

MAP NO.: 115 I 3
ASSESSMENT REPORT X
PROSPECTUS
CONFIDENTIAL X
OPEN FILE

DOCUMENT NO: 092771
MINING DISTRICT: Whitehorse
TYPE OF WORK: Geophysical, Drilling

REPORT FILED UNDER: Noranda Exploration Co. Ltd

DATE PERFORMED: 10 May-16 June, 1989

DATE FILED: 14 November, 1989

LOCATION: LAT.: 62°02'N

AREA: Mt Nansen

LONG.: 137°15'W

VALUE \$: 47 200.00

CLAIM NAME & NO.: DOWS 1-118 (YB007687-702, etc.)

WORK DONE BY: R. Diment

WORK DONE FOR: Noranda Exploration Co. Ltd

DATE TO GOOD STANDING:

REMARKS: #121 DOWS

Gold occurs in quartz-chalcedony veins associated with silicified feldspar porphyry dykes southwest of Mt Nansen. Exploration in 1989 included fill-in IP and magnetometer surveys and one diamond drill hole (198.7 m). The only significant intersection was a quartz breccia containing 2.43 g/t Au over 7.5 m including 10.2 g/t Au over 1.5 m.

DIAMOND DRILLING REPORT 1989

on the

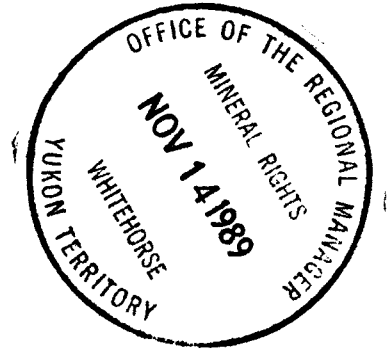
DOWS 1-118 CLAIMS

Whitehorse Mining District

N.T.S.: 115 I/3

Latitude: 62 02"N

Longitude: 137 15'W



0927711

Owner: Noranda Exploration Co. Ltd.
(no personal liability)

R. Diment
October, 1989

Approved as physical work



12 10 1911

SUMMARY

Noranda's Mt. Nansen property consists of 109 contiguous mineral claims in the Dawson Range Gold Belt, Yukon. It has 2WD road access to within 2.5 km of the claim group and a cat trail through to the property.

One hole (Dows 6) was drilled to test the vertical extention of the mineralized zones C1 and C2. The only significant intersection was a quartz breccia containing 2.43 gmt gold over 7.5m including 10.15 gmt over 1.5m. Furthermore it is believed that C1 and C2 are the same zone but has been offset by two N-S striking normal faults.

A 100km magnetometer survey, prospecting and soil sampling conducted over the rest of the property discovered no further anomalies of any economic potential.

It is recommended that no further work be done on the property since the width at depth (1.5m), grade (average of 4-5 gmt) and strike length (75m) are too limited to conceive that an economic deposit can be outlined.

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CHAPTER ONE: INTRODUCTION

1-1: Introductory Statement

The Dows 1-16, (YB07687-702), Dows 17-72 (YB12755-801) and Dows 73-118 (YB13055-100) are located approximately 50km due west of Carmacks, Yukon.

The claims were staked in 1987 and 1988 to cover mineralized subcrop and possible extensions. The current drill program was undertaken to test the vertical extent of mineralized zones (C1 & C2) found during the 1988 field season.

1-2: Location & Access

The property (NTS 115 I/3; Latitude 62 02N; Longitude 137 15'W) is located in the Dawson Range approximately 50km west of Carmacks, Y.T.. Access is by 2WD road from Carmacks to within 2.5km and a cat trail from this point through to the property.

1-3: Physiography & Vegetation

The claims lie within the Dawson Range, a region characterized by an unglaciated upland plateau dissected by present drainage. The claim group is located on a gentle west facing slope with maximum elevation of 1280m (4200'). Outcrops are generally restricted to ridge tops.

Vegetation, consists of sparse to moderately dense spruce forests on east and south facing slopes while thick moss and low buck brush predominate elsewhere in this area of discontinuous permafrost.

1-4: History of the Claims

Dows 1-16, (YB07687-702) were staked by Eugene Curley, on Aug. 25, 1987 and registered Aug. 31, 1987. Noranda Exploration

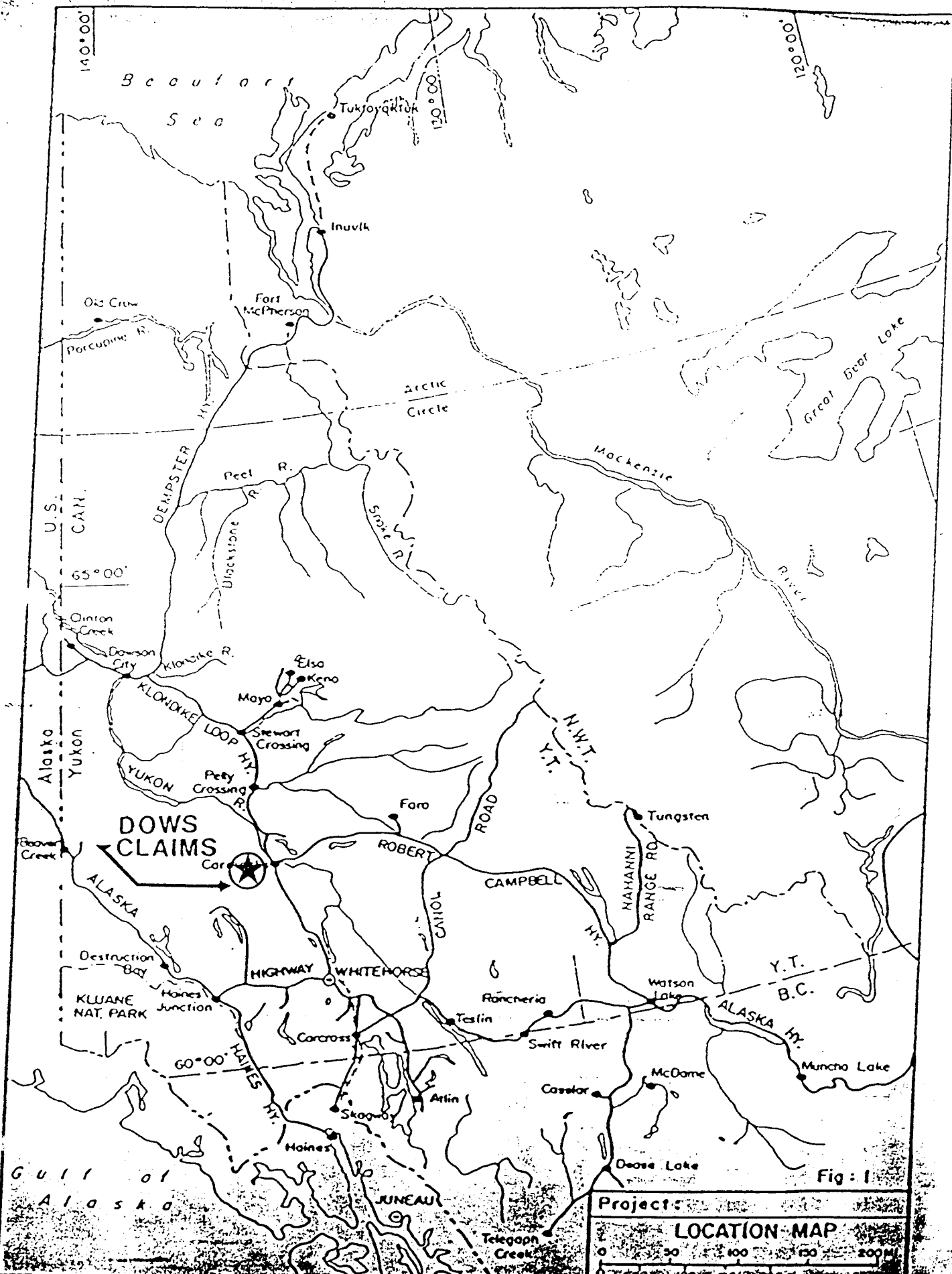


Fig. 1

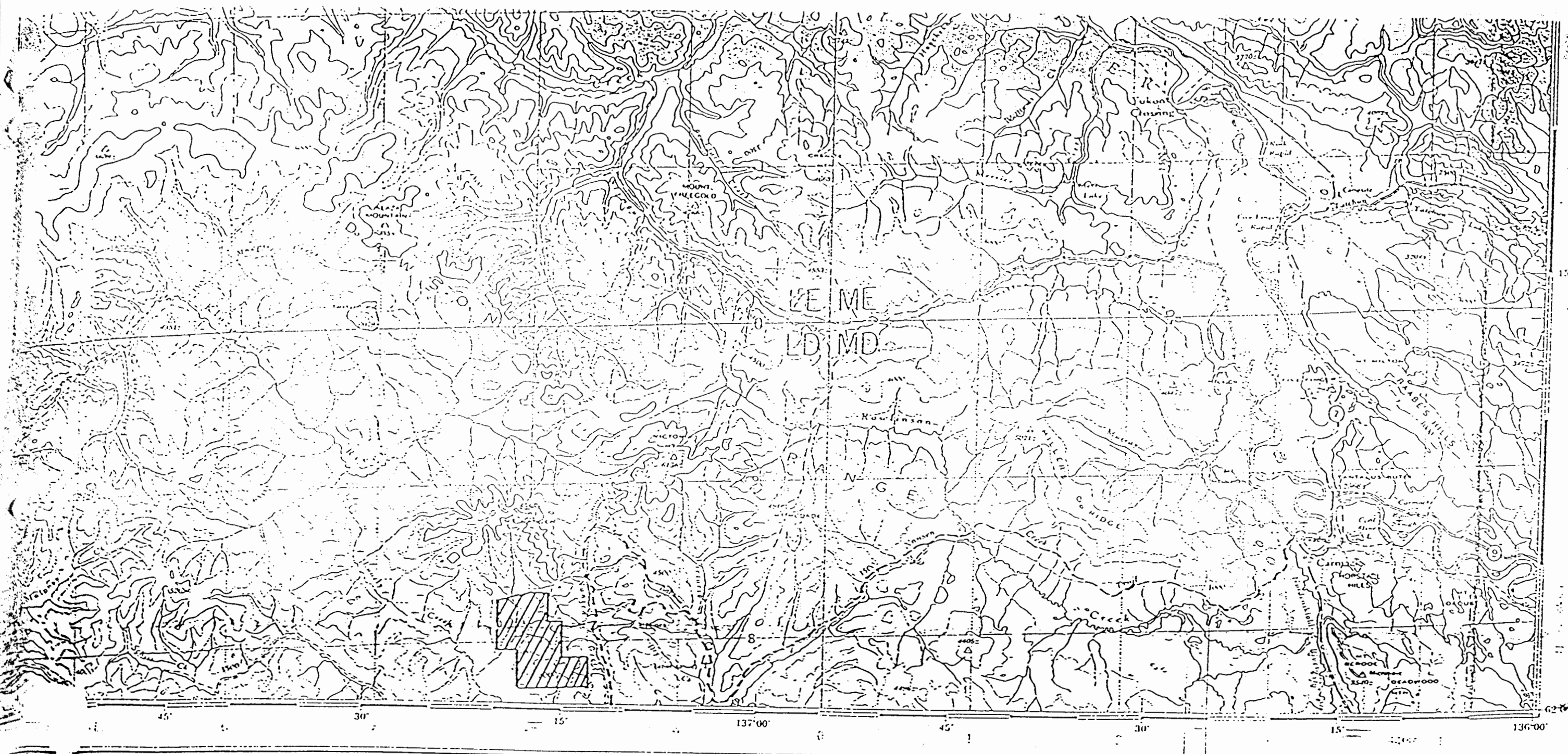
Project: _____

LOCATION MAP

0 50 100 150 200 Miles

0 50 100 150 200 Km

Scale 1:125,000



Printed 1969, by the SURVEYS AND MAPPING BRANCH,
DEPARTMENT OF ENERGY, MINES AND RESOURCES
Printed 1971

Magnetic declination 1970 varies from 31° 25' easterly at
centre of west edge to 32° 16' easterly at centre of east
edge Mean annual change 3.8' westerly

Interim Corrections 1972

CARMACKS YUKON TERRITORY

Scale 1:250,000 Échelle



CONTOUR ON 500 FEET
(Élévations en feet above Mean Sea Level)
Point datum on Datum 1927
Elevations from aneroid

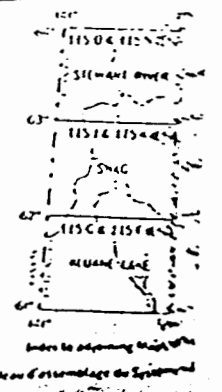
ÉLEVATIONS DES COTES 500 PIEDS
(Élévations en pieds au-dessus du niveau moyen de la mer)
Système de référence géodésique nord-américain, 1927
Point datum horizontal de Manicouag

Copies may be obtained from the Map Distribution Office,
Department of Energy, Mines and Resources, Ottawa.

Les Copies sont en vente au Bureau de Distribution des Cartes,
ministère de l'Énergie, des Mines et des Ressources, Ottawa.

Établi en 1969, par la DIRECTION DES SURVEYS ET DE LA CARTOGRAPHIE
MINISTÈRE DE L'ÉNERGIE, DES MINES ET DES RESSOURCES
Imprimé en 1971

| | | |
|---------------|--------------------------|------------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | CLAIM LOCATION MAP | |
| PROJ. No. 337 | SURVEY BY: R.G. | DATE: OCT 88 |
| FILE 1151/3 | DRAWN BY: | SCALE: 1:250,000 |
| DWG. No. | NORANDA EXPLORATION | |
| | OFFICE: WHITEHORSE | |



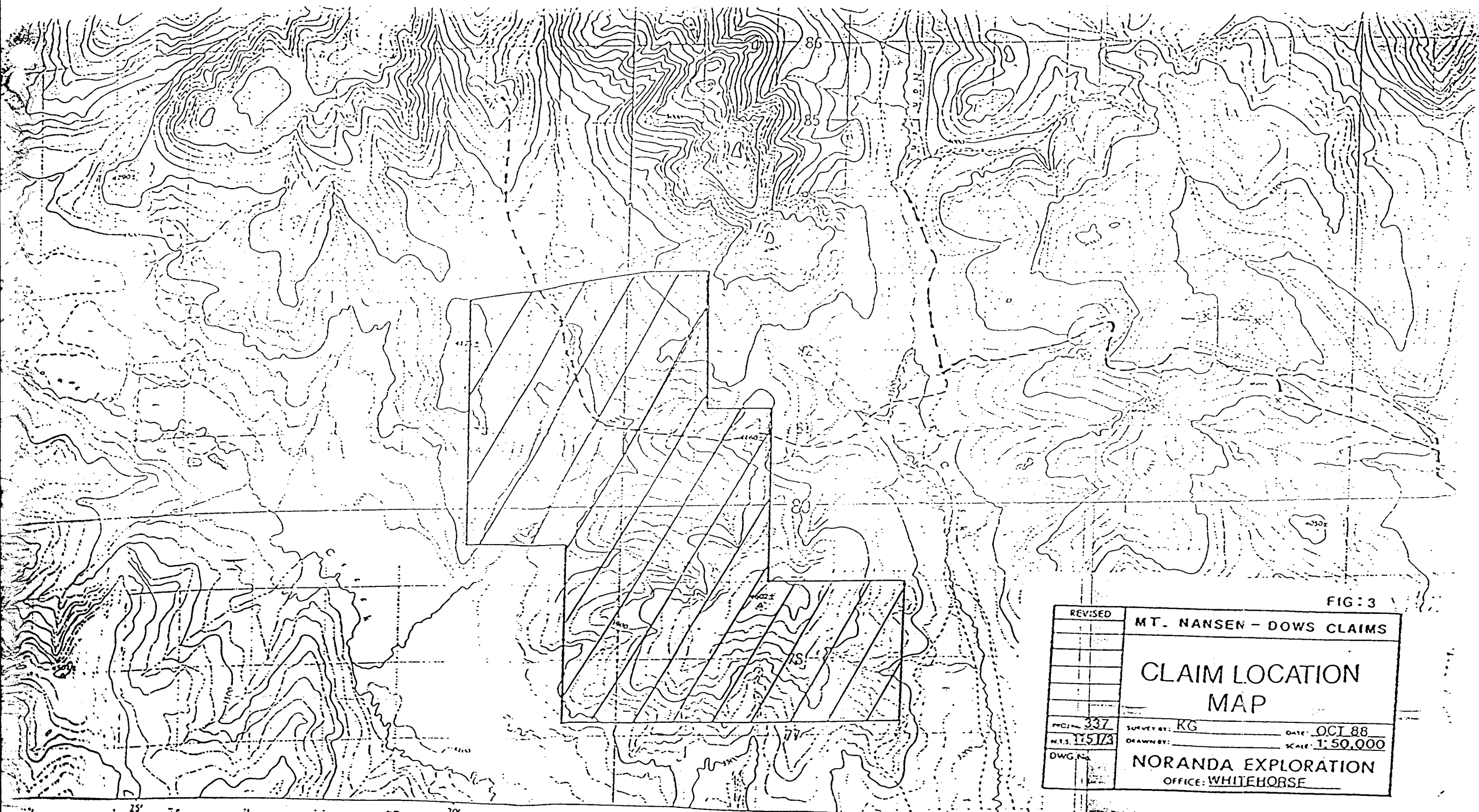
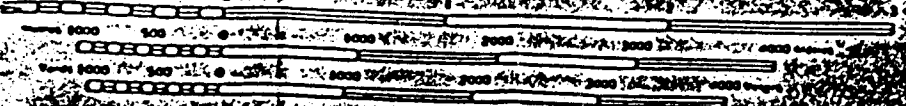


FIG: 3

| | | |
|--------------|---|-----------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | CLAIM LOCATION MAP | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| PROJ. 337 | SURVEY BY: KG | DATE: OCT 88 |
| M.T.S. 11513 | DRAWN BY: | SCALE: 1:50,000 |
| DWG. No. | NORANDA EXPLORATION OFFICE: WHITEHORSE | |

MOUNT NANSEN
YUKON TERRITORY

SCALE 1:50,000 ÉCHELLE



Routes:

| | | | |
|-----------------------------|---------------------------------|-------------------|-----------------|
| all weather | pavée, toute saison | more than 7 lanes | 7 lanes |
| weather | pavée, toute saison | less than 7 lanes | 2 lanes |
| graded surface, all weather | gravier aggloméré, toute saison | more than 7 lanes | 7 lanes or more |
| dry weather | de gravier, période sèche | less than 7 lanes | 2 lanes or plus |
| | de terre | | |
| | sentier ou portage | | |

CONTOUR INTERVAL 100 FEET
Elevations in feet above Mean Sea Level
North American Datum 1927
Transverse Mercator Projection

Some names on this map are not yet official.
Corrections or additions are invited by the
Survey and Mapping Branch.

