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DATE PERFORMED: JUNE 15-JULY 30, 1993 DATE FILED: DEC 30, 1993

LOCATION: LAT.: 62°43'N AREA: CASINO AREA

LONG.: 138°56'W VALUE \$: 36,000

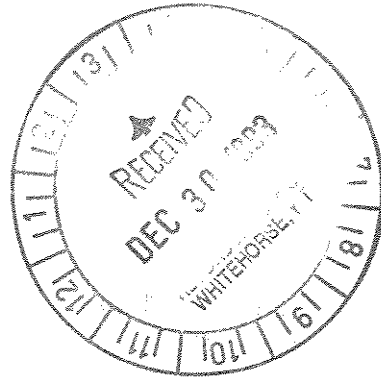
CLAIM NAME & NO.: AZTEC 1-12 (YB37540-551), AZTEC 17-28 (YB37557-567), AZTEC 33-52 (YB37572-91), MAYA 1-6 (YB37592-597), MAYA 11-16 (YB37602-606), MAYA 21-26 (YB37612-617), MAYA 31-36 (YB37622-627)

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WORK DONE FOR: EASTFIELD RESOURCES AND CANADIAN COMSTOCK

DATE TO GOOD STANDING:

REMARKS: ROAD BUILDING, GEOCHEM AND GEOPHYSICS.



Geological, Geochemical, Geophysical
Report
on the AZTEC Claims
for
Eastfield Resources Ltd.
and
Canadian Comstock Explorations Ltd.
by
Mincord Exploration Consultants Ltd.

093144

Dawson Range, Yukon Territory
NTS: 115J/10
Latitude: 62° 43'N
Longitude: 138° 56'W



October, 1993
Work undertaken: June 15-July 30, 1993

J. Chapman, P. Geo.
G. L. Garratt, P. Geo.

<u>Table of Contents</u>	<u>Page No.</u>
Summary	1
Introduction	1
Location, Access and Physiography	2
Property Status	3
History and Previous Work	3
Regional Geology	6
Property Geology	8
Alteration and Mineralization	11
Structure	13
Geochemical Survey	14
Geophysical Survey	15
Discussion	16
Conclusions and Recommendations	17
Recommended Work Program	18
Budget Proposal	19

List of Figures

1) Location Map (1:800,000)	Following page 2
2) Claim Map (1:50,000)	Following page 3
3) Regional Geology (1:250,000)	Following page 6

Attachments

1) Property Geology (1:5,000)
2a) Cu, Mo, Au Geochemistry (1:5,000)
2b) Pb, Zn, Ag, As Geochemistry (1:5,000)
3) Magnetism (1:5,000)
3a) Resistivity Plan (1:5,000)

Attachments Cont.

- 3b) Chargeability Plan (1:5,000)
- 3c) I.P. Pseudosections (1:10,000)

Appendices

- 1) Statement of Qualifications
- 2) Expenditure Statement
- 3) References
- 4) Certificates of Analyses
- 5) Rock Sample Descriptions
- 6) Geophysical Report, Scott Geophysics Ltd.

SUMMARY

The Aztec property, owned by Eastfield Resources Ltd. under option to Canadian Comstock Explorations Ltd. consists of 68 contiguous claims within the Whitehorse Mining District, Yukon Territory. The project area lies approximately 340 kilometers northwest of Whitehorse and 160 kilometers south of Dawson City. Fixed wing access is available from these centres to the Casino airstrip, located 6 kilometers northeast of the Aztec project. A four wheel drive access road now connects the Aztec property with the airstrip.

The Aztec project area adjoins to the west of the Casino property which hosts a copper-gold-molybdenum porphyry deposit currently being evaluated by Pacific Sentinel Gold Corp.

A field program consisting of road building, geological mapping, geochemical soil and rock sampling along with a ground magnetic and IP survey was initiated in mid June of this year and completed by the end of July.

INTRODUCTION

This report presents the results of the 1993 exploration program on the Aztec claims, Whitehorse Mining Division, Yukon Territory, and makes recommendations for further work.

Field work was carried out from mid June through the end of July by an eight man crew. A D-8 cat and operator were contracted to build an access road from the Casino airstrip to the camp location on the Ana property immediately north of the Aztec project area. This was to reduce dependence upon expensive air transportation for supplies. Ground geochemical and geophysical surveys and geologic mapping took place through June and July.

The exploration target is a copper-gold-molybdenum porphyry similar to the Casino deposit. At Casino, the mineralization is

hosted by Upper Cretaceous quartz monzonite intrusives and related breccias of the Casino complex, which invade the Cretaceous Dawson Range Batholith and earlier Proterozoic-Paleozoic Yukon Metamorphic Complex rocks along an east west trending belt.

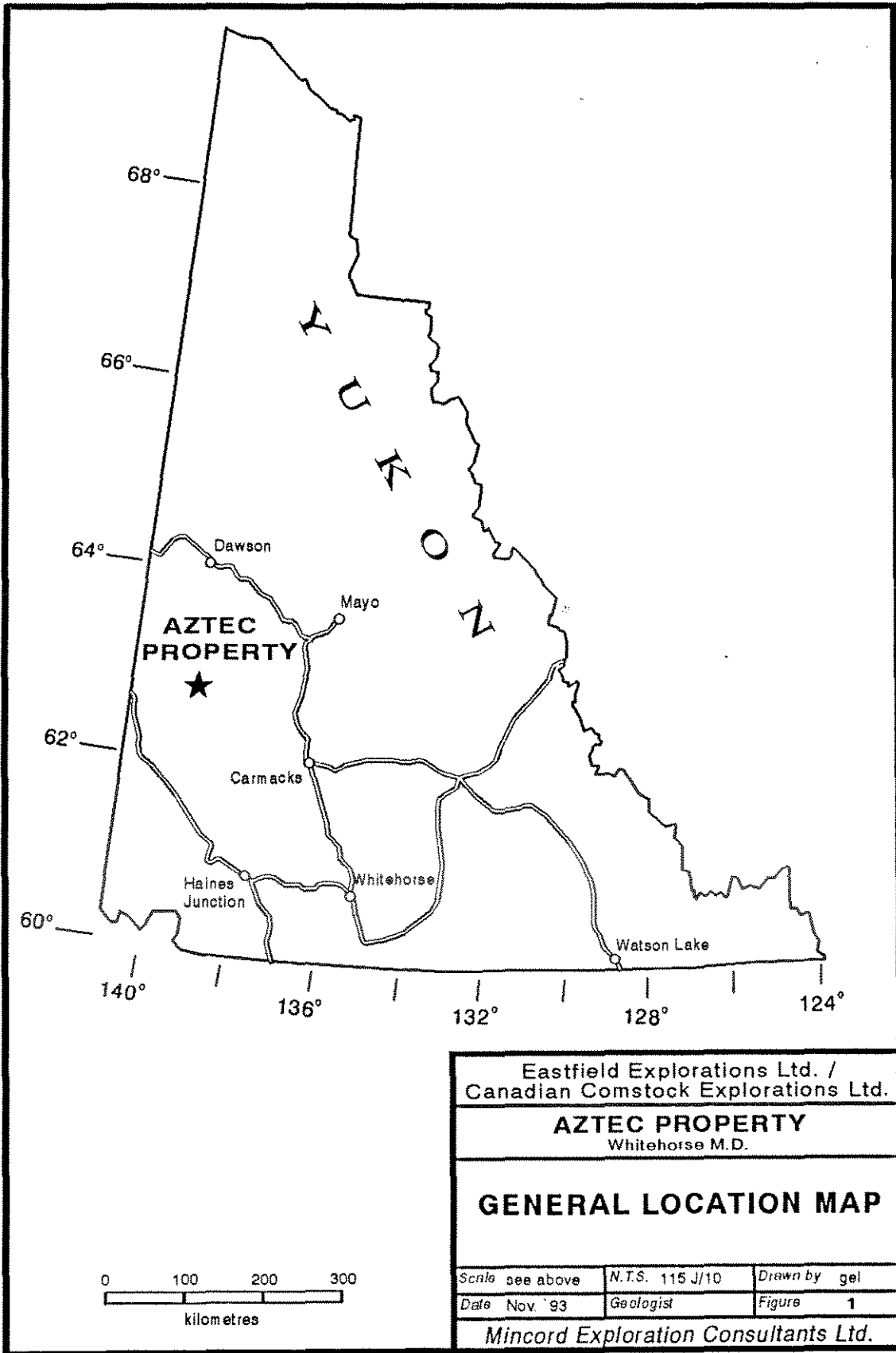
LOCATION, ACCESS AND PHYSIOGRAPHY

The Aztec property is located within the Dawson Range, in the west central portion of the Yukon Territory. It lies approximately 340 kilometers northwest of Whitehorse and 160 kilometers south of Dawson City on NTS map sheet 115J/10 centred at latitude 62° 43'N and Longitude 138° 56'W, (figure 1).

Access to the project area is possible by fixed wing aircraft from Whitehorse, Carmacks or Dawson City to the Casino airstrip approximately 6 kilometers northeast of the property. A 4-wheel drive road constructed during the 1993 field program connects the airstrip with the Aztec property. The majority of the claims lie above tree line and are predominantly moss covered, which makes large areas of the property accessible to 4-wheel drive ATV's. An old winter road traverses the west side of the property from north to south.

The project is located within the Dawson Range physiographic province. This unglaciated terrain consists of a northwest trending dissected plateau of dominantly low rounded hills with an average relief of approximately 300 meters. Vegetation consists of sparse isolated stands of trees in the valleys with mostly moss and low buck brush on the upper slopes. The majority of the claims lie above the 1,300 meter tree line.

Elevations on the Aztec property range from 950 meters in the drainages on the south and east sides to 1,510 meters on the main ridge through the northern portion of the property. Drainages on the Aztec property flow east and south.



Eastfield Explorations Ltd. / Canadian Comstock Explorations Ltd.		
AZTEC PROPERTY Whitehorse M.D.		
GENERAL LOCATION MAP		
Scale see above	N.T.S. 115 J/10	Drawn by gel
Date Nov. '93	Geologist	Figure 1
Mincord Exploration Consultants Ltd.		

PROPERTY STATUS

The Aztec property consists of 68 contiguous mineral claims in the Whitehorse Mining District. The claims are registered in the name of and are beneficially owned 100% by Eastfield Resources Ltd. Canadian Comstock Explorations Ltd. have an option to earn a 50% interest in the subject claims, (figure 2).

Pertinent claim data is as follows:

<u>Claim Names</u>	<u>Tag Numbers</u>	<u>Expiry Dates *</u>
Aztec 1 - 12	YB37540 - YB37551	Sept 21, 1998
Aztec 17 - 28	YB37557 - YB37567	Sept 21, 1998
Aztec 33 - 52	YB37572 - YB37591	Sept 21, 1998
Maya 1 - 6	YB37592 - YB37597	Sept 21, 1998
Maya 11 - 16	YB37602 - YB37606	Sept 21, 1998
Maya 21 - 26	YB37612 - YB37617	Sept 21, 1998
Maya 31 - 36	YB37622 - YB37627	Sept 21, 1998

*Based on acceptance of the 1993 work.

The total area covered by the claims is 1,421 hectares, or 3,468 acres.

The writer is not aware of any particular environmental, political, or regulatory problems that would adversely affect mineral exploration and development on the Ana property.

HISTORY AND PREVIOUS WORK

The Klondike gold rush of 1898 prompted the first prospecting in the area leading to the "Discovery" gold placer claim on Canadian Creek, 4.0 kilometers northeast of the subject claims, in 1911. From the 1930's to the 1960's, the area was actively explored for placer gold, silver-lead-zinc veins, and tungsten.

The porphyry potential of the region was recognized in 1967 with the discovery of the Casino mineralization, 2.5 kilometers southeast of the Canadian Creek placers.

Mineral occurrences in the area include:

CASINO DEPOSIT (see Figure 3)

This porphyry copper-gold-molybdenum deposit is hosted by the Upper Cretaceous Casino Complex consisting of quartz monzonite, feldspar porphyry and quartz/feldspar porphyry intrusives with related breccia pipes and dykes. A concentrically zoned hydrothermal alteration system is evident with a potassic core surrounded by phyllic, argillic and propylitic facies. Mineralization consisting primarily of chalcocite, chalcopyrite, pyrite and molybdenite occurs as disseminations and fracture fillings primarily in the outer regions of the potassic alteration zone.

Due to the unglaciated nature of the area and deep weathering, the deposit shows the leached cap, supergene enriched zone and hypogene mineralization typical of Arizona style porphyry deposits. Within the leached cap descending ground waters have remobilized the copper mineralization while the less mobile gold remained. This leached zone can be in excess of 170 meters thick. Underlying the leached cap the supergene zone forms an enriched blanket mineralized primarily with the copper sulphide chalcocite. Locally, the supergene zone is over 150 meters in thickness.

The lowermost hypogene zone contains pyrite, magnetite, chalcopyrite and molybdenite to depths of at least 750 meters with most holes ending in this mineralization.

To date, over 200 holes have been drilled to outline the deposit which has delineated a southern edge, however, the deposit remains open to the north, east and west. Preliminary reserve estimates published by Pacific Sentinel Gold Corp. indicate a high grade starter pit at the east end of the deposit which contains the following;

Starter Pit - Area Preliminary Reserve Estimate

	<u>Tonnes</u> <u>(Millions)</u>	<u>Cu</u> <u>%</u>	<u>Mo/S₂</u> <u>%</u>	<u>Au</u> <u>oz/ton</u>
Leached Cap	27	0.10	0.05	0.021
Supergene and Hypogene	99	0.40	0.05	0.014

A ten million dollar drilling program initiated in 1993 is expected to be completed by November of this year.

IDAHO CREEK

The Idaho Creek property, approximately 20 kilometers east of the Aztec project, consists of manganiferous gold bearing quartz veins within the granodiorite of the Dawson Range batholith. These veins contain pyrite, arsenopyrite, galena and sphalerite.

COCKFIELD (25 Kilometers to the southeast)

Hosted by intermediate volcanics of the Mt. Nansen suite and the Mt. Cockfield stock (believed to be Casino equivalent). Mineralization associated with the altered stock consists of disseminations and veinlets of pyrite, chalcopyrite, and molybdenite.

CASH (75 kilometers to the east-southeast)

A porphyry/vein/skarn prospect hosted by Mt. Nansen porphyry dykes and plugs, Yukon Metamorphic complex and Big Creek monzonite. Chip samples from trenches are reported to contain anomalous gold (79 to 253 ppb), copper (110 to 2300 ppm), and molybdenum (21 to 131 ppm).

MT. NANSEN (100 kilometers to the southeast)

An Arizona-style porphyry system hosted by a Tertiary porphyry complex intruding older quartz monzonite and quartz diorite.

Maximum copper grades encountered during 1970's drilling were reported in the 0.5% to 0.6% range.

ANA CLAIMS (adjoining to the north)

Casino style mineralization has been intersected in drilling of multi-element soil geochemical anomalies overlying Casino Complex intrusives. Values of up to 0.07% copper and 1928 ppb gold have been returned in core.

PREVIOUS WORK - AZTEC PROPERTY

1970:

Trans-Columbia Explorations Ltd. performed a soil geochemical survey over a large area west of the Casino deposit. Part of this survey included sampling over 70% of what is now the Aztec property.

1973 and 1987:

Regional mapping, which included the present Aztec property, was done by Tempelman-Kluit (1973) and Payne et al (1987).

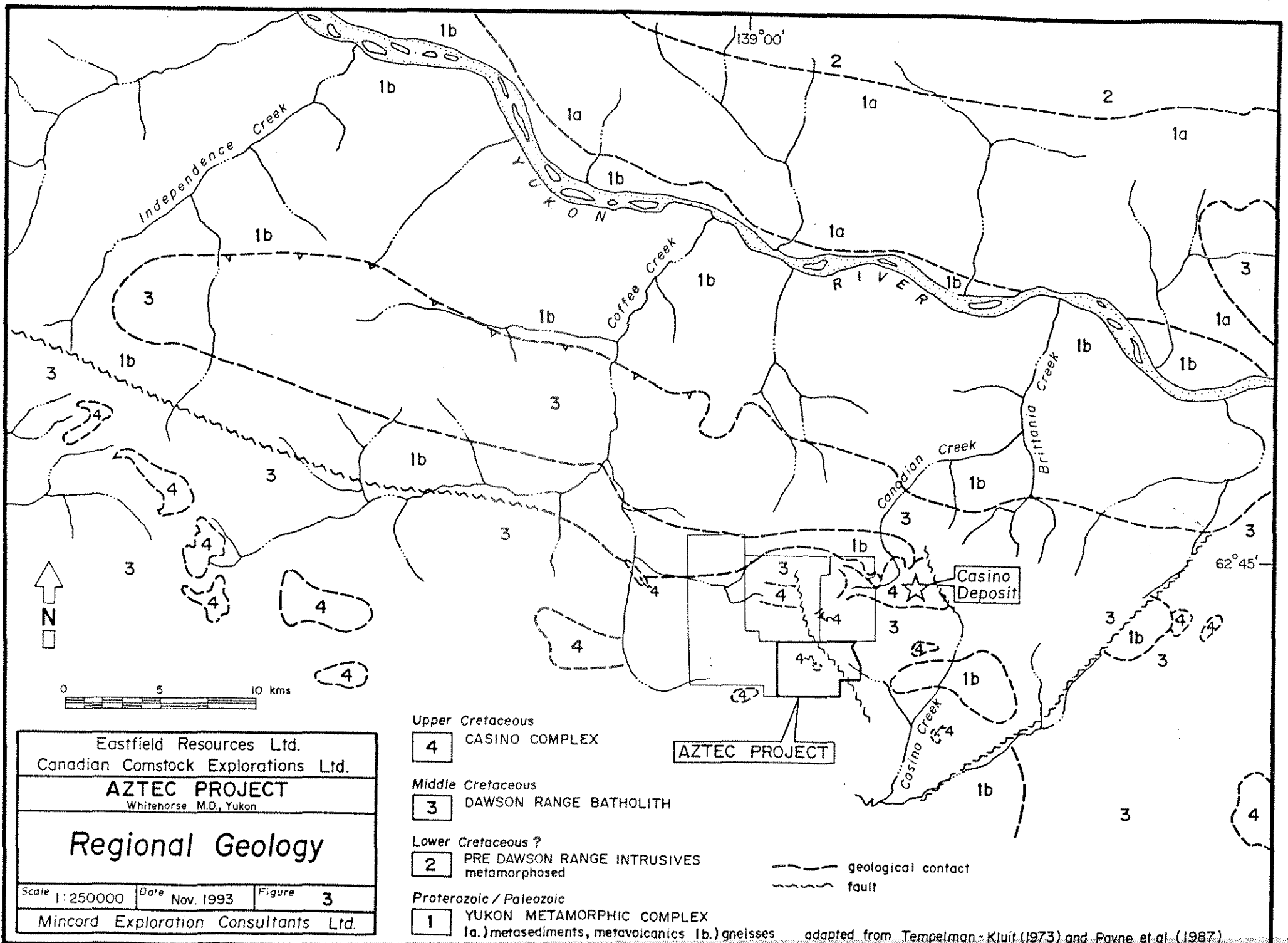
1992:

Renoble Holdings/Eastfield Resources staked the property as the Aztec claims.

Previous work has covered approximately 75% of the Aztec claim area however, no follow up work has been carried out on the geochemical anomalies generated. The southern and eastern boundaries of the claims have yet to be investigated.

REGIONAL GEOLOGY

The geology of the Casino and surrounding region is drawn from mapping by Tempelman-Kluit (1973), Payne et al (1987) and Eaton (1993), (figure 3). Payne is presently re-mapping the Casino property intrusive complex for Pacific Sentinel Gold Corp. and some lithologic and age relationships are expected to be



Eastfield Resources Ltd.
 Canadian Comstock Explorations Ltd.
AZTEC PROJECT
 Whitehorse M.D., Yukon
Regional Geology
 Scale 1:250000 Date Nov. 1993 Figure 3
 Mincord Exploration Consultants Ltd.

- Upper Cretaceous**
 4 CASINO COMPLEX
Middle Cretaceous
 3 DAWSON RANGE BATHOLITH
Lower Cretaceous ?
 2 PRE DAWSON RANGE INTRUSIVES metamorphosed
Proterozoic / Paleozoic
 1 YUKON METAMORPHIC COMPLEX
 1a.) metasediments, metavolcanics 1b.) gneisses

