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1996 ASSESSMENT REPORT

MAGNETOMETER, VLF-EM, & GEOCHEM SURVEY

on the

KR 1 - 238 CLAIMS

KLAZA GRIDS

Latitude 62°09' North

Longitude 137°15' West

Whitehorse, Mining District,

N.T.S 115 1/3

for

B.Y.G. NATURAL RESOURCES INC.

110 Industrial Road

Whitehorse, Yukon

Y1A 2T1

Survey by

SJ GEOPHYSICS LTD.

11762 - 94th Avenue

Delta, British Columbia

Canada V4C 3R7

B.Y.G. NATURAL RESOURCES INC.

Report by

Zoran Dujakovic

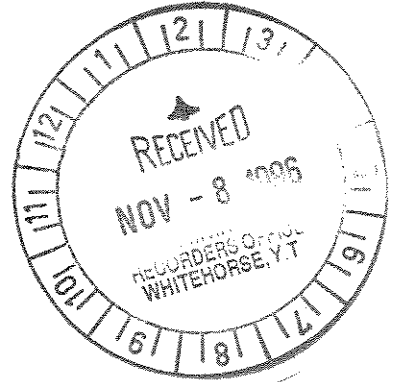
Syd Visser, P. Geo

S.J.V. CONSULTANTS LTD.

Eric Ewen

B.Y.G. NATURAL RESOURCES INC.

May 15, 1996 to Sept 15, 1996



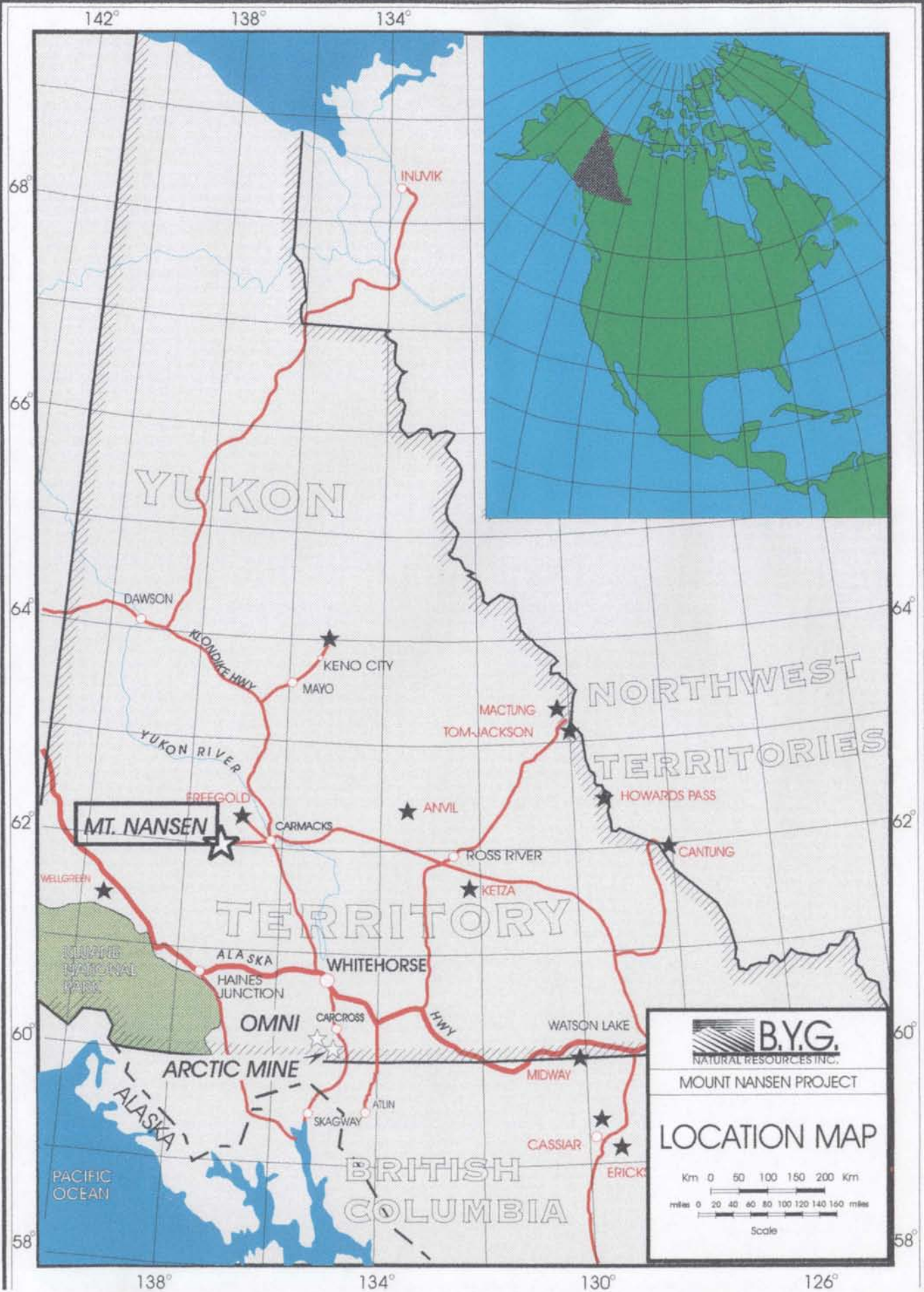


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LIST OF CLAIMS AND TAG NUMBERS

CLAIM NAME	TAG NUMBER	CLAIM NAME	TAG NUMBER	CLAIM NAME	TAG NUMBER
KR1	YB58184	KR42	YB58225	KR83	YB58266
KR2	YB58185	KR43	YB58226	KR84	YB58267
KR3	YB58186	KR44	YB58227	KR85	YB58268
KR4	YB58187	KR45	YB58228	KR86	YB58269
KR5	YB58188	KR46	YB58229	KR87	YB58270
KR6	YB58189	KR47	YB58230	KR88	YB58271
KR7	YB58190	KR48	YB58231	KR89	YB58272
KR8	YB58191	KR49	YB58232	KR90	YB58273
KR9	YB58192	KR50	YB58233	KR91	YB58274
KR10	YB58193	KR51	YB58234	KR92	YB58275
KR11	YB58194	KR52	YB58235	KR93	YB58276
KR12	YB58195	KR53	YB58236	KR94	YB58277
KR13	YB58196	KR54	YB58237	KR95	YB58278
KR14	YB58197	KR55	YB58238	KR96	YB58279
KR15	YB58198	KR56	YB58239	KR97	YB58280
KR16	YB58199	KR57	YB58240	KR98	YB58281
KR17	YB58200	KR58	YB58241	KR99	YB58282
KR18	YB58201	KR59	YB58242	KR100	YB58283
KR19	YB58202	KR60	YB58243	KR101	YB58284
KR20	YB58203	KR61	YB58244	KR102	YB58285
KR21	YB58204	KR62	YB58245	KR103	YB58286
KR22	YB58205	KR63	YB58246	KR104	YB58287
KR23	YB58206	KR64	YB58247	KR105	YB58288
KR24	YB58207	KR65	YB58248	KR106	YB58289
KR25	YB58208	KR66	YB58249	KR107	YB58290
KR26	YB58209	KR67	YB58250	KR108	YB58291
KR27	YB58210	KR68	YB58251	KR109	YB58292
KR28	YB58211	KR69	YB58252	KR110	YB58293
KR29	YB58212	KR70	YB58253	KR111	YB58294
KR30	YB58213	KR71	YB58254	KR112	YB58295
KR31	YB58214	KR72	YB58255	KR113	YB58296
KR32	YB58215	KR73	YB58256	KR114	YB58297
KR33	YB58216	KR74	YB58257	KR115	YB58298
KR34	YB58217	KR75	YB58258	KR116	YB58299
KR35	YB58218	KR76	YB58259	KR117	YB58300
KR36	YB58219	KR77	YB58260	KR118	YB66001
KR37	YB58220	KR78	YB58261	KR119	YB66002
KR38	YB58221	KR79	YB58262	KR120	YB66003
KR39	YB58222	KR80	YB58263	KR121	YB66004
KR40	YB58223	KR81	YB58264	KR122	YB66005
KR41	YB58224	KR82	YB58265	KR123	YB66006

CLAIM	TAG	CLAIM	TAG	CLAIM	TAG
NAME	NUMBER	NAME	NUMBER	NAME	NUMBER
KR124	YB66007	KR163	YB66046	KR202	YB66085
KR125	YB66008	KR164	YB66047	KR203	YB66086
KR126	YB66009	KR165	YB66048	KR204	YB66087
KR127	YB66010	KR166	YB66049	KR205	YB66088
KR128	YB66011	KR167	YB66050	KR206	YB66089
KR129	YB66012	KR168	YB66051	KR207	YB66090
KR130	YB66013	KR169	YB66052	KR208	YB66091
KR131	YB66014	KR170	YB66053	KR209	YB66092
KR132	YB66015	KR171	YB66054	KR210	YB66093
KR133	YB66016	KR172	YB66055	KR211	YB66094
KR134	YB66017	KR173	YB66056	KR212	YB66095
KR135	YB66018	KR174	YB66057	KR213	YB66096
KR136	YB66019	KR175	YB66058	KR214	YB66097
KR137	YB66020	KR176	YB66059	KR215	YB66098
KR138	YB66021	KR177	YB66060	KR216	YB66099
KR139	YB66022	KR178	YB66061	KR217	YB66100
KR140	YB66023	KR179	YB66062	KR218	YB66101
KR141	YB66024	KR180	YB66063	KR219	YB66102
KR142	YB66025	KR181	YB66064	KR220	YB66103
KR143	YB66026	KR182	YB66065	KR220	YB66103
KR144	YB66027	KR183	YB66066	KR221	YB66104
KR145	YB66028	KR184	YB66067	KR222	YB66105
KR146	YB66029	KR185	YB66068	KR223	YB66106
KR147	YB66030	KR186	YB66069	KR224	YB66107
KR148	YB66031	KR187	YB66070	KR225	YB66108
KR149	YB66032	KR188	YB66071	KR226	YB66109
KR150	YB66033	KR189	YB66072	KR227	YB66110
KR151	YB66034	KR190	YB66073	KR228	YB66111
KR152	YB66035	KR191	YB66074	KR229	YB66112
KR153	YB66036	KR192	YB66075	KR230	YB66113
KR154	YB66037	KR193	YB66076	KR231	YB66114
KR155	YB66038	KR194	YB66077	KR232	YB66115
KR156	YB66039	KR195	YB66078	KR233	YB66116
KR157	YB66040	KR196	YB66079	KR234	YB66117
KR158	YB66041	KR197	YB66080	KR235	YB66118
KR159	YB66042	KR198	YB66081	KR236	YB66119
KR160	YB66043	KR199	YB66082	KR237	YB66120
KR161	YB66044	KR200	YB66083	KR238	YB66121
KR162	YB66045	KR201	YB66084		

INTRODUCTION

Magnetic and a very low frequency electromagnetic (VLF-EM) surveys were completed on the Mt. Nansen property, Klaza grids, for B.Y.G. Natural Resources Inc., by SJ Geophysics Ltd. from June 10 to Sept 15, 1996. The Mt. Nansen property is located about 60km west of Carmacks (Figure 1), Yukon in the Whitehorse Mining District, NTS 115 I/3. The Geophysical data was compiled and reported on by Zoran Dujakovic.

Soil geochemistry was done on areas of the same grids as the geophysical survey and on extensions of these grids where geophysics had not been done yet. The Geochemistry was compiled and reported on by H. Eric Ewen.

The purposes of the surveys were to aid in the mapping of local geology, search for mineralized or conductive structures, follow up of government stream sediment, and B.Y.G. 1995 reconnaissance soil geochemical anomalies.

CLAIMS

The Klaza grids are located on the KR claims. These claims (Plate 1) are located in the Whitehorse Mining District and are held by B.Y.G. Natural Resources Inc. & Trumpeter Yukon Gold Inc. Co-ordinates of the claims are latitude 62°09' north and longitude 137°15' west. The list of claims and tag numbers are as provided on previous pages.

CLAIMS LOCATION AND ACCESS

The property can be reached by vehicle from Whitehorse by travelling 180 km north on Highway #2 to Carmacks, then 60 km west on a gravel access road to the B.Y.G. mine site. From the mine site access is via a gravel road over the Nansen Creek / Klaza River watershed approximately 12 kilometres to the Klaza River valley where the KR claims are located. A tent camp was situated at the end of the road to lessen access time to this property.

CLIMATE

The area is quite dry with average precipitation of about 25 cm, most of which falls as rain in the summer months. Late winter snow-pack is normally 30 to 40 cm deep. Average monthly temperatures range from -15°C in January to 15°C in July.

In general outside activities such as construction can be conducted readily from April to early November.

HISTORY

In 1943 prospectors Brown and McDade discovered lode deposit on Mount Nansen. Leitch Gold Mines forms Brown McDade Mines. Ltd.

In 1947 H. Heustis stacked gold-silver veins on Mt. Nansen. Mt. Nansen Mines Ltd. carried out surface exploration between 1962 and 1964, and in 1965 underground exploration began.

Between 1965 and 1967 two shafts were driven, one at the 1250 m level, and one at the 1309 m level.

In 1968 and 1969 Heustis and Webber veins were mined at a rate of 65-90 tonnes per day. In 1969 without cyanide circuit, 40% of the gold reports to the tailings ponds and production ceased.

In 1976 mill re-opens again with excellent grades from Heustis and mine operated for 10 months.

In 1984 B.Y.G. acquired the Mt. Nansen property and optioned it to Chevron who conducted extensive exploration and discover Brown-McDade oxide deposit.

In 1986 11 diamond drill holes totalling 576 m were completed. Seven holes encountered significant gold and silver values in the Flex vein zone.

In 1988 exploration consisted of road construction, bulldozer and excavator trenching, stripping, rehabilitation of underground workings and 5397 m of diamond drilling in 85 holes. Most of the drilling was done on the Brown-McDade zone.

In 1994 12 diamond drill holes totalling 1000 m were completed in the Flex, Heustis North, and Brown-McDade sulphide zones.

GENERAL GEOLOGY AND MINERALIZATION

Mt. Nansen is situated within the eastern part of the Yukon Crystalline Terrain, which lies between the Coast Plutonic Complex to the southwest, and the Yukon Cataclastic Terrain to the northwest.

The southern portion of the property is underlain by deformed, medium to high grade metamorphic rocks. These include interlayered quartz-feldspar-chlorite gneiss, quartzite, amphibolite and augen gneiss. Foliation within these rocks strikes northeast and dips steeply to the northwest.

The northeastern portion of property is underlain by Early Cretaceous coarse-grained granodiorite with lesser quartz diorite and quartz monzonite. These rocks may contain up to 25% stubby amphibole and are locally foliated. Coeval pegmatite and aplite dykes are common locally.

Two types of faults occur on the property. The first set strikes north-northwest and dips between 50° and 70° to the southwest. These faults are parallel to the veins and locally mineralized. The second set of faults strikes northeast and dips subvertically. These faults vary in their sense and magnitudes of displacement. Locally, they cut the mineralized zones.

Gold and silver occur in a number of quartz-sulphide vein zones which cut Palaeozoic metamorphic rocks and Cretaceous quartz monzonite stocks, feldspar porphyry dykes and plugs, andesitic flows and pyroclastic rocks. The vein strikes northwest and dips from 80° NE to 45° SW. The veins comprise quartz lenses with arsenopyrite, pyrite, sphalerite, galena, tetrahedrite and stibnite. Depth of total oxidation ranges from 0 to 100 m depending on the type of mineralization and orientation of the vein.

On the Tawa property, which parts of the grids cover, there are at least three shear zones striking approximately 300°. These zones are in granite diorites and are in part mineralized with gold bearing sulphides. Soil geochemistry, some trenching, and a limited amount of drilling has been done on this property.

GEOPHYSICAL REPORT

INTRODUCTION

Magnetic and a very low frequency electromagnetic (VLF-EM) surveys were completed on the Mt. Nansen property, Klaza grids, for B.Y.G. Natural Resources Inc., by SJ Geophysics Ltd. from June 10 to Sept 15, 1996. The Mt. Nansen property is located about 60km west of Carmacks (Figure 1), Yukon in the Whitehorse Mining District, NTS 115 I/3.

The purposes of the survey were to aid in the mapping of local geology, search for mineralized or conductive structures, follow up of government stream sediment, and B.Y.G. 1995 reconnaissance soil geochemical anomalies.

FIELD WORK AND INSTRUMENTATION

Magnetometer & VLF-EM surveys were completed June 10 to Sept 15, 1996. Data acquisition, processing and field presentation were performed by Zoran Dujakovic (Geophysicist). The Klaza grids are formed by three different grids as shown on maps. Grid 1 (lines 3600W to 8600W) was surveyed from June 10 to 30, Grid 2 (lines 601W to 8601W) from July 19 to August 07 and Grid 3 (lines 202W to 3302W) from August 12 to September 14. The Klaza grids consisted of flagged, compass and hip-chain lines. Surveying was performed at 12.5 metre intervals along the 100 m spaced lines for a total of approximately 243 kilometres.

An EDA OMNI PLUS combined proton precession magnetometer and VLF-EM system were used for data acquisition and an EDA OMNI IV proton precession magnetometer was used as a base station which recorded data in 30 seconds intervals. The VLF-EM survey used the signals from a Geonics NK27 portable transmitter transmitting at 18.6 kHz, Jim Creek (24.8 kHz, NLK) and Cutler (24.0 kHz, NAA). The portable Geonics transmitter was used on Grid 1 while the Jim Creek transmitter was not transmitting. The Jim Creek transmitter was used while it was transmitting on the remainder of the grid. The Cutler transmitter is poorly orientated for east/west lines and was used primarily for conformation of anomalies detected with the portable transmitter. The signal/noise from Cutler transmitter was very bad and data from this station is not presented. The direction of VLF-EM surveying is positive to the east.

All data was downloaded to a computer in the evening. The data was processed as time permitted by the geophysicist. The data was plotted on a Bubble Jet printer.

The data was re-plotted on a 36 inch Ink Jet colour plotter in Vancouver for the final presentation and interpretation.

DATA PRESENTATION

The claim and grid location, magnetic, VLF-EM data, filtered VLF-EM data and compilation of the magnetic and VLF-EM data are presented on the following plates:

TABLE 1 list of plates geophysics.

PLATE 1	KR CLAIM, GEOCHEMISTRY PLATE, & GRIDS LOCATION MAP	In Pocket
PLATE G1A	TOTAL FIELD MAGNETICS PROFILES	In Pocket
PLATE G1B	TOTAL FIELD MAGNETICS CONTOURS	In Pocket
PLATE G1C	TOTAL FIELD MAGNETICS COLOUR CONTOURS	In Pocket
PLATE G2A	VLF-EM PROFILES LOCAL Tx. 18.6 kHz AND JIM CREEK, NLK 24.8 kHz	In Pocket
PLATE G2B	VLF-EM CONTOURS OF FRASER FILTER DIP ANGLE LOCAL Tx. 18.6 kHz AND JIM CREEK, NLK 24.8 kHz	In Pocket
PLATE G2C	VLF-EM COLOUR CONTOURS OF FRASER FILTER DIP ANGLE LOCAL Tx. 18.6 kHz AND JIM CREEK, NLK 24.8 kHz	In Pocket
PLATE G3	MAGNETIC AND VLF-EM COMPILATION MAP	In Pocket

INTERPRETATION

The interpretation is presented on the compilation map, Plate G3. Discussions regarding directions on the grid will be in terms of grid east, north, south, and west.

MAGNETICS

The magnetic relief over the surveyed area is approximately 4000 nT. The magnetic highs appear to be mainly related to changes in lithology, whereas the magnetic lows can be related to structures. The survey area is divided in to 3 grids with Grid 1

located north of line 3000N, Grid 2 between 1500N and 3000N and Grid 3 south of 1500N

The highest susceptibilities on Grid 1 are noted in the north-western part and are bound on the southern (~ 4000N) and western (~6700W) edges by anomalous magnetic lows. It is not clear if the magnetic lows are changes in rock types or major structures. They appear to separate major changes in geology and are likely wide structures. The south-western part of Grid 1 has a very uniform susceptibility. The eastern part has a higher and more variable magnetic response. Inside the magnetic high or relative magnetic high zones are a number of magnetic low lineations. The majority of these magnetic lineations strike approximately north-west, parallel to the base line.

The magnetic responses on Grid 2 are characterised by magnetic lows at the northwest part that steadily increase to the south-east and the continuation of the north-west striking magnetic low structures. The trend of increasing magnetic susceptibility is cut by a magnetic low at approximately 4000W. This magnetic low appears to be a major northerly striking structure.

The magnetic data indicates a very strong magnetic high area on the central part of Grid 3. It is the highest magnetic response on the Klaza grids and may represent volcanic rock with high magnetic mineral content. The eastern part of Grid 3 has a magnetic low, whereas the north-western part has a higher and more variable magnetic response. Inside the magnetic high zones are a number of linear magnetic lows.

VLF-EM

The VLF-EM survey has delineated numerous north-west trending anomalies shown on the compilation map as strong, medium and weak conductors. There appear to be at least 3 major structures striking across the survey area but mainly located on Grid 2, the central part of the survey area. These major structures are locally offset by northerly striking cross structures located from the magnetic data and discontinuity in the VLF-EM anomalies. The anomalies appear to be stopped to the east by disappearing into a porphyry system and to the west by a major structure. In general the VLF-EM anomalies coincide with magnetic lineations. The following is a more detailed description of the VLF-EM anomalies.

The well defined VLF-EM anomalies from Grid 1 are labelled as V1 and V2.

Anomaly V1, located in the south-eastern part of the grid, appears to be associated with a magnetic lineation. The source of this anomaly could either be massive sulphides, conductive fault, or a combination of both.

Anomaly V2 is associated with a variable magnetic response and appears to be the edges of a conductive zone and possibly wide weakly conductive shears.

The VLF-EM anomalies located in the north-western part of Grid 1 shown as medium conductors, could be defined as strong conductors but the ratio of signal/noise at that part of grid wasn't good.

The remainder of VLF-EM anomalies from Grid 1, shown as medium and weak conductors, are not discussed, but presented on the compilation map. These anomalies are mostly associated with magnetic lineations and may represent resistive contacts or weakly conductive faults.

The most prominent VLF-EM anomalies from Grid 2 are well defined strong conductors labelled V3 to V10.

Anomalies V3 to V5 are located in the central part of the second grid. These anomalies appear to be associated with a magnetic lineation and may represent massive sulphides, long conductive faults or a combination of both.

Anomaly V6 could be the southeastern part of V5 which is cut by a major north-east structure. This anomaly is also associated with a magnetic lineation.

Anomalies V7 to V9 appear to be long strike length anomalies located in the eastern part of Grid 2 on the Tawa property. These anomalies are situated in the area with magnetic highs, but definitely appear to be associated with a magnetic lineation.

Anomaly V10, located in the eastern part of Grid 2, is associated with high magnetic response.

The well defined VLF-EM anomalies on Grid 3 are strong conductors labelled V11-V16.

Anomaly V11 located in the northern part of Grid 3 appears to be associated with a magnetic lineation and might be a south-eastern part of anomaly V6.

Anomalies V12 to V16, located in the central part of Grid 3 in the area with very high magnetic responses, are well defined anomalies which should have little topographic influence. The majority of these anomalies are associated with magnetic lineations.

The remainder of VLF-EM anomalies from Grid 3, shown as medium and weak conductors may represent resistive contacts or weakly conductive faults.

RECOMMENDATIONS

The geophysical data should be compiled with geological mapping and geochemical sampling to determine if more detail work or other geophysical techniques are required to enhance the geological mapping. If the results of the Mag/VLF survey correlate well with the geology, further interpretation of that correlation is recommended.

The strong VLF-EM anomalies mentioned in the above interpretation and shown on the compilation map G3, especially those correlating with a magnetic lineation, should be prospected carefully and possibly checked with trenching and/or geochemical sampling.

All strong VLF-EM anomalies should be checked by other geophysical techniques, such as Horizontal Loop EM (HLEM), before the diamond drilling program is started. Priority should be given to the Tawa property.

Grid 1 should be extended to the east in between lines 3600W and 600W to locate the extension of anomaly V10 and to locate any parallel anomalies.

The western parts of Grids 2 and 3 should be completed to 8600W. It is recommended to resurvey a few lines on the north west corner of Grid 1 and possibly extend the grid to the north in this region.

CONCLUSION

The magnetic susceptibility highs appear to indicate different lithologies. The lows appear to show magnetic lineations related to geological structures or contacts. The highest magnetic responses are noted in the south-western part of the survey area and may represent volcanic rock with high magnetic mineral content. The source of the magnetic low on the western part of the survey area is not clear without further work. The variation in the magnetic response in the remainder of the survey area is likely due to local variations in the susceptibility of the intrusive rocks.

The major features that stand out from the Mag/VLF survey are the parallel coincidental magnetic and VLF-EM anomalies striking across the length of the survey grid. These major structures are locally offset by northerly striking cross structures, located from the magnetic data and discontinuity, in the VLF-EM anomalies. The

anomalies appear to be stopped to the east by disappearing into a porphyry system and to the west by a major structure.

The source of all strong VLF-EM anomalies associated with a magnetic lineation could be either massive sulphides, conductive fault or the combination of both.

The remainder of VLF-EM anomalies, shown as medium and weak conductors, are mostly associated with magnetic lineations and may represent resistive contacts or weakly conductive faults.

All of these magnetic lineations and VLF-EM anomalies should be correlated closely to any local geology. They should be carefully prospected, soil sampled and possibly trenched to determine their potential for mineralization.



Zoran Dujakovic
Geophysicist
SJ Geophysics Ltd.
S.J.V. Consultants Ltd.

GEOCHEMISTRY REPORT

Soil geochemistry was done on areas of the same grids as the geophysical survey and on extensions of these grids where geophysics had not been done yet. As shown on plates C-1, C-1a, C-2, C-3, C-4, C-4a, & C-5 these surveys were conducted over 5 areas of grid. The surveys C1, C1a, C-3 & C-5 were done after the geophysics had been completed. Surveys C2, C4, C4a were in areas where geophysics were not done.

DATA PRESENTATION

The location maps and the geochemical data are presented on the following plates:

TABLE 2 list of plates geochemistry

PLATE 1	KR CLAIM, GEOCHEMISTRY PLATE, & GRIDS LOCATION MAP	In Pocket
PLATE C-1	GOLD SOIL GEOCHEMISTRY (EAST END GRID 2)	In Pocket
PLATE C-1A	GOPPER SOIL GEOCHEMISTRY (EAST END GRID 2)	In Pocket
PLATE C-2	GOLD SOIL GEOCHEMISTRY (WEST END GRID 3)	In Pocket
PLATE C-3	GOLD SOIL GEOCHEMISTRY (WEST END GRID 1)	In Pocket
PLATE C-4	GOLD SOIL GEOCHEMISTRY (WEST END GRID 3)	In Pocket
PLATE C-4A	LEAD SOIL GEOCHEMISTRY (WEST END GRID 3)	In Pocket
PLATE C-5	GOLD SOIL GEOCHEMISTRY (WEST END GRID 2)	In Pocket

GRID C-1

Soil samples were taken at 25 metre spacing on the east end of Grid 2 over portions of lines 801W, 901W, 1001W, 1101W and 1201W. This survey was done to extend the Cu anomaly that was noted on earlier soil sampling of the Tawa property. This Cu anomaly is thought to be caused by a halo from a nearby Cu porphyry body to the south east. Gold values were elevated in the survey of the earlier report and it was hoped that this trend would continue onto this extension. Geophysics in this area showed that the mineralized conductors to the west on the Tawa property did not continue into this region. It appears that the influence of the copper porphyry has altered these conductive mineralized shears and possibly created a more homogeneously mineralized area. This area could prove to be an economic gold deposit that would not have a conductive signature. Because of other commitments of time and manpower this survey was only begun.

Results of this survey show that the Cu anomaly definitely continues onto the lines surveyed and beyond. It also shows a very distinct cut off of the Cu anomaly at about 2300n to 2400n. High gold values appear to have a close relationship to the copper values. The gold anomaly appears to partially overlap and lie a bit outside the copper anomaly. The numbers are reasonably high and, no doubt, reflect bedrock mineralization. It does not appear to be the type of anomaly that would indicate a shear hosted source and may well be an altered area that has a large tonnage potential.

Proper interpretation will only be possible when the rest of the survey is completed and the entire anomaly is blocked out. It is recommended that the survey be continued to the south and east. Upon completion of the survey and delineation of the anomaly, trenching should be done to determine the source. It is expected that the mapping of trench drilling will be used to define the deposit.

It should also be noted that a soil survey was done on another grid to the south east on property held by Aurchem. This grid was laid out so that it would join up with Grid 1. At the time of writing this report, it is not known if this survey was complete and what were the results. When this grid's coverage and results are known, the space (if one exists) between the two will be covered and the two sets of data merged to show the size and intensity of this anomaly.

