2	5
L2900E 350N	1	8	6	53	<.3	18	6	176	1.78	2	<5	<2	3	13	.2	<2	2	34	.20	.033	12	20	.26	209	.04	3	.74	.01	.07	<2	12
L2900E 300N	1	11	9	51	<.3	27	8	272	2.79	6	<5	<2	7	20	<.2	<2	<2	54	.42	.047	28	46	.55	194	.05	<3	.98	.02	.06	2	15
L3100E 1350N	1	10	7	66	<.3	19	5	260	2.01	4	<5	<2	2	17	<.2	<2	<2	42	.28	.031	13	24	.31	409	.02	<3	1.07	.01	.09	<2	15
L3100E 1300N	1	6	9	73	<.3	12	6	437	1.67	<2	<5	<2	2	12	<.2	<2	2	37	.17	.055	11	18	.18	312	.03	<3	.89	.01	.07	2	12
L3100E 1250N	1	8	5	165	<.3	14	7	360	1.91	<2	<5	<2	3	11	.4	<2	2	42	.13	.047	15	24	.22	358	.04	<3	1.06	.01	.06	<2	7
L3100E 1200N	1	6	7	83	<.3	19	7	138	2.10	4	<5	<2	3	12	<.2	<2	<2	45	.16	.034	15	26	.31	313	.05	<3	1.11	.01	.05	2	24
L3100E 1150N	1	7	10	92	<.3	19	7	154	2.21	<2	<5	<2	3	10	<.2	2	<2	46	.14	.032	14	27	.31	227	.05	3	1.24	.01	.05	2	3
STANDARD C2/AU-S	20	57	40	138	6.3	69	34	1161	3.78	45	17	7	34	53	19.5	16	20	70	.55	.087	39	64	.96	211	.09	33	1.98	.06	.15	11	53

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3100E 1100N	<1	11	6	82	<.3	25	7	299	2.30	<2	<5	<2	5	13	<.2	2	<2	41	.17	.039	18	30	.38	265	.06	3	1.19	.01	.05	<2	10
L3100E 1050N	1	12	14	85	<.3	19	8	188	2.40	6	<5	<2	2	10	<.2	<2	<2	43	.12	.076	10	20	.29	176	.02	<3	.93	.01	.05	<2	13
L3100E 1000N	1	13	12	184	<.3	35	12	380	2.81	5	<5	<2	5	13	.7	<2	4	56	.20	.146	15	37	.43	307	.08	<3	1.66	.01	.06	<2	10
L3100E 950N	1	8	12	84	<.3	15	6	161	2.31	<2	<5	<2	3	12	.3	<2	<2	52	.17	.035	14	24	.24	244	.05	<3	1.09	.01	.04	<2	9
L3100E 900N	<1	8	11	83	<.3	8	6	204	1.79	2	<5	<2	2	8	.7	2	3	43	.11	.040	12	17	.11	235	.03	<3	.66	.01	.05	<2	8
L3100E 850N	1	6	8	54	<.3	9	6	440	1.80	4	<5	<2	<2	13	.4	2	3	46	.21	.020	11	19	.19	236	.03	<3	.75	.01	.05	<2	10
L3100E 800N	<1	5	8	188	<.3	15	8	447	2.26	<2	<5	<2	3	15	.4	<2	2	45	.24	.069	14	23	.26	318	.06	3	.96	.01	.08	<2	7
L3100E 750N	<1	8	9	124	<.3	19	8	472	2.29	5	<5	<2	3	14	.3	<2	2	47	.23	.061	16	29	.34	349	.06	<3	1.11	.01	.07	<2	6
L3100E 700N	<1	6	11	123	<.3	19	8	306	2.19	2	<5	<2	3	12	<.2	<2	<2	45	.21	.037	16	27	.30	253	.04	3	1.08	.01	.06	<2	14
L3100E 650N	<1	5	9	109	<.3	16	9	526	2.04	<2	<5	<2	2	14	.5	<2	<2	46	.23	.036	11	22	.25	329	.04	<3	.98	.01	.05	<2	6
L3100E 600N	1	8	7	99	<.3	20	9	602	2.42	3	<5	<2	3	17	.2	<2	<2	49	.28	.028	13	28	.33	335	.05	3	1.19	.01	.07	<2	10
L3100E 550N	1	9	8	77	<.3	21	8	373	2.12	4	<5	<2	2	17	<.2	<2	<2	43	.28	.022	12	22	.28	288	.04	<3	1.05	.01	.10	<2	17
L3100E 500N	1	6	7	56	<.3	7	4	131	1.55	<2	<5	<2	2	9	.4	2	<2	37	.13	.025	12	15	.14	214	.03	4	.61	.01	.05	<2	9
L3100E 450N	<1	11	10	115	<.3	26	12	283	2.84	6	<5	<2	4	15	.4	<2	2	57	.24	.056	16	33	.44	241	.06	<3	1.55	.01	.08	<2	5
L3100E 400N	1	6	6	59	<.3	13	5	143	1.88	2	<5	<2	2	10	.5	<2	3	39	.17	.030	11	19	.23	126	.04	<3	.80	.01	.05	<2	5
L3100E 350N	1	14	9	110	<.3	29	11	471	2.15	8	<5	<2	4	19	.3	<2	<2	41	.28	.056	15	24	.31	374	.04	4	1.01	.01	.10	<2	7
L3100E 300N	1	5	5	164	<.3	14	9	514	1.98	<2	<5	<2	3	12	1.0	<2	<2	40	.18	.090	13	21	.21	312	.03	5	.89	.01	.09	<2	3
L3100E 250N	1	13	6	83	.3	16	5	94	1.30	<2	<5	<2	2	15	.4	<2	<2	35	.21	.039	11	16	.17	250	.02	<3	1.05	.01	.04	<2	8
L3400E 1400N	<1	5	8	88	<.3	13	7	205	1.89	<2	<5	<2	3	15	.3	<2	<2	38	.20	.063	15	21	.26	317	.04	<3	.95	.01	.07	<2	6
L3400E 1350N	1	6	10	102	<.3	17	8	585	2.03	<2	<5	<2	3	14	.2	<2	<2	41	.20	.083	15	24	.29	425	.04	<3	1.10	.01	.08	<2	9
RE L3400E 1350N	<1	6	8	99	<.3	16	8	576	1.99	<2	<5	<2	2	14	.4	<2	<2	40	.20	.082	15	23	.28	410	.04	<3	1.07	.01	.08	<2	16
L3400E 1300N	1	7	9	157	<.3	20	8	630	2.13	<2	<5	<2	2	18	.5	<2	3	42	.24	.083	13	25	.27	358	.04	<3	1.07	.01	.09	<2	4
L3400E 1250N	<1	4	10	145	<.3	9	7	268	1.77	<2	<5	<2	2	11	.8	<2	<2	41	.14	.050	14	18	.15	274	.03	<3	.83	.01	.06	<2	5
L3400E 1200N	1	6	8	141	<.3	19	8	236	2.44	2	<5	<2	3	13	<.2	<2	<2	56	.20	.041	17	28	.32	365	.05	<3	1.27	.01	.06	<2	7
L3400E 1150N	<1	9	11	102	<.3	27	9	303	2.24	4	<5	<2	4	11	.4	<2	<2	41	.15	.074	15	28	.32	260	.04	<3	1.20	.01	.06	<2	5
L3400E 1100N	1	6	6	91	<.3	14	6	250	1.91	2	<5	<2	2	15	.2	<2	<2	43	.22	.049	12	22	.23	316	.03	<3	.92	.01	.06	<2	10
L3400E 1050N	1	6	11	63	<.3	12	6	169	1.85	3	<5	<2	<2	13	.3	<2	<2	49	.20	.041	13	21	.22	323	.04	4	.96	.01	.06	<2	12
L3400E 1000N	1	7	8	51	<.3	10	4	83	1.62	5	<5	<2	<2	19	.3	<2	<2	45	.24	.026	10	18	.15	345	.03	3	.65	.01	.06	<2	30
L3400E 950N	1	5	6	153	<.3	11	8	454	2.22	<2	<5	<2	<2	8	.3	<2	<2	47	.10	.093	13	22	.22	174	.03	<3	.97	.01	.05	<2	2
L3400E 900N	1	9	6	72	<.3	12	6	597	1.88	5	<5	<2	<2	10	.6	<2	<2	40	.14	.037	12	18	.17	241	.04	4	.65	.01	.06	<2	7
L3400E 850N	1	5	7	109	<.3	14	9	509	1.85	<2	<5	<2	3	15	.3	<2	<2	37	.23	.073	14	20	.25	287	.04	<3	.90	.01	.08	<2	8
L3400E 800N	<1	10	12	60	<.3	25	7	193	2.37	4	<5	<2	5	15	<.2	<2	<2	39	.25	.052	19	30	.44	161	.07	<3	1.14	.02	.09	<2	3
L3400E 750N	1	5	6	85	<.3	15	6	376	1.89	3	<5	<2	3	13	.2	<2	<2	38	.21	.039	14	23	.27	299	.04	4	.96	.01	.06	<2	5
L3400E 700N	1	7	10	112	.3	16	9	903	1.90	<2	<5	<2	2	20	.5	<2	2	37	.32	.075	13	21	.23	490	.03	5	.92	.01	.10	<2	9
L3400E 650N	1	10	10	88	<.3	24	10	594	2.57	6	<5	<2	3	17	.3	<2	3	49	.24	.026	13	27	.33	367	.03	4	1.12	.01	.09	<2	9
STANDARD C2/AU-S	20	57	41	142	6.3	74	34	1166	3.87	42	24	8	34	52	20.0	15	20	71	.54	.091	40	62	.98	206	.08	29	2.01	.06	.15	11	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
L3400E 600N	2	9	9	83	<.3	18	9	300	2.24	4	<5	<2	3	17	<.2	<2	2	52	.22	.018	15	27	.30	332	.03	<3	1.17	.01	.08	<2	12
L3400E 550N	<1	11	12	102	<.3	11	5	70	1.15	<2	<5	<2	2	17	.9	2	<2	40	.21	.026	12	20	.22	346	.03	5	1.26	.01	.06	<2	4
L3400E 500N	1	11	10	74	<.3	10	5	288	1.49	2	<5	<2	2	18	<.2	<2	2	40	.23	.031	12	17	.21	276	.03	<3	.94	.01	.06	<2	8
L3400E 450N	1	11	13	101	<.3	11	7	350	1.86	6	<5	<2	3	12	<.2	<2	<2	44	.14	.061	13	18	.18	198	.03	4	.84	.01	.07	<2	3
L3400E 400N	1	11	12	100	<.3	17	10	379	2.00	8	<5	<2	3	14	<.2	<2	<2	42	.19	.062	13	21	.23	241	.03	4	.83	.01	.08	<2	3
L3400E 350N	1	19	15	176	<.3	28	12	653	2.49	6	<5	<2	6	21	.5	<2	<2	44	.30	.082	19	28	.37	408	.04	4	1.15	.01	.10	<2	2
RE L3400E 350N	1	17	13	171	<.3	30	10	648	2.45	4	<5	<2	6	21	<.2	2	<2	43	.29	.080	19	27	.37	400	.04	5	1.12	.02	.10	<2	2
L3600E 1400N	1	12	11	85	<.3	24	11	368	2.66	<2	<5	<2	5	16	.2	<2	7	51	.20	.041	20	34	.49	299	.07	<3	1.59	.01	.07	<2	1
L3600E 1350N	<1	5	12	112	<.3	12	8	396	2.19	5	<5	<2	3	15	<.2	<2	4	52	.22	.059	16	27	.30	351	.04	4	1.32	.01	.07	<2	1
L3600E 1300N	1	5	12	141	<.3	14	8	543	2.02	2	<5	<2	3	15	.2	<2	<2	42	.20	.089	15	25	.25	349	.03	3	.98	.01	.09	<2	3
L3600E 1250N	2	12	15	116	<.3	20	8	396	2.40	5	<5	<2	2	19	<.2	<2	2	59	.22	.029	13	27	.28	453	.03	6	1.24	.01	.10	<2	1
L3600E 1200N	1	12	10	217	<.3	11	9	1043	1.87	4	<5	<2	2	16	.8	<2	3	41	.20	.149	13	20	.19	576	.03	<3	1.14	.02	.09	<2	3
L3600E 1150N	1	8	11	63	<.3	16	8	264	2.30	5	<5	<2	2	16	<.2	<2	<2	56	.20	.019	12	28	.30	342	.01	<3	1.13	.01	.06	<2	1
L3600E 1100N	1	9	8	70	<.3	20	8	291	2.19	5	<5	<2	4	15	<.2	<2	<2	46	.20	.027	16	30	.33	406	.04	<3	1.22	.01	.08	<2	<1
L3600E 1050N	1	9	13	90	<.3	27	8	355	2.27	5	<5	<2	5	15	<.2	<2	2	40	.19	.052	18	29	.35	340	.05	<3	1.15	.01	.11	<2	1
L3600E 1000N	<1	5	<3	53	<.3	6	2	142	.20	5	<5	<2	<2	419	.7	2	<2	6	40.24	.016	1	4	.77	120	.01	6	.21	.01	.02	<2	<1
L3600E 950N	2	19	13	163	<.3	14	7	182	3.33	8	<5	<2	<2	15	<.2	<2	4	71	.15	.091	13	25	.25	257	.05	<3	1.22	<.01	.07	<2	1
L3600E 900N	1	7	9	78	<.3	10	5	134	2.04	2	<5	<2	3	11	.3	<2	3	44	.15	.017	14	22	.22	185	.03	3	.72	.01	.08	<2	1
L3600E 850N	1	8	8	88	<.3	14	7	220	2.18	6	<5	<2	3	15	.3	<2	3	44	.17	.047	16	27	.29	243	.04	<3	1.06	.01	.06	<2	1
L3600E 800N	1	8	8	116	<.3	11	7	411	1.76	2	<5	<2	3	17	<.2	<2	2	41	.25	.069	14	22	.24	332	.04	<3	1.08	.01	.07	<2	<1
L3600E 750N	1	7	13	134	<.3	10	7	484	1.76	<2	<5	<2	3	14	.3	2	<2	40	.23	.047	14	19	.20	303	.04	<3	.80	.01	.08	<2	<1
L3600E 700N	1	13	11	161	<.3	24	10	679	2.25	4	<5	<2	3	23	.2	<2	2	45	.37	.036	15	25	.32	490	.04	3	1.15	.02	.12	<2	2
STANDARD C2/AU-S	20	59	35	142	6.5	68	34	1199	4.03	42	20	8	36	55	19.6	19	21	75	.54	.088	42	68	1.00	205	.09	25	2.10	.06	.16	12	55

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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GEOCHEMICAL EXTRACTION-ANALYSIS CERTIFICATE

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1022 - 470 Granville St., Vancouver BC V6C 1V5

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppb	Hg ppm	Se ppm	Te ppm	Ga ppm	Au+ ppb
4300N 5300E	.5	11.2	6.5	35.3	35	37	12	311	2.40	7.0	<5	6	16	.04	.4	.2	38	.25	.060	14	38	.57	150	.09	<2	1.03	.01	.07	<2	<.2	26	<.3	<.2	3.0	1
4300N 5325E	.5	10.2	6.1	41.1	<30	34	11	310	2.72	6.5	<5	4	19	.03	.2	.1	49	.28	.054	16	44	.44	206	.12	<2	1.39	.01	.05	<2	<.2	15	<.3	<.2	3.9	1
4300N 5350E	.5	9.7	6.6	35.4	<30	28	9	243	2.45	5.6	<5	6	17	.04	.2	.1	41	.27	.061	18	41	.40	185	.10	<2	1.27	.01	.04	<2	<.2	11	<.3	<.2	3.3	2
4300N 5375E	.3	9.5	7.0	38.9	<30	28	9	256	2.42	4.2	<5	4	20	.03	.2	.2	42	.34	.066	16	34	.44	189	.10	<2	1.21	.02	.04	<2	<.2	18	<.3	<.2	3.5	2
4300N 5400E	.4	13.1	6.2	35.4	<30	31	10	293	2.20	5.8	<5	4	21	.03	.3	.1	35	.34	.075	18	30	.50	162	.09	<2	.96	.02	.04	<2	<.2	27	<.3	<.2	2.8	1
4300N 5425E	.4	12.5	6.8	36.1	<30	34	10	301	2.56	6.9	<5	3	23	.03	.3	.1	45	.38	.074	21	40	.53	206	.11	<2	1.30	.02	.04	<2	<.2	27	<.3	<.2	3.9	1
4300N 5450E	.6	10.3	6.7	37.1	<30	31	12	283	2.62	7.4	<5	5	17	.04	.3	.1	43	.27	.068	16	37	.44	164	.10	<2	1.43	.01	.05	<2	<.2	25	<.3	<.2	3.6	1
4300N 5475E	.7	11.3	7.4	45.9	<30	34	13	244	2.88	8.0	<5	5	18	.05	.4	.1	53	.29	.051	15	47	.48	293	.13	<2	1.57	.01	.06	<2	<.2	<10	<.3	<.2	4.3	2
4300N 5500E	.7	10.7	8.1	41.7	<30	36	12	259	2.80	6.6	5	4	17	.06	.3	.2	48	.25	.085	16	39	.53	175	.10	<2	1.46	.01	.06	<2	<.2	15	<.3	<.2	4.1	1
4300N 5525E	.5	8.3	7.3	34.6	96	23	7	244	2.34	5.8	<5	3	21	.04	.3	.2	45	.32	.044	13	35	.39	179	.11	<2	1.28	.02	.05	<2	<.2	15	<.3	<.2	4.0	5
4300N 5550E	.6	9.9	7.0	44.6	<30	31	11	224	2.75	8.1	<5	5	18	.07	.3	.2	51	.26	.075	15	40	.42	248	.11	6	1.58	.01	.06	<2	<.2	10	<.3	<.2	4.2	1
4300N 5575E	.6	17.8	10.2	54.4	109	30	10	281	2.10	9.0	<5	4	19	.21	.7	.2	31	.47	.049	20	26	.40	281	.06	<2	1.01	.01	.06	<2	<.2	66	<.3	<.2	2.8	3
4250N 5300E	.8	12.3	8.2	43.4	<30	40	14	327	3.20	9.3	<5	7	17	.04	.4	.1	60	.23	.069	16	51	.45	200	.16	<2	1.75	.01	.09	<2	<.2	25	<.3	<.2	5.4	2
RE 4250N 5300E	.8	11.3	8.7	43.0	<30	40	14	325	3.22	7.7	5	9	17	.03	.3	.1	59	.22	.069	15	52	.45	201	.16	<2	1.74	.01	.08	<2	<.2	15	<.3	<.2	4.8	1
4250N 5325E	.4	17.1	7.0	35.9	34	33	10	326	2.43	7.5	<5	7	21	.03	.4	.1	37	.34	.076	25	34	.55	156	.08	<2	1.02	.02	.04	<2	<.2	18	<.3	<.2	2.9	1
4250N 5350E	.5	10.1	6.3	36.7	<30	36	10	290	2.30	6.0	5	5	16	.05	.3	.1	37	.26	.073	16	37	.56	124	.08	<2	.99	.01	.05	<2	<.2	16	<.3	<.2	2.6	<1
4250N 5375E	.4	9.6	7.0	33.7	32	29	9	185	2.48	5.5	<5	4	20	.02	.2	.2	42	.31	.075	16	36	.44	168	.11	<2	1.33	.02	.05	<2	<.2	10	<.3	<.2	3.7	7
4250N 5400E	.4	11.6	7.0	37.6	33	34	10	254	2.91	6.7	<5	7	22	.02	.4	.1	53	.36	.083	22	48	.46	199	.13	<2	1.50	.02	.06	<2	<.2	24	<.3	<.2	4.1	1
4250N 5425E	.4	14.4	5.9	42.9	33	45	12	413	2.91	6.8	<5	5	28	.03	.2	.1	49	.47	.086	21	43	.75	225	.13	<2	1.34	.03	.06	<2	<.2	18	<.3	<.2	3.9	3
4250N 5450E	.5	9.6	7.1	38.1	<30	45	12	287	2.44	6.9	<5	6	17	.05	.4	.1	38	.28	.075	15	36	.64	174	.09	<2	1.14	.01	.05	<2	<.2	13	<.3	<.2	2.9	1
4250N 5475E	.6	8.1	7.5	62.5	<30	41	12	245	2.53	5.8	5	5	15	.21	.3	.2	43	.23	.109	13	36	.55	222	.08	<2	1.33	.01	.06	<2	<.2	13	<.3	<.2	3.8	1
4250N 5500E	.4	7.0	7.8	44.1	46	22	7	202	2.30	4.8	<5	5	17	.03	.3	.1	45	.26	.035	15	35	.39	213	.11	<2	1.31	.01	.04	<2	<.2	<10	<.3	<.2	3.9	3
4250N 5525E	.5	11.7	6.9	39.0	<30	36	11	266	2.57	9.4	<5	6	18	.06	.5	.1	40	.27	.078	17	37	.53	155	.09	<2	1.24	.01	.06	<2	<.2	12	<.3	<.2	3.6	6
4250N 5550E	.4	10.9	6.8	39.7	36	28	9	235	2.48	5.8	<5	3	22	.02	.3	.1	44	.34	.076	18	36	.48	175	.11	<2	1.35	.01	.04	<2	<.2	11	<.3	<.2	3.9	2
4250N 5575E	.5	9.7	7.0	41.2	<30	34	11	194	2.61	7.6	<5	4	15	.07	.3	.1	45	.21	.056	12	38	.46	192	.10	<2	1.49	.01	.06	<2	<.2	<10	<.3	<.2	3.8	3
4200N 5300E	.7	9.5	7.1	44.4	<30	30	12	794	2.76	6.2	<5	5	15	.06	.4	.2	51	.24	.104	14	41	.40	279	.11	<2	1.52	.01	.06	<2	<.2	<10	<.3	<.2	4.5	1
4200N 5325E	.5	8.9	7.6	43.2	<30	30	11	262	2.82	6.0	<5	6	16	.03	.3	.1	53	.20	.034	16	44	.45	201	.13	<2	1.64	.01	.05	<2	<.2	15	<.3	<.2	4.5	4
4200N 5350E	.6	10.8	6.8	37.9	<30	31	12	235	2.89	7.5	<5	6	14	.02	.4	.1	54	.16	.031	18	49	.42	185	.13	<2	1.62	.01	.05	<2	<.2	15	<.3	<.2	4.0	2
4200N 5375E	.6	10.4	7.3	35.9	<30	44	13	235	2.44	7.7	<5	5	13	.07	.4	.1	40	.21	.094	13	40	.54	129	.09	<2	1.26	.01	.06	<2	<.2	15	<.3	<.2	3.5	2
4200N 5400E	.6	11.6	7.3	41.2	<30	39	13	412	2.94	8.9	<5	8	15	.04	.4	.1	51	.19	.056	18	47	.48	183	.12	<2	1.54	.01	.05	<2	<.2	<10	<.3	<.2	3.9	2
4200N 5425E	.6	8.9	7.7	49.2	40	27	10	298	2.64	5.5	<5	5	15	.05	.3	.1	51	.18	.038	14	42	.39	220	.12	<2	1.55	.01	.04	<2	<.2	13	<.3	<.2	5.0	2
4200N 5450E	.5	10.0	7.0	40.3	<30	31	15	467	2.74	9.1	<5	6	16	.07	.4	.1	43	.23	.081	17	40	.44	153	.09	<2	1.31	.01	.07	<2	<.2	<10	<.3	<.2	3.4	15
4200N 5475E	.5	10.4	7.1	37.5	<30	33	13	298	2.80	10.0	5	7	18	.07	.4	.2	47	.25	.063	17	45	.46	180	.11	<2	1.33	.01	.07	<2	<.2	13	<.3	<.2	3.5	2
4200N 5500E	.4	7.8	5.9	41.4	72	24	9	188	2.49	4.7	<5	4	15	.06	.2	.1	47	.18	.028	12	40	.38	173	.10	<2	1.35	.01	.05	<2	<.2	<10	<.3	<.2	4.2	1
4200N 5500E (A)	.4	7.9	6.7	42.6	119	24	8	178	2.43	5.3	<5	4	18	.03	.2	.1	48	.25	.030	14	34	.37	225	.11	<2	1.35	.01	.04	<2	<.2	12	<.3	<.2	4.6	2
STANDARD D2/HG-	25.9	129.0	113.6	265.2	1890	33	18	1082	4.41	80.8	22	19	61	2.33	8.1	21.1	81	.76	.106	17	60	1.19	266	.16	26	2.44	.05	.69	21	2.0	463	.6	2.1	6.8	45

Standard is STANDARD D2/HG-500/AU-S.

ICP - 15 GRAM SAMPLE IS DIGESTED WITH 90 ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 100 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K GA AND AL. SOLUTION ANALYSED DIRECTLY BY ICP. MO CU PB ZN AG AS AU CD SB BI TL HG SE TE AND GA ARE EXTRACTED WITH MIBK-ALIQWAT 336 AND ANALYSED BY ICP. ELEVATED DETECTION LIMITS FOR SAMPLES CONTAIN CU,PB,ZN,AS>1500 PPM,Fe>20%.

- SAMPLE TYPE: SOIL AU+ - AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 9 1996

DATE REPORT MAILED:

SIGNED BY:

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
4200N 5525E	.5	15.9	8.0	40.1	<30	34	10	225	2.81	6.4	<5	8	17	.08	<.2	.2	54	.26	.046	23	49	.42	200	.12	2	1.62	.01	.07	<2	<.2	34	<.3	.2	4.7	2
4200N 5575E	.6	15.2	8.4	43.7	<30	30	11	274	2.73	7.1	<5	9	17	.11	<.2	.2	50	.28	.064	17	43	.37	174	.10	2	1.51	.01	.07	<2	<.2	16	<.3	<.2	4.1	8
4150N 5300E	.7	14.1	8.2	40.4	<30	37	11	205	2.90	8.2	<5	7	12	.08	<.2	.3	55	.18	.060	14	48	.39	254	.10	2	1.82	.01	.05	<2	<.2	20	<.3	.3	4.8	12
4150N 5325E	.5	14.4	8.0	36.7	<30	38	10	217	2.64	7.1	<5	8	16	.06	<.2	.2	48	.27	.084	16	45	.47	197	.10	<2	1.43	.01	.07	<2	<.2	11	<.3	.2	3.7	1
4150N 5350E	.7	15.6	8.5	41.2	<30	39	13	216	3.20	8.5	<5	8	16	.05	.3	.2	65	.21	.053	17	61	.42	244	.14	2	1.87	.01	.07	<2	<.2	20	<.3	<.2	5.3	1
4150N 5375E	.5	12.0	7.1	32.2	<30	45	10	242	2.10	4.5	<5	6	12	.07	.2	.2	33	.22	.065	12	39	.56	142	.06	2	.91	.01	.05	<2	<.2	21	<.3	<.2	2.5	<1
4150N 5400E	.6	6.8	8.5	45.3	<30	20	7	143	2.57	4.2	<5	5	10	.11	<.2	.2	52	.15	.062	12	37	.27	113	.10	2	1.49	.01	.05	<2	<.2	26	<.3	.2	5.6	<1
4150N 5425E	.7	12.5	8.9	48.4	<30	34	11	262	2.98	6.5	<5	8	14	.11	.2	.2	57	.20	.086	13	44	.38	180	.10	2	1.77	.01	.06	<2	<.2	16	<.3	<.2	5.1	<1
4150N 5450E	.5	13.0	7.3	41.8	<30	37	14	392	2.84	5.0	<5	7	17	.07	.2	.1	51	.29	.090	14	43	.50	203	.12	<2	1.55	.01	.07	<2	<.2	25	<.3	.2	4.1	<1
4150N 5475E	.3	17.7	5.5	36.0	<30	30	8	184	2.44	5.9	<5	6	20	.03	.2	.2	42	.31	.065	20	38	.40	181	.12	<2	1.32	.02	.05	<2	<.2	25	<.3	.2	4.2	3
4150N 5500E	.7	11.0	7.8	39.9	<30	45	14	309	2.56	5.5	<5	7	14	.18	.3	.2	38	.25	.097	14	41	.59	159	.07	<2	1.20	.01	.06	<2	<.2	20	<.3	<.2	3.0	1
RE 4150N 5500E	.7	11.0	8.2	40.2	<30	48	14	312	2.61	6.0	<5	7	14	.19	.4	.2	39	.25	.098	14	43	.62	162	.07	2	1.24	.01	.06	<2	<.2	18	<.3	<.2	3.2	1
4150N 5525E	.7	11.5	9.3	53.9	<30	35	12	203	3.04	5.1	6	6	15	.10	.4	.2	56	.22	.072	14	46	.46	166	.12	2	1.73	.01	.10	2	<.2	<10	<.3	<.2	4.9	<1
4150N 5550E	.6	8.2	6.7	37.5	<30	28	11	357	2.17	4.7	<5	6	12	.07	.3	.1	34	.20	.074	14	34	.36	116	.08	<2	1.10	.01	.06	<2	<.2	21	<.3	<.2	2.9	<1
4150N 5575E	.7	12.6	7.7	38.9	<30	34	11	204	2.77	6.2	<5	8	15	.04	.3	.1	51	.19	.031	16	48	.40	183	.13	<2	1.53	.01	.08	<2	<.2	18	<.3	<.2	4.1	<1
4150N 5600E	.8	11.1	8.2	40.5	<30	48	10	284	2.59	8.6	<5	7	15	.05	.3	.2	42	.27	.072	16	40	.51	192	.08	2	1.32	.01	.06	<2	<.2	16	<.3	<.2	3.5	1
4150N 5625E	.5	16.0	8.6	39.1	44	37	10	293	2.32	6.2	<5	7	19	.07	.5	.2	35	.37	.070	24	35	.56	144	.07	2	.90	.02	.05	<2	<.2	29	<.3	<.2	2.9	1
4100N 5300E	.6	12.8	8.4	35.9	<30	45	11	243	2.48	6.1	<5	7	14	.04	.3	.1	41	.23	.067	15	44	.55	172	.08	2	1.15	.01	.06	<2	<.2	12	<.3	<.2	2.9	<1
4100N 5325E	.6	14.1	8.5	44.8	39	30	10	196	2.91	7.5	<5	7	17	.08	.3	.2	54	.26	.059	17	46	.37	176	.11	<2	1.62	.01	.07	<2	<.2	37	<.3	<.2	4.9	2
4100N 5350E	.6	15.6	8.2	41.1	<30	33	13	288	2.78	7.1	<5	8	13	.06	.2	.2	49	.18	.066	18	43	.36	191	.09	<2	1.58	.01	.05	<2	<.2	21	<.3	<.2	4.2	2
4100N 5375E	.7	13.7	8.6	39.5	<30	47	12	214	2.76	6.9	<5	7	13	.08	.2	.2	48	.21	.064	15	49	.52	279	.09	2	1.48	.01	.06	<2	<.2	13	<.3	.2	3.8	<1
4100N 5400E	.7	8.2	7.9	33.0	<30	21	11	253	2.28	4.4	<5	5	14	.06	.2	.1	42	.18	.061	12	34	.27	137	.08	<2	1.30	.01	.06	<2	<.2	24	<.3	<.2	3.9	1
4100N 5425E	.4	11.9	7.5	39.7	38	34	9	288	2.45	5.3	<5	6	20	.04	.2	.2	40	.36	.069	18	35	.46	214	.10	<2	1.17	.02	.05	<2	<.2	25	<.3	.2	3.6	1
4100N 5450E	.6	7.9	7.0	49.6	45	23	6	192	2.03	4.3	7	4	13	.07	<.2	.2	34	.21	.076	12	30	.36	158	.09	2	1.20	.01	.06	<2	.2	21	.4	<.2	4.2	1
4100N 5475E	.6	12.3	8.5	42.2	72	36	11	213	2.81	8.4	<5	8	17	.07	.4	.2	53	.27	.103	17	48	.43	188	.12	2	1.53	.01	.13	<2	<.2	20	<.3	.2	4.4	3
4100N 5500E	.8	11.1	7.1	36.8	<30	29	10	217	2.54	6.8	<5	8	13	.07	.2	.2	47	.18	.050	15	42	.36	152	.10	<2	1.42	.01	.06	<2	<.2	32	<.3	.2	3.7	1
4100N 5525E	.5	11.7	7.2	42.6	<30	27	8	171	2.19	3.9	<5	6	13	.09	.3	.2	37	.21	.043	17	37	.34	154	.10	2	1.36	.01	.06	<2	<.2	16	<.3	.2	4.3	8
4100N 5550E	.4	11.9	6.8	37.1	<30	27	8	189	2.24	2.4	<5	5	13	.07	<.2	.2	40	.21	.027	13	39	.38	199	.11	<2	1.36	.01	.04	<2	<.2	22	<.3	.2	3.9	1
4100N 5575E	.5	12.7	7.3	35.8	<30	33	9	250	2.46	6.0	<5	7	16	.06	.2	.2	41	.26	.057	16	41	.44	155	.09	2	1.17	.01	.06	<2	<.2	18	<.3	.2	3.5	2
4100N 5600E	.5	11.3	7.9	35.5	<30	25	8	166	2.52	5.0	<5	8	16	.05	<.2	.2	41	.25	.055	16	38	.35	144	.10	<2	1.37	.01	.06	<2	<.2	16	<.3	.3	3.7	3
4100N 5625E	.6	15.4	8.0	35.1	<30	34	10	195	2.85	6.5	6	8	14	.03	.4	.2	54	.22	.061	14	50	.38	206	.13	<2	1.59	.01	.08	2	<.2	15	<.3	.2	4.5	4
4100N 5650E	.7	11.5	8.2	40.8	44	28	11	242	2.65	6.4	<5	5	16	.05	.5	.2	47	.27	.074	11	38	.37	215	.09	<2	1.49	.01	.05	<2	<.2	19	<.3	.2	4.5	6
4100N 5675E	.7	13.0	7.8	53.5	44	34	10	226	2.97	7.7	10	6	15	.08	.3	.3	52	.29	.067	13	43	.46	246	.11	<2	1.73	.01	.07	<2	<.2	26	<.3	.4	5.5	2
4100N 5700E	.9	9.6	8.8	56.4	<30	26	9	256	2.58	5.8	9	4	12	.08	.5	.2	46	.22	.072	12	33	.37	248	.09	<2	1.47	.01	.07	<2	<.2	17	<.3	<.2	4.5	5
4050N 5300E	.5	13.3	7.5	37.1	<30	45	12	286	2.70	4.8	<5	7	14	.07	<.2	.2	43	.28	.077	17	47	.62	172	.08	<2	1.05	.01	.06	<2	<.2	20	<.3	.3	2.9	2
STANDARD D2/HG	28.8	136.7	114.3	279.4	1908	37	16	1161	4.54	82.5	22	20	54	2.30	8.8	20.5	80	.72	.111	18	54	1.22	273	.14	28	2.56	.05	.77	15	2.6	469	.5	2.5	7.2	49