--- geological contact
 ~~~~~ fault

adapted from Tempelman-Kluit (1973) and Payne et al (1987)

clarified by this work. This summary will rely on the historical references listed.

The property lies within the Dawson Range Batholith near and along its northern boundary with the Yukon Metamorphic Complex. The main batholith/metamorphic complex contact lies five kilometers north of the property and the metamorphic rocks in the property area occur as an inlier or roof pendant, though a structural contact related to the Hoochekoo Fault is possible.

The Yukon Metamorphic Complex is a Proterozoic/Paleozoic package of metavolcanics and metasediments and gneisses (unit 1). In the area of Figure 3 unit 1 includes quartzites, quartz-feldspar-mica schist, amphibolite, augen gneiss and minor marble; unit 1 has been referred to, in part, as the Pelly Gneiss, described as strongly foliated to gneissic muscovite chlorite biotite granodiorite.

Unit 2 is composed of weakly metamorphosed and foliated intrusives of pre Dawson Range Batholith age. These are predominantly quartz diorites and granodiorites in the vicinity of the Aztec property. No firm age has been determined for these rocks.

The Dawson Range Batholith (unit 3) is a middle Cretaceous massive medium to coarse grained intrusion that Payne et al (1987) divided into three varieties: hornblende potassic quartz diorite; biotite-hornblende granodiorite and; biotite bearing leucocratic granodiorite to quartz monzonite.

The Casino Complex (unit 4) intrudes the Dawson Range Batholith and was believed to be upper Cretaceous in age. Recent evidence (Eaton, 1993) suggests that the Casino Complex may form a late stage of the Dawson Range Batholith. The Complex comprises several phases of intrusives, breccias and, in some areas, volcanic extrusives. At the Casino deposit the mapped units include: intrusive and intrusion breccias of dominantly quartz monzonite composition; feldspar porphyry (Patton Porphyry); fine grained quartz monzonite; inequigranular quartz monzonite

and; tuff and tuff breccia (Eaton, 1993). The breccia pipes at Casino are cone shaped with surface diameters of up to 500 meters. The Casino Complex hosts a large gold-copper-molybdenum deposit that is presently being explored by Pacific Sentinel Gold Corp.

The structural setting of the region is largely unresolved but Payne et al (1987) and Eaton (1993) both refer to a major west-northwest trending fault in the central part of Figure 3 that is an extension of the Hoochekoo and Big Creek Faults to the southeast. This fault forms the contact between the Dawson Range Batholith and the Yukon Metamorphic Complex a few kilometers north of the property and is believed to be a southwest dipping thrust. Parallel to this feature, a fault mapped by Tempelman-Kluit along the southern contact of the inlier of YMT might represent a related structure. If projected southeasterly this fault would trace through the series of Casino intrusions from the headwaters of Coffee Creek to Casino Creek. The Dip Creek Fault, in the southeastern part of Figure 3, is northeast trending and is described by Payne et al (1987) as showing little offset. Airphotos display a number of northeast trending lineaments in the vicinity of Casino and it is suspected that these represent a regionally extensive fault set.

#### PROPERTY GEOLOGY

Within the Aztec-Casino area the oldest rocks belong to the Proterozoic-Paleozoic Yukon Metamorphic Complex which has been intruded by the Cretaceous Dawson Range granodiorite batholith and slightly younger Casino Complex intrusives.

The Yukon Metamorphic Complex consists predominantly of quartzites, gneisses and minor diorite, usually as xenoliths. The quartzites are generally fine grained, pale grey to grey-brown or grey-green, are competent and often show a weak foliation. Quartz and feldspar grains account for approximately 90-95% of the rock in a generally siliceous but locally weakly calcareous matrix.

Gneisses range from felsic to mafic in composition and are very fine to fine grained. The finer grained felsic varieties are very similar to the foliated quartzites and appear to have gradational contacts. Within the gneissic zones the transition from felsic to mafic varieties can be gradational over a few centimeters or tens of centimeters. Mafic gneisses can be dark grey-green to almost black with up to 80% fine grained biotite. Generally the biotite is extensively altered to chlorite. Pyrite occurs as fine grained linear disseminations and locally composes up to 20% of the rock. Only occasional float fragments of this material have been observed on the Aztec property.

Diorite occurs as fine grained generally weakly foliated dark green fragments within breccias and occasionally the Dawson Range batholith.

Cretaceous granodiorite of the Dawson Range Batholith is the most abundant rock type exposed on the Aztec property. This generally occurs as a relatively fresh medium grained to coarse grained weakly magnetic rock containing 10-25% mafics. Biotite is the dominant mafic occurring as books up to 5 millimeters in size. Hornblende is less common but occurs as phenocrysts up to 1 centimeter long. The plagioclase/orthoclase ratio varies from 95/5 to 75/25. All exposures in the grid area are granodiorite with the exception of a latite dyke crossing lines 9200W and 8800W at 8200N.

The Casino Complex consists of quartz monzonite, a rhyodacitic/dacitic unit known as the Patton Porphyry and various breccias. These are generally quite recessive and consequently have very little exposure. Volumetrically the quartz monzonite is the most abundant rock type and best exposed. It occurs as a fine to coarse grained, equigranular to inequigranular pale to medium grey rock. The dominant form is a medium grained equigranular grey unit with less than 10% mafics, predominantly biotite.

Inequigranular quartz monzonite contains phenocrysts of quartz and/or potassium feldspar (<10%) up to 5 millimeters generally in a fine grained to medium grained matrix, which occasionally exhibits a graphic or myrmeketic texture.

On the Casino property the Patton Porphyry has been subdivided into an earlier and a later phase, with the earlier occurring predominantly as clasts within intrusion breccias and containing only plagioclase phenocrysts. The later Patton Porphyry forms dykes or plugs with generally sharp and in part chilled contacts. It has a rhyodacite to dacite composition with a dark very fine grained to aphanitic groundmass with predominantly plagioclase phenocrysts however quartz, potassium feldspar and biotite phenocrysts may also be present. Patton Porphyry float was observed just north of the property in the vicinity of L8400W.

Several distinctive breccia units appear to be both temporally and spatially associated with the Casino Complex intrusions. In the vicinity of the Casino deposit these are known as a micro or milled breccia, a homolithic intrusion breccia and a heterolithic intrusion breccia. Economically the micro breccia and the homolithic intrusion breccia are the most significant units.

The micro breccia is composed of a matrix of very fine granular quartz and feldspar with fragments of granodiorite, quartz monzonite and/or Patton Porphyry. The micro breccia varies from matrix supported with less than 20% fragments, to clast supported with less than 10% matrix. Triangular quartz fragments are distinctive of this unit, which can also contain locally up to 5% tourmaline as clusters of radiating crystals or black amorphous masses.

The homolithic intrusion breccia at Casino is essentially a brecciated quartz monzonite occurring within or on the edge of the quartz monzonite stocks. It consists of fragments of quartz monzonite, which are locally indistinct, in a fine to medium grained monzonite groundmass. Fragment size is generally less than 10 centimeters.

Heterolithic intrusion breccias appear to be related to the margins of the Casino Complex as a whole. Fragments consist of Dawson Range granodiorite and diorite, gneisses and quartzites of the Yukon Metamorphic Complex, and minor quartz monzonite and Patton Porphyry in a fine to coarse grained quartz monzonite groundmass. The range of fragment sizes is much larger than in the homolithic intrusion breccia, varying from a few centimeters to over 10 meters. Similarly the groundmass ranges from less than 10% to greater than 80%. No Casino Complex rocks have been observed on the property.

A breccia zone associated with a northeasterly trending structure was mapped on the Ana claims immediately north of the Aztec boundary in the vicinity of L8600W. This breccia is matrix supported with granodiorite/quartz monzonite clasts (extensively leached and altered) up to 10 centimeters, within a dark grey very fine grained vuggy quartz, tourmaline and rock flour groundmass. The high tourmaline content distinguishes this unit from the typical intrusive breccia. No exposures of this material have yet been located on the Aztec claims.

A Cretaceous/Tertiary latite and porphyritic latite have been documented on the Casino property an example of which is exposed around lines 9200W and 8800W at 8200N. They may reflect the waning stages of the Casino intrusions. These are typically pale creamy to brown, fine grained and locally contain quartz or plagioclase phenocrysts. An explosive/intrusive latite breccia occurs within the eastern portion of the Casino deposit, however it is barren of any mineralization.

#### ALTERATION AND MINERALIZATION

The alteration patterns that are associated with the Casino deposit are typical of an Arizona type porphyry deposit. This consists of a potassic altered core surrounded by phyllic, argillic and propylitic zones forming concentric rings. At Casino the copper-gold mineralization is primarily associated with the zone of potassic alteration.

Propylitic alteration is characterized by chlorite, epidote, calcite and clay development. This assemblage is present in the granodiorites throughout the grid area. Chlorite replaces the biotite and/or hornblende while epidote occurs as clasts and vein-like aggregates. The carbonate is generally pervasive but also occurs as hairline to 2 millimeter white veins.

Argillic alteration has not been observed to date on the property. Characteristically, argillically altered rocks have a bleached appearance due to the abundant clay they contain. Pyrite is the dominant sulphide mineral along with minor chlorite and carbonate. Montmorillonite and kaolinite are the characteristic clay minerals.

Phyllic alteration is characterized by intense texturally destructive sericite-quartz development, often containing 5-10% pyrite. In extreme cases the rock is essentially 100% sericite and quartz. These rocks are generally white to very pale coloured and may contain tourmaline, kaolinite, hematite, calcite or ankerite as accessory minerals. No phyllic alteration was observed.

A sericite-clay-chlorite alteration zone locally exists between the phyllic and potassic zones at Casino. In this environment rocks develop a pale green to off white coloration due to the alteration of plagioclase to a greasy pale green aggregate of sericite and clay, along with chlorite replacing the biotite and hornblende. Original textures are preserved during this process resulting in a distinctive appearance. Any pre-existing potassic assemblages are preserved. Minor components consist of magnetite, calcite and hematite with a pyrite to chalcopyrite ratio of <2:1.

Potassic alteration as it exists at the Casino deposit is notable for secondary potassium feldspar flooding and secondary biotite along with quartz, sericite, magnetite, hematite, gypsum and some ankerite. Minor accessory minerals include tourmaline, chlorite, epidote and anhydrite. The total sulphide content within the

potassic zone is generally low with the pyrite/chalcopyrite ratio normally <2:1. No widespread potassic alteration has yet been observed on the Aztec property.

Pyrite is the most abundant sulphide on the Aztec property and is believed to carry the gold values. Copper mineralization at Casino occurs as chalcocite, chalcopyrite, covellite and bornite with lesser malachite and azurite. Trace amounts of molybdenite, sphalerite arsenopyrite and galena have also been noted. Limonite is extensive in all rock types due to the deep weathering and lack of glaciation in the area.

Surface rock sampling produced no strongly anomalous results in any elements ranging from 1-22 ppb gold, 4-250 ppm copper, 2-9 ppm molybdenum and 2-16 ppm arsenic.

Only 7 rock samples were collected from the grid area as all available material was propylitically altered granodiorites. One sample 93-AZ-6 returned anomalous lead, zinc and silver values of 129 ppm, 301 ppm and 2.4 ppm respectively. Only traces of disseminated pyrite and limonite were noted in the sample.

#### STRUCTURE

Airphoto interpretation shows several property scale structural features on the Aztec claims.

A large north northeasterly structure which trends through the centre of the grid is a continuation of a structural zone on the Ana property to the north. On the Ana claims several breccia zones are associated with this structure. To date no breccias have been identified along the trace of this feature on the Aztec claims possibly due to the extensive overburden cover. At approximately L9400W/8600N the NNE structure intersects a 330° trending feature which extends on to the Koffee property.

Two east-west linears are evident on the airphotos. One of these lies close to the northern boundary of the claim block in the

headwaters at Aztec Creek, and the other crosses through the approximate centre of the grid. These features may be related to the larger scale structures which form the northern and southern limits to the Dawson Batholith.

A northerly trending structure traverses the western edge of the property. As most of the Aztec property is overburden covered no surface expression of any of these structures was located.

#### GEOCHEMICAL SURVEY

The soil geochemical survey was carried out on a north south oriented grid. Twenty line kilometers of grid were established with a nominal 400 meter line spacing and sample intervals of 75 meters. An east west trending base line, L9500N, was chained and flagged across the northern edge of the property and 2.5 kilometer lines run southward.

Samples were collected from the B horizon, where possible, generally between 15 and 30 centimeter in depth. Occasionally organic A horizon material was used if the B horizon could not be obtained. A total of 236 soil samples were collected and shipped to Pioneer Laboratories in Vancouver, BC for analysis by 30 element ICP with AA gold. This grid provided approximately 50% coverage of the Aztec claims.

Sample results for copper and gold were contoured and the results are shown on map 2a. Copper values contoured at the 40 ppm level outline an anomalous region approximately 1,200 meters east-west by 1,000 meters north-south on the west half of the grid. A maximum value of 106 ppm occurs at the edge of the anomaly which remains open to the west.

Gold forms spotty small anomalies when contoured at the 10 ppb level, with the exception of a 3 line anomaly in the northwest corner of the grid. A possibly more significant gold anomaly on L8400W at 9400N may be related to an occurrence of intrusive breccia immediately to the north on the Ana claims.

Molybdenum contoured at 10 ppm produced the largest and most continuous anomalies. Two main trends are outlined, an east-west zone at approximately 7500N across the entire grid and a northeast trending zone in the northwest corner of the grid. Values are highest in the latter anomaly with up to 73 ppm and it remains open to the north and west. No outcrop is present in this area, which lies in the headwaters of Aztec Creek, however two northerly to northwest trending airphoto linears are plotted through the anomalous area.

The southern anomaly has a very sharp and linear northern limit but shows large bulges on the southern edge which correspond to drainages. An east-west trending dyke or fault zone is postulated as a source for the molybdenum and down-slope dispersion creates the bulges.

Only two base metal anomalies of greater than a single station were defined, map 2b. These occur on lines 8800W and 9200W in the vicinity of a latite dyke. Lead and zinc reach maximum values of 39 ppm and 127 ppm respectively.

#### GEOPHYSICAL SURVEY

Scott Geophysics Ltd., of Vancouver, B.C., was contracted to complete Induced Polarization and Magnetic surveys over the Aztec grid. The I.P. survey was carried out on lines 8400W, 9200W, 10000W and 10800W; only a portion of line 10000W was completed due to strong magnetic storms. The magnetic survey was carried out on 400 meter spaced lines from line 8400W through line 10800W with line 10000W cut short due to magnetic storms.

The I.P. survey failed to outline any significant anomalies with the possible exception of a small, weak anomaly at the north end of lines 8400W and 9200W. Although these are weak anomalies, they do stand out from background and correspond with lower resistivity values, suggesting a sulphide source. Additionally, spotty but anomalous gold and molybdenum soil results were returned from this area and these may tie in with similar

geochemical responses in the vicinity of an intrusive breccia occurrence a few hundred meters north, on the Ana property. The broad, 800 meter, spacing of the surveyed lines does not preclude the possibility of locating significant anomalies between lines, though it is evident that a system as large as has been outlined to the north on the Ana and Koffee properties does not exist on the Aztec grid.

The magnetic survey also failed to identify any strong anomalies. A weak magnetic response was identified around 8500N on lines 10400W and 10800W, displaying an apparent westerly trend. This locale corresponds with a topographic high with substantial rock outcropping, possibly explaining the slightly elevated magnetic response. This site does show anomalous molybdenum and copper values in soils but these could not be explained by prospecting the area.

#### DISCUSSION

The 1993 exploration program on the Aztec, Ana and Koffee properties was successful in dramatically advancing the understanding and exploration potential of the area. Prior to this work it was believed that the Casino intrusive complex and related hydrothermal system was largely restricted to the Casino property. Exploration and development work on the Casino property has outlined a hydrothermal sulphide system at least six kilometers in length. Work on the Ana and Koffee properties indicates that this system extends a further six kilometers westward, outlining an overall area of twelve by two kilometers of Casino intrusive related hydrothermal activity. The immense size of this system compares favourably with the largest porphyry systems in North America. It is common for these large systems to host several mineral deposits.

The exploration to date on the Aztec property has not located any exposures of Casino Complex intrusives or breccias on the current grid. All outcrop is of Dawson batholith with the exception of a late latite dyke.

Geochemical soil sampling produced small spotty anomalies in all elements with the exception of the large copper and molybdenum anomalies. Copper centres on the west end of the ridge which trends through the middle of the property. As the area of the anomaly appears to be underlain by granodiorite its significance is reduced.

The linear molybdenum anomaly on the southern portion of the grid is most likely associated with a structural feature such as a fault zone or a dyke. A stronger molybdenum anomaly in the northwest corner of the grid however may be associated with Casino complex rocks as it is on the margin of the observed trend of these intrusives. No outcrop is available in this area.

The area around L8400W to 8800W at the north edge of the grid contains a gold anomaly which may be related to intrusive breccia noted several hundred meters north on the Ana grid. A complete absence of outcrop in this area means trenching will be required to determine the underlying geology. Weak chargeability anomalies were recorded at the north ends of lines 8400W and 9200W which correspond with the gold geochemistry.

#### CONCLUSIONS AND RECOMMENDATIONS

Results of the 1993 exploration program were generally poor with only weak geochemical and geophysical anomalies generated. The geology of the claim block appears to be predominantly Dawson Range batholith however most of the property has little or no outcrop exposure. Geochemical, geological and geophysical results indicate the following areas to be the most prospective.

1. Weak geophysical and geochemical anomalies at the north end of lines 8400W, 8800W and 9200W occur in an area of no outcrop however abundant intrusive breccia float occurs to the north at the Aztec-Ana property boundary. A major northeast trending structure, associated with a series of exposures of this intrusive breccia, extends through the Aztec property.

2. A strong molybdenum anomaly remains open to the north and west in the northwest corner of the grid. Highly anomalous values were returned in this area of no outcrop.
3. The northernmost portion of the property has not been sampled or surveyed and this now appears to be the most prospective terrain.

#### Recommended Work Program

No further work is recommended for the Aztec property at this time, however, based on the receipt of positive information from work programs on the adjoining Casino, Ana and Koffee properties, several areas may then warrant additional evaluations. These include;

1. The northernmost portion of the claims along the boundary with the Ana and Koffee claims should be soil sampled at 200 meter line spacing. The magnetic and I.P. surveys should be completed to the northern border at 400 meter line spacing.
2. The eastern third of the property received no work this year as efforts were directed at evaluating the previously reported copper and molybdenum anomalies. An expansion of the grid at 400 meter line spacings to the Casino boundary should be implemented.
3. Little is known about the southernmost portion of the property due to almost complete overburden cover.
4. Additional work such as trenching and drilling would be dependent upon the receipt of positive results in any of the above areas.

Budget Proposal

Note: Should this program be undertaken in concert with work on the ANA and KOFFEE properties, costs could be significantly reduced. Without this support, the trenching program might be considered as a separate entity.

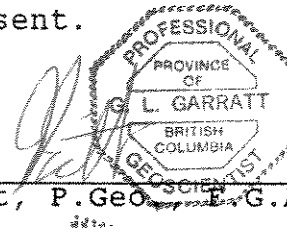
|                      |                         |                 |
|----------------------|-------------------------|-----------------|
| Personnel:           |                         |                 |
| Geologist            | 20 days @ \$350/day     | \$ 7,000.00     |
| 2 Samplers           | 20 days @ \$220/day     | 8,800.00        |
| Cook                 | 20 days @ \$220/day     | 4,400.00        |
| Supervision          | 5 days @ \$350/day      | 1,750.00        |
| Mob/Demob:           |                         | 7,000.00        |
| Communications:      |                         | 500.00          |
| Camp Costs:          | 20 days @ \$300/day     | 6,000.00        |
| Food:                | 25 days @ \$95/man/day  | 2,375.00        |
| Geophysics:          | 8 km @ \$1,500/km       | 12,000.00       |
| Bulldozer Trenching: | Mob/demob               | 20,000.00       |
|                      | 100 hrs @ \$180/hr      | 18,000.00       |
|                      | Fuel                    | 6,000.00        |
| Analyses:            | 120 soils @ \$12/sample | 1,440.00        |
|                      | 100 rocks @ \$15/sample | 1,500.00        |
| Freight:             |                         | 2,500.00        |
| Transportation:      | Commercial aircraft     | 5,000.00        |
|                      | Fixed wing - charter    | 8,000.00        |
| Report Prep:         |                         | <u>4,000.00</u> |
| Sub Total            |                         | \$116,265.00    |
| Contingency (5%)     |                         | <u>5,813.25</u> |
|                      | TOTAL                   | \$122,078.25    |

APPENDIX 1  
STATEMENT OF QUALIFICATIONS

Statement of Qualifications

I, Glen L. Garratt, of 110 - 325 Howe Street, in the City of Vancouver, British Columbia do hereby state that:

1. I am a practising geologist and have been since 1973 after completing the requirements for a B.Sc. (Geology) at the University of British Columbia.
2. I am a member in good standing of the Association of Professional Engineers, Geologists and Geophysicists of British Columbia and a Fellow of the Geological Association of Canada.
3. The work reported herein was carried out under my supervision.
4. I consent to the use of this report by Canadian Comstock Explorations Ltd. to fulfill the requirements of regulatory agencies. Excerpts or quotations or summaries from this report may only be used with my consent.



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G. L. Garratt, P. Geoscientist, G.A.C.

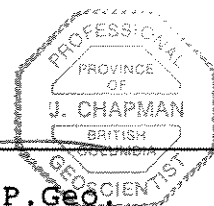
Dated at Vancouver, British Columbia, this 30th day of October, 1993

Statement of Qualifications

I, Jim Chapman, of Route 1, Box J-18, Bowen Island, British Columbia hereby certify:

1. I am a graduate of the University of British Columbia (1976) and hold a B.Sc. degree in geology.
2. I have been employed in my profession by various mining companies since graduation.
3. I am a Professional Geologist with the Association of Professional Engineers and Geoscientists of British Columbia.
4. The information contained in this report was obtained from on site supervision of the program described.
5. I have no interest, direct or indirect or in the securities of Canadian Comstock Explorations Ltd. or of the subject property.
6. I consent to and authorize the use of the attached report and my name in the Company's Prospectus, Statement of Material Facts or other public document.

  
\_\_\_\_\_  
Jim Chapman  
Consulting Geologist, P. Geo.



Dated at Vancouver, British Columbia this 29th day of October, 1993.

APPENDIX 2  
EXPENDITURE STATEMENT

EXPENDITURE STATEMENT  
 AZTEC PROPERTY  
 March 15 - October 22, 1993

PROFESSIONAL FEES:

|              |                        |             |
|--------------|------------------------|-------------|
| J. Chapman   | 19.88 days @ \$350/day | \$ 6,959.16 |
| G.L. Garratt | 6.67 days @ \$350/day  | 2,333.33    |
| J.W. Morton  | 5.66 days @ \$350/day  | 1,983.34    |

FIELD PERSONNEL FEES:

|             |                        |          |
|-------------|------------------------|----------|
| J. Campbell | 12.17 days @ \$220/day | 2,676.67 |
| S. Stannus  | 11.5 days @ \$220/day  | 2,530.73 |
| L. Horvat   | 15.33 days @ \$220/day | 3,373.33 |
| R. Bailey   | 9.83 days @ \$220/day  | 2,163.34 |
| N. Coopey   | 10.17 days @ \$220/day | 2,236.66 |

RENTALS:

|             |                           |          |
|-------------|---------------------------|----------|
| Vehicle     | 1.3 days @ \$60/day       | 80.00    |
| 3 ATVs      | 14.3 days @ \$60/day each | 2,574.00 |
| Camp        | 14.3 days @ \$175/day     | 2,502.50 |
| 6 Radios    | 14.3 days @ \$5/day each  | 429.00   |
| 3 Chainsaws | 14.3 days @ \$5/day each  | 214.50   |
| Genset      | 14.3 days @ \$500/month   | 233.34   |

TRANSPORTATION:

|                   |                         |          |
|-------------------|-------------------------|----------|
| Fixed Wing        | Charter                 | 3,322.04 |
| Helicopter        | 6.6 hours @ \$683.71/hr | 4,512.48 |
| Scheduled Flights |                         | 2,143.57 |
| Trailer           |                         | 547.17   |

TRAVEL EXPENSES:

837.21

FUEL:

4,120.89

FIELD EQUIPMENT:

1,751.02

SUB CONTRACTOR:

|               |                       |           |
|---------------|-----------------------|-----------|
| S. Main       | 2.33 days @ \$350/day | 816.67    |
| Road Building |                       | 13,478.09 |
| Expediting    |                       | 206.26    |
| Barge         |                       | 3,600.00  |
| Geophysical   |                       | 6,952.76  |

ANALYSES:

|      |                              |          |
|------|------------------------------|----------|
| Soil | 245 samples @ \$10.35/sample | 2,535.75 |
| Rock | 7 samples @ \$12.75/sample   | 89.25    |

SECRETARIAL:

|                     |       |
|---------------------|-------|
| 4 hours @ \$20/hour | 80.00 |
|---------------------|-------|

COMMUNICATION:

|                              |        |
|------------------------------|--------|
| Radio/Radio Telephone Rental | 263.93 |
| Telephone                    | 539.00 |
| Postage/courier              | 66.37  |

FREIGHT:

139.06

AZTEC EXPENDITURE STATEMENT  
Page 2

|                    |         |                 |
|--------------------|---------|-----------------|
| REPRODUCTION:      | Maps    | 2,705.50        |
|                    | Reports | 14.40           |
| DRAFTING:          |         | 250.00          |
| FOOD:              |         | 3,333.98        |
| MISCELLANEOUS:     |         | <u>48.43</u>    |
| SUB TOTAL:         |         | \$82,643.73     |
| GST on \$79,247.00 |         | <u>5,547.29</u> |
| TOTAL              |         | \$88,191.02     |

PROJECT PERSONNEL

|             |                                                    |            |
|-------------|----------------------------------------------------|------------|
| J. Chapman  | Box J-18<br>Bowen Island, BC V0N 1G0               | 19.88 days |
| G. Garratt  | 110 - 325 Howe Street<br>Vancouver, BC V6C 1Z7     | 6.67 days  |
| W. Morton   | 110 - 325 Howe Street<br>Vancouver, BC V6C 1Z7     | 5.66 days  |
| J. Campbell | 3965 Bear St.<br>Victoria, BC V8N 3P9              | 12.17 days |
| S. Stannus  | 9894 256th St. 16 days<br>Maple Ridge, BC V2X 8X7  | 11.5 days  |
| R. Bailey   | 4759 Mapleridge Dr.<br>North Vancouver, BC V7R 3T6 | 9.83 days  |
| N. Coopey   | 1 - 1315 Gladstone Ave.<br>Victoria, BC V8R 1R9    | 10.17 days |
| L. Horvat   | 202 - 1599 W. 71st Ave.<br>Vancouver, BC V6P 3C3   | 15.33 days |

SUB CONTRACTORS