GRID C-2

This grid was put on the far west end of Klaza Grid 3 to cover an area of anomalous soils from a B.Y.G. 1995 reconnaissance soil line. The intention was to extend this grid over the anomalous area. Because of the lateness of thawing, there were problems getting a good coverage of soils. This grid was left to be continued later in the season when frost would be less of a problem. This was not done and the soil coverage did not reach the area of the anomalous reconnaissance soil line.

Because of the background nature of all results only the gold values are plotted on plate C-2. Coverage was only partial on lines 10800W, 10700W, 10600W, and 10500W at an attempted station spacing of 50 metres. It is recommended that this survey be continued to the east on lines 10400W to 10000W and that the stations missed on those lines sampled be picked up. No geophysics was done here and it is hoped that in 1997, the 1996 survey be extended to cover this area of the grid.

It is expected that the area of shearing that is shown on the grids to the east will extend through this area and farther. Mag/VLF surveys will give targets to do more geochemistry.

GRID C-3

Soil grid 3 was located on lines 8500W to 7400W from 3500N to 4500N on the far west end of Klaza Grid 1 to test a strong VLF-EM conductor. Sample coverage was at 50 metre intervals resulting in approximately 250 samples. Coverage was good with only 5 or 6 sites missed.

This conductor appears to follow a lithologic contact, as determined from the magnetic data, for most of the length of this grid at approximately 4200N at an azimuth of about 110°. In the area of the soil survey, this conductor appears to be broken up into three distinct conductors which follow magnetic lows at approximately 080°. The geophysical data had all the signs of indicating shears and was chosen for follow up soil geochemistry. During the sampling, outcrops and rubble crops of relatively unaltered granodiorites were noted. These were topographically higher than the conductors. Generally, the areas of the conductor were subtle breaks in slope with no outcrop. On the Tawa property mineralized gold bearing shears, it was noted that alteration did not extend into the wall rock so seeing alteration of the granodiorites here was not expected.

Results of this soil survey were not as expected. There were some anomalous gold values in the area of the Klaza drainage, thought to be unreliable indications of bedrock mineralization, because of the extensive till coverage in this area. There were two anomalous gold values each just below the ends of the two conductors targeted. Over one of these conductors some slightly elevated gold values appear to follow the conductor. This may indicate gold mineralization in this shear and this area is targeted for closer spaced soil sampling.

GRID C-4

An area of altered, sheared, and bleached volcanic rock on a saddle that was part of a linear with a strike of approximately 110° was chosen in 1995 for the location of a reconnaissance soil line. This was also part of the drainage area of a stream which returned anomalous gold from a stream sediment sample. This soil line returned some anomalous gold values and was chosen in 1996 as the area to locate a soil grid.

This area is near the western end of Klaza Grid 3 and covers lines 4800W to 5700W from 0N to 1500N. A Mag/VLF survey was planned over this area but was terminated before it extended this far. Because of perma frost problems the soil coverage was about 75% of the grid area. Samples were taken at 50 metre spacing. It is thought that the coverage was sufficient to test possible bedrock mineralization.

The gold results of this survey did not seem to reach the values of the 1995 reconnaissance soil line but did return seven moderately anomalous values. These values do not show any trend other than they are all in the southern part of the grid. It is recommended that these stations be revisited, and closer spaced samples be taken, to attempt to determine the source of these values.

Of the other elements analyzed, the lead values are the most anomalous. Generally they fall on the southern part of the grid but do not appear to be related to the anomalous gold values. There are 15 values greater than 100 ppm and 3 values that are greater than 200 ppm. It is very difficult to see much of a pattern to these anomalous values. One anomalous area extends across 4 lines (400 metres) at about 340°. Another anomalous area extends across 6 lines, in a crescent shape, for a strike length of 800 metres at about 340°.

This 340° trend should be closely examined and these anomalous areas should be prospected. It is hoped that the Mag/VLF survey will be extended into this region of the grid in 1997 and that it may shed more light on these anomalies.

GRID C-5

A VLF-EM conductor with similar orientation as a mineralized conductor on the Tawa property, was selected and investigated in the area of lines 5100W through 5900W at about 2000N on western end of Klaza Grid 2. It was noted that this conductor follows an abrupt change in slope over lines 5100W to 5600W then strikes across a stream valley removing all doubt that the break in slope caused the anomaly. Line 5700W was chosen to run a soil line across this conductor. Soils were taken from the topographic high side of the conductor at 1900N, across it to its topographic low side at 2050N, and then for another 450 metres slightly downhill to 1500N. Soils were taken at 25 metre spacing.

The gold results of this single line of soils shows no outstanding anomaly over the conductor. It does show a slight rise in values over the conductor and another slight rise before the end of the line downhill from the conductor. It appears that geochemistry does

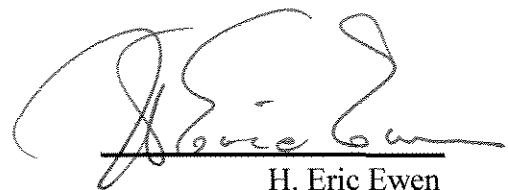
react over this conductor. It is recommended that a soil survey be done over the length of this conductor.

CONCLUSIONS AND RECOMMENDATIONS

This area is extensively underlain with perma frost which creates a problem for utilizing soil geochemistry to its fullest. Nevertheless, there are many areas where it can be effectively used. South and east facing slopes generally thaw earlier so surveys can begin there, then towards the end of the summer can be done in more shaded areas. Moss can be removed from sites to allow a few days to thaw before sampling. Surveys can be planned in specific areas rather than soils be taken as a reconnaissance tool. Areas of heavy till in wide stream valley can be avoided.

Soil geochemistry has proven successful in areas such as Grid C-1 and should be extended in these areas. On other grids, in areas of lesser anomalies, fill in sampling should be done to determine their source. Mag/VLF anomalies should be followed up with soil geochemistry where conditions lend themselves to this type of survey.

Because of the necessity of grids and the time taken to traverse the lines it is recommended that a close spaced (100m) line airborne survey be considered for such a large block of claims as the KR group. A more sophisticated electromagnetic survey than VLF could be used. There is also the possibility of adding a radiometric survey to the airborne Mag/EM. Although this survey would not give the detail of a ground survey, it would cover the area more cost effectively and show similar targets to conduct geochemistry over.



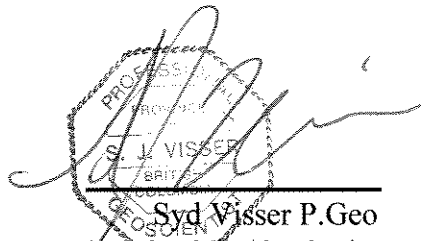
H. Eric Ewen
Mining Technician
B.Y.G. Natural Resources Inc.

SUMMARY

The Magnetic and VLF-EM surveys are very useful in delineating major structures as shown in the survey over the Klaza grid. It is not clear from the geophysics alone if these are related to mineralization. They have to be followed up with detailed geological and geochemical surveys which may include trenching and drilling. It is recommended to perform more sophisticated geophysical techniques over the areas of interest, such as HLEM or possibly I.P..

The geophysical grid should be extended with the area bounded by 0 to 8600W (possibly further) and 0 to 4000N complete with ground work. If the area is to be extended further, the feasibility of a detailed magnetic and multi-frequency EM survey should be considered.

The geochemistry on the eastern part of the survey area indicates that the geochemical grid should be extended to the east and south. The geophysical data should be tied into the data from the eastern property and any gaps surveyed. Geochemical follow-up should be done on any of the major VLF-EM anomalies where feasible.



Syd Visser P. Geo
Geophysicist/Geologist
S.J.V. Consultants Ltd.

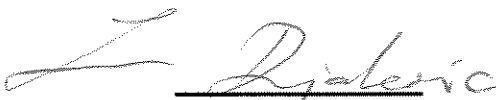
REFERENCES

- Melling, D.R., 1995** Summary Report: 1995 Exploration Program
- Sinclair, W.D., Maloney, J.M. and Craig, D.B., 1974** Mineral Industry Report
1974 Yukon Territory, p. 126-127.
- Indian and Northern Affairs Canada** Yukon Mining and Exploration
Overview 1988 p. 35-36.
- Indian and Northern Affairs Canada** Yukon Exploration 1985-1986 p. 337.

STATEMENT OF QUALIFICATIONS

I, Zoran Dujakovic of 4364 Vipond Place, Burnaby, in the Province of British Columbia, hereby certifies that:

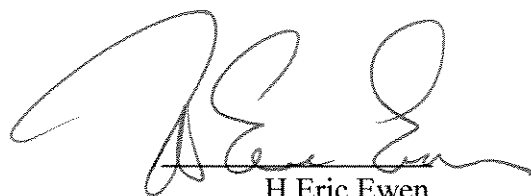
- 1) I am a graduate of the Belgrade University, Faculty of Mining and Geology - Geophysics Program with an Engineer of Geology degree in Geophysics.
- 2) I have been engaged in mining and petroleum exploration since 1981.
- 3) I am a registered as an Engineer of Geology - Geophysics Program with the Chamber of Commerce of Serbia.
- 4) This report is based on fieldwork carried out by SJ Geophysics Ltd. personnel in June/September 1996.
- 5) I own no shares, directly or indirectly in B.Y.G. Natural Resources Inc., nor do I expect to acquire any shares. I have no interest, directly or indirectly, in the Nansen Property.


Zoran Dujakovic
Geophysicists

STATEMENT OF QUALIFICATIONS

I, H. Eric Ewen of 3239 Ganymede Drive, Burnaby, British Columbia, hereby certifies that:

- 1) I am a graduate of Haileybury School of Mines, 1972.
- 2) I have been engaged in mining exploration since 1967.
- 3) THAT this report is based on field work carried out by BYG Natural Resources Inc., and SJ Geophysics Ltd. in May/September 1996.
- 4) THAT I own no shares, directly or indirectly in BYG Natural Resources Inc. I have no interest, directly or indirectly, in the Mt. Nansen Properties.



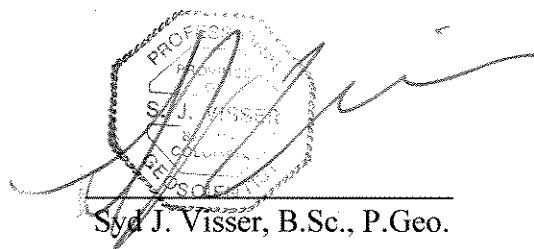
H.Eric Ewen

Mining Technician

STATEMENT OF QUALIFICATIONS

I, Syd J. Visser, of 11762 - 94th Avenue, Delta, British Columbia, hereby certifies that:

- 1) I am a graduate of the University of British Columbia, 1981, where I obtained a B.Sc. (Hon.) Degree in Geology and Geophysics.
- 2) I am a graduate of Haileybury School of Mines, 1971.
- 3) I have been engaged in mining exploration since 1968.
- 4) I am a professional Geoscientist registered in British Columbia.



Syd J. Visser, B.Sc., P.Geo.

Geophysicist/Geologist

APPENDIX I

LIST OF EXPENDITURES

APPENDIX I

LIST OF EXPENDITURES

A) PERSONEL

	<u>DAYS</u>	<u>WAGE</u>	<u>TOTAL</u>
Chris Caron c/o BYG - Mt. Nansen Carmacks, Yukon	64	125	\$ 8,000.00
		Field work,ran grid lines, took soil samples, operate GPS, general camp duties, supervise field work	
Robbie MacLean c/o BYG - Mt. Nansen Carmacks, Yukon	64	125	\$ 8,000.00
		Field work,ran grid lines, took soil samples, operate GPS	
Ryan Perie 48 Regen Cresent Georgetown, Ont.	64	125	\$ 8,000.00
		Field work,ran grid lines, took soil samples, operate GPS	
Wendy McPerson P.O. Box 3917 Whitehorse, Yukon	64	125	\$ 8,000.00
		Field work,ran grid lines, took soil samples, operate GPS	
H. Eric Ewen 3239 Ganymede Dr. Burnaby, B.C.	85	300	\$ 25,500.00
		Supervise exploration program presentation of data, prepare report	
<u>TOTAL WAGES EXPENDITURES</u>			<u>\$ 57,500.00</u>

B) MISCELLANEOUS

Camp costs (field supplies, food, fuel, kitchen trailer rental, etc.)

	<u>PERSONEL</u>	<u>DAYS</u>	<u>COST/DAY</u>		
	7	64	20	\$	8,960.00
<u>TOTAL MISCELLANEOUS</u>				<u>\$</u>	<u>8,960.00</u>

C) RENTALS

	<u>DAYS</u>	<u>COST</u>		
2 ATV's	64	42.8	\$	2,739.20
Suburban	2 MO	1200	\$	2,400.00
GPS	64	49	\$	3,136.00
Generator	2 MO	550	\$	1,100.00
<u>TOTAL RENTALS</u>			<u>\$</u>	<u>9,375.20</u>

D) CONTRACTERS

Twin Mt. Enterprises (Supplied crews and equipment to cut Base Lines) P.O Box 4006, Whitehorse, Yukon	\$	15,857.00
SJ Geophysics (Supplied crews and equipment to carry out mag/vlf surveys and produced geophysics report.) 11762-94 Ave, Delta, B.C., V4C 3R7	\$	46,414.86
ACME Analytical (Chem lab that did ICP analysis) 452 West Hastings St., Vancouver, B.C., V6A 1R6 \$13.75 per sample (analysis + shipping)	\$	10,560.00
<u>TOTAL CONTRACT EXPENDITURES</u>	\$	<u>72,831.86</u>

E) REPORT PREPERATION

	DAYS	COST		
WAGES	5	300	\$	1,500.00
PLOTTING			\$	1,500.00
<u>TOTAL EXPENDITURE OF REPORT PREPERATION</u>			\$	<u>3,000.00</u>

TOTAL EXPENDITURE ON GRIDS PARTIALLY ON KR CLAIMS **\$ 151,667.06**

RECIEPTS ARE AVAILABLE AT BYG NATURAL RESOURCES, 110 INDUSTRIAL RD.
WHITEHORSE, YUKON

THESE COSTS WERE INCURRED FROM MAY 15 1996 to SEPT 5 1996

APPENDIX II

EXPENDITURES AS PER CLAIM GROUP

APPENDIX II

EXPENDITURE AS PER CLAIM GROUP**GROUP #1**

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	2.2	(BASE LINE)	0.5
WAGES CHARGED ON GROUP (2.2/273X57,500)			\$	463.37
MISC. CHARGED ON GROUP (2.2/273X8,960)			\$	72.21
RENTALS CHARGED ON GROUP (2.2/273X9375.2)			\$	75.55
BASE LINE PREP CHARGED ON GROUP (0.5/34X15857)			\$	233.19
GEOPHYSICS CHARGED ON GROUP (2.2/273X46414.86)			\$	374.04
GEOCHEM CHARGED ON GROUP (35X13.75)			\$	481.25
REPORT PREP. CHARGED ON GROUP (2.2/273X3000)			\$	24.18
<u>TOTAL EXPENDITURES</u>			\$	<u>1,723.78</u>

GROUP #2

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	1.9	(BASE LINE)	0.6
WAGES CHARGED ON GROUP (1.9/273X57,500)			\$	400.18
MISC. CHARGED ON GROUP (1.9/273X8,960)			\$	62.36
RENTALS CHARGED ON GROUP (1.9/273X9375.2)			\$	65.25
BASE LINE PREP CHARGED ON GROUP (0.6/34X15857)			\$	279.83
GEOPHYSICS CHARGED ON GROUP (1.9/273X46414.86)			\$	323.03
GEOCHEM CHARGED ON GROUP (35X13.75)			\$	481.25
REPORT PREP. CHARGED ON GROUP (1.9/273X3000)			\$	20.88
<u>TOTAL EXPENDITURES</u>			\$	<u>1,632.78</u>

GROUP #3

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	5	(BASE LINE)	0
WAGES CHARGED ON GROUP (5/273X57,500)			\$	1,053.11
MISC. CHARGED ON GROUP (5/273X8,960)			\$	164.10
RENTALS CHARGED ON GROUP (5/273X9375.2)			\$	171.71
BASE LINE PREP CHARGED ON GROUP (0/34X15857)			\$	-
GEOPHYSICS CHARGED ON GROUP (5/273X46414.86)			\$	850.09
GEOCHEM CHARGED ON GROUP (100X13.75)			\$	1,375.00
REPORT PREP. CHARGED ON GROUP (5/273X3000)			\$	54.95
<u>TOTAL EXPENDITURES</u>			\$	<u>3,668.96</u>

GROUP #4

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4.5	(BASE LINE)	0

WAGES CHARGED ON GROUP (4.5/273X57,500)	\$	947.80
MISC. CHARGED ON GROUP (4.5/273X8,960)	\$	147.69
RENTALS CHARGED ON GROUP (4.5/273X9375.2)	\$	154.54
BASE LINE PREP CHARGED ON GROUP (0/34X15857)	\$	-
GEOPHYSICS CHARGED ON GROUP (4.5/273X46414.86)	\$	765.08
GEOCHEM CHARGED ON GROUP (40X13.75)	\$	550.00
REPORT PREP. CHARGED ON GROUP (4.5/273X3000)	\$	49.45

<u>TOTAL EXPENDITURES</u>	\$	<u>2,614.56</u>
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GROUP #5

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4.5	(BASE LINE)	0.9

WAGES CHARGED ON GROUP (4.5/273X57,500)	\$	947.80
MISC. CHARGED ON GROUP (4.5/273X8,960)	\$	147.69
RENTALS CHARGED ON GROUP (4.5/273X9375.2)	\$	154.54
BASE LINE PREP CHARGED ON GROUP (0.9/34X15857)	\$	419.74
GEOPHYSICS CHARGED ON GROUP (4.5/273X46414.86)	\$	765.08
GEOCHEM CHARGED ON GROUP (0X13.75)	\$	-
REPORT PREP. CHARGED ON GROUP (4.5/273X3000)	\$	49.45

<u>TOTAL EXPENDITURES</u>	\$	<u>2,484.31</u>
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GROUP #6

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4	(BASE LINE)	0

WAGES CHARGED ON GROUP (4/273X57,500)	\$	842.49
MISC. CHARGED ON GROUP (4/273X8,960)	\$	131.28
RENTALS CHARGED ON GROUP (4/273X9375.2)	\$	137.37
BASE LINE PREP CHARGED ON GROUP (0/34X15857)	\$	-
GEOPHYSICS CHARGED ON GROUP (4/273X46414.86)	\$	680.07
GEOCHEM CHARGED ON GROUP (0X13.75)	\$	-
REPORT PREP. CHARGED ON GROUP (4/273X3000)	\$	43.96

<u>TOTAL EXPENDITURES</u>	\$	<u>1,835.17</u>
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GROUP #7

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	8.6	(BASE LINE)	1

WAGES CHARGED ON GROUP (8.6/273X57,500)	\$	1,811.36
MISC. CHARGED ON GROUP (8.6/273X8,960)	\$	282.26
RENTALS CHARGED ON GROUP (8.6/273X9375.2)	\$	295.34
BASE LINE PREP CHARGED ON GROUP (1/34X15857)	\$	466.38
GEOPHYSICS CHARGED ON GROUP (8.6/273X46414.86)	\$	1,462.15
GEOCHEM CHARGED ON GROUP (70X13.75)	\$	962.50
REPORT PREP. CHARGED ON GROUP (8.6/273X3000)	\$	94.51

<u>TOTAL EXPENDITURES</u>	\$	<u>5,374.49</u>
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GROUP #8

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	8.6	(BASE LINE)	0.9

WAGES CHARGED ON GROUP (8.6/273X57,500)	\$	1,811.36
MISC. CHARGED ON GROUP (8.6/273X8,960)	\$	282.26
RENTALS CHARGED ON GROUP (8.6/273X9375.2)	\$	295.34
BASE LINE PREP CHARGED ON GROUP (0.9/34X15857)	\$	419.74
GEOPHYSICS CHARGED ON GROUP (8.6/273X46414.86)	\$	1,462.15
GEOCHEM CHARGED ON GROUP (00X13.75)	\$	-
REPORT PREP. CHARGED ON GROUP (8.6/273X3000)	\$	94.51

<u>TOTAL EXPENDITURES</u>	\$	<u>4,365.35</u>
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GROUP #9

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	2.3	(BASE LINE)	1.2

WAGES CHARGED ON GROUP (2.3/273X57,500)	\$	484.43
MISC. CHARGED ON GROUP (2.3/273X8,960)	\$	75.49
RENTALS CHARGED ON GROUP (2.3/273X9375.2)	\$	78.99
BASE LINE PREP CHARGED ON GROUP (1.2/34X15857)	\$	559.66
GEOPHYSICS CHARGED ON GROUP (2.3/273X46414.86)	\$	391.04
GEOCHEM CHARGED ON GROUP (00X13.75)	\$	-
REPORT PREP. CHARGED ON GROUP (2.3/273X3000)	\$	25.27

<u>TOTAL EXPENDITURES</u>	\$	<u>1,614.88</u>
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GROUP #10

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	2.5	(BASE LINE)	1.6

WAGES CHARGED ON GROUP (2.5/273X57,500)	\$	526.56
MISC. CHARGED ON GROUP (2.5/273X8,960)	\$	82.05
RENTALS CHARGED ON GROUP (2.5/273X9375.2)	\$	85.85
BASE LINE PREP CHARGED ON GROUP (1.6/34X15857)	\$	746.21
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (23X13.75)	\$	316.25
REPORT PREP. CHARGED ON GROUP (2.5/273X3000)	\$	27.47

<u>TOTAL EXPENDITURES</u>	\$	<u>1,784.40</u>
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GROUP #11

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4.2	(BASE LINE)	0

WAGES CHARGED ON GROUP (4.2/273X57,500)	\$	884.62
MISC. CHARGED ON GROUP (4.2/273X8,960)	\$	137.85
RENTALS CHARGED ON GROUP (4.2/273X9375.2)	\$	144.23
BASE LINE PREP CHARGED ON GROUP (0/34X15857)	\$	-
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (35X13.75)	\$	481.25
REPORT PREP. CHARGED ON GROUP (4.2/273X3000)	\$	46.15

<u>TOTAL EXPENDITURES</u>	\$	<u>1,694.10</u>
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GROUP #12

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4.5	(BASE LINE)	0

WAGES CHARGED ON GROUP (4.5/273X57,500)	\$	947.80
MISC. CHARGED ON GROUP (4.5/273X8,960)	\$	147.69
RENTALS CHARGED ON GROUP (4.5/273X9375.2)	\$	154.54
BASE LINE PREP CHARGED ON GROUP (0/34X15857)	\$	-
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (24X13.75)	\$	330.00
REPORT PREP. CHARGED ON GROUP (4.5/273X3000)	\$	49.45

<u>TOTAL EXPENDITURES</u>	\$	<u>1,629.48</u>
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GROUP #13

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	3.4	(BASE LINE)	1.9

WAGES CHARGED ON GROUP (3.4/273X57,500)	\$	716.12
MISC. CHARGED ON GROUP (3.4/273X8,960)	\$	111.59
RENTALS CHARGED ON GROUP (3.4/273X9375.2)	\$	116.76
BASE LINE PREP CHARGED ON GROUP (1.9/34X15857)	\$	886.13
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (8X13.75)	\$	110.00
REPORT PREP. CHARGED ON GROUP (3.4/273X3000)	\$	37.36

<u>TOTAL EXPENDITURES</u>	\$	<u>1,977.96</u>
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GROUP #14

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	0	(BASE LINE)	3.5

WAGES CHARGED ON GROUP (0/273X57,500)	\$	-
MISC. CHARGED ON GROUP (0/273X8,960)	\$	-
RENTALS CHARGED ON GROUP (0/273X9375.2)	\$	-
BASE LINE PREP CHARGED ON GROUP (3.5/34X15857)	\$	1,632.34
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (0X13.75)	\$	-
REPORT PREP. CHARGED ON GROUP (0/273X3000)	\$	-

<u>TOTAL EXPENDITURES</u>	\$	<u>1,632.34</u>
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GROUP #15

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4	(BASE LINE)	3.5

WAGES CHARGED ON GROUP (4/273X57,500)	\$	842.49
MISC. CHARGED ON GROUP (4/273X8,960)	\$	131.28
RENTALS CHARGED ON GROUP (4/273X9375.2)	\$	137.37
BASE LINE PREP CHARGED ON GROUP (3.5/34X15857)	\$	1,632.34
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (70X13.75)	\$	962.50
REPORT PREP. CHARGED ON GROUP (4/273X3000)	\$	43.96

<u>TOTAL EXPENDITURES</u>	\$	<u>3,749.93</u>
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GROUP #16

TOTAL LINE KILOMETRES OF SURVEY	(GRID)	273	(BASE LINE)	34
KILOMETRES OF LINE ON GROUP	(GRID)	4.8	(BASE LINE)	0

WAGES CHARGED ON GROUP (4.8/273X57,500)	\$	1,010.99
MISC. CHARGED ON GROUP (4.8/273X8,960)	\$	157.54
RENTALS CHARGED ON GROUP (4.8/273X9375.2)	\$	164.84
BASE LINE PREP CHARGED ON GROUP (0/34X15857)	\$	-
GEOPHYSICS CHARGED ON GROUP (0/273X46414.86)	\$	-
GEOCHEM CHARGED ON GROUP (60X13.75)	\$	825.00
REPORT PREP. CHARGED ON GROUP (4.8/273X3000)	\$	52.75

<u>TOTAL EXPENDITURES</u>	\$	<u>2,211.11</u>
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<u>TOTAL EXPENSES CHARGED BY GROUP</u>	\$	<u>39,993.59</u>
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APPENDIX III

GEOCHEMISTRY ANALYSIS RESULTS

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GEOCHEMICAL ANALYSIS CERTIFICATE

BYG Natural Resources Inc. PROJECT MT. NANSEN File # 96-2592 Page 1
110 Industrial Road, Whitehorse YT Y1A 2T9