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Hg ppm	Ba ppm	Ti ppm	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
4050N 5325E	.8	10.2	8.6	43.7	<30	43	12	246	2.95	8.8	<5	7	15	.06	.4	.2	54	.23	.071	14	49	.49	195	.12	4	1.61	.01	.07	<2	<.2	14	<.3	<.2	4.7	1
4050N 5350E	.5	12.0	7.4	38.3	<30	34	10	268	2.66	8.1	<5	7	18	.03	.4	.1	47	.26	.049	22	42	.48	189	.11	3	1.33	.01	.06	<2	<.2	10	<.3	<.2	4.3	2
4050N 5375E	.6	12.2	7.4	42.7	<30	39	11	339	2.55	6.9	<5	6	16	.05	.3	.1	44	.26	.061	15	37	.58	186	.11	2	1.41	.01	.09	<2	<.2	14	<.3	<.2	4.3	2
4050N 5400E	.3	10.9	7.1	36.0	<30	32	9	272	2.27	6.7	<5	6	23	.03	<.2	.1	36	.39	.081	20	31	.53	187	.09	3	1.10	.02	.05	<2	<.2	11	<.3	<.2	3.5	3
4050N 5425E	.5	12.0	7.6	39.3	<30	41	10	292	2.70	7.2	<5	7	20	.04	.2	.2	46	.32	.073	24	44	.58	187	.11	<2	1.30	.02	.05	<2	<.2	15	<.3	<.2	4.0	2
4050N 5450E	.3	12.1	7.9	35.1	<30	29	8	156	2.22	5.9	<5	5	18	.03	<.2	.2	37	.29	.061	20	30	.45	166	.08	2	1.20	.01	.04	<2	<.2	17	<.3	<.2	4.0	<1
4050N 5475E	.2	9.3	7.8	32.6	<30	24	8	157	2.22	4.3	<5	5	20	.02	<.2	.1	33	.32	.068	17	28	.44	211	.07	<2	1.13	.01	.03	<2	<.2	17	<.3	<.2	3.2	3
4050N 5500E	.3	10.1	7.3	37.5	<30	27	6	166	2.30	5.0	<5	5	17	.03	<.2	.1	40	.26	.049	20	35	.41	162	.10	<2	1.19	.01	.05	<2	<.2	14	<.3	<.2	3.6	3
4050N 5525E	.5	11.5	7.9	39.7	<30	37	9	268	2.46	6.8	<5	6	17	.06	.2	.1	41	.27	.059	21	37	.54	189	.10	<2	1.22	.01	.06	<2	<.2	25	<.3	<.2	3.9	4
4050N 5550E	.7	9.5	9.3	72.0	35	32	10	297	2.50	6.4	<5	4	13	.13	.2	.2	42	.22	.077	15	32	.41	218	.09	<2	1.59	.01	.08	<2	<.2	<10	<.3	<.2	4.9	5
4050N 5550E (A)	.3	8.7	7.7	34.2	<30	24	7	199	2.24	5.0	<5	5	22	.03	<.2	.1	37	.36	.073	18	34	.46	162	.11	<2	1.17	.02	.05	<2	<.2	10	<.3	<.2	4.2	2
4050N 5575E	.8	8.5	10.8	92.1	66	28	9	514	2.37	8.1	<5	3	18	.15	.3	.2	37	.37	.068	13	26	.39	467	.06	<2	1.50	.01	.11	<2	<.2	<10	<.3	<.2	4.6	2
4050N 5600E	.5	11.5	8.4	41.5	<30	29	9	196	2.51	6.7	<5	6	19	.03	.2	.2	45	.28	.055	19	36	.45	183	.11	<2	1.48	.01	.07	<2	<.2	33	<.3	<.2	4.7	<1
4050N 5650E	.8	12.6	9.1	50.3	<30	42	12	253	3.03	8.8	<5	7	18	.06	.3	.2	53	.28	.066	14	47	.50	256	.12	<2	1.76	.01	.08	<2	<.2	20	<.3	<.2	5.2	<1
RE 4000N 5325E	.7	12.1	9.2	40.8	<30	49	12	214	3.04	9.8	<5	9	15	.06	.4	.2	55	.19	.051	17	55	.49	216	.12	<2	1.71	.01	.08	<2	<.2	11	<.3	<.2	5.1	4
4050N 5700E	1.0	11.5	11.4	66.4	61	41	10	342	3.49	8.4	<5	6	15	.09	.7	.2	55	.23	.046	15	36	.47	280	.10	<2	1.64	.01	.07	<2	<.2	19	<.3	<.2	5.6	1
4000N 5300E	.7	10.2	8.9	41.4	<30	44	11	187	2.77	8.4	<5	6	13	.07	.3	.2	50	.20	.047	14	49	.49	257	.08	<2	1.51	.01	.05	<2	<.2	11	<.3	<.2	4.4	1
4000N 5325E	.8	12.4	9.7	41.0	<30	50	13	216	3.08	9.8	<5	9	15	.06	.4	.2	56	.19	.052	17	54	.49	219	.12	<2	1.73	.01	.08	<2	<.2	19	<.3	<.2	5.2	1
4000N 5350E	.6	10.5	8.1	38.8	<30	40	11	205	2.70	7.9	<5	8	13	.04	.3	.2	48	.18	.049	19	48	.46	184	.10	<2	1.38	.01	.07	<2	<.2	18	<.3	<.2	3.7	1
4000N 5375E	.6	10.5	8.6	47.1	<30	32	10	217	2.64	5.7	<5	5	16	.04	.2	.1	50	.20	.041	15	43	.44	184	.12	<2	1.54	.01	.07	<2	<.2	21	<.3	<.2	5.5	1
4000N 5400E	.6	10.9	8.1	38.6	<30	42	10	220	2.33	7.4	<5	5	13	.06	.3	.1	40	.22	.068	14	38	.54	149	.08	<2	1.17	.01	.06	<2	<.2	11	<.3	<.2	3.9	<1
4000N 5425E	.6	17.5	6.8	33.8	<30	45	10	323	2.19	7.6	5	6	14	.04	.3	.1	35	.26	.069	15	37	.59	141	.07	<2	.91	.01	.05	<2	<.2	10	<.3	<.2	2.8	2
4000N 5450E	.4	6.1	6.5	26.6	<30	16	4	105	1.67	4.5	<5	3	13	.01	<.2	.1	35	.18	.027	15	24	.27	111	.08	<2	.97	.01	.04	<2	<.2	25	<.3	<.2	3.8	1
4000N 5475E	.4	9.3	8.2	42.2	39	25	8	213	2.36	5.4	<5	4	22	.04	<.2	.1	42	.33	.046	15	34	.42	207	.11	4	1.35	.02	.06	<2	<.2	17	<.3	<.2	4.7	<1
4000N 5500E	.6	8.8	6.5	37.1	<30	33	10	185	2.08	6.7	5	4	13	.05	.2	.1	33	.22	.047	15	31	.52	128	.07	<2	1.10	.01	.05	<2	<.2	17	<.3	<.2	3.5	<1
4000N 5525E	.3	9.7	7.4	38.1	<30	26	7	250	2.17	5.8	<5	5	19	.05	.2	.1	37	.29	.048	16	30	.41	191	.09	<2	1.22	.02	.05	<2	<.2	10	<.3	<.2	4.4	<1
4000N 5550E	.5	11.6	7.3	36.4	<30	30	8	216	2.39	6.6	<5	7	18	.04	.3	.2	41	.26	.057	24	36	.42	166	.10	<2	1.35	.01	.05	<2	<.2	18	<.3	<.2	4.3	1
4000N 5575E	.4	9.7	6.6	45.1	<30	31	9	200	2.35	4.5	<5	6	17	.05	<.2	.1	43	.23	.032	18	37	.45	182	.11	<2	1.34	.01	.07	<2	<.2	18	<.3	<.2	3.7	1
4000N 5600E	.4	16.9	7.1	41.4	<30	29	8	274	2.34	5.7	<5	5	18	.04	.2	.1	42	.25	.051	14	35	.41	168	.10	<2	1.39	.01	.06	<2	<.2	19	<.3	<.2	4.1	1
4000N 5625E	.6	9.6	7.9	71.2	<30	35	13	423	2.70	7.5	<5	6	15	.10	.3	.2	43	.27	.163	16	35	.55	158	.09	<2	1.51	.01	.10	<2	<.2	<10	<.3	<.2	4.5	1
4000N 5650E	.5	8.3	8.6	57.4	78	29	9	419	2.02	5.2	<5	3	16	.09	<.2	.1	33	.26	.057	15	27	.35	338	.07	2	1.38	.01	.11	<2	<.2	18	<.3	<.2	4.3	<1
4000N 5675E	1.2	10.4	13.3	148.0	301	39	11	432	3.47	7.5	<5	4	17	.41	.4	.2	50	.27	.120	15	34	.42	435	.11	3	1.82	.01	.11	<2	<.2	25	<.3	<.2	6.0	1
4000N 5700E	.6	9.9	9.2	78.0	137	46	10	210	2.88	7.3	<5	6	11	.17	.3	.2	45	.21	.127	17	36	.58	151	.08	2	1.42	.01	.06	<2	<.2	18	<.3	<.2	4.6	<1
3950N 5300E	.7	12.2	8.4	48.0	<30	36	12	239	3.03	7.1	<5	6	16	.03	.2	.1	58	.17	.044	17	48	.51	231	.12	2	1.97	.01	.06	<2	<.2	24	<.3	<.2	5.8	<1
3950N 5325E	.9	10.9	8.4	64.2	31	39	13	364	3.19	7.6	<5	5	15	.07	.4	.2	59	.20	.102	14	44	.50	257	.11	3	2.03	.01	.07	<2	<.2	13	<.3	<.2	5.9	3
STANDARD D2/HG-	24.7	122.1	104.4	272.4	1907	34	16	1046	4.18	82.8	24	18	58	2.28	8.2	19.9	74	.71	.104	17	53	1.24	263	.14	28	2.36	.05	.73	15	2.3	541	.6	1.9	6.8	47

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3950N 5350E	.5	20.3	7.3	28.2	<30	27	7	170	2.36	14.4	<5	7	14	.02	.4	.1	35	.26	.068	28	32	.42	147	.07	<2	1.08	.01	.02	<2	<.2	32	<.3	<.2	3.6	1
3950N 5375E	.7	10.3	7.1	36.9	<30	23	7	151	2.56	8.7	<5	5	10	.04	.3	.1	46	.15	.028	13	39	.40	176	.10	<2	1.35	.01	.03	<2	<.2	23	<.3	<.2	4.8	45
3950N 5400E	.4	5.5	5.2	23.3	<30	27	8	172	1.73	4.6	<5	3	9	.03	.2	<.1	26	.19	.036	10	28	.46	143	.06	<2	.76	.01	.02	<2	<.2	11	<.3	<.2	2.7	2
3950N 5425E	1.1	12.5	8.7	44.4	<30	36	13	231	3.24	12.4	10	6	10	.06	.5	.2	53	.15	.078	14	46	.48	222	.10	2	1.80	.01	.05	<2	<.2	18	<.3	<.2	4.9	4
3950N 5450E	.2	8.4	5.7	28.9	33	31	7	237	1.67	4.2	<5	4	14	.04	.3	<.1	23	.39	.059	12	24	.58	157	.05	<2	.64	.02	.02	<2	<.2	12	<.3	<.2	2.3	1
3950N 5475E	.3	12.3	6.3	30.8	56	26	7	275	2.02	6.2	<5	5	22	.05	.3	.1	28	.44	.081	17	26	.44	205	.06	<2	.86	.02	.02	<2	<.2	27	<.3	<.2	3.2	3
3950N 5500E	.5	8.7	5.4	32.0	<30	26	8	171	2.12	5.6	5	5	15	.04	.3	.1	33	.25	.044	15	31	.40	181	.07	2	1.07	.01	.03	<2	<.2	17	<.3	<.2	3.1	6
3950N 5525E	.2	8.1	5.3	29.7	42	23	5	171	1.71	4.4	<5	5	18	.05	.3	.1	25	.38	.072	15	25	.46	160	.06	2	.72	.02	.02	<2	<.2	18	<.3	<.2	2.0	1
3950N 5550E	.6	11.2	6.9	37.5	<30	25	8	145	2.48	6.8	<5	5	13	.05	.4	.1	42	.17	.022	12	37	.40	148	.10	<2	1.27	.01	.07	<2	<.2	<10	<.3	<.2	4.2	2
RE 3950N 5550E	.6	10.5	6.7	36.7	<30	25	8	136	2.40	6.6	<5	5	13	.05	.4	.1	41	.17	.021	12	37	.39	143	.10	<2	1.25	.01	.06	<2	<.2	14	<.3	<.2	4.0	2
3950N 5575E	.6	10.9	6.9	39.7	<30	31	9	236	2.54	7.7	<5	6	15	.05	.4	.1	41	.23	.052	12	37	.51	166	.10	<2	1.39	.01	.05	<2	<.2	16	<.3	<.2	4.4	1
3950N 5600E	.5	18.2	7.8	48.6	76	30	8	270	2.48	6.6	9	6	21	.06	.4	.2	42	.38	.055	18	35	.55	239	.08	2	1.34	.01	.07	<2	<.2	40	<.3	<.2	4.0	2
3950N 5625E	.6	6.2	5.9	36.8	<30	23	5	131	2.16	5.4	<5	5	12	.05	.2	.1	33	.21	.055	13	28	.37	196	.08	2	1.14	.01	.09	<2	<.2	17	<.3	<.2	3.6	2
3950N 5650E	.7	12.8	10.8	144.7	229	37	10	369	3.02	7.2	<5	6	19	.39	.4	.1	47	.39	.226	16	36	.57	325	.10	2	1.68	.01	.11	<2	<.2	26	<.3	<.2	5.5	11
3950N 5675E	.7	7.9	9.0	102.2	89	24	9	192	3.19	6.5	<5	4	12	.35	.4	.2	51	.22	.177	15	33	.44	284	.07	2	1.42	.01	.06	<2	<.2	30	<.3	<.2	5.1	2
3950N 5700E	.9	9.8	8.8	53.5	48	53	12	224	3.25	10.6	7	7	11	.19	.6	.2	45	.23	.088	19	37	.85	125	.08	<2	1.35	.01	.03	<2	<.2	<10	<.3	<.2	3.9	2
3900N 5300E	.7	14.7	8.4	45.2	<30	37	11	237	3.05	10.8	<5	8	13	.07	.5	.2	53	.18	.055	15	49	.53	208	.11	<2	1.69	.01	.06	<2	<.2	18	<.3	<.2	5.0	1
3900N 5325E	.7	9.1	6.9	38.1	<30	28	9	163	2.58	8.5	6	5	10	.07	.4	.1	41	.16	.041	13	37	.41	151	.08	<2	1.30	.01	.04	<2	<.2	14	<.3	<.2	3.6	1
3900N 5350E	.4	7.9	5.3	31.1	<30	36	9	325	1.97	4.0	<5	4	15	.04	.2	.1	27	.30	.051	14	31	.71	166	.06	<2	.70	.02	.03	<2	<.2	23	<.3	<.2	2.1	2
3900N 5375E	.6	8.8	6.2	33.5	30	27	8	225	2.32	6.4	<5	6	16	.05	.3	.1	38	.29	.064	15	37	.43	163	.09	<2	1.17	.01	.03	<2	<.2	21	<.3	<.2	3.9	4
3900N 5400E	.4	7.1	5.3	31.0	<30	28	10	179	1.96	4.5	5	5	12	.05	.3	<.1	31	.19	.038	13	32	.48	125	.07	<2	.87	.01	.03	<2	<.2	22	<.3	<.2	2.5	2
3900N 5425E	.8	10.4	7.2	39.5	<30	37	10	195	2.49	8.7	5	5	10	.06	.4	.1	40	.16	.048	13	36	.50	175	.07	<2	1.40	.01	.05	<2	<.2	26	<.3	<.2	4.4	2
3900N 5450E	.5	12.7	6.6	38.3	<30	30	9	174	2.62	8.0	<5	8	13	.04	.4	.1	42	.19	.050	19	39	.45	158	.09	<2	1.34	.01	.06	<2	<.2	10	<.3	<.2	3.6	2
3900N 5475E	.7	9.3	7.2	47.3	<30	33	10	197	2.70	6.8	6	5	13	.06	.4	.1	47	.20	.056	13	37	.50	202	.09	<2	1.60	.01	.05	<2	<.2	31	<.3	<.2	4.5	1
3900N 5500E	.3	7.7	5.5	33.6	41	29	6	158	1.70	5.0	<5	5	15	.05	.3	.1	23	.32	.064	15	26	.56	126	.05	<2	.66	.01	.03	<2	<.2	13	<.3	<.2	2.3	2
3900N 5525E	.2	7.8	5.5	27.6	67	21	5	123	1.45	4.2	<5	3	20	.03	.2	.1	23	.51	.065	15	21	.34	298	.04	<2	.73	.02	.02	<2	<.2	27	.3	<.2	2.4	3
3900N 5550E	.4	5.1	6.3	29.3	49	12	5	167	2.30	7.2	<5	6	20	.01	<.2	.1	27	.44	.081	18	23	.36	152	.06	<2	.83	.02	.04	<2	<.2	44	<.3	<.2	3.4	1
3900N 5575E	.6	6.9	6.6	38.5	<30	22	6	147	2.25	4.3	<5	5	12	.05	.2	.1	40	.20	.025	13	31	.39	158	.09	<2	1.29	.01	.03	<2	<.2	18	<.3	<.2	4.4	2
3900N 5600E	.4	8.6	5.9	34.9	<30	27	7	201	2.05	6.6	<5	5	16	.03	.3	.1	28	.31	.075	17	25	.52	119	.07	<2	.92	.02	.06	<2	<.2	11	<.3	<.2	3.0	1
3850N 5300E	.6	14.3	6.6	45.4	55	42	13	318	3.23	7.6	7	7	19	.04	.4	.1	59	.30	.071	17	53	.61	254	.13	<2	1.80	.02	.06	<2	<.2	28	<.3	<.2	5.2	<1
3850N 5325E	.7	11.1	6.9	67.3	42	32	12	220	3.10	6.5	9	5	17	.08	.3	.2	58	.22	.033	14	48	.48	312	.11	<2	1.90	.01	.06	<2	<.2	35	<.3	<.2	5.7	1
3850N 5350E	.4	13.4	5.8	34.1	<30	40	9	263	2.30	5.1	<5	6	13	.05	.4	.1	34	.24	.062	19	37	.63	148	.07	<2	.94	.01	.03	<2	<.2	29	<.3	<.2	3.1	1
3850N 5375E	.3	7.5	4.9	30.3	<30	26	8	293	1.83	4.8	<5	4	16	.05	.2	<.1	26	.28	.057	15	25	.53	165	.06	<2	.77	.02	.03	<2	<.2	<10	<.3	<.2	2.7	<1
3850N 5400E	.2	12.4	5.4	32.3	<30	30	8	243	1.90	5.2	<5	5	16	.05	.2	.1	27	.30	.062	15	27	.54	173	.06	<2	.84	.02	.03	<2	<.2	10	<.3	<.2	3.0	1
3850N 5425E	.5	9.1	6.7	36.3	<30	29	10	223	2.49	5.7	<5	5	13	.03	.4	.1	41	.20	.072	15	39	.44	166	.08	<2	1.34	.01	.03	<2	<.2	<10	<.3	<.2	3.6	<1
STANDARD D2/HG	27.4	132.1	110.9	284.0	1957	34	16	1129	4.57	82.5	18	19	49	2.34	8.6	20.7	82	.80	.107	16	52	1.24	244	.18	26	2.25	.06	.77	15	2.5	479	.5	2.1	7.0	48