|                               |                                                                           |              |
|-------------------------------|---------------------------------------------------------------------------|--------------|
| Scott Geophysics              | 4013 W. 14th Ave.<br>Vancouver, BC V6R 2X3                                | Al Scott     |
| 10983 Yukon Ltd.<br>Bulldozer | Box 4866<br>Whitehorse, YT Y1A 4N6                                        | Bruce Cairns |
| Pioneer Labs                  | 5 - 730 Eaton Way<br>Annacis Business Park<br>New Westminster, BC V3M 6J9 |              |
| Rat River<br>Expediting       | Box 5787<br>Whitehorse, YT Y1A 5L5                                        | Mary Fitton  |

APPENDIX 3

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APPENDIX 4  
CERTIFICATES OF ANALYSES

089-002

GEOCHEMICAL ANALYSIS CERTIFICATE

EASTFIELD RESOURCES LTD.

Multi-element ICP Analysis - .500 gram sample is digested with 3 ml of aqua regia, diluted to 10 ml with Water. This leach is partial for Mn, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K and Al. Detection Limit for Au is 3 ppm. \*Au Analysis- 10 gram sample is digested with aqua regia, MIBK extracted, graphite furnace AA finished to 1 ppb detection.

Analyst RCam  
Report No. 9310552  
Date: August 06, 1993

Project:  
Sample Type: Soils

| ELEMENT SAMPLE | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd  | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg   | Ba  | Ti  | B   | Al   | Na  | K   | W   | Au* |
|----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|-----|
|                | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | %    | %    | ppm | ppm | %    | ppm | %   | ppm | %    | %   | ppm | ppb |     |
| 8400W+7025N    | 1   | 25  | 10  | 80  | .1  | 11  | 11  | 420  | 3.67 | 2   | 5   | ND  | 5   | 45  | 1.1 | 2   | 2   | 88  | .80  | .038 | 9   | 21  | 1.07 | 167 | .24 | 3   | 2.09 | .03 | .22 | 1   | 4   |
| 8400W+7100N    | 1   | 21  | 8   | 66  | .1  | 15  | 12  | 372  | 3.96 | 5   | 5   | ND  | 10  | 33  | 1.3 | 2   | 2   | 86  | .58  | .051 | 16  | 30  | 1.05 | 201 | .22 | 2   | 2.52 | .02 | .23 | 1   | 2   |
| 8400W+7175N    | 1   | 18  | 9   | 80  | .1  | 18  | 10  | 392  | 3.46 | 6   | 5   | ND  | 5   | 33  | .4  | 2   | 2   | 76  | .49  | .038 | 9   | 30  | .91  | 188 | .19 | 2   | 2.41 | .02 | .16 | 1   | 1   |
| 8400W+7250N    | 1   | 23  | 6   | 64  | .1  | 17  | 9   | 410  | 2.93 | 5   | 5   | ND  | 3   | 49  | .2  | 2   | 2   | 61  | .72  | .046 | 20  | 28  | .69  | 218 | .12 | 3   | 2.20 | .02 | .09 | 1   | 1   |
| 8400W+7325N    | 1   | 17  | 9   | 69  | .1  | 14  | 10  | 419  | 3.30 | 4   | 5   | ND  | 5   | 36  | .2  | 2   | 2   | 72  | .59  | .058 | 12  | 26  | .90  | 162 | .18 | 2   | 2.22 | .02 | .18 | 1   | 2   |
| 8400W+7400N    | 1   | 25  | 11  | 64  | .1  | 20  | 13  | 330  | 3.58 | 6   | 5   | ND  | 5   | 31  | .2  | 2   | 2   | 75  | .43  | .051 | 14  | 34  | .91  | 180 | .16 | 2   | 2.94 | .01 | .11 | 1   | 1   |
| 8400W+7475N    | 1   | 25  | 10  | 58  | .1  | 18  | 10  | 300  | 3.12 | 6   | 5   | ND  | 7   | 34  | .3  | 2   | 2   | 73  | .51  | .054 | 18  | 31  | .88  | 196 | .18 | 2   | 2.54 | .02 | .13 | 1   | 118 |
| 8400W+7550N    | 1   | 26  | 11  | 62  | .1  | 16  | 12  | 380  | 3.45 | 5   | 5   | ND  | 8   | 31  | .5  | 2   | 2   | 73  | .48  | .059 | 15  | 31  | .95  | 179 | .21 | 2   | 2.64 | .02 | .22 | 1   | 2   |
| 8400W+7625N    | 1   | 29  | 14  | 64  | .1  | 20  | 12  | 500  | 3.50 | 5   | 5   | ND  | 9   | 38  | .7  | 2   | 2   | 72  | .62  | .060 | 20  | 34  | .90  | 223 | .21 | 2   | 2.36 | .02 | .20 | 1   | 2   |
| 8400W+7700N    | 1   | 28  | 9   | 57  | .1  | 18  | 10  | 308  | 3.03 | 5   | 5   | ND  | 6   | 33  | .2  | 2   | 2   | 62  | .51  | .059 | 16  | 31  | .86  | 179 | .18 | 2   | 2.30 | .02 | .11 | 1   | 1   |
| 8400W+7775N    | 9   | 24  | 7   | 60  | .1  | 17  | 10  | 617  | 2.78 | 4   | 5   | ND  | 3   | 40  | .2  | 2   | 2   | 59  | .58  | .052 | 14  | 29  | .64  | 192 | .14 | 2   | 1.90 | .02 | .13 | 1   | 1   |
| 8400W+7850N    | 11  | 23  | 10  | 60  | .1  | 16  | 9   | 391  | 2.84 | 6   | 5   | ND  | 2   | 26  | .2  | 2   | 2   | 61  | .36  | .054 | 11  | 25  | .68  | 124 | .14 | 2   | 2.02 | .02 | .08 | 2   | 1   |
| 8400W+7925N    | 6   | 17  | 5   | 91  | .1  | 13  | 9   | 671  | 1.81 | 2   | 5   | ND  | 2   | 87  | 1.3 | 2   | 2   | 40  | 1.28 | .057 | 5   | 16  | .31  | 284 | .08 | 2   | .98  | .02 | .09 | 1   | 1   |
| 8400W+8000N    | 10  | 23  | 10  | 59  | .1  | 17  | 10  | 387  | 3.15 | 6   | 5   | ND  | 6   | 29  | .5  | 2   | 2   | 65  | .39  | .043 | 13  | 28  | .63  | 110 | .16 | 3   | 2.05 | .02 | .09 | 4   | 1   |
| 8400W+8075N    | 9   | 27  | 12  | 74  | .1  | 20  | 11  | 567  | 3.51 | 9   | 5   | ND  | 13  | 37  | .5  | 2   | 2   | 64  | .58  | .057 | 22  | 34  | .73  | 148 | .17 | 3   | 1.95 | .02 | .08 | 1   | 4   |
| 8400W+8150N    | 15  | 21  | 12  | 68  | .1  | 20  | 12  | 896  | 3.29 | 7   | 5   | ND  | 11  | 37  | .2  | 2   | 2   | 62  | .58  | .062 | 18  | 32  | .65  | 169 | .14 | 2   | 2.05 | .02 | .08 | 1   | 2   |
| 8400W+8225N    | 11  | 19  | 12  | 59  | .1  | 17  | 8   | 223  | 2.21 | 4   | 5   | ND  | 8   | 33  | .2  | 2   | 2   | 48  | .50  | .044 | 17  | 29  | .60  | 156 | .14 | 2   | 1.95 | .02 | .06 | 1   | 1   |
| 8400W+8300N    | 29  | 17  | 11  | 66  | .1  | 16  | 11  | 986  | 3.06 | 7   | 5   | ND  | 6   | 38  | .2  | 2   | 2   | 55  | .57  | .063 | 18  | 27  | .56  | 165 | .10 | 2   | 1.77 | .02 | .08 | 1   | 23  |
| 8400W+8375N    | 20  | 19  | 14  | 70  | .1  | 17  | 20  | 1729 | 3.50 | 11  | 5   | ND  | 4   | 45  | .2  | 2   | 2   | 73  | .59  | .079 | 19  | 30  | .59  | 211 | .10 | 2   | 1.89 | .02 | .07 | 1   | 4   |
| 8400W+8525N    | 3   | 21  | 15  | 84  | .1  | 19  | 14  | 916  | 3.15 | 10  | 5   | ND  | 10  | 43  | .2  | 2   | 2   | 60  | .58  | .056 | 24  | 29  | .66  | 196 | .13 | 2   | 1.90 | .03 | .07 | 1   | 1   |
| 8400W+8600N    | 6   | 17  | 11  | 66  | .1  | 16  | 9   | 365  | 3.73 | 16  | 5   | ND  | 8   | 32  | .7  | 2   | 2   | 72  | .47  | .059 | 12  | 28  | .63  | 132 | .13 | 2   | 1.93 | .02 | .07 | 1   | 3   |
| 8400W+8675N    | 9   | 29  | 4   | 37  | .1  | 12  | 14  | 1820 | 2.08 | 3   | 7   | ND  | 2   | 81  | .2  | 2   | 2   | 35  | 1.67 | .116 | 24  | 17  | .34  | 192 | .04 | 3   | 1.00 | .02 | .05 | 1   | 1   |
| 8400W+8750N    | 4   | 16  | 9   | 66  | .1  | 16  | 10  | 574  | 2.77 | 3   | 5   | ND  | 7   | 40  | .2  | 2   | 2   | 56  | .68  | .062 | 12  | 31  | .77  | 164 | .14 | 2   | 2.03 | .02 | .07 | 1   | 2   |
| 8400W+8825N    | 6   | 18  | 13  | 74  | .1  | 15  | 9   | 304  | 2.98 | 7   | 5   | ND  | 6   | 32  | .2  | 2   | 2   | 70  | .55  | .061 | 13  | 30  | .81  | 144 | .16 | 2   | 1.93 | .02 | .13 | 1   | 1   |
| 8400W+8900N    | 4   | 16  | 10  | 55  | .1  | 12  | 7   | 291  | 2.96 | 6   | 5   | ND  | 5   | 20  | .2  | 2   | 2   | 70  | .27  | .021 | 7   | 24  | .54  | 52  | .14 | 3   | 1.53 | .02 | .07 | 1   | 1   |
| 8400W+8975N    | 4   | 22  | 9   | 82  | .1  | 15  | 10  | 414  | 3.21 | 9   | 5   | ND  | 5   | 37  | .2  | 2   | 2   | 64  | .58  | .056 | 18  | 26  | .77  | 230 | .13 | 3   | 1.99 | .02 | .10 | 11  | 2   |
| 8400W+9050N    | 5   | 13  | 16  | 75  | .1  | 13  | 9   | 487  | 2.91 | 13  | 5   | ND  | 6   | 37  | .3  | 2   | 2   | 62  | .48  | .035 | 15  | 22  | .57  | 235 | .11 | 2   | 1.92 | .02 | .08 | 1   | 3   |
| 8400W+9125N    | 5   | 16  | 17  | 74  | .1  | 13  | 9   | 512  | 2.43 | 13  | 5   | ND  | 8   | 51  | .2  | 2   | 2   | 51  | .62  | .045 | 20  | 23  | .47  | 234 | .11 | 2   | 1.68 | .02 | .08 | 1   | 3   |
| 8400W+9200N    | 6   | 27  | 18  | 85  | .6  | 17  | 16  | 2132 | 2.50 | 14  | 5   | ND  | 2   | 122 | .2  | 2   | 2   | 44  | 1.39 | .095 | 52  | 23  | .34  | 443 | .05 | 2   | 1.66 | .02 | .08 | 1   | 3   |
| 8400W+9275N    | 4   | 16  | 21  | 78  | .1  | 14  | 7   | 353  | 2.89 | 22  | 5   | ND  | 7   | 45  | .6  | 2   | 2   | 56  | .56  | .047 | 13  | 28  | .57  | 214 | .11 | 2   | 1.99 | .02 | .08 | 1   | 5   |

Aster = 133

Ana = 34

Koffee = 88

Nice = 22

| ELEMENT<br>SAMPLE       | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 8400W+9350N             | 4         | 13        | 22        | 79        | .1        | 14        | 7         | 242       | 2.77    | 17        | 5        | ND        | 5         | 36        | .2        | 2         | 2         | 58       | .47     | .051   | 10        | 29        | .59     | 128       | .12     | 2        | 1.96    | .02     | .07    | 1        | 88        |
| 8400W+9425N             | 5         | 21        | 19        | 93        | .1        | 15        | 11        | 1181      | 3.13    | 24        | 5        | ND        | 8         | 62        | .8        | 2         | 2         | 61       | .77     | .068   | 18        | 29        | .58     | 288       | .10     | 2        | 1.94    | .02     | .11    | 1        | 46        |
| 8400W+9500N             | 5         | 26        | 6         | 65        | .2        | 15        | 8         | 1837      | 1.15    | 7         | 5        | ND        | 2         | 120       | .2        | 2         | 2         | 17       | 1.52    | .110   | 29        | 15        | .13     | 404       | .02     | 4        | .78     | .02     | .05    | 1        | 2         |
| 8400W+10075N <i>Ala</i> | 17        | 20        | 60        | 167       | 1.0       | 15        | 9         | 606       | 3.27    | 95        | 5        | ND        | 8         | 36        | .2        | 3         | 2         | 55       | .51     | .053   | 30        | 27        | .55     | 222       | .07     | 2        | 2.00    | .02     | .07    | 1        | 31        |
| 8400W+10150N            | 11        | 29        | 39        | 128       | 1.0       | 17        | 10        | 957       | 3.14    | 61        | 7        | ND        | 3         | 64        | .2        | 3         | 2         | 56       | .85     | .082   | 33        | 29        | .55     | 355       | .06     | 2        | 2.12    | .02     | .09    | 1        | 2         |
| 8400W+10225N            | 7         | 24        | 25        | 104       | .7        | 14        | 5         | 233       | 2.06    | 25        | 5        | ND        | 2         | 66        | .2        | 2         | 2         | 39       | .82     | .092   | 23        | 20        | .21     | 282       | .04     | 2        | 1.34    | .02     | .06    | 1        | 1         |
| 8400W+10300N            | 28        | 24        | 49        | 131       | .5        | 18        | 10        | 1169      | 5.01    | 157       | 5        | ND        | 13        | 34        | .9        | 5         | 2         | 60       | .43     | .052   | 23        | 30        | .63     | 263       | .11     | 2        | 1.99    | .02     | .09    | 1        | 11        |
| 8400W+10375N            | 3         | 19        | 44        | 169       | .5        | 16        | 8         | 551       | 2.81    | 56        | 5        | ND        | 4         | 40        | .2        | 2         | 2         | 56       | .44     | .050   | 14        | 28        | .58     | 244       | .08     | 2        | 1.93    | .02     | .06    | 1        | 40        |
| 8400W+10450N            | 3         | 29        | 56        | 208       | .7        | 19        | 10        | 592       | 3.66    | 90        | 5        | ND        | 12        | 39        | .4        | 3         | 2         | 68       | .54     | .066   | 24        | 32        | .78     | 248       | .13     | 2        | 2.16    | .01     | .09    | 1        | 12        |
| 8400W+10525N            | 2         | 30        | 84        | 191       | .4        | 16        | 11        | 944       | 3.13    | 174       | 5        | ND        | 2         | 53        | .2        | 2         | 2         | 63       | .62     | .098   | 14        | 28        | .55     | 295       | .06     | 2        | 1.71    | .02     | .07    | 1        | 5         |
| 8400W+10600N            | 3         | 46        | 110       | 269       | 3.5       | 17        | 6         | 226       | 3.62    | 275       | 5        | ND        | 2         | 43        | .2        | 4         | 2         | 58       | .51     | .109   | 46        | 30        | .60     | 256       | .04     | 2        | 2.53    | .02     | .07    | 1        | 4         |
| 8400W+10675N            | 1         | 24        | 46        | 181       | .1        | 15        | 12        | 865       | 3.70    | 57        | 5        | ND        | 11        | 39        | .5        | 2         | 2         | 67       | .45     | .060   | 19        | 25        | .86     | 254       | .10     | 2        | 2.17    | .01     | .09    | 1        | 6         |
| 8400W+10750N            | 1         | 20        | 19        | 107       | .1        | 12        | 8         | 286       | 2.71    | 16        | 5        | ND        | 9         | 36        | .2        | 2         | 2         | 58       | .45     | .039   | 15        | 22        | .72     | 236       | .12     | 2        | 1.76    | .01     | .08    | 1        | 11        |
| 8400W+10825N            | 1         | 26        | 20        | 87        | .2        | 11        | 9         | 876       | 2.78    | 21        | 5        | ND        | 2         | 48        | .2        | 2         | 2         | 56       | .56     | .065   | 22        | 20        | .56     | 337       | .07     | 2        | 1.88    | .02     | .07    | 1        | 6         |
| 8400W+10900N            | 2         | 30        | 18        | 111       | .3        | 14        | 10        | 520       | 3.75    | 46        | 5        | ND        | 2         | 37        | .2        | 2         | 2         | 71       | .39     | .062   | 22        | 26        | .85     | 316       | .06     | 2        | 2.71    | .01     | .06    | 2        | 3         |
| 8400W+10975N            | 2         | 26        | 12        | 82        | .2        | 15        | 8         | 405       | 3.23    | 36        | 5        | ND        | 2         | 36        | .2        | 2         | 2         | 64       | .41     | .059   | 13        | 27        | .74     | 276       | .08     | 2        | 2.27    | .01     | .06    | 1        | 33        |
| 8400W+11050N            | 2         | 31        | 27        | 100       | .4        | 13        | 10        | 345       | 3.89    | 71        | 5        | ND        | 9         | 49        | .2        | 2         | 2         | 76       | .65     | .060   | 41        | 23        | .93     | 378       | .12     | 2        | 2.68    | .02     | .10    | 1        | 12        |
| 8400W+11125N            | 4         | 24        | 14        | 75        | .1        | 15        | 12        | 683       | 3.57    | 15        | 5        | ND        | 2         | 45        | .2        | 2         | 2         | 72       | .50     | .055   | 17        | 28        | .78     | 308       | .09     | 2        | 2.36    | .02     | .06    | 1        | 2         |
| 8400W+11200N            | 3         | 25        | 10        | 79        | .2        | 15        | 9         | 409       | 3.53    | 11        | 5        | ND        | 3         | 39        | .2        | 2         | 2         | 72       | .44     | .044   | 18        | 25        | .88     | 309       | .09     | 2        | 2.45    | .01     | .06    | 1        | 57        |
| 8400W+11275N            | 5         | 27        | 18        | 91        | .1        | 9         | 13        | 1053      | 3.29    | 30        | 10       | ND        | 2         | 56        | .2        | 2         | 2         | 56       | .67     | .102   | 40        | 18        | .58     | 350       | .03     | 2        | 2.07    | .01     | .07    | 1        | 21        |
| 8400W+11350N            | 4         | 27        | 9         | 64        | .1        | 17        | 9         | 379       | 3.26    | 11        | 5        | ND        | 3         | 37        | .2        | 2         | 2         | 65       | .42     | .055   | 16        | 28        | .87     | 256       | .08     | 2        | 2.42    | .01     | .07    | 1        | 14        |
| 8400W+11425N            | 10        | 40        | 13        | 93        | .1        | 18        | 14        | 1288      | 4.03    | 15        | 5        | ND        | 2         | 41        | .2        | 2         | 2         | 79       | .48     | .117   | 13        | 31        | .72     | 246       | .03     | 2        | 2.24    | .01     | .06    | 1        | 18        |
| 8400W+11500N            | 8         | 55        | 8         | 64        | .1        | 15        | 9         | 362       | 3.28    | 16        | 5        | ND        | 3         | 25        | .2        | 2         | 2         | 59       | .33     | .039   | 17        | 24        | .71     | 176       | .05     | 2        | 2.26    | .01     | .06    | 1        | 17        |
| 8400W+11575N            | 4         | 46        | 10        | 71        | .1        | 18        | 8         | 321       | 2.50    | 7         | 5        | ND        | 2         | 35        | .2        | 2         | 2         | 54       | .51     | .070   | 18        | 28        | .70     | 182       | .08     | 2        | 1.83    | .02     | .06    | 1        | 23        |
| 8400W+11650N            | 6         | 88        | 16        | 69        | .1        | 20        | 11        | 464       | 3.30    | 23        | 5        | ND        | 3         | 28        | .2        | 2         | 2         | 60       | .33     | .052   | 19        | 28        | .75     | 141       | .06     | 2        | 2.36    | .01     | .07    | 1        | 14        |
| 8400W+11725N            | 2         | 61        | 11        | 61        | .1        | 20        | 10        | 477       | 3.44    | 14        | 5        | ND        | 5         | 44        | .2        | 2         | 2         | 68       | .49     | .046   | 22        | 26        | .89     | 153       | .07     | 2        | 2.24    | .02     | .07    | 1        | 16        |
| 8400W+11800N            | 2         | 44        | 9         | 61        | .1        | 20        | 11        | 508       | 3.39    | 13        | 5        | ND        | 3         | 24        | .3        | 2         | 2         | 66       | .24     | .071   | 16        | 31        | .77     | 122       | .08     | 2        | 2.75    | .01     | .07    | 3        | 7         |
| 8400W+11875N            | 6         | 77        | 19        | 89        | .2        | 28        | 14        | 628       | 3.73    | 28        | 5        | ND        | 4         | 53        | .2        | 2         | 2         | 69       | .76     | .064   | 24        | 53        | 1.44    | 188       | .06     | 2        | 2.62    | .03     | .13    | 1        | 10        |
| 8400W+11950N            | 5         | 68        | 16        | 78        | .3        | 23        | 11        | 647       | 3.01    | 28        | 5        | ND        | 2         | 49        | .2        | 2         | 2         | 56       | .96     | .083   | 24        | 37        | .69     | 180       | .05     | 2        | 2.01    | .02     | .08    | 1        | 11        |
| 8400W+12025N            | 3         | 53        | 10        | 70        | .1        | 36        | 12        | 423       | 3.47    | 20        | 5        | ND        | 7         | 38        | .2        | 2         | 2         | 72       | .54     | .063   | 21        | 66        | 1.36    | 225       | .12     | 2        | 2.41    | .02     | .15    | 1        | 11        |
| 8400W+12100N            | 4         | 58        | 23        | 120       | .9        | 35        | 11        | 372       | 3.39    | 68        | 5        | ND        | 2         | 31        | .2        | 2         | 2         | 74       | .33     | .093   | 24        | 44        | .78     | 235       | .04     | 2        | 2.51    | .01     | .08    | 1        | 7         |
| 8400W+12175N            | 3         | 49        | 51        | 135       | .3        | 31        | 10        | 489       | 3.29    | 64        | 5        | ND        | 2         | 26        | .3        | 2         | 2         | 72       | .31     | .078   | 16        | 38        | .64     | 267       | .07     | 2        | 1.68    | .01     | .07    | 1        | 3         |
| 8400W+12250N            | 3         | 59        | 67        | 173       | .9        | 30        | 11        | 371       | 2.65    | 82        | 5        | ND        | 2         | 37        | .2        | 2         | 2         | 62       | .46     | .080   | 27        | 37        | .64     | 299       | .04     | 2        | 2.05    | .01     | .07    | 1        | 3         |
| 8400W+12325N            | 4         | 53        | 57        | 157       | 1.3       | 22        | 11        | 712       | 3.26    | 118       | 5        | ND        | 2         | 59        | .2        | 2         | 2         | 58       | .89     | .095   | 39        | 31        | .56     | 274       | .04     | 2        | 2.12    | .01     | .08    | 1        | 1         |
| 8400W+12400N            | 2         | 20        | 57        | 236       | .4        | 13        | 8         | 1137      | 2.65    | 121       | 5        | ND        | 2         | 45        | .9        | 2         | 2         | 32       | .71     | .079   | 40        | 17        | .21     | 179       | .02     | 2        | 1.18    | .01     | .08    | 1        | 1         |

| ELEMENT<br>SAMPLE | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 8400W+12475N      | 2         | 34        | 57        | 128       | .7        | 24        | 8         | 261       | 2.84    | 162       | 5        | ND        | 2         | 29        | .2        | 5         | 2         | 57       | .33     | .070   | 19        | 36        | .67     | 248       | .05     | 2        | 2.15    | .01     | .07    | 1        | 10        |
| 8400W+12550N A    | 1         | 26        | 11        | 81        | .1        | 20        | 10        | 505       | 2.98    | 191       | 5        | ND        | 3         | 29        | .2        | 2         | 2         | 56       | .35     | .058   | 17        | 30        | .70     | 137       | .12     | 2        | 2.08    | .01     | .09    | 5        | 4         |
| 9200W+7025N AZ    | 2         | 21        | 8         | 64        | .1        | 17        | 10        | 452       | 2.80    | 8         | 5        | ND        | 2         | 41        | .2        | 2         | 2         | 59       | .52     | .056   | 20        | 29        | .68     | 200       | .10     | 2        | 2.23    | .02     | .07    | 1        | 1         |
| 9200W+7100N       | 3         | 22        | 9         | 68        | .1        | 18        | 9         | 332       | 2.72    | 6         | 5        | ND        | 2         | 35        | .2        | 2         | 2         | 58       | .47     | .051   | 10        | 30        | .69     | 183       | .12     | 2        | 2.19    | .02     | .07    | 1        | 1         |
| 9200W+7175N       | 3         | 20        | 8         | 60        | .1        | 18        | 10        | 366       | 2.78    | 8         | 5        | ND        | 3         | 32        | .2        | 2         | 2         | 61       | .42     | .045   | 11        | 28        | .68     | 161       | .12     | 2        | 2.10    | .02     | .07    | 1        | 1         |
| 9200W+7250N       | 6         | 23        | 7         | 74        | .2        | 18        | 11        | 447       | 3.03    | 6         | 5        | ND        | 4         | 43        | .2        | 2         | 2         | 65       | .65     | .055   | 13        | 29        | .87     | 179       | .13     | 2        | 2.36    | .02     | .09    | 1        | 1         |
| 9200W+7325N       | 14        | 30        | 6         | 86        | .2        | 17        | 13        | 675       | 3.45    | 2         | 5        | ND        | 5         | 52        | .2        | 2         | 2         | 75       | .75     | .054   | 20        | 30        | .96     | 245       | .16     | 2        | 2.98    | .03     | .16    | 1        | 4         |
| 9200W+7400N       | 12        | 28        | 5         | 74        | .1        | 14        | 11        | 409       | 3.39    | 5         | 5        | ND        | 7         | 44        | .2        | 2         | 2         | 74       | .71     | .049   | 21        | 25        | .94     | 234       | .16     | 2        | 2.76    | .03     | .18    | 1        | 2         |
| 9200W+7475N       | 9         | 32        | 6         | 80        | .1        | 17        | 11        | 474       | 3.33    | 5         | 5        | ND        | 4         | 47        | .2        | 2         | 2         | 70       | .68     | .051   | 20        | 29        | .92     | 229       | .15     | 2        | 3.11    | .02     | .12    | 3        | 1         |
| 9200W+7550N       | 12        | 29        | 8         | 75        | .1        | 16        | 11        | 548       | 3.60    | 2         | 5        | ND        | 5         | 49        | .2        | 2         | 2         | 73       | .73     | .048   | 15        | 29        | .91     | 187       | .12     | 2        | 2.58    | .02     | .10    | 1        | 1         |
| 9200W+7625N       | 14        | 28        | 7         | 67        | .1        | 16        | 12        | 631       | 3.69    | 3         | 5        | ND        | 7         | 36        | .2        | 2         | 2         | 72       | .59     | .053   | 15        | 29        | .83     | 189       | .11     | 2        | 2.27    | .02     | .13    | 1        | 1         |
| 9200W+7700N       | 12        | 26        | 10        | 75        | .1        | 14        | 13        | 750       | 3.29    | 5         | 5        | ND        | 6         | 42        | .2        | 2         | 2         | 70       | .64     | .051   | 18        | 27        | .87     | 214       | .14     | 2        | 2.61    | .02     | .13    | 1        | 3         |
| 9200W+7775N       | 16        | 42        | 8         | 71        | .2        | 16        | 11        | 512       | 3.22    | 4         | 5        | ND        | 3         | 56        | .2        | 2         | 2         | 69       | .85     | .063   | 27        | 29        | .78     | 245       | .12     | 2        | 2.66    | .03     | .08    | 1        | 2         |
| 9200W+7850N       | 12        | 25        | 6         | 60        | .1        | 17        | 12        | 510       | 2.92    | 3         | 5        | ND        | 3         | 54        | .2        | 2         | 2         | 63       | .77     | .061   | 16        | 29        | .71     | 194       | .14     | 2        | 2.17    | .03     | .07    | 1        | 1         |
| 9200W+7925N       | 18        | 50        | 7         | 76        | .2        | 25        | 12        | 364       | 3.07    | 3         | 9        | ND        | 2         | 63        | .2        | 2         | 2         | 72       | 1.00    | .073   | 26        | 36        | .87     | 265       | .11     | 2        | 3.29    | .03     | .08    | 1        | 2         |
| 9200W+8000N       | 7         | 62        | 10        | 72        | .2        | 24        | 10        | 342       | 3.02    | 3         | 5        | ND        | 4         | 55        | .2        | 2         | 2         | 68       | .85     | .069   | 27        | 35        | .91     | 261       | .13     | 2        | 3.08    | .03     | .07    | 1        | 2         |
| 9200W+8075N       | 4         | 37        | 7         | 75        | .1        | 20        | 11        | 396       | 3.39    | 5         | 5        | ND        | 6         | 41        | .2        | 2         | 2         | 75       | .62     | .065   | 16        | 32        | .94     | 171       | .19     | 2        | 2.51    | .03     | .14    | 1        | 9         |
| 9200W+8150N       | 8         | 28        | 12        | 82        | .1        | 20        | 10        | 1167      | 4.60    | 10        | 5        | ND        | 2         | 31        | .2        | 3         | 2         | 107      | .31     | .043   | 10        | 33        | .65     | 129       | .16     | 2        | 2.03    | .01     | .07    | 1        | 1         |
| 9200W+8225N       | 1         | 26        | 9         | 68        | .1        | 23        | 15        | 561       | 3.63    | 5         | 5        | ND        | 7         | 27        | .2        | 2         | 2         | 69       | .40     | .052   | 19        | 33        | .98     | 151       | .09     | 2        | 3.14    | .01     | .07    | 1        | 3         |
| 9200W+8300N       | 4         | 37        | 16        | 54        | .6        | 22        | 10        | 544       | 3.64    | 9         | 5        | ND        | 3         | 33        | .2        | 2         | 2         | 58       | .50     | .093   | 44        | 31        | .63     | 212       | .04     | 2        | 2.66    | .01     | .08    | 1        | 1         |
| 9200W+8375N       | 3         | 20        | 15        | 53        | .1        | 16        | 7         | 233       | 4.05    | 9         | 5        | ND        | 3         | 17        | .2        | 2         | 2         | 84       | .16     | .026   | 11        | 32        | .37     | 72        | .10     | 2        | 2.45    | .01     | .05    | 1        | 1         |
| 9200W+8450N       | 3         | 25        | 12        | 83        | .1        | 24        | 13        | 520       | 4.20    | 11        | 5        | ND        | 5         | 20        | .2        | 2         | 2         | 80       | .19     | .045   | 14        | 36        | .59     | 85        | .10     | 2        | 3.02    | .01     | .06    | 3        | 1         |
| 9200W+8525N       | 14        | 29        | 21        | 100       | .1        | 26        | 13        | 655       | 3.59    | 8         | 5        | ND        | 4         | 43        | .2        | 2         | 2         | 65       | .85     | .092   | 89        | 40        | .71     | 217       | .08     | 2        | 2.79    | .02     | .08    | 1        | 4         |
| 9200W+8600N       | 9         | 21        | 9         | 78        | .1        | 23        | 13        | 964       | 3.22    | 12        | 5        | ND        | 4         | 35        | .2        | 2         | 2         | 63       | .60     | .066   | 27        | 37        | .77     | 191       | .11     | 2        | 2.30    | .02     | .07    | 1        | 3         |
| 9200W+8675N       | 9         | 21        | 11        | 79        | .1        | 21        | 12        | 394       | 3.66    | 8         | 5        | ND        | 2         | 42        | .2        | 2         | 2         | 62       | .79     | .086   | 23        | 35        | .73     | 200       | .08     | 2        | 2.43    | .02     | .07    | 1        | 1         |