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
5700W 1500N	1	18	18	105	.3	13	8	641	2.86	4	<5	<2	2	31	.3	3	<2	65	.59	.051	13	24	.67	208	.09	5	1.90	.03	.13	<2	4
5700W 1450N	1	12	11	80	<.3	12	8	565	2.63	8	<5	<2	4	27	.2	<2	<2	62	.46	.036	14	23	.69	154	.11	5	1.72	.03	.14	2	3
5700W 1400N	1	20	6	72	<.3	13	8	499	2.87	9	<5	<2	2	28	<.2	2	3	69	.43	.043	17	24	.71	199	.11	3	2.32	.03	.14	<2	1
5700W 1000N	1	31	71	94	<.3	12	7	780	2.53	14	<5	<2	3	24	.5	4	9	59	.44	.049	19	20	.52	160	.07	<3	1.35	.03	.10	<2	1
5700W 950N	<1	23	19	63	<.3	13	6	471	2.39	13	<5	<2	5	27	.2	4	3	53	.39	.022	14	19	.52	129	.09	4	1.24	.03	.12	<2	2
5700W 900N	1	17	12	63	<.3	10	8	421	2.45	13	<5	<2	3	19	.3	<2	<2	54	.26	.020	17	19	.56	137	.08	3	1.75	.02	.09	<2	1
5700W 800N	1	14	50	113	<.3	10	8	738	2.66	29	<5	<2	<2	19	.4	<2	<2	60	.28	.058	21	17	.42	173	.06	3	1.34	.02	.11	<2	1
5700W 700N	1	17	19	77	<.3	10	8	828	2.68	31	<5	<2	<2	17	<.2	2	2	57	.25	.059	23	20	.49	153	.06	3	1.56	.02	.12	<2	1
5700W 650N	1	11	24	70	<.3	9	6	869	2.42	5	<5	<2	<2	17	<.2	<2	2	56	.25	.047	30	13	.37	167	.05	6	1.26	.02	.10	<2	4
5700W 600N	1	14	25	73	<.3	11	8	640	2.50	5	<5	<2	3	17	<.2	2	<2	53	.32	.060	28	20	.42	165	.06	<3	1.20	.02	.14	<2	19
5700W 500N	1	14	29	60	<.3	13	6	554	2.54	10	<5	<2	<2	13	.2	<2	<2	62	.16	.027	14	24	.34	80	.08	<3	1.12	.01	.06	<2	1
5700W 450N	1	9	18	57	<.3	12	5	334	2.01	6	<5	<2	3	13	.2	<2	<2	44	.20	.032	18	20	.34	77	.07	3	1.03	.01	.06	<2	<1
5700W 400N	1	9	23	64	<.3	11	4	423	1.96	8	<5	<2	5	14	.2	2	<2	41	.25	.034	25	19	.31	127	.07	3	.94	.02	.07	<2	2
5700W 300N	1	13	11	73	<.3	13	7	354	2.42	7	<5	<2	<2	13	<.2	<2	<2	54	.17	.032	15	26	.50	85	.08	<3	1.53	.01	.14	<2	2
5700W 250N	1	15	16	74	<.3	11	5	282	2.34	7	<5	<2	2	16	<.2	<2	<2	52	.21	.028	14	26	.46	112	.09	<3	1.53	.02	.10	<2	1
5700W 200N	1	11	12	69	<.3	13	8	553	2.34	6	<5	<2	2	19	<.2	<2	<2	53	.32	.061	20	23	.45	134	.08	<3	1.38	.02	.10	<2	48
5700W 150N	<1	13	14	63	<.3	12	7	463	2.77	3	<5	<2	3	22	<.2	<2	<2	67	.43	.075	21	26	.46	157	.08	5	1.24	.02	.11	<2	4
5700W 100N	1	30	21	132	.3	12	7	546	2.99	9	<5	<2	<2	22	<.2	2	<2	66	.24	.077	28	19	.46	270	.05	4	2.06	.02	.14	<2	3
5700W 50N	1	19	26	83	<.3	12	8	662	2.23	5	<5	<2	<2	26	.3	<2	2	52	.34	.061	16	21	.51	149	.07	<3	1.50	.02	.09	<2	3
5700W 0N	1	17	25	64	<.3	13	6	352	2.20	7	<5	<2	<2	21	<.2	<2	3	51	.24	.058	16	22	.45	142	.07	<3	1.47	.02	.08	<2	3
5600W 1500N	1	19	8	74	<.3	10	8	371	2.17	2	<5	<2	2	28	.2	3	<2	50	.55	.039	16	24	.59	175	.08	<3	1.56	.03	.10	<2	1
5600W 1450N	<1	14	8	60	<.3	11	10	470	2.45	5	<5	<2	3	27	<.2	<2	3	56	.40	.034	16	20	.58	153	.10	<3	1.54	.03	.13	2	2
5600W 1400N	1	27	11	108	.3	20	14	789	3.24	6	<5	<2	<2	50	.5	<2	<2	82	.89	.070	24	35	.88	294	.11	<3	2.87	.04	.15	<2	2
5600W 1350N	<1	14	8	61	<.3	13	7	362	2.13	6	<5	<2	2	25	<.2	<2	3	49	.43	.028	12	21	.56	145	.09	4	1.53	.03	.10	<2	<1
5600W 1150N	1	13	12	63	<.3	7	4	203	1.75	5	<5	<2	<2	19	<.2	3	3	42	.27	.052	14	16	.44	142	.04	3	1.37	.02	.05	<2	<1
5600W 1000N	1	19	8	80	<.3	11	6	489	2.24	9	<5	<2	2	28	.3	<2	3	51	.45	.048	17	22	.58	160	.08	<3	1.58	.03	.13	<2	2
RE 5600W 1000N	<1	18	10	75	<.3	9	6	454	2.14	8	<5	<2	2	26	.2	<2	<2	48	.43	.046	16	21	.55	152	.08	3	1.50	.02	.12	<2	5
5600W 950N	1	12	13	83	<.3	9	7	455	2.29	8	<5	<2	2	21	<.2	2	<2	57	.29	.031	10	22	.45	105	.10	<3	1.31	.02	.10	<2	1
5600W 850N	1	15	46	100	<.3	8	8	652	2.33	35	<5	<2	<2	21	<.2	2	3	48	.38	.058	28	17	.44	193	.04	<3	1.43	.02	.10	<2	5
5600W 800N	1	13	13	68	<.3	9	8	703	2.57	16	<5	<2	2	23	<.2	<2	<2	58	.38	.063	19	19	.57	161	.07	<3	1.56	.02	.14	<2	2
5600W 750N	1	14	28	83	<.3	9	10	1006	2.75	46	<5	<2	<2	19	<.2	3	<2	57	.26	.052	21	19	.54	182	.07	<3	1.68	.02	.20	<2	2
5600W 700N	1	9	13	55	<.3	8	5	499	2.05	15	5	<2	3	16	<.2	<2	<2	42	.30	.061	21	17	.40	143	.06	<3	1.18	.02	.12	<2	1
5600W 650N	2	30	11	72	<.3	10	7	754	2.76	5	<5	<2	<2	19	.2	<2	<2	75	.22	.071	22	22	.31	118	.08	4	1.42	.02	.06	<2	10
5600W 600N	1	18	10	80	<.3	15	6	432	2.75	7	<5	<2	<2	16	<.2	<2	3	66	.19	.036	12	23	.39	90	.08	<3	1.23	.02	.06	<2	5
5600W 550N	2	19	15	83	<.3	16	7	504	3.21	4	<5	<2	<2	16	<.2	<2	<2	77	.19	.037	13	31	.54	87	.11	3	1.64	.02	.10	<2	1
STANDARD C2/AU-S	19	55	36	137	6.0	70	35	1123	3.76	39	18	7	33	50	18.3	16	22	69	.55	.091	38	62	.96	195	.08	28	1.94	.06	.14	14	47

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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DATE RECEIVED: JUL 3 1996 DATE REPORT MAILED: July 10/96 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
5600W 500N	1	14	11	55	<.3	13	8	375	2.23	6	<5	<2	2	13	<.2	<2	<2	49	.17	.018	15	22	.43	84	.09	<3	1.29	.02	.07	<2	2
5600W 450N	1	12	12	58	<.3	11	6	388	2.28	3	<5	<2	<2	13	<.2	<2	<2	52	.15	.021	14	22	.36	80	.09	<3	1.12	.02	.07	<2	1
5600W 400N	1	11	14	73	<.3	15	7	586	2.10	<2	<5	<2	2	14	.2	2	<2	44	.21	.025	25	26	.49	114	.09	<3	1.52	.02	.13	<2	1
5600W 350N	1	15	6	69	<.3	17	8	350	2.86	7	<5	<2	2	16	.3	2	<2	69	.20	.029	14	35	.61	78	.12	<3	1.94	.02	.09	<2	2
5600W 300N	1	15	4	62	<.3	14	7	348	2.48	8	<5	<2	<2	13	<.2	<2	<2	56	.17	.034	17	29	.49	65	.09	<3	1.77	.02	.08	<2	19
5600W 250N	1	12	19	64	<.3	10	10	884	2.49	7	<5	<2	2	20	<.2	2	3	57	.33	.064	22	25	.42	142	.08	<3	1.31	.01	.10	<2	15
5600W 200N	1	33	31	118	<.3	12	13	1163	2.93	8	<5	<2	<2	31	.3	2	5	69	.37	.065	23	28	.83	320	.08	<3	2.20	.02	.23	<2	1
5600W 150N	1	20	16	83	<.3	12	9	601	2.76	12	<5	<2	2	24	.4	<2	<2	64	.31	.060	23	27	.58	213	.08	<3	1.73	.02	.13	<2	<1
5600W 100N	1	18	33	110	<.3	9	10	943	2.93	14	<5	<2	3	20	.2	4	3	63	.28	.052	25	19	.44	255	.05	3	1.63	.02	.16	<2	1
5600W 50N	1	16	12	61	<.3	10	6	353	2.37	4	<5	<2	<2	17	<.2	<2	<2	55	.21	.037	16	24	.42	110	.08	<3	1.22	.02	.07	<2	2
5600W 0N	2	17	17	77	<.3	13	8	545	2.54	8	<5	<2	<2	14	.2	<2	4	63	.14	.037	18	25	.37	107	.08	<3	1.56	.02	.09	<2	2
5500W 1500N	<1	16	3	53	<.3	14	9	503	2.40	5	<5	<2	2	20	<.2	<2	3	54	.25	.039	14	24	.60	111	.09	<3	1.98	.02	.11	<2	1
5500W 1450N	<1	17	5	58	<.3	15	10	395	2.64	11	<5	<2	2	31	<.2	2	4	64	.42	.040	18	25	.66	150	.11	4	2.26	.02	.12	<2	1
5500W 1400N	<1	16	5	66	<.3	10	8	412	2.43	8	<5	<2	2	29	.4	<2	2	58	.39	.035	13	22	.62	113	.10	<3	1.68	.04	.12	<2	2
5500W 1350N	1	17	6	64	<.3	13	9	346	2.56	7	<5	<2	2	22	.5	2	4	60	.31	.028	16	26	.54	156	.08	4	1.97	.02	.09	<2	<1
5500W 1300N	<1	13	11	71	<.3	9	7	587	2.31	6	<5	<2	2	31	<.2	<2	2	54	.54	.033	13	20	.63	129	.08	<3	1.63	.03	.11	<2	1
5500W 850N	1	20	23	87	<.3	10	12	685	3.08	11	<5	<2	4	23	.3	<2	3	74	.28	.034	14	26	.80	143	.07	<3	2.50	.02	.22	<2	3
5500W 800N	1	14	16	79	<.3	9	9	915	2.52	11	<5	<2	2	20	<.2	<2	<2	49	.28	.047	14	18	.41	189	.05	3	1.44	.02	.14	<2	2
5500W 750N	1	23	41	84	<.3	17	12	1115	3.07	16	<5	<2	3	18	<.2	<2	5	67	.21	.044	18	33	.73	196	.10	3	2.79	.02	.15	<2	3
5500W 700N	1	20	31	72	<.3	10	11	836	2.63	9	<5	<2	<2	19	<.2	2	3	59	.20	.045	25	24	.63	182	.07	<3	2.26	.02	.16	<2	2
5500W 650N	<1	14	11	76	<.3	5	11	973	2.64	<2	<5	<2	4	57	<.2	<2	<2	65	.64	.042	17	14	1.36	697	.02	<3	3.49	.01	.32	<2	1
5500W 600N	1	25	24	87	<.3	15	9	668	2.81	10	<5	<2	<2	29	<.2	2	5	65	.34	.074	21	33	.79	242	.07	<3	2.38	.02	.13	<2	1
5500W 500N	1	17	34	107	<.3	10	11	821	2.91	4	<5	<2	5	20	.5	<2	<2	63	.33	.043	31	29	.82	272	.08	<3	2.07	.02	.33	<2	4
5500W 450N	2	33	60	117	<.3	13	20	2664	2.79	8	<5	<2	<2	22	.3	<2	3	56	.23	.081	35	26	.69	318	.05	<3	2.63	.02	.14	<2	2
5500W 400N	1	45	291	94	<.3	13	7	1052	2.45	11	<5	<2	5	18	.5	4	<2	61	.30	.062	30	23	.42	200	.08	<3	1.29	.02	.11	<2	2
5500W 350N	1	17	19	64	<.3	13	7	419	2.59	4	<5	<2	<2	16	<.2	<2	2	64	.17	.036	12	25	.39	98	.09	<3	1.31	.02	.08	<2	2
5500W 300N	1	20	14	71	<.3	11	8	533	2.96	6	<5	<2	<2	16	<.2	<2	<2	84	.16	.048	11	21	.31	88	.10	<3	1.06	.01	.06	<2	<1
RE 5500W 250N	<1	19	17	84	<.3	13	7	510	2.41	8	<5	<2	3	21	.2	<2	3	58	.31	.050	17	27	.54	124	.10	<3	1.42	.02	.09	<2	10
5500W 250N	<1	21	20	88	<.3	16	9	525	2.47	8	<5	<2	3	22	<.2	<2	5	60	.32	.053	17	28	.56	132	.11	4	1.49	.02	.10	<2	46
5500W 200N	1	13	10	52	<.3	11	6	338	2.09	6	<5	<2	<2	13	<.2	<2	3	44	.16	.026	17	21	.44	123	.07	4	1.45	.02	.08	<2	<1
5500W 150N	<1	13	21	94	<.3	13	8	711	2.66	5	<5	<2	4	20	<.2	2	2	58	.37	.061	25	23	.59	215	.08	4	1.58	.02	.15	<2	15
5500W 100N	1	17	15	92	<.3	9	7	403	2.44	4	<5	<2	<2	17	.2	2	<2	62	.15	.049	13	16	.27	127	.06	<3	1.05	.02	.07	<2	3
5500W 50N	1	17	37	185	<.3	12	9	861	2.47	9	<5	<2	4	16	.8	2	4	48	.20	.034	28	24	.47	212	.07	<3	1.63	.02	.11	<2	41
5500W 0N	1	9	21	58	<.3	8	5	583	1.74	4	<5	<2	6	12	.4	3	6	36	.21	.040	27	14	.26	149	.06	5	.93	.01	.07	<2	2
5400W 1500N	<1	21	19	69	<.3	13	12	537	3.16	6	<5	<2	2	21	<.2	2	4	63	.31	.042	14	27	.62	112	.07	3	2.47	.02	.12	<2	2
STANDARD C2/AU-S	19	55	38	142	6.0	72	37	1139	3.87	42	20	8	35	52	19.4	17	23	72	.52	.088	41	65	.99	205	.09	31	2.02	.06	.15	13	53

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
5400W 1400N	1	25	21	71	<.3	12	9	856	3.09	5	<5	<2	5	36	<.2	<2	3	59	.47	.022	30	17	.52	255	.04	<3	1.94	.02	.10	<2	2
5400W 1300N	1	17	8	53	<.3	14	7	287	2.41	5	<5	<2	<2	22	<.2	<2	3	53	.29	.046	13	26	.52	118	.09	5	2.11	.01	.09	<2	2
5400W 1250N	2	28	26	72	<.3	10	13	1219	3.73	2	<5	<2	3	21	<.2	<2	11	73	.33	.057	16	15	.55	211	.06	3	1.62	.02	.15	<2	1
5400W 700N	1	22	32	97	<.3	13	9	1100	2.43	31	<5	<2	<2	24	.6	2	4	58	.31	.071	17	26	.51	190	.07	5	1.61	.02	.08	<2	1
5400W 600N	1	12	25	87	<.3	12	9	646	2.72	44	<5	<2	<2	17	.4	<2	<2	75	.25	.059	16	21	.38	151	.10	5	1.18	.02	.08	<2	3
5400W 500N	1	20	40	139	<.3	16	8	793	2.90	7	<5	<2	<2	23	.5	<2	2	67	.31	.067	22	30	.57	255	.08	<3	1.83	.01	.11	<2	3
5400W 450N	1	15	36	127	<.3	13	7	590	2.43	6	<5	<2	2	15	.2	<2	3	54	.21	.040	19	24	.42	119	.08	4	1.34	.02	.09	<2	1
5400W 400N	2	22	53	145	<.3	13	11	1257	2.90	13	<5	<2	<2	19	.7	<2	6	69	.23	.074	20	25	.40	198	.07	4	1.50	.02	.11	2	2
5400W 350N	2	9	141	120	<.3	5	3	665	1.37	8	<5	<2	4	14	.2	<2	4	18	.08	.028	32	7	.10	149	.01	4	.62	.01	.12	<2	1
5400W 300N	2	22	32	109	<.3	21	9	817	2.91	11	<5	<2	<2	16	.3	<2	3	68	.19	.044	13	30	.51	118	.09	3	1.57	.01	.08	<2	2
5400W 250N	1	16	23	81	<.3	19	7	510	2.58	7	<5	<2	2	15	<.2	<2	2	58	.21	.028	15	30	.58	101	.10	<3	1.72	.02	.10	<2	5
5400W 200N	1	16	20	73	<.3	18	7	524	2.18	13	<5	<2	3	13	.3	<2	2	48	.19	.020	14	24	.49	94	.09	4	1.40	.02	.08	<2	3
5400W 150N	2	7	27	105	<.3	6	4	1501	1.37	9	<5	<2	8	10	<.2	3	<2	22	.10	.005	23	8	.17	291	.05	<3	.66	.01	.06	<2	13
5400W 100N	<1	13	8	43	<.3	17	7	299	1.85	7	<5	<2	3	11	<.2	<2	<2	40	.17	.017	14	20	.40	71	.08	<3	1.29	.01	.06	<2	3
5400W 50N	<1	13	9	51	<.3	15	7	336	2.09	6	<5	<2	<2	13	.2	<2	<2	45	.18	.028	18	21	.44	129	.07	<3	1.47	.02	.08	<2	2
5400W 0N	1	26	17	81	<.3	11	12	1011	3.18	<2	<5	<2	<2	21	<.2	2	2	93	.26	.060	11	22	.73	482	.10	<3	1.81	.02	.19	<2	1
5350W 1500N	1	138	105	81	.8	13	10	608	2.49	6	<5	<2	7	26	.5	3	18	46	.58	.024	33	20	.58	282	.06	<3	1.46	.02	.10	<2	4
5350W 1450N	2	98	26	68	.6	18	12	1152	2.96	11	<5	<2	4	43	<.2	3	16	62	1.03	.066	43	30	.62	497	.05	<3	2.32	.02	.12	<2	3
5350W 1400N	1	28	15	70	.3	17	9	467	2.50	5	<5	<2	5	41	.4	<2	11	56	.57	.058	29	25	.57	155	.09	<3	1.57	.02	.09	<2	2
5350W 1350N	1	17	13	59	<.3	20	10	533	2.95	10	<5	<2	2	15	<.2	<2	4	61	.21	.033	14	31	.59	129	.09	<3	2.39	.02	.11	<2	4
5350W 1300N	1	14	7	45	<.3	18	9	283	2.57	7	<5	<2	4	18	<.2	<2	4	55	.25	.025	13	25	.48	108	.10	<3	2.05	.02	.07	<2	11
5350W 1250N	1	18	13	71	<.3	7	9	744	3.39	4	<5	<2	4	34	<.2	<2	11	76	.65	.029	17	19	.94	279	.09	<3	2.42	.04	.13	<2	1
5350W 1150N	1	18	12	61	<.3	14	10	529	3.33	15	<5	<2	6	25	<.2	<2	6	67	.37	.030	27	23	.68	274	.08	3	1.98	.02	.16	<2	3
5350W 1100N	1	10	10	73	<.3	14	8	657	2.19	23	<5	<2	3	20	.2	<2	2	47	.30	.021	11	20	.53	124	.08	<3	1.49	.02	.11	<2	31
RE 5350W 1100N	<1	11	11	74	<.3	12	8	676	2.23	23	<5	<2	3	22	<.2	<2	4	49	.31	.024	11	21	.54	124	.08	<3	1.54	.02	.12	<2	3
5350W 750N	1	43	65	119	.6	14	8	750	2.99	51	<5	<2	4	13	.9	11	<2	57	.17	.023	18	26	.45	107	.08	<3	1.47	.02	.09	<2	6
5350W 700N	1	19	28	86	<.3	13	8	843	2.62	27	<5	<2	2	17	<.2	<2	<2	56	.22	.043	21	26	.58	150	.07	<3	1.78	.01	.11	<2	4
5350W 650N	1	14	29	82	<.3	13	7	811	2.39	26	<5	<2	3	13	.4	<2	2	51	.17	.029	16	23	.46	124	.08	3	1.46	.02	.11	<2	3
5350W 600N	2	19	37	95	<.3	17	9	729	3.26	25	<5	<2	3	15	<.2	2	5	68	.17	.032	18	31	.62	119	.07	3	2.34	.01	.14	<2	3
5350W 550N	1	15	29	79	<.3	13	6	559	2.63	5	<5	<2	<2	13	.3	<2	2	62	.15	.027	15	26	.39	78	.06	<3	1.40	.01	.07	<2	1
5350W 500N	1	14	20	57	<.3	14	6	311	2.56	6	<5	<2	2	13	.2	<2	4	64	.17	.029	16	27	.43	81	.10	<3	1.62	.02	.07	<2	1
5350W 450N	1	9	12	44	<.3	10	5	453	2.16	4	<5	<2	4	11	<.2	<2	4	48	.19	.022	19	21	.38	69	.08	<3	1.10	.02	.09	<2	1
5350W 400N	1	19	16	75	<.3	23	9	443	2.89	9	<5	<2	4	16	.3	2	3	68	.22	.033	16	38	.70	121	.11	<3	2.36	.02	.09	<2	2
5350W 350N	1	8	24	74	<.3	10	6	725	1.82	16	<5	<2	8	12	.3	3	3	28	.11	.021	23	11	.24	161	.03	<3	1.02	.01	.14	<2	<1
5350W 300N	2	13	19	68	<.3	13	5	451	2.48	11	<5	<2	2	12	<.2	2	5	56	.14	.033	17	23	.32	80	.07	3	1.34	.02	.07	<2	4
STANDARD C2/AU-S	18	55	43	137	5.8	74	34	1098	3.67	36	16	7	33	49	18.6	16	24	69	.55	.093	38	62	.95	194	.09	27	1.92	.06	.14	15	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
5350W 250N	2	21	169	156	<.3	7	5	1016	2.08	26	<5	<2	6	10	.6	4	2	33	.09	.026	27	16	.24	151	.03	<3	1.03	.01	.07	<2	2
5350W 200N	1	13	149	186	<.3	6	3	646	1.67	6	<5	<2	7	9	.4	3	<2	22	.06	.020	28	11	.19	89	.03	<3	.99	.01	.09	<2	24
5350W 150N	1	13	41	81	<.3	11	6	472	2.19	8	<5	<2	3	11	.3	<2	2	47	.16	.019	18	21	.38	91	.07	<3	1.43	.02	.08	<2	9
5350W 100N	2	28	50	118	<.3	14	9	812	2.78	7	<5	<2	4	20	.4	3	<2	54	.22	.037	34	28	.64	287	.06	<3	2.30	.02	.18	<2	2
5350W 50N	2	34	76	80	<.3	18	9	791	2.90	5	<5	<2	4	16	.5	6	3	71	.29	.058	19	35	.70	94	.07	<3	1.48	.02	.11	2	14
5350W 0N	2	17	26	78	<.3	11	12	1395	2.97	12	<5	<2	2	17	<.2	4	2	59	.26	.045	17	21	.53	230	.04	<3	1.52	.02	.12	<2	1
5250W 1500N	3	19	19	46	<.3	7	7	389	2.72	6	<5	<2	3	20	<.2	<2	7	60	.25	.020	14	16	.28	98	.06	<3	1.25	.02	.07	<2	4
5250W 1450N	2	12	10	43	<.3	10	6	241	2.64	7	<5	<2	2	15	<.2	<2	<2	69	.20	.015	11	22	.43	68	.10	<3	1.81	.02	.08	<2	2
5250W 1400N	3	31	19	69	<.3	12	13	708	3.86	5	<5	<2	5	20	<.2	<2	3	69	.27	.024	20	21	.48	188	.05	<3	2.10	.02	.10	<2	2
5250W 1350N	4	134	41	106	.3	8	19	1692	4.26	64	<5	<2	6	18	<.2	10	12	54	.23	.014	22	14	.32	335	.04	<3	1.09	.02	.08	<2	2
5250W 1300N	2	23	24	62	<.3	17	9	386	3.10	8	<5	<2	5	14	.3	3	3	64	.18	.026	15	32	.52	111	.09	<3	2.14	.02	.08	2	11
5250W 1250N	4	49	61	275	.3	13	18	1173	4.92	<2	<5	<2	4	13	.7	2	10	103	.14	.041	13	40	.86	157	.05	5	3.71	.02	.15	2	1
5250W 1200N	1	26	33	119	.7	17	12	703	3.00	7	<5	<2	3	16	.8	<2	<2	61	.20	.034	13	27	.66	139	.10	3	3.14	.02	.13	2	3
5250W 1150N	3	21	13	83	<.3	14	15	869	4.03	15	<5	<2	6	26	.2	2	<2	81	.41	.028	38	27	.86	351	.10	<3	2.53	.04	.23	<2	1
5250W 900N	1	18	17	65	<.3	10	10	501	2.66	9	<5	<2	4	19	.4	3	<2	62	.31	.042	15	28	.55	143	.09	<3	1.80	.02	.12	<2	4
5250W 800N	1	30	25	83	.3	10	7	621	2.46	52	<5	<2	2	18	.2	5	<2	51	.29	.024	15	20	.46	159	.07	<3	1.19	.02	.11	2	5
5250W 750N	3	32	136	159	.8	9	8	972	2.94	14	<5	<2	<2	17	.4	6	2	58	.24	.046	14	19	.30	162	.05	<3	.95	.02	.12	<2	4
5250W 700N	1	16	28	74	<.3	8	6	423	2.45	26	<5	<2	2	15	.3	2	53	.20	.037	16	22	.39	98	.06	<3	1.31	.01	.09	<2	7	
5250W 650N	11	60	196	209	1.5	14	11	1619	3.67	18	5	<2	2	24	.7	8	6	62	.32	.061	20	26	.41	525	.04	3	1.51	.02	.11	<2	14
5250W 600N	2	13	39	78	<.3	7	6	848	2.26	62	<5	<2	4	14	<.2	3	5	40	.22	.028	18	17	.31	152	.05	<3	.90	.02	.08	3	3
RE 5250W 600N	2	15	40	78	<.3	9	5	889	2.28	67	<5	<2	4	15	.3	3	<2	41	.22	.029	20	17	.31	162	.05	<3	.89	.02	.08	<2	7
5250W 550N	3	39	143	160	1.0	7	5	1466	2.25	19	<5	<2	7	18	.5	9	2	40	.24	.032	22	18	.32	310	.05	<3	.99	.01	.09	<2	13
5250W 500N	2	16	41	78	<.3	15	6	436	2.51	10	<5	<2	2	12	<.2	<2	<2	58	.13	.026	14	25	.38	126	.08	<3	1.35	.01	.08	<2	7
5250W 450N	2	15	92	120	.4	4	3	316	1.08	6	<5	<2	8	10	.3	6	2	10	.05	.013	24	6	.10	84	.01	<3	.60	.02	.11	<2	6
5250W 400N	2	15	23	67	<.3	12	6	530	2.35	7	<5	<2	<2	16	<.2	<2	<2	57	.18	.044	12	24	.41	128	.06	4	1.45	.02	.09	<2	2
5250W 350N	1	15	38	132	<.3	11	9	862	3.02	23	<5	<2	3	18	<.2	3	<2	63	.21	.036	22	24	.72	270	.06	<3	2.57	.02	.21	<2	4
5250W 300N	3	14	48	105	.3	9	4	259	2.29	44	<5	<2	6	13	.4	6	3	48	.15	.019	17	19	.32	87	.09	3	1.12	.01	.10	<2	4
5250W 250N	4	24	83	148	1.0	8	7	1134	2.48	19	<5	<2	10	15	.6	19	8	39	.24	.035	28	16	.25	338	.05	<3	.86	.01	.09	<2	7
5250W 200N	1	16	25	52	<.3	12	5	346	2.39	9	<5	<2	2	10	<.2	2	4	45	.16	.034	14	27	.40	63	.09	3	1.49	.01	.09	<2	11
5250W 150N	3	37	90	161	<.3	15	10	1172	3.08	13	<5	<2	2	23	.8	4	2	62	.26	.050	29	33	.68	377	.06	<3	2.61	.01	.17	<2	3
5250W 100N	6	33	100	156	.9	14	14	1138	4.41	69	<5	<2	<2	28	.5	20	4	75	.33	.088	24	28	.47	292	.05	<3	1.80	.02	.11	<2	13
5250W 50N	5	23	25	137	<.3	13	19	782	4.00	61	<5	<2	4	37	.7	4	2	90	.50	.039	16	29	1.11	223	.07	<3	2.45	.09	.50	<2	2
5250W 0N	21	32	29	85	<.3	11	10	1585	3.20	7	<5	<2	<2	12	<.2	<2	<2	54	.18	.032	23	20	.48	136	.04	<3	1.38	.02	.07	<2	4
5100W 1500N	1	22	10	77	.3	11	7	587	2.40	2	<5	<2	<2	48	.5	<2	<2	57	.99	.071	23	26	.68	251	.08	<3	1.98	.03	.12	<2	2
5100W 1450N	1	16	10	64	<.3	15	9	516	2.77	3	<5	<2	4	25	.3	<2	<2	62	.38	.032	20	25	.70	171	.11	<3	2.11	.03	.13	<2	1
STANDARD C2/AU-S	20	57	34	140	6.2	68	36	1137	3.81	39	20	7	34	51	19.3	18	18	71	.55	.087	39	63	.95	192	.09	29	1.97	.06	.15	14	52