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3850N 5450E	.5	8.1	6.7	37.3	<30	40	11	184	2.37	5.8	<5	5	12	.08	.3	.1	38	.21	.069	11	38	.51	143	.07	3	1.01	.01	.05	<2	<2	33	<.3	<.2	3.4	<1
3850N 5475E	.2	12.1	5.6	38.1	31	31	9	403	2.29	4.4	<5	4	24	.04	<.2	.1	33	.47	.090	17	30	.47	229	.08	4	.93	.02	.04	<2	<2	15	<.3	<.2	2.6	2
3850N 5500E	.2	6.6	4.8	29.0	40	24	8	253	1.99	5.5	<5	4	22	.02	<.2	.1	28	.41	.083	16	26	.40	150	.07	4	.76	.02	.04	<2	<2	29	<.3	<.2	2.2	1
3850N 5525E	.4	7.4	6.7	38.9	<30	22	7	162	2.38	4.6	<5	5	18	.03	<.2	.1	45	.33	.027	15	34	.40	227	.09	3	1.37	.01	.04	<2	<2	18	<.3	<.2	3.6	1
3850N 5550E	.4	7.6	6.0	35.3	<30	27	9	169	2.52	5.4	<5	5	15	.03	.2	.1	42	.23	.039	12	36	.38	148	.09	3	1.38	.01	.03	<2	<2	12	<.3	<.2	3.3	1
3850N 5575E	.3	11.4	5.5	29.9	<30	32	8	175	2.26	6.7	<5	5	19	.02	.5	.1	31	.33	.075	20	28	.46	136	.08	3	1.02	.01	.05	<2	<2	16	<.3	<.2	2.7	1
3850N 5600E	.4	6.9	5.8	43.5	<30	29	10	257	2.64	6.0	<5	5	17	.06	.2	.1	40	.29	.063	16	33	.46	130	.09	3	1.15	.01	.06	<2	<2	16	<.3	<.2	2.6	<1
3850N 5625E	.5	6.3	6.5	45.0	<30	23	9	226	2.61	5.0	<5	4	15	.07	.2	.1	45	.25	.056	12	34	.34	180	.09	3	1.26	.01	.08	<2	<2	<10	<.3	<.2	3.4	1
3850N 5650E	.7	7.4	10.0	51.9	103	26	10	405	2.56	6.2	<5	3	19	.13	.2	.2	42	.40	.057	12	30	.35	513	.07	4	1.76	.01	.12	<2	<2	24	<.3	<.2	4.5	2
3850N 5675E	.7	10.8	11.1	79.1	213	39	12	327	3.20	8.6	<5	4	17	.31	.3	.2	51	.28	.201	15	36	.49	403	.08	4	1.84	.01	.10	<2	<2	28	<.3	<.2	5.5	<1
3850N 5700E	1.4	12.6	15.2	102.1	736	46	12	584	4.26	10.9	<5	4	18	.48	.4	.2	66	.27	.186	14	40	.46	353	.13	4	2.28	.01	.08	<2	<2	27	.3	<.2	7.0	2
3800N 5300E	.6	10.3	7.3	39.6	<30	31	10	172	2.95	9.5	<5	7	12	.03	.3	.2	46	.15	.042	15	46	.44	178	.09	2	1.48	.01	.06	<2	<2	<10	<.3	<.2	3.6	1
3800N 5325E	.6	10.3	5.8	42.0	<30	43	13	232	3.08	7.7	<5	6	15	.04	.3	.1	55	.20	.050	12	49	.53	247	.12	3	1.72	.01	.05	<2	<2	<10	<.3	<.2	4.2	1
3800N 5350E	.5	10.6	6.3	41.8	<30	37	12	228	3.05	8.0	<5	7	16	.04	.3	.1	54	.20	.056	18	48	.49	187	.12	3	1.59	.01	.06	<2	<2	17	<.3	<.2	3.9	1
3800N 5375E	.5	10.7	7.1	41.6	<30	44	14	302	3.27	7.9	<5	8	19	.04	.4	.2	57	.27	.065	20	52	.59	199	.13	2	1.57	.01	.04	<2	<2	14	<.3	<.2	4.1	3
3800N 5400E	.6	11.4	7.3	38.4	<30	45	12	180	2.91	9.8	<5	8	13	.06	.3	.2	47	.16	.055	14	49	.50	194	.09	5	1.50	.02	.06	<2	<2	15	<.3	<.2	3.7	<1
3800N 5425E	.6	11.1	6.8	42.4	<30	32	11	188	2.98	7.9	<5	7	15	.04	.3	.1	52	.17	.029	19	47	.44	176	.12	3	1.56	.01	.05	<2	<2	12	<.3	<.2	4.0	1
3800N 5450E	.3	10.2	6.7	38.9	46	32	10	249	2.79	7.0	<5	5	24	.03	<.2	.1	45	.50	.095	19	39	.50	240	.10	4	1.16	.02	.05	<2	<2	20	<.3	<.2	3.3	1
3800N 5475E	.2	10.7	5.8	33.4	37	29	9	223	2.41	6.6	<5	4	22	.02	<.2	.1	38	.38	.069	18	33	.43	183	.09	3	1.13	.02	.04	<2	<2	15	<.3	<.2	3.4	2
3800N 5500E	.6	9.8	6.4	35.9	<30	35	11	217	2.83	7.7	<5	8	13	.05	.3	.1	45	.19	.057	14	43	.43	162	.10	4	1.48	.01	.04	<2	<2	16	<.3	<.2	3.3	3
3800N 5525E	.2	16.2	6.2	37.5	82	34	10	313	2.63	8.2	<5	4	28	.05	.2	.2	40	.56	.094	20	31	.47	243	.09	2	1.14	.02	.03	<2	<2	<10	<.3	<.2	3.5	1
RE 3800N 5525E	.1	16.8	6.1	38.3	78	35	10	316	2.66	8.4	<5	4	29	.04	<.2	.1	40	.58	.097	21	33	.48	246	.09	2	1.17	.03	.03	<2	<2	19	<.3	<.2	3.3	2
3800N 5550E	.4	12.8	7.9	35.7	<30	32	8	161	2.37	7.3	<5	6	14	.03	.2	.1	38	.23	.039	15	32	.42	193	.06	4	1.34	.01	.04	<2	<2	<10	<.3	<.2	3.2	1
3800N 5575E	.5	8.4	6.5	44.6	<30	28	10	209	2.83	6.6	<5	6	14	.03	.3	.1	49	.19	.034	16	42	.45	150	.10	2	1.48	.01	.05	<2	<2	17	<.3	<.2	4.0	1
3800N 5600E	.5	7.4	6.1	42.3	40	33	9	215	2.53	6.4	<5	3	15	.07	.2	.1	38	.25	.131	13	31	.45	255	.07	3	1.30	.01	.07	<2	<2	<10	<.3	<.2	3.1	1
3800N 5625E	.6	8.3	6.2	40.5	<30	26	8	157	2.80	7.4	<5	5	12	.03	.2	.1	49	.17	.042	13	39	.37	144	.10	2	1.34	.01	.07	<2	<2	<10	<.3	<.2	3.8	1
3800N 5650E	.5	7.4	8.8	53.5	100	22	9	467	2.54	3.9	<5	2	23	.21	.2	.2	35	.49	.093	12	29	.33	482	.07	4	1.63	.01	.13	<2	<2	16	<.3	<.2	4.6	<1
3800N 5675E	.9	10.6	11.3	136.1	188	33	11	542	3.38	5.2	<5	2	23	.51	.3	.1	56	.38	.184	13	36	.45	548	.11	3	1.69	.01	.08	<2	<2	27	<.3	<.2	6.7	1
3800N 5700E	.9	6.8	12.2	83.8	139	19	10	508	3.14	5.3	<5	3	13	.42	.3	.1	56	.27	.094	13	30	.30	235	.09	3	1.35	.01	.05	<2	<2	14	<.3	<.2	5.9	173
3800N 5725E	.3	8.9	1.1	14.9	61	5	1	81	.25	.7	<5	2	302	.65	.2	<.1	3	35.04	<.002	1	22	.29	371	<.01	6	.10	.01	.01	<2	<2	33	5.6	<.2	<.5	2
3800N 5750E	2.4	4.1	.7	20.1	<30	5	1	120	.10	<.5	12	2	296	.22	.7	<.1	5	27.91	<.002	<.1	3	.31	421	<.01	13	.04	.01	<.01	<2	<2	29	14.8	<.2	<.5	2
3750N 5300E	.5	10.4	6.2	43.7	<30	36	11	357	2.78	7.0	<5	5	15	.05	.2	.1	49	.26	.104	12	42	.45	167	.10	2	1.51	.01	.06	<2	<2	<10	.4	<.2	4.6	1
3750N 5325E	.6	11.3	6.5	38.5	<30	34	12	219	2.94	8.3	<5	7	14	.04	.4	.1	51	.21	.059	19	49	.42	204	.11	2	1.40	.01	.06	<2	<2	17	<.3	<.2	4.1	1
3750N 5350E	.5	9.8	6.4	42.9	<30	34	11	204	2.90	7.4	<5	5	14	.04	.2	.1	52	.20	.081	12	44	.39	198	.10	<2	1.66	.01	.04	<2	<2	11	<.3	<.2	4.7	5
3750N 5375E	.7	7.8	8.2	86.6	133	31	12	526	3.11	5.5	<5	3	11	.18	.2	.1	56	.19	.154	11	36	.36	207	.10	2	1.83	.01	.06	<2	<2	21	<.3	<.2	6.0	1
STANDARD D2/HG-500/AU-S	26.7	134.0	111.1	276.5	1921	34	17	1080	4.56	89.5	26	21	57	2.35	8.5	20.3	82	.77	.114	18	59	1.21	263	.16	23	2.46	.05	.74	18	2.4	525	.4	2.1	7.1	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3750N 5400E	.4	8.7	6.1	37.5	<30	39	11	276	2.30	4.8	<5	5	13	.07	.3	.1	34	.28	.163	15	32	.68	89	.06	<2	.91	.01	.05	<2	<2	26	<.3	<.2	3.1	<1
3750N 5425E	.4	9.5	6.1	36.5	<30	28	8	183	2.55	4.5	<5	5	15	.01	.2	.2	47	.21	.036	16	38	.46	166	.11	2	1.46	.02	.03	<2	<2	15	<.3	<.2	5.1	1
3750N 5450E	.3	15.2	6.9	32.9	<30	28	10	263	2.41	6.1	<5	7	17	.02	.3	.1	38	.29	.070	25	36	.47	179	.09	<2	1.15	.02	.04	<2	<2	23	<.3	<.2	4.1	1
3750N 5475E	.2	7.2	6.0	26.9	34	24	6	197	1.85	4.1	<5	6	17	.03	.2	.1	28	.33	.057	16	28	.46	168	.07	<2	.85	.02	.02	<2	<2	26	<.3	<.2	3.5	2
3750N 5500E	.3	9.1	5.6	30.3	<30	27	7	168	2.02	4.9	<5	5	15	.02	<.2	.1	32	.26	.054	16	31	.45	146	.08	<2	1.00	.01	.03	<2	<2	<10	<.3	<.2	3.6	2
3750N 5525E	.5	8.3	6.3	33.2	<30	24	7	165	2.24	4.9	<5	4	12	.02	.2	.1	41	.18	.029	15	36	.39	170	.10	<2	1.23	.01	.03	<2	<2	12	<.3	<.2	4.4	1
3750N 5550E	.3	14.0	6.2	33.0	<30	29	6	199	2.37	5.6	<5	5	20	.01	.3	.1	41	.33	.056	18	36	.50	203	.11	<2	1.17	.02	.03	<2	<2	27	<.3	<.2	4.5	<1
3750N 5575E	.5	8.9	6.0	30.1	<30	19	6	178	1.93	3.8	<5	3	12	.04	<.2	<.1	36	.20	.022	11	29	.34	195	.08	2	1.17	.01	.05	<2	<2	<10	<.3	<.2	4.0	4
3750N 5600E	.7	11.1	8.8	49.1	<30	52	11	239	3.16	9.3	<5	7	16	.04	.4	.2	53	.30	.132	18	40	.67	172	.09	<2	1.70	.01	.07	<2	<2	14	<.3	<.2	5.0	<1
3750N 5625E	.6	10.0	7.3	40.4	<30	33	10	244	2.74	8.0	<5	6	16	.06	.4	.1	46	.30	.069	14	40	.51	191	.10	<2	1.38	.02	.07	<2	<2	16	<.3	<.2	4.8	<1
3750N 5650E	.4	9.1	6.4	32.7	<30	28	8	154	2.42	5.7	<5	6	16	.07	.2	.1	39	.30	.044	14	33	.40	178	.08	<2	1.09	.01	.06	<2	<2	17	<.3	<.2	3.8	3
3750N 5675E	.8	6.7	9.5	108.3	48	30	8	209	3.15	4.6	<5	4	15	.25	<.2	.2	60	.26	.059	11	38	.41	339	.12	2	1.94	.01	.06	<2	<2	13	<.3	<.2	6.8	1
3750N 5700E	.9	7.3	15.1	503.9	228	20	14	3230	2.95	1.3	<5	3	18	1.97	.2	.2	51	.33	.108	13	34	.24	723	.12	3	1.66	.01	.06	<2	<2	15	<.3	<.2	8.2	13
RE 3750N 5700E	.9	7.9	16.6	503.0	239	22	14	3303	2.98	1.1	<5	3	18	2.10	.2	.2	51	.33	.109	14	32	.24	733	.12	2	1.65	.01	.07	<2	<2	20	<.3	<.2	8.7	<1
3750N 5775E	.5	1.9	.7	30.1	<30	5	2	214	.14	.9	<5	<1	333	.16	.2	<.1	1	30.11	.006	<1	3	.33	202	<.01	6	.04	.01	<.01	<2	<2	<10	5.5	<.2	.5	<1
3700N 5300E	.5	10.1	6.9	53.8	<30	41	10	235	2.71	5.7	<5	6	13	.08	.3	.1	48	.35	.077	15	45	.61	224	.09	<2	1.43	.01	.05	<2	<2	12	.5	<.2	4.6	<1
3700N 5325E	.6	11.3	7.2	44.1	<30	39	10	279	2.52	6.9	<5	6	13	.07	.3	.2	40	.26	.101	16	38	.61	176	.08	<2	1.32	.01	.05	<2	<2	<10	.4	<.2	4.3	2
3700N 5350E	.7	12.3	9.2	58.5	36	44	12	329	2.90	7.3	14	6	12	.11	.4	.1	53	.19	.090	15	47	.55	205	.10	<2	1.85	.01	.06	<2	<2	16	<.3	<.2	6.2	<1
3700N 5375E	.6	12.4	6.9	40.7	<30	39	11	220	2.72	7.7	12	7	12	.06	.4	.1	46	.19	.098	15	43	.54	194	.09	<2	1.55	.01	.07	<2	<2	19	<.3	<.2	4.6	2
3700N 5400E	.6	10.6	6.9	43.8	<30	34	10	252	2.72	7.3	<5	6	15	.03	.2	.1	49	.21	.059	14	42	.51	199	.11	<2	1.59	.01	.06	<2	<2	23	<.3	<.2	5.1	2
3700N 5425E	.7	9.4	7.3	40.2	<30	36	9	224	2.82	7.0	5	5	11	.05	.3	.2	50	.19	.058	13	45	.48	184	.10	<2	1.54	.01	.06	<2	<2	21	<.3	<.2	5.0	3
3700N 5450E	.6	8.2	6.0	34.9	<30	39	8	240	2.27	6.7	<5	6	12	.05	.3	.2	38	.22	.056	11	36	.51	164	.08	<2	1.11	.01	.05	<2	<2	16	<.3	<.2	3.7	1
3700N 5475E	.7	24.0	8.9	64.1	167	33	9	393	2.01	6.4	9	6	117	.47	1.2	.1	40	5.15	.053	15	31	1.26	296	.07	2	1.00	.02	.08	<2	<2	97	<.3	<.2	3.5	2
3700N 5500E	.7	11.4	7.2	48.9	<30	41	14	280	2.85	7.1	11	6	17	.07	.3	.1	43	.31	.083	16	37	.69	150	.11	<2	1.63	.02	.07	<2	<2	<10	<.3	<.2	5.1	9
3700N 5525E	.3	6.9	5.8	29.1	48	16	4	101	1.81	4.5	<5	3	17	.03	.2	.1	30	.32	.080	17	26	.37	113	.06	<2	1.04	.01	.03	<2	<2	27	<.3	<.2	3.8	2
3700N 5550E	.1	4.4	6.6	23.1	39	13	3	96	2.00	4.9	<5	5	20	<.01	<.2	.1	32	.35	.080	19	24	.37	133	.09	<2	1.10	.02	.04	<2	<2	20	<.3	<.2	4.3	108
3700N 5575E	.4	5.7	6.2	24.0	<30	14	3	83	1.49	2.9	<5	7	13	.01	<.2	.1	27	.23	.052	17	21	.29	104	.07	<2	.86	.01	.03	<2	<2	10	<.3	<.2	3.3	2
3700N 5600E	.6	5.9	7.1	58.4	58	19	7	157	2.55	4.0	8	4	12	.10	.3	.1	50	.18	.051	13	33	.38	128	.10	<2	1.45	.01	.06	<2	<2	11	<.3	<.2	5.9	2
3700N 5625E	.7	10.9	7.9	57.6	44	38	10	265	3.13	7.8	<5	6	17	.10	.4	.1	53	.30	.088	16	41	.57	265	.11	<2	1.71	.01	.08	<2	<2	15	<.3	<.2	5.2	3
3700N 5650E	.5	8.0	6.1	31.0	<30	26	8	180	2.44	5.3	9	6	12	.04	.3	.1	38	.21	.047	11	32	.40	133	.08	<2	1.07	.01	.07	<2	<2	13	<.3	<.2	3.8	17
3700N 5675E	.7	5.6	7.9	63.2	69	22	7	373	2.43	4.0	<5	3	13	.18	.3	.1	43	.25	.060	12	27	.34	348	.08	<2	1.42	.01	.06	<2	<2	13	<.3	<.2	5.4	1
3700N 5700E	1.1	19.6	12.7	129.4	296	38	10	852	3.53	8.6	<5	5	24	.57	1.0	.3	57	.37	.182	15	39	.55	625	.10	2	1.82	.02	.07	<2	<2	23	.3	<.2	7.2	134
3700N 5725E	1.5	8.9	6.9	28.8	133	17	5	203	1.27	3.2	<5	2	108	.53	.3	.1	19	3.46	.034	4	17	.33	223	.03	7	.91	.03	.08	<2	<2	51	7.4	<.2	3.0	2
3700N 5750E	1.4	5.0	1.7	24.8	51	28	1	25	.13	1.1	16	1	204	.18	1.5	<.1	7	7.43	.022	<1	1	.36	466	<.01	5	.08	.01	<.01	<2	<2	21	17.2	<.2	<.5	2
3700N 5775E	.2	8.3	.4	63.2	37	5	1	50	.11	<.5	<5	2	374	.34	.3	<.1	1	34.73	<.002	<1	6	.39	290	<.01	5	.05	.01	.01	3	<.2	18	5.5	<.2	<.5	5
STANDARD D2/HG-500/AU-S	27.9	133.9	104.9	284.6	2024	34	16	1135	4.45	81.5	15	21	61	2.45	9.2	21.6	82	.78	.112	19	60	1.40	236	.16	26	2.20	.05	.70	17	2.4	532	.4	2.3	7.2	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3650N 5300E	.5	10.1	6.7	40.0	<30	50	11	229	2.45	7.3	<5	5	12	.08	.2	.1	41	.30	.072	13	43	.66	192	.08	2	1.18	.01	.04	<2	<2	21	<.3	<.2	3.2	<1
3650N 5325E	.5	10.4	5.9	40.9	<30	37	11	228	2.73	6.0	<5	5	14	.04	<.2	.1	52	.17	.055	15	46	.38	250	.11	2	1.56	.01	.04	<2	<2	20	<.3	<.2	4.2	1
3650N 5350E	.6	11.8	6.9	48.5	<30	37	11	231	3.05	6.9	<5	5	12	.07	<.2	.1	56	.14	.078	13	49	.48	219	.11	2	1.81	.01	.05	<2	<2	37	<.3	<.2	4.8	1
3650N 5375E	.6	9.4	8.0	47.1	<30	38	10	216	3.10	5.0	<5	5	15	.05	.2	.1	57	.18	.071	12	47	.44	234	.10	2	1.81	.01	.05	<2	<2	22	<.3	<.2	5.4	<1
3650N 5400E	.6	11.3	7.6	42.0	<30	45	11	206	3.08	7.4	<5	6	15	.04	.3	.1	54	.20	.046	11	49	.48	228	.11	<2	1.77	.01	.06	<2	<2	<10	<.3	<.2	4.3	<1
3650N 5425E	.7	9.0	7.2	45.8	<30	44	11	213	2.81	7.8	<5	5	14	.06	.4	.1	47	.23	.051	13	46	.55	212	.09	2	1.52	.01	.06	<2	<2	16	.3	<.2	3.8	<1
3650N 5450E	.6	10.1	6.9	50.7	<30	52	11	278	2.73	6.3	<5	5	15	.08	<.2	.1	46	.27	.104	13	40	.64	204	.09	<2	1.51	.01	.06	<2	<2	11	<.3	<.2	4.2	6
3650N 5475E	.6	9.8	7.3	52.4	33	37	9	211	3.02	5.0	<5	5	13	.06	.2	.1	56	.18	.031	13	49	.46	233	.12	<2	1.75	.01	.06	<2	<2	30	<.3	<.2	4.9	3
3650N 5500E	.5	7.9	6.5	42.6	33	56	10	240	2.54	5.4	<5	3	11	.06	.2	.1	44	.20	.055	10	46	.67	172	.08	<2	1.34	.01	.05	<2	<2	14	<.3	<.2	3.5	4
3650N 5525E	.6	7.2	7.5	50.7	<30	41	9	294	2.54	5.0	<5	3	13	.11	.2	.1	43	.26	.078	10	38	.56	234	.07	2	1.20	.01	.06	<2	<2	18	<.3	<.2	4.0	1
RE 3650N 5525E	.5	6.2	6.9	50.4	<30	40	9	281	2.42	4.7	<5	3	13	.10	.2	<.1	42	.26	.072	11	37	.55	220	.08	3	1.19	.01	.06	<2	<2	17	<.3	<.2	3.7	2
3650N 5550E	.8	6.7	7.5	106.6	98	35	10	454	2.55	3.9	<5	2	15	.35	<.2	.1	48	.30	.103	10	37	.40	267	.09	3	1.38	.01	.07	<2	<2	21	<.3	<.2	4.4	<1
3650N 5575E	.6	7.2	6.9	48.5	51	63	11	380	2.50	6.3	<5	2	16	.16	.2	.1	41	.33	.102	11	43	.78	173	.07	2	1.06	.01	.05	<2	<2	19	<.3	<.2	2.9	<1
3650N 5600E	.6	7.7	6.8	40.3	32	45	9	189	2.74	7.1	<5	5	13	.08	.3	<.1	46	.23	.058	11	49	.53	142	.09	<2	1.30	.01	.09	<2	<2	<10	<.3	<.2	3.6	<1
3650N 5625E	.5	7.3	6.8	55.4	<30	42	10	247	2.76	7.0	<5	4	13	.12	.2	.1	45	.23	.126	13	33	.59	179	.08	<2	1.17	.01	.06	<2	<2	10	<.3	<.2	3.4	66
3650N 5650E	.3	10.4	5.9	34.7	<30	42	10	224	2.51	6.6	<5	6	14	.05	.3	.1	39	.22	.049	14	32	.60	127	.08	<2	.90	.01	.06	<2	<2	<10	<.3	<.2	2.7	2
3650N 5675E	.4	7.6	6.4	32.4	<30	35	10	177	2.78	6.5	<5	5	13	.04	.2	.1	42	.23	.045	13	33	.46	175	.08	<2	1.13	.01	.06	<2	<2	18	<.3	<.2	3.0	1
3650N 5700E	.6	7.5	9.2	81.8	45	35	10	475	2.80	5.4	<5	4	14	.30	<.2	.2	47	.25	.144	13	32	.51	226	.09	2	1.26	.01	.05	<2	<2	16	<.3	<.2	4.3	45
3650N 5725E	.7	15.7	10.3	68.6	158	41	12	376	2.39	4.6	<5	2	21	.46	.4	.2	38	.34	.065	11	36	.48	294	.07	2	1.32	.01	.09	<2	<2	18	<.3	<.2	3.8	1
3650N 5750E	3.7	5.8	1.5	26.3	<30	3	1	68	.19	2.1	18	<1	100	.10	.3	<.1	7	3.24	.032	<1	2	.27	257	<.01	13	.08	.02	.03	<2	<2	65	5.3	<.2	<.5	6
3650N 5775E	4.9	4.9	1.3	35.7	<30	14	1	52	.38	.6	17	<1	154	.39	.6	<.1	13	5.50	.064	<1	4	.35	435	.01	5	.10	.01	.01	<2	<2	45	13.6	<.2	<.5	6
3650N 5800E	1.1	9.2	3.2	23.6	<30	26	8	165	1.14	3.0	5	1	170	.39	.6	.1	10	5.25	.038	2	15	.39	585	.01	5	.24	.01	.01	<2	<2	36	32.6	<.2	.7	1
3600N 5300E	.3	10.2	6.6	45.0	<30	35	9	297	2.49	5.3	<5	4	19	.05	<.2	.1	44	.28	.061	15	39	.51	222	.10	<2	1.37	.01	.04	<2	<2	24	.4	<.2	3.9	1
3600N 5325E	.5	10.5	7.2	46.5	<30	47	14	438	2.64	6.6	<5	6	12	.07	.3	.1	41	.22	.129	16	41	.68	120	.07	<2	1.31	.01	.04	<2	<2	12	<.3	<.2	3.5	86
3600N 5350E	.6	16.7	7.2	46.6	<30	51	13	339	2.83	6.8	<5	7	14	.06	.4	.1	48	.22	.087	13	45	.72	219	.12	<2	1.66	.01	.06	<2	<2	10	<.3	<.2	4.1	2
3600N 5375E	.5	13.4	7.7	39.7	<30	48	12	183	3.13	7.8	<5	9	16	.03	.3	.1	55	.20	.032	14	56	.48	218	.11	2	1.71	.01	.06	<2	<2	38	<.3	<.2	4.2	1
3600N 5400E	.8	10.9	7.7	45.3	<30	55	13	251	3.06	7.5	<5	6	13	.03	.2	.1	51	.21	.040	13	53	.65	265	.09	<2	1.71	.01	.06	<2	<2	14	<.3	<.2	3.7	2
3600N 5425E	.8	11.5	7.6	48.3	<30	53	14	264	3.01	7.4	<5	5	16	.04	.3	.1	49	.25	.069	12	44	.68	233	.12	<2	1.76	.01	.06	<2	<2	14	<.3	<.2	4.6	2
3600N 5450E	.7	10.4	7.7	45.2	<30	47	11	210	3.14	8.2	<5	5	15	.03	.2	.1	55	.21	.038	12	51	.50	244	.12	<2	1.94	.01	.07	<2	<2	16	<.3	<.2	4.2	3
3600N 5475E	.7	10.7	7.9	56.0	<30	48	11	234	3.10	7.5	<5	5	15	.05	.2	.1	56	.24	.068	13	46	.53	287	.12	<2	1.85	.01	.08	<2	<2	<10	<.3	<.2	4.8	2
3600N 5500E	.7	12.4	8.4	47.7	<30	66	12	252	3.40	8.8	<5	6	16	.04	.2	.1	60	.24	.065	11	63	.58	289	.13	<2	2.07	.01	.09	<2	<2	<10	<.3	<.2	4.6	1
3600N 5525E	.7	10.1	7.2	44.3	<30	55	12	268	2.91	7.4	<5	4	14	.04	<.2	.1	50	.23	.068	10	49	.62	227	.11	2	1.62	.01	.09	<2	<2	<10	<.3	<.2	3.9	113
3600N 5550E	.7	9.8	7.2	53.8	<30	46	10	224	2.68	5.7	<5	4	13	.07	.2	.1	49	.22	.047	11	44	.57	245	.10	2	1.57	.01	.07	<2	<2	10	<.3	<.2	4.1	3
3600N 5575E	.5	9.4	6.9	82.9	<30	43	10	385	2.73	3.9	<5	4	14	.08	<.2	.1	49	.21	.073	12	42	.55	240	.10	2	1.72	.01	.05	<2	<2	<10	<.3	<.2	4.6	2
3600N 5600E	.5	7.8	6.8	61.3	<30	40	10	230	2.73	4.6	<5	4	15	.07	.2	.1	50	.25	.070	10	47	.50	191	.10	2	1.46	.01	.07	<2	<2	12	<.3	<.2	4.2	1
STANDARD D2/HG	25.3	129.8	105.5	280.3	1937	35	16	1058	4.32	81.5	25	20	59	2.28	8.7	22.4	77	.72	.107	17	57	1.28	272	.15	26	2.45	.05	.70	18	2.6	537	.4	2.1	6.8	46

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3600N 5625E	.8	6.6	7.0	39.2	<30	33	9	210	2.72	4.8	<5	5	11	.08	<.2	.1	47	.24	.044	10	44	.46	180	.07	2	1.19	.01	.06	<2	<.2	13	<.3	<.2	4.2	7
3600N 5650E	.5	10.9	7.9	36.7	<30	40	13	260	3.28	7.6	<5	8	14	.05	<.2	.2	49	.25	.068	12	47	.54	175	.09	<2	1.31	.01	.07	<2	<.2	23	<.3	<.2	4.1	8
3600N 5675E	.5	9.0	6.2	33.1	<30	40	11	187	2.98	7.5	<5	6	14	.05	.2	.1	43	.25	.053	14	35	.55	128	.09	2	1.09	.01	.05	2	<.2	12	<.3	<.2	4.3	6
3600N 5700E	.8	10.2	10.0	64.5	<30	44	10	253	3.73	7.6	<5	8	16	.13	.2	.2	63	.24	.057	14	45	.52	384	.14	2	2.04	.01	.07	2	<.2	12	<.3	<.2	7.6	10
3600N 5725E	1.0	8.6	10.9	61.1	54	25	7	221	3.76	8.7	<5	6	14	.21	<.2	.3	73	.27	.066	15	38	.33	242	.10	2	1.38	.01	.05	<2	<.2	10	<.3	<.2	8.5	11
3600N 5750E	.7	10.7	11.7	106.8	<30	31	9	291	3.48	7.2	<5	5	19	.39	.2	.2	56	.32	.145	16	35	.48	323	.10	3	1.77	.01	.09	<2	<.2	13	<.3	<.2	7.9	12
3600N 5775E	1.7	23.9	2.5	16.9	159	13	3	295	.35	1.6	30	<1	260	.90	1.4	.1	10	7.99	.051	1	27	.45	752	<.01	348	.18	.02	.02	<2	<.2	52	21.2	<.2	.9	3
3600N 5800E	3.7	5.4	1.6	5.3	<30	4	1	16	.14	<.5	69	1	198	.28	2.6	<.1	16	5.85	.022	<1	8	.31	570	<.01	416	.09	.01	.01	<2	<.2	15	18.2	<.2	<.5	2
3550N 5300E	.7	13.7	9.9	47.5	<30	75	16	254	3.22	8.6	<5	6	13	.12	.5	.2	52	.32	.095	15	63	1.09	143	.09	3	1.35	.01	.06	<2	<.2	28	.8	<.2	4.1	10
3550N 5325E	.2	4.0	7.6	32.2	<30	18	4	101	1.49	2.2	<5	6	14	.04	<.2	.1	25	.29	.060	16	30	.33	119	.08	2	.90	.02	.05	<2	<.2	15	<.3	<.2	3.9	8
3550N 5350E	.6	11.7	8.2	41.9	39	40	10	247	2.67	7.2	<5	7	12	.08	.2	.2	44	.20	.077	14	41	.44	238	.08	<2	1.45	.01	.06	<2	<.2	<10	<.3	<.2	5.2	8
3550N 5375E	.5	12.6	7.5	40.2	<30	50	10	205	2.75	6.3	6	6	16	.06	.2	.1	44	.27	.079	14	47	.58	182	.08	<2	1.30	.01	.08	<2	<.2	15	<.3	<.2	4.6	8
3550N 5400E	.7	13.7	8.3	50.2	<30	40	10	185	3.08	6.1	<5	8	13	.06	.3	.2	54	.19	.036	14	52	.43	176	.12	2	1.43	.01	.09	<2	<.2	<10	.3	<.2	4.7	8
3550N 5425E	.6	14.2	7.1	44.5	<30	42	11	300	2.92	6.4	<5	6	17	.05	.3	.1	52	.26	.059	15	48	.50	246	.13	<2	1.49	.02	.09	<2	<.2	14	.5	<.2	5.2	7
3550N 5450E	.6	7.2	7.1	45.8	61	28	8	415	2.54	4.0	<5	3	15	.07	<.2	.1	49	.26	.049	12	36	.30	192	.09	2	1.36	.01	.07	<2	<.2	17	<.3	<.2	6.0	7
3550N 5475E	.6	13.0	7.4	35.7	<30	43	11	217	2.88	7.5	<5	8	14	.05	.3	.1	49	.21	.047	14	55	.47	158	.11	<2	1.32	.01	.07	<2	<.2	<10	<.3	<.2	4.4	7
3550N 5500E	.6	12.4	7.2	39.1	<30	51	11	236	2.73	6.6	12	7	14	.05	.3	.1	46	.29	.126	12	47	.62	195	.09	<2	1.28	.01	.08	<2	<.2	12	<.3	<.2	4.0	7
3550N 5525E	.6	10.9	7.4	52.1	<30	53	11	225	2.74	5.1	<5	6	12	.08	<.2	.1	45	.25	.067	13	46	.64	158	.09	2	1.26	.01	.06	<2	<.2	<10	<.3	<.2	4.4	7
3550N 5550E	.5	11.8	7.0	38.5	<30	55	11	237	2.45	6.1	<5	6	12	.06	.4	.1	37	.26	.087	12	40	.71	115	.08	<2	1.06	.01	.05	<2	<.2	<10	<.3	<.2	3.7	7
3550N 5575E	.6	12.9	8.4	69.5	<30	49	10	226	2.84	6.1	<5	5	13	.12	<.2	.2	50	.24	.118	14	46	.57	233	.10	2	1.56	.01	.07	<2	<.2	11	<.3	<.2	5.8	8
3550N 5600E	.6	8.7	8.1	96.9	32	52	9	163	3.08	5.7	<5	4	12	.12	<.2	.1	58	.25	.089	11	55	.51	197	.11	2	1.53	.01	.07	<2	<.2	22	<.3	<.2	5.8	8
RE 3550N 5600E	.6	10.2	8.9	99.3	51	55	10	172	3.30	6.0	<5	4	12	.15	<.2	.2	61	.26	.097	12	58	.55	210	.11	2	1.59	.01	.08	<2	<.2	15	<.3	<.2	6.6	9
3550N 5625E	.2	12.3	6.6	41.7	70	27	8	295	2.11	4.7	20	3	79	.09	<.2	.2	35	6.80	.022	12	29	.59	572	.07	2	1.01	.02	.04	<2	<.2	28	<.3	<.2	3.6	7
3550N 5650E	.5	10.8	6.2	41.4	<30	54	12	329	2.90	6.7	<5	7	17	.04	.3	.2	41	.37	.112	15	38	.76	139	.10	<2	1.04	.02	.07	<2	<.2	<10	<.3	<.2	3.8	6
3550N 5675E	.5	11.8	6.8	37.9	<30	56	13	322	3.24	6.9	<5	8	17	.07	<.2	.2	44	.35	.085	17	39	.82	146	.09	<2	1.01	.02	.07	<2	<.2	10	<.3	<.2	3.9	7
3550N 5700E	.7	8.2	8.9	50.6	40	24	7	344	2.55	5.1	<5	4	16	.18	.2	.2	42	.28	.101	15	27	.30	279	.09	<2	1.16	.01	.08	<2	<.2	14	<.3	<.2	5.6	9
3550N 5725E	.8	6.9	10.1	84.3	47	22	9	283	3.46	5.9	<5	4	10	.27	<.2	.3	66	.15	.081	14	33	.34	210	.10	2	1.37	.01	.05	<2	<.2	<10	<.3	<.2	7.5	10
3550N 5750E	.8	12.6	24.9	96.0	70	29	11	347	3.13	7.7	<5	6	14	.33	<.2	.3	49	.28	.109	17	34	.46	301	.07	2	1.77	.01	.12	<2	<.2	14	<.3	<.2	7.7	25
3500N 5300E	.5	12.0	6.9	46.6	<30	35	11	303	2.96	5.7	<5	6	19	.08	<.2	.2	54	.25	.062	15	47	.45	256	.13	<2	1.45	.02	.05	<2	<.2	<10	<.3	<.2	5.3	7
3500N 5325E	.5	15.2	6.3	39.0	<30	40	10	299	2.94	5.9	<5	6	19	.05	<.2	.2	53	.29	.076	22	49	.54	216	.12	<2	1.33	.02	.07	<2	<.2	11	<.3	<.2	5.1	6
3500N 5350E	.5	12.7	7.6	41.9	<30	63	13	232	2.83	6.3	<5	6	12	.09	.2	.1	45	.27	.081	14	51	.82	143	.08	2	1.16	.01	.05	<2	<.2	10	<.3	<.2	3.9	8
3500N 5375E	.7	13.9	8.1	43.5	<30	43	11	192	3.08	6.9	8	6	13	.06	<.2	.2	52	.20	.068	12	49	.46	212	.11	<2	1.55	.01	.09	<2	<.2	12	<.3	<.2	5.3	8
3500N 5400E	.9	12.6	7.0	36.7	<30	51	10	210	2.95	7.3	<5	5	14	.04	<.2	.2	49	.24	.045	10	51	.48	240	.12	2	1.40	.01	.09	<2	<.2	<10	<.3	<.2	4.9	7
3500N 5425E	1.0	10.7	7.6	52.5	<30	43	9	229	2.98	6.0	<5	3	11	.07	<.2	.3	50	.20	.033	10	49	.50	237	.11	2	1.46	.01	.09	<2	<.2	<10	<.3	<.2	4.9	8
3500N 5450E	1.0	15.4	11.1	58.8	76	67	14	463	3.31	7.3	<5	7	13	.10	.3	.3	50	.28	.170	20	54	.75	242	.08	<2	1.58	.01	.07	<2	<.2	16	<.3	<.2	4.9	11
STANDARD D2/HG	28.1	134.5	108.5	286.5	2090	36	16	1097	4.50	79.5	21	23	56	2.51	8.5	21.4	83	.80	.113	20	62	1.23	265	.16	21	2.41	.06	.73	16	2.5	534	.8	2.5	7.0	48