This Provisional Map is equivalent to a standard
map in accuracy of content.

ÉCHELLE
Élévations en pieds au
niveau de 1927
Projection

Certains noms
pas encore officiels
de la cartographie
S'il y a des corrections
à apporter, veuillez
nous en aviser.

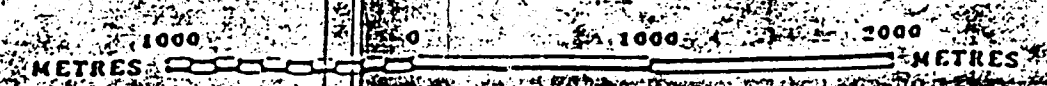
Cette carte provient
d'une carte officielle
de l'information



FIG: 4

| | | |
|--------------|----------------------------|--------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | CLAIM MAP | |
| PROJECT 337 | SURVEY BY: KG | DATE: OCT 88 |
| N.T.S. 15173 | DRAWN BY: | SCALE: |
| DWG. No. | NORANDA EXPLORATION | |
| | OFFICE: WHITEHORSE | |

SCALE 1:30,000



subsequently commissioned the staking of the remainder of the claims on Jan. 7, 1988 (registered Jan. 8, 1988).

Upon acceptance of this report, Dows 1-16, 49-60 and 65-68 will remain in good standing until February 28, 2001. Dows 73-105, 107, 109, 111 will remain in good standing until Feb. 28, 1996. The rest of the claims will remain in good standing until February 28, 1997.

1-5: Previous Exploration

Exploration in the Mt. Nansen area dates back to the turn of the century with most creeks being staked by placer miners on their way to the Klondike. The first geologist to visit the area was D.D. Carines of the G.S.C. in 1914. He examined the placer gold potential of Nansen and Victoria Creeks and made a reconnaissance survey of the area. H.S. Bostock also of the G.S.C. conducted a reconnaissance survey of the Carmacks district between 1932 and 1934.

In 1943, prospectors discovered Pb-Ag-Au veins which were later explored by Peso Silver Mines Ltd.. In 1968, Mt. Nansen Mines Ltd. opened a 400 t.p.d. mill to process ore mined from the Brown-McDade vein but it closed operations in 1969 due to poor mill head recoveries of the precious metals.

More recently, numerous companies are evaluating the region for potential bulk-mineable heap-leachable Au-Ag deposits. Important lode deposits already discovered in the area are:

| NAME | TONNES | Au (opt) | Ag (opt) |
|--------------|---------|----------|----------|
| Laforma | 198,000 | 0.32 | ? |
| Brown-McDade | 800,000 | 0.23 | 1.0 |
| Huestis | 85,728 | 0.45 | 9.11 |
| Webber | 58,524 | 0.34 | 19.29 |
| Tinta Hill | 516,000 | 0.12 | 6.4 |

In the immediate claim group area there is little evidence of previous exploration except for placer evaluation of the various creeks on the property. Prior to Noranda optioning of the property the only work done was that completed by the prospector, Mr. Eugene Curley. In 1987 Mr. Curley retrieved mineralized samples from pits dug in the area of a strong dowsing anomaly and then had two back-hoe trenches dug to expose these zones.

During 1988 a grid was established over the original sixteen claims. A geochemical survey consisting of 673 soil samples as well as 4.6 km of VLF, 4 km IP and 43 km of a magnetometer survey were completed on this grid. Later, a total of 5 trenches were dug and sampled (137 trench samples) and five diamond drill holes were drilled (388.01m) to test geophysical and geochemical anomalies.

1-6: Work Program

In May of 1989 one diamond drill hole (198.7m) was drilled by a four person crew from E. Caron Diamond Drilling Ltd., while a two person Noranda crew logged and split the core. Later in the same month a three person Noranda crew placed 100km of

flagged line over the remainder of the Dows property.

In June a six person crew from MPH Consulting Ltd. completed 10km of IP (infill of 1988 IP survey) and a 100km magnetometer survey over the remainder of the property. At the same time a two person Noranda crew collected 241 soil samples and 31 rock samples over the same area.

CHAPTER TWO: GEOLOGY

2-1: Regional Geology

The area sits on the boundary between the Yukon Cataclastic Terrane to the north and the Yukon Crystalline Terrane to the south. Paleozoic schists and gneisses of the Crystalline Terrane predominate as the basement in this area. These rocks have been intruded by two main igneous events; an early Jurassic plutonic suite comprised of syenite to monzonite which was later metamorphosed and foliated and younger Cretaceous suite of plutonic and related volcanic units.

Major regional structure generally trend northwest through the area, the most distinctive being the Big Creek Fault. This fault forms the northeast boundary of graben structure near Mt. Freegold. The southwest edge of this graben is not clearly defined but is thought to occur just south of Mt. Nansen in the area of the claim group.

Most mineralization in the area shows a special relationship to felsic porphyry dykes which are believed to be a late Cretaceous event. The porphyry units are often brecciated and fractured, possibly due to the explosive action of confined late stage volatiles. Areas of fracturing act as plumbing systems and

have contributed to localizing hydrothermal solutions. Advanced argillic and phyllic alteration mineral assemblages are often found in these brecciated core areas surrounded by irregular halos of argillic and propylitic alteration.

2-2: Property Geology

Like most of the region, outcrop is scarce on the property due to the lack of recent glaciation. A castellated outcropping of basement schist occurs on the ridges at the western and eastern edges of the property. Within this metamorphic complex are minor quartzite and pink granite gneiss. Small outcroppings of andesitic to basaltic flows of the Mt. Nansen Group are exposed in the southwest corner of Dows 16. Also small subcroppings of flow banded rhyolite (Mt. Nansen Group) occur in the eastern edge of Dows 22. Three separate subcrops of intense silica alteration (i.e. vein material) with disseminated sulphides were discovered at 6525 E 10025N, 7930 E 9500N, 10840 E 6730 N.

Bedrock exposed in the trenches consists of fresh to intensely clay altered schists, gneisses, quartzite and white marble of the basement metamorphic complex intruded by weak to strongly clay and/or silica altered (often foliated) quartz feldspar porphyry dykes believed to belong to the Cretaceous Mt. Nansen Volcanic Suite.

The basement rocks are characterized by quartzofeldspathic, medium to coarse grained schists and gneiss. These are generally brown in color and moderately siliceous with minor vitreous quartz layers. Also included is a white coarse crystalline

marble with minor local calc-silicate alteration.

The intrusive rocks noted to date are white to light tan weathering quartz-feldspar porphyrys. They are generally fine grained with quartz and/or plagioclase occurring as small phenocrysts less than 2mm in size. These porphyrys are often foliated and contain up to 10% pyrite in fresh unoxidized samples.

All rocks found in the trenches have been altered to some degree. Most have undergone at least weak clay alteration with moderate to intense clay alteration in places. Silica alteration is very local and consists of quartz flooding and veining. Two main zones of strong silica alteration with sulphides have been located in trenches NT-1 and approximately 100m east in NT-5. The Curley zone in the discovery trench (NT-1) is exposed over a width of 14m (not true width) while the second smaller zone has a near true width of 6m in two small sub zones. The zones strike at approximately 120 degrees and dip 60-65 degrees northeast. Carbonate alteration is quite strong around the marble unit and occurs at least 15m from the contact in trench NT-7. Calc-silicate alteration is very minor and occurs as pods and stringers within the marble unit.

TABLE OF FORMATION

17 Unconsolidated Alluvium

Mt. Nansen Suite

9 Porphyry dykes

9c Quartz-feldspar porphyry dykes; white weathering
commonly pyritic

9d Porphyritic granodiorite to quartz monzonite stock

7 Mt. Nansen Volcanics

7a andesite to latite massive flows and feeders

7at tuff, tuffaceous sediments, in part laharic

7ax flow breccia, probably in part intrusive

7c felsic dome-commonly flow banded, quartz & feldspar
porphyry

Dawson Range Plutonic Suite

5 Dawson Range Batholiths

5a casino granodiorite

Basement Metamorphic Complex

2c schist-gneiss subunit-includes biotite-quartz-
feldspar schist, feldspar augen gneiss, amphibolite
and minor quartzite and marble (2cm)

2d amphibolite

1 Metasedimentary Unit

1b quartz-feldspar-mica schist, quartzo-feldspathic
gneiss

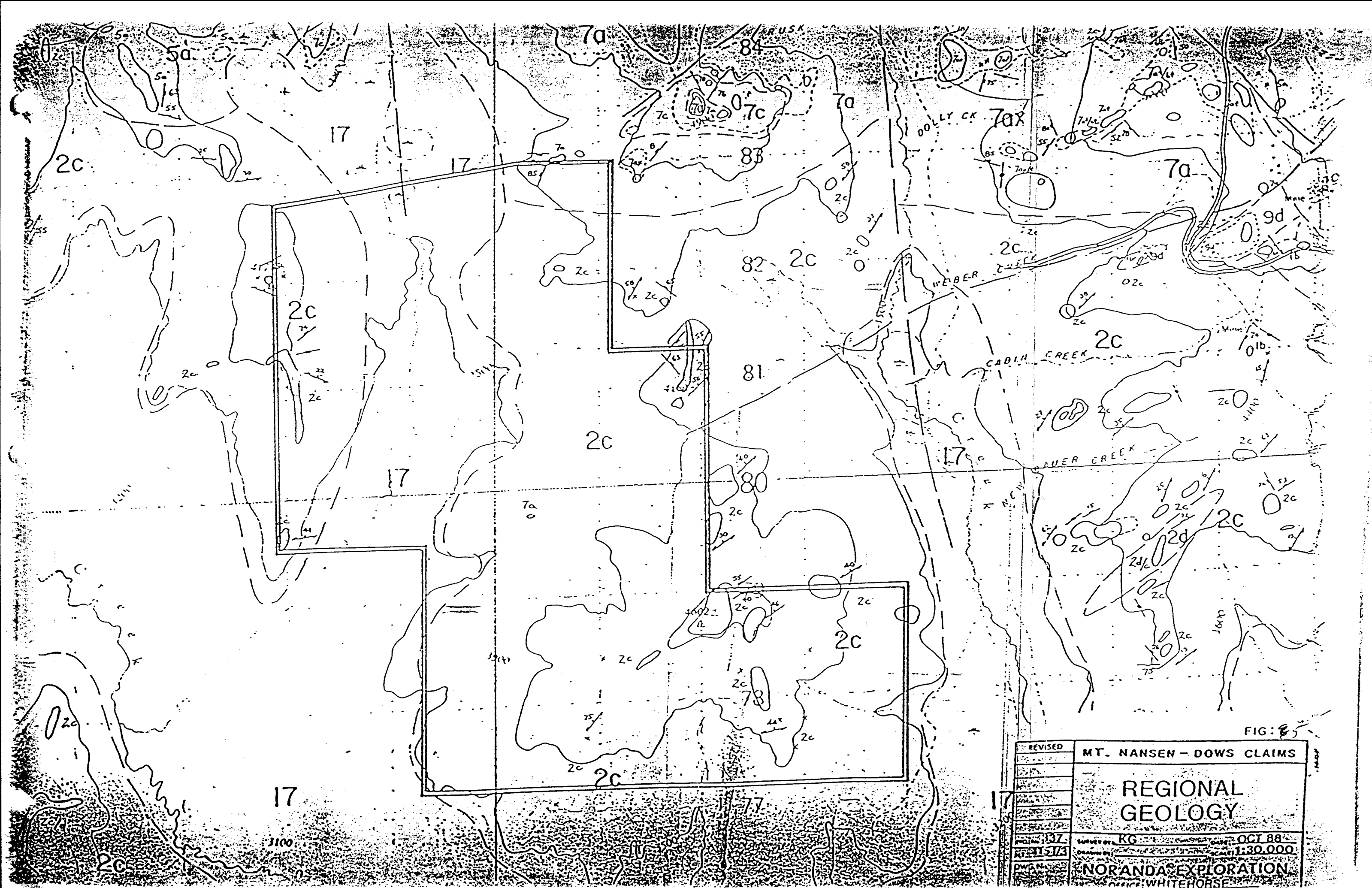


FIG: 85

| | | |
|----------------------------|--------------------------|-----------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | REGIONAL GEOLOGY | |
| PROJECT: 137 | SURVEY BY: KG | DATE: OCT 88 |
| DATE: 11-2/83 | DRAWN BY: | SCALE: 1:30,000 |
| NORANDA EXPLORATION | | |
| Office: WHITEHORSE | | |

CHAPTER THREE: GEOCHEMISTRY

3-1: Soil Geochemistry

Surveys conducted during the 1989 field season were limited to three areas on the extended grid where new mineralized subcrop and outcrop were discovered. Unfortunately no significant anomalies were found. One area at the western edge of the property a thick (1m) layer of light grey eolian sand was found directly beneath the "B" horizon. A large sand dune occurs \angle 7100E, 11,400N at the break in slope between the N-S trending ridge and the valley floor. It is very likely that this sand has been transported from some unknown source and therefore would mask bedrock geochemistry. Weak sporadic gold anomalies were encountered; however, these anomalies are probably reflecting the eolian sand geochemistry rather than local bedrock. For a more detailed description of procedures refer to Geological, Geochemical & Geophysical Report 1988 on the Dows 1-118 Claims by Ken Galambos. For soil sample results refer to Appendix IV.

3-2: Rock Geochemistry

Sampling of three subcrop that contained similar silicification and mineralization as the C1 zone revealed no significant gold anomalies. One sample of float approximately 50m north of the Curley Zone contained 5650 ppb gold. For a more detailed description of samples and results refer to appendices III and IV.

CHAPTER FOUR: GEOPHYSICS

4-1: Procedures

During the summer of 1989 magnetometer and IP surveys were completed on the Mt. Nansen grid. The magnetometer survey employed Omni 4 magnetometers manufactured by EDA Instruments of Toronto, Ontario. The Total Field readings were recorded at 12.5 metre intervals and all applicable corrections (diurnal and daily drift) were applied to the data to ensure an instrument accuracy of 0.1 nanoTeslas. True field accuracy is probably of the order of 2 to 5 nT.

The IP survey employed Time Domain equipment, in particular the IP-6 receiver manufactured by BRGM instruments. The survey used a 25 metre dipole-dipole array configuration with readings recorded down to the fifth separation ($n=1..5$).

All of the 1989 surveys were completed under contract by MPH Consulting of Toronto, Ontario. The 1989 data has been merged with the magnetic and IP data collected during the previous field season (1988). The 1988 IP data can be readily identified on the pseudo-sections as the readings were recorded down to only the fourth separation ($n=1..4$) as opposed to the five separations recorded by the 1989 IP survey. Similarly the 1988 magnetic survey was completed over the detail grid.

4-2: Magnetometer Survey

The data is presented in contoured form at a scale of 1:10,000 which does not provide a detailed representation of this data set. Several structural directions are evident at approximately 140 degrees - 150 degrees, 070 degrees and 045

degrees in order of decreasing signature expression. Small areas of high magnetic susceptibility are observed throughout the map area particularly around L.6100E/9700N and the northwest quadrant of the detail grid (L.9400E-8300E/10600N-11000N).

4-3: I.P. Survey

The I.P. survey was completed over sections of 14 grid lines in order to map the underlying geology and define targets of interest. The I.P. data has recorded weak but distinct chargeability anomalies and resistivity features that are as indicated on the I.P. pseudo-sections. A number of chargeability anomalies stand out in terms of chargeability amplitude and anomaly shape and these are as listed below.

| | | | |
|---------|---------------------|---------|-----------|
| L.8500E | /11062.5N | L.8800E | /10475.0N |
| | /11000.0N | | |
| L.8600E | /10250.0N | | |
| | /10337.5N | | |
| L.9100E | /10675.0N | | |
| | /10737.5N | | |
| L.9200E | /10350.0N | | |
| L.9500E | /10125.0N | | |
| L.9700E | /10775.0N-10875N(?) | | |

I.P. pseudo sections are located in Appendix I.