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
5100W 1250N	1	65	21	91	.9	15	8	487	2.63	8	<5	<2	4	23	<.2	3	6	57	.32	.031	20	26	.72	328	.09	<3	2.13	.03	.08	<2	2
5100W 1150N	2	49	56	128	6.9	12	7	558	3.02	34	<5	<2	<2	33	.7	14	5	75	.47	.075	15	22	.45	407	.04	<3	2.07	.02	.10	<2	3
5100W 1100N	<1	13	13	52	<.3	14	7	507	2.28	18	<5	<2	4	19	.2	<2	<2	45	.33	.045	16	20	.50	170	.07	<3	1.51	.02	.10	<2	2
5100W 1050N	<1	14	11	41	<.3	14	8	391	2.00	8	<5	<2	3	13	<.2	<2	3	42	.22	.033	13	21	.44	85	.08	<3	1.50	.02	.07	2	3
5100W 1000N	2	50	33	59	1.0	13	7	338	3.01	15	<5	<2	4	19	<.2	5	5	63	.26	.019	15	22	.53	141	.07	3	1.83	.02	.08	<2	7
5100W 950N	1	22	20	53	.3	13	7	300	2.92	14	<5	<2	2	13	.2	2	3	64	.16	.020	14	23	.44	106	.08	<3	1.80	.01	.07	2	15
5100W 900N	1	32	30	67	.3	17	9	449	3.07	13	<5	<2	2	13	.2	<2	4	56	.21	.037	13	25	.53	92	.07	<3	1.99	.02	.09	<2	2
5100W 850N	2	32	58	107	<.3	21	12	893	3.63	14	<5	<2	5	14	<.2	<2	4	71	.18	.036	16	34	.59	161	.08	<3	3.10	.01	.12	<2	6
5100W 750N	2	40	60	130	1.0	14	12	1027	3.29	24	<5	<2	<2	32	.9	7	5	61	.60	.101	23	27	.57	489	.02	<3	1.89	.01	.10	<2	8
5100W 700N	1	31	61	130	.5	13	11	931	3.19	12	<5	<2	2	31	.6	2	<2	65	.67	.052	19	22	.81	318	.04	3	2.13	.01	.13	<2	3
5100W 650N	1	27	51	126	.3	13	10	713	2.78	9	<5	<2	4	37	.7	3	<2	56	.35	.033	16	21	.79	274	.07	<3	2.28	.03	.14	<2	20
5100W 600N	1	24	65	135	.8	11	10	1034	3.36	44	<5	<2	2	32	.2	4	4	62	.80	.053	24	20	.77	337	.03	3	2.36	.02	.14	<2	5
5100W 500N	4	67	71	115	.8	16	8	578	2.39	35	<5	<2	5	15	.5	11	10	40	.21	.028	17	19	.38	154	.06	4	1.11	.01	.12	<2	5
5100W 450N	3	25	84	144	<.3	15	10	1040	2.94	13	<5	<2	3	21	.7	10	5	54	.29	.036	19	24	.64	296	.05	<3	1.96	.02	.14	<2	4
5100W 400N	2	28	48	84	.6	13	7	431	2.46	12	<5	<2	<2	20	.2	3	3	46	.33	.040	14	20	.43	193	.05	<3	1.48	.01	.09	<2	4
5100W 350N	2	37	62	98	1.2	12	6	687	2.30	7	<5	<2	<2	25	1.1	2	3	49	.36	.047	25	16	.32	273	.04	<3	1.55	.02	.08	2	3
RE 5100W 350N	2	40	60	99	1.3	9	7	689	2.31	7	<5	<2	<2	25	1.1	2	3	48	.36	.049	26	16	.32	280	.04	3	1.58	.02	.08	<2	5
5100W 300N	2	20	78	105	.4	14	7	564	2.52	12	<5	<2	3	15	.5	2	4	49	.22	.023	11	22	.46	105	.07	<3	1.52	.02	.09	<2	3
5100W 250N	2	37	92	126	.3	14	6	632	2.23	16	<5	<2	4	18	1.0	4	4	43	.30	.040	14	19	.43	190	.07	<3	1.08	.02	.09	2	5
5100W 200N	2	17	41	91	.4	8	8	589	2.32	12	<5	<2	2	23	.4	3	4	48	.35	.031	15	17	.52	314	.05	3	1.34	.01	.11	<2	7
5100W 150N	1	11	55	91	<.3	11	7	524	2.26	7	<5	<2	2	17	1.0	3	3	48	.28	.042	13	16	.40	118	.06	<3	1.01	.02	.10	<2	2
5100W 50N	2	19	29	84	<.3	16	9	703	2.72	7	<5	<2	2	25	<.2	2	3	62	.41	.037	16	22	.71	205	.07	<3	1.97	.02	.12	<2	5
5100W 0N	2	15	14	54	<.3	11	7	380	2.62	6	<5	<2	<2	20	<.2	<2	3	68	.23	.032	12	17	.48	109	.08	<3	1.40	.02	.08	<2	1
STANDARD C2/AU-S	19	55	39	135	5.9	74	34	1094	3.68	42	18	7	32	48	19.7	17	21	67	.54	.088	37	59	.95	196	.07	26	1.87	.06	.13	13	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

22

Term Samples
 $4 \times 34 + 22 = 158$

11

11

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T-900 1800	4	131	97	179	.5	12	5	244	3.19	20	12	<2	5	20	1.0	5	<2	69	.33	.050	17	26	.59	177	.09	<3	1.13	.01	.10	<2	14
T-900 1825	11	371	173	404	.6	18	11	1066	5.24	71	<5	<2	6	22	1.6	19	<2	50	.35	.088	24	22	.42	221	.02	3	1.04	.01	.09	<2	40
T-900 1850	10	440	131	325	1.5	16	8	425	3.94	46	<5	<2	5	30	4.0	8	<2	60	.43	.059	28	29	.56	308	.04	3	1.59	.01	.12	<2	95
T-900 1875	5	194	121	210	.8	15	7	380	3.38	38	16	<2	4	19	1.3	7	2	57	.34	.051	15	24	.41	201	.05	<3	1.25	.02	.10	<2	78
T-900 1900	5	319	79	202	2.0	12	7	604	3.03	46	16	<2	3	33	1.8	6	<2	60	.42	.040	16	24	.36	314	.04	<3	1.31	.02	.10	<2	37
T-900 1925	5	285	65	241	.8	13	7	523	3.56	53	15	<2	5	22	1.0	12	<2	56	.30	.036	17	24	.40	227	.05	<3	1.19	.01	.08	<2	31
T-900 1950	11	382	101	416	.7	14	8	770	4.75	101	<5	<2	5	34	3.2	15	<2	72	.37	.077	24	25	.37	272	.04	<3	1.14	.01	.10	<2	136
T-900 1975	17	1049	60	307	1.2	21	15	1240	4.98	59	16	<2	7	50	3.9	7	<2	96	.57	.094	28	40	1.23	364	.11	<3	2.21	.01	.20	<2	109
T-900 2000	17	958	37	204	2.1	17	8	475	3.71	42	17	<2	4	62	2.9	12	<2	64	.56	.070	32	27	.66	492	.04	<3	2.33	.02	.12	<2	42
T-900 2025	29	861	50	241	1.1	17	13	892	4.76	62	14	<2	5	37	3.4	12	<2	82	.42	.091	33	35	.79	372	.05	<3	1.91	.01	.12	<2	293
T-900 2050	24	678	46	244	1.3	15	11	557	4.98	50	13	<2	3	47	1.7	12	<2	91	.41	.084	24	33	.81	403	.06	<3	2.19	.02	.16	<2	66
T-900 2075	52	845	48	266	1.3	13	13	569	7.04	91	13	<2	8	26	1.7	8	4	84	.22	.076	22	36	.83	204	.05	<3	2.12	.01	.16	<2	117
T-900 2100	15	312	27	137	.7	12	6	408	3.38	41	13	<2	2	26	.8	7	<2	63	.26	.044	16	28	.55	246	.05	<3	1.70	.01	.12	<2	28
RE T-900 2100	14	311	29	135	.8	12	6	405	3.33	38	14	<2	2	25	.9	10	<2	62	.26	.043	15	28	.54	242	.06	<3	1.68	.01	.11	2	33
T-900 2125	15	567	33	205	1.0	10	9	581	4.46	80	11	<2	5	41	1.0	11	4	67	.38	.075	30	25	.56	328	.06	<3	1.41	.02	.11	<2	124
T-900 2150	26	868	70	366	2.6	11	19	1526	6.67	116	40	<2	8	57	2.1	16	9	74	.41	.096	65	26	.54	392	.03	<3	2.04	.01	.15	<2	392
T-900 2175	35	481	72	162	1.6	6	5	200	5.75	114	7	<2	9	49	.6	18	9	63	.20	.092	29	17	.53	375	.03	<3	1.45	.01	.17	2	201
T-900 2200	28	178	106	78	1.8	4	3	118	4.05	81	<5	<2	3	28	.4	11	4	49	.17	.082	27	11	.21	348	.02	<3	1.00	.02	.09	<2	84
T-900 2225	14	190	57	94	2.7	7	6	227	4.14	34	10	<2	2	26	1.1	13	4	79	.20	.106	20	15	.41	336	.03	<3	1.74	.02	.11	<2	46
T-900 2250	26	154	74	121	2.4	9	4	175	4.95	54	<5	<2	4	40	.6	10	5	67	.19	.087	26	19	.62	262	.02	<3	2.23	.02	.15	<2	120
T-900 2275	26	433	45	142	1.0	8	13	505	6.04	28	<5	<2	15	125	1.2	5	<2	104	.29	.125	40	19	1.40	391	.06	<3	2.65	.04	.36	<2	104
T-900 2300	14	123	38	85	1.0	9	4	187	2.96	25	18	<2	3	22	.3	9	<2	67	.27	.070	25	23	.53	230	.04	<3	1.75	.01	.13	<2	51
T-900 2325	18	181	62	144	1.0	11	7	342	4.80	34	5	<2	8	40	1.2	12	5	102	.34	.104	26	28	.97	319	.07	<3	2.38	.02	.16	<2	64
T-900 2350	4	73	97	137	1.9	8	7	258	3.73	50	12	<2	3	23	.6	10	5	65	.22	.089	20	22	.44	275	.02	<3	2.08	.01	.13	<2	64
T-900 2375	4	117	166	169	2.3	9	8	515	5.65	138	<5	<2	6	45	.9	35	43	76	.25	.085	28	23	.45	327	.03	<3	1.39	.02	.19	<2	214
T-900 2650	2	32	33	116	.5	13	6	349	3.54	39	5	<2	3	22	.5	4	4	84	.34	.038	17	29	.50	173	.07	<3	1.56	.01	.07	2	24
T-900 2675	3	87	52	188	1.9	18	8	404	3.94	59	7	<2	5	32	.9	8	6	91	.47	.060	23	37	.64	313	.04	<3	2.85	.01	.13	<2	71
T-900 2700	3	54	58	150	1.3	11	9	382	3.54	55	10	<2	5	28	.7	5	8	78	.45	.071	23	25	.61	220	.05	<3	2.00	.02	.09	<2	193
T-900 2725	2	30	58	180	.3	8	9	557	3.14	26	16	<2	5	26	.7	4	<2	75	.49	.087	16	19	.64	153	.09	<3	1.35	.02	.09	<2	26
T-900 2750	2	29	46	179	.5	11	6	257	3.07	42	9	<2	6	25	1.5	4	<2	67	.42	.062	18	24	.50	204	.06	<3	1.49	.02	.09	<2	65
T-900 2775	1	25	26	118	.3	13	5	241	3.01	24	<5	<2	5	22	.5	4	3	73	.42	.066	19	26	.43	177	.07	<3	1.37	.02	.08	<2	54
T-900 2800	2	26	37	119	.6	10	5	173	2.97	24	9	<2	5	23	.6	2	3	90	.44	.072	24	30	.41	171	.05	<3	1.46	.01	.08	<2	176
T-900 2825	3	33	43	145	.8	12	6	214	3.49	43	12	<2	4	23	.7	9	4	80	.39	.064	22	24	.57	194	.05	<3	1.93	.01	.09	<2	201
T-900 2850	2	24	36	107	<.3	10	7	309	2.91	30	5	<2	4	21	.4	4	<2	65	.39	.070	16	24	.49	158	.07	<3	1.40	.02	.07	<2	14
T-900 2875	1	18	31	97	.3	10	6	296	2.65	21	<5	<2	5	21	.4	2	2	66	.39	.069	18	24	.43	129	.07	<3	1.28	.01	.07	<2	8
STANDARD C2/AU-S	20	60	41	131	6.3	70	33	1120	3.73	46	24	8	35	48	19.5	19	18	70	.55	.101	40	63	.99	195	.08	28	1.92	.06	.13	12	43

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

- SAMPLE TYPE: SOIL AU* - IGNITED, AQUA-REGIA/MIBK EXTRACT, GF/AA FINISHED.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 16 1996

DATE REPORT MAILED:

Aug 28/96

SIGNED BY: C. L. JOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T-900 2900	1	22	27	103	<.3	14	5	235	3.02	20	<5	<2	5	23	.5	<2	<2	80	.42	.074	18	33	.54	183	.09	3	1.77	.02	.09	<2	9
T-1000 1925	7	259	11	91	.5	11	5	368	3.11	21	8	<2	3	22	.9	<2	<2	68	.29	.041	19	27	.51	231	.07	<3	1.46	.01	.09	<2	25
T-1000 1950	17	722	34	212	1.1	16	20	1328	4.16	43	<5	<2	2	39	2.6	6	<2	67	.31	.055	20	34	.64	488	.05	<3	2.52	.01	.14	<2	52
T-1000 2000	9	302	22	115	.5	12	8	354	3.69	31	<5	<2	5	24	.9	3	<2	87	.33	.055	13	28	.74	176	.10	<3	2.06	.01	.12	<2	31
T-1000 2025	41	759	60	241	.9	12	15	551	6.01	92	<5	<2	9	32	2.2	11	<2	92	.29	.090	24	25	1.02	325	.07	<3	2.43	.01	.16	<2	152
T-1000 2100	14	284	20	87	.3	7	3	208	2.90	27	<5	<2	5	19	.7	3	<2	51	.24	.055	16	17	.35	134	.05	<3	1.02	.01	.08	<2	53
T-1000 2125	24	535	57	143	1.5	11	10	718	6.94	74	13	<2	6	29	1.5	11	5	63	.20	.068	19	29	.43	259	.03	<3	2.21	.02	.13	<2	83
T-1000 2150	13	905	52	301	3.1	18	24	1953	4.15	53	16	<2	7	35	2.6	6	6	61	.26	.051	32	34	.49	404	.03	<3	2.81	.02	.12	<2	125
T-1000 2175	40	454	97	125	2.5	7	11	969	5.89	126	<5	<2	7	44	.7	15	14	54	.18	.095	28	19	.37	343	.01	<3	1.79	.02	.15	<2	677
T-1000 2200	32	169	131	99	3.8	7	6	377	4.55	96	<5	<2	4	30	.6	12	8	51	.19	.085	26	19	.33	327	.01	<3	1.70	.01	.12	<2	123
T-1000 2225	29	244	103	159	.8	7	7	389	4.64	92	<5	<2	8	34	.7	11	3	66	.15	.071	33	14	.35	271	.02	<3	1.27	.02	.18	<2	75
T-1000 2250	13	123	62	99	.6	5	13	1074	2.95	47	<5	<2	<2	21	.8	8	<2	50	.14	.053	18	13	.22	177	.02	<3	1.05	.02	.11	<2	35
T-1000 2275	10	128	54	126	.9	9	6	329	4.31	43	<5	<2	5	23	.7	8	3	74	.24	.078	22	23	.52	202	.05	<3	1.64	.01	.13	<2	117
T-1000 2300	2	100	35	92	.3	9	10	313	3.09	24	<5	<2	5	17	.7	4	2	62	.26	.069	21	22	.41	178	.05	<3	1.47	.02	.10	<2	90
RE T-1000 2300	2	99	34	90	.3	9	10	309	3.05	21	5	<2	5	17	.9	3	<2	62	.25	.066	19	21	.40	172	.05	<3	1.44	.01	.10	<2	71
T-1000 2325	1	52	29	102	.4	11	6	254	2.72	20	7	<2	3	15	1.0	2	<2	58	.20	.044	17	24	.38	189	.06	<3	1.68	.02	.11	2	21
T-1000 2350	2	50	40	100	.6	10	7	359	3.53	23	<5	<2	5	17	.8	6	<2	72	.24	.058	21	24	.40	158	.06	<3	1.44	.02	.08	<2	48
T-1000 2380	3	74	150	153	4.2	8	5	369	4.74	106	<5	<2	3	23	.8	10	8	38	.17	.082	18	18	.27	238	.01	<3	1.80	.01	.11	<2	98
T-1000 2400	3	87	145	199	2.1	11	8	392	4.41	83	<5	<2	6	28	1.7	17	6	65	.19	.060	26	23	.36	375	.02	<3	1.84	.01	.15	<2	108
T-1000 2425	2	53	51	187	1.0	7	21	1051	3.50	35	<5	<2	6	21	1.6	5	<2	59	.24	.046	25	20	.32	247	.04	<3	1.04	.01	.09	<2	445
T-1000 2450	2	28	30	135	.7	8	6	296	2.86	26	6	<2	4	18	.9	5	<2	60	.30	.066	20	21	.28	182	.04	<3	.88	.01	.09	<2	102
T-1000 2475	2	32	21	102	.3	8	5	317	3.28	22	<5	<2	6	17	.6	4	3	80	.30	.047	21	24	.30	193	.07	<3	.77	.01	.06	<2	67
T-1000 2500	4	78	54	164	1.5	11	7	241	3.87	48	<5	<2	9	25	1.3	5	4	64	.37	.066	28	23	.46	311	.02	<3	1.95	.01	.11	<2	91
T-1000 2525	3	23	43	142	.8	7	14	780	2.96	42	<5	<2	5	16	.7	5	12	57	.24	.045	18	17	.28	184	.03	<3	1.08	.02	.07	<2	87
T-1000 2550	3	32	44	125	1.6	10	7	511	2.70	42	7	<2	4	18	.7	6	6	51	.25	.039	16	20	.35	178	.04	<3	1.26	.01	.08	<2	126
T-1000 2575	2	25	35	74	.8	8	6	236	2.99	20	<5	<2	5	13	.5	2	<2	75	.24	.040	17	25	.25	99	.05	<3	1.06	.01	.06	<2	16
T-1000 2600	2	35	48	155	1.1	13	9	350	4.31	49	<5	<2	7	18	1.2	5	6	92	.26	.042	19	29	.44	155	.04	<3	1.74	.01	.09	<2	42
T-1000 2625	3	44	38	146	1.2	14	9	666	4.28	43	<5	<2	6	23	1.2	5	3	83	.33	.040	23	32	.49	245	.03	<3	1.92	.01	.09	<2	101
T-1000 2650	2	39	61	165	1.8	8	7	536	3.02	65	6	<2	3	25	1.1	4	5	58	.33	.064	16	17	.39	207	.03	<3	1.61	.03	.08	2	39
T-1000 2675	2	57	30	125	.8	16	7	354	3.83	35	<5	<2	6	22	1.1	7	3	88	.34	.044	21	31	.47	210	.05	<3	1.86	.01	.10	<2	33
T-1000 2700	2	36	28	109	.5	14	8	346	3.59	25	<5	<2	8	22	.9	6	<2	84	.33	.038	19	31	.55	177	.07	<3	1.64	.01	.07	3	39
T-1000 2725	1	22	16	82	.7	13	6	301	3.22	15	7	<2	5	20	.7	2	<2	83	.35	.044	17	30	.48	133	.09	<3	1.50	.01	.07	<2	6
T-1000 2750	3	36	51	188	.4	16	10	585	3.97	59	<5	<2	5	28	1.1	7	2	86	.42	.045	19	33	.63	249	.06	<3	2.07	.01	.09	<2	11
T-1000 2775	1	27	32	155	.3	15	6	320	3.92	32	<5	<2	7	22	.9	4	2	96	.39	.056	19	31	.60	170	.07	<3	1.47	.01	.08	<2	16
T-1000 2800	2	22	30	138	.3	12	5	242	2.91	27	<5	<2	5	19	.6	6	<2	73	.36	.058	19	26	.41	164	.06	<3	1.58	.01	.09	3	14
STANDARD C2/AU-S	20	60	39	139	6.1	71	36	1167	3.85	45	19	8	35	49	20.3	14	16	72	.55	.102	39	65	1.02	196	.08	27	2.04	.06	.14	11	38

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T-1000 2825	2	20	27	116	<.3	12	7	459	4.14	16	<5	<2	7	20	.5	<2	<2	112	.40	.071	23	36	.41	137	.08	<3	1.11	.01	.06	<2	92
T-1000 2850	2	23	26	113	<.3	11	5	251	3.05	17	<5	<2	7	20	.5	<2	4	81	.36	.053	22	28	.47	136	.09	<3	1.41	.01	.08	<2	102
T-1000 2875	2	26	29	111	.3	11	8	268	3.69	19	<5	<2	8	23	.8	3	3	94	.42	.086	22	27	.50	149	.08	<3	1.23	.02	.06	<2	10
T-1000 2900	2	32	45	161	<.3	9	11	499	4.01	43	<5	<2	9	23	1.0	<2	<2	64	.39	.069	22	20	.55	164	.08	<3	1.24	.02	.06	<2	48
T-1000 2925	1	20	35	95	<.3	10	6	333	2.55	31	<5	<2	7	21	.5	4	3	58	.37	.074	19	18	.38	132	.06	<3	1.01	.02	.06	<2	1825
T-1000 2950	1	23	25	117	.4	12	5	233	2.89	17	<5	<2	6	19	.4	3	4	75	.35	.061	21	27	.53	119	.09	<3	1.56	.02	.08	4	24
RE T-1000 2950	1	21	22	117	.4	13	5	229	2.90	16	<5	<2	6	19	.6	<2	<2	75	.35	.062	18	27	.53	122	.08	<3	1.57	.01	.08	3	29
T-1000 2975	2	30	43	128	.4	13	5	260	3.88	44	<5	<2	7	25	.8	4	<2	91	.44	.077	25	29	.52	157	.08	<3	1.55	.02	.06	<2	33
T-1000 3000	1	18	39	99	.3	9	5	230	3.03	26	<5	<2	6	21	.3	5	<2	69	.39	.069	19	22	.43	116	.08	<3	1.16	.02	.07	<2	24
T-1100 2300	6	99	269	164	2.9	7	4	164	4.04	121	<5	<2	13	35	.3	14	12	42	.15	.057	38	15	.28	276	.02	<3	.99	.01	.18	<2	1800
T-1100 2325	7	95	172	140	2.3	8	25	1216	4.67	73	<5	<2	11	27	1.3	5	11	42	.18	.059	52	17	.36	411	<.01	<3	1.84	.01	.12	<2	712
T-1100 2350	4	94	127	188	.8	8	10	486	4.75	67	<5	<2	12	27	.3	11	4	54	.16	.065	33	16	.27	240	.02	<3	.99	.02	.19	<2	83
T-1100 2375	5	129	98	254	1.4	10	9	490	5.37	91	<5	<2	11	24	1.7	17	7	63	.20	.080	37	21	.30	265	.02	<3	1.51	.01	.15	2	224
T-1100 2400	4	84	126	184	1.2	7	16	1348	5.22	93	<5	<2	9	30	.9	14	10	81	.17	.060	30	21	.26	270	.03	<3	1.14	.02	.21	<2	66
T-1100 2425	3	49	165	123	1.6	10	7	815	4.22	139	<5	<2	8	24	.6	8	4	64	.24	.066	22	21	.32	226	.05	<3	1.00	.01	.16	<2	160
T-1100 2450	4	64	154	324	1.8	9	13	651	4.80	100	<5	<2	10	27	1.9	4	6	59	.20	.063	33	18	.30	309	.01	<3	1.51	.01	.18	2	111
T-1100 2475	3	38	108	274	1.0	10	9	975	3.95	50	<5	<2	6	22	2.0	<2	5	62	.22	.049	26	20	.33	269	.02	<3	1.46	.01	.10	<2	98
T-1100 2500	79	70	190	290	2.6	7	26	810	6.65	120	<5	<2	12	18	.8	7	6	47	.18	.062	27	17	.30	292	.01	<3	1.64	.01	.11	<2	118
T-1100 2525	7	98	156	291	2.5	9	7	371	3.32	90	<5	<2	9	21	2.1	12	6	47	.23	.052	31	17	.33	423	.01	<3	1.38	.01	.12	2	130
T-1100 2550	7	39	116	374	.5	8	16	1102	5.45	68	<5	<2	16	22	1.2	4	4	62	.30	.084	47	17	.23	323	.02	<3	.85	.01	.13	<2	114
T-1100 2575	12	53	178	490	.6	8	34	1128	6.56	165	<5	<2	11	22	2.1	6	4	51	.23	.081	56	11	.26	225	.01	<3	1.26	.01	.10	2	111
T-1100 2600	3	32	55	188	.7	11	9	355	3.94	62	<5	<2	8	20	.8	3	2	80	.25	.045	23	23	.38	181	.06	<3	1.23	.01	.10	<2	78
T-1100 2625	3	31	62	179	.6	13	8	444	3.80	51	<5	<2	7	21	1.1	<2	3	76	.26	.029	24	27	.44	227	.05	<3	1.30	.01	.09	<2	145
T-1100 2650	3	23	41	146	.6	10	16	1329	3.72	44	<5	<2	7	21	.7	3	2	74	.31	.062	25	23	.36	239	.04	<3	1.05	.01	.08	<2	29
T-1100 2675	3	21	43	146	.5	10	6	281	3.13	30	<5	<2	7	19	.7	4	<2	68	.33	.065	24	22	.35	181	.05	<3	1.03	.02	.08	<2	34
T-1100 2700	2	31	37	196	1.1	15	6	245	3.41	25	<5	<2	8	21	.7	2	<2	80	.34	.052	22	30	.50	265	.05	<3	1.85	.01	.11	<2	32
T-1100 2725	2	32	39	173	.9	14	7	389	3.21	34	<5	<2	7	22	1.1	2	3	71	.36	.067	20	27	.47	183	.07	<3	1.46	.02	.10	<2	62
T-1100 2750	3	37	68	295	1.5	18	9	415	3.70	43	<5	<2	7	23	1.4	<2	4	79	.31	.042	18	32	.56	269	.04	<3	2.41	.01	.13	<2	44
T-1100 2775	2	20	45	151	.5	13	7	374	4.26	37	<5	<2	9	19	.9	3	<2	108	.34	.063	25	32	.39	163	.06	<3	1.17	.01	.09	<2	92
T-1100 2800	2	26	70	237	.9	14	5	253	3.46	55	<5	<2	9	22	1.2	<2	<2	77	.36	.059	24	28	.56	249	.05	<3	1.69	.02	.10	<2	85
T-1100 2825	2	21	73	180	.6	10	5	343	2.93	65	<5	<2	7	25	.9	<2	4	69	.35	.059	18	20	.46	183	.06	<3	1.25	.02	.08	<2	77
T-1100 2850	2	52	77	250	1.4	16	8	300	3.33	50	<5	<2	6	31	2.4	<2	3	88	.43	.055	28	31	.64	418	.03	<3	2.37	.02	.13	<2	68
T-1100 2875	2	26	53	159	.7	15	7	376	5.48	36	<5	<2	7	26	.6	4	4	67	.43	.063	20	28	.53	189	.07	<3	1.51	.02	.09	<2	25
T-1100 2900	2	45	56	139	.6	11	7	258	3.17	33	<5	<2	7	28	.9	<2	5	73	.42	.072	20	22	.59	188	.06	<3	1.50	.02	.07	<2	34
T-1100 2925	2	47	184	210	.5	10	8	443	4.19	57	<5	<2	8	42	1.0	<2	2	97	.58	.112	22	20	.71	247	.06	<3	1.76	.02	.09	<2	69
STANDARD C2/AU-S	22	62	41	147	6.6	75	37	1209	3.98	42	20	7	38	50	20.6	15	20	76	.54	.101	43	67	1.06	197	.08	28	2.07	.06	.15	11	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
T-1100 2950	2	24	34	101	.6	10	3	209	5.35	79	<5	<2	7	27	.8	2	3	121	.49	.065	20	24	.40	155	.04	<3	1.36	.01	.06	<2	16
T-1100 2975	1	24	19	105	.7	9	4	198	2.57	22	8	<2	6	26	.5	<2	4	72	.46	.075	20	22	.55	178	.08	<3	1.52	.02	.09	<2	66
T-1100 3000	2	39	26	129	.3	11	7	453	3.26	31	6	<2	5	27	.7	2	3	83	.46	.076	17	27	.63	187	.06	<3	1.79	.02	.08	<2	28
T-1200 2600	2	44	80	216	2.0	9	8	562	4.30	51	7	<2	5	25	1.6	3	6	103	.31	.079	24	15	.22	428	.07	<3	1.27	.02	.10	<2	75
T-1200 2625	2	34	62	177	1.5	9	5	350	3.52	53	<5	<2	4	19	1.2	<2	<2	68	.22	.034	25	20	.30	281	.04	<3	1.32	.01	.08	<2	46
T-1200 2650	3	34	64	154	.8	7	6	468	2.85	57	8	<2	<2	26	1.0	<2	4	63	.24	.050	23	17	.21	400	.02	<3	1.40	.01	.10	<2	38
T-1200 2675	3	29	87	220	.7	9	6	521	3.82	74	<5	<2	5	24	1.7	5	4	74	.32	.059	22	23	.34	307	.03	<3	1.17	.01	.10	<2	375
T-1200 2700	3	42	90	245	.9	9	7	498	3.71	79	<5	<2	10	25	1.9	6	5	62	.38	.080	26	21	.38	169	.06	<3	.89	.01	.10	<2	103
T-1200 2725	4	113	152	351	4.1	14	10	1200	3.84	151	<5	<2	3	34	4.7	5	8	58	.36	.046	30	26	.40	494	.02	<3	1.68	.01	.12	<2	120
T-1200 2750	3	24	91	246	.9	12	8	395	3.80	56	<5	<2	5	23	1.2	5	6	78	.35	.060	20	30	.48	226	.06	<3	1.48	.01	.09	<2	52
T-1200 2775	6	76	134	339	2.5	14	15	686	3.60	89	<5	<2	4	31	3.5	9	6	63	.37	.071	26	26	.44	456	.01	<3	2.11	.01	.12	<2	68
T-1200 2800	1	17	29	128	.3	10	5	237	3.85	24	<5	<2	5	17	1.1	2	2	102	.29	.036	22	30	.37	146	.07	<3	.93	.01	.06	<2	22
T-1200 2825	2	41	65	238	2.3	14	5	323	3.98	95	<5	<2	5	33	3.1	6	<2	99	.47	.076	21	26	.51	324	.03	<3	2.26	.02	.09	<2	53
T-1200 2850	2	45	48	258	1.1	15	7	466	3.63	48	7	<2	3	36	1.5	5	4	88	.47	.061	16	29	.61	294	.03	<3	2.30	.01	.09	<2	29
T-1200 2875	2	32	32	130	.9	14	6	281	2.90	23	<5	<2	<2	32	1.1	2	<2	72	.45	.044	13	27	.50	236	.04	<3	1.96	.01	.09	<2	19
T-1200 2900	2	57	37	170	1.1	17	8	538	3.63	41	<5	<2	3	47	1.4	5	4	84	.72	.051	15	32	.63	423	.03	<3	2.73	.01	.10	<2	28
T-1200 2925	1	57	26	167	.5	14	8	415	3.64	33	<5	<2	5	34	1.1	2	5	96	.56	.064	19	30	.86	214	.09	<3	1.95	.02	.07	<2	45
T-1200 2950	2	59	43	163	.4	14	9	537	4.05	65	<5	<2	4	31	1.0	3	3	96	.52	.064	16	28	.65	190	.06	<3	1.74	.02	.07	<2	46
T-1200 2975	2	78	28	157	.6	12	7	354	3.97	53	6	<2	2	34	.6	4	4	102	.52	.053	15	30	.80	201	.06	<3	2.02	.02	.06	<2	73
T-1200 3000	1	39	35	136	.5	10	6	289	4.04	40	<5	<2	6	30	.7	6	<2	130	.53	.072	20	29	.87	158	.11	<3	1.84	.02	.08	2	17
RE T-1200 3000	2	39	32	143	.4	10	7	302	4.02	42	<5	<2	7	30	.6	4	2	127	.53	.069	18	28	.91	168	.10	<3	1.91	.02	.09	<2	19
K-5100 1350	1	16	10	65	<.3	13	7	837	2.27	21	6	<2	2	33	<.2	2	<2	52	.65	.044	11	23	.58	287	.06	<3	1.60	.02	.08	4	1
K-5100 1400	2	28	33	72	1.2	13	11	2970	2.70	42	7	<2	3	39	.3	3	2	68	.67	.074	21	20	.53	291	.07	<3	1.80	.04	.09	<2	2
K-5350 1200	1	26	10	80	.3	19	11	862	3.54	11	<5	<2	5	31	.3	2	2	84	.54	.063	16	28	.93	232	.10	<3	2.31	.02	.15	<2	1
K-5500 950	1	17	14	92	<.3	10	8	463	2.62	12	9	<2	4	27	<.2	5	<2	61	.32	.058	16	28	1.14	201	.03	<3	2.56	.01	.27	<2	2
K-5500 1000	1	15	18	94	<.3	11	8	519	2.57	10	10	<2	4	28	.3	4	<2	58	.36	.047	17	28	1.09	232	.03	<3	2.72	.01	.24	<2	3
K-5500 1050	1	17	18	62	<.3	10	10	1012	1.94	13	<5	<2	<2	24	.2	<2	<2	42	.33	.100	18	26	.63	183	.03	<3	1.99	.01	.12	<2	9
K-5600 900	1	22	11	82	<.3	12	7	497	2.45	13	<5	<2	3	32	<.2	2	<2	55	.55	.058	19	25	.66	212	.07	<3	1.70	.02	.13	<2	2
K-5600 1050	1	24	15	79	.3	14	9	712	2.72	13	<5	<2	2	34	.3	2	<2	67	.56	.055	17	25	.66	196	.08	<3	1.80	.03	.12	<2	1
K-5600 1100	1	17	10	92	<.3	11	12	935	2.65	8	<5	<2	2	27	.2	<2	2	56	.35	.043	13	22	.73	212	.06	<3	2.06	.02	.11	<2	1
K-5600 1200	1	20	7	69	<.3	9	11	740	3.22	5	<5	<2	4	22	.4	<2	3	50	.45	.069	14	19	.56	154	.07	<3	1.52	.02	.10	<2	1
K-5600 1250	1	11	18	88	<.3	9	5	354	2.00	9	<5	<2	5	23	.2	2	<2	47	.44	.046	14	19	.59	156	.08	<3	1.63	.02	.11	2	17
K-5600 1300	2	30	16	110	.5	20	10	769	3.44	21	<5	<2	3	36	.3	3	3	79	.72	.055	18	34	.84	431	.07	<3	2.61	.03	.13	<2	4
K-5700 750	1	22	17	82	<.3	11	9	932	3.23	135	<5	<2	<2	27	<.2	5	<2	70	.56	.072	23	22	.82	214	.04	<3	2.14	.02	.16	<2	1
K-5700 850	1	18	31	72	.5	12	6	460	2.39	11	<5	<2	4	24	<.2	2	<2	52	.42	.034	17	25	.61	209	.07	<3	1.63	.02	.12	2	2
STANDARD C2/AU-S	21	60	43	144	6.4	77	37	1252	3.98	46	18	8	38	52	21.3	18	18	76	.56	.103	42	69	1.08	207	.08	28	2.08	.07	.14	11	41