| 9200W+8750N       | 5         | 18        | 13        | 89        | .1        | 18        | 11        | 360       | 3.19    | 6         | 5        | ND        | 6         | 34        | .3        | 2         | 2         | 67       | .57     | .051   | 12        | 31        | .97     | 166       | .14     | 2        | 2.47    | .02     | .06    | 1        | 1         |
| 9200W+8825N       | 5         | 19        | 10        | 87        | .1        | 14        | 12        | 655       | 3.51    | 5         | 5        | ND        | 9         | 33        | .2        | 2         | 2         | 72       | .61     | .064   | 19        | 27        | .97     | 130       | .15     | 2        | 2.37    | .02     | .11    | 4        | 1         |
| 9200W+8900N       | 7         | 28        | 9         | 107       | .1        | 18        | 14        | 948       | 3.89    | 5         | 5        | ND        | 6         | 60        | .2        | 2         | 2         | 78       | 1.00    | .067   | 34        | 34        | .99     | 243       | .14     | 2        | 3.11    | .02     | .10    | 2        | 5         |
| 9200W+8975N       | 4         | 23        | 7         | 102       | .1        | 15        | 10        | 517       | 2.94    | 6         | 5        | ND        | 3         | 72        | .2        | 2         | 2         | 65       | 1.28    | .053   | 29        | 25        | .86     | 195       | .14     | 2        | 2.31    | .03     | .09    | 1        | 1         |
| 9200W+9050N       | 6         | 23        | 6         | 73        | .1        | 15        | 10        | 398       | 3.10    | 4         | 5        | ND        | 4         | 43        | .2        | 2         | 2         | 69       | .61     | .043   | 14        | 27        | .87     | 200       | .16     | 2        | 2.43    | .02     | .07    | 1        | 4         |
| 9200W+9125N       | 6         | 20        | 8         | 77        | .1        | 15        | 11        | 688       | 3.07    | 2         | 5        | ND        | 5         | 36        | .3        | 2         | 2         | 68       | .57     | .053   | 12        | 28        | .92     | 171       | .15     | 2        | 2.43    | .02     | .09    | 1        | 1         |
| 9200W+9200N       | 5         | 18        | 6         | 69        | .1        | 11        | 18        | 1054      | 3.95    | 4         | 5        | ND        | 7         | 31        | .2        | 2         | 2         | 71       | .59     | .075   | 14        | 22        | .93     | 193       | .17     | 2        | 2.31    | .02     | .15    | 1        | 1         |
| 9200W+9275N       | 3         | 13        | 6         | 71        | .1        | 12        | 11        | 370       | 2.90    | 2         | 5        | ND        | 4         | 30        | .2        | 2         | 2         | 68       | .57     | .064   | 12        | 23        | .98     | 191       | .18     | 2        | 2.35    | .02     | .11    | 1        | 1         |
| 9200W+9350N       | 7         | 15        | 7         | 75        | .1        | 15        | 13        | 717       | 4.29    | 9         | 5        | ND        | 6         | 33        | .2        | 2         | 2         | 78       | .47     | .068   | 15        | 29        | .93     | 223       | .16     | 2        | 2.73    | .02     | .10    | 1        | 1         |
| 9200W+9425N       | 4         | 13        | 7         | 66        | .1        | 14        | 11        | 330       | 3.40    | 6         | 5        | ND        | 9         | 29        | .2        | 2         | 2         | 81       | .49     | .053   | 15        | 27        | 1.02    | 203       | .20     | 2        | 2.53    | .02     | .21    | 1        | 4         |

| ELEMENT<br>SAMPLE | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 9200W+9500N       | 1         | 15        | 23        | 86        | .1        | 13        | 11        | 793       | 2.56    | 7         | 5        | ND        | 6         | 33        | .2        | 2         | 2         | 61       | .59     | .065   | 15        | 25        | .73     | 179       | .12     | 2        | 1.98    | .01     | .05    | 1        | 12        |
| 10000W+7025N      | 1         | 27        | 9         | 67        | .1        | 23        | 13        | 399       | 3.49    | 10        | 5        | ND        | 5         | 31        | .2        | 2         | 2         | 69       | .50     | .065   | 14        | 35        | .97     | 178       | .16     | 2        | 2.93    | .01     | .14    | 1        | 1         |
| 10000W+7100N      | 1         | 24        | 8         | 67        | .1        | 22        | 11        | 276       | 3.11    | 6         | 5        | ND        | 4         | 32        | .2        | 2         | 2         | 73       | .48     | .066   | 14        | 34        | .95     | 182       | .15     | 2        | 2.72    | .02     | .12    | 1        | 1         |
| 10000W+7175N      | 1         | 25        | 8         | 63        | .1        | 23        | 11        | 281       | 2.99    | 6         | 5        | ND        | 4         | 32        | .2        | 2         | 2         | 66       | .51     | .069   | 16        | 33        | .89     | 184       | .15     | 2        | 2.55    | .02     | .09    | 1        | 1         |
| 10000W+7250N      | 1         | 29        | 7         | 65        | .1        | 21        | 11        | 331       | 3.28    | 5         | 5        | ND        | 6         | 37        | .2        | 2         | 2         | 67       | .60     | .070   | 18        | 32        | .96     | 201       | .17     | 2        | 2.34    | .02     | .11    | 1        | 1         |
| 10000W+7325N      | 3         | 32        | 9         | 48        | .1        | 17        | 8         | 268       | 2.90    | 5         | 5        | ND        | 4         | 27        | .4        | 2         | 2         | 55       | .35     | .049   | 14        | 26        | .61     | 129       | .12     | 3        | 2.13    | .02     | .07    | 1        | 3         |
| 10000W+7475N      | 2         | 41        | 9         | 61        | .1        | 21        | 9         | 366       | 3.31    | 7         | 5        | ND        | 4         | 26        | .2        | 2         | 2         | 65       | .39     | .059   | 12        | 32        | .79     | 154       | .15     | 2        | 2.38    | .01     | .09    | 1        | 5         |
| 10000W+7550N      | 3         | 39        | 9         | 63        | .2        | 16        | 12        | 750       | 3.17    | 5         | 5        | ND        | 2         | 35        | .4        | 2         | 2         | 65       | .44     | .057   | 20        | 26        | .72     | 185       | .12     | 3        | 2.21    | .02     | .10    | 1        | 2         |
| 10000W+7625N      | 2         | 43        | 9         | 61        | .1        | 20        | 12        | 520       | 3.51    | 5         | 5        | ND        | 5         | 24        | .3        | 2         | 2         | 70       | .36     | .057   | 17        | 27        | .90     | 133       | .15     | 2        | 2.85    | .02     | .13    | 1        | 1         |
| 10000W+7700N      | 6         | 46        | 7         | 57        | .1        | 20        | 12        | 824       | 3.06    | 5         | 5        | ND        | 3         | 30        | .2        | 2         | 2         | 63       | .41     | .061   | 15        | 32        | .71     | 147       | .14     | 3        | 2.40    | .02     | .08    | 1        | 3         |
| 10000W+7775N      | 10        | 52        | 9         | 68        | .1        | 18        | 10        | 384       | 3.18    | 3         | 5        | ND        | 6         | 31        | .4        | 2         | 2         | 68       | .47     | .061   | 17        | 30        | .94     | 171       | .18     | 2        | 2.41    | .02     | .13    | 1        | 1         |
| 10000W+7850N      | 13        | 47        | 11        | 62        | .1        | 21        | 11        | 437       | 3.45    | 6         | 5        | ND        | 3         | 34        | .2        | 2         | 2         | 72       | .44     | .062   | 16        | 34        | .83     | 215       | .14     | 2        | 2.65    | .02     | .08    | 1        | 2         |
| 10000W+7925N      | 4         | 55        | 9         | 65        | .1        | 20        | 11        | 436       | 3.37    | 6         | 5        | ND        | 7         | 34        | .2        | 2         | 2         | 70       | .49     | .065   | 20        | 32        | .89     | 212       | .18     | 2        | 2.38    | .02     | .13    | 1        | 1         |
| 10000W+8000N      | 2         | 43        | 12        | 74        | .1        | 21        | 12        | 519       | 3.47    | 7         | 5        | ND        | 6         | 32        | .4        | 2         | 2         | 74       | .42     | .049   | 14        | 28        | .87     | 191       | .17     | 2        | 2.38    | .02     | .15    | 4        | 3         |
| 10000W+8075N      | 2         | 48        | 12        | 83        | .1        | 23        | 13        | 690       | 3.40    | 4         | 5        | ND        | 5         | 35        | .3        | 2         | 2         | 73       | .54     | .076   | 14        | 29        | .93     | 166       | .17     | 2        | 2.21    | .02     | .16    | 2        | 1         |
| 10000W+8225N      | 3         | 51        | 11        | 77        | .1        | 20        | 12        | 593       | 3.73    | 5         | 5        | ND        | 9         | 28        | .5        | 2         | 2         | 74       | .43     | .062   | 19        | 28        | .93     | 188       | .16     | 2        | 2.57    | .02     | .14    | 1        | 1         |
| 10000W+8300N      | 2         | 52        | 8         | 66        | .1        | 18        | 10        | 395       | 3.44    | 5         | 5        | ND        | 7         | 30        | .2        | 2         | 2         | 71       | .49     | .067   | 20        | 31        | .93     | 157       | .19     | 2        | 2.41    | .02     | .22    | 1        | 2         |
| 10000W+8375N      | 9         | 166       | 10        | 64        | .1        | 21        | 12        | 580       | 3.13    | 7         | 5        | ND        | 4         | 34        | .2        | 2         | 2         | 67       | .46     | .070   | 13        | 26        | .71     | 145       | .16     | 2        | 2.23    | .02     | .13    | 7        | 1         |
| 10000W+8450N      | 1         | 31        | 7         | 53        | .1        | 19        | 9         | 315       | 2.99    | 5         | 5        | ND        | 5         | 26        | .2        | 2         | 2         | 61       | .41     | .060   | 12        | 29        | .68     | 106       | .15     | 2        | 2.25    | .02     | .08    | 1        | 3         |
| 10000W+8525N      | 11        | 69        | 10        | 97        | .1        | 25        | 15        | 783       | 4.38    | 5         | 5        | ND        | 7         | 29        | .7        | 2         | 2         | 90       | .32     | .041   | 25        | 39        | 1.16    | 214       | .17     | 2        | 3.82    | .02     | .08    | 1        | 1         |
| 10000W+8600N      | 11        | 64        | 8         | 86        | .1        | 18        | 12        | 566       | 3.50    | 4         | 5        | ND        | 5         | 32        | .2        | 2         | 2         | 76       | .49     | .061   | 13        | 26        | .96     | 172       | .17     | 2        | 2.68    | .02     | .17    | 1        | 1         |
| 10000W+8675N      | 9         | 77        | 8         | 69        | .1        | 16        | 14        | 700       | 3.67    | 4         | 5        | ND        | 8         | 27        | .2        | 2         | 2         | 80       | .43     | .052   | 13        | 23        | .99     | 182       | .19     | 2        | 2.33    | .03     | .24    | 7        | 1         |
| 10000W+8750N      | 5         | 35        | 9         | 62        | .1        | 17        | 12        | 522       | 3.43    | 6         | 5        | ND        | 5         | 26        | .2        | 2         | 2         | 75       | .40     | .064   | 13        | 26        | .87     | 135       | .16     | 2        | 2.28    | .02     | .14    | 5        | 7         |
| 10000W+8825N      | 2         | 37        | 7         | 63        | .1        | 19        | 12        | 649       | 3.28    | 6         | 5        | ND        | 7         | 40        | .2        | 2         | 2         | 76       | .63     | .071   | 15        | 29        | .89     | 158       | .18     | 2        | 1.82    | .04     | .16    | 2        | 1         |
| 10000W+8900N      | 3         | 30        | 6         | 85        | .1        | 21        | 14        | 908       | 3.86    | 7         | 5        | ND        | 10        | 35        | .2        | 2         | 2         | 81       | .55     | .054   | 15        | 29        | 1.10    | 224       | .18     | 2        | 2.59    | .03     | .22    | 1        | 1         |
| 10000W+8975N      | 4         | 32        | 5         | 68        | .1        | 15        | 13        | 586       | 3.50    | 5         | 5        | ND        | 9         | 30        | .2        | 2         | 2         | 77       | .47     | .069   | 16        | 28        | .95     | 120       | .19     | 2        | 2.26    | .02     | .21    | 1        | 44        |
| 10000W+9050N      | 11        | 38        | 8         | 79        | .1        | 21        | 13        | 513       | 3.78    | 7         | 5        | ND        | 7         | 50        | .2        | 2         | 2         | 82       | .80     | .064   | 31        | 31        | .98     | 253       | .16     | 2        | 2.82    | .03     | .17    | 1        | 1         |
| 10000W+9125N      | 9         | 31        | 10        | 78        | .1        | 19        | 11        | 387       | 3.58    | 4         | 5        | ND        | 6         | 47        | .2        | 2         | 2         | 80       | .75     | .066   | 28        | 28        | .95     | 241       | .15     | 2        | 2.72    | .03     | .17    | 1        | 1         |
| 10000W+9200N      | 73        | 22        | 5         | 25        | .1        | 9         | 11        | 3126      | 1.76    | 3         | 5        | ND        | 2         | 48        | .2        | 2         | 2         | 33       | .79     | .127   | 28        | 16        | .16     | 188       | .03     | 2        | .97     | .01     | .05    | 1        | 1         |
| 10000W+9275N      | 54        | 31        | 7         | 45        | .1        | 13        | 8         | 915       | 2.12    | 10        | 5        | ND        | 2         | 57        | .2        | 2         | 2         | 43       | .86     | .089   | 35        | 18        | .38     | 224       | .05     | 2        | 1.59    | .01     | .07    | 1        | 2         |
| 10000W+9350N      | 67        | 23        | 7         | 57        | .1        | 14        | 13        | 622       | 3.09    | 7         | 5        | ND        | 3         | 42        | .2        | 2         | 2         | 68       | .58     | .083   | 24        | 29        | .70     | 174       | .09     | 2        | 2.17    | .02     | .08    | 1        | 1         |
| 10000W+9425N      | 31        | 17        | 7         | 61        | .1        | 12        | 9         | 624       | 2.77    | 3         | 5        | ND        | 3         | 38        | .2        | 2         | 2         | 61       | .56     | .042   | 18        | 23        | .70     | 177       | .12     | 2        | 1.78    | .02     | .07    | 1        | 1         |
| 10000W+9500N      | AE 50     | 25        | 6         | 42        | .5        | 10        | 12        | 765       | 4.43    | 19        | 5        | ND        | 3         | 47        | .2        | 2         | 2         | 95       | .68     | .082   | 34        | 19        | .40     | 217       | .05     | 2        | 1.83    | .01     | .08    | 1        | 1         |
| 10600W+10675N     | 3         | 11        | 21        | 143       | .1        | 12        | 9         | 703       | 2.73    | 12        | 5        | ND        | 3         | 44        | .3        | 2         | 2         | 54       | .65     | .050   | 18        | 22        | .64     | 282       | .08     | 2        | 1.81    | .02     | .08    | 1        | 2         |
| 10600W+10750N     | 3         | 24        | 46        | 143       | .3        | 16        | 11        | 998       | 3.39    | 26        | 5        | ND        | 2         | 31        | .2        | 2         | 2         | 71       | .35     | .067   | 14        | 29        | .69     | 234       | .07     | 2        | 2.07    | .02     | .07    | 1        | 1         |

| ELEMENT<br>SAMPLE | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 10600W+10825N     | 3         | 42        | 20        | 139       | .1        | 19        | 12        | 604       | 3.07    | 25        | 5        | ND        | 3         | 34        | .2        | 2         | 2         | 60       | .49     | .058   | 10        | 37        | .88     | 290       | .12     | 2        | 2.28    | .03     | .10    | 3        | 2         |
| 10600W+10900N     | 2         | 38        | 17        | 110       | .1        | 14        | 12        | 557       | 3.28    | 17        | 5        | ND        | 3         | 50        | .3        | 2         | 2         | 69       | .48     | .038   | 8         | 23        | .80     | 276       | .09     | 2        | 2.52    | .02     | .09    | 1        | 7         |
| 10600W+10975N     | 3         | 81        | 8         | 69        | .1        | 13        | 7         | 266       | 2.85    | 12        | 5        | ND        | 3         | 30        | .2        | 2         | 2         | 61       | .47     | .051   | 11        | 30        | .72     | 237       | .09     | 2        | 2.09    | .02     | .17    | 1        | 86        |
| 10600W+11050N     | 1         | 32        | 13        | 88        | .1        | 10        | 10        | 565       | 3.57    | 14        | 5        | ND        | 6         | 34        | .2        | 2         | 2         | 69       | .36     | .040   | 13        | 20        | .83     | 278       | .13     | 2        | 1.78    | .01     | .14    | 3        | 14        |
| 10600W+11125N     | 1         | 43        | 13        | 77        | .2        | 12        | 9         | 555       | 2.97    | 11        | 5        | ND        | 4         | 56        | .2        | 2         | 2         | 56       | .53     | .071   | 21        | 22        | .67     | 445       | .09     | 2        | 1.97    | .02     | .10    | 1        | 120       |
| 10600W+11200N     | 1         | 26        | 15        | 71        | .1        | 12        | 10        | 584       | 2.99    | 14        | 5        | ND        | 8         | 50        | .2        | 2         | 2         | 55       | .58     | .054   | 24        | 21        | .67     | 275       | .10     | 2        | 1.88    | .02     | .11    | 1        | 20        |
| 10600W+11275N     | 1         | 13        | 87        | 232       | .4        | 17        | 6         | 265       | 2.38    | 108       | 5        | ND        | 8         | 31        | .3        | 7         | 2         | 44       | .49     | .047   | 20        | 29        | .65     | 128       | .11     | 2        | 1.79    | .01     | .09    | 1        | 3         |
| 10600W+11350N     | 24        | 225       | 27        | 79        | .2        | 10        | 11        | 617       | 3.39    | 33        | 5        | ND        | 7         | 40        | .3        | 2         | 2         | 50       | .39     | .056   | 26        | 17        | .43     | 417       | .06     | 2        | 1.79    | .01     | .13    | 1        | 35        |
| 10600W+11425N     | 11        | 218       | 34        | 102       | 1.7       | 18        | 13        | 707       | 4.03    | 68        | 5        | ND        | 6         | 51        | .2        | 2         | 2         | 63       | .56     | .085   | 34        | 30        | .64     | 401       | .07     | 2        | 2.59    | .01     | .12    | 1        | 41        |
| 10600W+11500N     | 6         | 225       | 16        | 107       | .3        | 19        | 7         | 403       | 2.23    | 61        | 5        | ND        | 2         | 81        | .2        | 2         | 2         | 40       | .95     | .066   | 28        | 22        | .42     | 369       | .06     | 2        | 1.74    | .01     | .09    | 1        | 1         |
| 10600W+11575N     | 4         | 58        | 24        | 213       | .3        | 20        | 8         | 592       | 2.80    | 206       | 5        | ND        | 2         | 64        | .2        | 2         | 2         | 53       | .78     | .060   | 14        | 30        | .64     | 361       | .10     | 2        | 1.93    | .02     | .10    | 1        | 7         |
| 10600W+11650N     | 17        | 171       | 26        | 166       | 1.0       | 18        | 46        | 5909      | 3.04    | 135       | 5        | ND        | 3         | 68        | 1.2       | 3         | 2         | 46       | .85     | .079   | 32        | 27        | .44     | 514       | .08     | 2        | 1.65    | .02     | .09    | 1        | 9         |
| 10600W+11725N     | 2         | 40        | 39        | 219       | .6        | 17        | 9         | 997       | 2.79    | 180       | 5        | ND        | 4         | 58        | .2        | 4         | 2         | 49       | .74     | .057   | 26        | 27        | .54     | 312       | .09     | 2        | 1.83    | .02     | .09    | 2        | 4         |
| 10600W+11800N     | 1         | 54        | 5         | 244       | .3        | 20        | 5         | 1714      | 1.05    | 28        | 5        | ND        | 2         | 136       | 2.0       | 2         | 2         | 10       | 2.52    | .117   | 82        | 12        | .15     | 259       | .01     | 3        | .68     | .01     | .04    | 1        | 3         |
| 10600W+11875N     | 1         | 79        | 31        | 247       | .9        | 19        | 8         | 1841      | 1.77    | 157       | 5        | ND        | 2         | 84        | 3.1       | 3         | 2         | 21       | 1.35    | .119   | 82        | 22        | .16     | 210       | .03     | 2        | 1.09    | .02     | .06    | 1        | 16        |
| 10600W+11950N     | 5         | 65        | 112       | 393       | 2.9       | 23        | 9         | 642       | 3.80    | 257       | 5        | ND        | 4         | 63        | .7        | 11        | 2         | 47       | .80     | .106   | 50        | 42        | .63     | 419       | .05     | 2        | 2.92    | .01     | .14    | 3        | 34        |
| 10600W+12025N     | 1         | 42        | 100       | 280       | 1.3       | 16        | 7         | 525       | 2.67    | 171       | 5        | ND        | 4         | 45        | .5        | 7         | 2         | 43       | .59     | .073   | 24        | 32        | .62     | 193       | .08     | 2        | 2.01    | .01     | .10    | 1        | 13        |
| 10600W+12100N     | 2         | 96        | 119       | 257       | 3.8       | 17        | 10        | 974       | 3.22    | 198       | 5        | ND        | 7         | 66        | 2.0       | 8         | 2         | 31       | .75     | .099   | 116       | 22        | .20     | 301       | .02     | 2        | 2.19    | .01     | .09    | 1        | 82        |
| 10600W+12175N     | 1         | 36        | 60        | 221       | .6        | 15        | 10        | 1102      | 3.27    | 147       | 5        | ND        | 4         | 42        | .4        | 4         | 2         | 52       | .53     | .080   | 22        | 30        | .58     | 203       | .07     | 2        | 1.92    | .01     | .09    | 1        | 20        |
| 10600W+12250N     | 1         | 42        | 24        | 84        | .7        | 7         | 1         | 227       | .60     | 42        | 5        | ND        | 2         | 48        | .6        | 3         | 2         | 8        | .85     | .118   | 17        | 13        | .07     | 99        | .01     | 2        | .57     | .01     | .03    | 1        | 13        |
| 10600W+12325N     | 1         | 32        | 161       | 324       | 2.1       | 16        | 10        | 852       | 2.94    | 318       | 5        | ND        | 2         | 39        | .8        | 3         | 2         | 47       | .55     | .082   | 20        | 29        | .57     | 163       | .06     | 2        | 1.77    | .02     | .07    | 1        | 205       |
| 10600W+12400N     | 1         | 27        | 57        | 201       | .8        | 15        | 6         | 882       | 1.40    | 115       | 5        | ND        | 2         | 78        | 3.0       | 2         | 2         | 22       | 1.34    | .065   | 41        | 15        | .17     | 248       | .04     | 2        | 1.05    | .01     | .06    | 1        | 4         |
| 10600W+12475N     | 1         | 30        | 31        | 209       | .7        | 14        | 5         | 987       | 1.09    | 108       | 5        | ND        | 2         | 84        | 4.3       | 4         | 2         | 15       | 1.44    | .090   | 58        | 11        | .13     | 227       | .02     | 2        | .95     | .01     | .06    | 1        | 7         |
| 10600W+12550N     | 2         | 23        | 59        | 113       | 1.0       | 16        | 8         | 1267      | 2.70    | 188       | 5        | ND        | 2         | 49        | .7        | 2         | 2         | 49       | .62     | .106   | 22        | 31        | .39     | 167       | .05     | 2        | 1.49    | .01     | .06    | 1        | 2         |
| 10600W+12625N     | 1         | 12        | 94        | 245       | .4        | 18        | 6         | 220       | 2.24    | 68        | 5        | ND        | 8         | 32        | .2        | 7         | 2         | 42       | .50     | .046   | 21        | 30        | .66     | 124       | .12     | 2        | 1.84    | .01     | .09    | 1        | 10        |
| 10600W+12700N     | 1         | 32        | 33        | 95        | .1        | 28        | 14        | 605       | 3.37    | 45        | 5        | ND        | 9         | 24        | .2        | 2         | 2         | 59       | .31     | .046   | 19        | 36        | .71     | 140       | .14     | 2        | 2.79    | .01     | .10    | 1        | 3         |
| 10600W+12775N     | 1         | 36        | 40        | 117       | .2        | 24        | 11        | 607       | 3.28    | 50        | 5        | ND        | 8         | 38        | .2        | 2         | 2         | 62       | .57     | .070   | 28        | 33        | .68     | 178       | .15     | 2        | 1.69    | .03     | .10    | 1        | 2         |
| 10600W+12850N     | 1         | 18        | 50        | 228       | .3        | 44        | 10        | 292       | 2.81    | 50        | 5        | ND        | 7         | 35        | .2        | 2         | 2         | 59       | .60     | .076   | 16        | 78        | 1.07    | 136       | .16     | 2        | 1.95    | .02     | .10    | 1        | 3         |
| 10600W+12925N     | 11        | 28        | 7         | 70        | .1        | 17        | 23        | 10281     | 2.68    | 147       | 5        | ND        | 2         | 98        | 1.2       | 4         | 2         | 16       | 1.88    | .122   | 14        | 10        | .14     | 453       | .02     | 2        | .63     | .01     | .02    | 1        | 1         |
| 10600W+13000N     | 1         | 22        | 27        | 102       | .1        | 21        | 13        | 2186      | 2.88    | 28        | 5        | ND        | 7         | 39        | .2        | 3         | 2         | 58       | .56     | .057   | 23        | 32        | .65     | 205       | .10     | 2        | 1.95    | .02     | .07    | 1        | 1         |
| 10600W+13075N     | 1         | 18        | 5         | 34        | .1        | 9         | 4         | 308       | .93     | 8         | 5        | ND        | 2         | 79        | .2        | 2         | 2         | 14       | 1.14    | .084   | 10        | 12        | .10     | 141       | .02     | 2        | .51     | .01     | .03    | 1        | 1         |
| 10600W+13150N K   | 1         | 15        | 20        | 108       | .1        | 14        | 6         | 255       | 1.98    | 25        | 5        | ND        | 2         | 44        | .2        | 2         | 2         | 35       | .63     | .073   | 14        | 20        | .42     | 135       | .07     | 2        | 1.25    | .01     | .07    | 1        | 1         |
| 10800W+7025N AZ 9 | 9         | 20        | 5         | 69        | .1        | 14        | 10        | 512       | 2.98    | 3         | 5        | ND        | 5         | 44        | .2        | 2         | 2         | 64       | .68     | .039   | 15        | 24        | .87     | 192       | .14     | 2        | 2.17    | .02     | .16    | 1        | 1         |
| 10800W+7100N      | 12        | 26        | 9         | 74        | .1        | 17        | 12        | 563       | 3.29    | 2         | 5        | ND        | 5         | 48        | .2        | 2         | 2         | 71       | .73     | .049   | 32        | 28        | .88     | 218       | .13     | 2        | 2.58    | .02     | .15    | 1        | 1         |
| 10800W+7175N      | 14        | 22        | 9         | 85        | .1        | 16        | 12        | 809       | 3.13    | 4         | 5        | ND        | 5         | 48        | .2        | 2         | 2         | 67       | .73     | .047   | 15        | 26        | .90     | 244       | .15     | 2        | 2.47    | .02     | .17    | 1        | 1         |

| ELEMENT<br>SAMPLE       | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Sc<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |    |
|-------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|----|
| 10800W+7250N            | 6         | 21        | 9         | 70        | .1        | 14        | 9         | 311     | 2.55      | 2        | 5         | ND        | 6         | 36        | .2        | 2         | 2        | 61      | .59    | .045      | 12        | 26      | .93       | 175     | .17      | 2       | 2.26    | .02    | .18      | 1         | 1  |