CHAPTER FIVE: DIAMOND DRILLING

5-1: Procedures

The purpose of the 1989 drilling program was to test the depth and lateral extent of mineralization in both the C-1 and C-2 zones. One hole, intersecting both zones, was drilled for a total of 198.73m. A drilling plan map showing the drill site and zones C1-1 and C-2 is provided in Appendix 1.

| HOLE # | DEP | LAT | AZ | ANG | TARGET | DEPTH |
|--------|--------|--------|-----|-----|--------------|--------|
| Dows 6 | 10525N | 92860E | 210 | -60 | C1 & C2 zone | 198.83 |
| | | | | | at depth | |

A long year "Super -38" diamond drill and a Caterpillar D6c bulldozer were used throughout the drill program. Equipment and crew were under contract from E. Caron Diamond Drilling Limited of Whitehorse.

Bad ground (i.e. caving) was experienced in the hole. However, using mud instead of water reduced caving problems considerably allowing the entire hole to be completed with HQ drill rods. Recoveries were generally good ranging between 46% and 100%. The poorer recoveries were experienced in intensely clay altered zones near the top of the hole (46%) and in mineralized sections (55%) where quartz fragments were contained within an intensely clay altered matrix.

The core was logged and split in 1.5m intervals except where major fault or mineralized zones warranted a slightly larger or smaller sample size. Samples were shipped to Acme Analytical Laboratories in Vancouver and analysed using their 30 element ICP plus A.A. for Au & Hg package.

5-2: Results

Significant Results

DOWS 6: 2.43 gmt/7.5m, includes 10.15 gmt/1.5m

The majority of the hole consisted of intensely clay altered gneiss at the top of the hole and well foliated silicified gneiss at depth. One quartz breccia zone was intersected containing clay altered feldspar porphyry fragments within a dark grey silicified matrix. Pyrite ranges between 10 and 20% within the matrix. This zone contained an average of 2.43 gmt gold over 7.5m which includes 10.15 gmt over 1.5m.

The last fifty metres of the hole consists primarily of a strongly clay altered volcanic agglomerate. Clasts range in size from 1-25 cm across with minor black siliceous clasts containing up to 15% pyrite. The hanging wall to the volcanic agglomerate consists of a 30m wide section of silicified gneiss with moderate amounts of fault breccia up to 1.5m wide. A complete drill log is located in Appendix II.

5-3: Discussion

From the information gained in Dows 6 the mineralized zones found in last years trenching and drilling may in fact be the same zone but offset by normal faulting. Surface trenches NT-1 and NT-5 outlined two mineralized zones (C1 & C2) which strike approximately 120 degrees and dip 60-65 degrees to the northeast. Taking this into account, Dows 6 should have intersected C1 zone between 100m and 120m. Instead a similar zone was intersected at 40m with a younger pyroclastic unit (relative to the gneiss) making up the bottom third of the hole. Fault breccia

intersected at 110m may represent a near vertical N-S striking normal fault in which the western block has been downdropped, preserving the pyroclastics. Subsequent erosion of the eastern block would have displaced the C-1 zone northward to where it was intersected at 40m in Dows 6. The C2 zone in surface trench Nt-5 is offset from the mineralized zone found in holes Dows 1 and 6. A similar N-S striking normal fault could also explain this offset. For a more detailed description refer to Long Section F-F'.

CHAPTER SIX: CONCLUSIONS & RECOMMENDATIONS

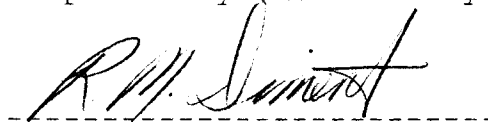
One hole, (Dows 6) was drilled to test the vertical extent of zones C1 & C2. The only significant intersection was a quartz breccia which contained 2.43 gmt gold over 7.5m including 10.15 gmt over 1.5m. From the information gained in Dows-6 it is believed that C1 & C2 are the same zone but have been offset by two parallel N-S striking normal faults.

A 100km magnetometer survey, prospecting and soil sampling failed to discover any significant anomalies on the rest of the property.

It is recommended that no further work be done on the property for the following reasons:

- 1) The mineralized zones narrow considerably with depth (i.e. 30m on surface to 7m at 40m depth).
- 2) The mineralized zones (C1 & C2) are believed to be one zone and not a series of parallel veins.
- 3) Although the type of mineralization is very similar to the Brown-McDade, Huestis and Weber veins the grade and strike length of the mineralized zones are very limited and are not sufficient enough to conceive that further work would outline an economic deposit.

Respectfully submitted by:



Rick Diment

Geologist

STATEMENT OF COSTS

LABOUR

114 person days @ \$150/day \$ 17,100.

SUPPLIES & LODGING

114 person days @ \$50/day 5,700.

DRILLING

198.7m (includes mob & demob costs) 54,965.

GEOPHYSICS

10km IP survey @ \$2000/day 24,000.

100km Mag survey @ \$150/km 15,000.

GEOCHEM ANALYSIS

241 soils @ \$15/sample 3,615.

31 rocks @ \$20/sample 620.

Report Writing, Drafting etc. 1,500.

TOTAL \$122,500.

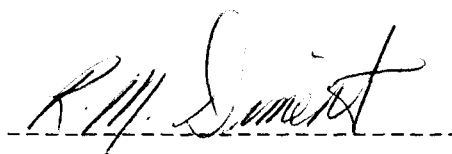
REFERENCES

- Bradish L.,; 1989 Nansen Grid Geophysical Survey; Internal
Noranda Memo
- Galambos K.,; 1988 Report on the Geological, Geochemical &
Geophysical Report on the Dows 1-118 Claims
- Galambos K.,; 1988 Diamond Drilling Report on the Dows 1-18,
49-60 & 65-68 Claims.

STATEMENT OF QUALIFICATIONS

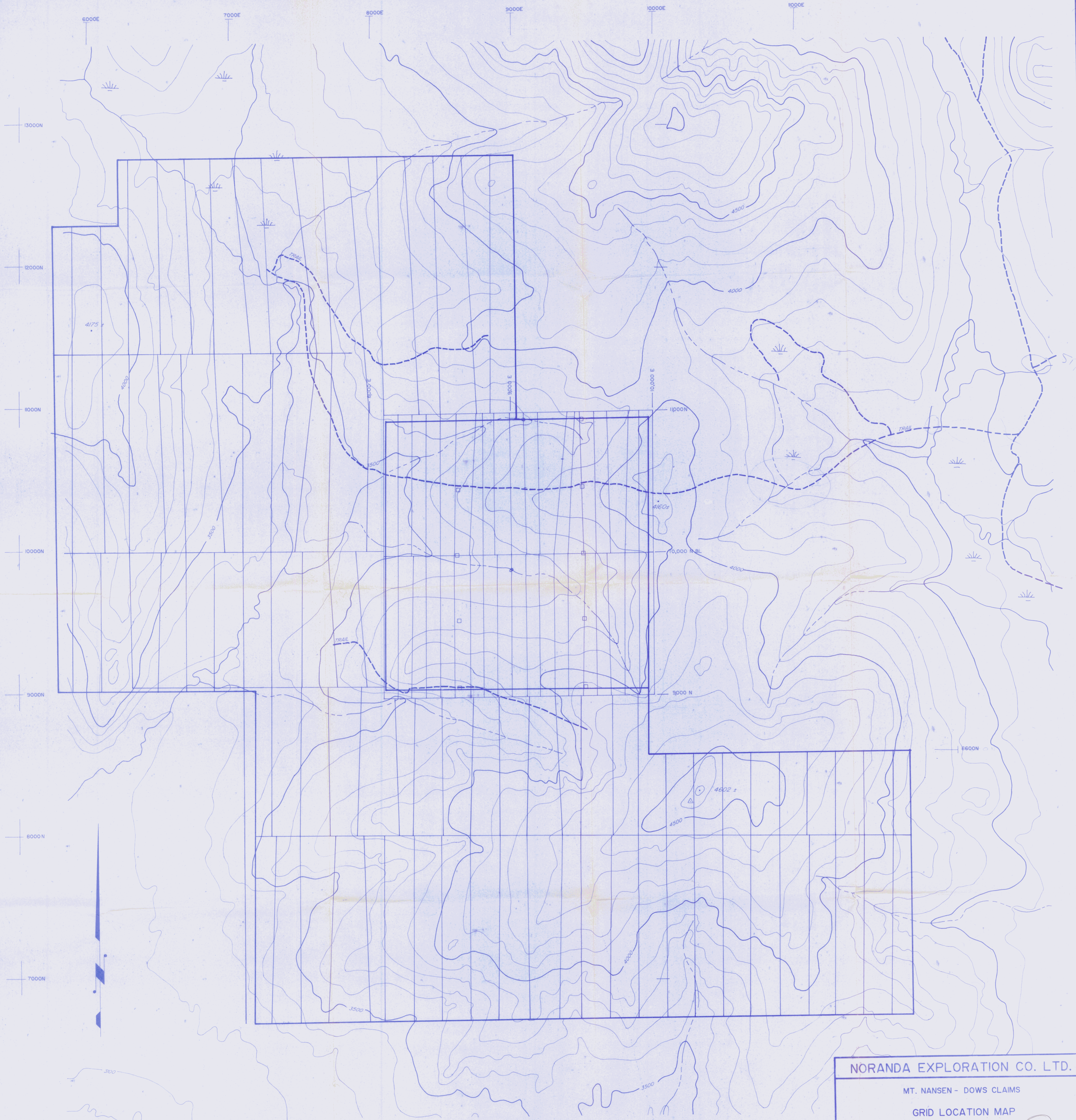
I, Richard M. Diment, do hereby certify that;

- 1) I have been an employee of Noranda Exploration Company Limited (NPL) in Whitehorse Yukon since April 1989.
- 2) I am a graduate of the University of British Columbia with a B. Sc. in Geology.
- 3) I have practiced my profession for the past three year in British Columbia.
- 4) I supervised and participated in field work done in 1989.

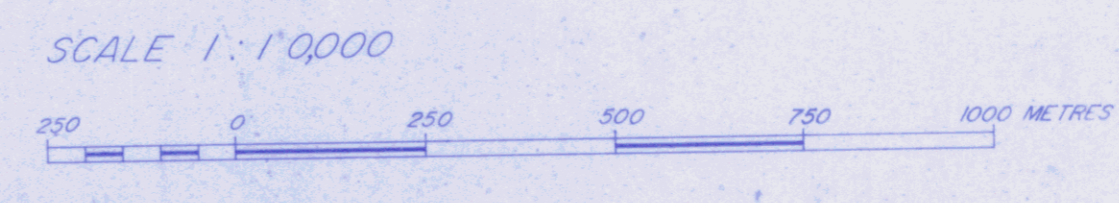
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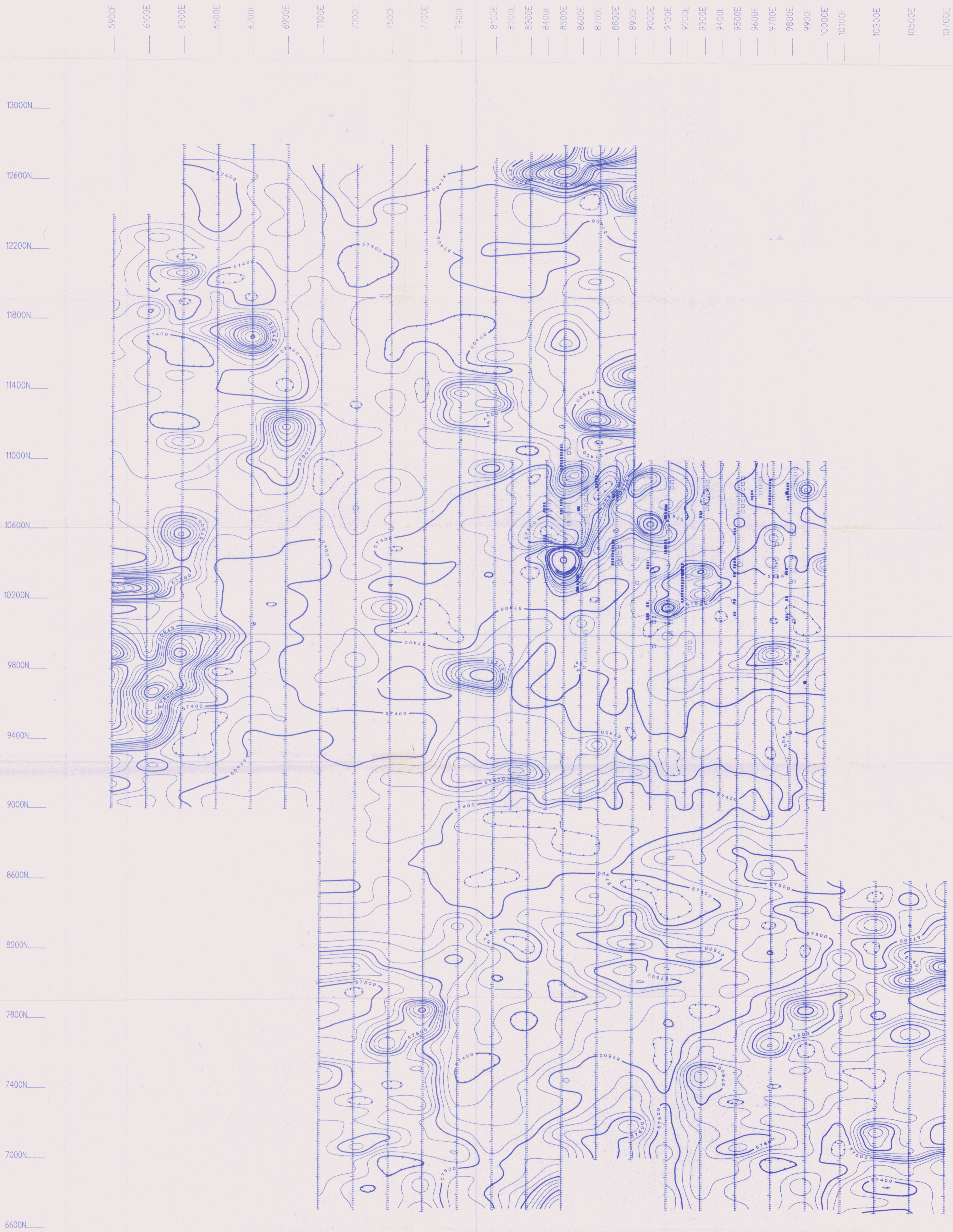
Richard M. Diment

Geologist



| | | |
|---|------------------|------------------|
| NORANDA EXPLORATION CO. LTD. | | |
| MT. NANSEN - DOWS CLAIMS | | |
| GRID LOCATION MAP | | |
| 0927711 138 | | |
| N.T.S. | SURVEYED: K.D.G. | DATE: JUNE, 1988 |
| SCALE: 1:10,000 | DRAUGHTING: R.H. | PROJ. NO. |



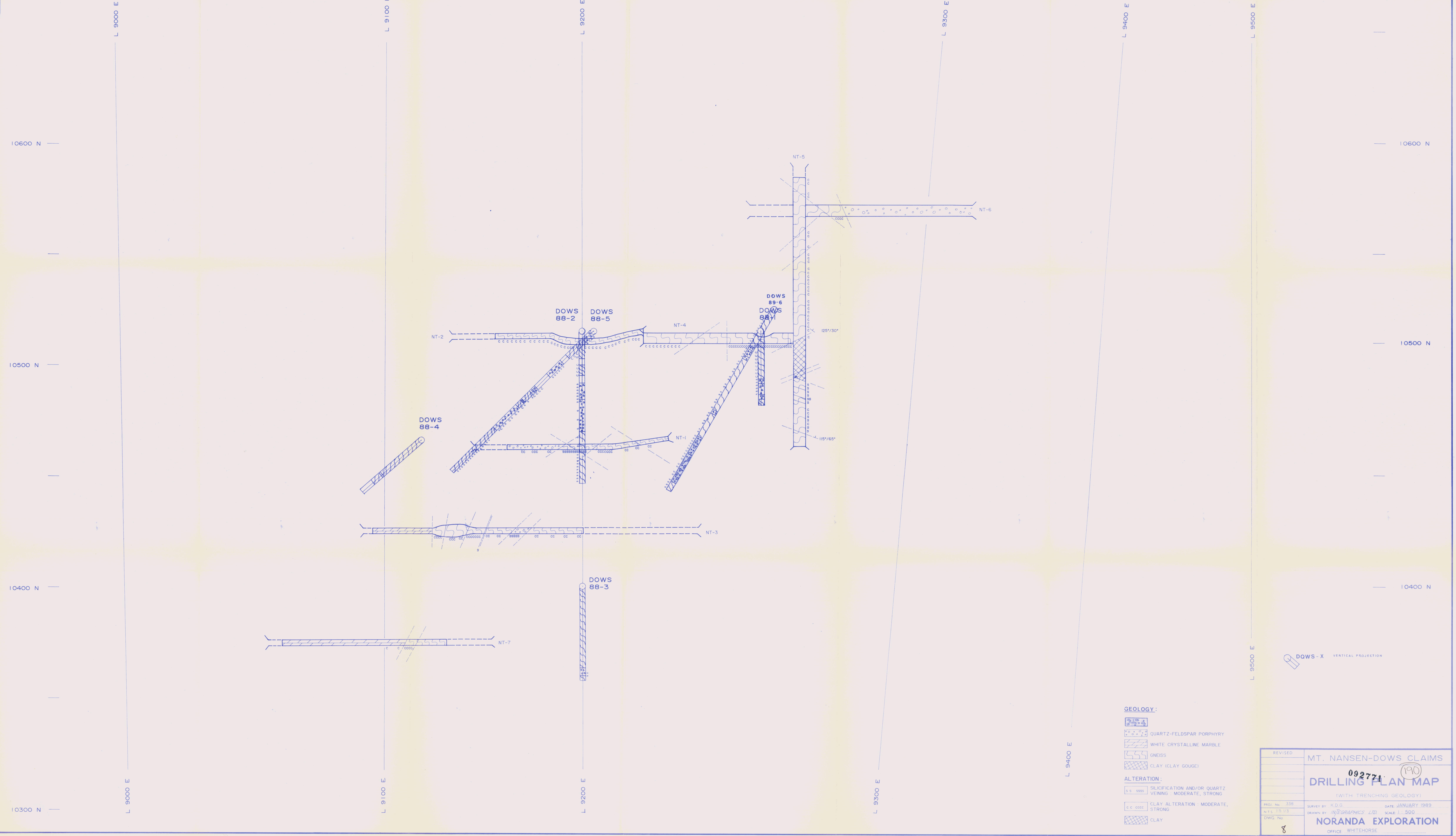


BASELINE 90°

- High I.P. Effect
- - - - - Moderate I.P. Effect
- ==== Low Resistivity Zone
- High Resistivity Zone