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3500N 5475E	.5	10.1	6.9	41.9	45	67	13	244	2.82	6.0	<5	5	12	.08	.2	.1	45	.25	.062	11	51	.87	191	.08	<2	1.31	.01	.05	<2	<.2	20	<.3	<.2	3.3	2
3500N 5500E	.5	10.3	6.2	40.2	<30	52	11	209	2.60	6.5	<5	5	14	.07	<.2	.2	44	.25	.070	11	44	.64	187	.09	<2	1.33	.01	.05	<2	<.2	14	<.3	<.2	3.2	<1
3500N 5525E	.6	10.0	6.6	39.0	<30	52	12	237	2.69	5.5	<5	5	14	.04	.3	.2	45	.24	.056	10	48	.68	212	.09	<2	1.28	.01	.06	<2	<.2	13	<.3	<.2	3.6	<1
3500N 5550E	.8	12.2	7.9	43.5	<30	51	13	247	3.10	6.9	<5	5	15	.05	.5	.2	54	.25	.052	11	59	.62	256	.10	<2	1.53	.01	.07	<2	<.2	18	<.3	<.2	4.6	4
3500N 5575E	.6	8.3	6.3	36.8	<30	24	6	133	1.89	5.5	<5	4	11	.03	.3	.1	27	.19	.021	14	25	.35	229	.04	<2	1.00	.01	.04	<2	<.2	13	<.3	<.2	2.9	<1
3500N 5600E	.5	11.0	6.3	41.1	<30	55	10	209	2.26	5.5	<5	4	14	.11	<.2	.2	37	.28	.057	9	44	.80	156	.07	2	1.47	.01	.07	<2	<.2	19	<.3	<.2	3.4	4
3500N 5625E	.6	4.8	7.6	65.4	<30	25	12	608	2.16	2.8	<5	3	15	.09	<.2	.1	40	.29	.072	9	31	.33	163	.06	2	1.10	.01	.07	<2	<.2	12	<.3	<.2	4.0	2
3500N 5650E	.4	7.0	5.7	35.9	<30	29	11	307	2.54	5.5	<5	5	23	.04	<.2	.2	40	.44	.073	14	33	.47	258	.10	<2	1.17	.02	.05	<2	<.2	20	<.3	.2	3.5	<1
3500N 5675E	.5	10.1	6.3	36.6	<30	37	11	217	2.73	6.0	<5	6	14	.04	<.2	.1	43	.23	.051	11	38	.50	216	.09	<2	1.30	.01	.05	<2	<.2	22	<.3	<.2	3.5	1
3500N 5700E	.6	8.8	6.8	43.1	<30	31	10	221	2.80	6.3	<5	4	18	.04	.2	.3	45	.27	.047	12	37	.48	171	.09	<2	1.54	.01	.04	<2	<.2	15	<.3	<.2	4.4	1
3500N 5725E	.9	8.9	9.1	98.3	41	36	11	341	3.39	8.1	<5	4	17	.19	.4	.3	59	.29	.056	14	39	.47	383	.11	<2	2.05	.01	.09	<2	<.2	20	<.3	<.2	6.5	<1
3500N 5750E	1.1	6.0	10.1	59.8	31	18	7	235	2.85	5.1	<5	3	14	.24	.2	.2	59	.24	.055	13	29	.28	207	.09	<2	1.10	.01	.07	<2	<.2	15	<.3	<.2	6.0	37
3500N 5775E	.9	9.7	9.1	65.3	138	35	11	272	3.17	8.0	<5	6	16	.17	.6	.3	53	.33	.058	17	37	.51	203	.07	<2	1.35	.01	.07	<2	<.2	25	<.3	<.2	5.0	183
3500N 5800E	1.3	18.6	8.4	44.5	145	20	10	314	2.67	12.6	<5	1	42	.15	2.3	.2	17	.91	.024	11	10	.14	327	.01	2	.68	.01	.04	<2	<.2	34	.6	<.2	2.1	3
RE 3500N 5300E	.5	10.3	6.3	36.5	<30	46	11	208	2.67	6.3	<5	6	12	.04	.4	.1	45	.21	.047	14	50	.54	236	.08	<2	1.23	.01	.05	<2	<.2	12	<.3	<.2	3.6	1
3450N 5300E	.5	11.2	6.8	38.8	<30	50	12	223	2.86	6.2	<5	7	13	.05	.4	.1	49	.22	.049	14	52	.59	252	.08	<2	1.30	.01	.05	<2	<.2	16	<.3	<.2	4.0	<1
3450N 5325E	.4	11.8	5.8	37.4	<30	40	11	280	2.61	6.5	<5	6	15	.05	.3	.2	44	.22	.060	21	46	.52	169	.09	<2	1.17	.01	.05	<2	<.2	22	<.3	<.2	3.6	<1
3450N 5350E	.4	11.7	6.5	39.2	<30	44	12	235	2.68	6.0	<5	6	15	.06	.3	.2	46	.23	.064	17	48	.54	204	.09	<2	1.22	.01	.05	<2	<.2	14	<.3	.2	3.7	3
3450N 5375E	.4	10.4	6.0	41.5	<30	43	11	249	2.68	4.7	<5	5	14	.04	.4	.1	46	.24	.060	12	44	.62	273	.10	<2	1.27	.01	.08	<2	<.2	17	<.3	<.2	3.8	<1
3450N 5400E	.5	11.1	6.6	39.7	<30	40	10	232	2.70	6.5	<5	6	14	.03	.5	.2	44	.20	.048	16	44	.51	221	.09	<2	1.32	.01	.05	<2	<.2	21	<.3	<.2	4.1	9
3450N 5425E	.5	8.6	7.2	56.4	32	56	11	292	2.82	4.5	<5	5	13	.07	.4	.1	47	.27	.098	13	45	.69	246	.08	<2	1.24	.01	.06	<2	<.2	12	<.3	<.2	4.3	42
3450N 5450E	.6	10.2	6.6	47.1	<30	38	11	254	2.86	5.1	<5	6	15	.04	.3	.2	51	.22	.049	13	47	.52	227	.11	<2	1.54	.01	.07	<2	<.2	19	<.3	<.2	4.8	2
3450N 5475E	.6	10.8	7.2	42.0	32	47	11	195	2.78	7.3	<5	5	13	.05	.4	.1	47	.24	.067	11	45	.52	167	.09	<2	1.35	.01	.06	<2	<.2	14	<.3	<.2	4.1	2
3450N 5500E	.5	9.6	6.2	39.8	<30	43	11	215	2.78	5.5	<5	4	14	.05	<.2	.2	48	.19	.042	10	46	.49	233	.10	<2	1.53	.01	.06	<2	<.2	<10	<.3	.2	4.3	2
3450N 5525E	.6	11.3	6.4	40.7	55	39	10	194	2.99	6.2	<5	6	16	.02	.5	.1	53	.22	.044	10	50	.44	225	.12	<2	1.64	.01	.07	<2	<.2	14	<.3	<.2	4.6	1
3450N 5550E	.6	10.8	7.2	42.6	<30	43	11	228	2.85	6.7	<5	5	14	.02	.5	.1	49	.22	.047	12	45	.56	234	.11	<2	1.47	.01	.05	<2	<.2	16	<.3	<.2	4.5	2
3450N 5575E	.7	10.4	8.7	43.7	136	50	11	225	2.31	6.3	<5	3	15	.05	.8	.1	31	.24	.106	9	41	.73	200	.05	<2	.99	.01	.06	<2	<.2	19	<.3	<.2	3.2	1
3450N 5600E	.5	8.3	5.3	38.6	<30	40	9	181	2.79	4.7	<5	4	15	.06	<.2	.2	50	.32	.053	12	51	.51	209	.09	2	1.19	.01	.07	<2	<.2	15	<.3	.3	3.4	2
3450N 5625E	.5	9.1	7.3	64.0	<30	39	10	301	2.82	4.7	<5	3	14	.11	<.2	.2	50	.25	.060	12	44	.49	266	.09	<2	1.54	.01	.06	<2	<.2	<10	<.3	<.2	5.3	1
3450N 5650E	.4	9.0	5.7	37.3	<30	36	10	243	2.45	6.6	<5	5	13	.02	.4	.1	34	.25	.095	14	28	.61	102	.08	<2	.98	.01	.06	<2	<.2	15	<.3	<.2	3.4	1
3450N 5675E	.5	5.8	5.6	47.4	<30	18	6	142	2.32	3.4	<5	3	9	.06	.2	.1	42	.10	.019	10	27	.29	90	.09	<2	1.09	.01	.05	<2	<.2	<10	<.3	<.2	4.3	1
3450N 5700E	.4	9.1	5.5	36.8	<30	41	10	218	2.30	4.8	<5	5	13	.02	.5	.1	32	.22	.070	11	28	.64	95	.08	<2	.94	.01	.06	<2	<.2	14	<.3	<.2	3.3	1
3450N 5725E	.7	8.6	8.7	60.3	105	34	10	328	3.11	6.0	<5	3	13	.13	.3	.1	54	.21	.063	12	37	.42	329	.09	<2	1.65	.01	.05	<2	<.2	19	<.3	<.2	6.3	1
3450N 5750E	.7	9.8	7.8	63.7	255	30	9	686	3.03	7.0	<5	3	14	.16	.5	.1	49	.27	.085	13	33	.40	384	.06	<2	1.58	.01	.07	2	<.2	47	<.3	<.2	5.4	750
3450N 5775E	.8	7.9	8.3	53.2	<30	32	10	203	2.96	7.3	<5	4	12	.09	.5	.2	47	.19	.042	12	35	.39	254	.09	<2	1.56	.01	.06	<2	<.2	19	<.3	<.2	5.6	1
STANDARD D2/HG	26.3	130.9	102.7	293.9	2017	35	17	1113	4.52	81.6	22	19	61	2.46	9.8	20.3	81	.75	.113	18	57	1.21	278	.15	29	2.49	.05	.70	18	2.5	514	.4	2.3	7.2	54

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3450N 5800E	.6	10.7	9.3	40.3	<30	25	8	150	2.37	11.1	<5	6	12	.09	.4	.2	35	.21	.026	17	29	.40	130	.06	<2	1.32	.01	.05	<2	<.2	23	<.3	<.2	3.6	6
3400N 5300E	.4	17.6	8.1	45.4	<30	48	12	298	2.81	6.9	<5	7	16	.08	<.2	.2	48	.26	.076	17	47	.73	261	.10	<2	1.49	.01	.06	<2	<.2	25	<.3	<.2	4.3	1
3400N 5325E	.3	12.9	8.0	37.8	<30	41	10	308	2.67	7.0	<5	6	19	.04	.4	.2	44	.35	.040	19	44	.58	289	.11	<2	1.20	.02	.06	<2	<.2	20	<.3	<.2	4.2	2
3400N 5350E	.5	14.7	7.2	40.5	<30	50	11	255	2.69	7.0	<5	6	13	.07	.4	.2	46	.26	.064	15	51	.68	247	.09	<2	1.25	.01	.07	<2	<.2	26	<.3	<.2	4.1	2
3400N 5375E	.5	11.5	7.6	37.7	<30	51	10	273	2.74	7.7	<5	6	14	.10	.3	.2	48	.29	.049	17	59	.69	208	.10	<2	1.10	.01	.06	<2	<.2	23	<.3	<.2	3.4	1
3400N 5400E	.5	14.4	8.1	43.8	<30	56	12	278	2.93	8.7	<5	8	16	.07	.3	.2	52	.29	.062	16	56	.68	286	.11	<2	1.48	.02	.07	<2	.2	25	<.3	<.2	4.7	1
3400N 5425E	.4	13.8	6.5	35.8	<30	45	10	268	2.55	7.2	<5	6	16	.06	.3	.1	42	.29	.056	20	49	.68	183	.10	<2	1.03	.01	.07	<2	<.2	11	<.3	<.2	3.4	1
3400N 5450E	.5	14.8	8.1	35.0	<30	47	10	189	2.68	9.1	<5	7	15	.05	.4	.1	46	.22	.042	14	46	.58	232	.10	<2	1.33	.01	.04	<2	<.2	20	<.3	<.2	3.9	1
3400N 5475E	.6	12.6	8.5	41.0	<30	41	9	232	2.37	6.0	<5	5	11	.06	.4	.1	39	.21	.049	12	43	.61	201	.08	<2	1.13	.01	.06	<2	<.2	16	<.3	<.2	3.6	1
RE 3400N 5475E	.6	12.0	8.1	41.5	<30	43	10	231	2.41	6.6	<5	5	12	.06	.3	.2	41	.22	.051	13	44	.63	207	.09	2	1.16	.01	.05	<2	<.2	14	<.3	<.2	3.7	1
3400N 5500E	.8	14.2	10.5	47.5	34	54	12	214	2.61	12.3	<5	6	15	.07	.2	.3	44	.26	.071	15	43	.68	277	.08	2	1.45	.01	.07	<2	<.2	16	<.3	<.2	3.5	2
3400N 5525E	.5	13.4	7.6	34.7	<30	48	10	168	2.59	7.8	<5	5	14	.04	.2	.2	43	.23	.051	13	41	.61	158	.09	<2	1.29	.01	.05	<2	<.2	17	<.3	<.2	3.8	1
3400N 5550E	.9	13.4	9.9	55.1	<30	50	11	290	2.87	8.2	<5	4	13	.10	.2	.3	53	.24	.061	15	48	.59	222	.10	2	1.70	.01	.05	<2	<.2	26	<.3	<.2	5.5	<1
3400N 5575E	.7	11.0	8.2	41.2	<30	38	8	180	2.66	8.4	5	5	14	.04	.2	.1	47	.24	.059	14	41	.47	224	.10	<2	1.46	.01	.07	<2	<.2	13	<.3	<.2	4.3	1
3400N 5600E	.6	8.0	8.4	50.1	<30	26	7	156	2.77	8.7	<5	5	16	.14	<.2	.2	51	.25	.032	13	43	.42	169	.12	<2	1.44	.01	.09	<2	<.2	15	<.3	.3	4.8	4
3400N 5625E	.5	12.0	9.4	40.6	<30	52	13	253	3.68	12.8	<5	9	17	.06	.3	.3	62	.32	.070	18	52	.78	172	.11	<2	1.30	.01	.07	<2	<.2	30	<.3	<.2	4.5	3
3400N 5650E	.7	10.8	9.4	36.5	35	35	8	154	2.73	12.2	<5	5	12	.04	.2	.2	45	.20	.048	13	39	.43	155	.10	<2	1.42	.01	.08	<2	<.2	<10	<.3	<.2	4.5	3
3400N 5675E	.6	11.2	9.3	43.3	<30	48	12	222	3.08	11.0	<5	7	14	.08	<.2	.2	46	.25	.065	15	39	.73	118	.10	<2	1.31	.01	.06	<2	<.2	17	<.3	<.2	3.7	21
3400N 5700E	.7	10.7	9.0	38.0	<30	55	12	213	2.90	9.7	<5	7	11	.05	.4	.1	40	.24	.073	16	39	.76	78	.07	<2	1.13	.01	.04	<2	<.2	17	<.3	<.2	3.1	9
3400N 5725E	.6	6.7	8.8	50.1	<30	16	6	144	2.42	7.1	<5	4	12	.10	<.2	.2	48	.15	.021	16	34	.31	166	.10	<2	1.40	.01	.05	<2	<.2	11	<.3	<.2	5.3	<1
3400N 5750E	1.1	11.2	10.6	62.9	42	35	10	216	3.31	8.3	<5	5	13	.12	<.2	.2	59	.19	.059	13	42	.45	318	.11	<2	2.21	.01	.05	<2	<.2	13	<.3	<.2	6.4	123
3400N 5775E	1.0	8.7	10.7	53.4	35	26	8	190	2.95	10.2	<5	5	12	.10	.2	.3	51	.21	.074	15	35	.40	194	.09	<2	1.67	.01	.06	<2	<.2	<10	<.3	<.2	5.6	<1
3400N 5800E	.7	6.6	9.3	54.7	<30	21	7	164	2.30	8.0	<5	5	12	.07	<.2	.2	41	.20	.046	17	29	.36	171	.09	<2	1.41	.01	.07	<2	<.2	30	<.3	<.2	4.7	53
3350N 5300E	.5	12.5	10.4	61.0	49	35	10	249	2.79	5.8	5	6	12	.10	.2	.2	49	.19	.090	14	45	.49	251	.10	<2	1.53	.01	.06	<2	<.2	19	<.3	<.2	4.9	3
3350N 5325E	.4	10.6	7.9	47.0	<30	27	8	153	2.40	6.3	<5	4	12	.09	<.2	.1	43	.17	.056	14	39	.39	171	.11	<2	1.37	.01	.05	<2	<.2	20	<.3	<.2	4.9	1
3350N 5350E	.6	21.3	7.8	38.6	<30	40	11	212	2.85	8.6	<5	7	17	.06	.2	.1	50	.24	.057	25	50	.50	202	.13	<2	1.49	.01	.07	<2	<.2	29	<.3	<.2	4.6	1
3350N 5375E	.7	12.4	9.1	50.3	<30	44	10	188	2.86	11.2	<5	7	14	.07	<.2	.2	51	.22	.078	16	49	.51	233	.10	<2	1.69	.01	.08	<2	<.2	19	<.3	<.2	5.0	1
3350N 5400E	.5	11.9	8.7	76.7	<30	52	11	363	2.92	5.6	<5	5	13	.15	<.2	.2	53	.28	.102	13	54	.59	257	.09	<2	1.58	.01	.06	<2	<.2	27	<.3	<.2	4.9	2
3350N 5425E	.5	12.5	8.5	45.1	<30	49	11	241	2.69	7.3	5	5	13	.09	<.2	.2	47	.26	.072	13	50	.63	202	.09	<2	1.37	.01	.05	<2	<.2	29	<.3	.2	3.9	35
3350N 5450E	.5	14.6	7.5	36.1	<30	43	10	197	2.66	7.4	5	7	13	.07	<.2	.2	46	.21	.049	13	47	.50	226	.09	<2	1.35	.01	.04	<2	<.2	<10	<.3	<.2	4.0	<1
3350N 5475E	.5	10.9	8.1	62.8	<30	37	9	260	2.59	5.5	<5	5	12	.10	<.2	.1	48	.21	.050	12	46	.41	256	.09	<2	1.42	.01	.05	<2	<.2	20	<.3	<.2	4.9	62
3350N 5500E	.5	15.2	8.2	40.4	<30	39	10	161	2.86	6.8	7	6	12	.06	<.2	.2	52	.18	.046	12	52	.42	312	.09	<2	1.59	.01	.06	<2	<.2	20	<.3	<.2	4.5	2
3350N 5525E	.5	11.5	7.0	38.8	<30	42	10	224	2.73	9.0	5	5	13	.05	.3	.1	42	.24	.078	12	38	.63	163	.08	4.24	1.18	.01	.06	<2	<.2	16	<.3	<.2	3.5	1
3350N 5550E	.7	8.2	9.2	66.3	98	32	10	454	2.89	7.4	8	4	13	.19	<.2	.2	52	.24	.083	15	40	.40	289	.08	<2	1.55	.01	.06	3	<.2	34	<.3	.2	5.5	310
3350N 5575E	.8	8.6	10.4	83.7	40	37	11	510	3.03	7.6	<5	4	13	.24	<.2	.4	54	.26	.120	16	41	.47	313	.08	<2	1.56	.01	.06	<2	<.2	22	<.3	<.2	5.8	87
STANDARD D2/HG	26.6	126.3	97.2	273.7	1851	34	16	1081	4.39	78.0	20	18	55	2.24	9.2	19.1	77	.72	.103	18	63	1.22	263	.18	26	2.47	.06	.74	14	2.3	496	.8	2.1	6.6	46

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



AAE ANALYTICAL



AAE ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3350N 5600E	.6	8.3	7.3	36.7	51	17	5	177	1.55	5.0	<5	3	11	.10	.3	.2	24	.20	.027	9	19	.19	218	.04	2	.82	.01	.06	<2	<2	26	<.3	<.2	2.7	3
3350N 5625E	.8	10.4	8.9	43.8	35	37	8	173	2.97	7.8	<5	4	12	.08	.2	.2	50	.22	.072	12	39	.48	162	.10	<2	1.38	.01	.06	<2	<2	54	<.3	<.2	5.2	69
3350N 5650E	1.0	11.0	11.1	39.6	35	34	8	261	2.86	8.3	<5	4	13	.08	.2	.3	46	.21	.047	10	39	.45	186	.09	<2	1.46	.01	.07	<2	<2	25	<.3	<.2	5.2	3
3350N 5675E	.9	7.7	9.5	57.0	<30	27	14	289	2.90	4.3	<5	5	12	.11	.3	.2	48	.21	.077	14	34	.49	115	.09	<2	1.25	.01	.07	<2	<2	25	<.3	<.2	5.2	3
3350N 5700E	.9	11.6	10.0	44.9	<30	61	17	332	3.78	7.0	<5	7	12	.17	.4	.2	57	.27	.134	16	43	1.00	125	.07	<2	1.19	.01	.04	2	<2	33	<.3	<.2	4.6	1
3350N 5725E	1.2	10.3	10.5	40.0	<30	23	7	160	2.47	7.7	<5	8	14	.08	.4	.2	37	.27	.062	15	32	.38	124	.07	<2	1.17	.01	.07	<2	<2	26	.3	<.2	3.8	1
3350N 5750E	1.1	15.6	11.6	53.4	195	43	11	210	3.43	12.1	<5	7	13	.11	.3	.3	59	.20	.072	18	47	.49	242	.09	<2	2.03	.01	.06	2	<2	34	<.3	<.2	6.2	395
3350N 5775E	.6	14.1	9.6	35.9	<30	28	9	242	2.40	10.1	<5	9	13	.05	.5	.3	34	.24	.074	20	31	.43	117	.06	<2	1.08	.01	.05	<2	<2	13	<.3	<.2	2.9	4
3300N 5300E	.6	16.7	7.4	36.9	<30	41	10	214	2.65	6.4	<5	7	16	.08	.2	.2	47	.24	.065	20	47	.52	256	.10	<2	1.38	.01	.04	<2	<2	27	<.3	<.2	4.4	1
3300N 5325E	.8	18.9	9.1	46.1	<30	61	13	240	3.52	9.3	<5	10	17	.10	.3	.3	70	.26	.105	20	70	.65	319	.13	2	2.01	.01	.06	<2	<2	17	<.3	<.2	5.8	<1
3300N 5350E	.7	19.5	10.9	80.7	67	60	14	257	3.26	8.5	<5	7	12	.19	.3	.2	60	.21	.154	19	55	.70	257	.12	3	2.19	.01	.06	<2	<2	38	<.3	<.2	5.6	<1
3300N 5375E	.8	18.2	10.5	56.7	104	48	13	328	3.17	6.5	<5	8	13	.13	.4	.2	58	.21	.115	17	51	.59	339	.11	<2	1.99	.01	.06	<2	<2	27	<.3	<.2	5.5	38
3300N 5400E	.6	14.8	7.7	38.7	<30	48	11	386	2.67	6.1	<5	8	14	.10	.3	.2	45	.28	.085	17	50	.64	172	.09	<2	1.21	.01	.05	<2	<2	22	<.3	<.2	4.0	<1
3300N 5425E	.8	19.4	10.4	46.4	<30	49	13	200	3.43	6.4	<5	9	15	.07	.3	.2	70	.17	.072	18	65	.50	329	.13	2	2.22	.01	.05	<2	<2	27	<.3	<.2	6.3	<1
RE 3300N 5425E	.6	17.1	8.7	44.0	<30	45	12	189	3.23	6.3	<5	7	14	.06	.2	.2	65	.16	.067	17	61	.47	307	.13	<2	2.08	.01	.05	<2	<2	17	<.3	<.2	5.9	1
3300N 5450E	.7	16.3	9.7	39.1	<30	44	11	178	3.14	6.8	<5	7	14	.06	.2	.2	60	.18	.060	15	61	.43	248	.12	2	1.81	.01	.06	<2	<2	22	<.3	<.2	5.2	1
3300N 5475E	.7	16.0	9.1	51.6	35	56	11	224	3.13	6.8	5	7	14	.09	.2	.2	58	.23	.070	13	61	.55	327	.10	2	1.87	.01	.05	<2	<2	26	<.3	<.2	5.3	1
3300N 5500E	.6	13.5	9.1	49.2	54	59	11	222	2.99	5.9	<5	5	12	.10	.2	.2	53	.24	.112	12	51	.64	237	.09	<2	1.56	.01	.06	<2	<2	25	<.3	<.2	4.9	1
3300N 5525E	.8	15.2	11.9	100.1	185	55	13	412	3.44	8.4	<5	7	16	.25	.2	.2	66	.31	.128	17	53	.53	331	.11	3	2.16	.01	.07	<2	<2	34	<.3	<.2	6.2	13
3300N 5550E	.8	17.2	11.8	77.2	84	56	13	323	3.60	7.5	<5	8	13	.14	.2	.3	69	.21	.091	21	59	.58	380	.12	3	2.19	.01	.05	<2	<2	130	<.3	<.2	5.8	21
3300N 5575E	.8	16.4	13.2	111.0	136	55	14	326	3.37	6.6	<5	6	13	.16	.2	.2	64	.24	.100	17	55	.54	423	.11	2	2.25	.01	.06	<2	<2	46	<.3	<.2	6.0	3
3300N 5600E	.7	10.1	11.0	57.4	48	35	9	257	2.59	6.8	9	4	11	.12	.3	.2	47	.23	.062	12	41	.40	272	.08	2	1.61	.01	.08	2	<2	63	<.3	<.2	4.6	<1
3300N 5625E	.9	34.3	11.8	59.8	197	43	10	419	2.42	6.5	8	5	100	.31	.7	.3	51	3.99	.052	18	45	1.03	319	.08	3	1.37	.02	.10	<2	<2	104	<.3	<.2	4.5	1
3300N 5650E	.9	8.4	10.0	57.0	48	26	8	252	2.61	5.3	<5	5	16	.15	<.2	.1	48	.26	.043	14	37	.42	239	.09	2	1.34	.01	.09	<2	<2	21	<.3	<.2	5.2	3
3300N 5675E	.7	7.4	9.4	36.8	57	27	7	169	1.84	6.1	<5	3	12	.06	.2	.2	31	.25	.043	10	28	.42	162	.05	2	.97	.01	.07	<2	<2	44	<.3	<.2	3.6	1
3300N 5700E	.7	7.0	7.8	53.8	<30	20	8	146	2.80	4.2	<5	6	11	.09	<.2	.1	49	.17	.023	13	37	.35	126	.10	2	1.35	.01	.07	<2	<2	22	<.3	<.2	4.2	1
3300N 5725E	2.0	17.3	8.0	25.6	122	32	11	940	2.35	5.9	<5	4	43	.14	.4	.2	35	1.04	.052	16	30	.47	297	.05	2	.90	.01	.03	<2	<2	36	1.5	<.2	3.7	<1
3300N 5750E	.5	14.4	4.0	9.0	185	10	3	201	.43	.6	7	1	169	.46	<.2	.1	7	5.48	.043	<1	6	.33	372	<.01	6	.31	.01	.01	<2	<2	133	8.4	<.2	.9	8
3300N 5775E	1.0	38.2	2.6	33.8	92	41	8	74	.73	<.5	9	<1	174	.96	.4	.1	5	5.87	.010	<1	3	.39	320	<.01	22	.15	.01	.01	<2	<2	68	18.8	<.2	<.5	2
3300N 5800E	.8	11.6	10.5	97.6	65	38	11	238	3.12	6.1	6	6	13	.18	.3	.2	55	.21	.087	14	41	.43	263	.11	2	1.92	.01	.06	<2	<2	36	.5	<.2	6.5	2
3250N 5300E	.7	15.0	8.0	41.6	<30	49	12	242	2.84	9.5	<5	7	14	.10	<.2	.2	50	.25	.108	13	46	.65	182	.11	<2	1.49	.01	.06	<2	<2	29	.3	<.2	4.5	1
3250N 5325E	.5	19.1	7.7	41.2	<30	51	12	305	2.76	6.0	<5	6	13	.08	.3	.1	49	.23	.074	17	51	.73	224	.10	<2	1.39	.01	.05	<2	<2	24	<.3	<.2	4.3	1
3250N 5350E	.5	20.7	7.8	37.0	<30	48	10	186	2.43	4.7	<5	6	13	.08	.2	.2	45	.22	.065	18	49	.55	188	.09	<2	1.36	.01	.03	<2	<2	23	.3	<.2	4.3	1
3250N 5375E	.4	17.0	6.5	32.5	<30	45	11	295	2.52	5.9	<5	7	15	.08	<.2	.2	44	.24	.057	22	50	.58	182	.10	<2	1.18	.01	.04	<2	<2	24	<.3	<.2	3.9	1
3250N 5400E	.7	19.7	9.4	52.4	<30	62	14	221	3.36	8.5	10	8	13	.20	.2	.2	64	.22	.108	18	63	.71	316	.11	2	2.15	.01	.05	<2	<2	28	<.3	<.2	6.1	<1
STANDARD D2/HG	27.9	134.4	107.7	273.4	1904	37	16	1108	4.56	78.8	17	20	52	2.31	9.8	21.3	79	.70	.107	17	66	1.34	264	.19	31	2.44	.06	.76	13	2.4	502	.5	2.0	6.9	49