| 10800W+7325N            | 34        | 30        | 8         | 69        | .1        | 16        | 15        | 1381    | 3.13      | 2        | 5         | ND        | 2         | 58        | .2        | 2         | 2        | 63      | .89    | .085      | 20        | 28      | .67       | 277     | .09      | 2       | 2.52    | .02    | .11      | 1         | 1  |
| 10800W+7400N            | 18        | 33        | 9         | 66        | .1        | 15        | 11        | 299     | 2.82      | 2        | 5         | ND        | 10        | 32        | .2        | 2         | 2        | 74      | .54    | .041      | 23        | 28      | .94       | 177     | .18      | 2       | 2.42    | .02    | .21      | 1         | 5  |
| 10800W+7475N            | 16        | 31        | 9         | 77        | .1        | 18        | 13        | 808     | 3.22      | 3        | 5         | ND        | 3         | 48        | .2        | 2         | 2        | 67      | .67    | .059      | 16        | 29      | .85       | 245     | .12      | 2       | 2.52    | .02    | .11      | 1         | 1  |
| 10800W+7550N            | 17        | 26        | 6         | 72        | .1        | 16        | 11        | 442     | 3.17      | 2        | 5         | ND        | 5         | 31        | .2        | 2         | 2        | 69      | .44    | .039      | 13        | 26      | .85       | 182     | .15      | 2       | 2.36    | .02    | .13      | 1         | 1  |
| 10800W+7625N            | 19        | 27        | 10        | 105       | .2        | 18        | 13        | 540     | 3.74      | 3        | 5         | ND        | 3         | 52        | .2        | 2         | 2        | 78      | .76    | .069      | 11        | 31      | .94       | 267     | .13      | 2       | 2.84    | .02    | .16      | 1         | 1  |
| 10800W+7700N            | 25        | 26        | 10        | 70        | .1        | 12        | 10        | 604     | 3.19      | 5        | 5         | ND        | 5         | 41        | .2        | 2         | 2        | 76      | .63    | .043      | 11        | 24      | .92       | 195     | .16      | 2       | 2.25    | .02    | .14      | 1         | 1  |
| 10800W+7775N            | 22        | 40        | 7         | 93        | .2        | 11        | 14        | 1740    | 3.23      | 2        | 5         | ND        | 5         | 65        | .3        | 2         | 2        | 73      | 1.07   | .087      | 21        | 22      | 1.14      | 295     | .14      | 2       | 2.11    | .03    | .11      | 1         | 1  |
| 10800W+7850N            | 14        | 33        | 12        | 94        | .1        | 17        | 12        | 757     | 3.34      | 4        | 5         | ND        | 3         | 46        | .2        | 2         | 2        | 69      | .66    | .058      | 15        | 27      | .89       | 250     | .11      | 2       | 2.28    | .02    | .11      | 1         | 1  |
| 10800W+7925N            | 6         | 22        | 7         | 70        | .3        | 11        | 11        | 405     | 2.80      | 2        | 5         | ND        | 7         | 41        | .2        | 2         | 2        | 62      | .77    | .072      | 15        | 25      | 1.21      | 223     | .18      | 2       | 2.48    | .03    | .17      | 1         | 1  |
| 10800W+8000N            | 18        | 27        | 9         | 59        | .1        | 12        | 10        | 367     | 3.44      | 10       | 5         | ND        | 7         | 30        | .2        | 2         | 2        | 125     | .52    | .043      | 13        | 23      | 1.06      | 180     | .18      | 2       | 2.45    | .02    | .15      | 1         | 1  |
| 10800W+8075N            | 12        | 46        | 11        | 81        | .5        | 17        | 11        | 551     | 3.07      | 4        | 5         | ND        | 3         | 64        | .2        | 2         | 2        | 70      | .99    | .090      | 27        | 29      | .94       | 295     | .09      | 2       | 2.66    | .02    | .10      | 1         | 3  |
| 10800W+8150N            | 14        | 23        | 8         | 47        | .4        | 11        | 6         | 485     | 2.16      | 2        | 5         | ND        | 2         | 44        | .2        | 2         | 2        | 57      | .59    | .058      | 13        | 17      | .36       | 175     | .10      | 2       | 1.25    | .02    | .08      | 1         | 1  |
| 10800W+8225N            | 11        | 39        | 8         | 66        | .1        | 18        | 11        | 413     | 3.29      | 5        | 5         | ND        | 5         | 21        | .2        | 2         | 2        | 70      | .32    | .049      | 15        | 27      | .92       | 127     | .15      | 2       | 2.48    | .02    | .15      | 1         | 1  |
| 10800W+8300N            | 11        | 36        | 10        | 77        | .1        | 20        | 10        | 571     | 3.27      | 7        | 5         | ND        | 3         | 32        | .2        | 2         | 2        | 67      | .45    | .053      | 11        | 29      | .88       | 172     | .14      | 2       | 2.14    | .02    | .10      | 1         | 2  |
| 10800W+8375N            | 12        | 106       | 9         | 66        | .1        | 21        | 12        | 299     | 3.57      | 8        | 5         | ND        | 8         | 33        | .2        | 2         | 2        | 79      | .51    | .064      | 24        | 31      | .96       | 211     | .19      | 2       | 2.56    | .02    | .22      | 1         | 2  |
| 10800W+8450N            | 7         | 53        | 9         | 76        | .2        | 18        | 12        | 1051    | 2.85      | 5        | 5         | ND        | 2         | 51        | .2        | 2         | 2        | 61      | .64    | .083      | 12        | 25      | .65       | 223     | .10      | 2       | 1.59    | .02    | .10      | 1         | 1  |
| 10800W+8525N            | 2         | 46        | 9         | 67        | .1        | 19        | 13        | 469     | 3.73      | 4        | 5         | ND        | 9         | 40        | .2        | 2         | 2        | 79      | .66    | .065      | 25        | 31      | 1.14      | 229     | .19      | 2       | 2.43    | .03    | .31      | 1         | 7  |
| 10800W+8600N            | 10        | 20        | 7         | 43        | .1        | 10        | 8         | 621     | 2.23      | 4        | 5         | ND        | 2         | 24        | .2        | 2         | 2        | 50      | .26    | .045      | 8         | 21      | .35       | 79      | .09      | 2       | 1.40    | .02    | .07      | 1         | 2  |
| 10800W+8675N            | 7         | 35        | 5         | 66        | .1        | 18        | 11        | 427     | 3.39      | 3        | 5         | ND        | 9         | 38        | .2        | 2         | 2        | 74      | .55    | .060      | 25        | 29      | 1.07      | 217     | .18      | 2       | 2.47    | .02    | .16      | 1         | 5  |
| 10800W+8750N            | 4         | 27        | 11        | 69        | .1        | 15        | 14        | 731     | 3.95      | 5        | 5         | ND        | 12        | 36        | .2        | 2         | 2        | 76      | .57    | .060      | 33        | 26      | .92       | 191     | .16      | 2       | 2.21    | .02    | .19      | 1         | 3  |
| 10800W+8825N            | 3         | 30        | 8         | 65        | .1        | 16        | 12        | 564     | 3.43      | 5        | 5         | ND        | 10        | 31        | .2        | 2         | 2        | 74      | .48    | .068      | 25        | 26      | .90       | 177     | .18      | 2       | 2.04    | .02    | .22      | 2         | 12 |
| 10800W+8900N            | 10        | 27        | 13        | 74        | .1        | 18        | 10        | 431     | 3.42      | 7        | 5         | ND        | 3         | 50        | .2        | 2         | 2        | 77      | .80    | .052      | 12        | 29      | .89       | 236     | .14      | 2       | 2.13    | .02    | .09      | 1         | 4  |
| 10800W+8975N            | 1         | 24        | 7         | 70        | .1        | 19        | 12        | 581     | 3.50      | 5        | 5         | ND        | 11        | 29        | .2        | 2         | 2        | 76      | .46    | .065      | 16        | 26      | 1.01      | 189     | .18      | 2       | 2.29    | .02    | .23      | 1         | 19 |
| 10800W+9050N            | 3         | 29        | 9         | 55        | .1        | 19        | 11        | 296     | 2.98      | 4        | 5         | ND        | 9         | 26        | .2        | 2         | 2        | 67      | .39    | .051      | 21        | 32      | .84       | 176     | .16      | 2       | 2.38    | .02    | .14      | 1         | 10 |
| 10800W+9125N            | 5         | 24        | 8         | 64        | .1        | 18        | 11        | 640     | 3.25      | 6        | 5         | ND        | 5         | 32        | .2        | 2         | 2        | 71      | .49    | .061      | 18        | 28      | .85       | 189     | .14      | 2       | 2.20    | .02    | .12      | 1         | 3  |
| 10800W+9200N            | 4         | 21        | 8         | 68        | .1        | 13        | 12        | 439     | 3.44      | 5        | 5         | ND        | 10        | 29        | .2        | 2         | 2        | 76      | .46    | .061      | 22        | 25      | .91       | 185     | .17      | 2       | 2.18    | .02    | .21      | 1         | 1  |
| 10800W+9275N            | 2         | 24        | 8         | 65        | .1        | 17        | 9         | 385     | 3.29      | 5        | 5         | ND        | 7         | 28        | .2        | 2         | 2        | 74      | .46    | .066      | 12        | 28      | .87       | 175     | .16      | 2       | 2.24    | .02    | .19      | 1         | 2  |
| 10800W+9300N            | 5         | 20        | 6         | 68        | .1        | 15        | 10        | 539     | 3.14      | 4        | 5         | ND        | 3         | 32        | .2        | 2         | 2        | 68      | .45    | .067      | 9         | 22      | .82       | 163     | .12      | 2       | 2.03    | .03    | .11      | 1         | 8  |
| 10800W+9425N            | 6         | 17        | 6         | 74        | .1        | 16        | 12        | 714     | 3.71      | 5        | 5         | ND        | 4         | 36        | .2        | 2         | 2        | 72      | .46    | .049      | 10        | 29      | .84       | 166     | .14      | 2       | 2.26    | .01    | .12      | 1         | 1  |
| 10800W+9500N <i>AZ4</i> | 17        | 7         | 62        | .1        | 14        | 9         | 498       | 2.99    | 3         | 5        | ND        | 3         | 28        | .2        | 2         | 2         | 68       | .39     | .050   | 9         | 26        | .68     | 138       | .12     | 2        | 1.90    | .01     | .09    | 2        | 2         |    |
| 11400W+10675N <i>K</i>  | 3         | 26        | 28        | 157       | .1        | 18        | 11        | 549     | 3.22      | 43       | 5         | ND        | 11        | 33        | .2        | 2         | 2        | 65      | .46    | .045      | 22        | 33      | .82       | 165     | .14      | 2       | 2.31    | .01    | .14      | 1         | 5  |
| 11400W+10750N           | 6         | 66        | 188       | 415       | 1.0       | 18        | 8         | 502     | 3.52      | 492      | 5         | ND        | 11        | 43        | .6        | 3         | 2        | 60      | .50    | .052      | 22        | 32      | .69       | 121     | .13      | 2       | 1.93    | .02    | .17      | 1         | 63 |
| 11400W+10825N           | 3         | 24        | 118       | 296       | .6        | 17        | 10        | 613     | 3.28      | 203      | 5         | ND        | 9         | 26        | .3        | 2         | 2        | 64      | .32    | .032      | 24        | 32      | .67       | 99      | .12      | 2       | 2.27    | .01    | .09      | 1         | 8  |
| 11400W+10900N           | 6         | 14        | 49        | 133       | .1        | 13        | 8         | 389     | 4.04      | 36       | 5         | ND        | 3         | 19        | .2        | 3         | 2        | 84      | .22    | .026      | 8         | 23      | .40       | 104     | .14      | 2       | 1.60    | .01    | .06      | 1         | 9  |

| ELEMENT SAMPLE | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P %  | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au ppb |
|----------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------|--------|--------|--------|--------|--------|--------|-------|------|------|--------|--------|------|--------|------|-------|------|------|-----|-------|--------|
| 11400W+10975N  | 9      | 25     | 108    | 300    | .5     | 19     | 15     | 627    | 4.13 | 87     | 6     | ND     | 6      | 29     | .2     | 2      | 2      | 71    | .40  | .062 | 25     | 33     | .63  | 157    | .10  | 2     | 2.21 | .01  | .09 | 1     | 4      |
| ✓11400W+11050N | 4      | 22     | 7      | 55     | .3     | 6      | 3      | 450    | .51  | 6      | 5     | ND     | 2      | 35     | .8     | 2      | 2      | 9     | .60  | .108 | 12     | 11     | .05  | 129    | .01  | 2     | .45  | .01  | .02 | 1     | 5      |
| ✓11400W+11125N | 19     | 18     | 18     | 101    | .1     | 10     | 11     | 1121   | 3.52 | 30     | 5     | ND     | 2      | 34     | .2     | 2      | 2      | 73    | .57  | .096 | 11     | 23     | .40  | 128    | .07  | 2     | 1.17 | .01  | .05 | 1     | 2      |
| ✓11400W+11200N | 4      | 21     | 4      | 55     | .1     | 9      | 3      | 533    | .78  | 2      | 5     | ND     | 2      | 51     | .4     | 2      | 2      | 12    | 1.00 | .089 | 14     | 9      | .09  | 141    | .02  | 2     | .51  | .01  | .02 | 1     | 3      |
| ✓11400W+11275N | 15     | 18     | 5      | 68     | .3     | 7      | 36     | 2777   | 4.04 | 11     | 5     | ND     | 2      | 46     | .2     | 2      | 2      | 41    | .79  | .104 | 18     | 13     | .18  | 159    | .03  | 2     | .71  | .01  | .05 | 1     | 1      |
| 11400W+11350N  | 10     | 11     | 13     | 65     | .1     | 10     | 8      | 515    | 3.03 | 7      | 5     | ND     | 2      | 31     | .2     | 2      | 2      | 55    | .46  | .080 | 9      | 21     | .40  | 135    | .09  | 2     | 1.23 | .02  | .05 | 1     | 3      |
| ✓11400W+11425N | 11     | 14     | 11     | 73     | .1     | 9      | 32     | 1461   | 5.60 | 24     | 5     | ND     | 3      | 37     | .3     | 2      | 2      | 76    | .55  | .083 | 11     | 17     | .36  | 143    | .07  | 3     | 1.07 | .01  | .07 | 1     | 3      |
| 11400W+11500N  | 7      | 17     | 16     | 101    | .1     | 11     | 14     | 1040   | 3.63 | 16     | 5     | ND     | 7      | 35     | .2     | 2      | 2      | 83    | .47  | .063 | 14     | 22     | .76  | 163    | .15  | 2     | 1.74 | .02  | .14 | 1     | 31     |
| 11400W+11575N  | 5      | 41     | 12     | 57     | .1     | 8      | 6      | 208    | 2.84 | 7      | 5     | ND     | 2      | 51     | .2     | 2      | 2      | 62    | .34  | .046 | 14     | 17     | .72  | 220    | .11  | 2     | 1.76 | .03  | .17 | 1     | 50     |
| 11400W+11650N  | 2      | 26     | 54     | 159    | .4     | 14     | 7      | 366    | 2.53 | 82     | 5     | ND     | 6      | 27     | .3     | 2      | 2      | 45    | .34  | .038 | 17     | 26     | .45  | 155    | .09  | 2     | 1.94 | .01  | .08 | 1     | 29     |
| 11400W+11725N  | 2      | 33     | 37     | 136    | .5     | 13     | 6      | 356    | 2.17 | 86     | 5     | ND     | 2      | 27     | .2     | 2      | 2      | 38    | .33  | .048 | 18     | 24     | .40  | 165    | .07  | 2     | 1.59 | .01  | .07 | 1     | 40     |
| 11400W+11800N  | 2      | 22     | 56     | 157    | .5     | 13     | 11     | 729    | 2.67 | 131    | 5     | ND     | 3      | 28     | .2     | 2      | 2      | 46    | .35  | .048 | 15     | 27     | .44  | 145    | .08  | 2     | 1.79 | .01  | .08 | 1     | 6      |
| 11400W+11875N  | 3      | 39     | 44     | 134    | .6     | 12     | 14     | 1238   | 2.14 | 72     | 5     | ND     | 2      | 34     | .3     | 2      | 2      | 31    | .39  | .065 | 24     | 23     | .27  | 218    | .05  | 2     | 1.36 | .01  | .06 | 1     | 16     |
| 11400W+11950N  | 7      | 57     | 58     | 126    | .4     | 13     | 9      | 329    | 3.11 | 114    | 5     | ND     | 6      | 48     | .2     | 2      | 2      | 41    | .54  | .046 | 25     | 22     | .40  | 222    | .07  | 2     | 1.74 | .01  | .08 | 1     | 36     |
| 11400W+12050N  | 4      | 43     | 36     | 164    | .1     | 19     | 8      | 545    | 2.51 | 72     | 5     | ND     | 2      | 72     | 1.5    | 4      | 2      | 41    | .77  | .074 | 35     | 24     | .39  | 386    | .06  | 2     | 1.66 | .01  | .09 | 2     | 11     |
| 11400W+12125N  | 7      | 62     | 41     | 108    | .7     | 17     | 12     | 917    | 3.09 | 74     | 5     | ND     | 3      | 63     | .4     | 4      | 2      | 44    | .62  | .089 | 32     | 26     | .40  | 435    | .05  | 2     | 2.07 | .01  | .08 | 1     | 23     |
| 11400W+12200N  | 6      | 38     | 35     | 104    | .3     | 12     | 5      | 206    | 2.95 | 62     | 5     | ND     | 5      | 47     | .2     | 2      | 2      | 47    | .47  | .039 | 19     | 21     | .46  | 295    | .07  | 2     | 2.04 | .01  | .10 | 1     | 34     |
| 11400W+12275N  | 4      | 72     | 27     | 86     | .5     | 15     | 6      | 296    | 2.47 | 40     | 5     | ND     | 2      | 50     | .4     | 2      | 2      | 38    | .50  | .069 | 27     | 21     | .36  | 355    | .05  | 2     | 1.65 | .01  | .07 | 1     | 20     |
| 11400W+12350N  | 3      | 60     | 26     | 56     | .3     | 10     | 6      | 231    | 4.71 | 45     | 5     | ND     | 8      | 42     | .2     | 2      | 2      | 35    | .41  | .063 | 33     | 17     | .35  | 331    | .04  | 2     | 2.22 | .01  | .07 | 1     | 32     |
| 11400W+12425N  | 3      | 57     | 14     | 51     | .6     | 8      | 5      | 196    | 3.13 | 20     | 5     | ND     | 7      | 42     | .2     | 2      | 2      | 34    | .40  | .064 | 32     | 13     | .24  | 361    | .04  | 2     | 3.07 | .01  | .08 | 1     | 44     |
| 11400W+12500N  | 3      | 53     | 18     | 64     | .6     | 10     | 6      | 187    | 2.59 | 26     | 5     | ND     | 4      | 39     | .2     | 2      | 2      | 46    | .34  | .058 | 35     | 18     | .46  | 348    | .07  | 2     | 2.15 | .01  | .10 | 1     | 60     |
| 11400W+12575N  | 2      | 90     | 12     | 90     | .6     | 20     | 35     | 4793   | 2.32 | 10     | 5     | ND     | 3      | 47     | .3     | 2      | 2      | 42    | .40  | .033 | 32     | 17     | .38  | 317    | .08  | 2     | 1.33 | .02  | .10 | 1     | 22     |
| 11400W+12650N  | 2      | 50     | 12     | 73     | .4     | 13     | 9      | 944    | 2.02 | 9      | 5     | ND     | 2      | 27     | .2     | 2      | 2      | 44    | .20  | .044 | 14     | 16     | .16  | 187    | .04  | 2     | 1.06 | .02  | .09 | 1     | 19     |
| ✓11400W+12725N | 4      | 54     | 10     | 82     | .9     | 9      | 7      | 323    | 3.54 | 17     | 5     | ND     | 5      | 46     | .2     | 2      | 2      | 56    | .48  | .076 | 23     | 16     | .69  | 328    | .08  | 2     | 2.35 | .01  | .19 | 1     | 64     |
| 11400W+12800N  | 2      | 43     | 16     | 56     | .6     | 13     | 5      | 196    | 2.42 | 14     | 5     | ND     | 2      | 31     | .2     | 2      | 2      | 45    | .28  | .047 | 18     | 24     | .43  | 208    | .07  | 2     | 1.75 | .01  | .08 | 1     | 46     |
| 11400W+12875N  | 1      | 39     | 25     | 95     | .4     | 16     | 11     | 374    | 3.77 | 25     | 5     | ND     | 11     | 34     | .2     | 2      | 2      | 63    | .46  | .059 | 23     | 28     | .82  | 303    | .15  | 2     | 1.99 | .01  | .11 | 1     | 52     |
| 11400W+12950N  | 1      | 94     | 67     | 162    | 1.0    | 18     | 13     | 515    | 4.14 | 32     | 5     | ND     | 12     | 28     | .2     | 2      | 3      | 63    | .34  | .049 | 27     | 30     | .73  | 202    | .12  | 2     | 2.13 | .01  | .14 | 1     | 30     |
| 11400W+13025N  | 1      | 31     | 39     | 125    | .3     | 17     | 10     | 456    | 3.32 | 24     | 5     | ND     | 7      | 29     | .4     | 2      | 2      | 59    | .39  | .055 | 16     | 30     | .69  | 204    | .13  | 2     | 2.12 | .01  | .09 | 1     | 10     |
| 11400W+13100N  | 1      | 34     | 32     | 115    | .4     | 19     | 12     | 329    | 3.51 | 36     | 5     | ND     | 9      | 31     | .2     | 2      | 2      | 71    | .40  | .045 | 22     | 33     | .70  | 256    | .13  | 2     | 2.40 | .01  | .09 | 1     | 20     |
| 12800W+9025N   | 4      | 33     | 10     | 67     | .1     | 16     | 13     | 468    | 3.88 | 16     | 5     | ND     | 5      | 32     | .2     | 2      | 2      | 69    | .50  | .056 | 15     | 27     | .88  | 180    | .13  | 2     | 2.37 | .02  | .13 | 1     | 2      |
| 12800W+9100N   | 3      | 52     | 7      | 67     | .1     | 16     | 12     | 380    | 3.94 | 5      | 5     | ND     | 9      | 34     | .2     | 2      | 2      | 77    | .63  | .048 | 12     | 36     | 1.16 | 207    | .10  | 2     | 2.94 | .01  | .24 | 1     | 1      |
| 12800W+9175N   | 4      | 42     | 12     | 52     | .1     | 10     | 8      | 354    | 3.49 | 8      | 5     | ND     | 3      | 36     | .2     | 2      | 2      | 76    | .55  | .046 | 27     | 21     | .58  | 203    | .10  | 2     | 2.02 | .01  | .13 | 3     | 1      |
| 12800W+9250N   | 3      | 14     | 5      | 54     | .1     | 10     | 9      | 308    | 2.30 | 6      | 5     | ND     | 5      | 26     | .2     | 2      | 2      | 41    | .48  | .055 | 13     | 21     | .67  | 184    | .14  | 2     | 1.88 | .02  | .07 | 5     | 1      |
| 12800W+9325N   | 10     | 16     | 7      | 76     | .1     | 14     | 11     | 550    | 3.00 | 13     | 5     | ND     | 4      | 36     | .2     | 2      | 2      | 63    | .52  | .057 | 13     | 25     | .86  | 200    | .13  | 2     | 2.10 | .02  | .11 | 1     | 1      |
| 12800W+9400N   | 2      | 15     | 7      | 64     | .1     | 15     | 17     | 1041   | 4.05 | 11     | 5     | ND     | 5      | 40     | .2     | 2      | 2      | 80    | .53  | .063 | 18     | 28     | .69  | 252    | .12  | 2     | 2.24 | .02  | .10 | 1     | 2      |

| ELEMENT<br>SAMPLE           | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-----------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 12800W+9475N                | 1         | 13        | 5         | 68        | .1        | 15        | 10        | 626       | 3.01    | 6         | 5        | ND        | 6         | 33        | .2        | 2         | 2         | 66       | .55     | .065   | 12        | 25        | .91     | 169       | .18     | 2        | 2.11    | .02     | .18    | 1        | 1         |
| 12800W+9550N                | 3         | 15        | 8         | 58        | .1        | 14        | 12        | 471       | 3.39    | 8         | 5        | ND        | 6         | 29        | .2        | 2         | 2         | 75       | .43     | .065   | 14        | 28        | .87     | 170       | .16     | 2        | 2.32    | .02     | .17    | 1        | 1         |
| 12800W+9625N                | 11        | 17        | 10        | 60        | .1        | 13        | 34        | 3092      | 5.38    | 17        | 5        | ND        | 6         | 35        | .2        | 2         | 2         | 99       | .49     | .089   | 20        | 26        | .66     | 234       | .12     | 2        | 2.13    | .02     | .11    | 1        | 1         |
| 12800W+9700N                | 1         | 12        | 7         | 56        | .1        | 14        | 14        | 468       | 2.97    | 7         | 5        | ND        | 5         | 29        | .2        | 2         | 2         | 57       | .46     | .056   | 11        | 26        | .80     | 176       | .15     | 2        | 2.17    | .02     | .11    | 1        | 2         |
| 12800W+9775N                | 3         | 9         | 7         | 63        | .1        | 13        | 20        | 1010      | 3.33    | 8         | 5        | ND        | 4         | 27        | .2        | 2         | 2         | 72       | .45     | .074   | 11        | 22        | .71     | 155       | .15     | 2        | 1.94    | .02     | .13    | 1        | 1         |
| 12800W+9850N <sup>AE</sup>  | 3         | 12        | 11        | 53        | .3        | 12        | 5         | 171       | 2.99    | 8         | 5        | ND        | 3         | 20        | .2        | 2         | 2         | 70       | .22     | .016   | 15        | 23        | .37     | 168       | .14     | 2        | 1.64    | .01     | .04    | 1        | 1         |
| 12800W+10000N               | 3         | 12        | 5         | 74        | .3        | 14        | 8         | 499       | 2.77    | 2         | 5        | ND        | 2         | 25        | .2        | 2         | 2         | 59       | .33     | .034   | 13        | 24        | .69     | 165       | .14     | 2        | 1.85    | .02     | .09    | 1        | 1         |
| 12800W+10075N               | 5         | 16        | 4         | 77        | .2        | 13        | 10        | 590       | 4.28    | 6         | 5        | ND        | 5         | 30        | .2        | 2         | 2         | 86       | .49     | .068   | 15        | 25        | .72     | 160       | .13     | 2        | 1.85    | .02     | .15    | 1        | 1         |
| 12800W+10225N               | 2         | 10        | 6         | 80        | .5        | 15        | 8         | 301       | 3.20    | 11        | 5        | ND        | 4         | 26        | .4        | 2         | 2         | 73       | .46     | .066   | 11        | 27        | .86     | 155       | .15     | 3        | 2.09    | .02     | .12    | 1        | 1         |
| 12800W+10300N               | 1         | 9         | 8         | 70        | .2        | 15        | 8         | 254       | 2.20    | 2         | 5        | ND        | 4         | 24        | .4        | 2         | 2         | 48       | .36     | .038   | 13        | 28        | .72     | 160       | .14     | 2        | 2.08    | .02     | .09    | 1        | 1         |
| 12800W+10375N               | 1         | 7         | 11        | 65        | .3        | 13        | 7         | 196       | 2.05    | 6         | 5        | ND        | 3         | 23        | .4        | 2         | 2         | 41       | .39     | .043   | 10        | 25        | .66     | 142       | .14     | 2        | 1.89    | .01     | .09    | 3        | 1         |
| 12800W+10450N               | 1         | 13        | 9         | 71        | .3        | 18        | 8         | 204       | 2.59    | 5         | 5        | ND        | 5         | 23        | .2        | 2         | 2         | 50       | .38     | .045   | 12        | 29        | .71     | 147       | .15     | 2        | 2.17    | .01     | .08    | 1        | 1         |
| 12800W+10525N               | 1         | 7         | 7         | 54        | .2        | 12        | 5         | 164       | 1.74    | 2         | 5        | ND        | 2         | 24        | .2        | 2         | 3         | 32       | .32     | .039   | 9         | 24        | .52     | 147       | .12     | 2        | 1.66    | .01     | .04    | 1        | 1         |
| 12800W+10600N               | 1         | 10        | 5         | 74        | .2        | 15        | 8         | 404       | 3.09    | 6         | 5        | ND        | 3         | 25        | .3        | 2         | 2         | 58       | .38     | .058   | 12        | 26        | .69     | 158       | .13     | 2        | 1.91    | .01     | .08    | 1        | 1         |
| 13600W+10600N               | 4         | 13        | 9         | 79        | .4        | 16        | 7         | 236       | 2.68    | 6         | 5        | ND        | 6         | 28        | .2        | 2         | 2         | 60       | .42     | .043   | 19        | 26        | .75     | 189       | .15     | 3        | 1.96    | .02     | .13    | 1        | 1         |
| 13600W+10675N               | 7         | 14        | 11        | 84        | .3        | 11        | 8         | 343       | 3.21    | 8         | 7        | ND        | 8         | 29        | .5        | 3         | 2         | 66       | .50     | .061   | 16        | 27        | .85     | 202       | .14     | 2        | 2.03    | .02     | .20    | 2        | 1         |
| 13600W+10700N               | 50        | 11        | 5         | 89        | .3        | 11        | 24        | 2541      | 4.85    | 7         | 6        | ND        | 7         | 38        | .2        | 2         | 2         | 81       | .59     | .061   | 19        | 21        | .73     | 268       | .13     | 2        | 1.84    | .02     | .18    | 1        | 1         |
| 13600W+10825N               | 1         | 15        | 8         | 77        | .3        | 14        | 8         | 443       | 3.18    | 8         | 5        | ND        | 6         | 32        | .4        | 2         | 2         | 66       | .56     | .052   | 21        | 26        | .78     | 250       | .14     | 2        | 2.35    | .02     | .16    | 1        | 1         |
| 13600W+10900N <sup>AE</sup> | 1         | 11        | 12        | 90        | .2        | 15        | 13        | 597       | 4.29    | 5         | 5        | ND        | 7         | 21        | .3        | 2         | 3         | 88       | .34     | .040   | 13        | 29        | .91     | 163       | .17     | 2        | 2.73    | .02     | .14    | 1        | 1         |
| 13600W+10975N <sup>N</sup>  | 1         | 13        | 5         | 74        | .2        | 13        | 8         | 285       | 3.11    | 13        | 5        | ND        | 3         | 32        | .3        | 2         | 3         | 61       | .55     | .047   | 17        | 24        | .77     | 193       | .13     | 2        | 1.97    | .02     | .08    | 1        | 2         |