Instrument : OMNI
 Field : TOTAL
 Datum : 00 nT
 Contour Interval : 25 nT
 Conductor Axis :
 20m 100m 200m 400m

| | |
|----------------------------|-----------------|
| MT. NANSEN | |
| MAGNETOMETER SURVEY | |
| 092771 | |
| PROJECT: MT. NANSEN | PROJECT #: 0337 |
| BASELINE AZIMUTH : 90 Deg. | |
| SCALE = 1 : 10000 | DATE : 6/10/89 |
| SURVEY BY : MPH | NTS : 115I 5 |
| FILE: M033789 | |
| NORANDA EXPLORATION | |



10600 N
10500 N
10400 N
10300 N

L 9000 E
L 9100 E
L 9200 E
L 9300 E
L 9400 E

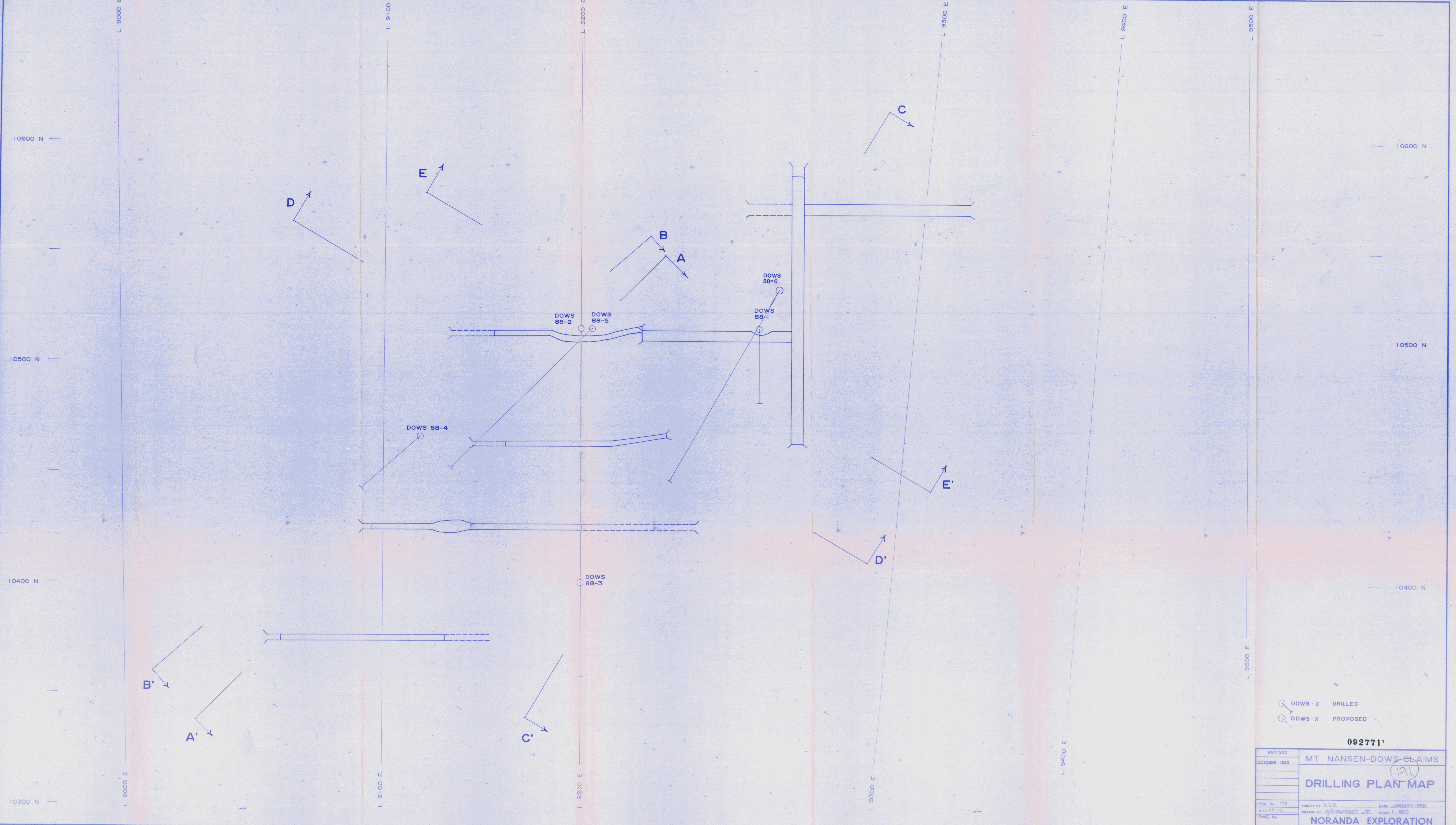
L 9100 E
L 9200 E
L 9300 E
L 9400 E
L 9500 E

10600 N
10500 N
10400 N

- GEOLOGY:**
- QUARTZ-FELDSPAR PORPHYRY
 - WHITE CRYSTALLINE MARBLE
 - GNEISS
 - CLAY (CLAY GOUGE)
- ALTERATION:**
- SILICIFICATION AND/OR QUARTZ VEINING - MODERATE, STRONG
 - CLAY ALTERATION - MODERATE, STRONG
 - CLAY

DOWS - X VERTICAL PROJECTION

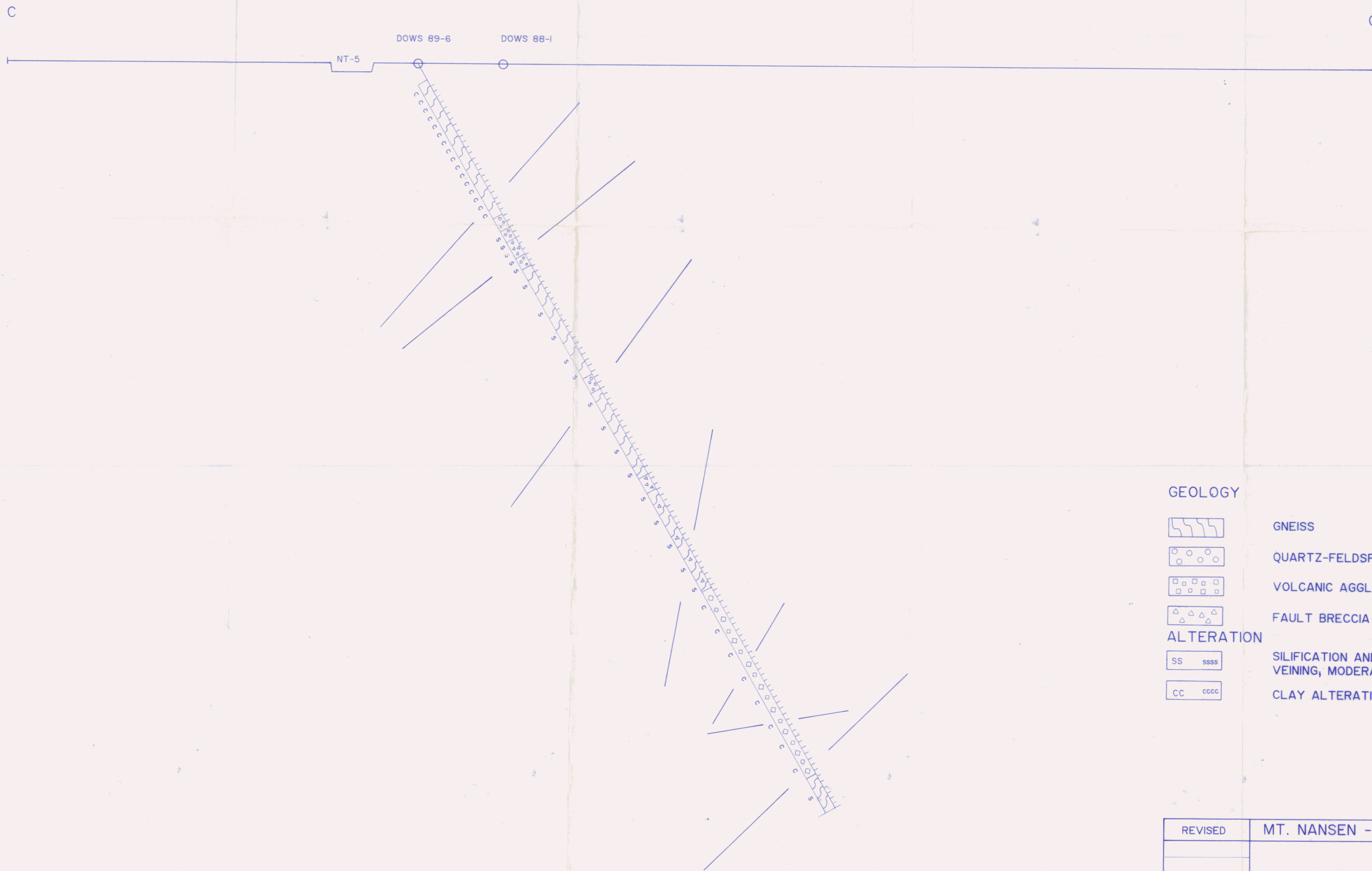
| | | |
|----------------|----------------------------|-------------------|
| REVISED | MT. NANSEN-DOWS CLAIMS | |
| | 092771 190 | |
| | DRILLING PLAN MAP | |
| | (WITH TRENCHING GEOLOGY) | |
| PROJ No. 338 | SURVEY BY K.D.G. | DATE JANUARY 1989 |
| N.T.S. 1/5 1/3 | DRAWN BY IN/EGRAPHICS LTD. | SCALE 1:500 |
| DWG No. | NORANDA EXPLORATION | |
| | OFFICE WHITEHORSE | |




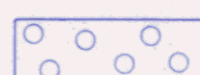

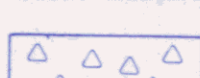
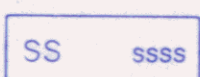
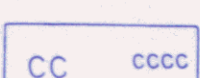
- DOWS - X DRILLED
- DOWS - X PROPOSED

092771

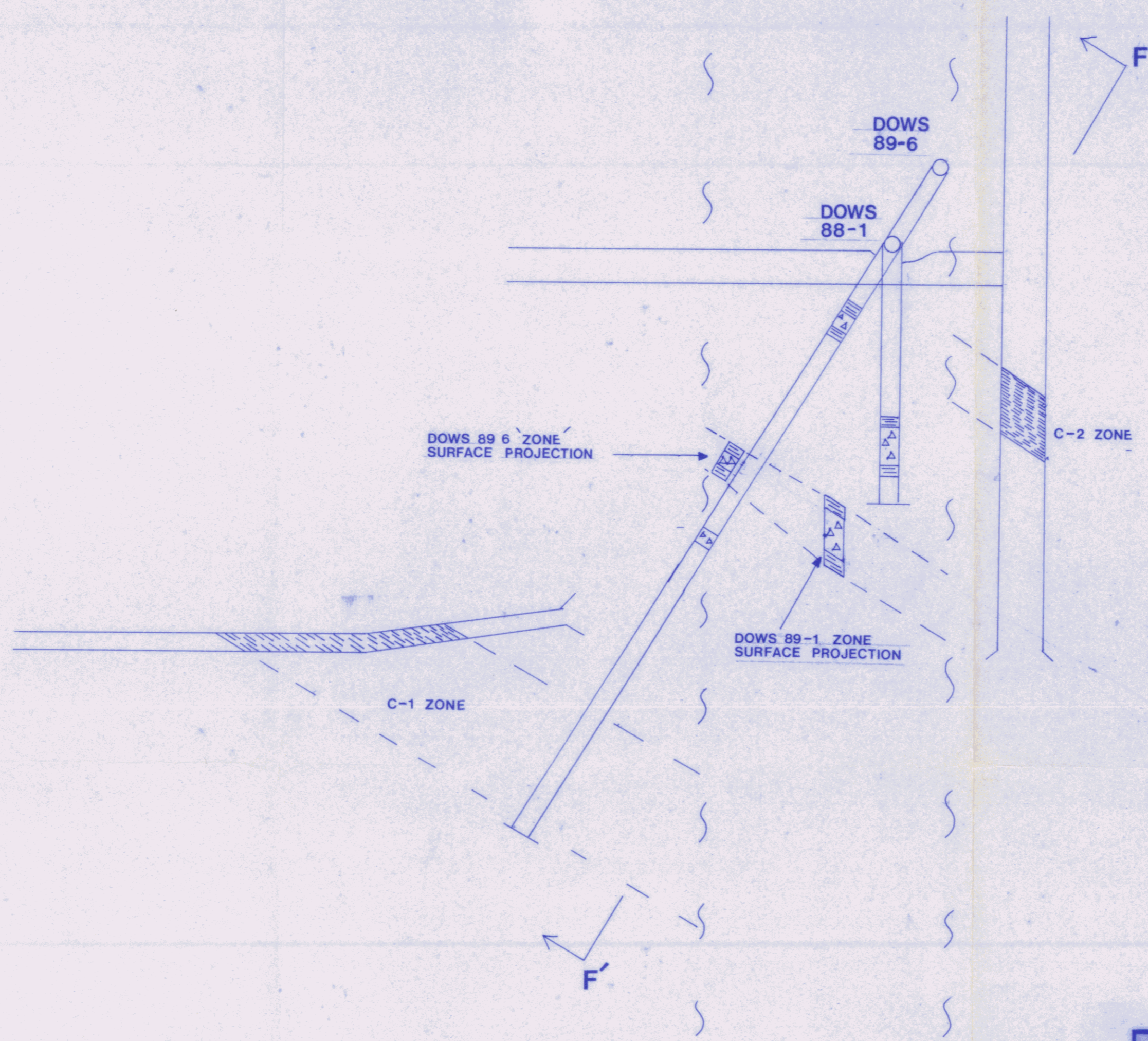
| | | |
|-----------------|----------------------------|--------------------|
| REVISED | MT. NANSEN-DOWS CLAIMS | |
| OCTOBER 1989 | 191 | |
| | DRILLING PLAN MAP | |
| PROJ. No. 338 | SURVEY BY: K.D.C. | DATE: JANUARY 1989 |
| N.T.S. 1:50,000 | DRAWN BY: M/EGRAPHICS LTD. | SCALE: 1:500 |
| DWG. No. | NORANDA EXPLORATION | |
| 9 | OFFICE: WHITEHORSE | |