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
K-5700 1050	2	38	61	108	.4	12	9	735	3.08	14	<5	<2	3	34	.2	5	<2	64	.66	.059	23	23	.64	180	.07	<3	1.77	.02	.13	<2	1
K-5700 1100	1	33	27	78	.3	16	8	559	2.70	11	<5	<2	3	31	.4	3	3	62	.56	.036	21	26	.64	190	.09	<3	1.74	.03	.12	<2	2
K-5700 1150	1	27	23	90	<.3	14	8	586	2.62	10	<5	<2	2	31	<.2	4	2	60	.53	.056	15	26	.70	177	.09	<3	1.75	.03	.12	<2	2
K-5700 1200	1	17	11	64	<.3	8	5	393	2.26	7	<5	<2	<2	26	<.2	3	<2	57	.37	.071	14	15	.37	170	.06	<3	1.39	.03	.05	<2	2
K-5700 1250	2	13	22	64	<.3	7	7	709	6.99	53	<5	<2	5	25	.7	4	3	79	.50	.074	17	18	.36	181	.04	<3	1.24	.02	.09	<2	<1
K-5700 1300	1	18	13	65	.3	12	7	829	2.69	11	10	<2	3	30	.2	4	4	55	.56	.067	19	24	.58	222	.07	<3	1.70	.02	.13	3	1
K-7400 3900	1	17	7	49	<.3	11	7	442	2.60	5	<5	<2	5	29	<.2	3	3	63	.62	.049	35	20	.64	510	.08	<3	1.69	.03	.12	<2	<1
K-7400 3950	1	13	9	69	<.3	11	11	605	3.67	7	<5	<2	10	25	.2	3	<2	98	.49	.036	16	23	.99	377	.12	<3	2.28	.02	.19	<2	1
K-7400 4000	1	12	5	48	<.3	11	6	369	2.57	4	<5	<2	8	23	<.2	<2	3	65	.51	.035	24	21	.64	363	.09	<3	1.41	.02	.10	<2	2
K-7400 4050	<1	12	7	58	<.3	10	9	508	3.29	<2	<5	<2	12	27	<.2	2	<2	84	.58	.044	31	21	.96	654	.09	<3	2.01	.02	.12	<2	1
K-7400 4100	1	12	13	50	<.3	8	8	608	2.85	<2	<5	<2	12	25	<.2	4	<2	69	.50	.034	23	17	.78	464	.06	<3	1.88	.02	.12	<2	1
K-7400 4150	2	8	12	62	<.3	8	7	577	3.04	3	8	<2	16	20	<.2	3	2	71	.34	.030	15	18	.64	253	.10	<3	1.79	.02	.21	<2	1
K-7400 4200	1	11	11	64	<.3	9	7	598	3.08	8	<5	<2	17	20	<.2	2	<2	65	.35	.034	19	17	.53	336	.08	<3	1.72	.02	.16	2	12
K-7400 4250	2	14	8	83	<.3	7	7	434	3.83	<2	<5	<2	9	38	.2	5	<2	107	.81	.072	25	17	.65	428	.08	<3	1.72	.02	.16	5	<1
K-7400 4300	2	20	28	93	.5	8	10	709	4.38	<2	<5	<2	17	25	.6	7	3	108	.64	.080	29	17	.76	494	.11	<3	1.67	.02	.22	<2	1
K-7400 4350	1	16	9	66	.3	10	9	670	4.13	<2	<5	<2	8	34	.7	5	2	128	.80	.068	29	24	.69	423	.09	<3	1.55	.02	.13	2	2
K-7400 4400	1	20	10	75	<.3	8	12	833	4.28	4	<5	<2	14	37	.4	6	<2	92	.67	.057	25	15	.77	502	.06	<3	1.61	.02	.14	3	<1
K-7400 4450	1	14	10	53	<.3	11	7	481	2.99	2	<5	<2	7	28	<.2	3	<2	67	.51	.035	18	23	.71	365	.09	<3	1.67	.02	.13	2	6
K-7400 4500	2	21	8	66	.3	9	9	378	4.07	3	<5	<2	11	32	.4	<2	<2	93	.70	.064	32	21	.88	408	.08	<3	1.93	.02	.11	2	1
K-7500 3905	1	8	13	41	<.3	6	3	300	2.23	4	<5	<2	19	25	<.2	2	<2	35	.36	.022	23	11	.41	203	.02	<3	1.10	.01	.14	<2	<1
K-7500 3950	1	11	16	61	<.3	7	8	696	3.52	5	<5	<2	20	25	.2	5	<2	75	.63	.060	36	13	.72	542	.07	<3	1.56	.02	.17	2	30
K-7500 4000	1	13	7	50	<.3	8	6	357	2.70	4	7	<2	7	33	<.2	2	<2	74	.82	.053	25	20	.61	383	.08	<3	1.34	.02	.10	2	1
RE K-7500 4000	1	15	7	51	<.3	10	6	367	2.67	5	<5	<2	7	35	<.2	3	<2	72	.86	.053	25	19	.64	399	.09	<3	1.41	.02	.10	<2	1
K-7500 4050	1	21	12	64	.3	12	10	588	3.42	4	<5	<2	14	38	.4	2	<2	85	.81	.054	40	21	1.12	558	.10	<3	2.25	.02	.15	<2	1
K-7500 4100	1	16	10	51	<.3	9	8	546	3.02	<2	<5	<2	8	34	<.2	4	<2	76	.50	.023	15	18	.80	315	.09	<3	1.79	.02	.10	<2	1
K-7500 4150	2	18	9	56	<.3	9	8	590	3.18	<2	5	<2	9	26	<.2	4	<2	76	.45	.028	17	17	.74	438	.08	<3	1.78	.02	.16	2	1
K-7500 4200	1	19	12	82	<.3	8	9	697	3.55	6	<5	<2	16	25	<.2	3	<2	74	.51	.036	22	15	.73	416	.08	<3	1.68	.02	.15	<2	2
K-7500 4250	1	10	14	66	<.3	9	10	594	3.17	5	11	<2	12	17	.3	2	2	70	.23	.023	14	19	.66	233	.12	<3	1.69	.01	.23	<2	1
K-7500 4300	1	9	16	65	<.3	9	6	463	2.55	6	<5	<2	9	21	<.2	<2	<2	53	.29	.018	18	16	.47	286	.08	<3	1.28	.01	.14	<2	1
K-7500 4350	1	9	24	61	<.3	6	6	522	2.63	5	<5	<2	11	25	.2	5	2	48	.28	.024	22	13	.30	335	.03	<3	.96	.01	.12	<2	1
K-7500 4400	1	9	19	81	<.3	5	6	443	2.73	3	9	<2	14	26	.7	3	2	52	.37	.026	22	10	.39	393	.04	<3	1.12	.02	.15	<2	<1
K-7500 4450	1	6	12	46	<.3	7	5	363	2.62	2	6	<2	12	31	<.2	<2	<2	60	.36	.027	19	16	.49	223	.09	<3	1.12	.02	.15	<2	6
K-7500 4500	2	11	11	57	<.3	6	8	548	2.36	2	<5	<2	11	22	<.2	<2	<2	70	.34	.025	14	14	.71	297	.09	<3	1.70	.02	.17	2	2
K-7500 4550	1	16	10	51	<.3	12	9	618	3.12	6	<5	<2	8	23	<.2	<2	<2	74	.38	.032	15	21	.78	338	.10	<3	1.85	.02	.13	2	8
K-7500 4590	1	15	11	54	<.3	11	8	551	3.15	3	<5	<2	9	24	<.2	3	<2	73	.44	.033	22	20	.74	488	.09	<3	1.81	.02	.12	<2	2
STANDARD C2/AU-S	20	59	43	137	6.4	73	35	1212	3.91	42	17	8	36	50	20.5	19	19	72	.54	.098	42	64	1.04	203	.08	28	2.06	.06	.13	12	43

Sample type: SDTL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
K-7700 4250R	1	10	9	49	<.3	12	7	295	2.82	9	<5	<2	5	19	<.2	<2	<2	65	.30	.018	12	22	.56	235	.08	<3	1.75	.01	.12	<2	10
K-7800 4275	1	13	7	45	<.3	11	7	370	2.41	6	<5	<2	7	19	.2	<2	<2	57	.30	.017	14	20	.50	252	.09	3	1.39	.02	.10	<2	1
K-7800 4300R	1	10	7	38	<.3	7	7	390	2.33	4	<5	<2	11	21	<.2	<2	<2	49	.35	.044	25	13	.35	351	.04	<3	1.04	.01	.08	<2	1
RE K-8000 4350R	1	9	6	36	<.3	13	6	198	2.53	9	<5	<2	4	17	<.2	<2	<2	59	.28	.035	12	22	.37	210	.08	<3	1.23	.01	.08	<2	1
K-8000 4350R	1	10	6	37	<.3	14	6	198	2.52	11	<5	<2	4	17	<.2	<2	<2	58	.28	.034	12	22	.38	214	.08	<3	1.25	.01	.08	<2	<1
K-8100 4400	1	13	8	46	<.3	14	8	317	2.76	4	5	<2	7	18	<.2	<2	5	65	.30	.027	13	18	.54	241	.08	3	1.80	.01	.12	<2	<1
K-8300 4400	1	18	7	57	<.3	19	12	341	3.20	9	<5	<2	5	19	<.2	<2	<2	71	.27	.032	11	27	.72	227	.08	3	2.94	.01	.11	<2	1

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

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GEOCHEMICAL ANALYSIS CERTIFICATE

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BYG Natural Resources Inc. PROJECT KLAZA RIVER File # 96-3234 Page 1

110 Industrial Road, Whitehorse YT Y1A 2T9

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
4800 0 K	3	29	100	126	.6	15	9	758	2.63	66	<5	<2	<2	34	.8	6	<2	61	.47	.105	20	27	.51	268	.04	<3	1.76	.02	.10	<2	7
4800 50 K	2	25	32	95	.3	14	10	739	2.60	17	<5	<2	<2	53	.2	<2	<2	60	.69	.077	13	23	.51	369	.04	<3	1.62	.03	.09	<2	<2
4800 100 K	5	33	254	230	.8	15	9	1116	2.92	99	<5	<2	<2	31	.9	3	2	61	.45	.077	17	27	.50	146	.05	<3	1.73	.02	.11	<2	<2
4800 150 K	2	29	98	111	.6	15	10	804	2.97	16	<5	<2	<2	23	.8	<2	<2	71	.22	.091	13	28	.41	82	.08	<3	1.93	.01	.08	<2	<2
4800 200 K	1	15	24	65	<.3	13	6	422	2.12	8	<5	<2	4	26	<.2	<2	<2	48	.39	.052	17	22	.44	119	.09	<3	1.10	.03	.08	<2	<2
4800 250 K	2	20	36	86	<.3	15	9	810	2.86	12	<5	<2	2	33	4.5	<2	<2	62	.47	.066	18	26	.56	210	.06	<3	1.68	.02	.10	<2	3
4800 300 K	1	19	23	72	<.3	15	7	500	2.59	42	<5	<2	<2	28	<.2	<2	<2	67	.36	.067	13	23	.45	121	.08	<3	1.42	.02	.09	<2	<2
4800 350 K	1	18	19	57	<.3	15	6	410	2.31	14	<5	<2	2	26	<.2	<2	<2	60	.34	.060	14	24	.44	108	.09	<3	1.32	.02	.08	<2	<2
4800 400 K	2	49	33	54	.3	16	11	1782	2.19	12	<5	<2	<2	59	.4	<2	<2	43	.87	.170	46	21	.39	238	.03	<3	2.04	.02	.05	<2	<2
4800 450 K	2	20	64	97	<.3	11	7	615	2.38	20	6	<2	3	22	<.2	4	<2	60	.29	.056	16	19	.40	146	.07	<3	1.24	.02	.08	<2	4
4800 500 K	2	17	68	105	<.3	12	9	927	2.60	27	<5	<2	<2	23	.3	6	<2	59	.26	.067	14	23	.49	164	.05	<3	1.46	.02	.10	<2	3
4800 550 K	2	24	41	68	<.3	7	6	564	2.08	18	<5	<2	<2	26	.4	3	<2	50	.30	.061	17	15	.32	185	.04	<3	1.22	.02	.09	<2	<2
4800 600 K	1	23	40	83	.7	8	5	407	1.86	18	<5	<2	<2	26	.5	4	<2	49	.33	.082	16	13	.25	150	.04	<3	1.26	.03	.05	<2	<2
4800 700 K	2	23	59	100	<.3	12	8	919	2.49	19	<5	<2	<2	27	.3	4	<2	62	.38	.063	18	20	.47	207	.05	<3	1.45	.02	.09	<2	<2
4800 750 K	2	19	78	107	<.3	10	9	658	2.65	21	<5	<2	<2	27	.4	3	<2	62	.31	.049	17	19	.58	194	.03	<3	1.65	.01	.09	<2	<2
4800 800 K	1	17	48	93	<.3	12	5	219	1.93	15	<5	<2	3	21	<.2	4	<2	44	.35	.068	17	22	.48	123	.06	<3	1.31	.02	.08	<2	9
4800 850 K	1	12	35	74	<.3	10	5	233	1.55	7	<5	<2	<2	23	.5	3	<2	44	.28	.053	13	24	.43	171	.05	<3	1.47	.02	.06	<2	<2
4800 900 K	3	18	34	95	<.3	14	16	1697	4.01	27	<5	<2	<2	31	<.2	<2	<2	83	.43	.075	11	30	.59	299	.06	<3	1.93	.02	.07	2	<2
4800 1000 K	1	15	33	67	<.3	11	5	523	2.04	17	<5	<2	2	21	<.2	<2	<2	48	.32	.041	12	22	.46	186	.07	<3	1.47	.02	.07	<2	5
4800 1200 K	2	15	40	75	<.3	9	8	940	2.26	21	<5	<2	<2	32	<.2	3	<2	62	.37	.063	12	20	.44	269	.03	<3	1.42	.02	.06	<2	<2
4800 1250 K	2	19	44	105	<.3	9	8	896	2.64	26	<5	<2	2	28	<.2	4	2	58	.40	.054	14	18	.52	204	.06	<3	1.29	.02	.12	<2	2
4800 1300 K	2	17	59	82	<.3	9	7	584	2.43	20	<5	<2	<2	23	.3	5	2	52	.24	.062	15	17	.40	132	.04	<3	1.42	.02	.07	<2	<2
4800 1450 K	2	8	3	24	<.3	2	18	1789	3.99	<2	<5	<2	<2	34	<.2	<2	<2	29	.49	.096	5	4	.09	107	.04	<3	.34	.04	.01	<2	<2
4900 0 K	2	31	60	79	<.3	10	8	727	2.84	73	<5	<2	<2	44	<.2	3	<2	69	.53	.098	22	17	.49	196	.06	<3	1.65	.02	.10	<2	49
RE 4800 800 K	1	18	43	90	<.3	12	5	223	1.97	14	<5	<2	3	22	.3	4	<2	45	.36	.069	18	21	.49	124	.07	<3	1.35	.02	.09	<2	3
4900 50 K	2	32	37	65	.4	12	5	437	2.34	<2	<5	<2	<2	31	.2	7	<2	63	.40	.113	22	21	.45	205	.06	<3	1.69	.02	.06	2	7
4900 100 K	1	24	15	62	<.3	10	7	586	3.09	<2	<5	<2	<2	33	<.2	<2	<2	96	.49	.073	15	18	.36	141	.12	<3	1.33	.04	.06	<2	<2
4900 150 K	2	32	23	92	<.3	16	10	1384	2.75	4	<5	<2	<2	59	.9	<2	<2	57	1.05	.120	24	24	.63	261	.05	<3	2.34	.02	.10	<2	46
4900 200 K	1	20	20	61	<.3	10	5	247	1.79	4	<5	<2	<2	25	.3	<2	<2	47	.32	.061	14	18	.44	124	.07	<3	1.48	.02	.07	2	3
4900 250 K	2	16	23	57	<.3	10	8	999	2.75	4	<5	<2	<2	25	<.2	<2	<2	57	.37	.079	16	19	.44	137	.07	<3	1.56	.02	.07	<2	<2
4900 300 K	3	25	54	102	1.2	13	7	749	2.97	4	<5	<2	<2	23	<.2	<2	<2	77	.29	.089	20	30	.50	347	.06	<3	2.16	.01	.12	<2	6
4900 350 K	4	36	109	65	1.4	10	4	261	3.07	138	<5	<2	2	18	<.2	5	2	65	.25	.077	21	24	.38	216	.05	<3	1.69	.01	.10	<2	12
4900 400 K	2	28	69	122	.9	13	7	954	2.56	8	<5	<2	<2	35	1.0	3	<2	52	.50	.051	19	23	.48	227	.06	<3	1.63	.01	.13	2	<2
4900 450 K	1	20	37	108	<.3	11	6	578	2.34	13	<5	<2	3	76	<.2	<2	<2	49	.38	.042	15	22	.58	206	.09	<3	1.56	.02	.12	<2	4
4900 500 K	2	27	87	199	.3	12	9	1138	3.11	90	<5	<2	3	31	.7	2	<2	65	.42	.036	16	21	.68	220	.07	<3	2.00	.01	.14	<2	11
STANDARD C2/AU-S	24	63	45	142	6.4	82	36	1201	4.09	42	19	8	38	55	20.7	18	21	74	.55	.101	43	70	1.02	199	.09	28	2.08	.07	.15	12	49

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.

ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB

- SAMPLE TYPE: P1-P13 SOIL GEO P14 ROCK ASSAY AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.

Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 29 1996

DATE REPORT MAILED:

SIGNED BY: *D. Toye*, D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
4900 550 K	2	21	190	257	.4	8	6	816	2.62	72	<5	<2	6	24	1.1	4	2	52	.47	.041	19	16	.72	189	.05	<3	1.72	.01	.19	<2	8
4900 600 K	1	24	73	122	<.3	14	11	935	2.71	63	<5	<2	5	19	.4	<2	<2	60	.31	.045	15	24	.57	165	.08	<3	1.65	.02	.12	<2	4
4900 650 K	3	46	222	290	1.8	17	13	1762	3.16	53	<5	<2	3	42	1.4	4	<2	70	.86	.090	21	33	.67	379	.04	<3	2.76	.02	.16	<2	21
4900 700 K	2	34	49	124	.9	13	7	545	2.70	18	<5	<2	<2	39	1.1	2	<2	60	.81	.106	16	22	.40	354	.04	3	1.69	.02	.08	<2	<2
4900 750 K	1	24	13	61	<.3	8	6	359	2.89	3	<5	<2	<2	28	<.2	2	2	103	.49	.082	15	16	.26	172	.12	<3	.93	.02	.04	<2	<2
4900 800 K	1	25	21	59	.3	9	5	218	2.26	6	<5	<2	2	18	<.2	2	2	69	.29	.065	14	21	.42	149	.06	<3	1.52	.02	.07	<2	<2
4900 850 K	1	31	38	92	.9	9	5	328	2.22	212	<5	<2	3	22	.2	5	2	59	.32	.057	17	22	.53	276	.03	<3	1.87	.01	.10	<2	19
4900 950 K	2	37	85	172	2.0	12	7	861	2.57	19	<5	<2	7	27	1.2	10	<2	56	.49	.072	21	25	.47	251	.09	<3	1.34	.02	.14	<2	9
4900 1000 K	1	17	18	62	<.3	10	6	518	2.19	20	<5	<2	2	23	<.2	<2	<2	52	.39	.043	13	21	.45	159	.06	<3	1.33	.02	.07	<2	5
4900 1050 K	2	27	25	80	.5	13	8	604	2.71	26	<5	<2	<2	32	<.2	3	3	63	.52	.078	13	26	.52	253	.05	<3	1.80	.02	.09	<2	5
4900 1100 K	1	18	14	67	<.3	11	5	407	1.92	7	<5	<2	3	19	.2	3	2	45	.32	.048	14	24	.51	133	.08	<3	1.51	.02	.09	<2	4
4900 1150 K	1	20	23	73	<.3	12	4	239	2.00	14	<5	<2	3	20	<.2	2	<2	61	.34	.049	13	25	.58	158	.08	<3	1.66	.02	.08	<2	<2
4900 1200 K	2	16	5	37	<.3	4	18	3267	4.65	21	<5	<2	<2	22	<.2	<2	<2	91	.34	.084	8	10	.09	158	.10	<3	.46	.03	.01	<2	6
4900 1250 K	1	22	4	53	<.3	7	8	954	2.73	<2	<5	<2	<2	36	<.2	<2	<2	96	.66	.083	6	12	.14	212	.12	<3	.60	.03	.02	<2	<2
4900 1300 K	1	18	20	72	<.3	10	6	388	2.44	<2	<5	<2	2	27	<.2	2	2	68	.43	.051	10	22	.48	149	.10	<3	1.36	.02	.06	<2	<2
4900 1450 K	1	8	<3	29	<.3	3	7	921	1.67	2	<5	<2	<2	22	<.2	<2	<2	55	.37	.068	6	6	.09	62	.09	<3	.33	.05	.03	<2	<2
4900 1500 K	1	9	<3	30	<.3	3	13	1242	1.91	<2	<5	<2	<2	31	<.2	<2	<2	58	.45	.067	10	6	.09	88	.08	<3	.36	.07	.03	<2	<2
5000 0 K	2	27	31	72	<.3	15	9	615	2.73	6	<5	<2	<2	28	<.2	<2	<2	67	.39	.069	22	26	.66	201	.07	<3	2.20	.02	.12	<2	7
5000 50 K	1	16	31	63	<.3	12	7	549	2.37	6	<5	<2	2	22	<.2	<2	<2	56	.34	.049	15	22	.52	138	.07	<3	1.42	.02	.10	<2	3
RE 5000 50 K	1	17	40	65	<.3	12	7	577	2.46	7	<5	<2	2	23	<.2	2	<2	58	.36	.053	16	23	.54	144	.07	3	1.47	.02	.11	<2	<2
5000 100 K	1	27	28	60	<.3	12	6	582	2.36	5	<5	<2	2	28	<.2	<2	<2	55	.35	.049	14	23	.51	172	.08	<3	1.54	.02	.09	<2	7
5000 150 K	1	19	72	126	<.3	10	7	718	2.75	2	<5	<2	2	25	.4	<2	<2	62	.36	.051	14	20	.60	174	.06	<3	1.61	.02	.13	<2	2
5000 200 K	4	33	67	150	.9	16	12	1814	3.36	10	<5	<2	2	33	.4	5	<2	70	.43	.078	27	31	.59	615	.03	<3	2.67	.01	.15	<2	17
5000 250 K	4	41	86	163	1.3	13	10	996	3.22	102	<5	<2	2	22	.8	5	3	61	.22	.063	24	29	.46	449	.03	<3	2.29	.01	.14	<2	<2
5000 300 K	3	19	94	88	.3	12	5	329	2.37	9	<5	<2	3	17	.3	<2	<2	54	.20	.023	12	23	.40	91	.09	<3	1.43	.01	.09	<2	<2
5000 350 K	2	23	32	61	.3	9	4	306	1.92	9	<5	<2	<2	18	.2	<2	<2	49	.15	.055	12	18	.19	119	.04	<3	.97	.01	.07	<2	<2
5000 400 K	2	21	57	71	.4	11	5	360	2.41	9	<5	<2	2	12	<.2	2	2	50	.15	.029	11	21	.36	87	.06	<3	1.34	.01	.09	<2	<2
5000 450 K	3	16	27	65	<.3	7	4	412	2.03	18	<5	<2	<2	17	<.2	2	<2	62	.20	.060	10	17	.22	110	.07	<3	.83	.01	.10	<2	5
5000 500 K	3	24	85	141	.4	10	6	556	2.42	11	<5	<2	2	13	<.2	3	<2	52	.14	.035	15	24	.40	146	.05	<3	1.32	.01	.09	<2	15
5000 550 K	3	33	112	138	.6	14	7	503	2.65	16	<5	<2	5	16	.4	3	3	59	.20	.029	14	29	.51	131	.07	<3	1.68	.01	.11	<2	6
5000 600 K	2	31	67	150	.6	15	21	3825	3.51	200	<5	<2	2	26	<.2	4	4	70	.41	.097	14	30	.57	186	.06	3	2.10	.02	.15	<2	65
5000 650 K	1	23	27	78	.3	12	10	807	2.79	12	<5	<2	<2	22	<.2	<2	<2	68	.35	.059	12	26	.50	165	.07	<3	1.68	.02	.10	<2	8
5000 700 K	2	28	51	134	<.3	12	8	742	2.97	13	<5	<2	2	35	<.2	<2	2	67	.80	.058	15	22	.75	251	.06	<3	1.93	.02	.11	<2	<2
5000 900 K	2	19	60	169	.5	13	6	935	2.60	9	<5	<2	4	31	.3	2	<2	52	.56	.031	15	24	.49	225	.08	<3	1.33	.02	.09	<2	10
5000 950 K	1	18	29	132	.9	13	8	587	2.52	8	<5	<2	3	19	.3	<2	2	56	.27	.031	13	27	.52	133	.08	<3	1.60	.02	.11	<2	10
STANDARD C2/AU-S	22	59	41	143	6.1	76	37	1183	3.92	40	17	8	36	51	19.7	18	18	76	.56	.096	40	72	1.02	214	.08	27	1.96	.06	.14	10	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
5000 1000 K	2	61	40	128	.9	12	10	591	3.15	25	<5	<2	3	30	.3	5	4	70	.51	.081	29	25	.59	390	.06	<3	2.03	.02	.16	<2	16
5000 1050 K	1	19	23	68	<.3	16	8	461	2.65	7	<5	<2	2	21	<.2	<2	<2	58	.32	.046	16	28	.59	158	.10	<3	1.84	.02	.09	2	14
5000 1100 K	1	24	27	78	.3	13	7	667	2.32	8	<5	<2	3	24	<.2	2	<2	52	.41	.055	16	22	.49	188	.08	<3	1.49	.03	.07	<2	3
5000 1200 K	1	16	13	64	<.3	12	5	237	2.73	10	<5	<2	3	21	<.2	3	<2	60	.40	.056	13	24	.57	167	.07	<3	1.66	.02	.08	<2	2
5100 800 K	1	19	26	107	<.3	16	9	717	3.00	9	<5	<2	3	22	<.2	2	<2	65	.35	.045	22	30	.59	295	.07	<3	1.97	.02	.10	<2	<2
5100 1200 K	1	21	14	90	.3	17	9	779	3.27	8	<5	<2	3	31	<.2	<2	<2	66	.63	.047	20	31	.64	401	.06	<3	2.09	.02	.13	<2	3
5100 1300 K	3	30	45	110	<.3	13	9	823	3.34	6	<5	<2	6	25	<.2	4	<2	72	.51	.072	17	26	.66	226	.08	<3	1.81	.02	.11	<2	<2
RE 5250 950 K	1	15	14	68	<.3	12	6	440	2.34	8	<5	<2	4	25	.2	<2	2	57	.50	.077	14	25	.54	119	.10	<3	1.23	.02	.09	<2	4
5100 1350 K	2	27	14	84	.3	14	9	780	2.74	9	<5	<2	2	31	<.2	3	<2	62	.65	.068	26	26	.56	264	.05	<3	1.77	.02	.08	<2	5
5100 1400 K	1	28	19	74	.5	12	9	808	2.52	32	<5	<2	3	36	<.2	<2	4	61	.61	.050	16	23	.54	292	.08	<3	1.80	.03	.11	<2	2
5250 850 K	2	35	34	96	.6	14	9	850	2.78	19	<5	<2	<2	42	.3	3	<2	63	.81	.155	26	28	.48	807	.04	<3	1.76	.02	.12	<2	3
5250 950 K	1	14	11	62	<.3	12	5	412	2.17	7	<5	<2	3	25	<.2	<2	<2	53	.46	.071	12	24	.50	122	.10	<3	1.19	.02	.10	<2	<2
5250 1000 K	1	17	8	59	<.3	11	6	422	2.73	16	<5	<2	2	20	<.2	2	3	67	.34	.061	14	24	.51	152	.08	<3	1.38	.02	.10	<2	<2
5250 1050 K	2	21	9	68	.3	5	19	2291	4.22	33	<5	<2	<2	26	<.2	<2	<2	82	.39	.169	10	21	.51	199	.05	<3	1.74	.02	.07	<2	2
5250 1100 K	1	22	43	126	2.7	12	6	530	2.66	16	<5	<2	4	24	.3	4	2	59	.34	.033	13	23	.73	270	.06	<3	2.19	.02	.13	<2	3
5350 800 K	1	14	15	52	<.3	7	4	284	1.47	17	<5	<2	<2	14	.2	3	<2	37	.21	.052	17	18	.30	169	.03	<3	1.04	.01	.08	<2	5
5350 850 K	1	34	24	62	.7	8	7	908	2.18	21	<5	<2	<2	28	.3	2	<2	56	.40	.155	16	25	.36	311	.03	<3	1.56	.02	.08	<2	<2
5350 900 K	5	24	104	71	.3	6	1	239	14.82	252	<5	<2	6	18	<.2	<2	<2	220	.33	.059	28	20	.13	325	.03	<3	1.19	.01	.07	<2	2
5350 950 K	1	12	28	67	<.3	4	4	203	2.60	28	<5	<2	3	9	.4	3	2	54	.20	.052	14	12	.21	147	.03	<3	.93	.01	.10	<2	13
5350 1000 K	1	15	13	50	<.3	7	4	174	2.58	58	<5	<2	3	16	<.2	2	2	54	.32	.065	16	16	.35	148	.05	<3	1.26	.01	.13	<2	2
5350 1050 K	1	16	13	91	.3	11	7	583	3.87	25	<5	<2	2	18	<.2	<2	2	59	.27	.060	13	25	.54	159	.06	<3	1.65	.02	.10	<2	6
5400 550 K	2	20	42	85	<.3	14	7	586	2.62	6	<5	<2	2	17	<.2	<2	<2	63	.22	.057	17	29	.49	134	.09	<3	1.47	.01	.12	<2	<2
5400 600 K	1	15	26	84	<.3	10	7	580	2.57	40	<5	<2	<2	17	<.2	<2	<2	73	.22	.064	15	23	.36	172	.09	<3	1.20	.02	.07	<2	2
5400 650 K	1	21	39	93	<.3	12	8	791	2.37	34	<5	<2	<2	22	.5	<2	<2	58	.25	.073	15	28	.44	212	.05	<3	1.47	.02	.07	<2	<2
5400 750 K	1	21	41	71	<.3	12	6	502	2.30	12	<5	<2	<2	19	.2	<2	<2	57	.29	.062	12	22	.36	133	.06	<3	1.04	.02	.07	<2	<2
5400 800 K	2	20	31	79	<.3	12	8	884	2.48	31	<5	<2	<2	20	<.2	2	<2	61	.23	.078	15	27	.48	137	.06	<3	1.40	.01	.08	<2	14
5400 850 K	2	17	31	69	<.3	9	5	504	1.66	23	<5	<2	<2	17	.3	2	<2	44	.19	.072	14	24	.39	120	.05	<3	1.16	.01	.07	<2	<2
5400 900 K	2	17	52	60	<.3	9	4	193	1.69	28	<5	<2	3	14	.3	3	<2	57	.26	.063	17	21	.38	103	.07	<3	1.31	.01	.10	<2	10
5400 950 K	<1	11	28	63	<.3	7	3	165	1.07	4	<5	<2	4	15	.2	3	2	33	.30	.057	15	17	.37	99	.09	<3	1.02	.01	.11	<2	4
5400 1000 K	<1	8	19	60	<.3	7	3	291	1.08	3	<5	<2	3	16	.2	2	<2	28	.33	.059	11	16	.34	147	.08	<3	.97	.02	.10	<2	19
5400 1050 K	<1	10	20	57	<.3	6	3	283	1.02	5	<5	<2	4	15	<.2	2	2	29	.29	.048	13	17	.36	140	.08	<3	.92	.01	.09	<2	<2
5400 1095 K	2	25	15	106	.4	13	6	638	2.80	40	<5	<2	<2	29	.6	<2	2	69	.43	.143	16	33	.55	249	.04	<3	1.92	.02	.10	<2	4
5400 1150 K	1	14	10	60	<.3	11	15	1295	3.21	8	<5	<2	2	24	<.2	<2	<2	66	.36	.054	16	27	.57	233	.05	<3	1.86	.02	.10	<2	6
5400 1200 K	<1	10	11	33	<.3	7	3	118	1.01	<2	<5	<2	4	16	<.2	<2	9	27	.28	.042	13	17	.33	110	.07	<3	1.04	.01	.05	<2	2
5400 1340 K	2	20	23	62	<.3	17	16	1426	3.63	3	<5	<2	5	16	.2	<2	8	76	.20	.040	15	28	.71	184	.06	<3	3.36	.02	.11	<2	2
STANDARD C2/AU-S	20	58	39	137	6.1	69	34	1100	3.70	35	20	7	35	49	18.3	16	16	71	.53	.101	39	65	.93	198	.08	24	1.90	.06	.14	10	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
5400 1450 K	1	45	16	56	<.3	20	9	444	2.63	12	<5	<2	4	22	<.2	3	6	56	.36	.030	18	28	.64	258	.09	4	1.81	.02	.14	<2	2
5500 550 K	1	16	54	152	<.3	14	5	479	2.38	9	5	<2	2	21	.6	2	2	50	.21	.050	23	23	.40	199	.05	3	1.72	.01	.14	<2	3
5500 600 K	1	13	15	59	<.3	10	6	412	2.58	13	8	<2	2	18	<.2	5	2	66	.21	.053	16	20	.37	115	.07	4	1.21	.01	.12	<2	<2
5500 1100 K	<1	9	17	54	<.3	9	5	190	1.12	5	<5	<2	4	17	<.2	3	<2	31	.31	.056	13	20	.43	124	.10	3	1.22	.02	.09	<2	7
5500 1150 K	<1	15	16	62	<.3	10	5	210	1.47	2	<5	<2	7	21	<.2	3	2	48	.34	.042	17	21	.55	192	.08	<3	1.67	.02	.16	<2	4
5500 1200 K	4	19	28	66	<.3	11	7	367	0.22	87	<5	<2	4	25	.2	3	0	208	.45	.072	14	26	.54	150	.08	<3	1.60	.02	.11	<2	7
5500 1250 K	1	29	16	58	<.3	10	5	199	2.18	21	<5	<2	2	26	<.2	2	22	58	.52	.050	16	20	.50	233	.05	3	1.55	.02	.11	<2	<2
5700 550 K	1	16	28	116	<.3	13	10	1036	2.64	14	<5	<2	4	15	.8	3	3	48	.18	.069	39	19	.48	246	.06	<3	1.95	.01	.21	<2	<2
7400 1750 K	2	30	16	94	<.3	15	9	830	2.88	6	<5	<2	<2	31	.4	3	2	66	.35	.078	15	30	.50	357	.06	3	1.96	.02	.14	<2	13
7500 3650 K	2	17	10	126	.3	13	8	2766	2.49	9	6	<2	<2	40	.4	<2	<2	41	.49	.081	11	17	.37	329	.04	<3	1.53	.03	.06	<2	<2
7500 3700 K	1	26	7	63	<.3	9	7	775	1.86	7	<5	<2	2	35	<.2	<2	<2	44	.44	.081	13	14	.34	224	.06	<3	1.21	.04	.04	<2	2
7500 3750 K	1	11	12	58	<.3	11	6	391	1.77	8	<5	<2	3	41	.2	<2	<2	40	.49	.074	15	17	.37	270	.05	<3	1.18	.02	.05	<2	<2
7500 3800 K	1	20	12	56	<.3	9	6	329	2.75	20	<5	<2	<2	45	<.2	<2	<2	54	.54	.093	15	16	.36	198	.07	<3	1.08	.03	.05	<2	<2
7500 3850 K	<1	11	14	59	<.3	9	5	237	1.74	7	<5	<2	3	35	<.2	<2	<2	46	.49	.094	16	17	.38	181	.06	<3	1.05	.02	.05	<2	4
7500 3900 K	1	8	10	47	<.3	7	5	181	1.52	7	<5	<2	3	25	<.2	<2	<2	40	.41	.084	14	13	.31	151	.06	<3	.87	.02	.05	<2	5
7500 3950 K	1	21	3	45	<.3	10	7	362	2.16	7	<5	<2	3	46	.2	<2	<2	53	1.15	.060	28	18	.54	632	.05	<3	1.40	.02	.10	<2	2
7500 4050 K	<1	22	5	46	<.3	11	8	315	2.38	3	<5	<2	5	44	<.2	<2	<2	61	1.05	.055	54	21	.67	673	.06	<3	1.82	.02	.10	<2	<2
7500 4100 K	1	14	3	47	<.3	10	8	384	2.54	3	<5	<2	4	30	<.2	<2	<2	66	.45	.026	15	16	.55	285	.09	<3	1.50	.03	.10	<2	7
7500 4150 K	1	11	6	47	<.3	9	7	427	2.42	6	<5	<2	5	23	<.2	<2	<2	62	.37	.020	15	20	.59	320	.11	<3	1.36	.02	.14	<2	<2
7500 4200 K	1	19	8	100	<.3	8	10	1055	3.57	5	<5	<2	16	30	<.2	<2	<2	75	.56	.042	20	16	.70	470	.06	<3	1.88	.02	.15	<2	<2
7500 4250 K	1	13	9	70	<.3	15	8	426	3.13	5	<5	<2	5	31	<.2	<2	<2	84	.42	.021	15	34	.72	394	.15	3	1.89	.02	.16	<2	<2
7500 4300 K	1	9	7	57	<.3	10	6	348	2.28	6	<5	<2	7	22	<.2	<2	<2	53	.31	.020	20	19	.51	276	.10	3	1.35	.02	.14	<2	14
7500 4350 K	1	14	7	48	<.3	9	7	383	2.16	4	6	<2	3	29	<.2	2	<2	50	.44	.033	15	17	.37	445	.05	3	1.32	.02	.14	<2	7
RE 7500 3950 K	1	23	5	50	.3	11	8	407	2.40	3	<5	<2	3	51	.2	<2	<2	58	1.30	.069	32	21	.61	725	.06	<3	1.57	.02	.10	<2	2
7500 4400 K	1	13	11	51	<.3	6	6	379	2.08	5	<5	<2	3	35	.3	<2	<2	46	.55	.051	20	11	.31	485	.04	<3	1.18	.03	.12	<2	2
7500 4450 K	1	7	6	51	<.3	7	7	446	2.65	7	<5	<2	8	45	.2	<2	<2	64	.46	.037	20	15	.48	270	.09	<3	1.21	.02	.13	<2	<2
7500 4500 K	1	12	6	59	<.3	11	9	483	2.98	5	<5	<2	4	30	<.2	<2	2	75	.43	.021	14	23	.69	309	.12	<3	1.81	.02	.15	<2	<2
7500 4550 K	1	15	6	55	<.3	15	9	473	2.89	6	<5	<2	6	29	<.2	<2	<2	68	.42	.033	14	28	.70	307	.11	<3	2.06	.02	.12	<2	<2
7500 4590 K	1	18	6	58	.3	13	10	551	3.09	6	<5	<2	6	32	<.2	<2	2	70	.53	.042	26	24	.73	570	.07	<3	2.24	.02	.13	<2	3
7600 3500 K	4	32	<3	23	<.3	6	5	337	4.29	25	<5	<2	<2	37	.2	2	<2	78	.47	.112	11	16	.12	304	.05	<3	.96	.04	.03	<2	<2
7600 3550 K	1	17	<3	76	<.3	7	16	3868	1.67	<2	<5	<2	<2	73	.5	<2	<2	40	1.98	.062	24	9	.26	815	.04	4	.97	.03	.05	<2	<2
7600 3600 K	4	18	5	188	<.3	16	13	6930	3.04	20	<5	<2	<2	66	1.1	<2	3	44	.72	.072	11	17	.37	533	.04	<3	1.46	.03	.06	<2	2
7600 3650 K	2	24	5	169	<.3	18	11	1212	1.89	8	6	<2	<2	31	.6	2	<2	47	.38	.057	9	20	.35	430	.05	<3	1.67	.04	.07	<2	<2
7600 3700 K	1	20	12	74	<.3	11	7	665	1.82	2	<5	<2	<2	72	.5	<2	<2	60	.75	.094	12	17	.36	344	.08	3	1.17	.02	.04	<2	42
7600 3750 K	<1	35	16	98	.4	13	7	376	1.91	10	<5	<2	<2	67	.6	<2	<2	49	.72	.088	17	21	.50	289	.07	3	1.39	.02	.06	<2	6
STANDARD C2/AU-S	19	55	35	137	6.2	71	36	1140	3.90	43	14	8	34	51	20.6	14	21	71	.54	.104	39	64	1.00	205	.08	29	1.97	.06	.15	14	48

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
7600 3800 K	1	7	12	56	<.3	6	5	247	2.24	4	<5	<2	3	31	<.2	<2	<2	70	.45	.080	15	16	.29	127	.07	<3	.72	.02	.05	<2	64
7600 3850 K	1	12	9	46	<.3	8	6	331	2.56	5	<5	<2	5	33	<.2	<2	<2	76	.78	.033	16	16	.51	337	.08	<3	1.24	.02	.10	<2	<2
7600 3900 K	1	18	6	57	<.3	8	7	467	2.54	<2	<5	<2	8	45	.2	2	<2	73	1.17	.063	39	19	.68	528	.07	<3	1.62	.02	.10	<2	18
7600 4000 K	1	27	9	45	<.3	11	7	490	2.50	<2	<5	<2	5	48	<.2	<2	<2	64	1.20	.058	58	21	.56	669	.04	<3	1.87	.02	.12	<2	2
7600 4050 K	1	10	4	51	<.3	7	6	315	2.54	2	<5	<2	4	23	<.2	<2	<2	72	.41	.021	9	13	.53	326	.07	<3	1.30	.02	.17	<2	<2
7600 4100 K	2	28	5	50	<.3	13	9	520	2.58	2	<5	<2	6	30	<.2	<2	<2	68	.52	.034	33	26	.53	566	.08	<3	1.80	.02	.11	<2	<2
7600 4150 K	1	20	9	50	<.3	12	8	451	2.63	5	<5	<2	12	30	<.2	2	<2	65	.51	.032	25	20	.55	475	.08	3	1.77	.02	.13	<2	<2
7600 4200 K	1	9	10	63	<.3	9	6	457	2.46	2	<5	<2	6	21	<.2	<2	<2	73	.21	.012	12	22	.50	238	.14	<3	1.35	.01	.18	<2	<2
7600 4250 K	1	10	12	50	<.3	8	5	410	2.18	6	<5	<2	9	21	<.2	<2	<2	51	.26	.016	18	14	.35	250	.06	<3	.95	.01	.12	<2	4
7600 4300 K	1	10	7	55	<.3	11	6	468	2.67	2	<5	<2	9	24	<.2	<2	<2	65	.33	.016	15	22	.55	308	.10	<3	1.50	.01	.17	<2	<2
7600 4350 K	2	26	9	59	.3	13	8	461	3.08	2	<5	<2	4	49	<.2	<2	<2	68	1.00	.071	40	20	.55	770	.05	3	2.22	.02	.14	<2	<2
7600 4400 K	2	16	9	54	<.3	12	8	432	2.98	2	<5	<2	6	49	<.2	<2	<2	75	.48	.030	18	23	.65	445	.09	<3	1.95	.02	.13	<2	<2
7600 4500 K	1	16	9	55	<.3	14	8	447	2.89	5	<5	<2	5	26	<.2	<2	2	75	.41	.029	14	26	.70	337	.11	<3	1.82	.02	.12	<2	<2
7600 4550 K	1	15	6	53	<.3	12	8	457	2.98	4	<5	<2	6	24	<.2	<2	<2	75	.38	.030	13	25	.72	254	.10	<3	2.00	.01	.12	<2	<2
7600 4650 K	2	24	12	129	<.3	13	8	2109	2.31	9	<5	<2	<2	47	.4	<2	<2	38	.49	.078	12	16	.33	313	.03	<3	1.51	.03	.05	<2	2
7700 3500 K	2	44	10	88	<.3	10	5	481	2.88	18	<5	<2	<2	32	1.7	2	<2	46	.42	.067	17	16	.29	309	.03	<3	1.59	.02	.05	<2	<2
7700 3550 K	8	22	3	99	<.3	12	40	6554	11.34	14	<5	<2	<2	54	<.2	<2	<2	19	.67	.097	10	6	.09	743	.01	<3	.66	.02	.01	<2	<2
7700 3600 K	4	20	14	155	<.3	17	14	7271	2.35	10	<5	<2	<2	81	1.3	<2	<2	41	.77	.052	13	15	.37	824	.04	<3	1.36	.04	.05	<2	<2
7700 3650 K	1	8	9	58	<.3	8	5	442	1.61	8	<5	<2	2	30	<.2	2	<2	40	.38	.056	13	14	.31	147	.05	<3	.86	.02	.05	<2	<2
RE 7700 3650 K	1	8	10	57	<.3	8	4	429	1.65	6	<5	<2	2	31	<.2	<2	<2	42	.40	.060	13	14	.31	150	.05	<3	.88	.02	.05	<2	<2
7700 3700 K	1	10	13	54	<.3	8	5	270	1.96	8	<5	<2	3	31	<.2	<2	<2	55	.41	.071	17	17	.34	153	.06	<3	.96	.02	.04	<2	17
7700 3750 K	1	9	12	58	<.3	8	5	229	2.51	7	<5	<2	5	31	<.2	<2	<2	78	.48	.091	21	19	.33	136	.08	<3	.86	.02	.05	<2	54
7700 3800 K	1	10	14	51	<.3	9	4	257	1.58	6	6	<2	2	51	.3	<2	<2	41	.55	.068	13	14	.33	187	.05	<3	.89	.02	.04	<2	4
7700 3850 K	1	15	10	42	<.3	8	4	223	1.85	5	<5	<2	3	36	<.2	3	<2	48	.44	.022	13	17	.37	308	.08	<3	1.07	.02	.12	<2	<2
7700 3900 K	1	7	5	39	<.3	8	4	218	2.14	4	<5	<2	5	18	<.2	<2	<2	58	.26	.010	10	15	.43	185	.09	<3	1.27	.02	.13	<2	<2
7700 3950 K	1	18	<3	38	<.3	8	5	322	1.79	3	<5	<2	2	46	<.2	<2	<2	44	1.08	.054	32	12	.40	582	.05	<3	1.24	.03	.11	<2	<2
7700 4000 K	1	26	4	33	<.3	10	7	509	1.91	3	<5	<2	<2	36	<.2	<2	<2	57	.54	.042	18	11	.19	365	.07	<3	.94	.03	.05	<2	<2
7700 4050 K	<1	7	<3	5	<.3	1	1	80	.35	<2	<5	<2	<2	23	<.2	<2	<2	9	.34	.026	3	2	.06	134	.02	<3	.32	.05	.03	<2	<2
7700 4100 K	1	8	8	45	<.3	11	4	279	2.24	4	<5	<2	3	24	<.2	2	<2	64	.42	.010	11	24	.53	196	.12	<3	1.17	.01	.16	<2	2
7700 4150 K	1	29	5	29	<.3	9	5	302	1.67	3	<5	<2	<2	31	<.2	<2	<2	41	.57	.038	12	14	.32	291	.05	<3	1.07	.03	.08	<2	<2
7700 4200 K	<1	10	<3	11	<.3	3	2	122	.58	<2	<5	<2	<2	44	<.2	2	<2	17	.96	.046	5	3	.09	286	.03	<3	.41	.04	.02	<2	<2
7700 4250 K	3	28	<3	15	<.3	7	14	2943	1.26	4	<5	<2	<2	79	<.2	<2	<2	34	2.20	.096	24	6	.11	580	.02	3	1.00	.03	.02	<2	<2
7700 4300 K	1	10	10	43	<.3	10	6	308	2.59	3	<5	<2	7	20	.2	<2	<2	65	.32	.019	15	18	.54	286	.09	<3	1.61	.01	.12	<2	<2
7700 4350 K	1	35	7	28	<.3	9	8	445	1.81	2	<5	<2	2	27	<.2	<2	<2	46	.33	.036	14	14	.29	319	.06	<3	1.18	.03	.08	<2	<2
7700 4400 K	1	9	7	50	<.3	10	6	342	2.87	3	<5	<2	6	23	<.2	<2	<2	76	.35	.029	12	21	.63	252	.10	<3	1.59	.01	.15	<2	<2
STANDARD C2/AU-S	22	60	42	135	6.6	79	38	1204	3.97	40	16	8	38	53	21.0	16	19	78	.54	.100	42	66	1.03	211	.08	28	2.05	.07	.14	11	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
7700 4450 K	1	10	7	45	<.3	13	5	294	2.41	4	<5	<2	5	23	<.2	<2	<2	64	.33	.019	13	24	.60	199	.12	<3	1.57	.01	.10	<2	3
7700 4500 K	1	17	6	47	<.3	13	7	610	2.36	8	<5	<2	3	22	<.2	<2	<2	60	.34	.028	13	22	.50	215	.10	<3	1.45	.01	.09	<2	5
7700 4550 K	1	11	8	55	<.3	12	5	308	2.53	5	<5	<2	4	22	.2	2	<2	69	.30	.014	11	23	.56	257	.11	<3	1.58	.01	.09	<2	3
7800 3500 K	1	10	15	88	<.3	8	5	437	2.30	7	<5	<2	3	40	.3	<2	<2	62	.52	.071	16	17	.37	183	.06	<3	.97	.02	.06	<2	12
7800 3550 K	1	11	13	76	<.3	9	7	520	1.97	9	<5	<2	3	33	.4	<2	<2	55	.46	.076	17	17	.38	174	.06	<3	.99	.02	.05	<2	34
7800 3600 K	1	9	10	54	<.3	8	4	185	1.44	5	<5	<2	3	35	.2	<2	<2	37	.43	.066	16	13	.30	157	.05	<3	.85	.02	.04	<2	3
7800 3650 K	1	11	15	70	<.3	8	5	229	1.79	6	<5	<2	3	40	.3	<2	<2	49	.49	.073	16	16	.37	188	.06	<3	1.00	.02	.05	<2	23
7800 3700 K	1	10	23	58	<.3	6	4	384	1.46	11	<5	<2	4	26	.3	<2	<2	34	.35	.059	15	11	.27	157	.05	<3	.75	.02	.05	<2	3
7800 3750 K	<1	11	<3	18	<.3	4	3	160	.97	2	<5	<2	<2	33	<.2	<2	<2	26	.58	.053	11	6	.13	365	.04	<3	.58	.05	.04	<2	<2
7800 3800 K	1	12	<3	23	<.3	5	4	277	1.40	2	<5	<2	<2	34	<.2	<2	<2	39	.60	.045	15	8	.16	436	.05	3	.76	.04	.05	<2	3
7800 3850 K	1	13	10	44	<.3	9	8	406	2.62	4	<5	<2	6	29	<.2	<2	<2	65	.54	.041	33	18	.49	613	.07	<3	1.40	.02	.10	<2	<2
7800 3900 K	1	19	7	42	<.3	9	7	471	2.49	<2	<5	<2	4	44	<.2	<2	2	70	.83	.051	30	12	.34	708	.07	<3	1.29	.03	.08	<2	<2
7800 3950 K	1	15	9	51	<.3	10	9	586	3.06	2	<5	<2	8	33	<.2	2	<2	72	.67	.034	31	19	.60	618	.06	<3	1.88	.02	.15	<2	<2
7800 4000 K	<1	17	3	33	<.3	6	5	298	1.84	2	<5	<2	<2	24	.4	<2	<2	49	.36	.032	14	9	.22	302	.04	<3	.91	.03	.10	<2	<2
7800 4050 K	1	27	11	40	<.3	8	9	577	2.58	3	<5	<2	5	50	<.2	<2	<2	60	1.10	.058	43	17	.44	797	.03	<3	1.75	.03	.11	<2	<2
7800 4100 K	1	7	8	54	<.3	5	8	521	3.36	2	<5	<2	10	22	<.2	2	2	87	.34	.025	16	13	.58	268	.06	<3	1.24	.02	.19	<2	<2
7800 4150 K	1	16	<3	23	<.3	7	5	1005	1.47	3	<5	<2	2	44	<.2	<2	<2	32	.99	.050	28	7	.16	672	.03	<3	.92	.04	.05	<2	<2
RE 7800 4500 K	1	16	7	45	<.3	13	5	252	2.65	6	<5	<2	3	21	.2	<2	<2	73	.26	.031	13	24	.48	173	.11	<3	1.76	.02	.07	<2	<2
7800 4200 K	1	11	8	56	<.3	8	9	610	3.31	<2	<5	<2	8	29	<.2	<2	2	86	.45	.028	13	17	.69	338	.09	<3	1.74	.02	.15	<2	<2
7800 4250 K	1	16	8	65	<.3	11	11	732	3.68	4	<5	<2	12	30	<.2	<2	<2	96	.62	.050	29	23	.88	512	.13	<3	2.01	.02	.12	<2	7
7800 4300 K	<1	12	<3	25	<.3	4	4	176	1.76	<2	<5	<2	2	23	<.2	<2	<2	45	.51	.053	10	6	.11	427	.05	<3	.99	.06	.06	<2	<2
7800 4350 K	1	14	10	50	<.3	11	8	511	2.67	2	<5	<2	10	25	<.2	2	<2	63	.41	.045	23	20	.49	522	.07	<3	1.66	.02	.11	<2	6
7800 4400 K	1	25	10	76	<.3	20	10	563	3.92	5	<5	<2	6	29	.5	<2	<2	93	.35	.031	13	30	.83	423	.12	<3	3.12	.02	.16	<2	<2
7800 4500 K	1	16	7	47	<.3	13	5	261	2.74	5	<5	<2	3	21	<.2	<2	<2	75	.26	.032	12	24	.51	181	.11	<3	1.84	.02	.08	<2	2
7900 3500 K	1	11	15	81	<.3	9	6	288	3.63	4	<5	<2	5	43	<.2	<2	<2	121	.58	.092	23	24	.40	198	.11	<3	1.02	.02	.05	3	<2
7900 3550 K	1	12	13	72	<.3	9	5	236	1.74	8	<5	<2	3	44	.4	<2	<2	44	.51	.075	17	17	.38	201	.06	<3	1.06	.02	.06	<2	9
7900 3600 K	1	8	10	49	<.3	6	4	146	1.36	5	<5	<2	3	30	<.2	2	<2	35	.40	.065	13	12	.27	132	.06	<3	.77	.02	.05	<2	<2
7900 3650 K	1	15	16	79	<.3	11	8	369	1.90	9	<5	<2	4	43	.4	<2	<2	46	.50	.069	20	18	.38	228	.06	<3	1.11	.02	.06	<2	5
7900 3700 K	1	21	9	52	<.3	10	7	595	2.66	4	<5	<2	8	52	<.2	2	<2	67	1.19	.063	30	18	.51	814	.08	3	1.39	.02	.13	<2	<2
7900 3750 K	1	13	3	40	<.3	5	8	477	2.45	<2	<5	<2	2	36	<.2	<2	<2	82	.74	.068	17	11	.19	442	.10	<3	.72	.04	.05	<2	<2
7900 3800 K	1	24	6	35	<.3	9	5	360	1.71	3	<5	<2	2	67	.3	<2	<2	37	1.46	.061	47	13	.31	1016	.03	<3	1.51	.03	.09	<2	<2
7900 3850 K	<1	16	5	43	<.3	6	5	267	2.23	<2	<5	<2	4	44	<.2	<2	<2	60	.88	.045	24	12	.34	561	.06	<3	1.31	.03	.11	<2	<2
7900 3900 K	1	15	3	32	<.3	6	4	220	1.82	<2	<5	<2	3	43	<.2	<2	<2	51	.90	.043	24	9	.23	546	.05	<3	1.00	.03	.07	<2	<2
7900 3950 K	1	19	5	34	<.3	7	5	297	1.79	2	<5	<2	3	58	<.2	<2	<2	41	1.31	.051	49	10	.32	838	.04	<3	1.36	.03	.10	<2	4
7900 4000 K	1	27	7	51	<.3	10	7	448	2.56	2	<5	<2	7	49	<.2	<2	<2	54	1.16	.052	87	14	.48	1079	.03	<3	2.28	.02	.20	<2	<2
STANDARD C2/AU-S	22	58	44	135	6.5	77	39	1197	4.03	43	19	7	36	52	20.8	17	19	79	.56	.101	42	65	1.04	204	.09	29	2.08	.06	.14	11	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ACME ANALYTICAL



ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
7900 4050 K	1	12	4	31	<.3	4	4	192	1.66	<2	<5	<2	4	30	<.2	<2	<2	39	.51	.032	22	7	.28	383	.05	<3	1.06	.04	.08	<2	4
7900 4100 K	1	23	7	50	<.3	9	6	394	2.25	3	<5	<2	3	56	.4	<2	<2	53	1.09	.061	20	18	.39	626	.04	3	1.31	.02	.11	<2	5
7900 4150 K	<1	22	3	34	<.3	6	5	279	1.49	2	<5	<2	<2	52	<.2	<2	<2	41	1.05	.043	9	12	.23	475	.05	<3	.79	.03	.07	<2	5
7900 4200 K	1	23	<3	19	<.3	6	4	416	.52	3	<5	<2	<2	90	.4	2	<2	10	2.07	.069	9	5	.12	847	.01	5	.66	.03	.03	<2	<2
7900 4250 K	1	11	9	40	<.3	9	4	281	2.09	2	<5	<2	3	23	<.2	<2	<2	59	.31	.011	11	23	.44	199	.11	<3	1.16	.01	.10	<2	2
7900 4300 K	1	19	3	15	<.3	7	4	161	.89	<2	<5	<2	<2	72	<.2	2	<2	16	1.03	.067	19	7	.10	656	.02	<3	1.02	.04	.04	<2	<2
7900 4350 K	2	11	9	47	<.3	8	9	561	2.92	3	<5	<2	8	23	<.2	7	3	68	.36	.033	16	17	.49	779	.07	<3	1.21	.01	.15	<2	<2
7900 4400 K	2	28	12	44	<.3	12	15	1688	2.67	<2	<5	<2	3	28	<.2	<2	<2	65	.31	.028	15	24	.40	300	.07	<3	1.81	.03	.09	<2	2
7900 4450 K	1	15	9	48	<.3	8	5	417	2.64	3	<5	<2	5	19	<.2	<2	<2	69	.20	.020	11	17	.33	227	.07	<3	1.30	.01	.09	<2	<2
7900 4500 K	2	10	14	45	<.3	9	6	517	3.11	7	<5	<2	4	14	.2	<2	<2	93	.15	.039	10	21	.35	113	.11	<3	1.35	.01	.08	<2	<2
8000 3500 K	1	10	16	66	<.3	9	5	490	1.72	3	<5	<2	3	32	<.2	<2	<2	40	.45	.056	14	20	.42	183	.07	<3	1.23	.02	.06	<2	<2
8000 3550 K	1	9	12	56	<.3	7	4	185	2.06	5	<5	<2	3	32	<.2	<2	<2	58	.46	.075	17	18	.32	129	.06	<3	.85	.02	.04	<2	32
8000 3600 K	1	11	14	67	<.3	8	5	219	1.99	7	<5	<2	3	34	.2	<2	2	52	.46	.071	16	17	.35	150	.06	<3	.90	.02	.05	<2	51
8000 3650 K	1	11	15	70	<.3	8	5	246	1.87	6	<5	<2	2	43	.2	2	<2	47	.54	.075	15	18	.36	165	.05	<3	.96	.02	.05	<2	2
RE 7900 4250 K	1	13	8	42	<.3	10	4	295	2.20	3	<5	<2	3	25	<.2	<2	<2	62	.32	.011	12	24	.47	218	.11	<3	1.27	.01	.11	<2	<2
8000 3700 K	1	8	12	58	<.3	7	4	271	1.52	5	<5	<2	3	32	<.2	<2	<2	38	.46	.073	15	15	.30	136	.05	<3	.82	.02	.04	<2	2
8000 3750 K	1	14	16	76	<.3	8	6	401	1.86	8	<5	<2	3	42	.2	<2	<2	45	.54	.071	17	19	.37	201	.06	<3	1.06	.02	.06	<2	2
8000 3800 K	1	14	10	38	<.3	9	4	202	1.78	4	<5	<2	6	24	<.2	<2	<2	44	.45	.038	17	21	.37	297	.07	<3	1.06	.02	.07	<2	8
8000 3850 K	1	15	9	34	<.3	8	5	400	2.02	7	<5	<2	5	26	<.2	<2	<2	46	.43	.039	20	20	.27	367	.05	<3	1.10	.02	.08	<2	<2
8000 3900 K	1	15	8	42	<.3	10	5	326	2.28	9	<5	<2	3	27	<.2	<2	<2	54	.37	.019	12	24	.37	375	.06	<3	1.35	.02	.10	<2	5
8000 3950 K	1	15	9	38	<.3	8	5	286	2.22	6	<5	<2	4	27	<.2	<2	<2	53	.45	.045	18	20	.33	373	.05	<3	1.03	.02	.10	<2	136
8000 4000 K	1	18	10	60	<.3	18	7	312	3.11	8	<5	<2	5	25	<.2	<2	2	75	.30	.017	14	37	.65	462	.10	<3	2.17	.02	.10	<2	5
8000 4050 K	2	25	13	68	<.3	13	7	621	3.05	5	<5	<2	4	28	<.2	<2	2	79	.34	.019	18	30	.52	601	.10	<3	1.75	.02	.16	<2	5
8000 4100 K	1	13	9	64	<.3	10	9	521	3.54	<2	<5	<2	9	27	.3	<2	<2	88	.49	.030	18	20	.83	410	.10	<3	2.04	.02	.20	<2	<2
8000 4150 K	1	19	8	57	<.3	12	6	355	2.65	<2	<5	<2	5	31	<.2	<2	<2	68	.46	.025	17	26	.59	424	.10	<3	1.81	.02	.17	<2	<2
8000 4200 K	1	17	10	60	<.3	13	8	516	3.03	2	<5	<2	9	25	<.2	<2	<2	72	.42	.025	19	25	.67	411	.11	<3	1.82	.02	.14	<2	<2
8000 4250 K	1	19	10	50	<.3	12	7	352	2.64	<2	<5	<2	8	32	.3	<2	<2	69	.58	.038	28	26	.64	472	.10	<3	1.76	.02	.12	<2	<2
8000 4300 K	1	18	3	31	<.3	6	6	489	1.81	<2	5	<2	4	34	<.2	<2	<2	45	.69	.041	27	11	.23	414	.04	3	1.31	.04	.07	<2	<2
8000 4350 K	1	17	10	49	<.3	14	8	415	2.91	2	<5	<2	7	23	<.2	<2	<2	73	.28	.025	18	25	.53	353	.10	<3	1.89	.02	.10	<2	<2
8000 4400 K	1	14	9	48	<.3	14	6	265	2.78	4	<5	<2	4	23	<.2	<2	<2	70	.29	.021	11	25	.49	202	.09	<3	1.56	.01	.09	<2	<2
8000 4450 K	1	19	9	53	<.3	13	7	365	3.01	4	<5	<2	6	26	.2	<2	<2	74	.28	.021	13	25	.52	292	.09	<3	1.87	.01	.13	<2	5
8000 4500 K	2	24	19	68	<.3	11	10	547	3.43	<2	<5	<2	9	27	<.2	<2	2	63	.24	.027	21	17	.41	449	.02	<3	2.35	.01	.12	<2	<2
8000 4550 K	1	21	11	61	<.3	21	9	326	3.42	<2	<5	<2	11	19	<.2	<2	<2	78	.21	.023	16	31	.65	229	.09	<3	2.99	.01	.12	<2	<2
8100 3500 K	1	15	13	84	<.3	10	7	1461	1.65	4	<5	<2	<2	51	<.2	<2	<2	33	.57	.061	11	19	.38	253	.05	<3	1.26	.02	.05	<2	<2
8100 3550 K	1	17	14	79	<.3	11	5	286	2.02	4	5	<2	3	38	<.2	<2	<2	52	.46	.065	19	21	.42	185	.06	<3	1.20	.02	.07	<2	<2
STANDARD C2/AU-S	22	58	43	142	5.8	75	37	1195	3.91	37	15	7	32	50	21.7	17	16	73	.56	.096	38	71	1.01	181	.08	25	1.90	.05	.13	10	49

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
8100 3600 K	1	12	18	75	<.3	9	5	248	2.09	10	<5	<2	3	41	<.2	<2	<2	52	.57	.088	18	18	.39	172	.06	<3	.99	.02	.06	<2	3
8100 3650 K	1	13	14	69	<.3	9	6	451	2.10	9	5	<2	2	42	.3	<2	<2	40	.56	.082	16	17	.37	235	.05	<3	1.09	.02	.05	<2	6
8100 3700 K	1	10	14	66	<.3	7	5	536	1.92	11	<5	<2	4	28	.4	2	<2	45	.44	.076	16	14	.31	154	.05	<3	.78	.02	.06	<2	<2
8100 3750 K	1	11	12	71	<.3	8	5	327	2.05	6	<5	<2	3	41	.2	2	<2	52	.59	.091	17	18	.37	188	.06	<3	1.04	.02	.06	<2	45
8100 3800 K	1	10	9	70	<.3	8	4	224	2.51	6	<5	<2	4	36	<.2	<2	2	73	.54	.085	19	20	.34	169	.06	<3	.95	.02	.05	<2	188
8100 3850 K	1	35	11	41	<.3	11	5	265	2.28	5	5	<2	3	34	<.2	<2	2	52	.74	.047	35	18	.26	1115	.04	3	1.44	.03	.11	<2	6
8100 3900 K	2	16	11	53	<.3	13	6	342	3.04	6	<5	<2	4	18	.2	<2	2	75	.21	.056	11	29	.43	235	.07	<3	2.24	.02	.10	7	<2
8100 3950 K	1	11	7	38	<.3	10	4	269	2.40	6	<5	<2	2	22	<.2	<2	2	66	.26	.017	11	23	.40	224	.08	<3	1.46	.02	.09	2	<2
8100 4000 K	1	17	9	62	<.3	18	6	285	3.31	6	<5	<2	4	28	<.2	<2	<2	80	.35	.017	12	37	.65	422	.09	<3	2.51	.02	.11	<2	<2
8100 4050 K	1	16	9	49	<.3	12	6	264	2.90	9	<5	<2	3	25	<.2	<2	<2	64	.27	.025	15	24	.42	379	.04	<3	1.86	.02	.10	<2	<2
8100 4100 K	1	15	5	47	<.3	12	5	405	2.78	8	<5	<2	4	17	<.2	2	<2	68	.19	.014	13	24	.36	337	.08	<3	1.56	.01	.07	<2	3
8100 4150 K	1	12	4	31	<.3	7	4	198	1.96	5	<5	<2	2	23	<.2	<2	<2	54	.25	.020	7	13	.24	182	.08	<3	1.05	.03	.12	<2	<2
8100 4200 K	<1	3	<3	17	<.3	2	2	80	1.21	<2	<5	<2	<2	13	<.2	<2	<2	43	.20	.051	2	3	.06	50	.07	<3	.20	.05	.03	<2	<2
8100 4250 K	1	22	9	72	<.3	14	9	678	3.18	6	<5	<2	5	30	<.2	<2	<2	79	.46	.034	16	30	.67	387	.09	<3	2.39	.02	.15	<2	<2
RE 8100 3750 K	1	11	13	71	<.3	9	5	333	2.10	8	<5	<2	3	42	.3	2	<2	53	.60	.091	16	18	.38	192	.06	<3	1.06	.02	.06	3	64
8100 4300 K	2	44	11	55	<.3	14	17	1930	3.18	3	<5	<2	3	36	.2	<2	2	85	.42	.052	42	29	.52	724	.08	<3	2.31	.02	.15	<2	2
8100 4350 K	1	16	8	58	<.3	16	7	356	3.45	7	<5	<2	5	24	<.2	2	<2	86	.36	.030	17	34	.72	324	.12	<3	2.25	.02	.16	2	<2
8100 4450 K	1	55	7	48	<.3	8	6	524	2.30	3	<5	<2	6	34	.3	<2	<2	48	.44	.038	28	14	.38	604	.05	<3	1.46	.03	.11	<2	<2
8100 4500 K	1	15	7	62	<.3	13	7	417	3.35	3	<5	<2	5	26	<.2	6	<2	71	.35	.045	14	25	.68	280	.06	<3	2.06	.01	.16	<2	3
8100 4550 K	1	13	7	45	<.3	12	5	365	2.74	6	<5	<2	3	21	<.2	<2	2	74	.24	.040	11	25	.45	181	.11	<3	1.50	.02	.10	<2	<2
8100 4600 K	1	25	9	30	<.3	8	3	262	1.81	2	<5	<2	<2	20	.2	<2	<2	54	.20	.029	10	15	.21	223	.06	<3	1.19	.02	.05	<2	<2
8200 1835 K	1	32	124	98	<.3	11	12	1042	3.07	2	<5	<2	17	22	.8	<2	<2	44	.30	.057	27	18	.43	281	.02	<3	1.57	.01	.10	<2	44
8200 1860 K	1	22	17	54	<.3	18	9	513	3.43	3	<5	<2	10	14	<.2	<2	<2	69	.18	.047	19	35	.47	103	.07	3	2.59	.01	.09	<2	<2
8200 3500 K	1	10	12	59	<.3	8	4	247	1.87	7	<5	<2	3	41	.2	<2	<2	46	.58	.082	18	18	.36	178	.06	3	.99	.02	.05	<2	5
8200 3550 K	1	14	15	69	<.3	10	5	454	2.03	9	<5	<2	3	47	<.2	<2	<2	45	.61	.085	18	18	.40	234	.05	<3	1.17	.02	.05	<2	9
8200 3600 K	1	8	10	57	<.3	8	4	191	1.89	8	<5	<2	3	31	<.2	<2	2	50	.50	.085	18	16	.31	152	.06	<3	.91	.02	.04	<2	3
8200 3650 K	<1	9	8	53	<.3	7	4	268	1.58	5	<5	<2	3	29	<.2	<2	<2	39	.44	.071	14	14	.30	164	.05	<3	.87	.02	.04	<2	82
8200 3700 K	1	8	9	52	<.3	6	4	241	1.74	5	<5	<2	3	36	<.2	<2	<2	45	.53	.081	15	16	.32	175	.06	<3	.89	.02	.05	2	<2
8200 3750 K	<1	15	4	32	<.3	8	3	196	1.66	5	<5	<2	5	27	<.2	<2	<2	38	.52	.050	16	16	.35	426	.05	<3	1.01	.02	.09	2	10
8200 3800 K	1	15	6	48	<.3	9	7	591	2.20	4	<5	<2	6	29	<.2	<2	<2	49	.52	.036	17	19	.45	536	.07	<3	1.43	.02	.11	<2	4
8200 3850 K	1	20	8	51	<.3	12	7	583	2.24	2	<5	<2	4	30	<.2	<2	<2	51	.60	.043	19	20	.50	673	.07	<3	1.46	.02	.13	<2	7
8200 3900 K	<1	11	4	60	<.3	6	6	418	2.50	4	<5	<2	6	23	<.2	<2	<2	60	.47	.036	16	15	.52	372	.09	<3	1.15	.02	.20	<2	<2
8200 3950 K	1	20	11	44	<.3	10	6	476	2.39	3	<5	<2	11	25	<.2	<2	<2	52	.49	.048	61	20	.41	846	.05	<3	1.64	.02	.11	<2	172
8200 4000 K	1	13	9	56	<.3	14	6	319	2.91	5	<5	<2	4	29	<.2	<2	<2	71	.46	.024	13	28	.57	555	.07	<3	1.88	.02	.11	<2	3
8200 4050 K	1	16	8	59	<.3	17	7	318	3.00	5	<5	<2	5	22	<.2	<2	<2	74	.36	.028	12	31	.63	311	.11	<3	2.03	.02	.14	<2	3
STANDARD C2/AU-S	20	59	38	133	6.1	69	33	1176	3.82	40	17	7	35	50	19.4	15	16	70	.55	.104	40	66	.97	199	.08	27	1.96	.06	.13	12	44

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
8200 4100 K	1	16	8	53	<.3	14	9	418	3.33	4	<5	<2	5	18	<.2	<2	<2	81	.26	.036	14	25	.67	266	.10	<3	2.15	.02	.14	<2	2
8200 4150 K	1	15	7	50	<.3	18	9	395	3.24	6	<5	<2	9	26	<.2	<2	<2	77	.33	.025	15	25	.68	471	.11	<3	2.31	.02	.14	<2	5
8200 4200 K	1	25	8	45	<.3	13	7	593	2.52	5	<5	<2	2	27	<.2	<2	<2	64	.38	.036	14	24	.46	380	.10	<3	1.60	.02	.11	<2	2
8200 4250 K	<1	16	4	52	<.3	17	8	383	3.00	2	<5	<2	5	26	<.2	3	<2	79	.33	.023	13	31	.72	477	.12	<3	2.65	.02	.13	<2	<2
8200 4300 K	1	19	7	47	<.3	17	7	309	3.14	5	<5	<2	5	26	<.2	<2	<2	80	.30	.031	13	30	.65	271	.14	<3	2.14	.02	.10	<2	2
8200 4350 K	<1	22	6	38	<.3	13	6	245	2.73	6	<5	<2	4	22	<.2	<2	<2	60	.27	.038	12	23	.45	184	.10	<3	1.84	.02	.09	<2	3
8200 4400 K	1	17	8	46	<.3	15	7	279	3.09	5	<5	<2	5	19	.2	<2	<2	67	.25	.035	13	25	.53	183	.09	<3	2.06	.02	.08	<2	<2
8200 4450 K	1	14	10	46	<.3	11	7	344	3.26	2	<5	<2	5	22	<.2	2	<2	78	.24	.034	12	20	.53	215	.07	<3	2.20	.01	.08	<2	<2
8200 4500 K	1	17	7	55	<.3	17	7	324	3.20	4	<5	<2	7	19	<.2	<2	<2	71	.25	.030	14	30	.63	200	.10	<3	2.28	.01	.09	<2	5
8300 3500 K	<1	12	5	32	<.3	7	2	157	1.13	2	<5	<2	<2	23	<.2	<2	2	28	.36	.044	9	11	.22	139	.05	<3	.88	.03	.04	<2	3
8300 3600 K	1	9	13	58	<.3	8	5	218	2.13	4	<5	<2	4	37	.2	2	3	60	.50	.078	18	17	.35	147	.07	<3	.95	.02	.06	<2	54
8300 3650 K	<1	9	9	55	<.3	7	4	186	1.77	6	<5	<2	3	37	<.2	<2	<2	47	.47	.074	15	13	.31	157	.06	<3	.84	.02	.05	<2	6
8300 3700 K	1	9	8	60	<.3	7	5	270	2.24	8	<5	<2	3	32	<.2	<2	<2	61	.47	.079	17	16	.33	147	.07	<3	.91	.02	.06	<2	92
8300 3750 K	1	9	12	51	<.3	7	5	211	1.70	8	<5	<2	3	33	.2	<2	<2	42	.44	.073	15	13	.31	143	.06	<3	.85	.02	.05	<2	4
8300 3800 K	1	10	11	49	<.3	7	5	391	1.94	9	<5	<2	4	40	<.2	<2	<2	50	.51	.073	17	14	.33	192	.06	<3	.91	.02	.04	<2	13
8300 3850 K	2	19	5	36	<.3	7	4	296	2.07	5	<5	<2	4	27	<.2	<2	<2	60	.44	.038	16	14	.28	372	.09	<3	.81	.03	.08	<2	<2
8300 3900 K	1	10	5	26	<.3	4	3	209	1.73	4	<5	<2	3	20	<.2	<2	<2	52	.27	.043	11	8	.12	255	.07	<3	.65	.04	.07	<2	2
8300 3950 K	1	14	13	48	<.3	9	6	418	2.76	4	<5	<2	5	24	<.2	<2	<2	67	.35	.023	15	20	.48	418	.07	<3	1.70	.02	.14	<2	3
8300 4000 K	1	9	8	58	<.3	7	7	443	3.17	2	<5	<2	13	25	<.2	<2	<2	77	.27	.038	20	14	.68	239	.11	<3	1.31	.02	.24	<2	<2
8300 4050 K	<1	14	11	48	<.3	10	6	363	2.50	5	<5	<2	6	21	<.2	<2	<2	61	.33	.030	14	20	.49	303	.08	<3	1.47	.02	.10	<2	3
RE 8200 4250 K	1	16	7	52	<.3	17	8	387	3.03	2	<5	<2	6	27	<.2	<2	<2	80	.34	.023	13	32	.73	482	.12	<3	2.66	.02	.13	<2	<2
8300 4100 K	1	12	9	45	<.3	12	6	328	2.71	4	<5	<2	3	24	<.2	<2	<2	68	.30	.022	10	23	.42	331	.07	<3	1.64	.02	.10	<2	2
8300 4150 K	<1	14	10	44	<.3	12	8	521	3.02	5	<5	<2	3	20	<.2	<2	<2	77	.20	.018	10	20	.46	387	.08	<3	1.76	.02	.09	<2	2
8300 4200 K	1	15	12	57	<.3	11	10	427	3.55	2	<5	<2	10	24	<.2	<2	<2	86	.29	.018	13	22	.74	385	.06	<3	2.28	.02	.14	<2	<2
8300 4250 K	1	20	3	56	<.3	19	10	315	3.29	5	<5	<2	6	21	<.2	<2	<2	80	.28	.030	12	29	.65	250	.10	<3	2.42	.02	.14	<2	2
8300 4300 K	1	18	6	56	<.3	18	8	461	3.14	3	<5	<2	5	23	<.2	2	<2	81	.30	.025	12	27	.70	339	.13	<3	2.13	.02	.14	<2	7
8300 4350 K	1	24	8	55	<.3	17	9	624	3.60	5	<5	<2	5	26	.3	<2	<2	81	.34	.047	14	31	.66	398	.10	<3	2.34	.02	.15	<2	<2
8300 4400 K	1	22	9	49	<.3	12	8	477	3.19	4	<5	<2	3	23	.3	<2	2	95	.28	.034	11	23	.55	289	.11	<3	1.99	.02	.09	<2	<2
8300 4450 K	1	24	6	60	<.3	22	14	480	3.78	2	<5	<2	7	32	.3	<2	12	84	.42	.039	13	36	.97	382	.06	<3	3.80	.01	.12	<2	2
8300 4500 K	1	30	6	53	<.3	14	10	408	3.10	<2	<5	<2	9	25	<.2	<2	3	75	.29	.030	17	19	.64	433	.07	3	3.13	.02	.15	<2	3
8300 4550 K	1	12	5	30	<.3	9	4	265	2.25	9	<5	<2	2	15	<.2	<2	<2	62	.17	.025	10	17	.32	114	.10	<3	1.08	.02	.07	<2	<2
8300 4600 K	1	21	8	33	<.3	10	4	182	2.19	4	<5	<2	2	23	<.2	<2	<2	62	.23	.024	12	18	.34	200	.08	<3	1.52	.02	.06	<2	<2
8300 4650 K	1	16	15	64	<.3	12	11	684	3.46	3	<5	<2	13	22	.3	<2	<2	65	.28	.037	24	20	.53	306	.04	<3	2.30	.01	.11	<2	<2
8400 3450 K	<1	12	14	51	<.3	9	4	181	1.34	5	<5	<2	2	28	<.2	<2	<2	35	.45	.066	14	15	.35	157	.06	<3	1.03	.02	.06	<2	22
8400 3500 K	<1	11	11	53	<.3	8	4	213	1.55	7	<5	<2	3	42	<.2	<2	<2	38	.50	.065	17	14	.36	193	.06	<3	1.04	.02	.05	<2	10
STANDARD C2/AU-S	22	64	36	135	6.7	76	38	1266	4.11	40	19	8	38	53	21.2	19	19	79	.56	.103	42	63	1.06	213	.08	30	2.14	.07	.15	11	51