| 13600W+11050NA              | 1         | 13        | 9         | 71        | .2        | 16        | 11        | 771       | 3.28    | 52        | 5        | ND        | 3         | 26        | .2        | 2         | 2         | 63       | .42     | .045   | 15        | 28        | .69     | 219       | .12     | 2        | 2.07    | .02     | .05    | 1        | 1         |
| 13600W+11050NB              | 1         | 10        | 11        | 83        | .4        | 14        | 10        | 383       | 3.47    | 83        | 5        | ND        | 4         | 21        | .7        | 3         | 2         | 71       | .27     | .026   | 9         | 28        | .77     | 126       | .15     | 2        | 1.98    | .02     | .06    | 1        | 7         |
| 13600W+11125N               | 1         | 11        | 10        | 89        | .2        | 15        | 11        | 337       | 3.54    | 23        | 5        | ND        | 5         | 24        | .3        | 2         | 2         | 72       | .41     | .042   | 9         | 27        | .93     | 170       | .17     | 2        | 2.32    | .02     | .14    | 1        | 1         |
| 13600W+11200N               | 1         | 11        | 5         | 84        | .2        | 14        | 10        | 276       | 3.22    | 6         | 5        | ND        | 5         | 27        | .2        | 2         | 2         | 62       | .47     | .044   | 12        | 29        | .90     | 161       | .17     | 2        | 2.26    | .02     | .13    | 1        | 1         |
| 13600W+11275N               | 1         | 10        | 3         | 86        | .4        | 12        | 11        | 421       | 3.56    | 3         | 5        | ND        | 5         | 21        | .3        | 2         | 2         | 77       | .37     | .038   | 9         | 24        | 1.00    | 124       | .19     | 2        | 2.15    | .02     | .25    | 3        | 1         |
| 13600W+11350N               | 1         | 19        | 2         | 82        | .3        | 16        | 10        | 370       | 3.12    | 2         | 5        | ND        | 4         | 23        | .2        | 2         | 2         | 62       | .39     | .040   | 10        | 30        | .84     | 121       | .17     | 2        | 2.17    | .02     | .10    | 1        | 1         |
| 13600W+11425N               | 2         | 40        | 8         | 52        | .2        | 20        | 12        | 226       | 3.35    | 5         | 5        | ND        | 3         | 9         | .3        | 2         | 3         | 72       | .28     | .027   | 7         | 41        | .64     | 65        | .10     | 2        | 1.54    | .03     | .06    | 3        | 1         |
| 13600W+11500N               | 1         | 15        | 7         | 85        | .5        | 8         | 72        | 8743      | 8.06    | 17        | 5        | ND        | 12        | 69        | .2        | 2         | 4         | 66       | 1.14    | .084   | 33        | 16        | .70     | 1223      | .10     | 2        | 1.71    | .01     | .21    | 1        | 3         |
| 13600W+11575N               | 1         | 12        | 4         | 75        | .1        | 10        | 12        | 1324      | 3.49    | 36        | 5        | ND        | 11        | 44        | .2        | 2         | 2         | 51       | .82     | .056   | 28        | 12        | .65     | 620       | .06     | 2        | 1.85    | .01     | .23    | 1        | 1         |
| 13600W+11650N               | 1         | 12        | 8         | 81        | .2        | 11        | 10        | 529       | 3.75    | 15        | 5        | ND        | 11        | 28        | .3        | 2         | 2         | 63       | .55     | .055   | 24        | 17        | .80     | 385       | .12     | 2        | 2.02    | .01     | .25    | 1        | 1         |
| 13600W+11725N               | 1         | 21        | 13        | 99        | .1        | 7         | 10        | 304       | 3.93    | 18        | 5        | ND        | 12        | 35        | .4        | 2         | 2         | 71       | .99     | .086   | 23        | 13        | .99     | 658       | .09     | 2        | 2.16    | .01     | .30    | 1        | 1         |
| 13600W+11800N               | 1         | 20        | 10        | 71        | .1        | 18        | 9         | 224       | 2.83    | 5         | 5        | ND        | 2         | 29        | .2        | 2         | 2         | 54       | .45     | .044   | 10        | 26        | .66     | 142       | .12     | 2        | 1.88    | .02     | .06    | 1        | 8         |
| 13600W+11875N               | 1         | 22        | 6         | 66        | .1        | 14        | 7         | 305       | 2.39    | 5         | 5        | ND        | 2         | 33        | .2        | 2         | 2         | 46       | .55     | .044   | 10        | 25        | .66     | 142       | .11     | 2        | 1.59    | .03     | .05    | 1        | 1         |
| 13600W+11950N               | 1         | 14        | 8         | 72        | .1        | 16        | 9         | 458       | 2.74    | 9         | 5        | ND        | 2         | 38        | .2        | 2         | 5         | 53       | .74     | .057   | 10        | 27        | .68     | 139       | .12     | 2        | 1.46    | .03     | .08    | 1        | 17        |
| 13600W+12025N               | 1         | 13        | 3         | 66        | .1        | 18        | 8         | 368       | 2.32    | 6         | 5        | ND        | 2         | 35        | .2        | 2         | 2         | 44       | .59     | .039   | 7         | 25        | .60     | 117       | .11     | 2        | 1.38    | .02     | .05    | 1        | 2         |

089-002

GEOCHEMICAL ANALYSIS CERTIFICATE

EASTFIELD RESOURCES LTD.

Project:

Sample Type: Soils/Rocks

Multi-element ICP Analysis - .500 gram sample is digested with 3 ml of aqua regia, diluted to 10 ml with Water. This leach is partial for Mn, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K and Al. Detection Limit for Au is 3 ppm. \*Au Analysis- 10 gram sample is digested with aqua regia, MIBK extracted, graphite furnace AA finished to 1 ppb detection.

Analyst RSam  
Report No. 9330556  
Date: August 12, 1993

Table with columns: ELEMENT, Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, W, Au+. Rows list various sample IDs (e.g., 7200W+11650N) and their corresponding element concentrations in ppm and ppb.

Ana = 99

Aztec = 11

Nice = 20

Morton = 1

089-002

GEOCHEMICAL ANALYSIS CERTIFICATE

Multi-element ICP Analysis - .500 gram sample is digested with 3 ml of aqua regia, diluted to 10 ml with Water. This leach is partial for Mn, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K and Al. Detection Limit for Au is 3 ppm. \*Au Analysis- 10 gram sample is digested with aqua regia, MIBK extracted, graphite furnace AA finished to 1 ppb detection.

Analyst RSan  
 Report No. 9320547  
 Date: July 27, 1993

EASTFIELD RESOURCES LTD.

Project:  
 Sample Type: Rocks

| ELEMENT SAMPLE      | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca %  | P %  | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au* ppb |
|---------------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------|--------|--------|--------|--------|--------|--------|-------|-------|------|--------|--------|------|--------|------|-------|------|------|-----|-------|---------|
| JC-93-K1            | 6      | 25     | 5      | 11     | .1     | 2      | 2      | 42     | 2.41 | 52     | 5     | ND     | 4      | 22     | .2     | 2      | 3      | 6     | .03   | .005 | 9      | 87     | .02  | 255    | .01  | 2     | .36  | .01  | .28 | 1     | 49      |
| JC-93-K2            | 5      | 20     | 14     | 42     | .3     | 3      | 1      | 171    | .87  | 137    | 5     | ND     | 16     | 5      | .6     | 3      | 2      | 3     | .02   | .004 | 23     | 81     | .06  | 95     | .01  | 2     | .46  | .08  | .17 | 1     | 1       |
| JC-93-K3            | 3      | 37     | 3      | 80     | .3     | 9      | 14     | 668    | 4.02 | 3      | 5     | ND     | 2      | 119    | .4     | 2      | 2      | 105   | 2.06  | .051 | 3      | 71     | 1.15 | 228    | .16  | 2     | 3.50 | .59  | .16 | 1     | 1       |
| JC-93-K5            | 5      | 14     | 19     | 3      | .1     | 2      | 1      | 35     | 1.46 | 4      | 5     | ND     | 14     | 25     | .2     | 2      | 4      | 4     | .05   | .010 | 26     | 103    | .04  | 193    | .01  | 2     | .44  | .04  | .35 | 1     | 1       |
| JC-93-K6            | 3      | 51     | 3      | 26     | .2     | 5      | 8      | 262    | 3.49 | 2      | 5     | ND     | 9      | 35     | .2     | 2      | 2      | 87    | .72   | .042 | 17     | 79     | 1.79 | 60     | .25  | 2     | 2.13 | .21  | .83 | 1     | 7       |
| JC-93-K7            | 7      | 37     | 7      | 4      | .1     | 4      | 5      | 66     | 3.33 | 131    | 5     | ND     | 3      | 11     | .2     | 3      | 2      | 6     | .12   | .008 | 6      | 128    | .05  | 18     | .01  | 6     | .45  | .01  | .25 | 1     | 91      |
| JC-93-K8            | 6      | 56     | 3      | 13     | .1     | 3      | 7      | 143    | 2.84 | 2      | 5     | ND     | 7      | 22     | .2     | 2      | 2      | 45    | .30   | .030 | 13     | 104    | .76  | 49     | .09  | 3     | 1.13 | .13  | .60 | 1     | 4       |
| JC-93-K9            | 4      | 18     | 14     | 3      | .2     | 3      | 6      | 31     | 1.78 | 107    | 5     | ND     | 3      | 7      | .2     | 4      | 2      | 7     | .02   | .004 | 17     | 95     | .04  | 72     | .01  | 10    | .48  | .01  | .28 | 1     | 89      |
| JC-93-K10           | 12     | 24     | 15     | 7      | .1     | 2      | 1      | 46     | 1.21 | 16     | 5     | ND     | 13     | 18     | .2     | 2      | 2      | 4     | .03   | .007 | 22     | 106    | .07  | 369    | .01  | 3     | .54  | .03  | .35 | 1     | 18      |
| JC-93-K11           | 23     | 11     | 14     | 2      | .3     | 2      | 1      | 30     | 1.88 | 15     | 5     | ND     | 11     | 12     | .2     | 3      | 2      | 4     | .02   | .007 | 16     | 91     | .04  | 207    | .01  | 3     | .42  | .01  | .48 | 1     | 52      |
| JC-93-K12           | 7      | 37     | 6      | 9      | .1     | 2      | 1      | 41     | 3.09 | 2      | 5     | ND     | 15     | 12     | .2     | 2      | 2      | 6     | .03   | .019 | 7      | 77     | .07  | 86     | .01  | 3     | .54  | .03  | .31 | 1     | 2       |
| JC-93-K15           | 3      | 32     | 3      | 54     | .1     | 33     | 13     | 567    | 3.10 | 2      | 5     | ND     | 10     | 35     | .4     | 2      | 2      | 64    | 1.03  | .044 | 15     | 189    | 1.47 | 366    | .28  | 2     | 1.89 | .24  | .89 | 1     | 18      |
| JC-93-K16           | 7      | 18     | 2      | 8      | .1     | 2      | 1      | 51     | 1.85 | 2      | 5     | ND     | 3      | 32     | .2     | 2      | 2      | 15    | .06   | .012 | 14     | 130    | .41  | 283    | .01  | 2     | .81  | .04  | .37 | 1     | 280     |
| JC-93-AC1           | 4      | 20     | 10     | 14     | .1     | 5      | 2      | 29     | 1.48 | 4      | 5     | ND     | 15     | 17     | .2     | 2      | 2      | 6     | .06   | .016 | 26     | 117    | .10  | 161    | .01  | 2     | .60  | .06  | .31 | 1     | 27      |
| JC-93-AC2           | 5      | 6      | 13     | 5      | .8     | 2      | 1      | 31     | 1.24 | 28     | 5     | ND     | 5      | 2      | .2     | 4      | 2      | 2     | .02   | .003 | 24     | 115    | .03  | 58     | .01  | 3     | .36  | .01  | .26 | 1     | 21      |
| JC-93-AC3           | 5      | 37     | 30     | 18     | 1.7    | 3      | 1      | 24     | 5.37 | 6      | 5     | ND     | 9      | 4      | .2     | 3      | 2      | 2     | .02   | .008 | 9      | 128    | .04  | 52     | .01  | 4     | .46  | .02  | .19 | 1     | 20      |
| JC-93-AC4           | 5      | 16     | 50     | 13     | 1.2    | 2      | 1      | 44     | .84  | 9      | 5     | ND     | 16     | 16     | .2     | 2      | 2      | 2     | .07   | .014 | 30     | 105    | .07  | 58     | .01  | 2     | .56  | .01  | .21 | 1     | 16      |
| JC-93-AC5           | 2      | 10     | 107    | 8      | .4     | 1      | 1      | 22     | .96  | 8      | 5     | ND     | 30     | 10     | .2     | 4      | 2      | 3     | .02   | .017 | 45     | 71     | .06  | 70     | .01  | 2     | .71  | .01  | .19 | 1     | 39      |
| JC-93-AZ1 <u>AZ</u> | 3      | 250    | 3      | 40     | .3     | 3      | 6      | 338    | 2.40 | 2      | 5     | ND     | 19     | 53     | .3     | 2      | 3      | 52    | .90   | .022 | 17     | 106    | .81  | 255    | .21  | 2     | 2.24 | .41  | .86 | 1     | 2       |
| JC-93-AZ2           | 6      | 7      | 3      | 44     | .1     | 4      | 8      | 418    | 3.01 | 2      | 5     | ND     | 11     | 50     | .2     | 2      | 2      | 60    | .89   | .026 | 14     | 115    | .91  | 251    | .22  | 2     | 2.24 | .37  | .82 | 1     | 1       |
| JC-93-AZ3           | 3      | 13     | 3      | 46     | .1     | 4      | 8      | 486    | 2.64 | 2      | 5     | ND     | 10     | 52     | .3     | 2      | 2      | 55    | 1.06  | .026 | 16     | 97     | .90  | 142    | .22  | 2     | 2.15 | .39  | .35 | 1     | 1       |
| JC-93-AZ4           | 4      | 4      | 2      | 42     | .1     | 4      | 4      | 458    | 2.18 | 2      | 5     | ND     | 16     | 60     | .3     | 3      | 2      | 45    | 1.09  | .024 | 25     | 101    | .92  | 44     | .18  | 2     | 1.72 | .05  | .10 | 1     | 1       |
| JC-93-AZ5           | 2      | 83     | 6      | 57     | .8     | 4      | 12     | 629    | 3.37 | 2      | 5     | ND     | 9      | 64     | .3     | 2      | 2      | 53    | 1.45  | .042 | 13     | 64     | 1.55 | 72     | .24  | 2     | 2.28 | .08  | .15 | 1     | 1       |
| JC-93-AZ6           | 9      | 13     | 129    | 301    | 2.4    | 3      | 4      | 448    | 2.05 | 16     | 5     | ND     | 19     | 8      | 21.2   | 2      | 2      | 28    | .12   | .012 | 13     | 132    | .58  | 65     | .07  | 2     | .96  | .09  | .45 | 1     | 12      |
| JC-93-AZ7 <u>AZ</u> | 4      | 13     | 13     | 58     | .1     | 3      | 1      | 175    | .87  | 12     | 5     | ND     | 15     | 8      | .4     | 4      | 2      | 6     | .07   | .015 | 17     | 97     | .08  | 80     | .01  | 2     | .46  | .09  | .16 | 1     | 22      |
| JC-93-A28           | 11     | 40     | 24     | 50     | .4     | 11     | 3      | 332    | 2.25 | 31     | 5     | ND     | 5      | 15     | .2     | 2      | 2      | 44    | .26   | .078 | 14     | 173    | .48  | 145    | .02  | 4     | 1.03 | .01  | .24 | 1     | 1       |
| JC-93-A29           | 14     | 35     | 4      | 57     | .1     | 10     | 14     | 628    | 4.66 | 6      | 5     | ND     | 3      | 49     | .4     | 2      | 2      | 103   | 1.50  | .044 | 9      | 71     | 1.59 | 62     | .18  | 5     | 1.83 | .19  | .10 | 1     | 5       |
| JC-93-A30           | 4      | 11     | 5      | 51     | .1     | 9      | 14     | 530    | 4.92 | 28     | 5     | ND     | 6      | 79     | .2     | 2      | 3      | 53    | 1.07  | .041 | 7      | 87     | 1.15 | 33     | .21  | 4     | 2.29 | .33  | .59 | 1     | 7       |
| 93-GR7              | 1      | 23     | 3      | 50     | .2     | 5      | 4      | 1550   | 4.47 | 13     | 5     | ND     | 2      | 476    | .2     | 2      | 2      | 43    | 16.40 | .143 | 6      | 11     | .88  | 41     | .01  | 2     | .44  | .02  | .05 | 1     | 1       |
| 93-GR8              | 3      | 68     | 2      | 21     | .1     | 14     | 9      | 315    | 2.15 | 2      | 5     | ND     | 2      | 187    | .2     | 2      | 2      | 70    | 1.91  | .054 | 3      | 63     | .61  | 56     | .22  | 2     | 2.52 | .66  | .20 | 1     | 1       |

*Kobee* *D-ina* *Z-Intec*

089-002

GEOCHEMICAL ANALYSIS CERTIFICATE

EASTFIELD RESOURCES LTD.

Multi-element ICP Analysis - .500 gram sample is digested with 3 ml of aqua regia, diluted to 10 ml with Water. This leach is partial for Mn, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K and Al. Detection Limit for Au is 3 ppm. \*Au Analysis- 10 gram sample is digested with aqua regia, MIBK extracted, graphite furnace AA finished to 1 ppb detection.

Analyst RSam  
 Report No. 9330569  
 Date: August 31, 1993

Project:  
 Sample Type: Soils/Rocks

| ELEMENT<br>SAMPLE | Mo     | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As   | U   | Au  | Th  | Sr  | Cd  | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B | Al   | Na  | K   | W   | Au* |
|-------------------|--------|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|------|-----|---|------|-----|-----|-----|-----|
|                   | ppm    | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm  | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | % | %    | %   | ppm | ppb |     |
| 8400W+9575N       | 3      | 16  | 19  | 86  | .2  | 15  | 8   | 338  | 2.43 | 16   | 5   | ND  | 10  | 42  | .2  | 2   | 2   | 49  | .63 | .054 | 14  | 26  | .63 | 187  | .12 | 2 | 1.65 | .02 | .07 | 2   | 3   |
| 8400W+9650N       | 4      | 16  | 17  | 79  | .1  | 15  | 9   | 544  | 2.80 | 21   | 5   | ND  | 8   | 40  | .2  | 2   | 2   | 54  | .63 | .063 | 14  | 27  | .64 | 164  | .13 | 2 | 1.60 | .02 | .08 | 1   | 55  |
| 8400W+9725N       | 7      | 13  | 25  | 85  | .3  | 14  | 7   | 302  | 2.62 | 22   | 5   | ND  | 8   | 38  | .2  | 2   | 2   | 50  | .58 | .048 | 13  | 25  | .61 | 206  | .10 | 2 | 1.82 | .02 | .05 | 1   | 9   |
| 8400W+9800N       | 11     | 24  | 40  | 122 | .6  | 18  | 11  | 986  | 3.34 | 43   | 8   | ND  | 6   | 58  | .3  | 2   | 2   | 58  | .79 | .061 | 36  | 29  | .62 | 328  | .08 | 2 | 2.28 | .02 | .08 | 1   | 1   |
| 8400W+9875N       | 9      | 18  | 32  | 121 | .7  | 17  | 13  | 1694 | 3.39 | 42   | 5   | ND  | 7   | 29  | .7  | 2   | 2   | 59  | .40 | .043 | 17  | 25  | .63 | 223  | .10 | 2 | 1.91 | .02 | .10 | 1   | 6   |
| 8400W+9950N       | AE 12  | 22  | 39  | 143 | .6  | 16  | 10  | 889  | 3.28 | 61   | 5   | ND  | 7   | 49  | .5  | 3   | 2   | 56  | .71 | .058 | 22  | 26  | .59 | 256  | .08 | 3 | 1.99 | .02 | .09 | 1   | 3   |
| 9800W+12100N      | K 1    | 33  | 139 | 726 | 2.0 | 20  | 8   | 792  | 3.31 | 654  | 5   | ND  | 2   | 56  | 2.0 | 16  | 2   | 47  | .81 | .078 | 50  | 30  | .63 | 187  | .07 | 2 | 2.14 | .02 | .10 | 1   | 28  |
| 9800W+12175N      | 1      | 23  | 141 | 284 | .5  | 16  | 10  | 807  | 2.98 | 221  | 5   | ND  | 8   | 27  | 1.1 | 10  | 2   | 47  | .35 | .043 | 29  | 25  | .48 | 116  | .10 | 3 | 1.57 | .02 | .06 | 1   | 40  |
| 9800W+12250N      | 1      | 29  | 114 | 248 | .7  | 19  | 11  | 1108 | 3.82 | 379  | 5   | ND  | 10  | 30  | 1.2 | 10  | 2   | 48  | .35 | .032 | 25  | 26  | .58 | 131  | .08 | 2 | 1.73 | .01 | .10 | 1   | 33  |
| 9800W+12325N      | 2      | 28  | 383 | 388 | 3.0 | 18  | 8   | 823  | 3.91 | 734  | 5   | ND  | 4   | 34  | 1.3 | 10  | 3   | 50  | .40 | .065 | 31  | 28  | .42 | 178  | .05 | 3 | 1.94 | .01 | .12 | 1   | 25  |
| 9800W+12400N      | 2      | 20  | 310 | 134 | 3.4 | 9   | 7   | 1401 | 1.85 | 262  | 5   | ND  | 2   | 27  | 1.8 | 4   | 3   | 36  | .29 | .061 | 33  | 16  | .10 | 95   | .03 | 2 | 1.05 | .02 | .05 | 1   | 24  |
| 9800W+12475N      | 3      | 31  | 133 | 255 | 1.3 | 19  | 13  | 1143 | 4.13 | 765  | 5   | ND  | 2   | 35  | 1.8 | 5   | 2   | 62  | .44 | .071 | 18  | 30  | .43 | 149  | .06 | 3 | 2.16 | .01 | .10 | 1   | 9   |
| 10200W+12100N     | 1      | 26  | 63  | 147 | .4  | 21  | 11  | 765  | 3.49 | 155  | 5   | ND  | 5   | 24  | .4  | 9   | 2   | 57  | .32 | .056 | 25  | 29  | .66 | 117  | .12 | 2 | 1.96 | .02 | .11 | 1   | 6   |
| 10200W+12175N     | 4      | 27  | 99  | 154 | 1.0 | 14  | 10  | 931  | 2.58 | 284  | 5   | ND  | 2   | 50  | 1.5 | 23  | 2   | 45  | .67 | .113 | 16  | 20  | .18 | 131  | .05 | 2 | .99  | .02 | .10 | 1   | 1   |
| 10200W+12250N     | 2      | 18  | 28  | 87  | .3  | 13  | 7   | 547  | 2.83 | 93   | 5   | ND  | 2   | 24  | .3  | 3   | 2   | 54  | .23 | .042 | 9   | 21  | .35 | 85   | .09 | 2 | 1.20 | .02 | .06 | 1   | 3   |
| 10200W+12325N     | 1      | 25  | 35  | 86  | .1  | 22  | 10  | 481  | 3.42 | 67   | 5   | ND  | 2   | 21  | .2  | 8   | 2   | 59  | .22 | .039 | 11  | 30  | .60 | 96   | .10 | 3 | 1.92 | .01 | .06 | 1   | 1   |
| 10200W+12400N     | 1      | 37  | 137 | 333 | 1.0 | 22  | 11  | 1461 | 4.04 | 1026 | 5   | ND  | 2   | 57  | 1.0 | 44  | 2   | 49  | .90 | .090 | 39  | 31  | .66 | 223  | .05 | 3 | 2.41 | .01 | .12 | 1   | 36  |
| 10200W+12475N     | 1      | 24  | 74  | 224 | .8  | 19  | 9   | 887  | 3.41 | 655  | 5   | ND  | 5   | 29  | .5  | 23  | 2   | 47  | .31 | .048 | 17  | 27  | .60 | 112  | .07 | 2 | 1.81 | .01 | .10 | 1   | 27  |
| JC93 K-24         | 3      | 28  | 67  | 27  | 3.1 | 5   | 5   | 100  | 2.52 | 30   | 5   | ND  | 9   | 30  | .4  | 5   | 2   | 11  | .05 | .024 | 25  | 53  | .04 | 1523 | .01 | 2 | .58  | .01 | .30 | 1   | 17  |
| JC93 K-25         | K 4    | 20  | 12  | 48  | .1  | 5   | 7   | 448  | 2.69 | 17   | 5   | ND  | 7   | 27  | .2  | 2   | 2   | 44  | .37 | .034 | 9   | 60  | .43 | 181  | .08 | 2 | 1.16 | .07 | .15 | 2   | 20  |
| JC93 A-54         | ANA 21 | 42  | 53  | 244 | .2  | 7   | 19  | 2515 | 5.04 | 77   | 21  | ND  | 19  | 9   | .6  | 6   | 4   | 34  | .12 | .029 | 53  | 48  | .03 | 472  | .01 | 3 | .66  | .01 | .25 | 4   | 1   |
| JC93 A-55         | 7      | 23  | 26  | 198 | .2  | 8   | 7   | 2201 | 2.58 | 21   | 5   | ND  | 19  | 23  | .7  | 3   | 2   | 39  | .27 | .030 | 27  | 55  | .20 | 465  | .07 | 2 | 1.05 | .05 | .33 | 1   | 1   |

Ana = 2      Koffee = 14      Aztec = 6

089-002

GEOCHEMICAL ANALYSIS CERTIFICATE

EASTFIELD RESOURCES LTD.

Project:

Sample Type: Soils

Multi-element ICP Analysis - .500 gram sample is digested with 3 ml of aqua regia, diluted to 10 ml with Water. This leach is partial for Mn, Fe, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K and Al. Detection Limit for Au is 3 ppm. \*Au Analysis- 10 gram sample is digested with aqua regia, MIBK extracted, graphite furnace AA finished to 1 ppb detection.

Analyst RS

Report No. 9310548

Date: July 27, 1993

Table with columns: ELEMENT, Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, W, Au\*. Rows list various sample IDs and their corresponding element concentrations in ppm and ppb.

106 Aztec

141 Kopee

| ELEMENT<br>SAMPLE | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Mo<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |    |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|----|
| 8800W+9275N       | 3         | 15        | 11        | 66        | .1        | 15        | 6         | 434     | 2.72      | 2        | 5         | ND        | 9         | 26        | .6        | 2         | 2        | 45      | .46    | .057      | 15        | 23      | .59       | 180     | .13      | 2       | 2.01    | .01    | .08      | 1         | 4  |
| 8800W+9350N       | 4         | 27        | 14        | 89        | .2        | 21        | 8         | 488     | 3.88      | 8        | 5         | ND        | 14        | 27        | .4        | 2         | 2        | 65      | .42    | .058      | 24        | 35      | .74       | 226     | .16      | 2       | 2.84    | .01    | .13      | 1         | 3  |
| 8800W+9425N       | 6         | 18        | 10        | 74        | .2        | 14        | 8         | 757     | 3.39      | 8        | 5         | ND        | 7         | 32        | .2        | 2         | 2        | 62      | .47    | .071      | 18        | 27      | .57       | 212     | .11      | 3       | 1.95    | .01    | .07      | 1         | 1  |
| 8800W+9500N       | 3         | 21        | 14        | 75        | .2        | 16        | 6         | 342     | 2.52      | 6        | 5         | ND        | 8         | 28        | .3        | 2         | 2        | 46      | .42    | .047      | 19        | 31      | .66       | 195     | .13      | 2       | 2.30    | .01    | .09      | 1         | 1  |
| 9600W+7025N       | 1         | 30        | 2         | 58        | .1        | 19        | 7         | 366     | 3.15      | 6        | 5         | ND        | 3         | 23        | .3        | 3         | 2        | 55      | .41    | .057      | 10        | 30      | .75       | 107     | .16      | 3       | 2.13    | .01    | .09      | 1         | 1  |
| 9600W+7100N       | 3         | 20        | 2         | 63        | .1        | 22        | 10        | 321     | 3.56      | 2        | 5         | ND        | 4         | 30        | .4        | 2         | 2        | 59      | .57    | .067      | 13        | 37      | .83       | 181     | .15      | 2       | 2.87    | .01    | .09      | 2         | 3  |
| 9600W+7175N       | 3         | 21        | 6         | 62        | .1        | 21        | 8         | 323     | 3.03      | 2        | 5         | ND        | 3         | 30        | .5        | 2         | 2        | 55      | .55    | .051      | 12        | 34      | .81       | 171     | .15      | 2       | 2.50    | .02    | .08      | 1         | 4  |
| 9600W+7250N       | 7         | 21        | 15        | 73        | .1        | 24        | 12        | 1195    | 3.33      | 2        | 5         | ND        | 2         | 32        | .8        | 2         | 2        | 59      | .50    | .053      | 12        | 29      | .58       | 173     | .11      | 3       | 2.20    | .02    | .07      | 1         | 1  |
| 9600W+7325N       | 1         | 23        | 5         | 71        | .1        | 24        | 9         | 458     | 3.35      | 2        | 5         | ND        | 5         | 26        | .2        | 2         | 2        | 62      | .49    | .059      | 12        | 31      | .81       | 116     | .17      | 6       | 2.08    | .02    | .12      | 1         | 2  |
| 9600W+7400N       | 1         | 31        | 6         | 60        | .3        | 19        | 10        | 471     | 3.13      | 3        | 5         | ND        | 4         | 29        | .4        | 2         | 2        | 55      | .41    | .041      | 14        | 32      | .69       | 147     | .15      | 3       | 2.23    | .02    | .09      | 1         | 7  |
| 9600W+7475N       | 1         | 9         | 2         | 34        | .1        | 7         | 2         | 100     | 1.04      | 2        | 5         | ND        | 2         | 11        | .3        | 3         | 2        | 29      | .07    | .030      | 2         | 11      | .08       | 41      | .07      | 2       | .33     | .02    | .03      | 1         | 1  |
| 9600W+7550N       | 1         | 37        | 4         | 65        | .1        | 24        | 10        | 293     | 3.26      | 13       | 5         | ND        | 5         | 25        | .2        | 2         | 2        | 60      | .47    | .050      | 14        | 32      | .81       | 133     | .17      | 2       | 2.49    | .02    | .10      | 2         | 1  |
| 9600W+7625N       | 1         | 30        | 5         | 59        | .1        | 14        | 6         | 317     | 2.75      | 2        | 5         | ND        | 5         | 28        | .2        | 2         | 2        | 52      | .56    | .067      | 16        | 28      | .81       | 111     | .18      | 2       | 1.89    | .02    | .13      | 1         | 6  |
| 9600W+7700N       | 8         | 29        | 6         | 77        | .1        | 17        | 9         | 456     | 3.25      | 5        | 5         | ND        | 5         | 34        | 1.8       | 2         | 2        | 59      | .61    | .037      | 14        | 26      | .90       | 166     | .16      | 3       | 2.42    | .02    | .16      | 3         | 1  |
| 9600W+7775N       | 4         | 30        | 4         | 73        | .1        | 18        | 9         | 507     | 3.51      | 9        | 5         | ND        | 6         | 22        | .2        | 2         | 2        | 63      | .40    | .056      | 11        | 30      | .82       | 131     | .17      | 4       | 2.65    | .01    | .13      | 1         | 2  |
| 9600W+7850N       | 12        | 39        | 5         | 75        | .1        | 21        | 7         | 535     | 3.24      | 2        | 5         | ND        | 4         | 29        | .4        | 2         | 2        | 60      | .54    | .057      | 14        | 27      | .79       | 158     | .15      | 3       | 2.35    | .02    | .10      | 7         | 1  |
| 9600W+7925N       | 15        | 45        | 5         | 91        | .1        | 16        | 9         | 562     | 3.21      | 11       | 5         | ND        | 3         | 35        | .8        | 2         | 2        | 59      | .60    | .058      | 14        | 30      | .80       | 185     | .14      | 5       | 2.50    | .02    | .07      | 1         | 1  |
| 9600W+8000N       | 11        | 32        | 6         | 74        | .1        | 19        | 10        | 853     | 3.06      | 5        | 5         | ND        | 2         | 35        | .2        | 2         | 2        | 55      | .59    | .063      | 15        | 28      | .73       | 155     | .12      | 2       | 2.27    | .02    | .06      | 2         | 1  |
| 9600W+8075N       | 4         | 29        | 4         | 65        | .1        | 19        | 7         | 409     | 3.30      | 9        | 5         | ND        | 3         | 24        | .2        | 2         | 2        | 57      | .41    | .045      | 12        | 31      | .78       | 146     | .14      | 3       | 2.50    | .01    | .07      | 2         | 2  |
| 9600W+8150N       | 2         | 35        | 13        | 71        | .1        | 22        | 9         | 495     | 3.12      | 2        | 5         | ND        | 2         | 31        | .2        | 2         | 2        | 57      | .52    | .052      | 15        | 33      | .74       | 167     | .14      | 2       | 2.34    | .02    | .07      | 1         | 1  |
| ✓9600W+8225N      | 7         | 37        | 10        | 63        | .3        | 20        | 10        | 764     | 2.98      | 2        | 5         | ND        | 2         | 25        | 1.2       | 2         | 2        | 50      | .29    | .088      | 19        | 26      | .43       | 118     | .05      | 3       | 2.10    | .02    | .05      | 1         | 1  |
| 9600W+8300N       | 3         | 71        | 5         | 67        | .1        | 16        | 11        | 344     | 3.82      | 2        | 5         | ND        | 6         | 23        | .3        | 2         | 2        | 69      | .49    | .059      | 14        | 34      | 1.00      | 155     | .18      | 2       | 3.17    | .02    | .14      | 1         | 2  |