GEOLOGY

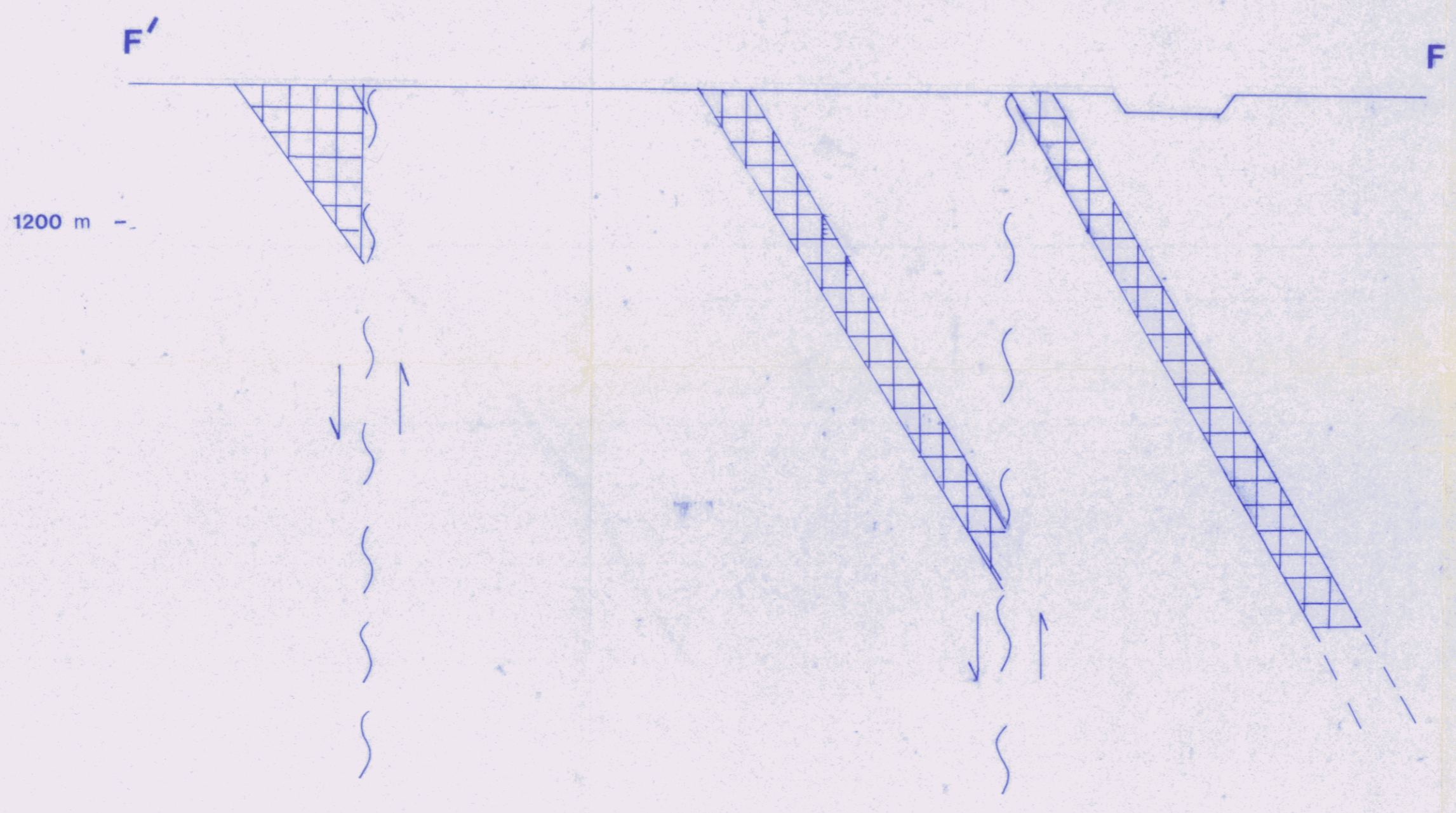
-  GNEISS
 -  QUARTZ-FELDSPAR PORPHYRY
 -  VOLCANIC AGGLOMERATE
 -  FAULT BRECCIA
- ALTERATION**
-  SILIFICATION AND/OR QUARTZ VEINING, MODERATE, STRONG
 -  CLAY ALTERATION: MODERATE, STRONG

| | | |
|----------------------------|---|--------------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | SECTION C-C' 192 | |
| | 092771 115 13 | |
| | (LOOKING SOUTHEAST) | |
| PROJ. No. 336 | SURVEYED BY, R.D. | DATE: OCTOBER 1989 |
| N.T.S. 1/5 1/3 | | SCALE 1:500 |
| NORANDA EXPLORATION | | |
| OFFICE.....WHITEHORSE | | |



10400N
L 9200 E

| | | |
|-----------|----------------------------|--------------|
| REVISED | | |
| | PLAN VIEW | |
| PROJ. No. | SURVEY BY: | DATE: 1.3.00 |
| N.T.S. | DRAWN BY: | SCALE: |
| DWG. No. | NORANDA EXPLORATION | |
| | OFFICE | |

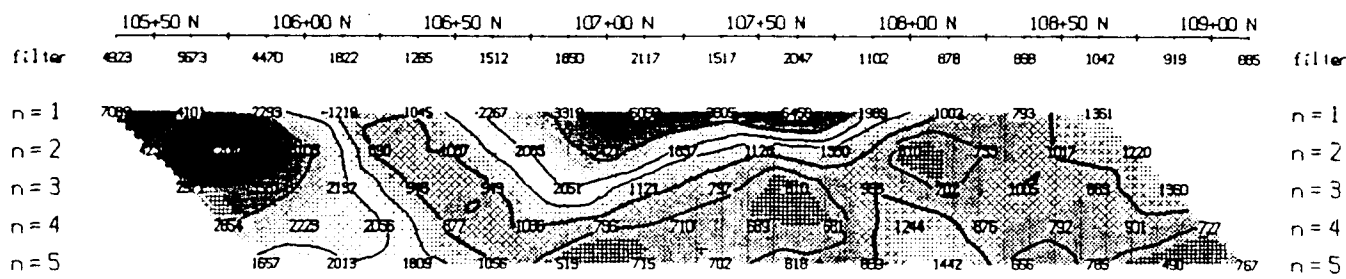
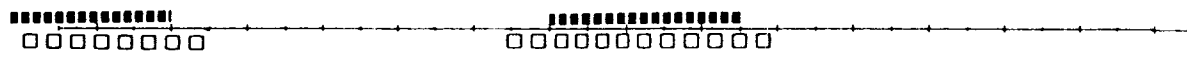
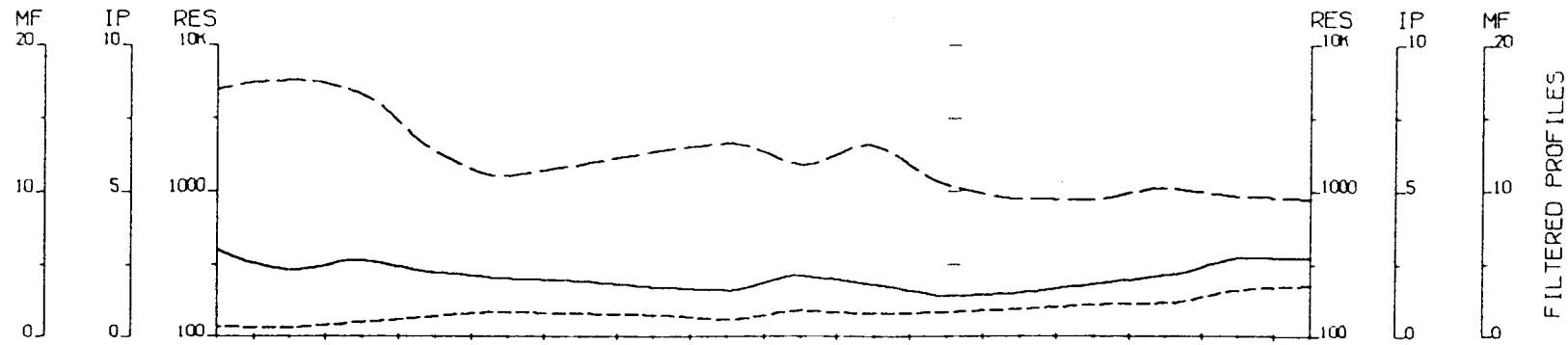


MINERALIZED ZONE

092771

| | | |
|---------------|---------------------------------|--------------------|
| REVISED | MT. NANSEN - DOWS CLAIMS | |
| | LONG SECTION F-F | |
| | (LOOKING NORTHWEST) | |
| PROJ. No. 338 | SURVEY BY: R.D. | DATE: OCTOBER 1999 |
| N.T.S. 1151/3 | DRAWN BY: | SCALE: 1:500 |
| DWG. No. 11 | NORANDA EXPLORATION | |
| | OFFICE | |

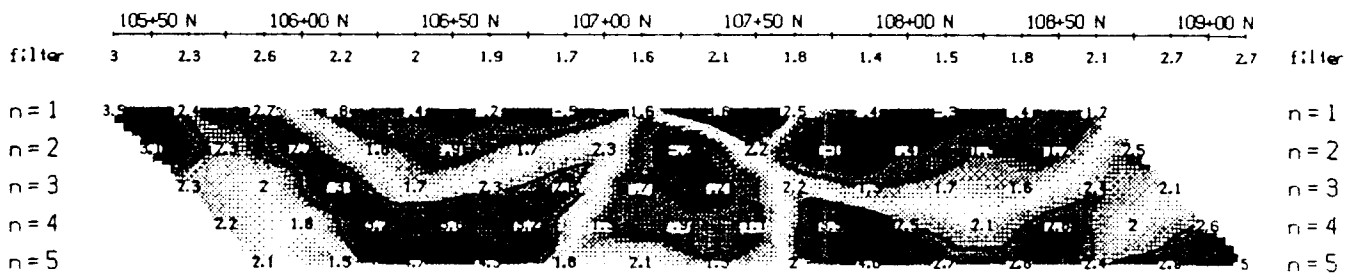
APPENDIX I
GEOPHYSICS RESULTS



INTERP

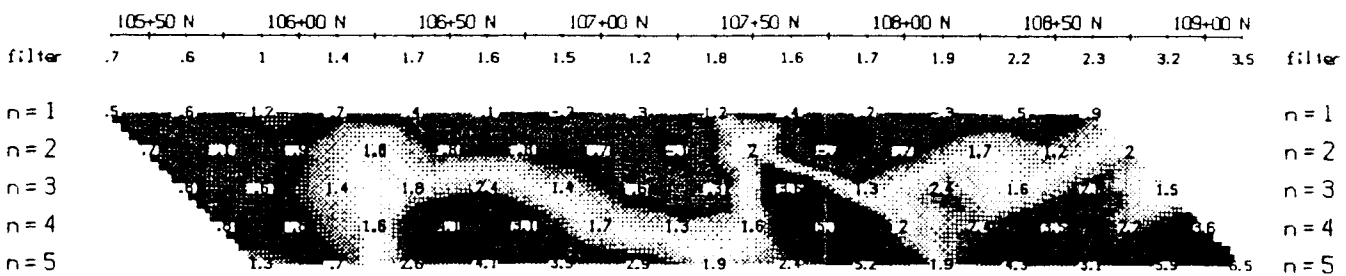
RESISTIVITY

(ohm-m)



Chargeability

(msec)

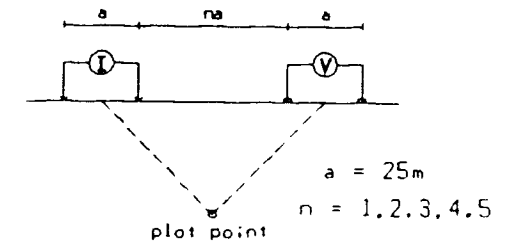


METAL FACTOR

(ip/res * 1000)

Line 8400 E

Dipole-Dipole Array



Filtered Profiles

| | | | |
|--------------|-------|--------|------|
| Resistivity | ----- | filter | * |
| Polarization | ===== | | ** |
| Metal Factor | ----- | | *** |
| | | | **** |

Logarithmic Contours
1, 3, 5, 7.5, 10, ...

Instrument : EOA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

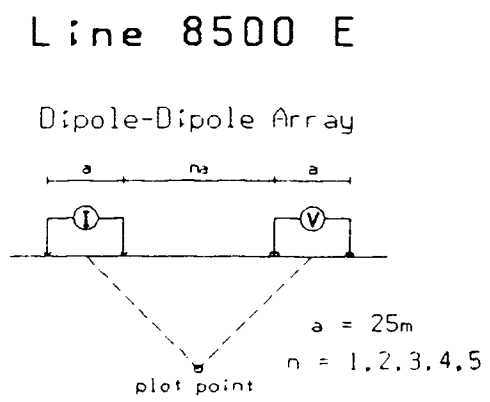
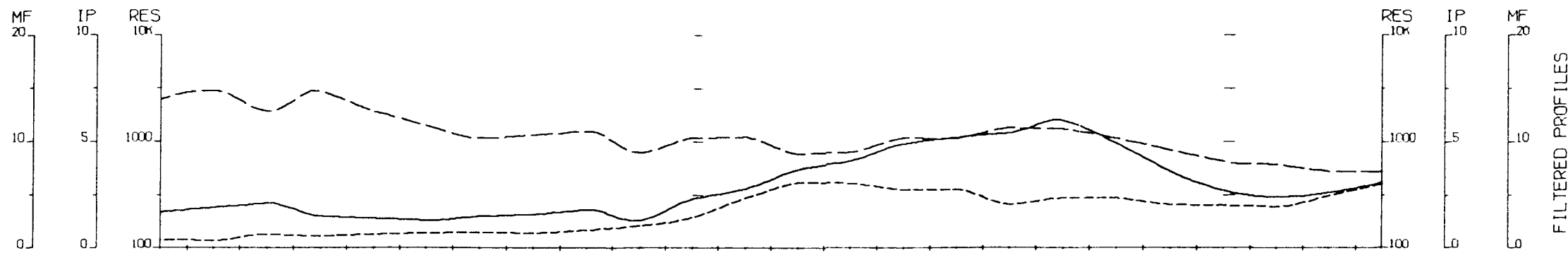
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

Line 8400 E
Yukon

Date: 89/06/15 N.T.S 115/I
Interpretation by: L. Bradish
Scale: 1 : 2500

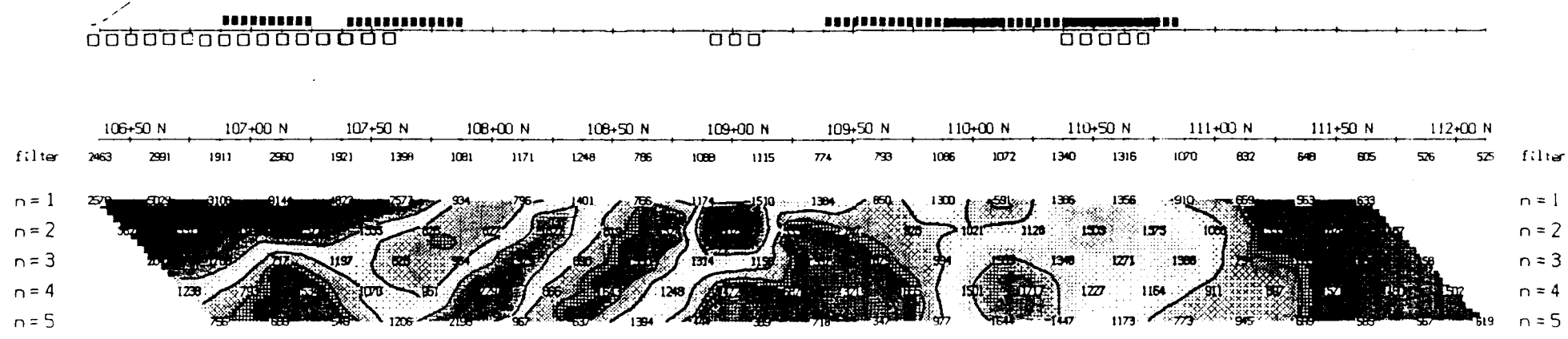
n o r a n d a



INTERP

Filtered Profiles

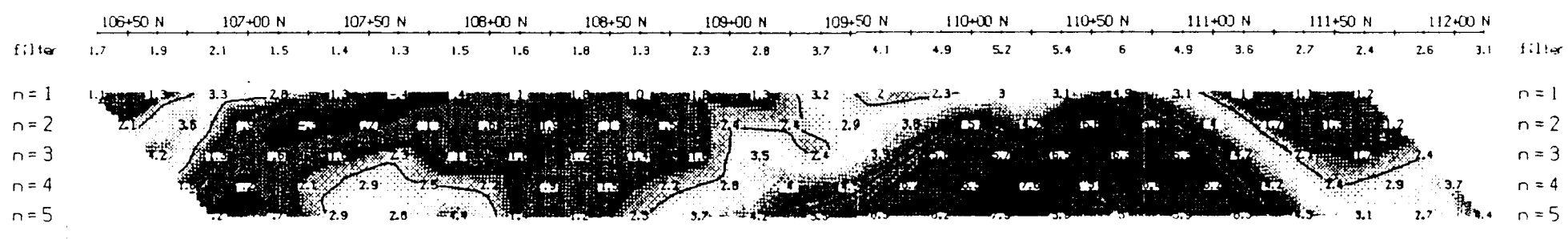
| | | |
|--------------|-------|---------|
| Resistivity | ----- | filter |
| Polarization | ===== | * * |
| Metal Factor | ----- | * * * |
| | | * * * * |



RESISTIVITY (ohm-m)

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

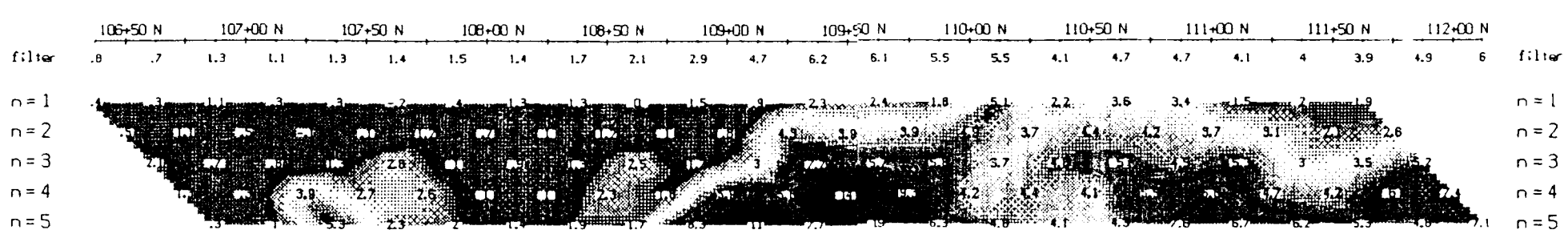
Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH



Chargeability (msec)

INTERPRETATION

- █ Strong increase in polarization
- ▒ Moderate increase in polarization
- Pronounced resistivity increase
- ===== Pronounced resistivity decrease



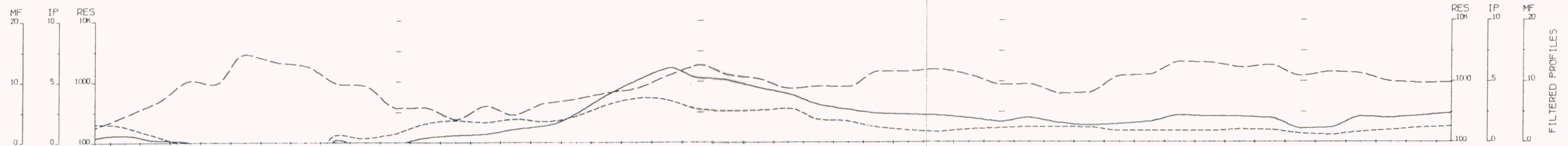
METAL FACTOR (ip/res * 1000)