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3250N 5425E	.6	13.2	8.9	59.5	<30	48	13	286	2.98	7.7	<5	5	13	.13	.3	.1	53	.21	.103	15	48	.63	268	.10	3	1.79	.01	.05	<2	<2	32	<.3	<.2	4.9	2
3250N 5450E	.7	11.2	9.6	52.6	<30	33	12	317	3.25	5.4	<5	4	15	.07	.2	.1	58	.19	.092	14	52	.60	275	.12	2	1.77	.01	.05	<2	<2	27	<.3	<.2	5.8	1
3250N 5475E	.5	13.0	7.4	36.9	<30	54	12	259	2.80	5.4	<5	5	15	.06	.2	.1	50	.21	.054	15	54	.63	257	.10	2	1.40	.01	.05	<2	<2	<10	<.3	<.2	4.3	1
3250N 5500E	.7	12.3	7.6	40.8	<30	42	11	185	2.97	4.5	<5	5	13	.04	.4	.2	56	.16	.031	15	54	.50	311	.11	2	1.54	.01	.04	<2	<2	19	<.3	<.2	4.9	1
3250N 5525E	.5	10.8	7.6	43.3	<30	59	13	232	2.97	7.1	<5	4	15	.07	.2	.1	53	.23	.075	12	54	.77	225	.10	2	1.58	.01	.06	<2	<2	10	<.3	<.2	4.5	1
3250N 5550E	.6	12.3	8.4	47.0	<30	56	12	197	3.26	6.9	<5	6	14	.11	.2	.1	60	.21	.066	15	66	.60	278	.11	3	1.72	.01	.06	<2	<2	12	<.3	<.2	5.3	2
3250N 5575E	.5	11.5	7.4	50.0	72	55	12	243	2.76	5.7	<5	4	13	.13	<.2	.1	50	.23	.076	12	54	.76	231	.09	2	1.43	.01	.05	<2	<2	19	<.3	<.2	4.4	1
3250N 5600E	.8	11.4	11.7	73.9	<30	48	13	390	3.67	8.0	<5	6	12	.17	<.2	.3	64	.22	.128	19	53	.62	220	.08	3	1.63	.01	.04	<2	<2	32	<.3	<.2	5.4	13
3250N 5625E	.6	12.7	9.2	41.4	<30	45	11	211	2.46	7.2	<5	5	12	.09	<.2	.2	39	.22	.071	14	40	.73	178	.07	3	1.21	.01	.05	<2	<2	14	<.3	<.2	3.6	3
3250N 5650E	.8	10.6	9.0	41.7	<30	36	9	166	2.45	8.3	<5	3	13	.10	.3	.2	44	.21	.049	12	36	.43	202	.08	2	1.40	.01	.04	<2	<2	<10	<.3	<.2	4.3	2
3250N 5675E	.7	9.7	8.8	67.3	<30	29	8	279	2.16	5.3	<5	3	14	.14	.2	.1	38	.24	.071	12	30	.37	250	.07	2	1.26	.01	.07	<2	<2	15	<.3	<.2	4.2	2
3250N 5700E	.6	11.5	7.8	39.7	<30	44	11	265	2.83	7.1	<5	6	15	.04	.3	.1	44	.25	.062	14	40	.77	138	.10	2	1.17	.01	.07	<2	<2	28	<.3	<.2	4.0	2
3250N 5725E	.5	11.1	6.4	37.1	<30	39	11	267	2.46	6.1	<5	5	13	.04	.3	.1	34	.23	.059	14	30	.77	104	.09	<2	.98	.01	.06	<2	<2	<10	<.3	<.2	3.2	5
3250N 5750E	3.9	15.7	12.9	49.3	127	28	7	137	2.44	6.5	<5	4	30	.20	.8	.1	29	.57	.074	18	27	.50	168	.07	2	.92	.02	.06	<2	<2	41	.5	<.2	3.7	<1
3250N 5775E	2.8	20.3	10.8	66.1	39	35	12	250	3.10	4.7	<5	2	36	.31	.5	.2	21	.98	.057	15	21	.54	177	.03	3	.84	.01	.06	<2	<2	26	2.4	<.2	3.1	2
3250N 5800E	1.8	8.0	1.3	70.0	<30	5	5	299	.96	.7	<5	<1	138	.30	<.2	<.1	2	4.25	.031	<1	2	.36	271	<.01	3	.07	.02	<.01	<2	<2	49	12.4	<.2	<.5	1
3200N 5300E	.7	11.6	10.8	52.5	31	41	12	233	3.14	9.2	<5	6	14	.11	.3	.2	59	.19	.052	20	52	.51	323	.10	2	1.93	.01	.04	<2	<2	11	.6	<.2	6.0	3
3200N 5325E	.6	12.7	12.1	68.2	41	48	13	287	3.00	8.7	<5	7	12	.17	<.2	.2	49	.20	.123	20	42	.62	240	.07	2	1.75	.01	.05	<2	<2	20	<.3	<.2	4.7	17
3200N 5350E	.6	11.6	10.2	39.4	<30	33	10	220	2.36	5.7	<5	5	15	.09	<.2	.1	41	.23	.053	14	40	.46	267	.08	2	1.41	.01	.04	<2	<2	15	<.3	<.2	4.1	6
3200N 5375E	.5	10.6	14.5	36.2	<30	31	9	165	2.05	11.0	<5	6	9	.09	.2	.1	31	.14	.069	24	30	.39	228	.04	<2	1.19	<.01	.04	<2	<2	19	<.3	<.2	3.2	28
RE 3200N 5375E	.5	9.9	13.6	35.2	<30	31	9	162	2.02	12.3	<5	6	9	.09	.2	.1	31	.13	.066	24	30	.38	223	.04	2	1.17	<.01	.04	<2	<2	24	<.3	<.2	3.2	7
3200N 5400E	.4	11.6	7.4	44.9	<30	52	12	315	2.62	5.8	<5	5	13	.11	.2	.1	43	.26	.079	14	46	.81	209	.08	2	1.27	.01	.05	<2	<2	<10	<.3	<.2	3.5	1
3200N 5425E	.6	13.0	11.6	75.1	57	57	13	180	2.31	5.1	<5	5	12	.16	.3	.2	59	.20	.086	15	59	.72	213	.12	2	1.98	.01	.05	<2	<2	14	<.3	<.2	6.3	4
3200N 5450E	.9	12.0	8.7	55.2	<30	42	12	230	3.25	5.8	<5	5	12	.12	.2	.1	58	.13	.074	16	49	.56	359	.13	2	2.02	.01	.04	<2	<2	17	<.3	<.2	6.0	1
3200N 5475E	.6	14.3	10.3	116.8	37	52	14	221	2.80	6.0	<5	5	13	.24	<.2	.1	57	.18	.107	15	55	.66	293	.12	3	2.10	.01	.06	<2	<2	29	<.3	<.2	5.7	130
3200N 5500E	.5	11.9	7.2	38.6	<30	51	11	260	2.74	5.2	<5	6	14	.06	.3	.1	47	.22	.051	16	51	.70	256	.10	2	1.35	.01	.05	<2	<2	20	<.3	<.2	3.6	5
3200N 5525E	.5	12.0	7.2	40.6	<30	49	12	303	2.66	4.7	<5	5	13	.06	<.2	.1	47	.22	.067	14	47	.73	234	.10	2	1.33	.01	.05	<2	<2	11	<.3	<.2	4.2	11
3200N 5550E	.6	12.4	7.5	48.8	<30	45	12	222	3.10	5.8	<5	5	15	.09	.2	.1	59	.21	.057	14	57	.64	345	.10	2	1.81	.01	.04	<2	<2	18	<.3	<.2	5.3	3
3200N 5575E	.5	13.4	7.5	46.0	<30	50	11	263	2.75	6.6	<5	5	14	.09	.2	.1	49	.22	.077	14	47	.68	296	.10	2	1.44	.01	.05	<2	<2	19	<.3	<.2	4.2	2
3200N 5600E	.7	10.3	8.6	47.2	<30	48	12	246	2.88	6.7	<5	5	13	.09	<.2	.2	50	.20	.076	13	47	.68	279	.09	2	1.68	.01	.05	<2	<2	15	<.3	<.2	4.7	3
3200N 5625E	.7	13.7	10.1	46.7	191	71	16	299	3.77	8.9	<5	6	12	.11	.5	.2	60	.27	.086	16	67	1.27	161	.08	5	1.22	.02	.04	<2	<2	15	<.3	<.2	4.4	3
3200N 5650E	.8	6.9	10.2	96.2	63	22	10	682	2.41	3.1	<5	2	13	.35	<.2	.1	47	.26	.086	11	31	.32	315	.07	2	1.32	.01	.06	<2	<2	11	<.3	<.2	5.5	1
3200N 5675E	.7	9.3	9.1	75.2	34	45	11	408	2.72	5.2	<5	3	16	.18	.2	.1	47	.33	.116	12	43	.70	258	.09	2	1.25	.01	.06	<2	<2	<10	<.3	<.2	4.9	1
3200N 5700E	.9	8.7	8.3	41.4	59	26	7	214	2.48	6.3	<5	3	13	.09	<.2	.1	43	.21	.033	10	33	.37	173	.09	2	1.25	.01	.07	<2	<2	<10	<.3	<.2	4.5	1
3200N 5725E	.5	10.8	7.3	35.8	<30	42	12	394	2.72	6.0	<5	6	24	.03	<.2	.1	39	.45	.090	25	36	.80	217	.10	2	1.03	.02	.05	<2	<2	21	<.3	<.2	3.6	2
STANDARD D2/HG	26.6	132.4	109.9	276.0	1894	34	17	1109	4.48	79.0	25	18	61	2.34	8.7	20.6	81	.76	.108	18	60	1.22	265	.15	28	2.50	.05	.71	19	2.5	548	.4	2.2	7.2	45

Standard is STANDARD D2/HG-500/AU-S. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppb	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppb	Se ppm	Te ppm	Ga ppm	Au+ ppb
3200N 5750E	.4	7.2	5.9	34.7	<30	34	10	242	2.28	5.3	<5	5	22	.04	.2	.1	32	.45	.049	17	26	.63	129	.07	<2	.85	.02	.04	<2	<.2	22	<.3	<.2	2.5	5
3200N 5775E	1.0	13.0	5.7	40.6	46	31	11	290	2.02	4.5	<5	3	49	.09	.7	.1	23	1.98	.057	12	20	.56	156	.05	2	.62	.02	.05	<2	<.2	39	<.3	<.2	2.1	1
3200N 5800E	2.1	21.6	11.0	112.7	53	34	15	275	3.17	6.6	<5	3	48	.34	.9	.2	20	1.31	.060	12	21	.35	350	.03	3	.78	.01	.04	<2	<.2	62	7.2	<.2	2.3	1

Sample type: SOIL.

AA
LL

GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-3697 Page 1
1022 - 470 Granville St., Vancouver BC V6C 1V5AA
LL

SAMPLE#	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Au* ppb
PROFILE L3250N 5625E 15cm	14	11	57	<.3	4	96
PROFILE L3250N 5625E 30cm	12	11	46	<.3		1
PROFILE L3250N 5625E 45cm	11	8	48	<.3	<2	4
PROFILE L3250N 5625E 60cm	10	11	40	<.3	2	4
PROFILE L3250N 5625E 75cm	12	11	45	<.3	5	2
PROFILE L3250N 5625E 1m	14	8	48	<.3	2	5
PROFILE L3350N 5600E 15cm	12	10	46	<.3	<2	2
PROFILE L3350N 5600E 30cm	17	13	53	<.3	5	1
PROFILE L3350N 5600E 45cm	22	15	67	<.3	6	2
PROFILE L3350N 5600E 60cm	21	13	64	<.3	3	3
PROFILE L3350N 5600E 75cm	16	5	50	<.3	3	2
PROFILE L3350N 5600E 1m	14	6	53	<.3	4	89
PROFILE L3450N 5575E 15cm	4	11	91	<.3	<2	3
PROFILE L3450N 5575E 30cm	8	16	78	<.3	<2	7
PROFILE L3450N 5575E 45cm	16	15	54	<.3	2	1
PROFILE L3450N 5575E 60cm	16	17	61	<.3	4	2
PROFILE L3450N 5575E 75cm	15	16	55	<.3	4	1
PROFILE L3450N 5575E 1m	14	9	52	<.3	<2	2
RE PROFILE L3450N 5575E 1m	13	12	50	<.3	2	11
PROFILE L3550N 5550E 15cm	12	13	45	<.3	<2	2
PROFILE L3550N 5550E 20cm	12	11	43	<.3	<2	4
PROFILE L3550N 5550E 45cm	13	9	48	<.3	<2	1
PROFILE L3550N 5550E 60cm	20	8	46	<.3	<2	2
PROFILE L3550N 5550E 75cm	19	7	45	<.3	<2	2
PROFILE L3550N 5550E 1m	8	9	85	<.3	<2	3
PROFILE L3650N 5550E 15cm	35	15	52	<.3	<2	8
PROFILE L3650N 5550E 30cm	9	8	52	<.3	<2	4
PROFILE L3650N 5550E 45cm	8	11	38	<.3	3	3
PROFILE L3650N 5550E 60cm	10	13	48	<.3	4	1
PROFILE L3650N 5550E 75cm	11	10	47	<.3	2	1
PROFILE L3650N 5550E 1m N.S.	-	-	-	-	-	-
PROFILE L3750N 5550E 15cm	12	9	37	<.3	<2	1
PROFILE L3750N 5550E 30cm	17	10	37	<.3	<2	2
PROFILE L3750N 5550E 45cm	18	11	41	<.3	2	3
PROFILE L3750N 5550E 60cm N.S.	-	-	-	-	-	-
STANDARD C2/AU-S	59	47	142	6.6	45	41

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 12 1996

DATE REPORT MAILED: Aug 29/96

SIGNED BY: C. Leong D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

N.S. - Broken bags when received, all samples lost during shipping

SAMPLE#	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Au* ppb
PROFILE L3750N 5550E 75cm	22	11	47	<.3	9	2
PROFILE L3750N 5550E 1m	21	11	55	<.3	10	1
PROFILE L3850N 5550E 15cm	9	10	37	<.3	10	<1
PROFILE L3850N 5550E 30cm	9	7	37	<.3	11	1
PROFILE L3850N 5550E 45cm	15	14	39	<.3	7	3
PROFILE L3850N 5550E 60cm	30	9	65	<.3	11	2
PROFILE L3950N 5550E 15cm	10	8	37	<.3	9	1
PROFILE L3950N 5550E 30cm	10	6	38	<.3	8	1
PROFILE L3950N 5550E 45cm	12	8	41	<.3	8	2
PROFILE L3950N 5550E 60cm	24	13	58	<.3	9	3
PROFILE L3950N 5550E 75cm	26	9	58	<.3	11	2
PROFILE L3950N 5550E 1m	22	12	55	<.3	9	4
RE PROFILE L4050N 5575E 15cm	11	9	59	<.3	9	<1
PROFILE L4050N 5575E 15cm	10	8	60	<.3	8	1
PROFILE L4050N 5575E 30cm	12	8	48	<.3	11	1
PROFILE L4050N 5575E 45cm	12	9	46	<.3	13	1
PROFILE L4050N 5575E 60cm	10	4	51	<.3	9	1
PROFILE L4050N 5575E 75cm	23	10	56	<.3	9	2
PROFILE L4050N 5575E 1m	30	12	70	<.3	8	5
PROFILE L4150N 5600E 15cm	10	8	56	<.3	10	1
PROFILE L4150N 5600E 30cm	9	6	49	<.3	10	1
PROFILE L4150N 5600E 45cm	16	8	49	<.3	6	1
PROFILE L4150N 5600E 60cm	29	15	66	<.3	8	7
STANDARD C2/AU-S	56	39	132	6.0	42	43

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

AA
LL

GEOCHEMICAL ANALYSIS CERTIFICATE

KRL Resources Corp. File # 96-5667

1022 - 470 Granville St., Vancouver BC V6C 1V5

AA
LL

SAMPLE#	Cu ppm	Zn ppm	Ni ppm	Co ppm	As ppm	Cd ppm	Au* ppb
TR-1-02	16	18	17	8	5	<.2	7
TR-1-03	27	19	23	11	4	.3	1
TR-1-04	8	13	11	5	4	.3	<1
TR-2-01	17	65	23	11	12	.2	<1
TR-3-02	4	1	4	<1	<2	<.2	1
TR-3-03	79	26	11	6	43	<.2	2
TR-4-01	18	19	23	8	13	.2	2
TR-4-02	25	15	20	13	18	<.2	1
TR-4-03	7	16	9	3	<2	<.2	1
RE TR-4-03	8	16	9	3	<2	<.2	<1
TR-4-04	26	12	16	13	9	<.2	<1
TR-4-05	4	28	23	12	23	1.5	<1
TR-4-06	6	31	15	3	6	.5	<1
STANDARD C2/AU-R	58	142	73	37	44	19.8	460

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB

- SAMPLE TYPE: ROCK AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.(10 GM)

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 30 1996

DATE REPORT MAILED:

Nov 7/96

SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



GEOCHEMICAL ANALYSIS CERTIFICATE



KRL Resources Corp. PROJECT WATSON File # 96-5596 Page 1
1022 - 470 Granville St., Vancouver BC V6C 1V5

SAMPLE#	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Hg ppm	Au* ppb
TR-4-07	11	6	18	<.3	8	<1	<1
TR-4-08	20	<3	27	<.3	15	<1	<1
TR-4-09	21	4	28	<.3	9	<1	<1
TR-4-10	18	5	45	<.3	7	<1	<1
TR-4-11	24	8	166	<.3	10	<1	<1
TR-4-12	94	30	130	.5	15	<1	2
TR-4-13	46	27	79	.3	14	<1	1
TR-4-14	64	22	48	.5	14	<1	2
TR-4-15	132	17	31	.6	13	<1	9
TR-4-16	124	18	25	.5	11	<1	9
TR-4-17	136	20	26	.6	11	<1	8
RE TR-4-17	129	24	26	.6	11	<1	8
TR-4-18	101	18	42	<.3	11	<1	7
TR-4-19	28	14	59	<.3	8	<1	1
YLC-01	43	109	156	.5	50	<1	6
YLC-02	129	620	291	1.3	66	<1	4
BR-01	43	19	72	<.3	4	<1	1
STANDARD C2/AU-R	62	40	149	7.0	44	2	459

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: P1 ROCK P2 SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.(10 GM)
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: OCT 28 1996 DATE REPORT MAILED: Nov 5/96 SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Hg ppm	Au* ppb
TR-1-01	27	13	87	<.3	6	<1	2
TR-3-01	39	15	91	<.3	6	<1	5
RE TR-3-01	37	13	87	<.3	7	<1	2

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL LABORATORIES LTD.

852 E. Hastings St. Vancouver, B.C. Canada V6A 1R6

Phone: (604) 253-3158 Fax: (604) 253-1716

Toll Free: 1-800-990-ACME E-Mail: acme_labs@minklink.bc.ca

METHOD FOR WET GEOCHEM GOLD ANALYSIS

Sample Preparation

Soils and sediments are dried(60 deg. C) and sieve to -80 mesh.

Rocks and cores are crushed and pulverized to -100 mesh.

Sample digestion

1. 10g samples in 250 ml beaker, ignite at 600 deg. C for four hours.
2. Add 40 ml of 3:1:2 mixture HCL:HNO₃:H₂O .
3. Cover beaker with lids.
4. Boil in hot water bath for one hour.
5. Swirl samples 2 to 3 times within the hour.
6. Cool, add 60 ml of distilled water and settle.
7. Pour 50 ml of leached solution using a graduated cylinder into 100ml volumetric flask.
8. Add 10 ml of MIBK and 25 ml of distilled water.
9. Shake 3 to 4 mins in shaker.
10. Add additional 25 ml of distilled water to stripe out excess iron.
11. Shake each flask 10 times.
12. Pour MIBK into container for graphite AA finished.



ACME ANALYTICAL LABORATORIES LTD.

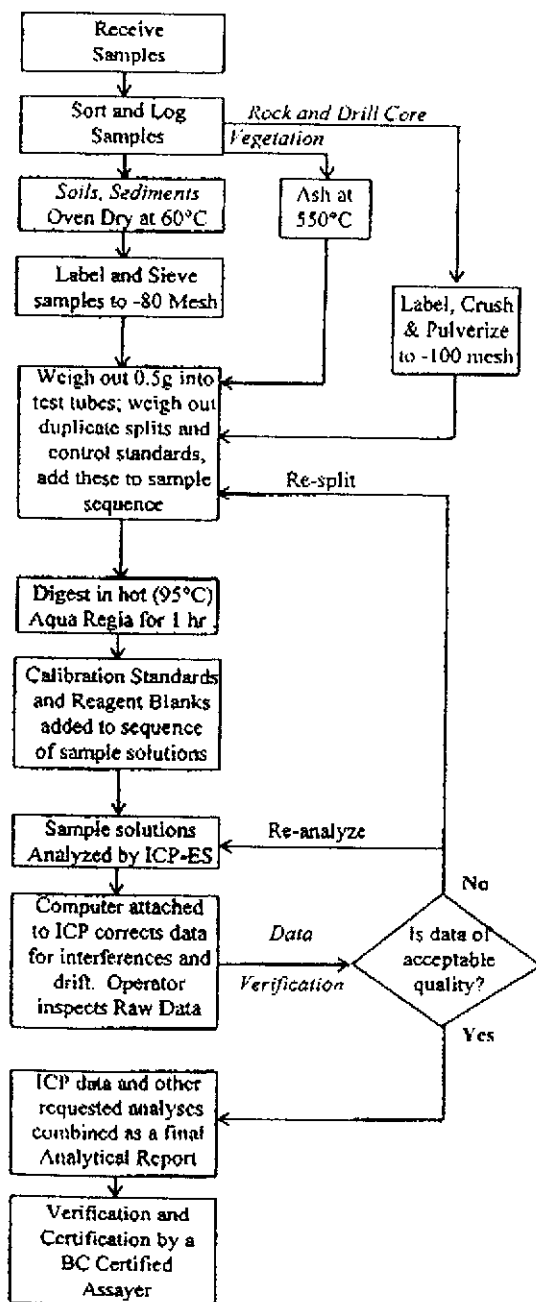
Assaying & Trace Analysis

852 E. Hastings St., Vancouver, B.C., Canada V6A 1R6

Telephone: (604) 253-3158 Fax: (604) 253-1716

METHODS AND SPECIFICATIONS FOR ANALYTICAL PACKAGE GROUP 1D - 30 ELEMENT ICP BY AQUA REGIA

Analytical Process



Comments

Sample Preparation

Soils and sediments are dried (60°C) and sieved to -80 mesh (-177 microns), rocks and drill core are crushed and pulverized to -100 mesh (-150 microns). Plant samples are dried (60°C) and pulverized or dry ashed (550°C). Moss-mat samples are dried (60°C), pounded to loosen trapped sediment then sieved to -80 mesh. At the clients request, moss mats can be ashed at 550°C then sieved to -80 mesh although this can result in the potential loss by volatilization of Hg, As, Sb, Bi and Cr. A 0.5 g split from each sample is placed in a test tube. A duplicate split is taken from 1 sample in each batch of 34 samples for monitoring precision. A sample standard is added to each batch of samples to monitor accuracy.

Sample Digestion

Aqua Regia is a 3:1:2 mixture of ACS grade conc. HCl, conc. HNO₃ and demineralized H₂O. Aqua Regia is added to each sample and to the empty reagent blank test tube in each batch of samples. Sample solutions are heated for 1 hr in a boiling hot water bath (95°C).

Sample Analysis

Sample solutions are aspirated into and ICP emission spectrograph (Jarrel Ash AtomComp model 800 or 975) for the determination of 30 elements comprising: Ag, Al, As, Au, B, Ba, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sr, Th, Ti, U, V, W, Zn.

Data Evaluation

Raw and final data from the ICP-ES undergoes a final verification by a British Columbia Certified Assayer who then signs the Analytical Report before it is released to the client. Chief Assayer is Clarence Leong, other certified assayers are Dean Toye and Jacky Wang.

APPENDIX D

1996 Liard Canyon Claims Cost Statement

(A) Costs Attributed to the Following Claims:

Liard 1-28, Watson 1-30, Steph 1-6, Lee 1-10, Luck 1-10 (84 claims)

<u>Item</u>	<u>Cost</u>	<u>Cost/Claim</u>
Airborne Geophysics (Magnetics & VLF-EM) } (March, 1996) 177 line km @ \$29.50/km	5221.50	62.16
Travel to Property 4 people @ \$180/day	720.00	8.57
Vehicle Rental } (June 7-8, 1996) 2 days @ \$80/day + 2036 km @ \$0.30/km	770.80	9.18
Gas	<u>550.00</u>	<u>6.55</u>
Total:	7262.30	86.46

(B) Costs Attributed to the Following Claims: (June 7-21, 1996)

Watson 12,14-20, 23-30, Lee 8,10 (18 claims)

<u>Item</u>	<u>Cost</u>	<u>Cost/Claim</u>
Grid Layout 16 person days @ \$200/day	3200.00	177.78
Line Cutting 10 person days @ \$200/day	2000.00	111.11
Helipad, trail construction 2 days @ \$150/day	300.00	16.67
Ground Geophysics 3 days @ \$250/day	750.00	41.67
Soil Sampling 4 person days @ \$180/day	720.00	40.00
Soil Analyses 139 samples @ \$15.29/sample	2125.31	118.07
Supervision 2 days @ \$330/day	660.00	36.67
Room & Board 37 person days @ \$75/day	2775.00	154.17
Helicopter support	450.00	25.00
Boat rental 13 days @ \$35/day	455.00	25.28
Vehicle rental 15 days @ \$80/day	<u>1200.00</u>	<u>66.67</u>
Total:	14635.31	813.07

③ **Costs Attributed to the Following Claims:** (June 20-21, 1996)
Lee 9, Watson 10, 19, 21, 26-28, 30 (8 claims)

<u>Item</u>	<u>Cost</u>	<u>Cost/Claim</u>
Prospecting		
2 days @ \$200/day	400.00	50.00
Analyses		
11 rock samples @ \$19.45/sample (30 element ICP + Au)	213.95	26.74
Room & Board		
2 days @ \$75/day	<u>150.00</u>	<u>18.75</u>
Total:	763.95	95.49

④ **Costs Attributed to the Following Claims:** (August 3-9, 1996)
Watson 23-26, 29, 30, Lee 10 (7 claims)

<u>Item</u>	<u>Cost</u>	<u>Cost/Claim</u>
Soil Sampling		
12 person days @ \$180/day	2160.00	308.57
Soil Analyses		
411 samples @ \$15.29/sample		
+ 54 samples @ \$6.50/sample	6635.19	947.88
Room & Board		
12 person days @ \$75/day	900.00	128.57
Helicopter support		
6 days \$450/day	2700.00	385.71
Vehicle rental		
7 days @ \$80/day	<u>560.00</u>	<u>80.00</u>
Total:	12955.19	1850.74

⑤ **Costs Attributed to the Following Claims:** (October 17-24, 1996)
Watson 16, 18, 23, 25, 26, 29, 30, Lee 10 (8 claims)

<u>Item</u>	<u>Cost</u>	<u>Cost/Claim</u>
Trenching, Trail Construction		
46 hrs. @ \$135/hr. + 2 hrs. @ \$120/hr.	6450.00	806.25
Supervision, Sampling		
7 days @ \$300/day + 7 days @ \$125/day	2975.00	371.88
Analyses		
42 samples @ \$14.30/sample (6 element ICP + Au)	604.00	75.50
Helicopter support		
7 days @ \$561/day	3928.00	491.00
Accommodation / Meals		
16 person days @ \$100/day	1600.00	200.00
Travel Costs		
2 persons, return airfare Vancouver-Whitehorse	<u>1526.00</u>	<u>190.75</u>
Total:	17083.00	2135.38

Grand Total: 52699.75

HEAD OFFICE:

2115-129TH ST.

SURREY, B.C.

V4A-8H6

TEL: (604) 538-4542

FAX: (604) 538-7798

JEDWAY ENTERPRISES LTD.

BRANCH OFFICE

BOX 332

WATSON LAKE, Y.T.

VOA-1C0

TEL: (403) 536-2611

FAX: (403) 536-2617

I N V O I C E

October 29, 1996

KRL Resources Corp.
Suite 1022 - 470 Granville Street
Vancouver, B.C., V6C 1V5

Re: LS3400 Linkbelt Excavator
Trenching - Chames
October 18 - 24, 1996

October 18 -	6 Hours
" 19 -	7 "
" 20 -	6 "
" 21	7 "
" 22	6.5 "
" 23	6 "
" 24	<u>7.5 "</u>

46 Hours @ \$135.00 =

\$6,210.00

2 Hours trucking excavator Watson Lake - Upper Liard &
return to Watson Lake @ \$120.00 per hour =

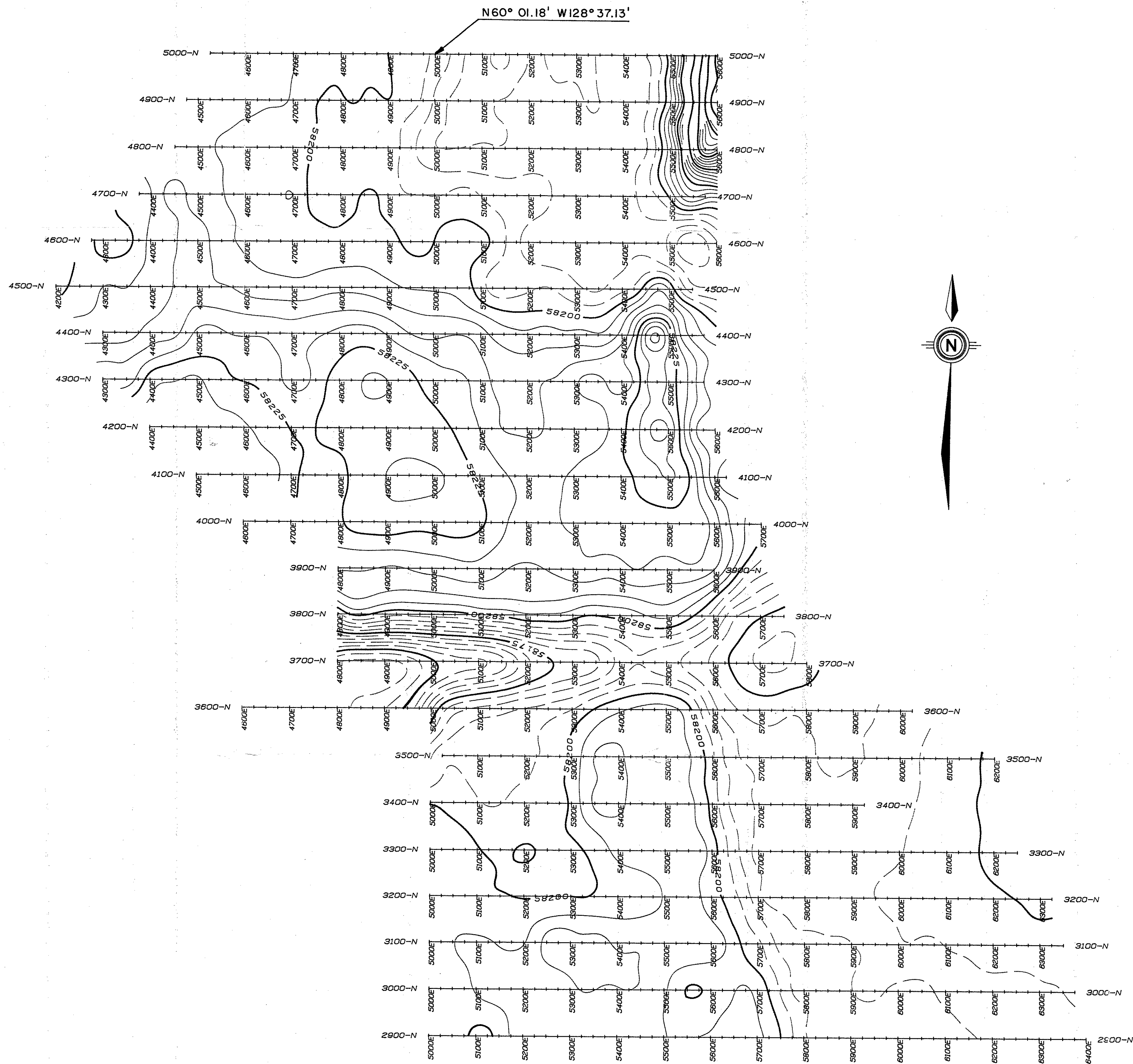
7% G.S.T. #102621455

TOTAL

240.00
<u>\$6,450.00</u>
<u>451.50</u>
\$6,901.50

RECEIVED NOV 1 1996





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DWG ①

KRL RESOURCES CORP.