| 9600W+8375N       | 5         | 22        | 2         | 42        | .1        | 7         | 3         | 102     | 1.76      | 2        | 5         | ND        | 2         | 27        | .2        | 2         | 2        | 34      | .31    | .063      | 13        | 21      | .20       | 110     | .07      | 2       | 1.04    | .02    | .05      | 1         | 1  |
| 9600W+8450N       | 9         | 26        | 8         | 65        | .1        | 15        | 6         | 477     | 2.77      | 2        | 5         | ND        | 2         | 46        | .6        | 3         | 2        | 57      | .69    | .070      | 12        | 28      | .52       | 188     | .09      | 2       | 1.63    | .02    | .06      | 1         | 1  |
| 9600W+8525N       | 5         | 25        | 6         | 90        | .1        | 20        | 10        | 369     | 3.64      | 2        | 5         | ND        | 4         | 28        | .2        | 2         | 2        | 68      | .51    | .048      | 10        | 30      | 1.05      | 144     | .18      | 2       | 2.60    | .02    | .08      | 2         | 1  |
| 9600W+8600N       | 9         | 50        | 2         | 74        | .1        | 23        | 9         | 428     | 3.63      | 3        | 5         | ND        | 4         | 29        | 1.3       | 2         | 2        | 66      | .49    | .059      | 17        | 36      | .93       | 196     | .15      | 4       | 2.86    | .02    | .09      | 1         | 1  |
| 9600W+8675N       | 10        | 42        | 9         | 72        | .1        | 22        | 11        | 613     | 3.44      | 2        | 5         | ND        | 6         | 29        | .2        | 2         | 2        | 69      | .51    | .057      | 17        | 32      | .88       | 172     | .16      | 2       | 2.64    | .02    | .11      | 2         | 4  |
| 9600W+8750N       | 10        | 25        | 3         | 86        | .1        | 14        | 10        | 505     | 3.32      | 2        | 5         | ND        | 4         | 32        | .8        | 2         | 2        | 61      | .56    | .054      | 13        | 27      | .86       | 201     | .14      | 3       | 2.55    | .02    | .08      | 1         | 13 |
| 9600W+8825N       | 6         | 23        | 7         | 76        | .1        | 14        | 7         | 466     | 2.99      | 2        | 5         | ND        | 4         | 27        | 1.2       | 2         | 2        | 57      | .49    | .054      | 10        | 24      | .81       | 141     | .15      | 2       | 2.19    | .02    | .09      | 3         | 13 |
| 9600W+8900N       | 9         | 30        | 3         | 66        | .1        | 20        | 7         | 449     | 2.89      | 4        | 5         | ND        | 3         | 33        | .2        | 2         | 2        | 56      | .50    | .060      | 13        | 27      | .76       | 173     | .13      | 2       | 2.22    | .02    | .07      | 1         | 1  |
| 9600W+8975N       | 8         | 24        | 2         | 70        | .1        | 21        | 8         | 279     | 3.19      | 2        | 5         | ND        | 4         | 26        | .6        | 2         | 2        | 66      | .51    | .056      | 13        | 27      | .80       | 139     | .15      | 2       | 2.32    | .02    | .09      | 4         | 4  |
| 9600W+9050N       | 12        | 19        | 3         | 50        | .1        | 10        | 16        | 2153    | 2.71      | 2        | 5         | ND        | 2         | 33        | .2        | 2         | 2        | 56      | .61    | .119      | 17        | 22      | .60       | 175     | .10      | 2       | 1.64    | .02    | .06      | 2         | 3  |
| 9600W+9125N       | 7         | 15        | 7         | 91        | .1        | 15        | 9         | 456     | 3.36      | 2        | 5         | ND        | 3         | 32        | .7        | 2         | 2        | 64      | .60    | .062      | 10        | 29      | .83       | 173     | .16      | 2       | 2.35    | .02    | .09      | 1         | 1  |
| 9600W+9200N       | 12        | 15        | 2         | 87        | .1        | 15        | 10        | 658     | 2.91      | 8        | 5         | ND        | 3         | 42        | .7        | 2         | 2        | 59      | .75    | .064      | 10        | 30      | .79       | 185     | .14      | 2       | 2.26    | .02    | .09      | 1         | 1  |
| 9600W+9275N       | 6         | 14        | 2         | 65        | .1        | 12        | 8         | 274     | 3.17      | 6        | 5         | ND        | 5         | 26        | .2        | 2         | 2        | 59      | .50    | .058      | 11        | 30      | .86       | 139     | .18      | 2       | 2.38    | .02    | .11      | 1         | 1  |

| ELEMENT<br>SAMPLE     | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-----------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 9600W+9350N           | 21        | 11        | 2         | 63        | .1        | 14        | 7         | 373       | 2.82    | 6         | 5        | ND        | 5         | 31        | .3        | 2         | 2         | 58       | .65     | .060   | 13        | 24        | .81     | 125       | .17     | 2        | 1.94    | .02     | .13    | 1        | 1         |
| 9600W+9425N           | 29        | 19        | 3         | 71        | .1        | 17        | 12        | 937       | 3.53    | 4         | 5        | ND        | 5         | 35        | .3        | 2         | 2         | 63       | .59     | .073   | 15        | 37        | .77     | 218       | .16     | 2        | 2.54    | .02     | .10    | 1        | 5         |
| 9600W+9500N <i>Az</i> | 47        | 16        | 4         | 63        | .3        | 13        | 10        | 1140      | 2.87    | 2         | 5        | ND        | 2         | 36        | .9        | 2         | 3         | 55       | .48     | .111   | 11        | 32        | .59     | 183       | .09     | 2        | 1.93    | .02     | .06    | 1        | 1         |
| 9800W+10600N <i>K</i> | 2         | 31        | 10        | 138       | .3        | 14        | 8         | 284       | 3.16    | 21        | 5        | ND        | 9         | 29        | .6        | 2         | 2         | 60       | .51     | .047   | 15        | 33        | .79     | 201       | .15     | 2        | 2.17    | .01     | .10    | 2        | 18        |
| 9800W+10675N          | 1         | 88        | 6         | 71        | .2        | 10        | 16        | 648       | 2.77    | 38        | 5        | ND        | 6         | 27        | .4        | 5         | 3         | 42       | .49     | .064   | 14        | 20        | .66     | 145       | .11     | 2        | 1.52    | .01     | .08    | 2        | 180       |
| 9800W+10750N          | 1         | 56        | 13        | 76        | .2        | 8         | 7         | 279       | 3.57    | 23        | 5        | ND        | 11        | 23        | .2        | 2         | 2         | 51       | .43     | .060   | 14        | 26        | .71     | 155       | .13     | 2        | 2.04    | .01     | .10    | 1        | 95        |
| 9800W+10825N          | 1         | 59        | 14        | 109       | .6        | 12        | 11        | 1991      | 2.89    | 27        | 5        | ND        | 2         | 82        | .5        | 3         | 2         | 37       | 1.51    | .120   | 38        | 21        | .40     | 538       | .05     | 6        | 1.55    | .01     | .06    | 1        | 5         |
| 9800W+10900N          | 2         | 28        | 18        | 95        | .5        | 7         | 33        | 8406      | 6.44    | 78        | 5        | ND        | 5         | 39        | .2        | 2         | 2         | 51       | .63     | .088   | 31        | 25        | .49     | 498       | .09     | 2        | 1.82    | .01     | .09    | 1        | 13        |
| 9800W+10975N          | 2         | 21        | 21        | 109       | .3        | 11        | 12        | 862       | 4.19    | 46        | 5        | ND        | 10        | 25        | .4        | 2         | 2         | 64       | .49     | .066   | 15        | 30        | .76     | 190       | .14     | 2        | 2.13    | .01     | .13    | 1        | 18        |
| 9800W+11050N          | 1         | 25        | 20        | 102       | .1        | 18        | 9         | 296       | 3.06    | 8         | 5        | ND        | 9         | 27        | .2        | 2         | 2         | 58       | .50     | .056   | 20        | 33        | .79     | 234       | .17     | 2        | 1.98    | .02     | .11    | 1        | 4         |
| 9800W+11125N          | 1         | 15        | 18        | 78        | .3        | 15        | 14        | 1375      | 3.36    | 17        | 5        | ND        | 6         | 35        | .5        | 2         | 2         | 58       | .62     | .067   | 12        | 32        | .73     | 244       | .12     | 2        | 2.14    | .01     | .09    | 1        | 6         |
| 9800W+11200N          | 1         | 17        | 23        | 67        | .5        | 10        | 7         | 648       | 2.63    | 11        | 5        | ND        | 2         | 37        | .9        | 2         | 2         | 42       | .57     | .106   | 11        | 32        | .52     | 266       | .07     | 4        | 1.72    | .01     | .06    | 1        | 1         |
| 9800W+11275N          | 2         | 25        | 15        | 92        | .5        | 16        | 9         | 762       | 3.16    | 19        | 5        | ND        | 4         | 38        | .2        | 2         | 2         | 53       | .70     | .070   | 23        | 25        | .72     | 276       | .11     | 5        | 1.98    | .01     | .10    | 1        | 2         |
| 9800W+11350N          | 1         | 29        | 20        | 98        | .2        | 18        | 8         | 797       | 3.22    | 20        | 5        | ND        | 4         | 41        | .2        | 2         | 2         | 54       | .68     | .056   | 27        | 25        | .67     | 305       | .12     | 4        | 1.97    | .02     | .10    | 1        | 4         |
| 9800W+11425N          | 2         | 21        | 10        | 41        | .1        | 7         | 3         | 168       | 2.14    | 2         | 5        | ND        | 2         | 15        | .5        | 2         | 2         | 41       | .12     | .059   | 7         | 19        | .24     | 50        | .08     | 2        | 1.24    | .02     | .05    | 1        | 1         |
| 9800W+11500N          | 1         | 33        | 72        | 221       | 2.0       | 13        | 8         | 1127      | 3.79    | 320       | 5        | ND        | 6         | 47        | .4        | 2         | 2         | 57       | .76     | .066   | 30        | 27        | .71     | 340       | .11     | 2        | 2.21    | .02     | .12    | 1        | 6         |
| 9800W+11575N          | 2         | 23        | 6         | 65        | .2        | 14        | 7         | 1230      | 2.22    | 2         | 5        | ND        | 2         | 21        | 1.3       | 2         | 2         | 42       | .21     | .095   | 7         | 19        | .20     | 118       | .05     | 2        | 1.19    | .01     | .04    | 1        | 2         |
| 9800W+11650N          | 2         | 27        | 40        | 190       | .4        | 16        | 8         | 878       | 3.58    | 138       | 5        | ND        | 5         | 40        | 1.0       | 3         | 2         | 59       | .68     | .052   | 17        | 28        | .71     | 262       | .12     | 2        | 2.02    | .01     | .11    | 1        | 5         |
| 9800W+11725N          | 2         | 33        | 24        | 85        | .2        | 20        | 6         | 566       | 2.88    | 42        | 5        | ND        | 2         | 38        | .8        | 2         | 2         | 54       | .47     | .047   | 21        | 30        | .40     | 191       | .09     | 2        | 1.72    | .01     | .05    | 1        | 1         |
| 9800W+11800N          | 2         | 44        | 68        | 533       | 1.8       | 23        | 8         | 719       | 3.35    | 458       | 5        | ND        | 2         | 42        | 3.3       | 20        | 2         | 48       | .69     | .062   | 32        | 35        | .69     | 210       | .09     | 5        | 2.25    | .01     | .10    | 1        | 13        |
| 9800W+11875N          | 2         | 17        | 40        | 351       | .1        | 20        | 6         | 508       | 3.81    | 137       | 5        | ND        | 4         | 21        | 2.1       | 3         | 2         | 66       | .27     | .036   | 11        | 34        | .64     | 124       | .15     | 3        | 1.94    | .01     | .09    | 1        | 2         |
| 9800W+11950N          | 1         | 23        | 38        | 135       | .7        | 23        | 10        | 395       | 3.07    | 94        | 5        | ND        | 8         | 26        | .6        | 24        | 2         | 49       | .46     | .045   | 21        | 32        | .71     | 122       | .15     | 4        | 1.88    | .02     | .14    | 1        | 2         |
| 9800W+12025N          | 2         | 31        | 435       | 262       | 4.5       | 16        | 7         | 449       | 3.62    | 437       | 5        | ND        | 5         | 21        | .2        | 25        | 2         | 48       | .30     | .047   | 17        | 33        | .63     | 108       | .11     | 3        | 1.96    | .01     | .11    | 1        | 27        |
| 9800W+12100N          | 1         | 26        | 24        | 102       | .8        | 15        | 7         | 387       | 2.91    | 64        | 5        | ND        | 2         | 25        | 1.0       | 4         | 2         | 45       | .32     | .068   | 16        | 28        | .51     | 107       | .09     | 2        | 1.59    | .01     | .07    | 1        | 1         |
| 10200W+10675N         | 2         | 26        | 20        | 115       | .4        | 3         | 42        | 4905      | 8.84    | 22        | 5        | ND        | 3         | 38        | 1.8       | 2         | 5         | 43       | .60     | .074   | 24        | 19        | .41     | 312       | .07     | 2        | 1.52    | .01     | .05    | 1        | 7         |
| 10200W+10750N         | 2         | 36        | 22        | 82        | .6        | 11        | 9         | 513       | 5.23    | 24        | 5        | ND        | 5         | 40        | .2        | 2         | 2         | 80       | .55     | .106   | 20        | 29        | .73     | 318       | .12     | 2        | 2.37    | .01     | .08    | 1        | 8         |
| 10200W+10825N         | 1         | 70        | 3         | 16        | .7        | 8         | 8         | 291       | 2.26    | 2         | 5        | ND        | 2         | 63        | .8        | 2         | 2         | 38       | .85     | .135   | 39        | 10        | .10     | 375       | .02     | 3        | .65     | .01     | .02    | 1        | 1         |
| 10200W+10900N         | 1         | 45        | 18        | 43        | .4        | 11        | 5         | 418       | 3.83    | 4         | 5        | ND        | 3         | 61        | .2        | 2         | 2         | 47       | .63     | .083   | 27        | 19        | .47     | 450       | .07     | 3        | 1.95    | .01     | .06    | 1        | 27        |
| 10200W+10975N         | 1         | 53        | 9         | 51        | .4        | 13        | 22        | 1527      | 1.80    | 4         | 5        | ND        | 2         | 90        | 1.4       | 3         | 2         | 21       | 1.22    | .121   | 43        | 10        | .23     | 529       | .03     | 3        | 1.15    | .01     | .05    | 1        | 1         |
| 10200W+11050N         | 1         | 39        | 8         | 55        | .4        | 14        | 11        | 711       | 3.34    | 17        | 5        | ND        | 7         | 42        | .4        | 2         | 2         | 45       | .46     | .052   | 43        | 20        | .57     | 322       | .09     | 3        | 1.99    | .01     | .09    | 1        | 20        |
| 10200W+11125N         | 1         | 32        | 15        | 74        | .4        | 12        | 11        | 1460      | 2.97    | 14        | 5        | ND        | 3         | 58        | .2        | 2         | 2         | 43       | .86     | .081   | 27        | 21        | .55     | 380       | .08     | 2        | 1.94    | .01     | .08    | 1        | 9         |
| 10200W+11200N         | 1         | 15        | 22        | 87        | .4        | 14        | 4         | 293       | 2.97    | 27        | 5        | ND        | 5         | 32        | .2        | 2         | 2         | 57       | .48     | .044   | 12        | 24        | .65     | 239       | .11     | 3        | 1.91    | .01     | .08    | 1        | 12        |
| 10200W+11275N         | 1         | 16        | 4         | 74        | .1        | 13        | 8         | 686       | 3.34    | 15        | 5        | ND        | 8         | 29        | .2        | 2         | 2         | 57       | .53     | .060   | 14        | 25        | .79     | 248       | .15     | 2        | 1.72    | .02     | .14    | 1        | 6         |
| 10200W+11350N         | 1         | 23        | 19        | 75        | .2        | 14        | 6         | 364       | 3.10    | 9         | 5        | ND        | 7         | 42        | .8        | 2         | 2         | 53       | .64     | .043   | 18        | 21        | .72     | 195       | .14     | 2        | 1.72    | .01     | .10    | 1        | 18        |
| 10200W+11425N         | 1         | 40        | 15        | 62        | .4        | 7         | 5         | 291       | 2.67    | 21        | 5        | ND        | 12        | 52        | .2        | 2         | 2         | 35       | .47     | .052   | 34        | 13        | .45     | 307       | .07     | 2        | 1.56    | .02     | .09    | 3        | 8         |

| ELEMENT<br>SAMPLE | M    | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Mo  | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg   | Ba  | Ti  | B   | Al   | Na  | K   | W   | Au  |
|-------------------|------|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|-----|
|                   | ppm  | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | %    | %    | ppm | ppm | %    | ppm | %   | ppm | %    | %   | %   | ppm | ppb |
| 10200W+11500N     | 2    | 27  | 21  | 87  | .6  | 15  | 6   | 553  | 2.45 | 35  | 5   | ND  | 3   | 52  | .8  | 2   | 2   | 45  | .73  | .041 | 15  | 25  | .56  | 264 | .11 | 2   | 1.63 | .02 | .09 | 1   | 5   |
| 10200W+11575N     | 2    | 48  | 15  | 216 | .9  | 31  | 8   | 1014 | 2.87 | 180 | 5   | ND  | 3   | 48  | .6  | 2   | 2   | 45  | .72  | .055 | 20  | 30  | .65  | 276 | .11 | 2   | 1.97 | .01 | .09 | 1   | 8   |
| 10200W+11650N     | 2    | 59  | 21  | 249 | 1.6 | 22  | 9   | 2031 | 2.94 | 383 | 5   | ND  | 2   | 78  | 2.5 | 7   | 2   | 44  | 1.39 | .122 | 28  | 24  | .43  | 285 | .06 | 2   | 1.29 | .01 | .05 | 1   | 5   |
| 10200W+11725N     | 1    | 51  | 26  | 136 | 1.2 | 20  | 7   | 961  | 1.63 | 66  | 8   | ND  | 2   | 98  | 2.9 | 8   | 2   | 22  | 1.57 | .098 | 61  | 16  | .32  | 498 | .04 | 2   | 1.25 | .01 | .07 | 1   | 3   |
| 10200W+11800N     | 2    | 69  | 68  | 320 | 2.1 | 20  | 5   | 1280 | 2.36 | 288 | 5   | ND  | 2   | 66  | 5.3 | 14  | 2   | 32  | 1.17 | .101 | 73  | 22  | .41  | 228 | .05 | 2   | 1.48 | .01 | .07 | 1   | 16  |
| 10200W+11875N     | 1    | 32  | 29  | 150 | .5  | 13  | 6   | 595  | 2.07 | 59  | 10  | ND  | 2   | 58  | .9  | 3   | 3   | 30  | 1.53 | .084 | 57  | 23  | .42  | 158 | .07 | 4   | 1.45 | .01 | .05 | 1   | 1   |
| 10200W+11950N     | 1    | 42  | 21  | 316 | 1.3 | 9   | 3   | 200  | 1.22 | 98  | 5   | ND  | 2   | 81  | 3.5 | 3   | 2   | 16  | 1.73 | .082 | 33  | 14  | .23  | 133 | .04 | 2   | .74  | .01 | .06 | 1   | 38  |
| 10200W+12025N     | 1    | 34  | 100 | 407 | 2.6 | 19  | 6   | 651  | 3.22 | 549 | 5   | ND  | 4   | 39  | 2.4 | 8   | 2   | 38  | .67  | .057 | 29  | 29  | .60  | 151 | .08 | 3   | 1.95 | .01 | .10 | 1   | 40  |
| 10200W+12100N     | 1    | 54  | 142 | 738 | 3.2 | 12  | 7   | 833  | 3.22 | 682 | 10  | ND  | 3   | 55  | 4.3 | 17  | 2   | 36  | 1.02 | .077 | 78  | 30  | .54  | 203 | .07 | 6   | 2.10 | .01 | .10 | 1   | 25  |
| 10400W+7000N      | AZ 4 | 18  | 6   | 76  | .2  | 12  | 7   | 351  | 3.11 | 2   | 5   | ND  | 4   | 33  | .2  | 2   | 2   | 57  | .60  | .042 | 12  | 29  | .85  | 184 | .15 | 2   | 2.34 | .02 | .12 | 2   | 1   |
| 10400W+7025N      | 5    | 23  | 3   | 76  | .2  | 9   | 9   | 472  | 3.28 | 2   | 5   | ND  | 4   | 39  | .4  | 2   | 2   | 59  | .70  | .052 | 17  | 29  | .85  | 175 | .14 | 6   | 2.47 | .02 | .10 | 1   | 16  |
| 10400W+7150N      | 11   | 29  | 10  | 71  | .3  | 12  | 8   | 511  | 3.28 | 2   | 6   | ND  | 4   | 34  | .7  | 2   | 3   | 60  | .60  | .060 | 20  | 30  | .78  | 174 | .13 | 3   | 2.42 | .02 | .08 | 1   | 8   |
| 10400W+7225N      | 8    | 21  | 2   | 63  | .1  | 6   | 9   | 428  | 3.31 | 2   | 5   | ND  | 4   | 21  | .3  | 2   | 2   | 60  | .36  | .035 | 10  | 27  | .75  | 113 | .16 | 2   | 2.22 | .01 | .09 | 3   | 9   |
| 10400W+7300N      | 11   | 30  | 2   | 73  | .2  | 13  | 5   | 352  | 2.92 | 2   | 5   | ND  | 4   | 40  | 1.5 | 2   | 2   | 53  | .67  | .061 | 14  | 25  | .75  | 187 | .12 | 2   | 2.30 | .02 | .12 | 1   | 1   |
| 10400W+7375N      | 13   | 33  | 6   | 72  | .2  | 10  | 8   | 594  | 3.00 | 2   | 5   | ND  | 3   | 48  | .2  | 2   | 2   | 54  | .84  | .060 | 20  | 29  | .75  | 196 | .12 | 4   | 2.29 | .02 | .07 | 1   | 1   |
| 10400W+7450N      | 21   | 45  | 8   | 75  | .2  | 17  | 9   | 620  | 3.37 | 4   | 5   | ND  | 4   | 31  | .6  | 2   | 2   | 60  | .58  | .051 | 15  | 30  | .80  | 174 | .15 | 2   | 2.43 | .02 | .09 | 3   | 1   |
| 10400W+7525N      | 22   | 30  | 4   | 78  | .2  | 14  | 9   | 462  | 3.29 | 2   | 5   | ND  | 4   | 34  | 1.1 | 2   | 2   | 60  | .65  | .035 | 10  | 27  | .82  | 147 | .16 | 3   | 2.19 | .02 | .10 | 1   | 1   |
| 10400W+7600N      | 18   | 32  | 2   | 80  | .2  | 13  | 9   | 656  | 3.47 | 2   | 5   | ND  | 3   | 35  | .6  | 2   | 2   | 62  | .65  | .056 | 14  | 32  | .86  | 182 | .14 | 2   | 2.45 | .02 | .08 | 1   | 1   |
| 10400W+7675N      | 16   | 24  | 3   | 93  | .2  | 16  | 8   | 416  | 3.65 | 3   | 5   | ND  | 3   | 34  | .9  | 3   | 2   | 68  | .69  | .048 | 9   | 31  | .94  | 214 | .16 | 2   | 2.36 | .02 | .07 | 1   | 1   |
| 10400W+7750N      | 22   | 22  | 3   | 78  | .2  | 6   | 8   | 380  | 3.48 | 2   | 5   | ND  | 6   | 34  | 1.0 | 2   | 2   | 68  | .78  | .036 | 16  | 24  | 1.00 | 165 | .18 | 2   | 2.33 | .02 | .15 | 1   | 1   |
| 10400W+7825N      | 16   | 43  | 9   | 81  | .2  | 16  | 10  | 409  | 3.81 | 2   | 5   | ND  | 8   | 31  | .2  | 2   | 2   | 81  | .76  | .055 | 20  | 30  | 1.03 | 197 | .18 | 2   | 2.70 | .02 | .21 | 1   | 1   |
| 10400W+7900N      | 16   | 22  | 2   | 77  | .2  | 17  | 9   | 546  | 3.72 | 2   | 5   | ND  | 3   | 32  | .7  | 3   | 2   | 69  | .70  | .051 | 17  | 31  | .93  | 189 | .15 | 2   | 2.44 | .01 | .08 | 1   | 6   |
| 10400W+7975N      | 17   | 23  | 10  | 74  | .1  | 15  | 9   | 574  | 3.86 | 2   | 5   | ND  | 4   | 25  | .7  | 2   | 2   | 69  | .50  | .048 | 14  | 32  | .89  | 146 | .16 | 2   | 2.46 | .01 | .09 | 2   | 1   |
| 10400W+8050N      | 13   | 27  | 8   | 71  | .2  | 24  | 12  | 581  | 3.84 | 6   | 5   | ND  | 3   | 28  | .2  | 2   | 2   | 68  | .55  | .052 | 13  | 33  | .89  | 155 | .16 | 2   | 2.40 | .02 | .09 | 2   | 1   |
| 10400W+8125N      | 5    | 29  | 11  | 74  | .1  | 24  | 10  | 576  | 4.14 | 8   | 5   | ND  | 4   | 26  | 1.2 | 2   | 2   | 70  | .53  | .050 | 15  | 37  | .95  | 131 | .17 | 3   | 2.56 | .01 | .08 | 1   | 1   |
| 10400W+8200N      | 7    | 34  | 4   | 81  | .1  | 21  | 10  | 644  | 4.16 | 2   | 5   | ND  | 3   | 29  | .9  | 2   | 2   | 73  | .62  | .060 | 12  | 37  | .91  | 128 | .17 | 3   | 2.21 | .01 | .10 | 1   | 1   |
| 10400W+8275N      | 3    | 32  | 2   | 68  | .2  | 19  | 9   | 453  | 3.46 | 7   | 5   | ND  | 4   | 27  | .2  | 2   | 2   | 66  | .55  | .060 | 13  | 32  | .81  | 116 | .17 | 2   | 1.76 | .02 | .09 | 2   | 6   |
| 10400W+8350N      | 16   | 50  | 7   | 87  | .2  | 19  | 8   | 742  | 3.74 | 2   | 5   | ND  | 2   | 29  | 1.3 | 2   | 2   | 67  | .47  | .075 | 9   | 34  | .73  | 123 | .14 | 4   | 1.84 | .02 | .09 | 1   | 1   |
| 10400W+8425N      | 3    | 90  | 12  | 63  | .2  | 29  | 10  | 507  | 3.93 | 5   | 5   | ND  | 3   | 21  | .8  | 2   | 2   | 67  | .36  | .036 | 12  | 37  | .82  | 91  | .16 | 3   | 2.51 | .01 | .08 | 1   | 1   |
| 10400W+8500N      | 1    | 24  | 5   | 62  | .1  | 23  | 7   | 320  | 3.11 | 4   | 5   | ND  | 3   | 29  | .2  | 2   | 2   | 53  | .45  | .062 | 16  | 32  | .79  | 119 | .16 | 2   | 2.15 | .02 | .09 | 1   | 1   |
| 10400W+8575N      | 3    | 80  | 5   | 73  | .1  | 25  | 10  | 732  | 3.77 | 13  | 5   | ND  | 3   | 32  | .7  | 2   | 2   | 60  | .53  | .085 | 23  | 29  | .81  | 137 | .12 | 2   | 2.29 | .03 | .10 | 2   | 1   |
| 10400W+8650N      | 5    | 44  | 3   | 73  | .1  | 19  | 11  | 625  | 3.76 | 2   | 5   | ND  | 6   | 28  | .2  | 2   | 2   | 65  | .51  | .062 | 21  | 31  | .94  | 154 | .16 | 2   | 2.58 | .02 | .14 | 1   | 5   |
| 10400W+8725N      | 2    | 28  | 2   | 73  | .1  | 16  | 8   | 499  | 3.90 | 4   | 5   | ND  | 9   | 28  | .5  | 2   | 2   | 69  | .62  | .061 | 20  | 30  | 1.01 | 161 | .18 | 2   | 2.48 | .02 | .22 | 1   | 3   |
| 10400W+8800N      | 2    | 19  | 5   | 78  | .1  | 18  | 10  | 324  | 3.78 | 5   | 5   | ND  | 10  | 24  | .2  | 2   | 2   | 71  | .50  | .044 | 15  | 29  | 1.01 | 154 | .19 | 2   | 2.76 | .02 | .18 | 1   | 2   |
| 10400W+8900N      | 9    | 29  | 2   | 78  | .2  | 25  | 10  | 358  | 3.49 | 8   | 5   | ND  | 7   | 28  | 1.0 | 2   | 2   | 68  | .44  | .049 | 25  | 33  | .87  | 214 | .16 | 2   | 2.80 | .02 | .11 | 1   | 1   |

| ELEMENT<br>SAMPLE      | M<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |    |
|------------------------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|----|
| 10400W+8975N           | 4        | 20        | 2         | 64        | .1        | 16        | 8         | 566       | 3.40    | 2         | 5        | ND        | 6         | 28        | .3        | 2         | 2        | 61      | .52    | .053      | 13        | 27      | .86       | 144     | .17      | 2       | 2.16    | .02    | .12      | 1         | 12 |
| 10400W+9050N           | 8        | 27        | 3         | 71        | .2        | 15        | 8         | 551       | 3.76    | 11        | 5        | ND        | 8         | 26        | 1.2       | 2         | 2        | 65      | .49    | .045      | 16        | 30      | .92       | 156     | .16      | 3       | 2.41    | .02    | .15      | 1         | 3  |
| 10400W+9125N           | 10       | 24        | 3         | 64        | .1        | 19        | 9         | 737       | 3.74    | 2         | 5        | ND        | 8         | 25        | .2        | 2         | 2        | 67      | .50    | .061      | 22        | 29      | .98       | 160     | .19      | 2       | 2.42    | .02    | .22      | 1         | 1  |
| 10400W+9200N           | 21       | 22        | 4         | 66        | .1        | 18        | 7         | 420       | 3.26    | 2         | 5        | ND        | 7         | 23        | .3        | 2         | 2        | 59      | .44    | .055      | 15        | 27      | .81       | 119     | .16      | 4       | 2.33    | .02    | .12      | 2         | 1  |
| 10400W+9275N           | 26       | 28        | 8         | 56        | .2        | 9         | 8         | 280       | 3.24    | 5         | 5        | ND        | 10        | 24        | 1.6       | 2         | 2        | 73      | .47    | .046      | 19        | 31      | .94       | 150     | .19      | 2       | 2.61    | .02    | .19      | 1         | 2  |
| 10400W+9350N           | 15       | 28        | 2         | 55        | .1        | 11        | 9         | 420       | 3.50    | 2         | 5        | ND        | 8         | 29        | 1.1       | 2         | 2        | 64      | .55    | .061      | 21        | 30      | .88       | 162     | .19      | 6       | 2.21    | .02    | .19      | 3         | 8  |
| 10400W+9425N           | 14       | 29        | 4         | 58        | .1        | 12        | 10        | 714       | 3.57    | 2         | 5        | ND        | 8         | 29        | .2        | 2         | 2        | 64      | .55    | .062      | 19        | 33      | .86       | 183     | .18      | 6       | 2.20    | .02    | .21      | 2         | 1  |
| 10400W+9500N <i>12</i> | 9        | 21        | 2         | 56        | .2        | 14        | 8         | 466       | 3.19    | 2         | 5        | ND        | 7         | 25        | 1.6       | 2         | 2        | 57      | .48    | .061      | 15        | 31      | .83       | 152     | .17      | 3       | 2.22    | .02    | .15      | 3         | 1  |
| 11000W+10675N <i>K</i> | 1        | 24        | 3         | 64        | .1        | 14        | 9         | 408       | 3.81    | 2         | 5        | ND        | 8         | 29        | .8        | 2         | 2        | 62      | .53    | .052      | 16        | 36      | .80       | 172     | .18      | 3       | 2.34    | .02    | .09      | 2         | 1  |
| 11000W+10750N          | 1        | 15        | 2         | 66        | .2        | 19        | 8         | 460       | 2.96    | 2         | 5        | ND        | 5         | 30        | 1.3       | 2         | 2        | 58      | .53    | .056      | 12        | 29      | .75       | 116     | .16      | 5       | 1.93    | .02    | .12      | 1         | 1  |
| 11000W+10825N          | 2        | 16        | 9         | 85        | .2        | 10        | 11        | 1034      | 3.41    | 9         | 5        | ND        | 6         | 23        | .4        | 3         | 2        | 62      | .42    | .050      | 10        | 28      | .83       | 112     | .17      | 4       | 2.12    | .02    | .14      | 2         | 3  |
| 11000W+10900N          | 2        | 17        | 121       | 105       | .8        | 13        | 21        | 1353      | 3.94    | 23        | 5        | ND        | 4         | 28        | .9        | 2         | 2        | 52      | .39    | .075      | 20        | 36      | .56       | 171     | .11      | 5       | 2.34    | .01    | .08      | 1         | 2  |