MT. NANSEN PROJECT

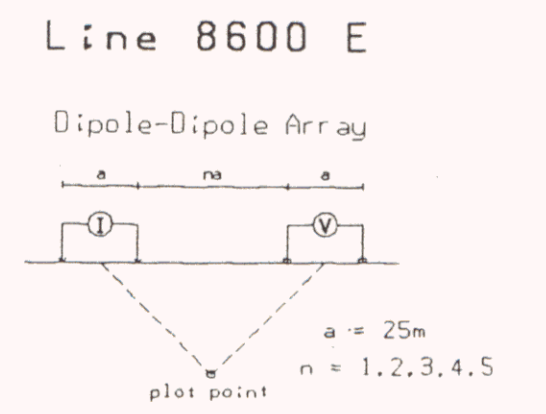
INDUCED POLARIZATION SURVEY
Line 8500 E
Yukon

Date: 89/06/15 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a



FILTERED PROFILES



INTERP

Filtered Profiles

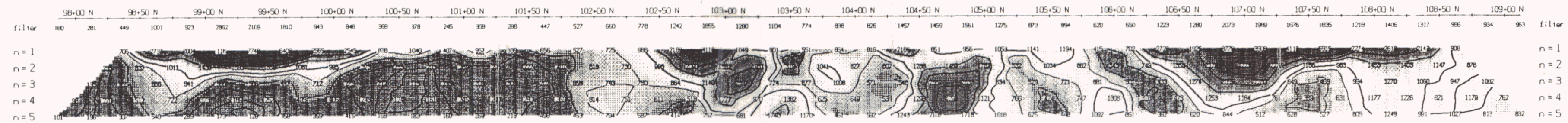
| | | |
|--------------|-----|--------|
| Resistivity | --- | filter |
| Polarization | --- | * |
| Metal Factor | --- | ** |
| | | *** |
| | | **** |

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

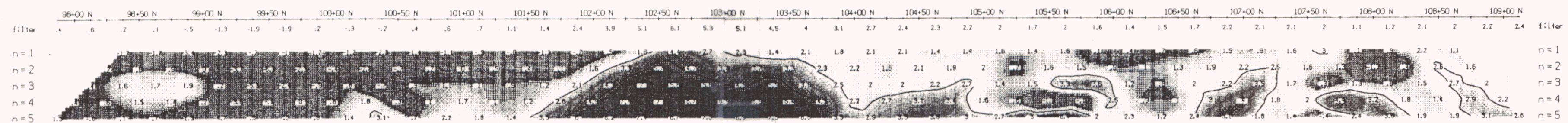
Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

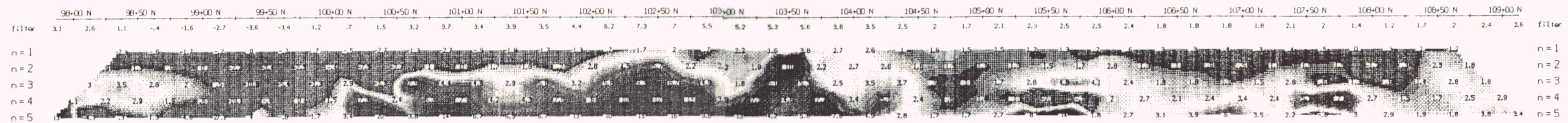
- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease



RESISTIVITY (ohm-m)



Chargeability (msec)



METAL FACTOR (ip/res * 1000)

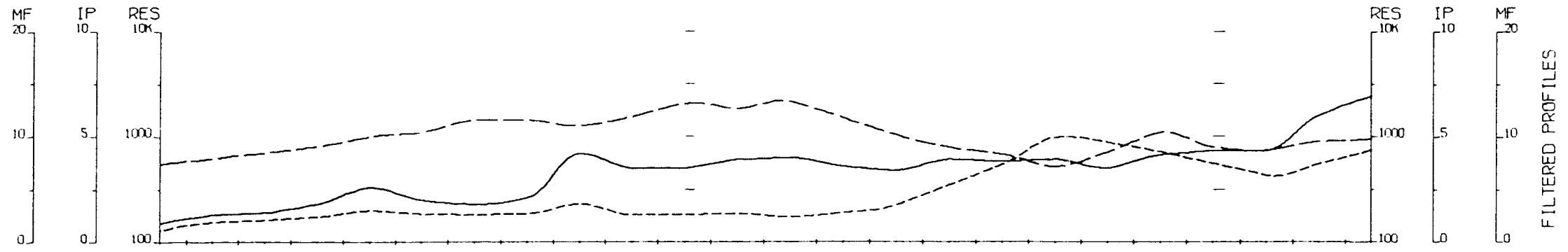
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

Line 8600 E
Yukon

Date: 89/06/16 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

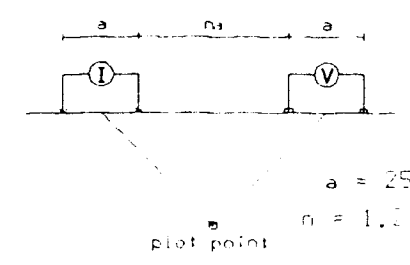
n o r a n d a



FILTERED PROFILES

Line 8700 E

Dipole-Dipole Array

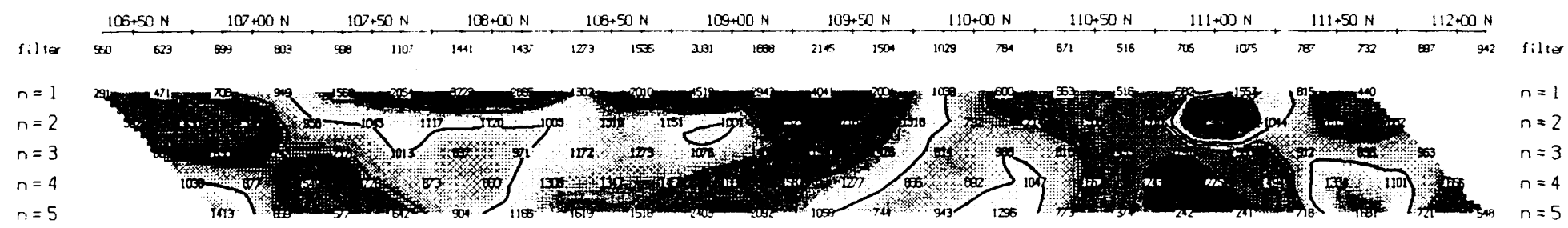


a = 25m
n = 1, 2, 3, 4, 5

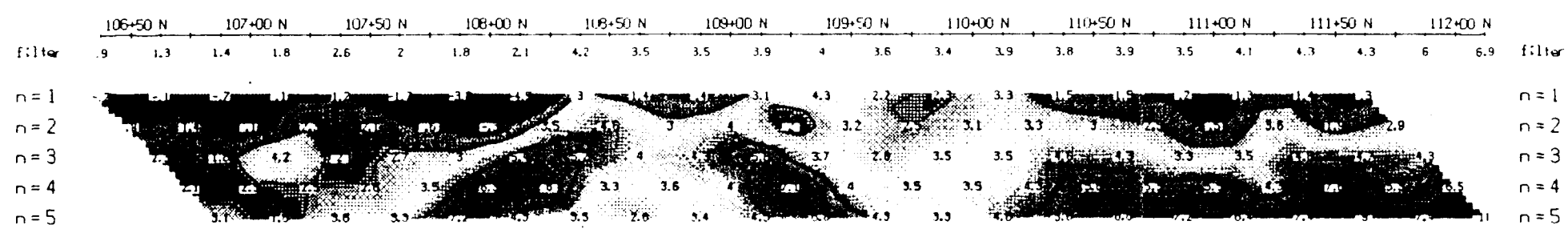
INTERP

Filtered Profiles

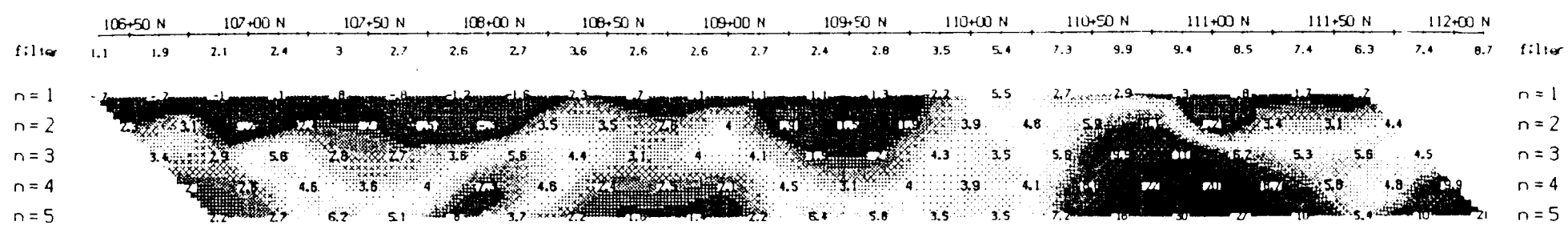
Resistivity filter *
 Polarization **
 Metal Factor ***



RESISTIVITY
(ohm-m)



Chargeability
(msec)



METAL FACTOR
(ip/res * 1000)

Logarithmic Contours 1, 3, 5, 7.5, 10, ...
 Instrument : EDA IP 6
 Time Base : 2 sec
 Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

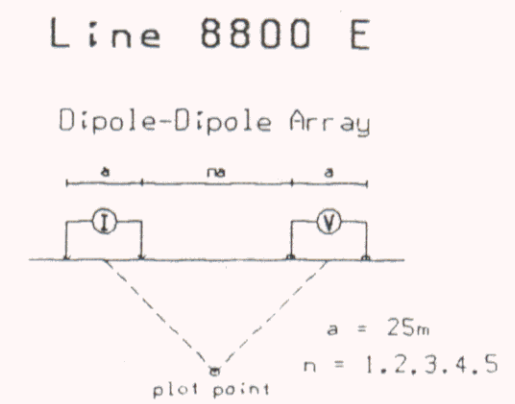
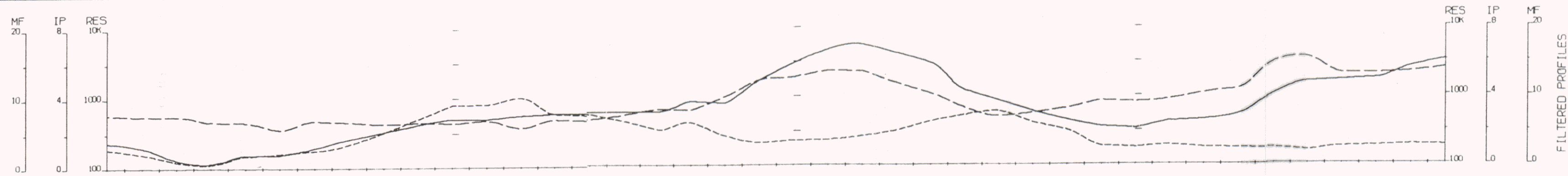
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

Line 8700 E
Yukon

Date: 89/06/15 N.T.S 115/1
 Interpretation by: L. Bradish
 Scale: 1 : 2500

n o r a n d a



INTERP

Filtered Profiles

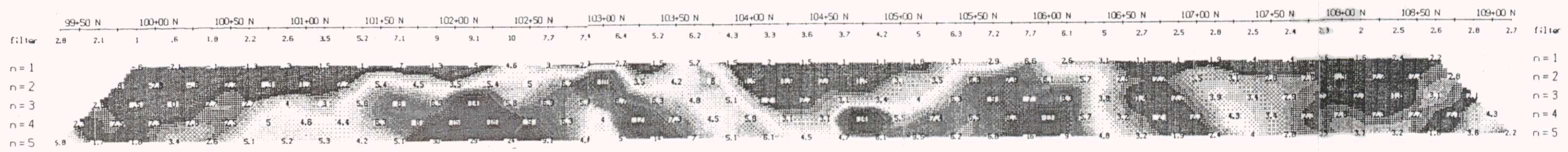
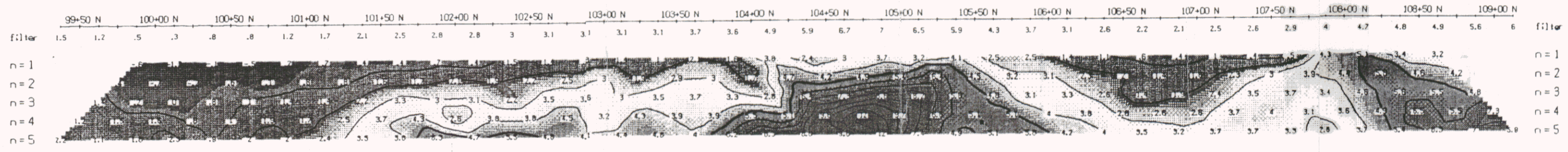
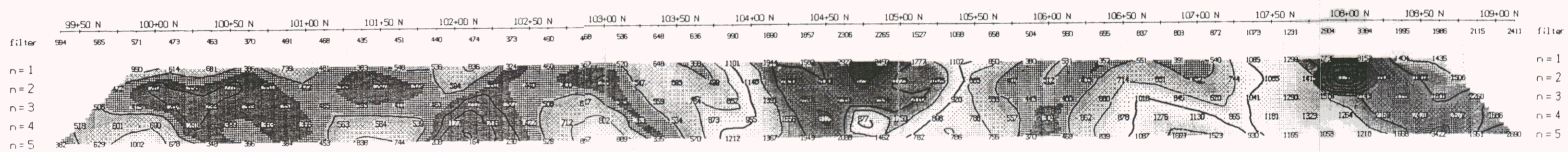
Resistivity ——— filter *
Polarization - - - - - **
Metal Factor - - - - - ***

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Chargeability (msec)
- █ Strong increase in polarization
 - ▒ Moderate increase in polarization
 - Pronounced resistivity increase
 - ▬▬▬ Pronounced resistivity decrease



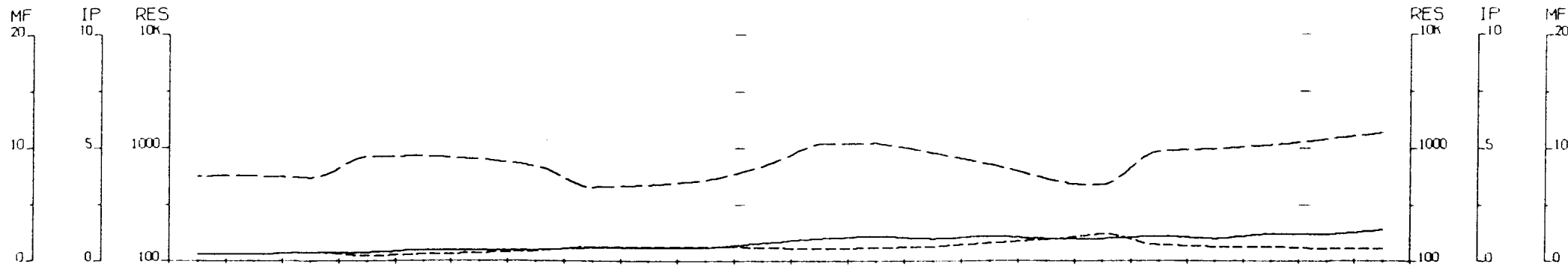
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

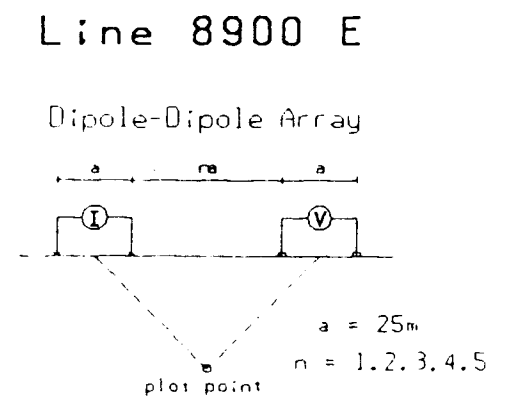
Line 8800 E
Yukon

Date: 89/06/19 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a



INTERP



Filtered Profiles

Resistivity ----- filter
Polarization ----- * *
Metal Factor ----- * * * *

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

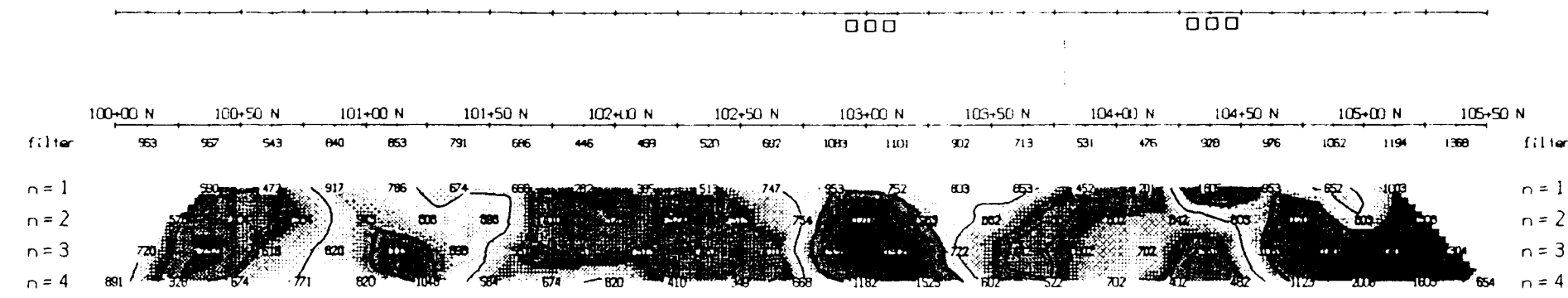
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