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
8400 3550 K	1	9	9	57	<.3	6	4	234	1.83	8	<5	<2	3	34	.2	<2	<2	47	.48	.079	17	15	.32	154	.06	3	.89	.02	.04	<2	120
8400 3600 K	1	8	10	53	<.3	7	4	290	1.68	8	<5	<2	3	35	.2	<2	<2	39	.47	.075	16	14	.32	162	.05	3	.86	.02	.04	<2	3
8400 3650 K	1	10	10	56	<.3	8	5	196	1.81	7	<5	<2	2	41	<.2	<2	<2	46	.50	.070	15	16	.35	193	.06	3	.98	.02	.04	<2	5
8400 3700 K	1	13	8	29	<.3	8	3	159	1.62	7	<5	<2	6	22	<.2	<2	<2	43	.34	.044	14	17	.34	239	.08	4	.87	.02	.07	<2	7
8400 3800 K	2	21	9	48	<.3	14	7	348	2.48	8	<5	<2	8	24	<.2	<2	<2	57	.34	.023	28	30	.56	626	.09	3	1.67	.02	.08	<2	2
8400 3850 K	1	18	10	44	<.3	12	7	451	2.50	7	<5	<2	5	28	.2	<2	<2	68	.31	.018	14	27	.44	501	.00	5	1.66	.02	.08	<2	6
8400 3900 K	1	12	7	37	<.3	10	6	198	2.29	8	<5	<2	5	17	.2	<2	<2	53	.18	.019	12	19	.33	273	.05	<3	1.38	.01	.10	<2	9
8400 3950 K	1	13	11	48	<.3	12	6	379	2.59	5	<5	<2	3	24	.2	<2	<2	65	.28	.017	14	26	.46	437	.08	<3	1.67	.01	.13	<2	<2
8400 4000 K	1	10	9	42	<.3	10	4	201	2.73	8	<5	<2	4	20	<.2	<2	<2	65	.24	.020	11	22	.40	248	.07	3	1.38	.01	.11	<2	<2
8400 4050 K	1	14	8	44	<.3	11	6	363	2.64	3	<5	<2	5	18	<.2	<2	<2	63	.19	.014	12	21	.39	308	.08	<3	1.60	.02	.07	<2	<2
8400 4100 K	1	13	8	81	<.3	11	10	574	4.47	<2	<5	<2	13	21	.2	<2	<2	113	.26	.026	13	23	1.12	346	.16	<3	3.04	.02	.20	<2	<2
8400 4150 K	<1	15	6	77	<.3	10	13	941	4.15	<2	<5	<2	15	34	<.2	<2	2	97	.34	.041	18	21	.94	505	.09	3	2.84	.02	.17	<2	<2
8400 4200 K	<1	23	5	48	<.3	11	7	353	2.85	5	<5	<2	10	30	.3	2	<2	72	.42	.032	25	22	.59	519	.11	3	1.91	.02	.14	<2	2
8400 4250 K	1	15	6	50	<.3	11	5	289	2.80	2	<5	<2	6	23	<.2	<2	<2	77	.30	.019	13	25	.57	289	.14	<3	2.05	.02	.12	<2	3
8400 4300 K	1	12	7	46	<.3	8	8	307	2.73	3	<5	<2	8	18	<.2	<2	<2	65	.29	.052	19	19	.57	222	.10	3	1.86	.02	.08	<2	<2
8400 4350 K	1	19	7	71	<.3	16	8	442	3.43	6	<5	<2	7	26	.2	<2	<2	85	.31	.026	15	30	.69	372	.13	3	2.59	.02	.14	<2	2
RE 8400 4400 K	1	21	4	59	<.3	20	10	330	3.10	3	<5	<2	8	19	<.2	<2	<2	69	.26	.027	12	30	.67	242	.11	3	2.86	.02	.11	<2	16
8400 4400 K	1	20	4	56	<.3	20	10	322	3.01	2	<5	<2	7	18	<.2	<2	<2	66	.25	.027	12	29	.65	234	.11	3	2.76	.01	.10	<2	4
8400 4450 K	1	18	4	54	<.3	10	8	724	3.08	<2	<5	<2	8	30	<.2	<2	<2	76	.44	.055	22	20	.60	463	.10	3	1.71	.02	.10	<2	2
8400 4500 K	1	23	4	55	<.3	17	9	329	3.57	2	<5	<2	9	21	<.2	<2	<2	80	.24	.026	14	28	.64	225	.09	<3	2.86	.01	.10	<2	3
8500 3550 K	<1	7	<3	20	<.3	2	2	77	.95	<2	<5	<2	<2	42	<.2	<2	<2	31	.64	.062	2	4	.08	110	.05	3	.29	.05	.03	<2	5
8500 3600 K	1	11	12	59	<.3	8	5	273	1.78	7	<5	<2	3	37	.2	<2	<2	41	.48	.074	17	17	.37	192	.06	4	1.08	.02	.04	<2	8
8500 3650 K	1	10	15	55	<.3	8	5	297	2.04	8	<5	<2	3	34	.2	<2	<2	52	.44	.074	17	17	.35	185	.06	3	1.01	.02	.04	2	42
8500 3700 K	1	11	13	83	<.3	9	6	484	1.81	7	<5	<2	2	55	.6	2	<2	41	.61	.066	15	17	.39	237	.05	4	1.09	.02	.05	<2	2
8500 3750 K	1	12	22	72	<.3	7	5	371	1.71	10	<5	<2	4	29	.3	<2	<2	39	.41	.069	16	14	.31	185	.06	<3	.88	.02	.06	<2	5
8500 3800 K	1	26	7	73	<.3	10	10	1496	2.33	2	<5	<2	<2	48	<.2	<2	<2	40	.71	.086	13	16	.32	829	.03	3	1.15	.02	.06	<2	5
8500 3900 K	<1	6	<3	15	<.3	2	1	76	.86	2	<5	<2	<2	12	<.2	<2	<2	22	.14	.019	5	6	.12	183	.03	<3	.52	.04	.05	<2	2
8500 3950 K	1	14	10	52	<.3	9	6	540	2.49	5	<5	<2	3	20	.2	<2	<2	61	.21	.040	11	22	.39	247	.07	<3	1.50	.01	.10	<2	3
8500 4000 K	<1	3	<3	6	<.3	1	1	32	.33	<2	<5	<2	<2	9	<.2	<2	<2	8	.12	.025	3	2	.04	132	.01	<3	.31	.05	.04	<2	<2
8500 4050 K	1	11	7	34	<.3	8	3	171	2.21	6	<5	<2	5	17	<.2	2	<2	55	.19	.024	12	16	.29	159	.06	<3	1.24	.02	.08	<2	<2
8500 4100 K	1	13	8	47	<.3	13	6	299	2.99	5	<5	<2	3	24	<.2	2	<2	74	.27	.022	12	30	.54	319	.09	3	1.88	.01	.12	<2	<2
8500 4150 K	1	11	12	50	<.3	12	5	312	2.95	3	<5	<2	3	17	<.2	2	2	75	.18	.019	12	24	.35	332	.06	<3	1.74	.01	.07	<2	5
8500 4200 K	<1	9	<3	24	<.3	4	4	253	1.37	3	<5	<2	<2	17	<.2	<2	<2	36	.16	.016	5	10	.18	165	.06	<3	.81	.04	.06	<2	5
8500 4250 K	1	13	5	58	<.3	9	9	707	3.07	<2	<5	<2	5	25	<.2	<2	<2	75	.36	.051	15	19	.60	339	.10	<3	1.81	.02	.16	<2	<2
8500 4300 K	1	20	<3	42	<.3	9	6	409	2.50	3	<5	<2	3	24	.2	<2	2	64	.32	.029	16	20	.39	385	.10	<3	1.49	.02	.10	<2	<2
STANDARD C2/AU-S	21	60	37	140	6.5	74	36	1216	4.03	42	18	8	37	52	20.7	19	17	74	.53	.100	41	68	1.04	207	.08	28	2.06	.06	.14	11	53

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
8500 4350 K	1	18	8	27	<.3	5	5	641	1.47	4	<5	<2	<2	23	<.2	<2	2	45	.25	.027	14	14	.20	284	.08	3	.98	.02	.08	<2	5
8500 4400 K	1	7	6	33	<.3	6	3	177	1.64	7	<5	<2	3	16	<.2	<2	<2	49	.21	.009	10	17	.32	144	.12	3	.93	.01	.09	<2	4
8500 4450 K	1	12	7	65	<.3	13	7	386	2.78	9	<5	<2	6	21	<.2	<2	<2	72	.31	.031	12	21	.60	277	.13	<3	1.68	.02	.12	<2	4
8500 4500 K	2	28	4	51	.3	12	10	960	3.17	<2	<5	<2	11	33	<.2	<2	<2	76	.38	.037	72	25	.52	937	.07	3	2.90	.02	.10	<2	4
8500 4550 K	<1	8	<3	40	<.3	9	5	291	2.07	7	<5	<2	4	19	<.2	<2	<2	53	.31	.044	14	18	.43	220	.11	<3	1.07	.02	.07	<2	<2
8500 4600 K	1	10	6	51	<.3	12	6	278	2.68	7	<5	<2	5	19	<.2	<2	<2	65	.24	.022	12	23	.50	265	.10	3	1.61	.01	.09	<2	2
8600 3500 K	1	10	11	49	<.3	7	4	218	1.56	5	<5	<2	2	41	<.2	<2	<2	38	.49	.065	13	15	.34	178	.06	<3	1.01	.02	.04	<2	4
8600 3550 K	1	7	8	49	<.3	7	4	175	1.54	7	<5	<2	3	34	<.2	2	<2	40	.46	.075	15	13	.31	153	.06	<3	.86	.02	.05	<2	10
RE 8500 4550 K	<1	9	5	38	<.3	8	5	276	1.97	8	<5	<2	4	18	<.2	<2	<2	51	.30	.043	14	17	.41	209	.10	3	1.02	.02	.07	<2	2
8600 3600 K	1	9	12	51	<.3	7	4	223	1.47	7	<5	<2	3	36	<.2	<2	2	35	.44	.064	15	14	.31	182	.06	3	.89	.02	.04	<2	5
8600 3650 K	<1	14	12	62	<.3	8	5	263	1.76	8	6	<2	2	42	.2	<2	<2	44	.49	.075	15	15	.34	225	.06	<3	1.03	.02	.05	<2	9
8600 3750 K	<1	7	3	24	<.3	5	2	132	1.05	5	<5	<2	2	19	<.2	<2	<2	28	.30	.051	11	13	.24	207	.06	<3	.66	.03	.07	<2	7
8600 3800 K	1	13	9	37	<.3	8	4	317	1.87	8	<5	<2	4	26	<.2	<2	<2	48	.38	.041	16	19	.33	400	.07	<3	.98	.02	.09	<2	<2
8600 3850 K	1	8	6	33	<.3	6	4	269	1.66	5	<5	<2	4	21	<.2	<2	<2	44	.29	.022	15	15	.29	319	.09	<3	.78	.02	.08	<2	7
8600 3900 K	1	6	3	19	<.3	2	5	469	1.52	4	<5	<2	<2	18	<.2	<2	<2	44	.29	.044	9	5	.08	270	.06	<3	.59	.05	.05	<2	<2
8600 3950 K	1	12	8	46	<.3	11	5	352	2.50	9	<5	<2	9	23	<.2	<2	<2	56	.27	.014	19	22	.45	539	.07	<3	1.56	.02	.10	<2	2
8600 4000 K	1	25	13	52	<.3	12	7	727	2.70	4	<5	<2	6	29	<.2	<2	<2	64	.35	.020	29	27	.47	1113	.05	<3	2.15	.01	.11	<2	<2
8600 4050 K	1	18	11	54	<.3	18	8	519	3.00	8	<5	<2	6	22	<.2	<2	<2	63	.25	.025	16	29	.51	536	.06	3	2.14	.02	.10	<2	3
8600 4100 K	1	15	10	45	<.3	15	6	298	2.64	6	<5	<2	11	16	<.2	<2	<2	52	.15	.019	19	23	.39	314	.06	3	2.05	.01	.08	<2	<2
8600 4150 K	1	16	9	61	<.3	14	10	1059	2.98	9	<5	<2	5	22	<.2	<2	2	62	.20	.047	14	24	.39	215	.06	3	1.81	.01	.12	<2	<2
8600 4200 K	1	26	10	59	<.3	21	11	342	3.37	5	<5	<2	8	19	<.2	<2	<2	76	.20	.032	13	34	.59	257	.10	3	3.22	.02	.14	<2	<2
8600 4250 K	1	13	6	55	<.3	9	6	307	2.82	6	<5	<2	8	24	<.2	<2	<2	68	.30	.017	15	21	.49	376	.09	<3	1.70	.02	.13	<2	<2
8600 4300 K	1	19	7	49	<.3	6	8	782	2.43	4	<5	<2	4	22	<.2	<2	2	68	.27	.036	18	15	.41	360	.12	<3	1.44	.03	.12	<2	<2
8600 4350 K	1	10	6	52	<.3	6	4	304	2.32	6	<5	<2	5	21	<.2	<2	<2	69	.27	.021	12	15	.48	270	.15	<3	1.13	.02	.14	<2	13
8600 4400 K	1	11	7	54	<.3	7	7	490	2.60	3	<5	<2	6	18	<.2	<2	2	70	.25	.035	14	15	.41	191	.09	<3	1.22	.02	.09	<2	<2
8600 4450 K	1	16	10	49	<.3	7	7	396	2.90	7	<5	<2	6	24	.2	2	3	72	.26	.028	19	14	.38	438	.08	<3	1.43	.02	.10	<2	<2
8600 4500 K	1	10	<3	41	<.3	7	4	274	1.85	5	<5	<2	3	18	<.2	<2	<2	48	.24	.016	14	14	.35	237	.08	<3	.92	.02	.08	<2	<2
10500 50 K	1	20	6	63	<.3	18	10	381	2.55	6	<5	<2	3	34	.3	<2	<2	62	.59	.038	17	33	.69	208	.09	3	1.76	.03	.11	<2	<2
10500 450 K	1	20	5	73	<.3	17	11	536	3.03	4	<5	<2	5	35	<.2	<2	<2	85	.65	.039	12	44	1.10	219	.14	3	2.04	.02	.10	<2	<2
10500 500 K	1	20	7	92	<.3	15	11	444	3.19	3	<5	<2	5	36	.2	<2	2	83	.71	.037	15	41	.94	255	.09	<3	1.91	.02	.10	<2	2
10500 550 K	1	20	6	74	<.3	16	10	462	3.02	5	<5	<2	6	31	.2	<2	<2	79	.56	.027	16	40	.95	246	.12	<3	1.94	.02	.12	<2	<2
10500 900 K	<1	19	5	68	<.3	10	5	268	1.96	3	<5	<2	<2	41	.4	<2	<2	48	.84	.059	15	23	.44	280	.05	3	1.29	.03	.05	<2	<2
10500 950 K	<1	16	7	111	<.3	15	11	516	3.52	2	<5	<2	8	35	.6	4	<2	96	.78	.043	22	46	1.01	287	.09	<3	1.86	.02	.14	<2	<2
10500 1000 K	1	23	30	105	<.3	11	9	532	2.37	4	<5	<2	3	42	.7	<2	<2	57	.78	.049	16	23	.46	294	.06	3	1.29	.03	.07	<2	<2
10500 1050 K	<1	16	7	117	<.3	17	13	605	3.72	<2	<5	<2	9	31	.5	<2	<2	106	.62	.042	18	53	1.51	227	.11	3	2.32	.02	.12	<2	<2
STANDARD C2/AU-S	21	59	35	139	6.3	73	36	1173	3.93	44	16	8	35	51	19.8	15	18	74	.53	.096	40	64	1.00	196	.08	29	1.99	.06	.14	11	43

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
10500 1100 K	<1	12	12	77	<.3	10	8	383	2.56	4	<5	<2	4	25	.2	<2	<2	66	.45	.028	12	28	.58	161	.09	3	1.33	.03	.08	<2	5
10500 1150 K	1	37	9	106	<.3	23	13	637	4.00	<2	<5	<2	6	46	.5	<2	<2	102	.91	.068	33	48	1.15	349	.10	<3	2.68	.02	.14	<2	6
10500 1200 K	<1	17	7	65	<.3	16	11	371	3.41	3	<5	<2	6	27	<.2	2	<2	94	.33	.017	13	42	.89	128	.15	<3	2.25	.02	.08	<2	<2
10500 1250 K	<1	22	4	82	<.3	19	14	518	4.23	<2	<5	<2	9	37	<.2	<2	<2	126	.80	.044	19	60	1.65	265	.13	<3	2.88	.03	.13	<2	2
10500 1300 K	1	20	11	97	<.3	19	13	601	3.66	4	<5	<2	10	31	<.2	2	<2	96	.56	.031	17	40	.87	237	.15	3	1.83	.03	.20	<2	9
10500 1350 K	<1	19	5	90	<.3	19	16	856	4.54	<2	<5	<2	16	34	.2	<2	2	132	1.03	.081	27	64	1.50	270	.15	<3	2.19	.03	.20	<2	<2
10500 1400 K	1	14	6	86	<.3	16	12	523	4.21	<2	<5	<2	11	24	<.2	<2	2	102	.44	.033	16	40	.73	195	.11	<3	1.85	.02	.14	<2	<2
10500 1450 K	1	30	14	77	<.3	16	8	352	2.61	6	<5	<2	2	38	.2	<2	<2	65	.68	.044	11	34	.61	223	.09	<3	1.50	.02	.09	<2	<2
10500 1500 K	16	35	6	141	<.3	18	17	915	5.05	2	<5	<2	24	23	.3	3	<2	119	.58	.075	18	55	1.08	163	.12	<3	1.82	.02	.20	3	<2
10600 950 K	1	23	4	56	<.3	10	7	510	2.44	<2	<5	<2	2	53	.3	<2	<2	75	1.29	.096	27	24	.36	308	.07	3	1.22	.03	.06	<2	<2
10600 1050 K	<1	23	13	155	<.3	17	13	554	3.75	<2	<5	<2	7	31	.5	2	<2	97	.73	.030	17	41	1.10	282	.11	<3	1.97	.02	.19	<2	2
10600 1100 K	<1	26	3	44	<.3	7	3	167	.94	<2	<5	<2	<2	70	1.4	<2	<2	22	1.51	.063	14	10	.18	421	.03	3	.74	.03	.04	<2	<2
10600 1150 K	<1	24	14	134	<.3	17	13	567	3.98	2	<5	<2	8	28	<.2	<2	2	105	.61	.038	18	49	1.29	222	.15	<3	2.05	.02	.23	<2	2
10600 1250 K	1	21	5	64	<.3	14	8	382	2.72	2	<5	<2	4	30	<.2	2	3	70	.59	.030	14	33	.69	180	.11	<3	1.41	.02	.09	<2	2
10600 1300 K	1	31	<3	29	<.3	9	8	941	1.31	<2	<5	<2	<2	63	.5	<2	<2	30	1.20	.076	28	9	.16	301	.04	<3	.86	.04	.03	<2	<2
10600 1350 K	1	13	4	60	<.3	10	11	813	3.97	<2	<5	<2	4	39	<.2	<2	2	123	.96	.074	12	27	.52	221	.15	3	1.09	.03	.08	<2	4
10600 1400 K	2	36	8	75	<.3	18	11	517	3.25	2	<5	<2	5	47	<.2	<2	<2	88	.92	.058	23	42	.97	351	.12	<3	2.08	.02	.13	<2	7
10600 1450 K	2	30	6	61	<.3	14	11	539	2.94	2	<5	<2	4	36	<.2	<2	2	79	.67	.060	20	37	.81	263	.10	<3	1.63	.02	.09	<2	<2
10600 1500 K	9	39	9	73	<.3	17	12	542	3.77	2	<5	<2	14	27	<.2	3	<2	98	.58	.061	21	43	1.01	233	.15	<3	1.92	.02	.13	2	<2
10700 50 K	<1	17	5	31	<.3	8	4	174	1.98	2	<5	<2	<2	41	<.2	<2	2	35	1.18	.056	15	14	.25	214	.04	<3	.83	.04	.04	<2	2
10700 300 K	1	19	6	63	<.3	16	9	411	3.02	5	<5	<2	5	39	<.2	<2	<2	76	.88	.060	14	39	.84	198	.10	<3	1.78	.03	.08	<2	4
RE 10500 1200 K	<1	17	5	63	<.3	16	11	364	3.34	4	<5	<2	7	28	<.2	<2	<2	93	.33	.016	12	40	.89	128	.15	<3	2.21	.02	.07	<2	<2
10700 350 K	1	23	9	62	<.3	16	9	398	2.68	3	<5	<2	3	50	<.2	<2	<2	70	1.09	.062	18	40	.92	216	.09	3	1.94	.02	.08	<2	3
10700 400 K	<1	14	6	83	<.3	18	11	388	3.41	<2	<5	<2	6	29	<.2	<2	<2	90	.48	.019	10	50	1.26	130	.15	<3	2.61	.02	.16	<2	4
10700 600 K	1	11	8	64	<.3	10	10	421	3.18	2	<5	<2	5	23	<.2	<2	<2	93	.42	.033	10	37	.62	146	.07	<3	1.35	.02	.14	<2	2
10700 750 K	1	17	10	59	<.3	10	8	554	2.62	5	<5	<2	3	33	<.2	<2	<2	65	.69	.087	11	26	.46	257	.07	<3	1.35	.03	.05	<2	2
10700 800 K	<1	11	3	27	<.3	5	4	159	1.95	2	<5	<2	<2	23	<.2	<2	<2	67	.44	.068	6	8	.10	115	.10	<3	.52	.05	.03	<2	<2
10700 850 K	<1	27	3	45	<.3	8	5	261	1.76	2	<5	<2	<2	45	<.2	<2	<2	53	.92	.094	14	21	.33	268	.06	<3	1.19	.03	.04	<2	<2
10700 950 K	<1	15	9	86	<.3	13	8	250	2.86	<2	<5	<2	7	25	<.2	<2	<2	89	.56	.070	16	37	.93	211	.14	<3	1.97	.03	.16	<2	2
10700 1050 K	3	27	<3	113	<.3	11	40	4642	12.32	30	<5	<2	<2	62	<.2	<2	<2	128	1.43	.108	34	19	.20	551	.02	<3	1.04	.02	.03	<2	<2
10700 1100 K	1	25	13	108	<.3	11	8	446	2.59	3	<5	<2	3	44	1.0	<2	<2	70	.87	.061	20	25	.49	377	.09	<3	1.23	.03	.11	<2	<2
10700 1150 K	<1	17	21	113	<.3	10	7	387	2.55	4	<5	<2	7	32	.5	3	<2	62	.53	.037	17	25	.56	270	.09	<3	1.18	.02	.14	<2	<2
10700 1200 K	<1	11	<3	55	<.3	10	6	231	2.03	4	<5	<2	3	27	<.2	<2	<2	53	.52	.036	13	23	.47	136	.09	<3	1.09	.02	.07	<2	2
10700 1350 K	<1	13	3	28	<.3	4	3	174	1.43	<2	<5	<2	<2	38	<.2	<2	<2	44	.75	.058	12	7	.14	161	.06	<3	.48	.04	.03	<2	2
10700 1450 K	2	59	10	84	<.3	20	12	732	3.46	5	<5	<2	7	42	<.2	<2	<2	91	.69	.078	43	41	.89	397	.09	<3	2.58	.03	.14	<2	2
STANDARD C2/AU-S	20	57	33	133	6.0	69	34	1127	3.73	41	18	7	35	50	19.0	16	19	70	.55	.105	40	64	.96	192	.08	27	1.89	.06	.14	10	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au** ppb
10700 1500 K	2	26	3	69	<.3	19	14	556	3.73	3	<5	<2	11	30	<.2	<2	<2	99	.43	.032	22	44	1.15	262	.13	<3	2.94	.02	.12	<2	9
10800 50 K	1	23	<3	24	<.3	7	4	410	1.24	3	<5	<2	<2	66	<.2	<2	<2	38	1.84	.085	8	7	.16	175	.05	5	.55	.04	.03	<2	10
10800 100 K	<1	18	4	66	<.3	11	7	419	1.84	4	<5	<2	<2	65	.2	2	<2	48	1.68	.054	9	20	.49	201	.06	4	1.21	.03	.07	<2	<2
10800 150 K	1	23	<3	42	<.3	9	4	297	1.25	3	<5	<2	<2	79	<.2	2	<2	37	2.05	.066	5	9	.23	149	.05	6	.70	.03	.05	<2	<2
10800 200 K	1	27	4	43	<.3	10	4	579	.82	6	<5	<2	<2	92	.2	<2	<2	20	2.34	.069	5	9	.20	188	.03	6	.62	.04	.04	<2	<2
10800 250 K	<1	18	4	48	<.3	10	11	719	2.14	5	<5	<2	<2	52	<.2	2	2	58	1.16	.054	15	22	.46	179	.07	4	1.20	.03	.08	<2	<2
10800 300 K	<1	7	<3	13	<.3	3	2	120	.66	<2	<5	<2	<2	33	<.2	<2	<2	19	.63	.044	2	3	.68	49	.03	<3	.32	.05	.03	<2	2
10800 350 K	1	14	<3	53	<.3	11	6	236	2.15	6	<5	<2	<2	28	<.2	<2	<2	59	.44	.039	9	22	.48	140	.08	<3	1.26	.03	.09	<2	8
10800 400 K	1	33	6	70	<.3	31	16	403	3.48	10	<5	<2	5	23	.2	<2	<2	78	.28	.017	13	42	.92	183	.12	<3	3.18	.02	.11	<2	4
10800 450 K	1	14	9	47	<.3	8	6	261	1.67	6	<5	<2	2	27	<.2	3	<2	44	.46	.046	9	18	.37	126	.05	<3	1.01	.04	.07	<2	3
10800 500 K	<1	17	5	67	<.3	19	12	428	3.32	2	<5	<2	6	27	<.2	<2	<2	88	.51	.039	13	44	1.08	153	.16	<3	2.19	.03	.14	<2	3
10800 550 K	<1	18	34	138	<.3	18	13	648	3.65	2	<5	<2	9	27	.2	3	<2	97	.51	.036	18	45	1.15	163	.18	<3	1.96	.02	.17	<2	<2
10800 600 K	1	16	19	111	<.3	23	14	540	3.58	5	<5	<2	4	26	.2	2	<2	86	.41	.019	17	40	.80	197	.11	<3	2.30	.02	.13	<2	3
10800 650 K	1	16	66	407	<.3	27	23	1590	7.06	5	<5	<2	14	34	1.7	4	<2	155	.62	.059	25	64	.98	313	.05	<3	2.14	.02	.26	<2	3
10800 700 K	1	15	8	85	<.3	16	9	410	3.47	<2	<5	<2	6	21	.8	<2	2	96	.26	.031	12	36	.72	153	.17	<3	2.08	.02	.15	<2	13
10800 750 K	<1	12	11	78	<.3	11	9	233	3.35	4	<5	<2	7	24	<.2	2	3	82	.42	.054	21	36	.69	226	.08	<3	2.11	.02	.07	<2	6
10800 800 K	1	12	12	122	<.3	13	12	498	3.32	<2	<5	<2	6	27	.2	<2	<2	94	.50	.068	18	40	.92	255	.09	<3	2.43	.02	.22	<2	5
10800 850 K	1	12	15	90	<.3	12	8	224	2.68	5	<5	<2	5	27	.2	2	2	75	.47	.055	15	33	.79	200	.09	<3	2.15	.02	.10	<2	7
RE 10800 500 K	<1	16	6	61	<.3	18	11	396	3.09	<2	<5	<2	4	26	<.2	<2	<2	83	.48	.038	13	41	1.00	142	.15	<3	2.04	.03	.13	<2	<2
10800 900 K	1	10	10	78	<.3	9	8	296	3.12	<2	<5	<2	3	29	<.2	<2	<2	83	.46	.058	13	35	.64	173	.08	<3	1.58	.02	.06	<2	2
10800 1200 K	1	56	25	126	<.3	11	9	469	2.63	11	<5	<2	8	25	.8	12	5	55	.41	.022	19	18	.42	160	.07	<3	.94	.02	.11	<2	2
10800 1250 K	1	26	25	135	<.3	10	9	537	2.59	8	<5	<2	13	29	.9	6	<2	46	.43	.022	18	18	.47	174	.06	<3	1.11	.01	.12	<2	5
10800 1300 K	1	14	17	74	<.3	6	4	277	1.36	6	<5	<2	3	22	.3	<2	<2	26	.36	.021	9	15	.24	114	.03	<3	.61	.01	.07	<2	5
10800 1350 K	1	12	11	67	<.3	10	5	174	1.98	7	7	<2	3	24	.4	<2	<2	58	.36	.014	10	20	.33	138	.08	<3	1.11	.02	.09	<2	2
10800 1450 K	2	39	9	106	.4	21	13	566	3.76	5	<5	<2	8	40	<.2	<2	3	87	.61	.063	35	37	.85	430	.08	<3	2.98	.02	.18	<2	3
10800 1500 K	1	26	72	133	.4	17	11	470	2.69	5	<5	<2	4	37	.5	4	<2	56	.62	.054	25	31	.59	494	.06	<3	1.66	.02	.11	<2	5
STANDARD C2/AU-S	20	56	37	145	6.5	77	38	1193	4.11	43	20	8	37	54	22.2	17	23	74	.56	.100	41	67	1.02	214	.09	29	2.04	.06	.16	16	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.