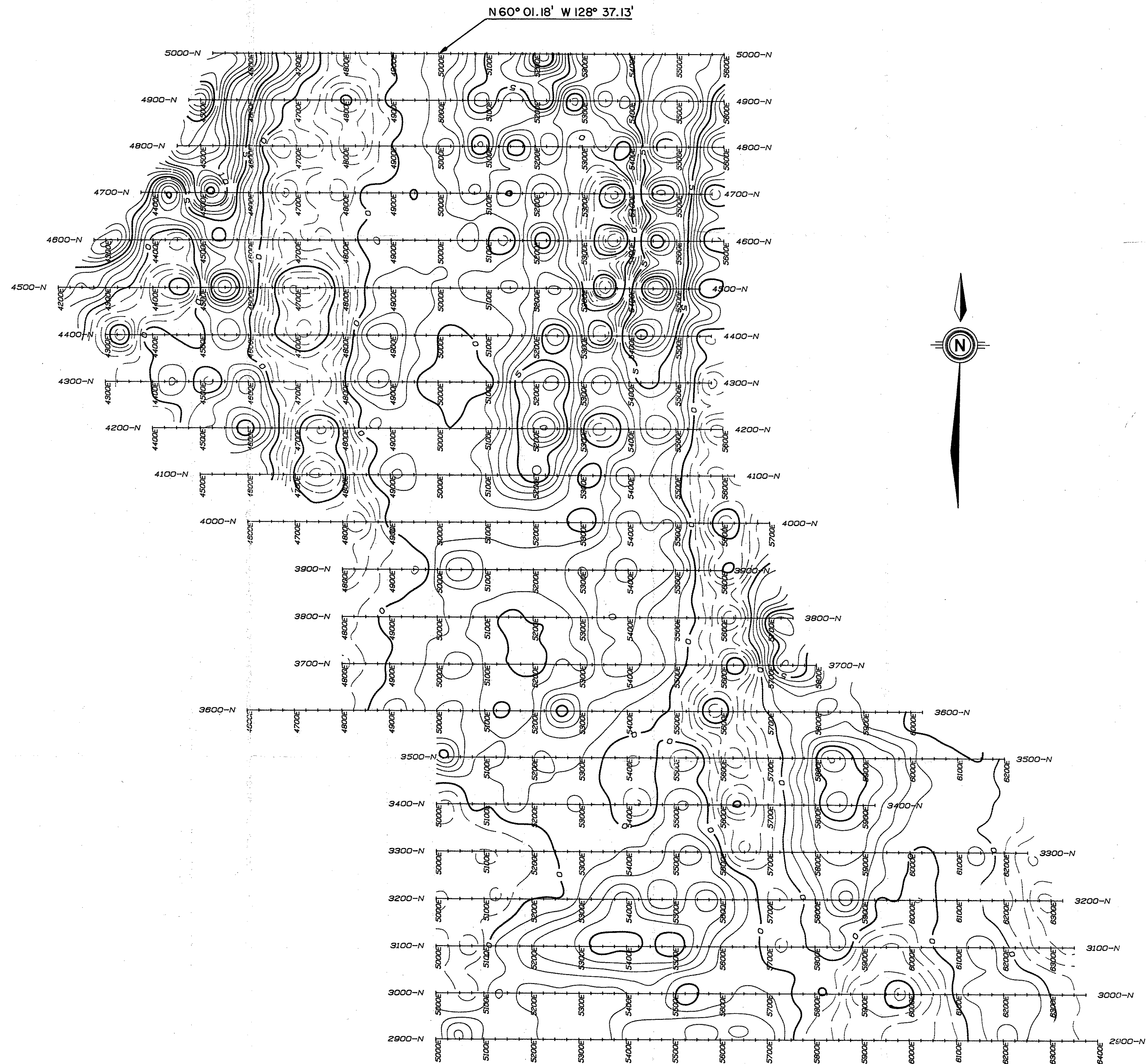
LIARD CANYON, Y.T.

TOTAL MAGNETIC FIELD
CONTINUED UPWARD 20 M
CONTOUR INTERVAL 5 nT

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED	N.T.S	DATE	FIG. NO
F. Syberg		JULY, 1996	5



093739

Dwg 2

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

VLF-EM 21.4 kHz QUADRATURE

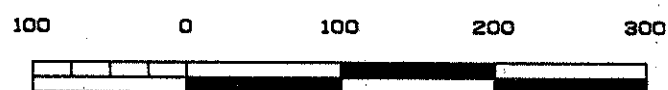
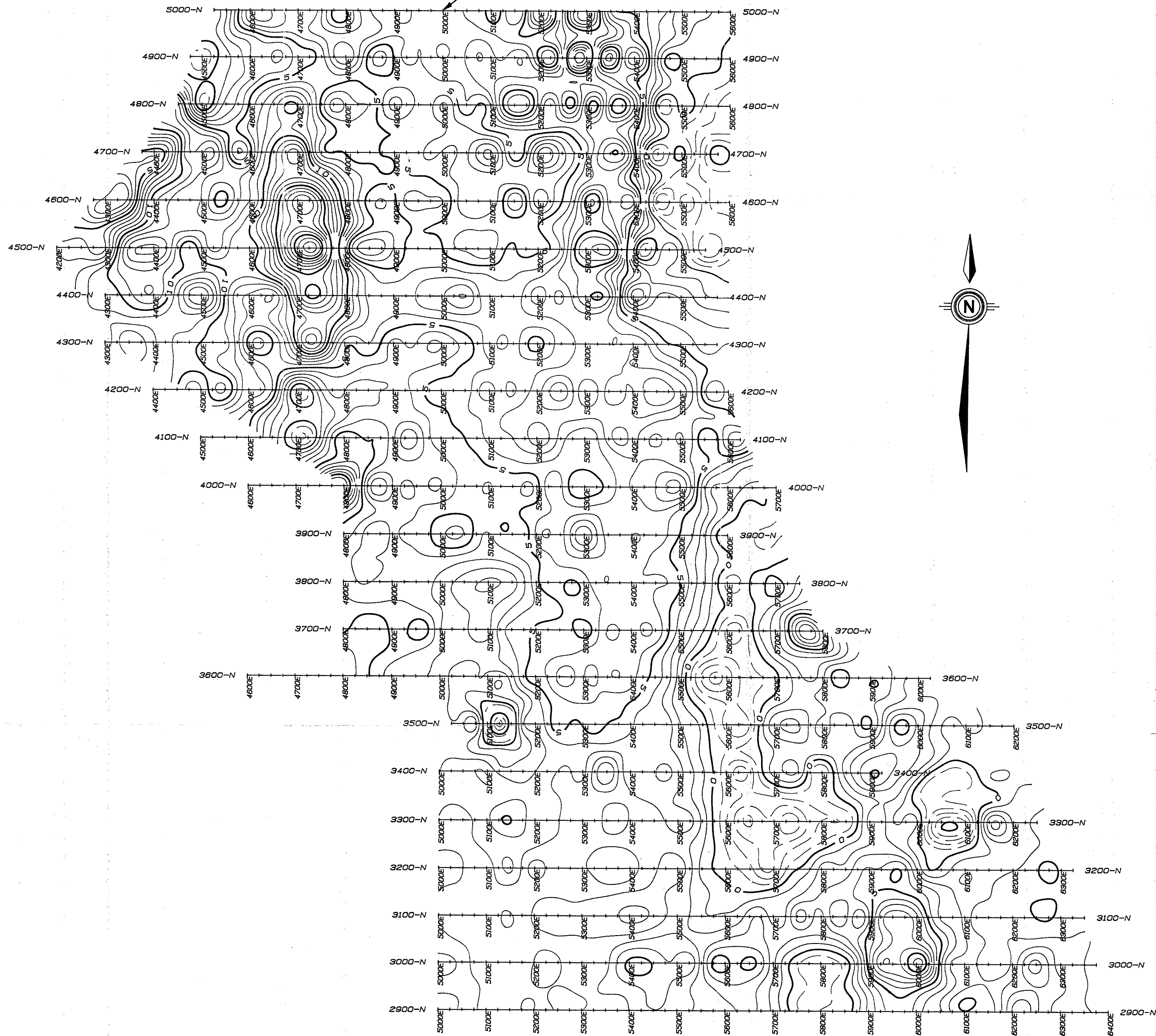
CONTOUR INTERVAL 1.0%

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED F. Syberg	N.T.S.	DATE JULY, 1986	FIG. NO 6
-----------------------	--------	--------------------	--------------

N 60° 01.18' W 128° 37.13'



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Dwg 3

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

VLF-EM 21.4 kHz DIP ANGLE

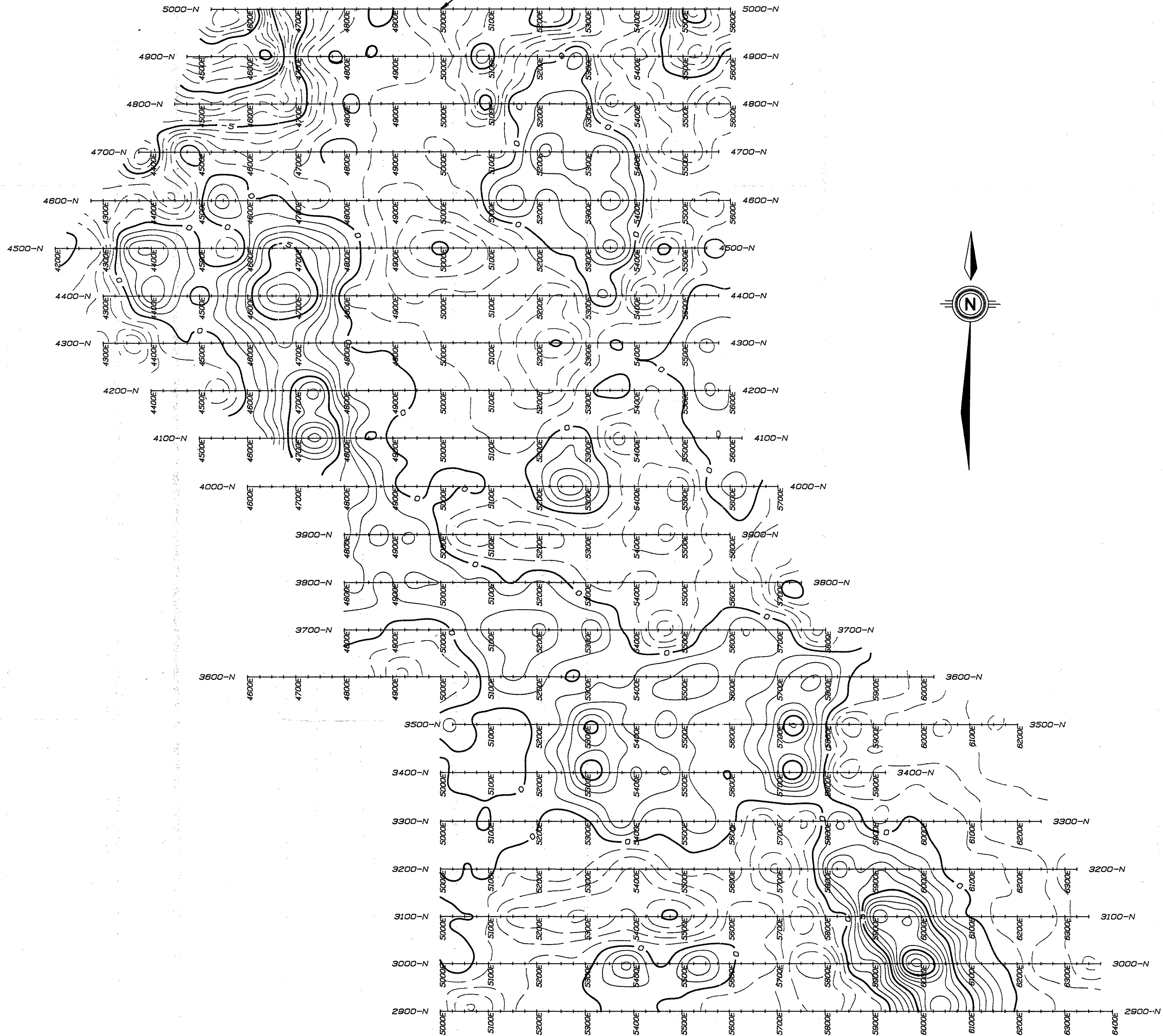
CONTOUR INTERVAL 1.0°

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED F. Syberg	N.T.S	DATE JULY, 1996	FIG. NO 7
-----------------------	-------	--------------------	--------------

N60° 01.18' W128° 37.13'



093739

Dwg ④

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

VLF-EM 24 KHz QUADRATURE

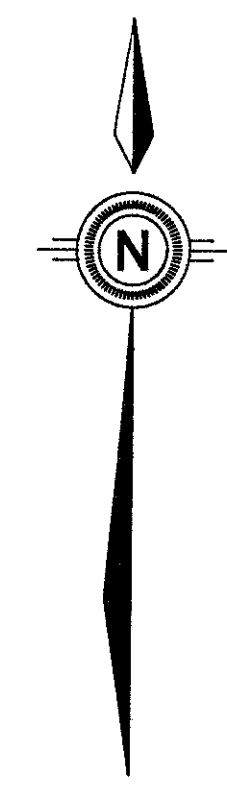
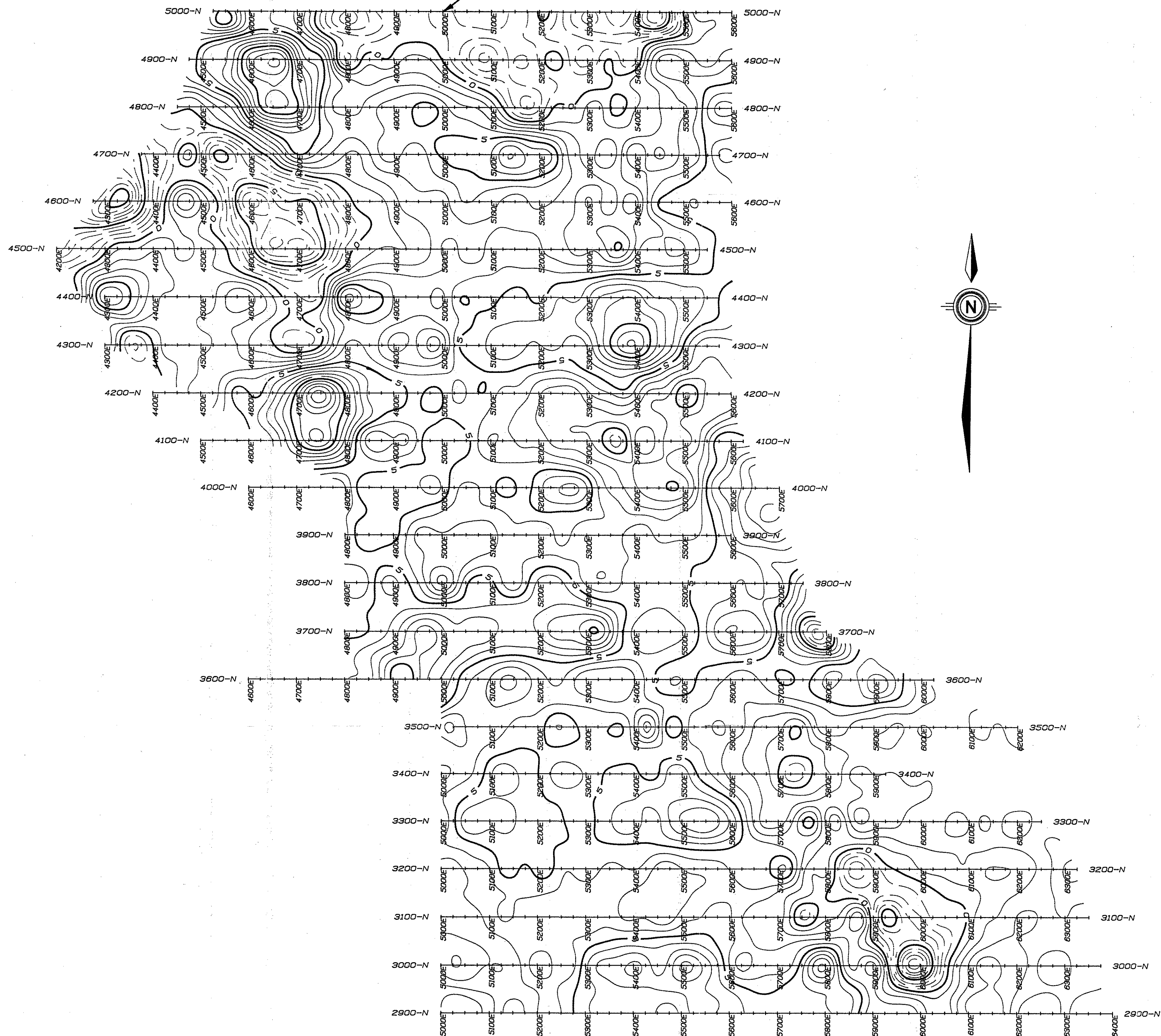
CONTOUR INTERVAL 1.0 %

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED	N.T.S	DATE	FIG. NO
F. Syberg		JULY, 1996	8

N60°01.18' W128°37.13'



093739

Dwg 5

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

VLf-EM 24 KHz DIP ANGLE

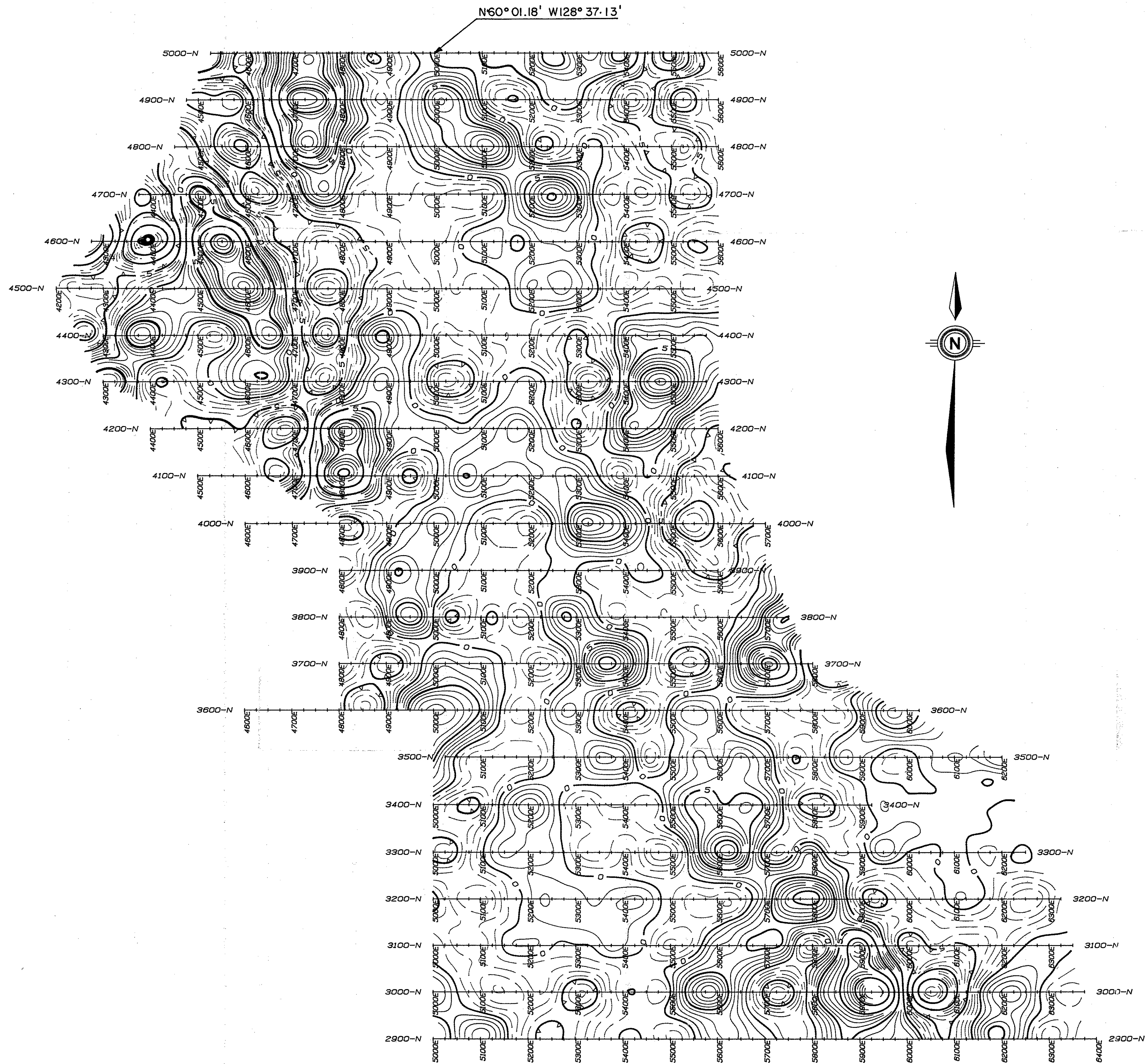
CONTOUR INTERVAL 1.0°

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED	N.T.S	DATE	FIG. NO
F. Syberg		JULY, 1996	9

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DWG (6)

KRL RESOURCES CORP.

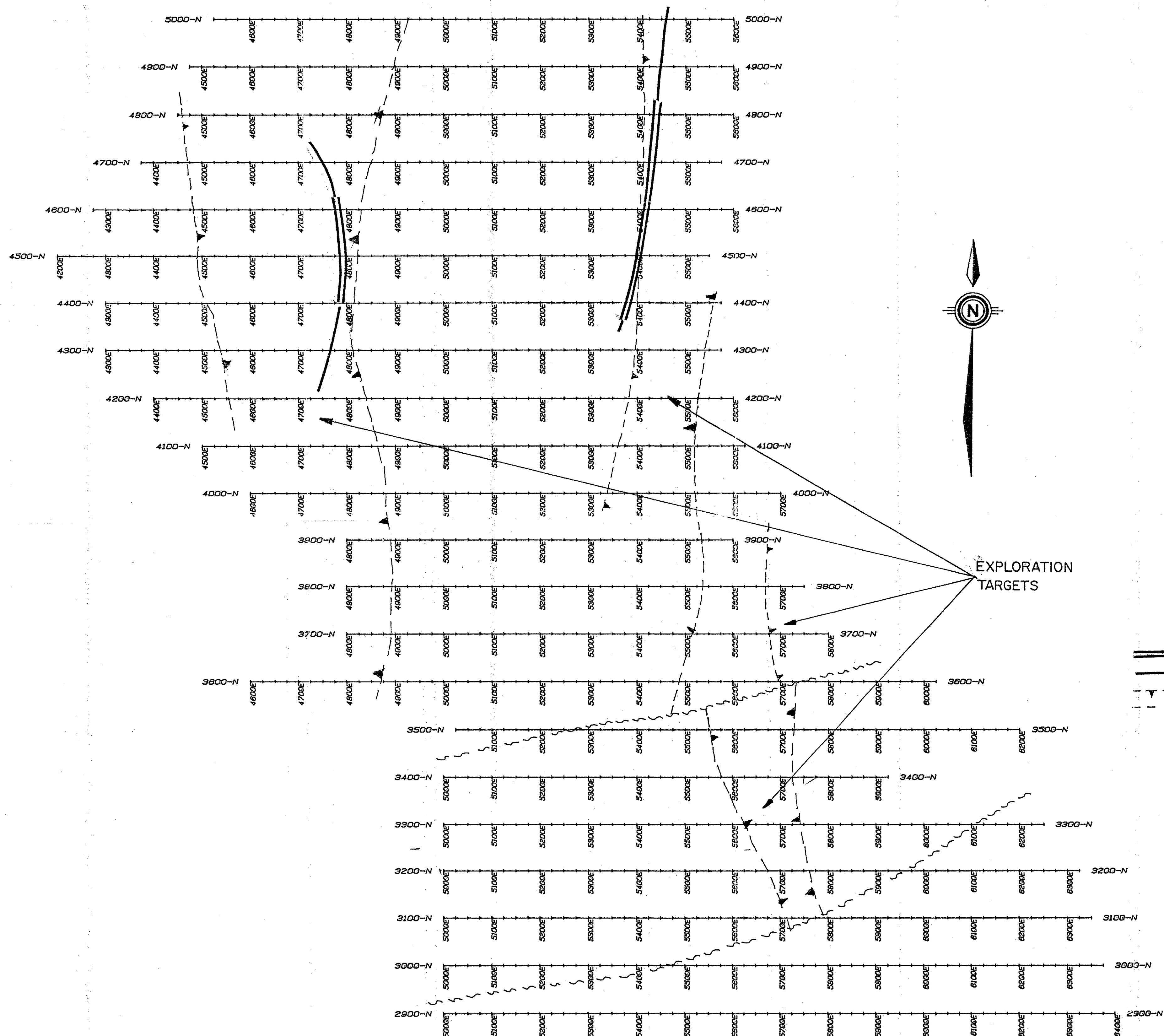
LIARD CANYON, Y.T.

VLF-EM 24 kHz DIP ANGLE
FRASER FILTERED
CONTOUR INTERVAL 1.0°

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED	N.T.S.	DATE	FIG. NO
F. Syberg		JULY, 1996	10



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- === STRONG CONDUCTOR
 --- WEAK CONDUCTOR
 ▲ EXPLORATION TARGETS

DWG 7

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

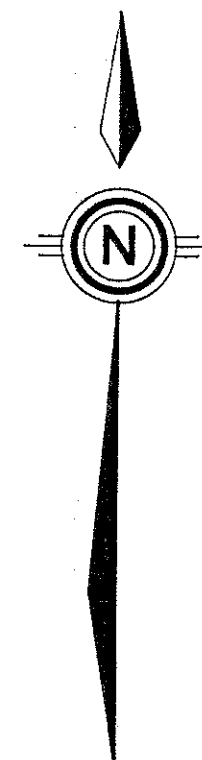
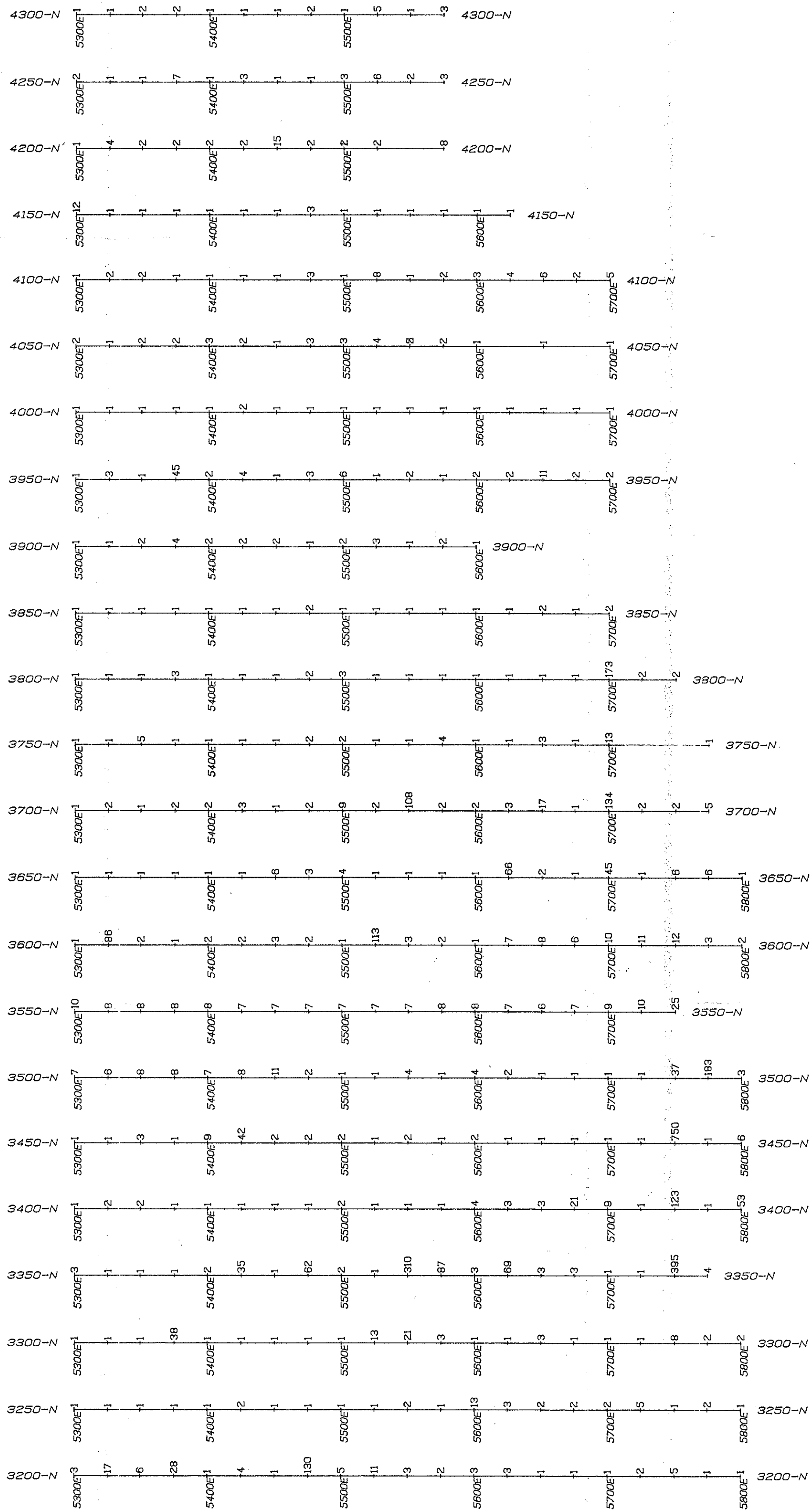
GEOPHYSICAL INTERPRETATION

LIARD CANYON, YUKON TERRITORY

DONEGAL DEVELOPMENTS LTD

COMPILED	N.T.S.	DATE	FIG. NO
F. Syberg		JULY, 1966	11

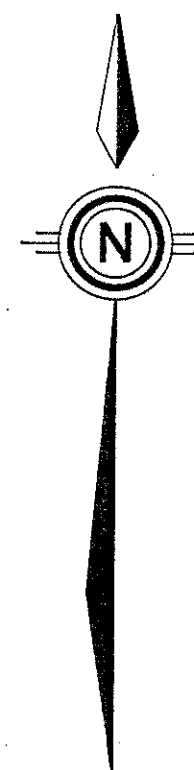
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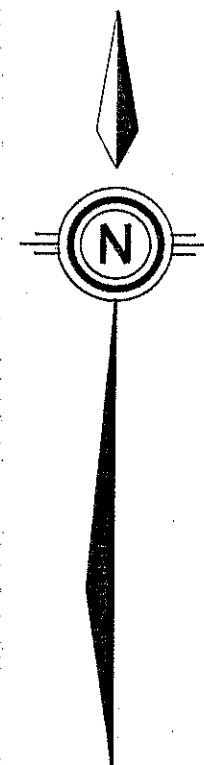
Dwg 8

KRL RESOURCES CORP.			
LIARD CANYON, Y.T.			
SOIL SAMPLE ANALYSIS			
Au ppb			
LIARD RIVER, YUKON TERRITORY.			
DONEGAL DEVELOPMENTS LTD.			
COMPILED	N.T.S.	DATE	FIG. NO.
F. Syberg	105A/2	AUG., 1996.	12



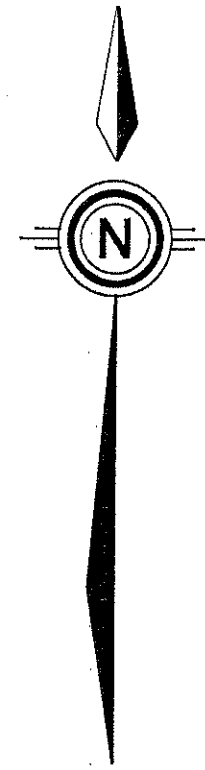
Dw6 ⑨

13



Dwtg (10)