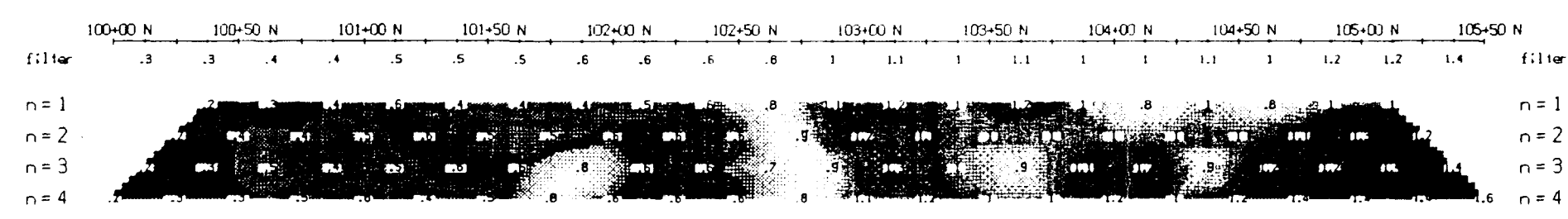
Line 8900 E
Yukon

Date: 89/06/15 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

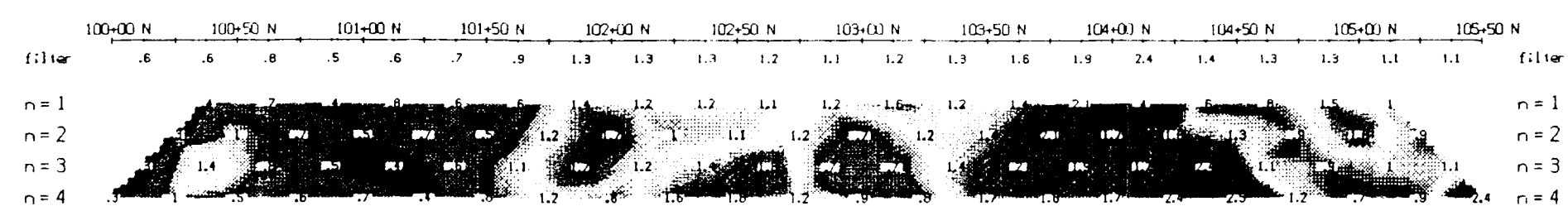
n o r a n d a



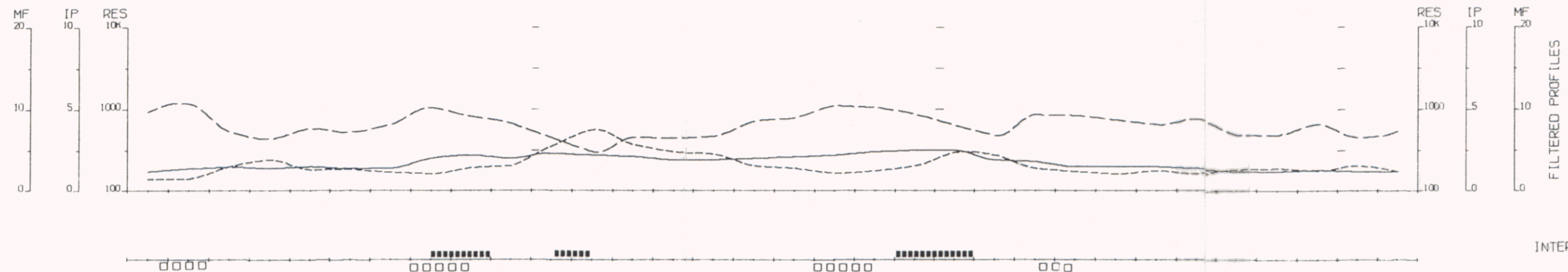
RESISTIVITY
(ohm-m)



Chargeability
(msec)

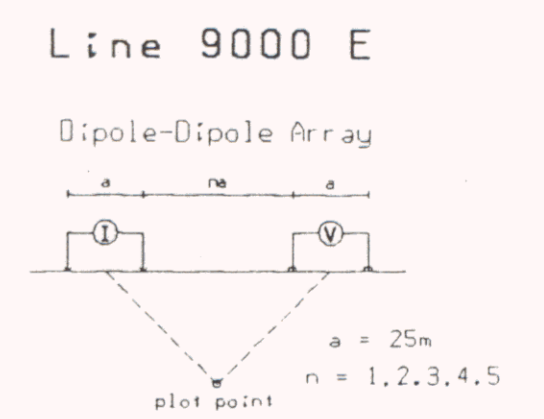


METAL FACTOR
(ipines * 1000)



FILTERED PROFILES

INTERP



Filtered Profiles

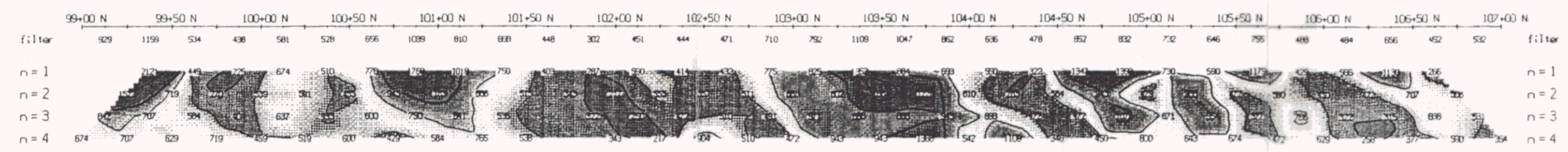
Resistivity ——— filter
Polarization ——— * *
Metal Factor - - - - - * * *
* * * *

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

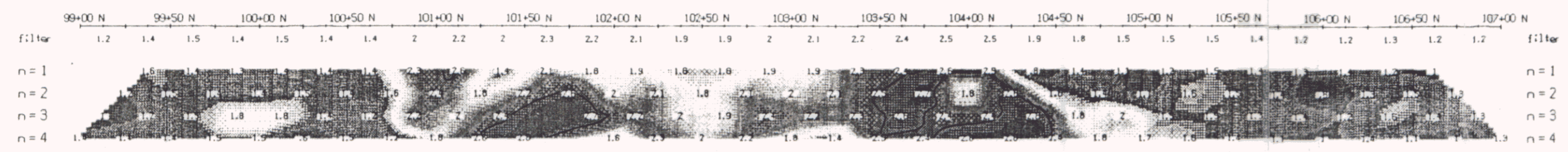
Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

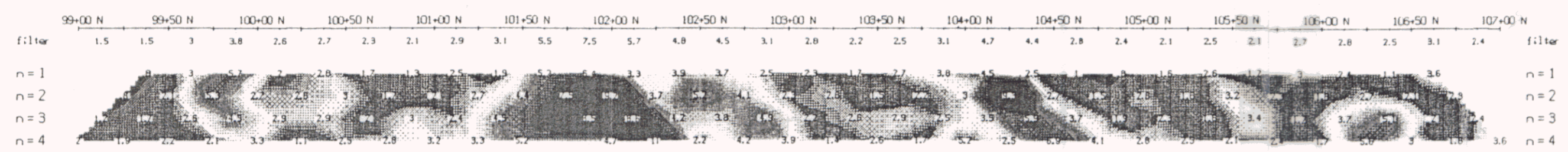
- █ Strong increase in polarization
- ▒ Moderate increase in polarization
- Pronounced resistivity increase
- ══ Pronounced resistivity decrease



RESISTIVITY (ohm-m)



Chargeability (msec)



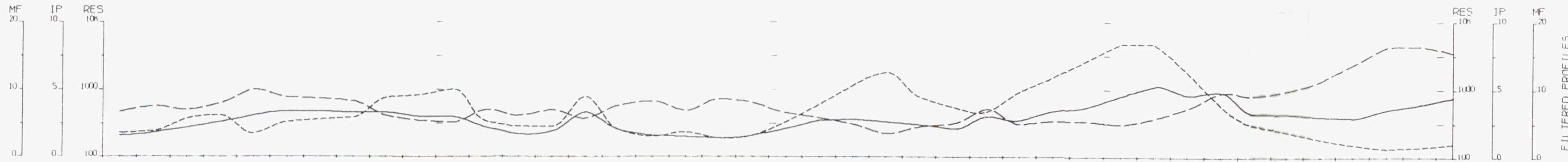
METAL FACTOR (ip/res * 1000)

MT. NANSEN PROJECT

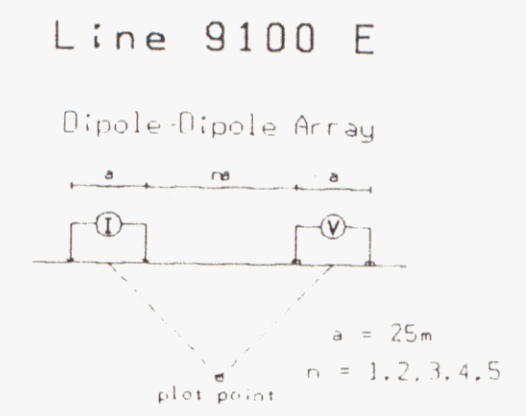
INDUCED POLARIZATION SURVEY
Line 9000 E
Yukon

Date: 89/06/15 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a .



FILTERED PROFILES



INTERP

Filtered Profiles

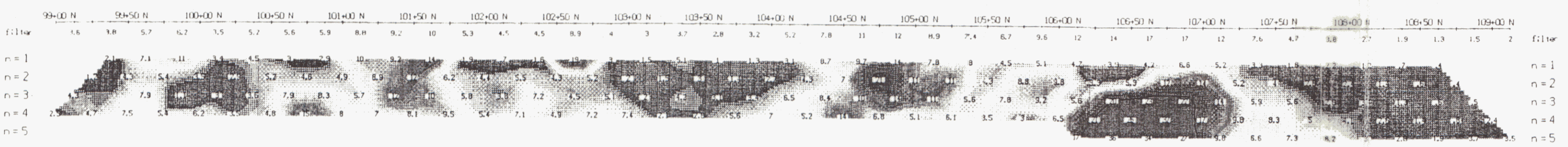
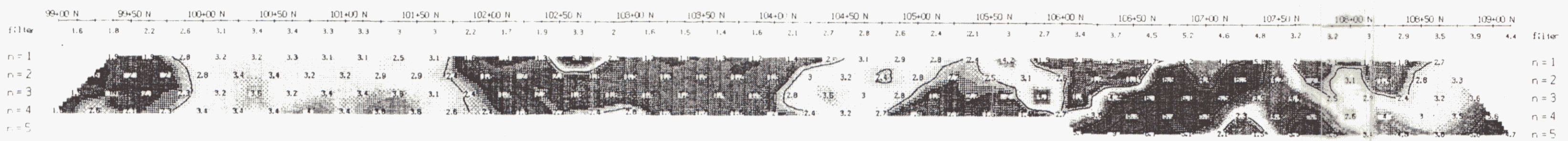
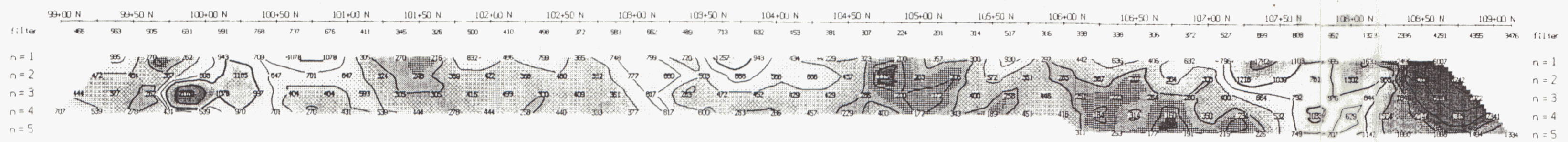
Resistivity filter
Polarization +
Metal Factor + + +
+ + + +

Logarithmic
Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Chargeability (msec)
- Strong increase in polarization
 - Moderate increase in polarization
 - Pronounced resistivity increase
 - Pronounced resistivity decrease

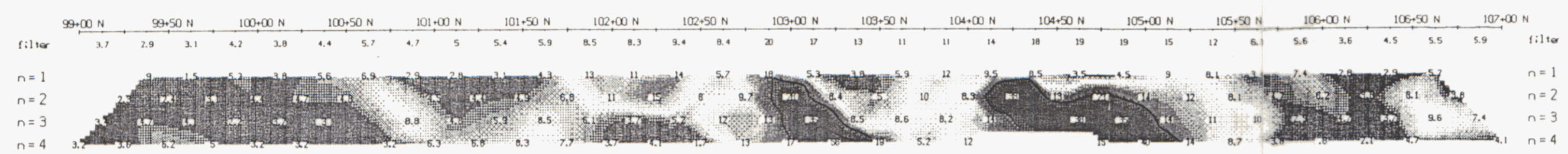
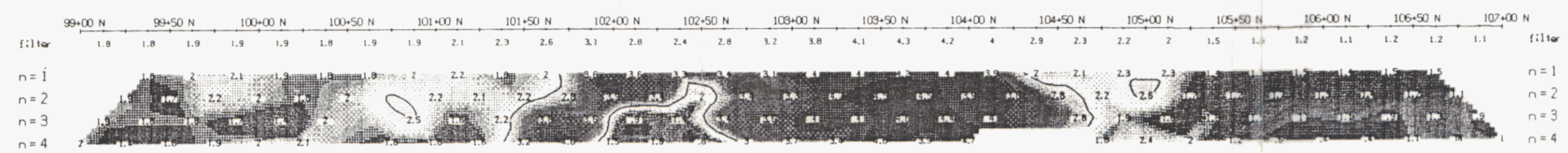
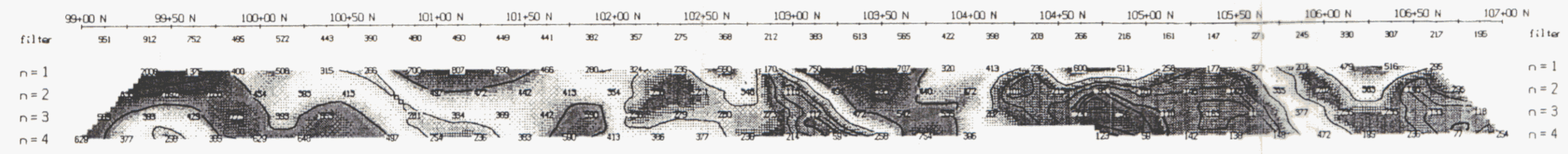
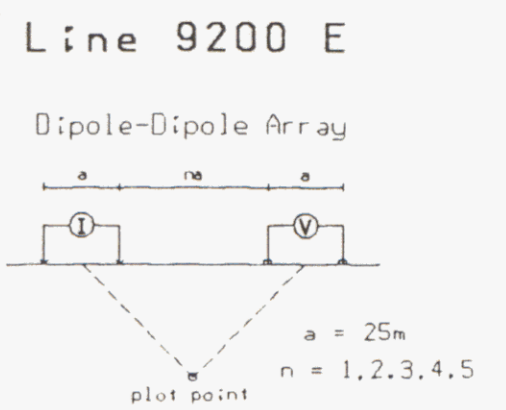
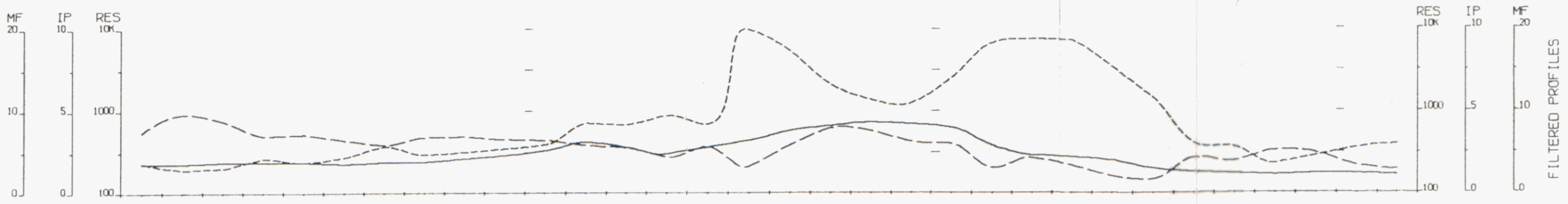


MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY
Line 9100 E
Yukon

Date: 89/06/15 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a



INTERP

Filtered Profiles

Resistivity
Polarization
Metal Factor

filter
*
**

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

Strong increase in polarization
Moderate increase in polarization
Pronounced resistivity increase
Pronounced resistivity decrease

MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

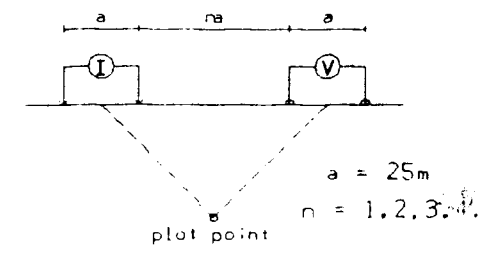
Line 9200 E
Yukon

Date: 89/06/15 N.T.S 115/1
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a