| 11000W+10975N          | 4        | 12        | 50        | 84        | .3        | 8         | 4         | 271       | 2.61    | 17        | 5        | ND        | 2         | 13        | .5        | 2         | 2        | 54      | .17    | .032      | 8         | 22      | .37       | 55      | .12      | 5       | 1.53    | .01    | .06      | 2         | 13 |
| 11000W+11050N          | 12       | 23        | 25        | 105       | .6        | 9         | 10        | 722       | 2.54    | 10        | 5        | ND        | 2         | 53        | .6        | 2         | 2        | 47      | 1.00   | .065      | 24        | 23      | .49       | 202     | .10      | 2       | 1.66    | .01    | .07      | 1         | 1  |
| 11000W+11125N          | 4        | 13        | 6         | 25        | .3        | 6         | 2         | 73        | .92     | 2         | 5        | ND        | 2         | 20        | .6        | 2         | 2        | 15      | .24    | .065      | 8         | 10      | .07       | 92      | .03      | 4       | .40     | .02    | .03      | 1         | 2  |
| 11000W+11200N          | 4        | 17        | 13        | 78        | .2        | 15        | 7         | 235       | 3.34    | 5         | 5        | ND        | 8         | 25        | .2        | 2         | 2        | 59      | .42    | .044      | 14        | 31      | .74       | 131     | .17      | 6       | 2.19    | .01    | .11      | 2         | 4  |
| 11000W+11275N          | 11       | 15        | 17        | 69        | .3        | 12        | 5         | 292       | 4.78    | 14        | 5        | ND        | 4         | 27        | .2        | 2         | 2        | 62      | .49    | .060      | 12        | 24      | .59       | 136     | .14      | 5       | 1.67    | .01    | .09      | 2         | 8  |
| 11000W+11350N          | 4        | 50        | 5         | 71        | .2        | 8         | 9         | 376       | 3.54    | 3         | 5        | ND        | 5         | 32        | .9        | 2         | 2        | 45      | .46    | .058      | 13        | 25      | .62       | 161     | .12      | 2       | 1.92    | .01    | .09      | 2         | 4  |
| 11000W+11425N          | 3        | 38        | 5         | 75        | .1        | 13        | 12        | 712       | 3.30    | 10        | 5        | ND        | 5         | 26        | .8        | 2         | 2        | 55      | .43    | .054      | 12        | 28      | .69       | 143     | .15      | 2       | 2.01    | .01    | .10      | 2         | 1  |
| 11000W+11500N          | 5        | 115       | 25        | 133       | .4        | 12        | 8         | 454       | 2.70    | 88        | 5        | ND        | 5         | 44        | .3        | 3         | 2        | 44      | .67    | .049      | 19        | 27      | .61       | 207     | .13      | 4       | 1.85    | .01    | .11      | 2         | 21 |
| 11000W+11575N          | 3        | 40        | 28        | 130       | .7        | 13        | 6         | 579       | 2.49    | 82        | 5        | ND        | 3         | 60        | 1.7       | 5         | 2        | 39      | .88    | .068      | 23        | 30      | .52       | 228     | .10      | 4       | 1.84    | .01    | .10      | 1         | 9  |
| 11000W+11650N          | 1        | 26        | 32        | 183       | .7        | 19        | 8         | 701       | 2.49    | 105       | 5        | ND        | 5         | 41        | 2.8       | 4         | 2        | 35      | .69    | .055      | 19        | 27      | .51       | 185     | .11      | 2       | 1.82    | .01    | .10      | 2         | 91 |
| 11000W+11725N          | 3        | 78        | 25        | 205       | 1.2       | 24        | 18        | 4227      | 2.17    | 118       | 5        | ND        | 2         | 88        | 4.0       | 4         | 2        | 26      | 1.42   | .117      | 40        | 23      | .29       | 348     | .04      | 5       | 1.06    | .01    | .04      | 1         | 14 |
| 11000W+11800N          | 8        | 55        | 50        | 148       | .9        | 14        | 23        | 2060      | 4.76    | 133       | 5        | ND        | 2         | 40        | 2.3       | 8         | 2        | 45      | .56    | .089      | 28        | 26      | .35       | 251     | .05      | 5       | 1.44    | .01    | .05      | 1         | 12 |
| ✓11000W+11875N         | 4        | 40        | 27        | 120       | .5        | 9         | 11        | 1088      | 1.52    | 65        | 5        | ND        | 2         | 59        | 1.7       | 3         | 2        | 18      | .91    | .101      | 41        | 13      | .20       | 302     | .03      | 7       | .73     | .01    | .04      | 1         | 9  |
| ✓11000W+11950N         | 14       | 69        | 47        | 126       | 1.1       | 12        | 58        | 4179      | 3.80    | 225       | 7        | ND        | 2         | 61        | 2.0       | 3         | 2        | 36      | .88    | .135      | 45        | 20      | .16       | 343     | .03      | 6       | .82     | .01    | .03      | 1         | 8  |
| 11000W+12025N          | 13       | 48        | 25        | 72        | .3        | 16        | 18        | 910       | 4.27    | 33        | 5        | ND        | 7         | 25        | .7        | 2         | 2        | 55      | .29    | .050      | 14        | 32      | .55       | 153     | .11      | 5       | 2.06    | .01    | .09      | 1         | 83 |
| 11000W+12100N          | 7        | 48        | 17        | 39        | .3        | 12        | 4         | 112       | 1.26    | 16        | 5        | ND        | 2         | 24        | .4        | 2         | 2        | 20      | .21    | .050      | 13        | 13      | .13       | 143     | .02      | 2       | .68     | .01    | .05      | 1         | 14 |
| 11000W+12175N          | 3        | 25        | 68        | 184       | .6        | 14        | 4         | 395       | 3.04    | 122       | 5        | ND        | 3         | 36        | .9        | 2         | 2        | 45      | .50    | .055      | 14        | 31      | .59       | 194     | .09      | 3       | 2.29    | .01    | .09      | 2         | 17 |
| 11000W+12250N          | 2        | 49        | 43        | 171       | .8        | 20        | 12        | 2028      | 2.34    | 63        | 6        | ND        | 2         | 67        | 1.8       | 2         | 2        | 32      | 1.12   | .090      | 26        | 25      | .38       | 251     | .05      | 2       | 1.59    | .01    | .06      | 1         | 3  |
| 11000W+12325N          | 4        | 24        | 20        | 92        | .4        | 16        | 10        | 1463      | 3.66    | 73        | 5        | ND        | 4         | 36        | .9        | 3         | 2        | 39      | .54    | .083      | 18        | 29      | .56       | 210     | .10      | 2       | 1.55    | .01    | .09      | 1         | 16 |
| 11000W+12400N          | 5        | 51        | 30        | 81        | 1.1       | 12        | 13        | 1475      | 2.25    | 63        | 5        | ND        | 2         | 45        | 2.2       | 4         | 2        | 31      | .56    | .111      | 24        | 22      | .30       | 307     | .04      | 4       | 1.42    | .01    | .05      | 1         | 11 |
| 11000W+12475N          | 5        | 41        | 31        | 92        | .7        | 13        | 7         | 828       | 2.42    | 58        | 5        | ND        | 2         | 48        | 1.4       | 5         | 2        | 35      | .72    | .094      | 21        | 26      | .49       | 305     | .08      | 2       | 1.75    | .01    | .08      | 2         | 23 |
| 11000W+12550N          | 3        | 39        | 23        | 61        | 1.0       | 13        | 5         | 366       | 2.27    | 30        | 5        | ND        | 2         | 41        | .8        | 4         | 2        | 35      | .52    | .093      | 18        | 28      | .45       | 268     | .07      | 4       | 1.83    | .01    | .08      | 1         | 98 |
| 11000W+12625N          | 4        | 33        | 13        | 46        | .1        | 5         | 5         | 696       | 2.12    | 19        | 5        | ND        | 2         | 27        | 1.0       | 2         | 2        | 41      | .30    | .040      | 17        | 18      | .30       | 139     | .10      | 2       | 1.07    | .01    | .06      | 1         | 13 |

| ELEMENT<br>SAMPLE | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Ca<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Au<br>ppb |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-----------|
| 12200W+12925N     | 2         | 16        | 22        | 82        | .3        | 16        | 7         | 397       | 2.81    | 36        | 5        | ND        | 4         | 26        | 1.0       | 2         | 2         | 51       | .34     | .032   | 14        | 27        | .54     | 146       | .10     | 2        | 1.86    | .01     | .07    | 1        | 2         |
| 12200W+13000N     | 2         | 15        | 20        | 78        | .4        | 7         | 4         | 235       | 2.74    | 33        | 5        | ND        | 5         | 21        | .5        | 2         | 2         | 54       | .21     | .020   | 14        | 26        | .51     | 115       | .11     | 2        | 1.87    | .01     | .07    | 1        | 1         |
| 12200W+13075N     | 2         | 14        | 17        | 81        | .3        | 15        | 9         | 401       | 3.54    | 70        | 5        | ND        | 9         | 18        | .5        | 4         | 2         | 57       | .26     | .027   | 14        | 27        | .60     | 102       | .12     | 2        | 2.13    | .01     | .07    | 1        | 7         |
| JC-93-AZ-8        | 7         | 20        | 4         | 65        | .1        | 6         | 9         | 508       | 3.86    | 2         | 6        | ND        | 7         | 28        | .2        | 2         | 2         | 78       | .66     | .053   | 15        | 21        | .90     | 107       | .17     | 2        | 2.36    | .03     | .19    | 6        | 1         |
| JC-93-K-4         | 3         | 72        | 12        | 73        | .3        | 13        | 13        | 284       | 4.11    | 2         | 5        | ND        | 2         | 67        | .3        | 2         | 2         | 105      | .82     | .024   | 5         | 35        | 1.08    | 171       | .14     | 2        | 3.80    | .10     | .15    | 1        | 7         |
| ✓JC-93-K-13       | 3         | 71        | 15        | 49        | .4        | 5         | 5         | 319       | 3.48    | 28        | 5        | ND        | 9         | 37        | .8        | 2         | 2         | 43       | .40     | .046   | 22        | 13        | .56     | 255       | .09     | 2        | 2.00    | .01     | .12    | 1        | 10        |
| ✓JC-93-K-14       | 2         | 42        | 12        | 41        | .2        | 4         | 2         | 201       | 4.31    | 34        | 5        | ND        | 9         | 32        | .2        | 2         | 2         | 39       | .36     | .049   | 19        | 12        | .47     | 219       | .08     | 2        | 1.62    | .01     | .09    | 1        | 15        |

Samples with ✓ mark are prepared -35 mesh.

JC Series are silts.

APPENDIX 5

ROCK SAMPLE DESCRIPTIONS

AZTEC ROCK SAMPLE DESCRIPTIONS

| <u>Sample No.</u> | <u>Location</u>   | <u>Rock Type</u>  | <u>Description</u>                                                                                                                                                                                                                                               | <u>Geochem</u><br><u>(Cu/Au/Mo)</u><br><u>(ppm/ppb/ppm)</u> |
|-------------------|-------------------|-------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------|
| JC-93-AZ-1        | L9670W/<br>8350N  | Grano-<br>Diorite | Medium grained-coarse grained, fresh, weakly oxidized on weathered surface. No visible sulfides.                                                                                                                                                                 | 250/2/3                                                     |
| JC-93-AZ-2        | L10220W/<br>8750N | Grano-<br>Diorite | Medium grained coarse grained fresh, weakly oxidized on weathered surface. No visible sulfides.                                                                                                                                                                  | 7/1/6                                                       |
| JC-93-AZ-3        | L10360W/<br>7800N | Grano-<br>Diorite | Medium grained coarse grained fresh, weakly oxidized on weathered surface. No visible sulfides.                                                                                                                                                                  | 13/1/3                                                      |
| JC-93-AZ-4        | L10000W/<br>7700N | Grano-<br>Diorite | Coarse grained, weak chlorite-epidote-alteration peripheral to small vein.                                                                                                                                                                                       | 4/1/4                                                       |
| JC-93-AZ-5        | L9140/<br>8300N   | Diorite           | Strongly chloritic, pervasive hairline fracturing, dark green fine grained to medium grained, locally brecciated (fragments of angular quartz in very fine grained greenish matrix) propylitic alteration, secondary biotite after hornblende. Trace -1% pyrite. | 83/1/2                                                      |
| JC-93-AZ-6        | L9000W/<br>8300N  | Grano-<br>Diorite | Coarse grained limonitic, weak chlorite alteration, trace -1% fine grained disseminated pyrite.                                                                                                                                                                  | 13/12/9                                                     |
| JC-93-AZ-7        | L9020W/<br>8450N  | Latite            | Weakly foliated dyke 33 <sup>5</sup> /80S, 20 m wide, weakly limonitic.                                                                                                                                                                                          | 13/22/4                                                     |

APPENDIX 6

GEOPHYSICAL REPORT, SCOTT GEOPHYSICS LTD.

GEOPHYSICAL REPORT  
INDUCED POLARIZATION AND MAGNETOMETER SURVEYS

AZTEC PROPERTY  
CASINO AREA, YUKON

on behalf of

EASTFIELD RESOURCES LTD.  
110 - 325 Howe Street  
Vancouver, B.C. V6C 1Z7

Field work completed: July 13 to 17, 1993

by

Alan Scott, Geophysicist  
SCOTT GEOPHYSICS LTD.  
4013 West 14th Avenue  
Vancouver, B.C. V6R 2X3

December 10, 1993

TABLE OF CONTENTS

|                   | page |
|-------------------|------|
| 1 Introduction    | 1    |
| 2 Survey coverage | 1    |
| 3 Personnel       | 1    |
| 4 Instrumentation | 2    |
| 5 Recommendations | 2    |

Appendix

|                             |                |
|-----------------------------|----------------|
| Statement of Qualifications | rear of report |
|-----------------------------|----------------|

Maps accompanying report

|                                       |          |
|---------------------------------------|----------|
| Stacked IP/resistivity pseudosections | map roll |
| Chargeability contour plan            | map roll |
| Resistivity contour plan              | map roll |
| Magnetometer contour plan             | map roll |

## 1. INTRODUCTION

Induced polarization/resistivity and magnetometer surveys were performed on the Aztec Property, Casino Area, Yukon, in the period July 13 to 17, 1993. The surveys were conducted by Scott Geophysics Ltd. on behalf of Eastfield Resources Ltd.

The induced polarization survey was of a reconnaissance nature, with an interline spacing of 800 meters. The magnetometer survey included intermediate lines.

The pole dipole array was used for the induced polarization survey, with an "a" spacing of 75 meters and "n" separations of 1, 2, 3, and 4. The current electrode was to the north of the receiving electrodes on all survey lines.

Magnetometer readings were taken at 25 meter intervals and all values were corrected for diurnal variation with reference to a fixed base station.

This report describes the instrumentation and procedures and presents the results of those surveys.

## 2. SURVEY LOCATION AND COVERAGE

The Aztec Property is located southwest of the Casino Property, Yukon.

Induced polarization survey coverage totalled 8.2 kms and magnetometer survey coverage totalled 16.1 kms.

## 3. PERSONNEL

Eric Hards, geophysicist, was the party chief on the survey, on behalf of Scott Geophysics.

Jim Chapman, geologist, was the Eastfield representative on site for the duration of the project.

#### 4. INSTRUMENTATION AND PROCEDURES

A Scintrex IPR12 receiver and IPC7 (2.5 kw) transmitter were used on the induced polarization survey. Readings were taken in the time domain using a 2 second current pulse.

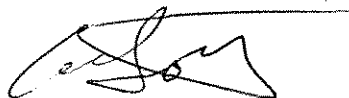
The chargeability plotted on the accompanying pseudosections and plan maps is for the interval 690 to 1050 milliseconds after shutoff (midpoint at 870 milliseconds). This corresponds to the M7 value for the IPR11.

Two Scintrex IGS-MP4 magnetometers were used for the magnetometer survey, one as the field unit and the other as a fixed base station.

#### 5. RECOMMENDATIONS

A preliminary evaluation of the results of the geophysical surveys performed on the Aztec Property did not detect any features that could be recommended for additional work at this time.

Respectfully Submitted,

A handwritten signature in black ink, appearing to read 'Alan Scott', written over a horizontal line.

Alan Scott, P. Geos.

Statement of Qualifications

for

Alan Scott, Geophysicist

of

4013 West 14th Avenue  
Vancouver, B.C. V6R 2X3

I, Alan Scott, hereby certify the following statements regarding my qualifications, and my involvement in the program of work described in this report.

1. The work was performed by individuals sufficiently trained and qualified for its performance.
2. I have a material interest in the Aztec Property, on which the surveys discussed in this report were performed. I am a shareholder and director of Eastfield Resources Ltd.
3. I graduated from the University of British Columbia with a Bachelor of Science degree (Geophysics) in 1970, and with a Master of Business Administration degree in 1982.
4. I am a member of the Association of Professional Engineers and GeoScientists of British Columbia.
5. I have been practicing my profession as a Geophysicist in the field of Mineral Exploration since 1970.

Respectfully submitted,



Alan Scott

*needs approval*

MINFILE: 115J 036  
PAGE NO: 1 of 1  
UPDATED: 06/24/94

**YUKON MINFILE  
STANDARD REPORT  
EXPLORATION AND GEOLOGICAL SERVICES DIVISION, DIAND  
WHITEHORSE**

NAME(S): Zappa  
MINFILE #: 115J 036  
MAJOR COMMODITIES: Cu  
MINOR COMMODITIES: Mo  
TECTONIC ELEMENT: Northern Stikine Terrane

NTS MAP SHEET: 115 J 10  
LATITUDE: 62°44'15"N  
LONGITUDE: 138°58'02"W  
DEPOSIT TYPE: Porphyry  
STATUS: Anomaly

---

**CLAIMS (PREVIOUS AND CURRENT)**

ZAPPA, MOTHERS, AZTEC, RAT, WET, KOFFEE, MAYA

**WORK HISTORY**

Staked as Zappa and Mothers cl (Y36184) in Aug/69 by Dawson Range JV (Straus E Inc, Martin Marietta Corp, Molybdenum Corp of America, Trojan Cons M, and Great Plains Dev C of Can L), which explored by grid soil sampling and mapping in 1969 and a mag survey in 1970. The adjoining Aztec, etc cl (Y37004) were staked in Sep/69 by Trans Columbia EL, which conducted airborne mag and spectrometer surveys followed by grid soil sampling of anomalous areas in 1970.

The Trans Columbia claims were restaked in June-Aug/73 as Rat and Wet cl (Y75586) by Casino Silver ML.

Restaked as Koffee cl (YA8205) in Sep/76 by Archer, Cathro & Assoc Ltd and explored with mapping and sampling in 1980 by Denison ML under an option. Staked again as Koffee 1-58 cl (YB37524) by Renoble Holdings Inc. (YB37482) in Sep/92. Restaked Sep/92 as Maya 1-40 cl (YB37592) by Renoble Holdings Inc. In Mar/93, Renoble consolidated its land holdings with Eastfield Resources Ltd, which acquired a 100% interest subject to a profit sharing agreement. The Achievers Training Group acquired a 50% interest in May/93. Eastfield Resources conducted a program of geological mapping, geochemical sampling and geophysical surveying (ground magnetometer and induced polarization surveys) on the Koffee claims in June/93.

**GEOLOGY**

The claims overlie Triassic Klotassin granodiorite intruded by a small stock of pyritized and altered quartz porphyry. Strong copper response is associated with the quartz porphyry while a moderate molybdenum soil anomaly occurs immediately to the northwest.

The 1993 program outlined a large multielement soil geochemical anomaly which was coincident with a magnetic high and a chargeability anomaly.

**REFERENCES**

EASTFIELD RESOURCES LTD., Assessment Report #093143 by J. Chapman and G.L. Garratt.

EASTFIELD RESOURCES LTD., Assessment Report #093144 by J. Chapman and G.L. Garratt.

GEORGE CROSS NEWSLETTER, 22 Feb/93; 10 Mar/93; 13 May/93.

MINERAL INDUSTRY REPORT 1969 and 70, p. 46-47.

YUKON GEOLOGY AND EXPLORATION 1979-80, p. 266.

*needs  
approval*

MINFILE: 115J 101  
PAGE NO: 1 of 1  
UPDATED: 06/24/94

**YUKON MINFILE  
STANDARD REPORT  
EXPLORATION AND GEOLOGICAL SERVICES DIVISION, DIAND  
WHITEHORSE**

NAME(S): Ana  
MINFILE #: 115J 101  
MAJOR COMMODITIES: -  
MINOR COMMODITIES: -  
TECTONIC ELEMENT: Mt Nansen volcanics

NTS MAP SHEET: 115 J 10  
LATITUDE: 62°44'15"N  
LONGITUDE: 138°54'22"W  
DEPOSIT TYPE: Unknown  
STATUS: Anomaly

---

**CLAIMS (PREVIOUS AND CURRENT)**

AZTEC, ANA, KOFFEE

**WORK HISTORY**

Staked as Aztec, etc cl (Y37004) in Sep/69 by Trans Columbia EL, which conducted airborne mag and spectrometer surveys and grid soil geochem surveys in 1970. Restaked as ANA cl (YA86735) in May/85 by Nordac Mg Corp, which conducted a grid geochem survey later in the year and optioned the claims to Auspex Gold Ltd in spring.

Eastfield Resources Ltd optioned the Ana claims in Mar/93. Breckinridge Resources Ltd purchased a 20% interest from Eastfield in Apr/93, with an option to acquire an additional 50% on completion of a 4 year exploration program. Eastfield Resources conducted a program of geological mapping, geochemical sampling and geophysical surveying (ground magnetometer and induced polarization surveys) on the Koffee claims in June/93.

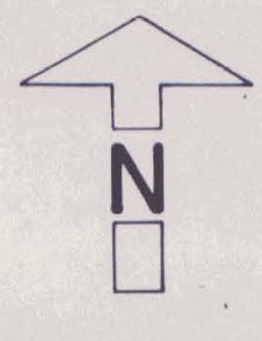
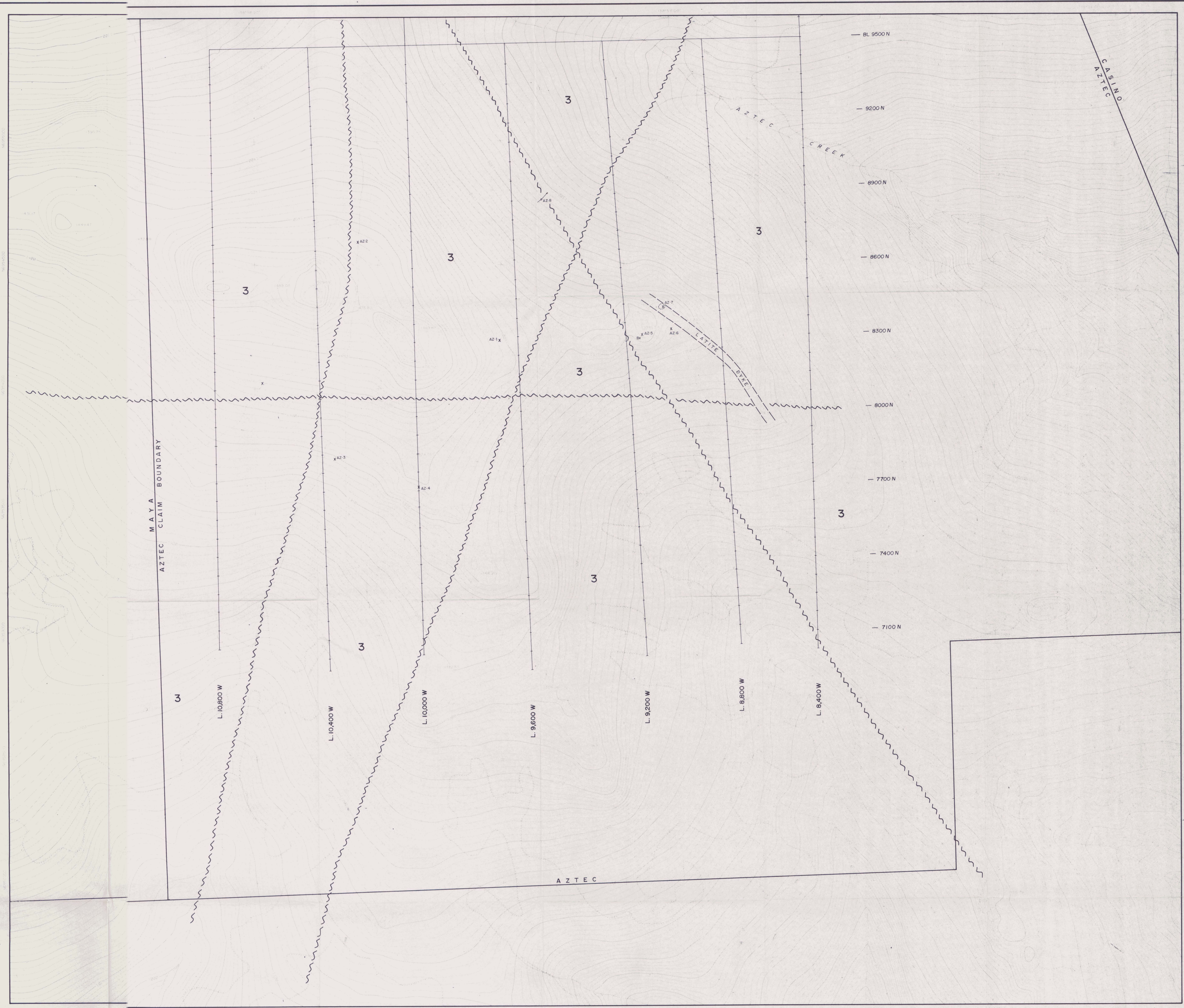
**GEOLOGY**

A tourmalinized heterolithic breccia pipe of the Lower Cretaceous Mt Nansen Group has been intruded along the contact between Paleozoic gneiss and the Triassic Klotassin Batholith. Trans Columbia located a copper-molybdenum anomaly west of the breccia, while Nordac sampling showed that the area around the breccia carries anomalous values of up to 395 ppb Au.

The 1993 program outlined a large multielement soil geochemical anomaly which was coincident with a magnetic high and a chargeability anomaly.

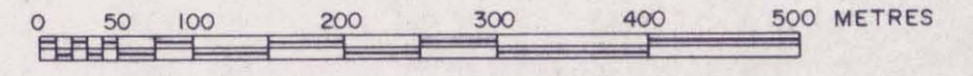
**REFERENCES**

- EASTFIELD RESOURCES LTD., Assessment Report #093143 by J. Chapman and G.L. Garratt.
- EASTFIELD RESOURCES LTD., Assessment Report #093144 by J. Chapman and G.L. Garratt.
- GEORGE CROSS NEWSLETTER, 15 Mar/93; 15 Apr/93.
- TRANS COLUMBIA EXPLORATIONS LTD, 1970. Assessment Report #060227 by S.L. Sandner.
- TRANS COLUMBIA EXPLORATIONS LTD, 1970. Assessment Report #019922 by W.R. Newman.
- TRANS COLUMBIA EXPLORATIONS LTD, Sep/70. Assessment Report #061956 by D.R. Cochrane & A.J. Sinclair.
- TRANS COLUMBIA EXPLORATIONS LTD, 1972. Assessment Report #019923 by S.L. Sandner.

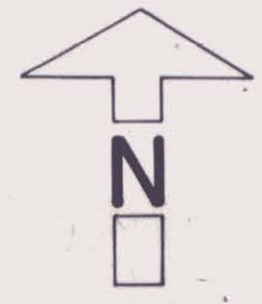
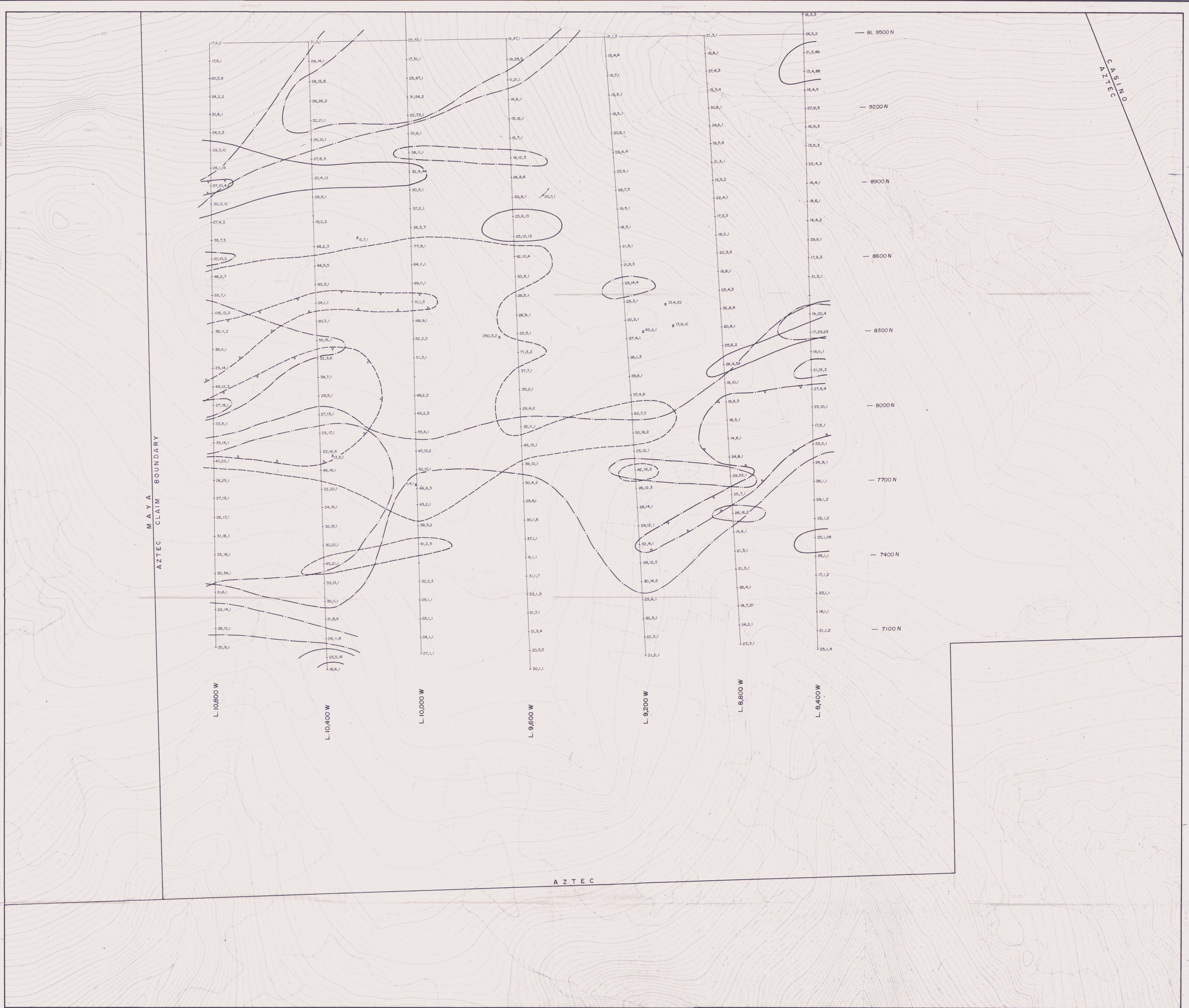


LEGEND  
 Trails  
 Trench  
 Lake  
 River  
 Stream  
 Trees  
 Contour  
 Index  
 Intermediate

- 3** DAWSON RANGE BATHOLITH - undivided
- Outcrop
- Faults interpreted from airphoto
- AZ-7 X Rock sample site and sample number
- AZ-6 X Silt " " " "
- BX Breccia



|                                                                   |       |                          |
|-------------------------------------------------------------------|-------|--------------------------|
| Eastfield Resources Ltd. /<br>Canadian Comstock Explorations Ltd. |       |                          |
| <b>AZTEC PROJECT</b><br>Whitehorse, M.D., Yukon                   |       |                          |
| <b>GEOLOGY</b> <i>Dwg 211</i><br>093144                           |       |                          |
|                                                                   | Scale | 1 : 5000                 |
|                                                                   | Date  | October 1993             |
|                                                                   | By    |                          |
|                                                                   |       | NTS 115-J/10<br>Figure 1 |



LEGEND

- Trails
- Trench
- Lake
- River
- Stream
- Trees
- Contours
- Index
- Intermediate

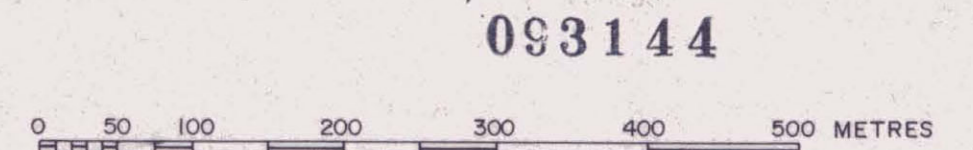
Geochemical Sample Sites

SILT { Cu, Mo (ppm), Au (ppb)

ROCK { x

SOIL { Cu, Mo (ppm), Au (ppb)

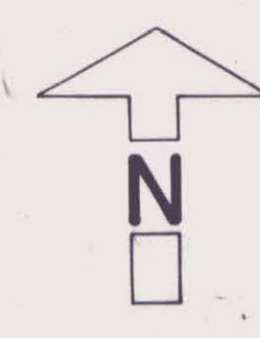
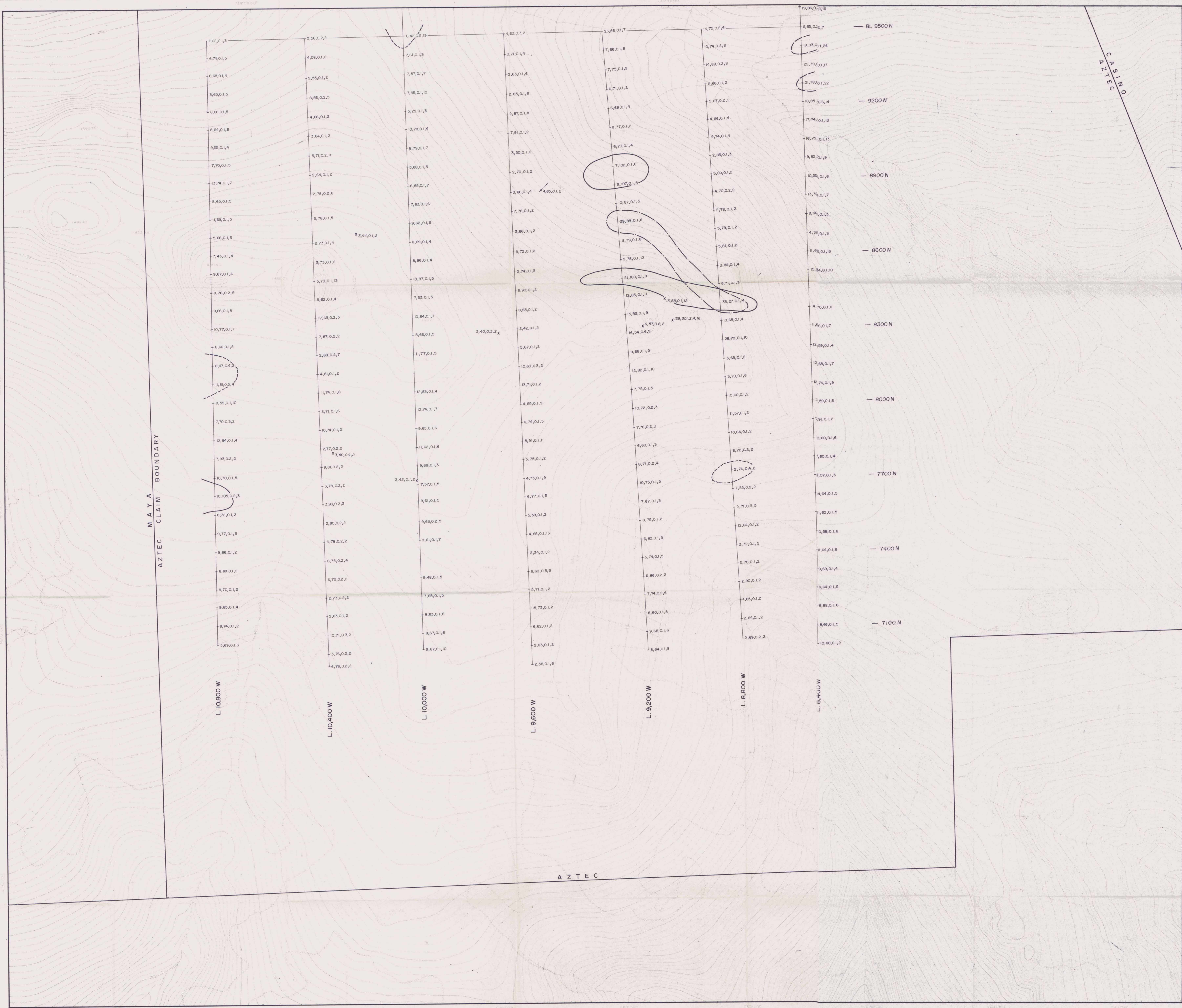
- 40 ppm Copper contour
- 10 ppb Gold contour
- 15 ppm Molybdenum contour
- 10 ppm Molybdenum contour



083144

DWG 212

|                                                                |                                              |                           |
|----------------------------------------------------------------|----------------------------------------------|---------------------------|
| Eastfield Resources Ltd. / Canadian Comstock Explorations Ltd. |                                              |                           |
| <b>AZTEC PROJECT</b>                                           |                                              |                           |
| Whitehorse, M.D., Yukon                                        |                                              |                           |
| <b>ROCK, SILT and SOIL GEOCHEMISTRY</b>                        |                                              |                           |
| <b>Cu, Mo (ppm), Au (ppb)</b>                                  |                                              |                           |
| MINCORD EXPLORATION CONSULTANTS LIMITED                        | Scale 1 : 5000<br>Date October 1993<br>By JC | NTS 115-J/10<br>Figure 2a |



LEGEND

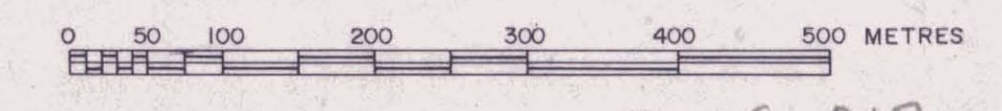
- Trails
- Trench
- Lake
- River
- Stream
- Trees
- Contours
- Index
- Intermediate

Geochemical Sample Sites

- SILT  $\times$  Pb, Zn, Ag, As (ppm)
- ROCK  $x$  Pb, Zn, Ag, As (ppm)
- SOIL  $\dagger$  Pb, Zn, Ag, As (ppm)

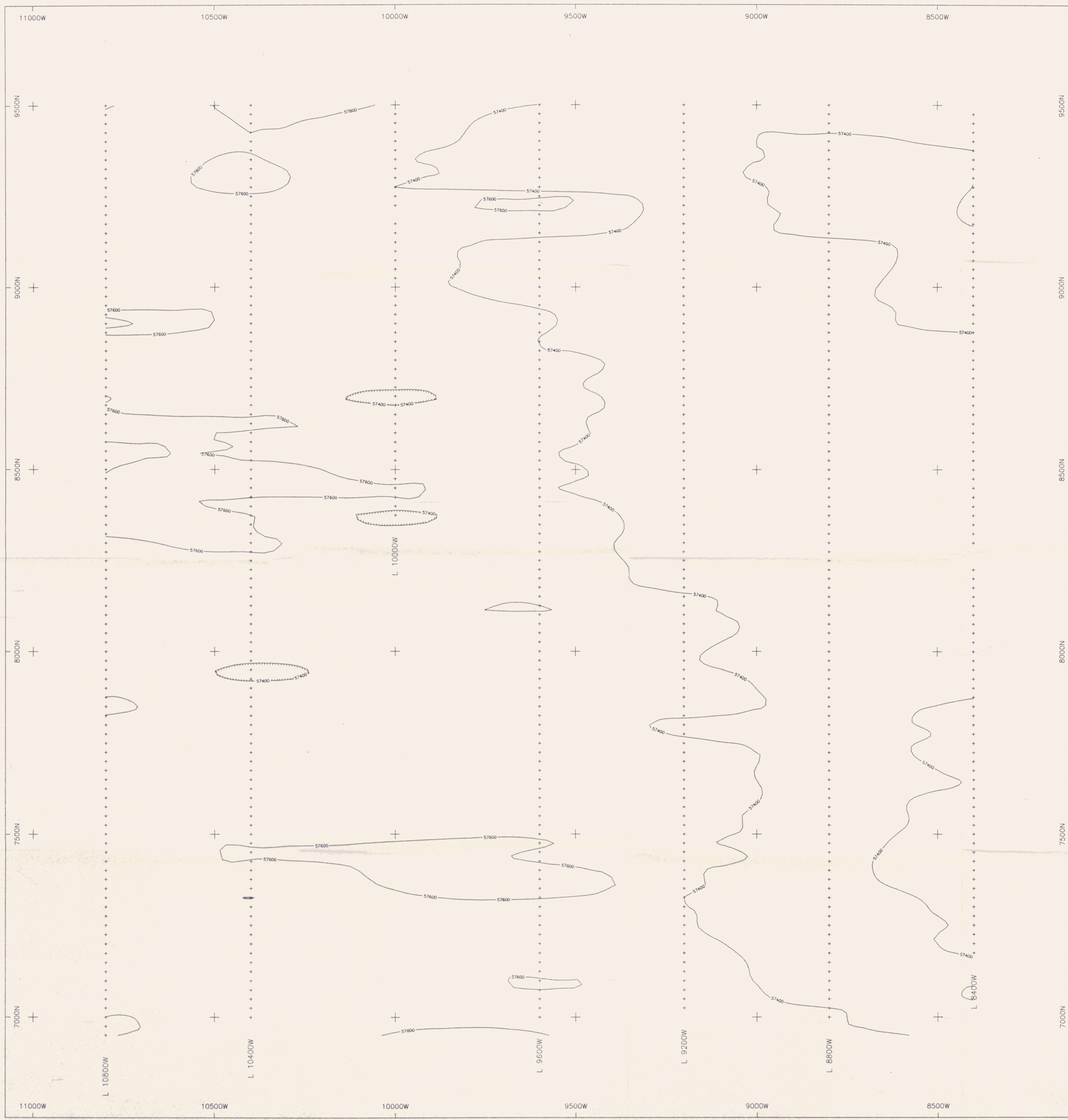
- 30 ppm Lead contour
- 20 ppm Arsenic contour
- 0.4 ppm Silver contour
- 100 ppm Zinc contour

093144



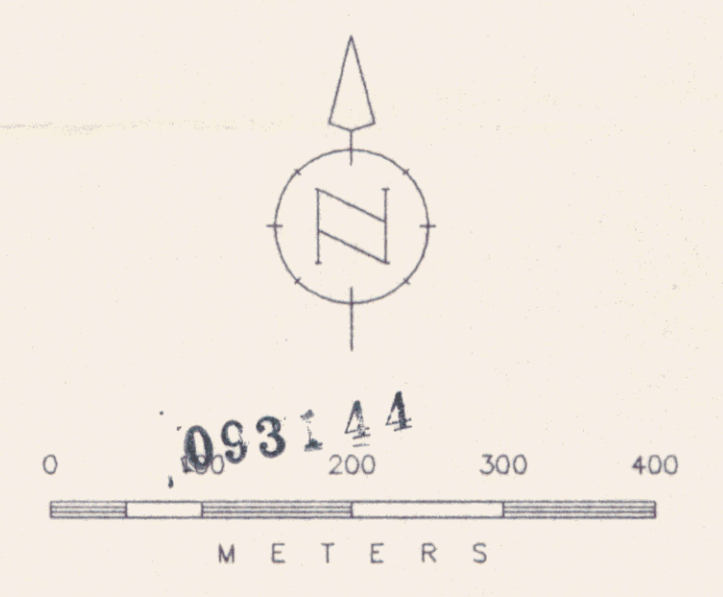
DWG 213

|                                                                  |       |              |
|------------------------------------------------------------------|-------|--------------|
| Eastfield Resources Ltd./<br>Canadian Comstock Explorations Ltd. |       |              |
| <b>AZTEC PROJECT</b>                                             |       |              |
| Whitehorse M.D., Yukon                                           |       |              |
| <b>ROCK, SILT and SOIL<br/>GEOCHEMISTRY</b>                      |       |              |
| <b>Pb, Zn, Ag, As (ppm)</b>                                      |       |              |
|                                                                  | Scale | 1 : 5000     |
|                                                                  | Date  | October 1993 |
|                                                                  | By    | JC           |
|                                                                  |       | Figure       |
|                                                                  |       | 115-J/10     |
|                                                                  |       | <b>2b</b>    |



SURVEY SPECIFICATIONS

|                        |                           |
|------------------------|---------------------------|
| survey magnetometer    | Scintrex 1GS              |
| base magnetometer      | Scintrex MP4              |
| type measurement units | proton total field gammas |
| diurnal corrections    | base station              |
| base cycle time        | 30 seconds                |
| contour interval       | 200 gammas                |



EASTFIELD RESOURCES LTD.

AZTEC PROPERTY  
CASINO AREA, YUKON  
MAGNETOMETER CONTOUR PLAN  
contour interval = 200 gammas

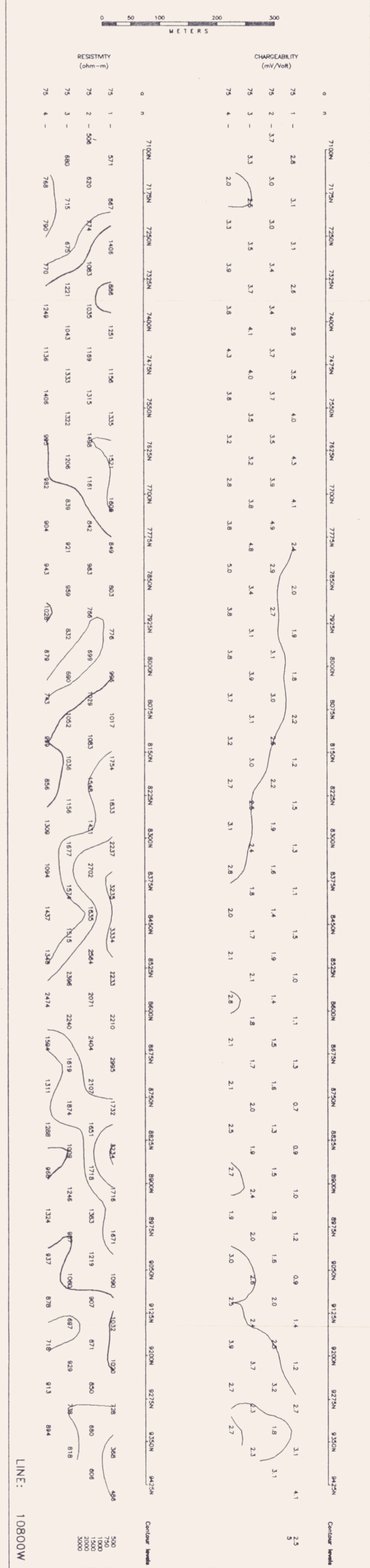
DWG 815

DRAWN BY: ars      DATE: July/93  
SCOTT GEOPHYSICS LTD.



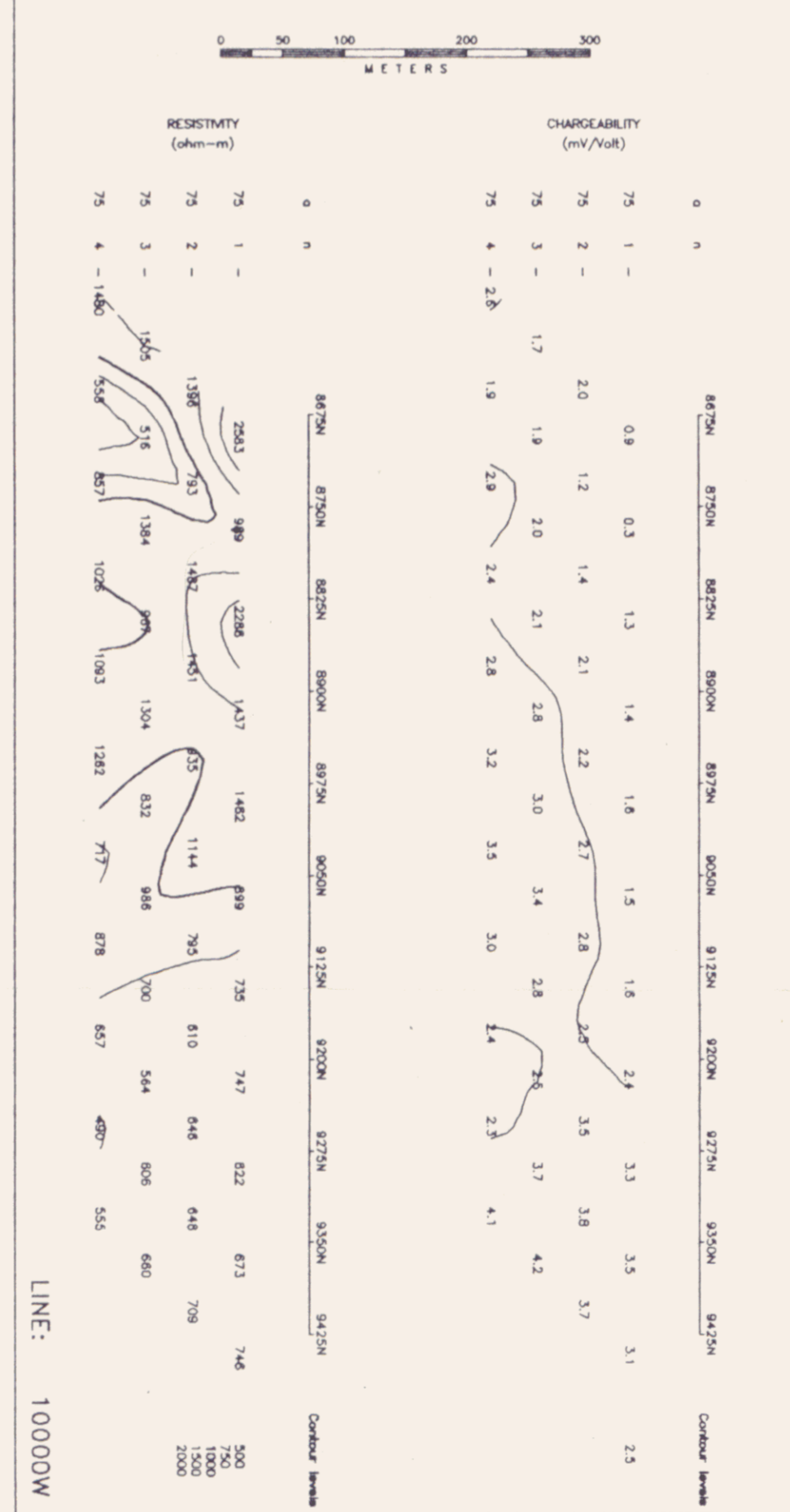
EASTFIELD RESOURCES LTD.

AZTEC PROPERTY, CASINO AREA, YUKON  
 LINE: 10800W  
 INDUCED POLARIZATION SURVEY (Pole-Dipole Array)  
 SCOTT GEOPHYSICS LTD. Scintrex IPR12  
 July/93 Pulse Rate: 2 sec  
 current electrode north of receiving electrodes  
 Mx Chargeability is for interval 690 to 1050 msec after shutoff



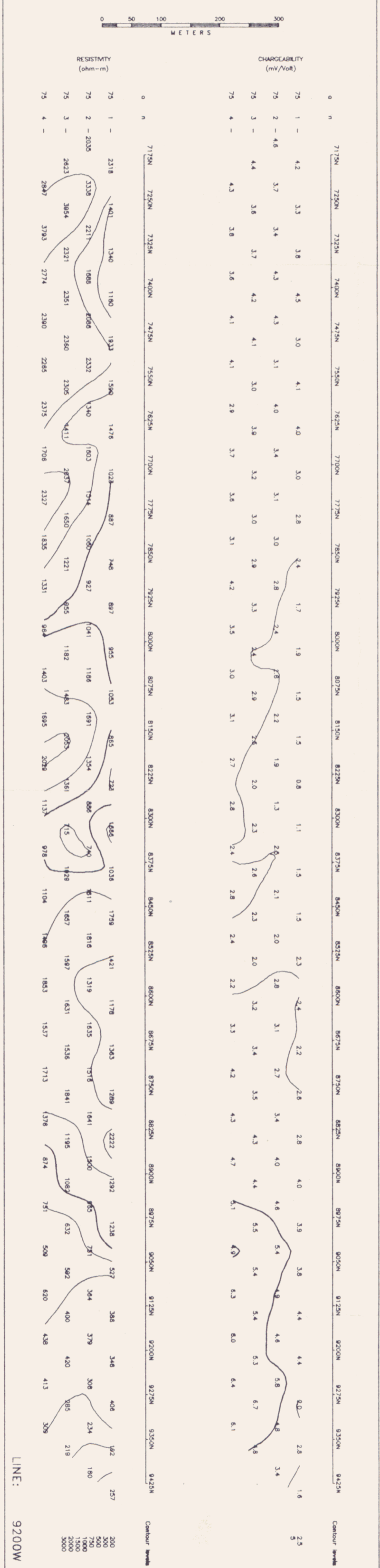
EASTFIELD RESOURCES LTD.

AZTEC PROPERTY, CASINO AREA, YUKON  
 LINE: 10000W  
 INDUCED POLARIZATION SURVEY (Pole-Dipole Array)  
 SCOTT GEOPHYSICS LTD. Scintrex IPR12  
 July/93 Pulse Rate: 2 sec  
 current electrode north of receiving electrodes  
 Mx Chargeability is for interval 690 to 1050 msec after shutoff



EASTFIELD RESOURCES LTD.

AZTEC PROPERTY, CASINO AREA, YUKON  
 LINE: 9200W  
 INDUCED POLARIZATION SURVEY (Pole-Dipole Array)  
 SCOTT GEOPHYSICS LTD. Scintrex IPR12  
 July/93 Pulse Rate: 2 sec  
 current electrode north of receiving electrodes  
 Mx Chargeability is for interval 690 to 1050 msec after shutoff



EASTFIELD RESOURCES LTD.

AZTEC PROPERTY, CASINO AREA, YUKON  
 LINE: 8400W  
 INDUCED POLARIZATION SURVEY (Pole-Dipole Array)  
 SCOTT GEOPHYSICS LTD. Scintrex IPR12  
 July/93 Pulse Rate: 2 sec  
 current electrode north of receiving electrodes  
 Mx Chargeability is for interval 690 to 1050 msec after shutoff