4300-N	5300E 35.3	5300E 41.1	5300E 35.4	5300E 38.9	4300-N
4250-N	5300E 43.4	5300E 35.9	5300E 41.1	5300E 36.7	4250-N
4200-N	5300E 44.4	5300E 43.2	5300E 37.9	5300E 35.9	4200-N
4150-N	5300E 40.4	5300E 36.7	5300E 41.2	5300E 32.2	4150-N
4100-N	5300E 35.9	5300E 44.8	5300E 41.1	5300E 35.5	4100-N
4050-N	5300E 37.1	5300E 43.7	5300E 38.3	5300E 42.7	4050-N
4000-N	5300E 41.4	5300E 41.0	5300E 38.8	5300E 47.1	4000-N
3950-N	5300E 48.0	5300E 64.2	5300E 28.2	5300E 36.9	3950-N
3900-N	5300E 45.2	5300E 38.1	5300E 31.1	5300E 33.5	3900-N
3850-N	5300E 45.4	5300E 67.3	5300E 34.1	5300E 30.3	3850-N
3800-N	5300E 39.6	5300E 42.0	5300E 41.8	5300E 41.6	3800-N
3750-N	5300E 43.7	5300E 38.5	5300E 42.9	5300E 46.6	3750-N
3700-N	5300E 53.8	5300E 44.1	5300E 58.5	5300E 40.7	3700-N
3650-N	5300E 40.0	5300E 40.9	5300E 48.5	5300E 47.1	3650-N
3600-N	5300E 45.0	5300E 46.5	5300E 46.6	5300E 39.7	3600-N
3550-N	5300E 47.5	5300E 51.2	5300E 41.9	5300E 40.2	3550-N
3500-N	5300E 46.6	5300E 39.0	5300E 41.9	5300E 43.5	3500-N
3450-N	5300E 38.8	5300E 37.4	5300E 39.2	5300E 41.5	3450-N
3400-N	5300E 45.4	5300E 37.8	5300E 40.5	5300E 37.7	3400-N
3350-N	5300E 61.0	5300E 47.0	5300E 36.6	5300E 50.3	3350-N
3300-N	5300E 36.9	5300E 46.1	5300E 40.7	5300E 56.7	3300-N
3250-N	5300E 41.6	5300E 41.2	5300E 37.0	5300E 32.5	3250-N
3200-N	5300E 52.5	5300E 69.2	5300E 39.4	5300E 36.2	3200-N
5400E 44.9	5400E 52.4	5400E 59.5	5400E 52.6	5400E 36.9	5400E 44.9
5400E 38.7	5400E 45.1	5400E 39.1	5400E 51.6	5400E 40.4	5400E 38.7
5400E 39.7	5400E 42.9	5400E 40.3	5400E 42.2	5400E 37.5	5400E 39.7
5400E 41.2	5400E 38.3	5400E 41.8	5400E 36.0	5400E 42.2	5400E 41.2
5400E 45.3	5400E 39.7	5400E 48.6	5400E 39.9	5400E 42.6	5400E 45.3
5400E 33.0	5400E 36.8	5400E 37.1	5400E 37.5	5400E 41.5	5400E 33.0
5400E 38.0	5400E 38.1	5400E 38.1	5400E 38.1	5400E 41.4	5400E 38.0
5400E 48.6	5400E 48.6	5400E 48.6	5400E 48.6	5400E 48.6	5400E 48.6
5400E 34.9	5400E 34.9	5400E 34.9	5400E 34.9	5400E 34.9	5400E 34.9
5400E 43.5	5400E 43.5	5400E 43.5	5400E 43.5	5400E 43.5	5400E 43.5
5400E 42.3	5400E 42.3	5400E 42.3	5400E 42.3	5400E 42.3	5400E 42.3
5400E 49.1	5400E 49.1	5400E 49.1	5400E 49.1	5400E 49.1	5400E 49.1
5400E 58.4	5400E 58.4	5400E 58.4	5400E 58.4	5400E 58.4	5400E 58.4
5400E 40.3	5400E 40.3	5400E 40.3	5400E 40.3	5400E 40.3	5400E 40.3
5400E 61.3	5400E 61.3	5400E 61.3	5400E 61.3	5400E 61.3	5400E 61.3
5400E 41.1	5400E 41.1	5400E 41.1	5400E 41.1	5400E 41.1	5400E 41.1
5400E 36.9	5400E 36.9	5400E 36.9	5400E 36.9	5400E 36.9	5400E 36.9
5400E 50.6	5400E 50.6	5400E 50.6	5400E 50.6	5400E 50.6	5400E 50.6
5400E 43.1	5400E 43.1	5400E 43.1	5400E 43.1	5400E 43.1	5400E 43.1
5400E 36.8	5400E 36.8	5400E 36.8	5400E 36.8	5400E 36.8	5400E 36.8
5400E 38.0	5400E 38.0	5400E 38.0	5400E 38.0	5400E 38.0	5400E 38.0
5400E 44.9	5400E 44.9	5400E 44.9	5400E 44.9	5400E 44.9	5400E 44.9
5400E 53.8	5400E 53.8	5400E 53.8	5400E 53.8	5400E 53.8	5400E 53.8
5400E 25.6	5400E 25.6	5400E 25.6	5400E 25.6	5400E 25.6	5400E 25.6
5400E 9.0	5400E 9.0	5400E 9.0	5400E 9.0	5400E 9.0	5400E 9.0
5400E 33.8	5400E 33.8	5400E 33.8	5400E 33.8	5400E 33.8	5400E 33.8
5400E 97.6	5400E 97.6	5400E 97.6	5400E 97.6	5400E 97.6	5400E 97.6
5700E 41.4	5700E 39.7	5700E 37.1	5700E 49.3	5700E 40.6	5700E 41.4
5700E 53.8	5700E 53.8	5700E 53.8	5700E 53.8	5700E 53.8	5700E 53.8
5700E 70.0	5700E 70.0	5700E 70.0	5700E 70.0	5700E 70.0	5700E 70.0
5700E 112.7	5700E 112.7	5700E 112.7	5700E 112.7	5700E 112.7	5700E 112.7



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Dwg 11

KRL RESOURCES CORP.

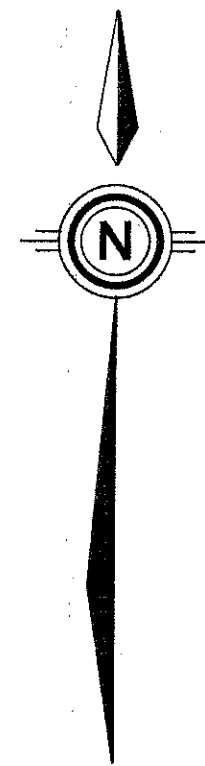
LIARD CANYON, Y.T.
SOIL SAMPLE ANALYSIS
Zn ppm

LIARD RIVER, YUKON TERRITORY.
DONEGAL DEVELOPMENTS LTD.

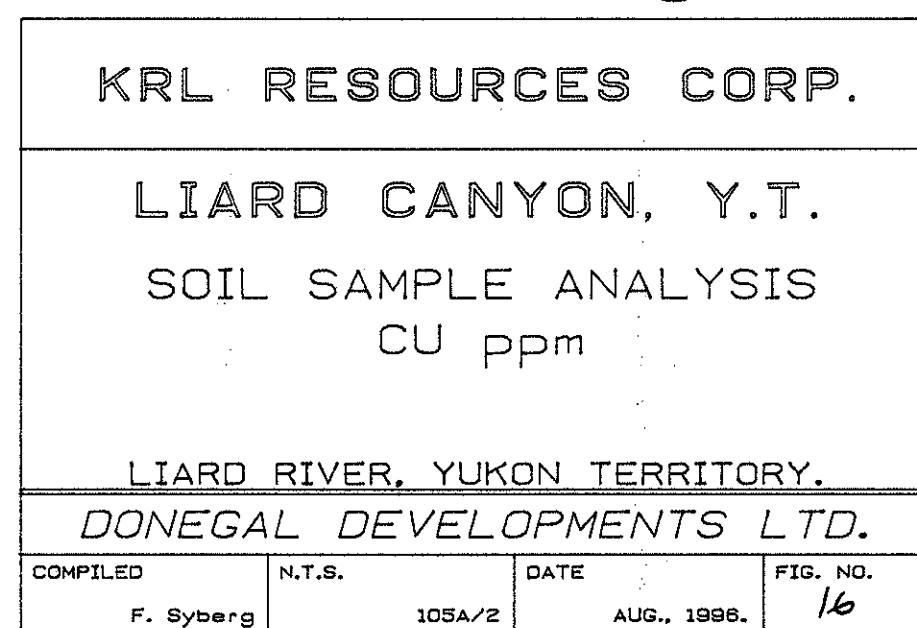
COMPILED	N.T.S.	DATE	FIG. NO.
F. Syberg	105A/2	AUG., 1996.	15

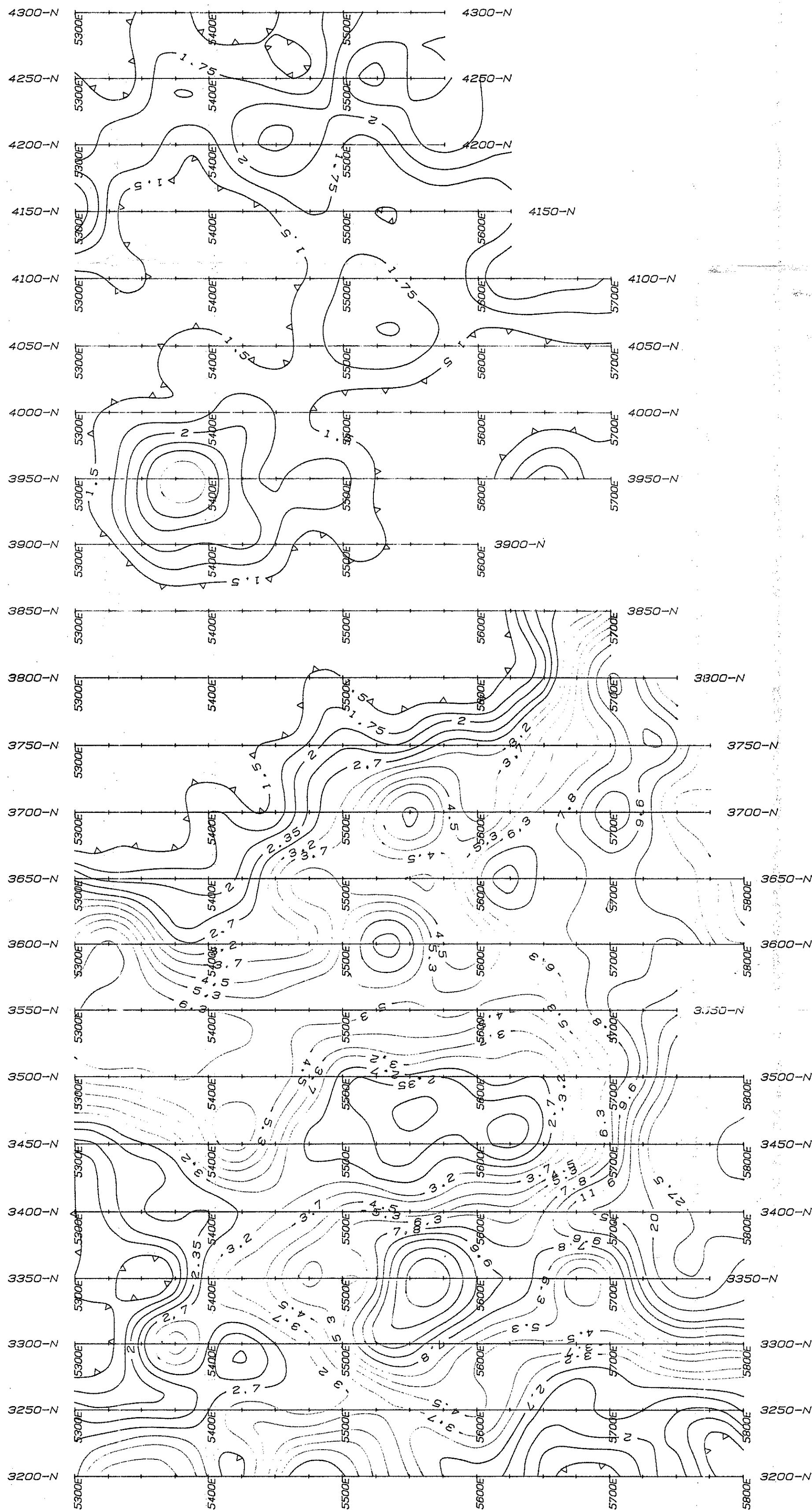
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Dw 4 (12)





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DWG 14

KRL RESOURCES CORP.

LIARD CANYON, Y.T.

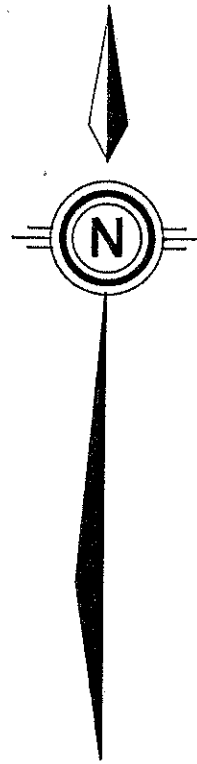
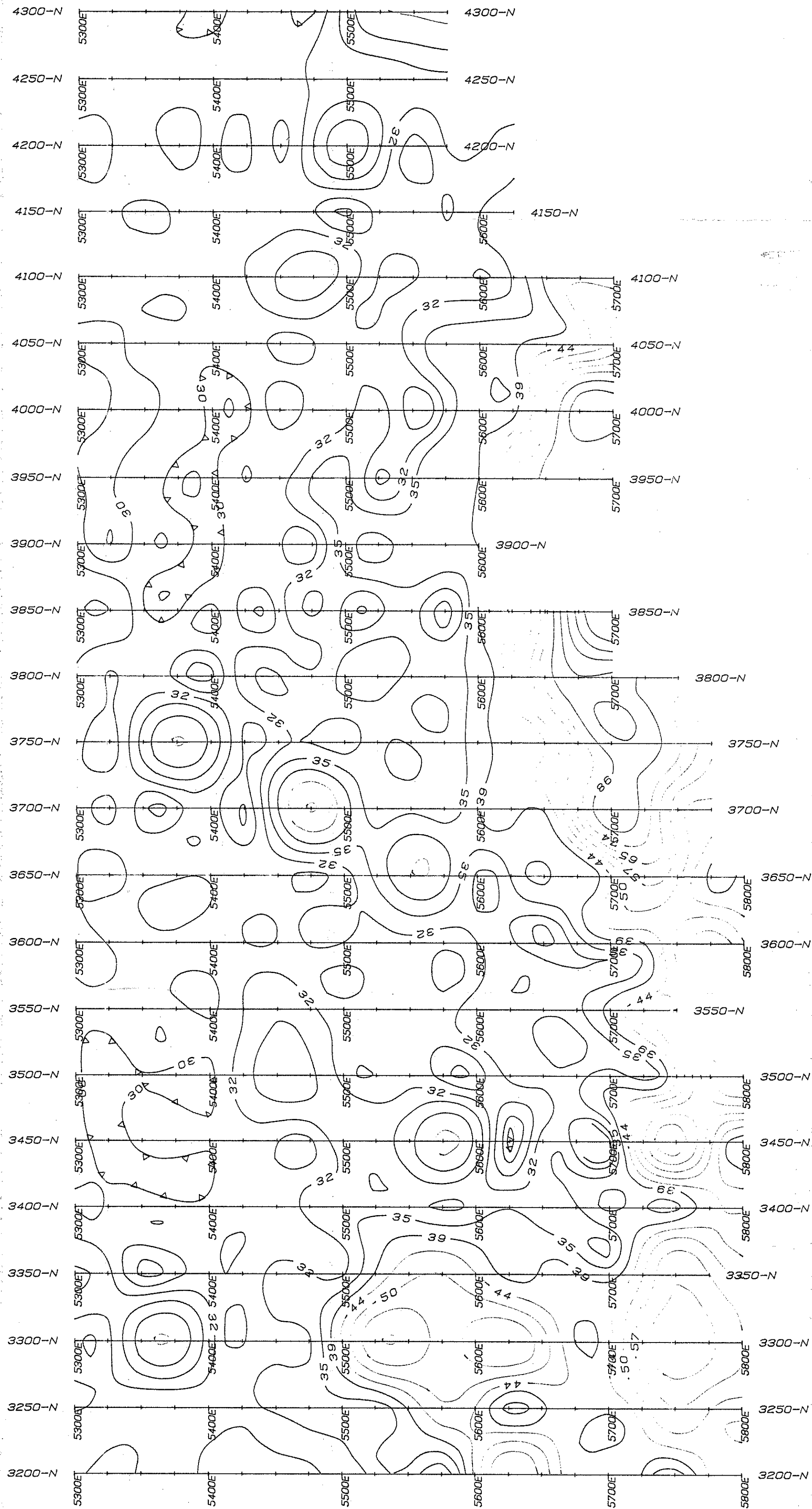
SOIL SAMPLE ANALYSIS
Au ppb

LIARD RIVER, YUKON TERRITORY.

DONEGAL DEVELOPMENTS LTD.

COMPILED F. Syberg	N.T.S. 105A/2	DATE AUG., 1998.	FIG. NO. 18
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Dwg 15

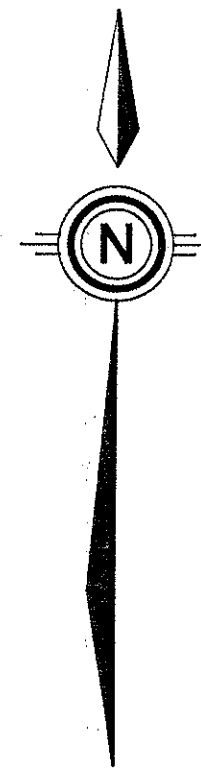
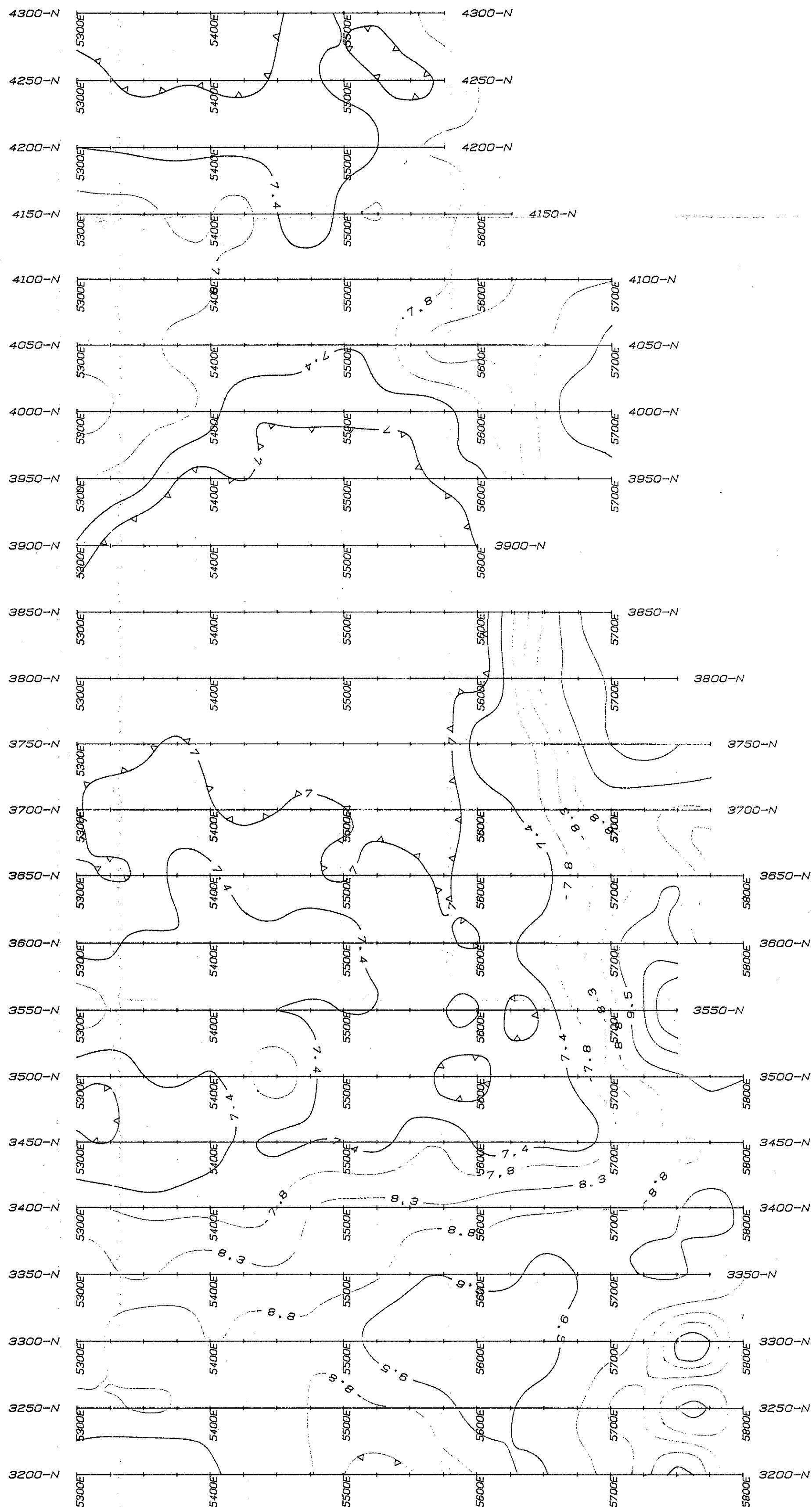
KRL RESOURCES CORP.

LIARD CANYON, Y.T.
SOIL SAMPLE ANALYSIS
Ag ppb

LIARD RIVER, YUKON TERRITORY.

DONEGAL DEVELOPMENTS LTD.

COMPILED F. Syberg	N.T.S.	DATE 105A/2 AUG., 1995.	FIG. NO. 19
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093739

DWG 116

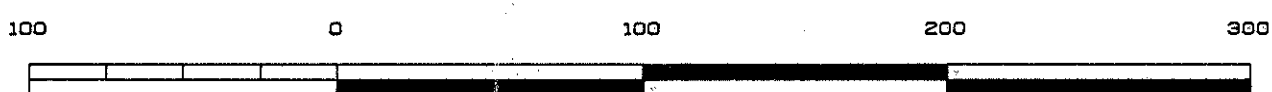
KRL RESOURCES CORP.

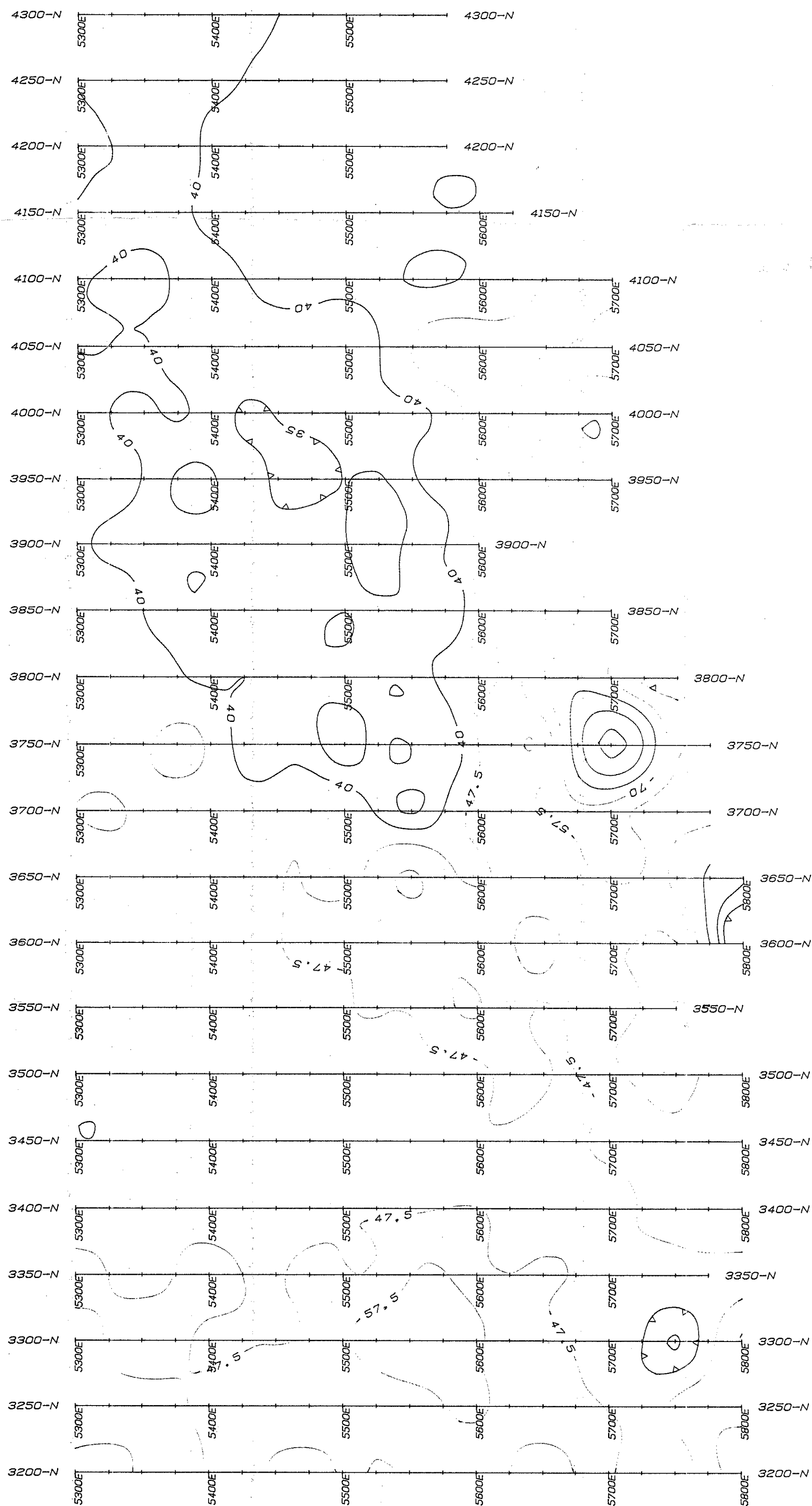
LIARD CANYON, Y.T.
SOIL SAMPLE ANALYSIS
Pb ppm

LIARD RIVER, YUKON TERRITORY.

DONEGAL DEVELOPMENTS LTD.

COMPILED	N.T.S.	DATE	FIG. NO.
F. Syberg	105A/2	AUG., 1998.	20



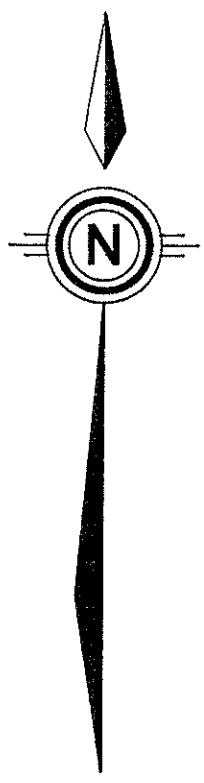
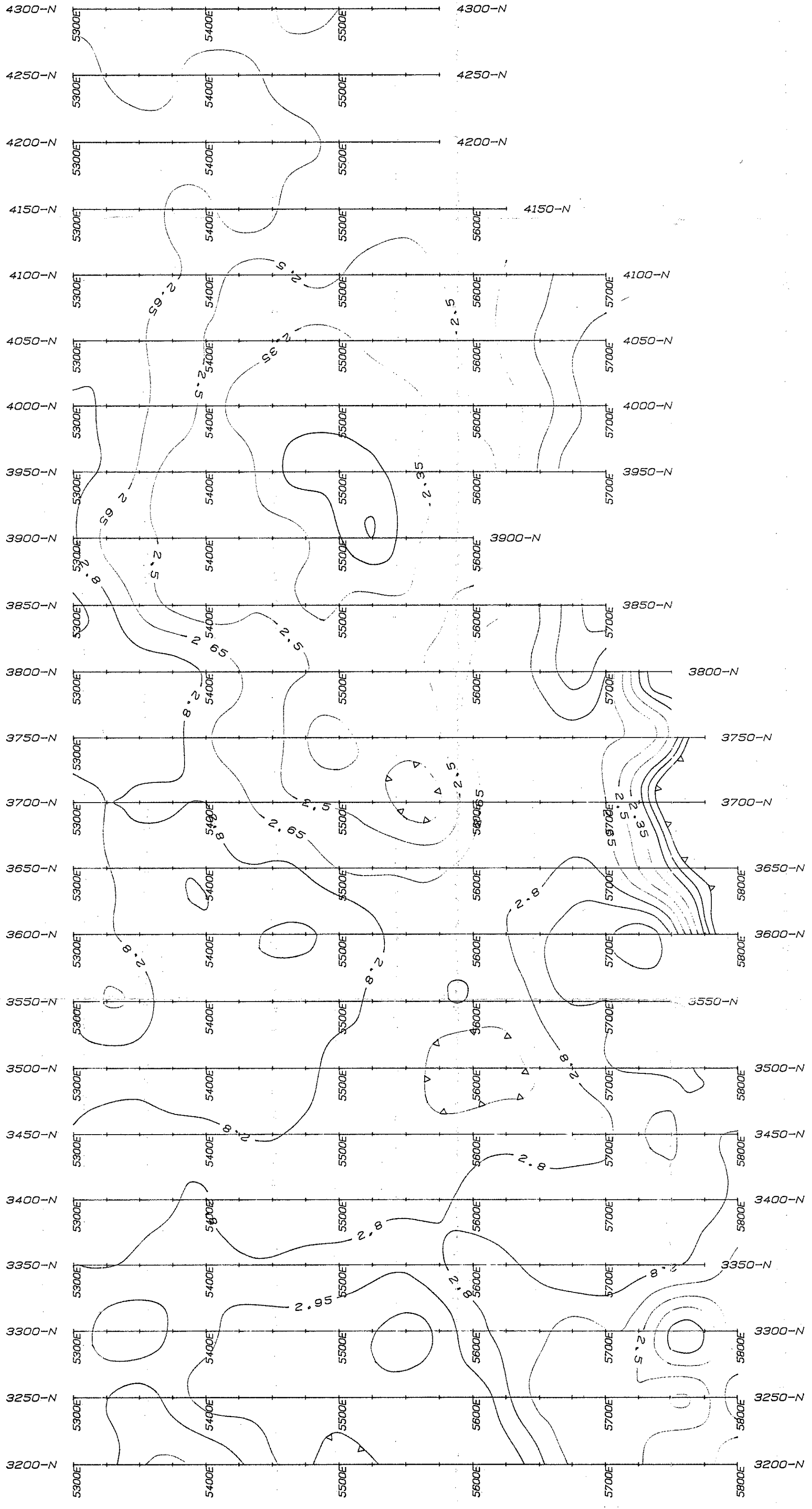


093739

Dwg 17

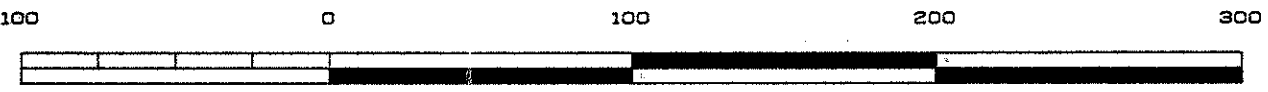


KRL RESOURCES CORP.			
LIARD CANYON, Y.T.			
SOIL SAMPLE ANALYSIS			
Zn ppm			
LIARD RIVER, YUKON TERRITORY.			
DONEGAL DEVELOPMENTS LTD.			
COMPILED	N.T.S.	DATE	FIG. NO.
F. Syberg	105A/2	AUG., 1996.	21

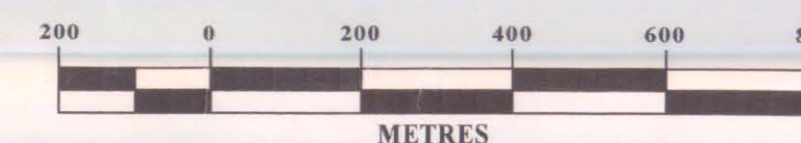
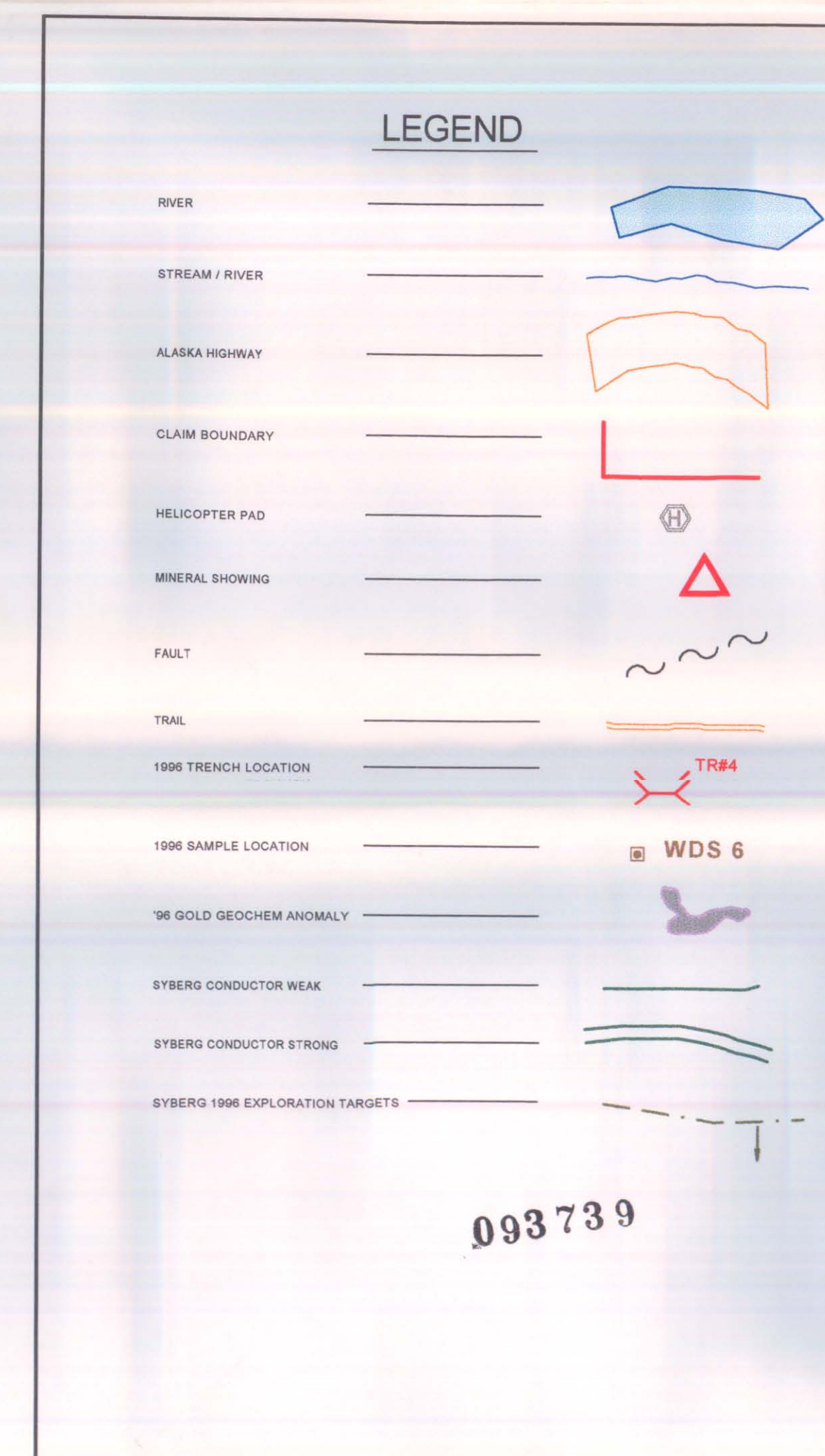
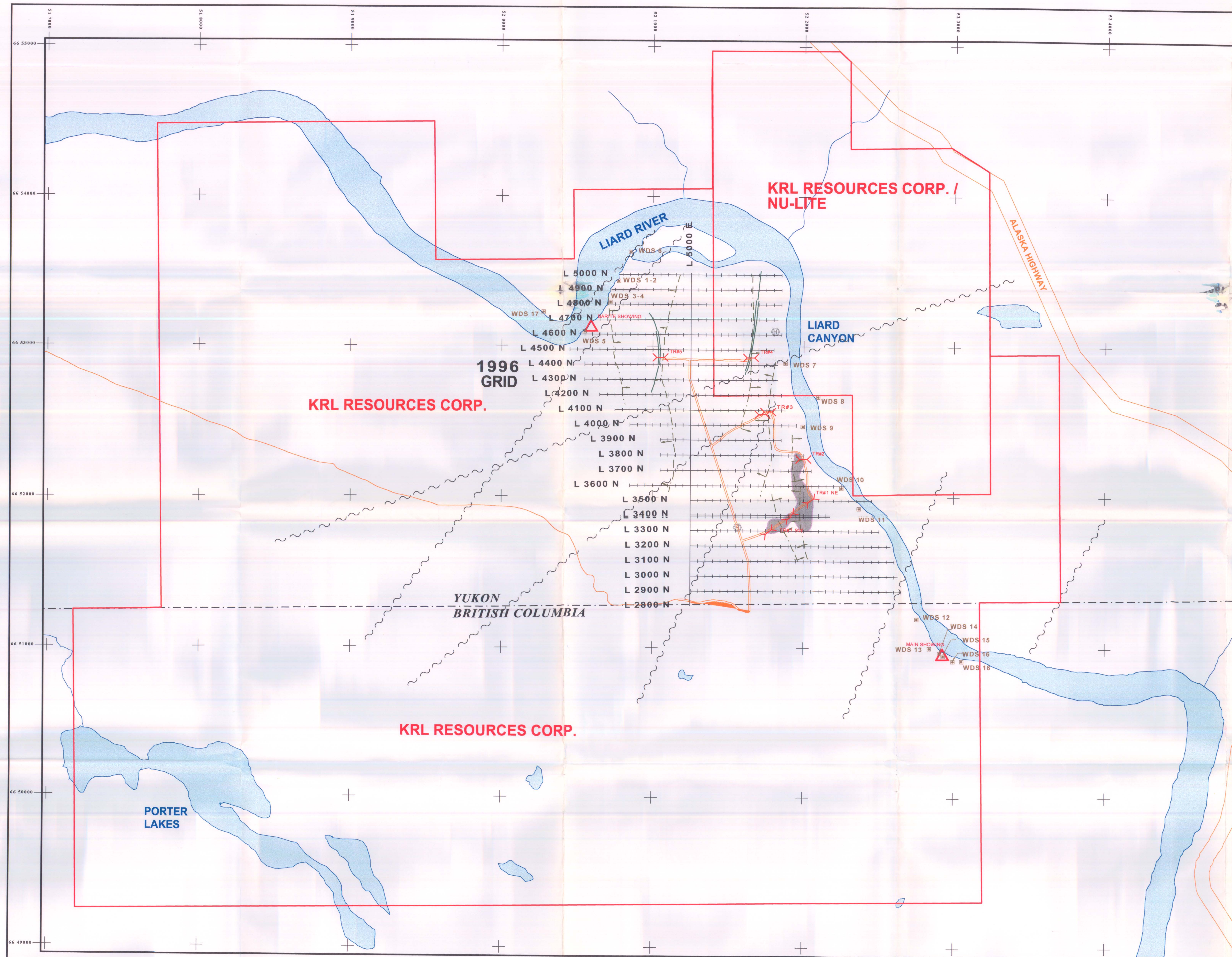


093739

DWG (19)



KRL RESOURCES CORP.			
LIARD CANYON, Y.T.			
SOIL SAMPLE ANALYSIS			
Fe %			
LIARD RIVER, YUKON TERRITORY.			
DONEGAL DEVELOPMENTS LTD.			
COMPILED	N.T.S.	DATE	FIG. NO.
F. Syberg	105A/2	AUG., 1986.	23



KRL Resources Corp.			
WATSON PROJECT			
COMPILATION MAP			
1996 WORK PROGRAM			
Drawn: J.D.	Checked: R.C.	Scale: 1:10 000	Drawing: WLCOMP.DWG
Date: FEB.1997	Revised:	Province: BC / Yukon Territory	NTS: 105A2 / 104P15

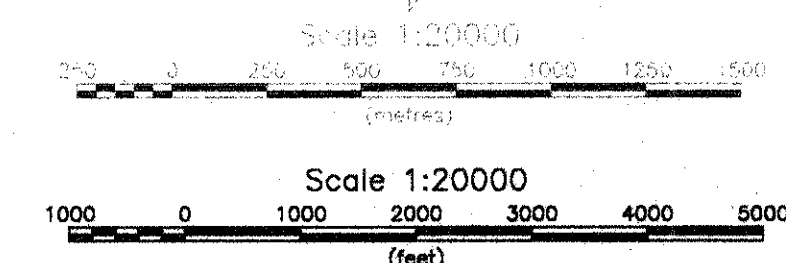
FIG. 24

DWG 20

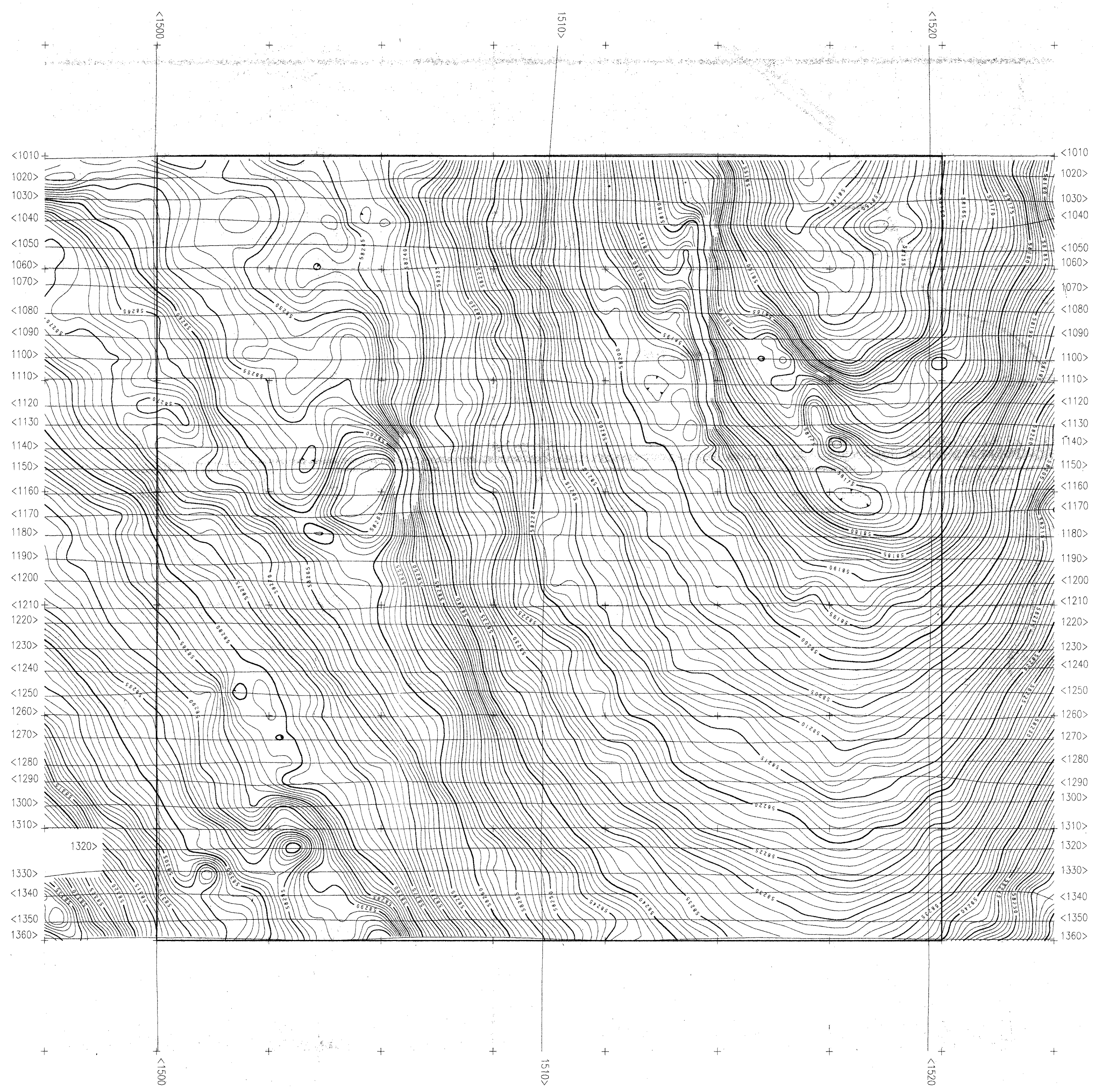
DIAND - YUKON REGION, LIBRARY

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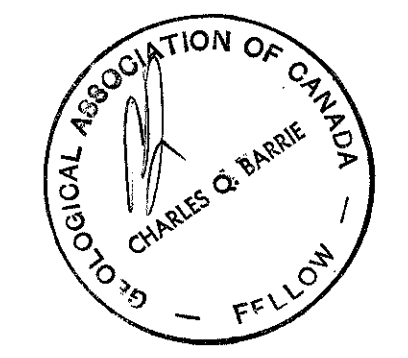
093739



OPERATIONAL INFORMATION
AIRCRAFT: CESSNA 441Q
CONFIGURATION: TAIL, LEFT AND RIGHT MAG SENSORS
SENSOR: DESIGN VAPOR MAG
FLIGHT PLAN: 100 METRE LINE SPACING, E-W LINE DIRECTION
MINIMUM TERRAIN CLEARANCE: 75 METRES
FLIGHT: SPRING, 1996
GPS: HALLMARK POST CODED DIFFERENTIAL FLIGHT PATH RECOVERY
MAP: 15000 SHIPPOID NAV 1987



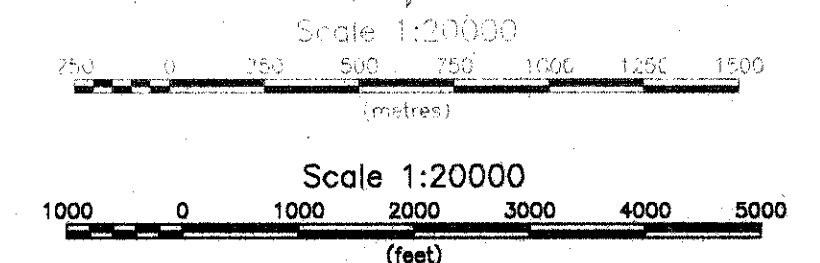
093739



Dwg (21)

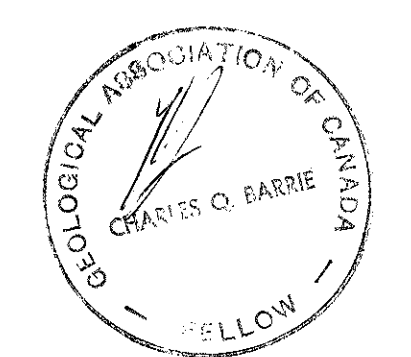
K R L RESOURCES CORP.
LIARD CANYON, YUKON TERRITORY
Total Magnetic Field
Contours
Surveyed By
TERRAQUEST LTD.
Data Compiled and Plotted By
PATERSON, GRANT & WATSON LTD.
April, 1996
Figure A-954B-1

093739



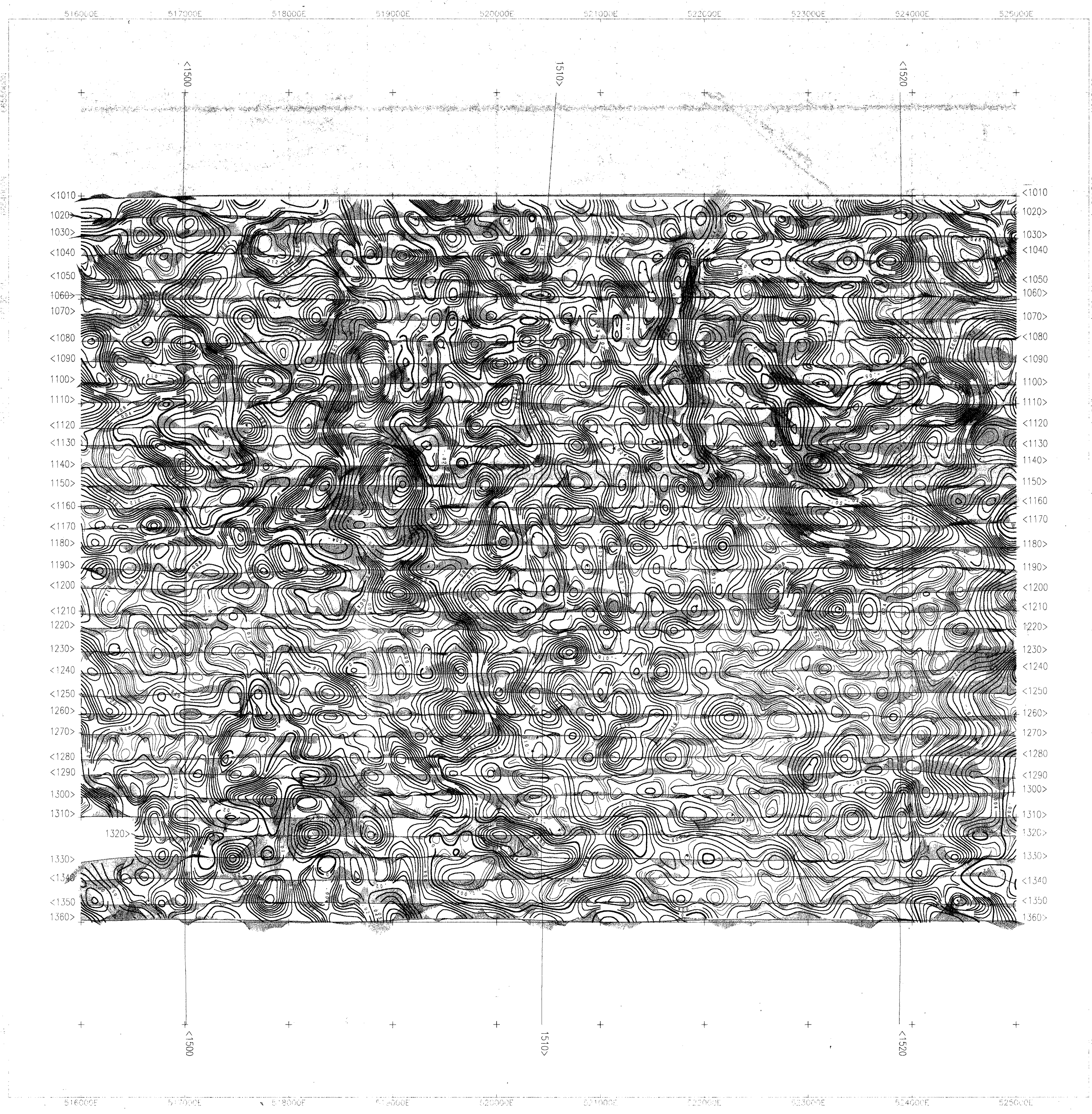
OPERATIONAL INFORMATION
 AIRCRAFT: CESSNA 440Q
 CONFIGURATION: TAIL, LEFT AND RIGHT MAG SENSORS
 SENSOR: CESSNA JAPPHAR MAG
 FLIGHT PLAN: 20 METRE LINE SPACING, E-W LINE DIRECTION
 NOMINAL TERRAIN: 1. PARALLEL TO AIRTRAC
 FLOW: SPRING, 1996
 GPS NAVIGATION: POST FLIGHT ORTERPUSAL FLIGHT PATH RECOVERY
 DATE: 1996 SEP 22/23/24/25/26

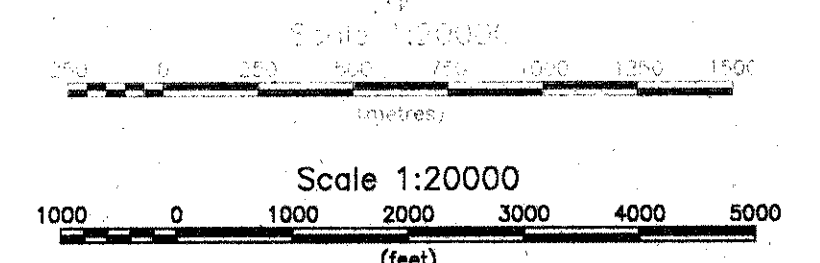
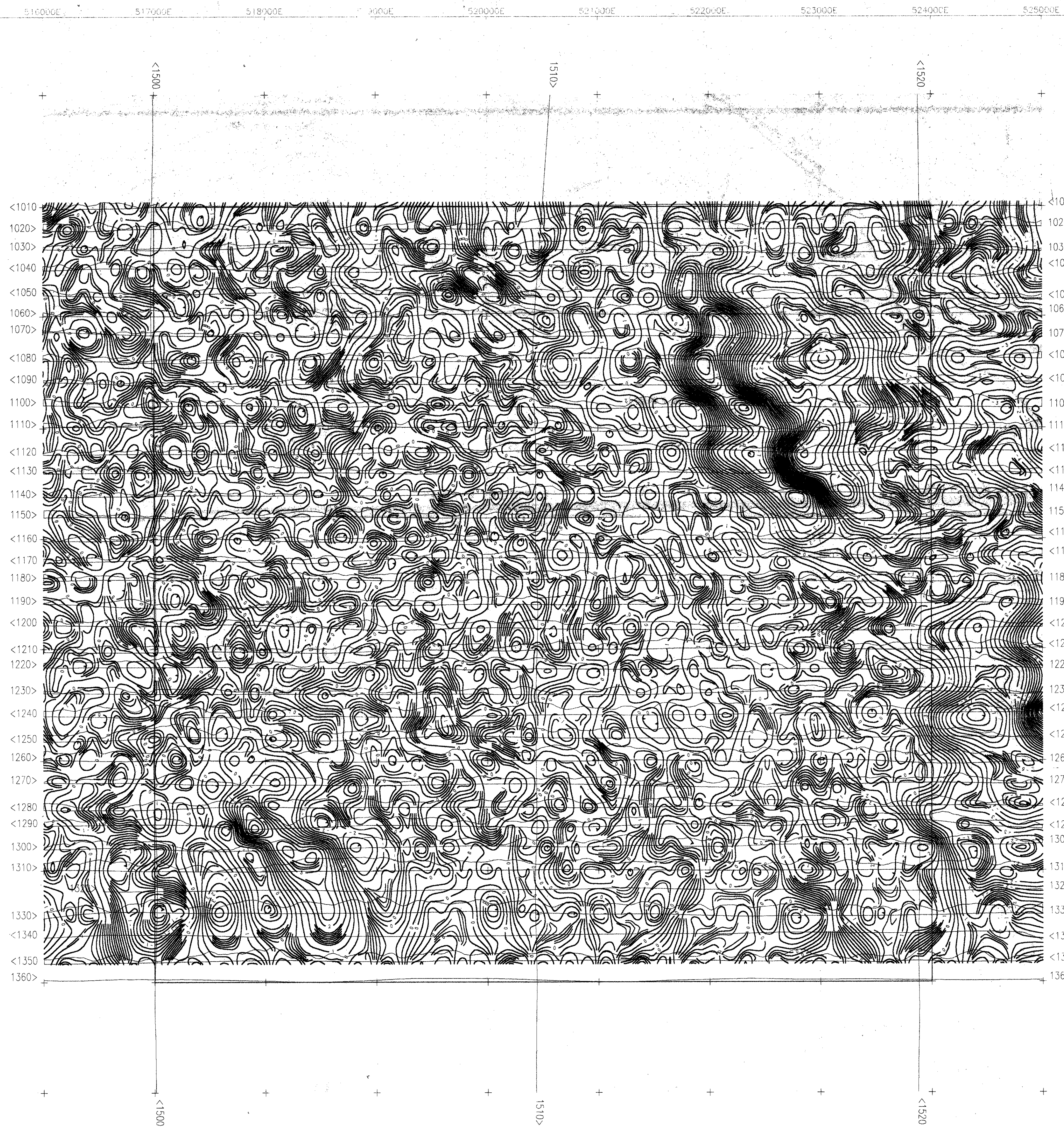
093739



DWG 22

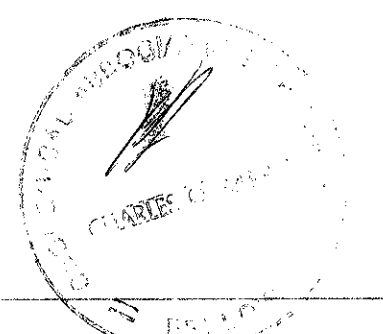
K R L RESOURCES CORP.
 LIARD CANYON, YUKON TERRITORY
 Vertical Gradient and
 Horizontal Gradient Vectors
 Surveyed By
TERRAQUEST LTD.
 Data Compiled and Plotted By
PATERSON, GRANT & WATSON LTD.
 April, 1996
 Figure 1: Map of Liard Canyon, Yukon Territory
 YUKON - YUKON REGION, LIBRARY





OPERATIONAL INFORMATION
 AIRCRAFT: CESSNA 441
 SENSORS: TAIL, LEFT AND RIGHT MAG SENSORS
 SOFTWARE: CESSNA MAG MAP
 FLIGHT PLAN: 200 METRE LINE SPACING, L-W LINE DIRECTION
 MAGNETIC FLIGHT ELEVATION: 15 METRES
 FLIGHT SPEED: 100 KTS
 GPS: GARMIN 1000 POST FLIGHT DATA LOG, DATA PATH RESOLUTION
 1 METRE, 1500 METRE, 1500 METRE

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DWG 23

K R L RESOURCES CORP.

LIARD CANYON, YUKON TERRITORY

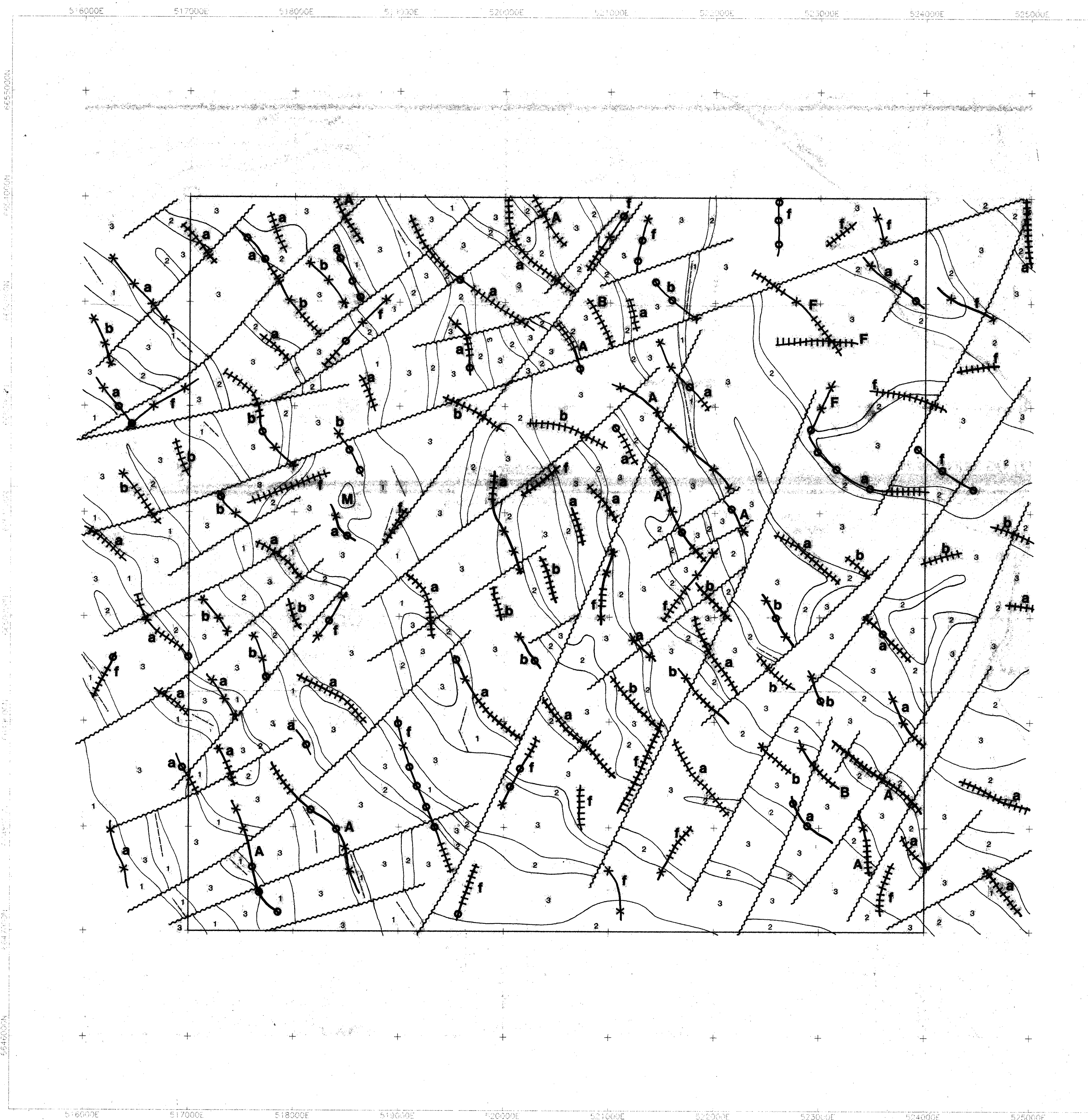
**VLF EM Total Field
Contours & Quadrature Profiles**

Surveyed By
TERRAQUEST LTD.

Data Compiled and Plotted By
PATERSON, GRANT & WATSON LTD.

April, 1996
Figure A-254B-3

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Scale 1:20000
250 0 250 500 750 1000 1250 1500
(metres)

Scale 1:20000
1000 0 1000 2000 3000 4000 5000
(feet)

OPERATIONAL INFORMATION

AIRCRAFT: CESSNA 440Q
CONFIGURATION: TAIL, LEFT AND RIGHT MAG SENSORS
SENSOR: CESSNA VAPOUR MAG
FLIGHT PLAN: 200 METRE LINE SPACING, E-W LINE DIRECTION
NOMINAL TERRAIN CLEARANCE: 75 METRES
FLYING: SPRING, 1996
GPS NAVIGATION: POST FLIGHT DIFFERENTIAL FLIGHT PATH RECOVERY
CLARKE 1886 SPHEROID/NAF 1127

GEOLOGICAL LEGEND	
3	Magnetic background
2	Weakly magnetic unit
1	Highly magnetic unit

SYMBOLS

- Contact of Magnetic Unit
- Horizontal Gradient Axis
- ~~~~ Fault, Shear Zone, Tight Fold Axis
- M Near Surface Magnetic Attraction (see text)

VLF-EM CONDUCTOR AXES

- *** Normal Quadrature
- Reverse Quadrature
- ++++ Total Field Only

VLF TRANSMITTER:
NLK Seattle 24.8 kHz, Azimuth 159°

See text for classification of VLF-EM conductors

093730

DWG 24



K R L RESOURCES CORP.

LIARD CANYON, YUKON TERRITORY

Interpretation

Surveyed By

TERRAQUEST LTD.

Data Compiled and Plotted By

PATERSON, GRANT & WATSON LTD.

April, 1996

Figure 1-954E-1

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