Line 9300 E

Dipole-Dipole Array



Filtered Profiles

- Resistivity
 - Polarization
 - Metal Factor
- Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
 Time Base : 2 sec
 Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

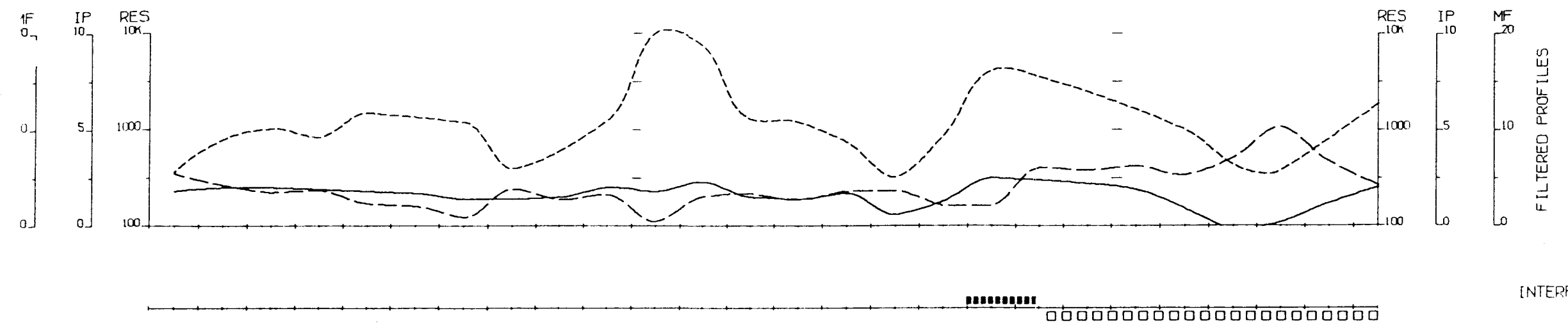
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

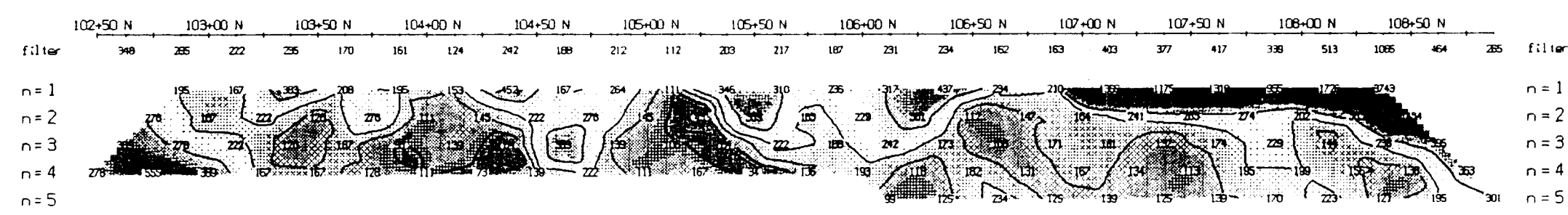
Line 9300 E
 Yukon

Date: 89/06/15 N.T.S 115/1
 Interpretation by: L. Bradish
 Scale: 1 : 2500

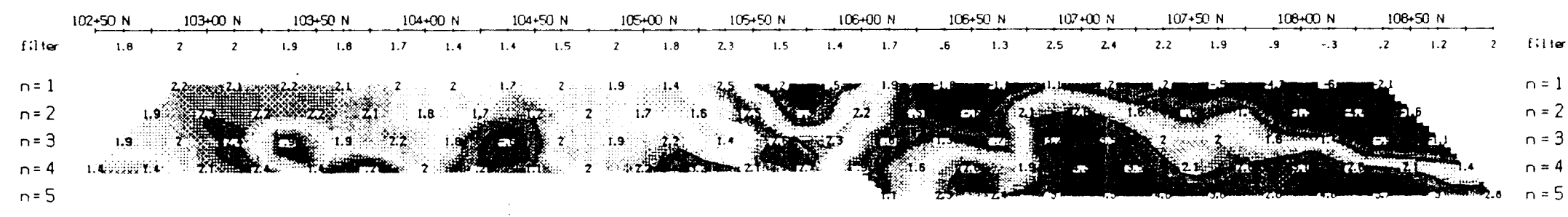
n o r a n d a



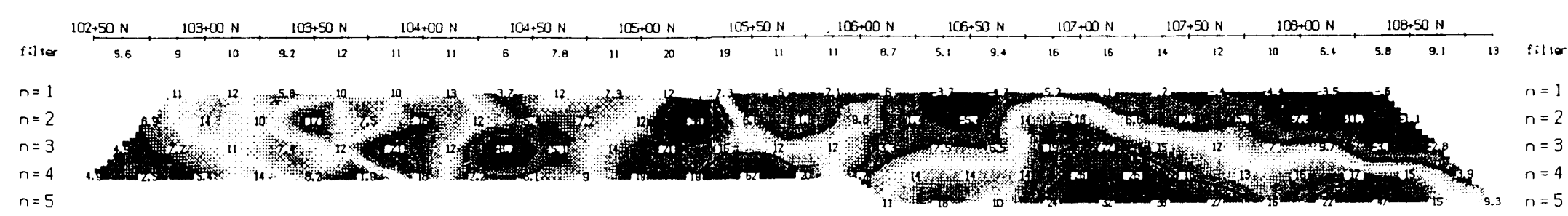
[INTERP]



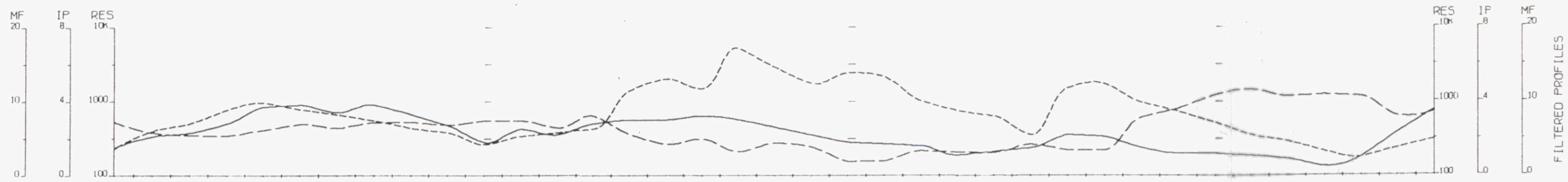
RESISTIVITY
 (ohm-m)



Chargeability
 (insec)



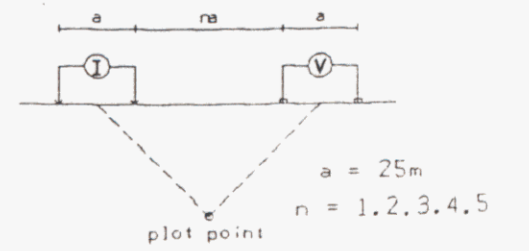
METAL FACTOR
 (ip/res * 1000)



FILTERED PROFILES

Line 9500 E

Dipole-Dipole Array



INTERP

Filtered Profiles

Resistivity ———— filter
 Polarization ———— * *
 Metal Factor - - - - * * * *

Logarithmic
 Contours 1, 3, 5, 7.5, 10, ...

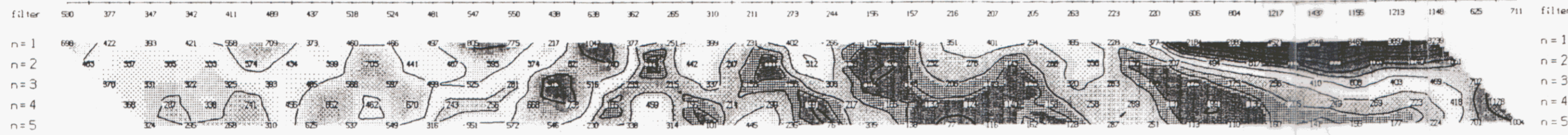
Instrument : EDA IP 6
 Time Base : 2 sec
 Operator : MPH

INTERPRETATION

- █ Strong increase in polarization
- ▣ Moderate increase in polarization
- Pronounced resistivity increase
- ▬ Pronounced resistivity decrease

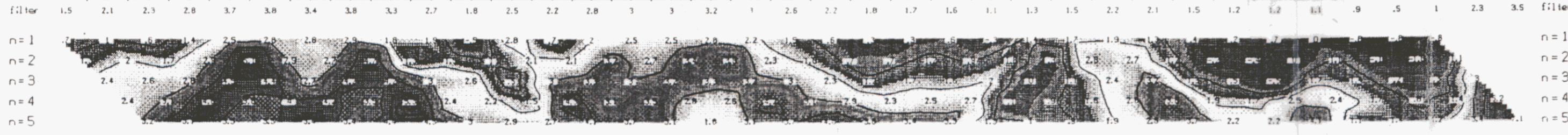


100+50 N 101+00 N 101+50 N 102+00 N 102+50 N 103+00 N 103+50 N 104+00 N 104+50 N 105+00 N 105+50 N 106+00 N 106+50 N 107+00 N 107+50 N 108+00 N 108+50 N 109+00 N



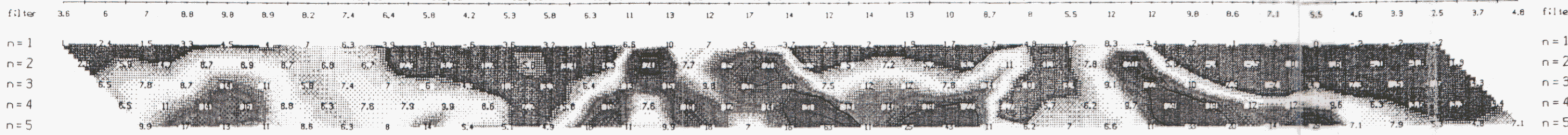
RESISTIVITY
 (ohm-m)

100+50 N 101+00 N 101+50 N 102+00 N 102+50 N 103+00 N 103+50 N 104+00 N 104+50 N 105+00 N 105+50 N 106+00 N 106+50 N 107+00 N 107+50 N 108+00 N 108+50 N 109+00 N



Chargeability
 (msec)

100+50 N 101+00 N 101+50 N 102+00 N 102+50 N 103+00 N 103+50 N 104+00 N 104+50 N 105+00 N 105+50 N 106+00 N 106+50 N 107+00 N 107+50 N 108+00 N 108+50 N 109+00 N



METAL FACTOR
 (ip/res * 1000)

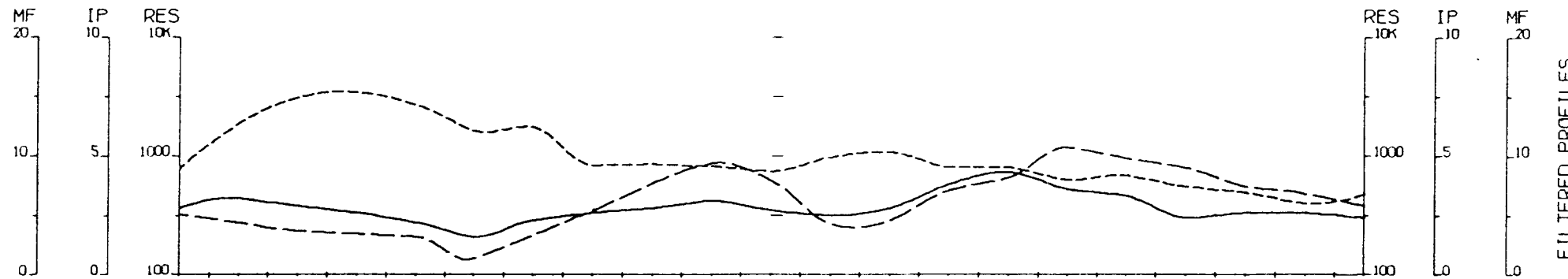
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

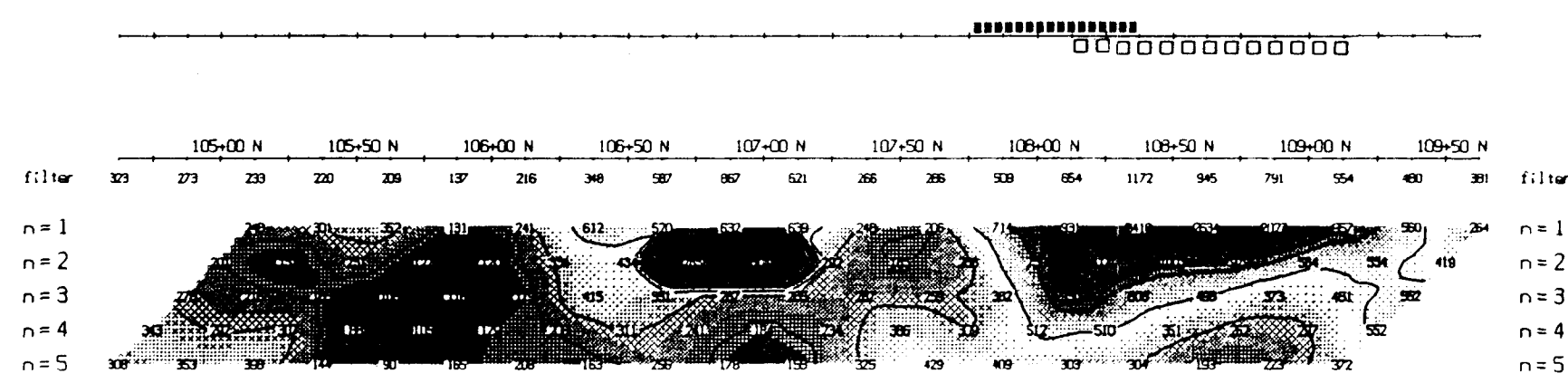
Line 9500 E
 Yukon

Date: 89/06/15 N.T.S 115/1
 Interpretation by: L. Bradish
 Scale: 1 : 2500

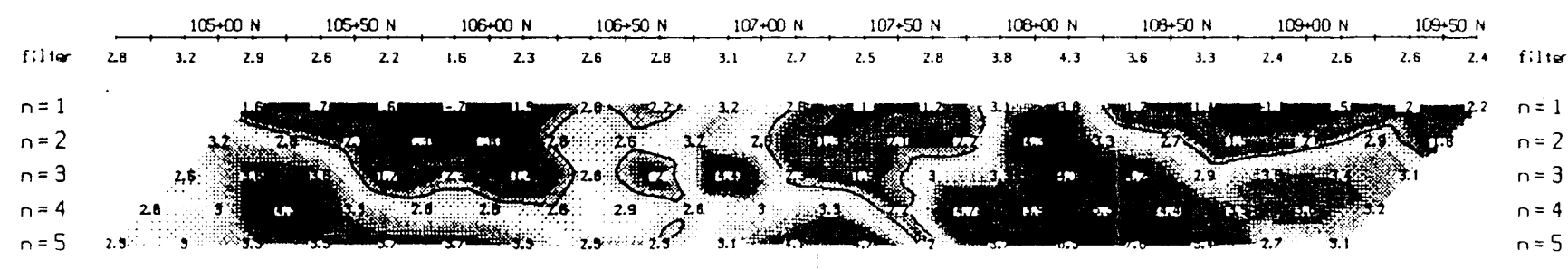
n o r a n d a



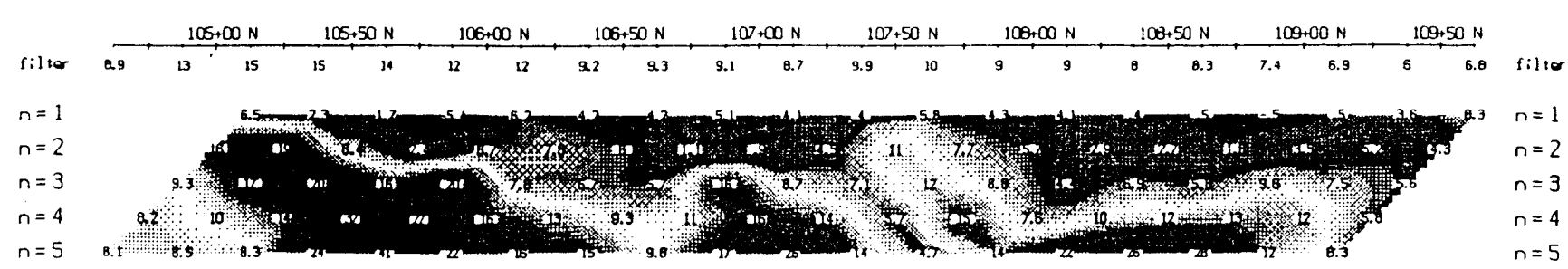
INTERP



RESISTIVITY
(ohm-m)



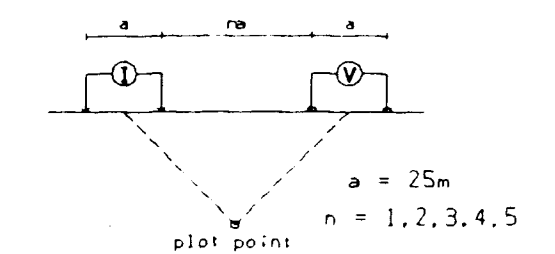
Chargeability
(msec)



METAL FACTOR
(ip/res * 1000)

Line 9600 E

Dipole-Dipole Array



Filtered Profiles

| | | |
|--------------|-----------|--------|
| Resistivity | ----- | filter |
| Polarization | ===== | ** |
| Metal Factor | -.-.-.-.- | **** |

Logarithmic
Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

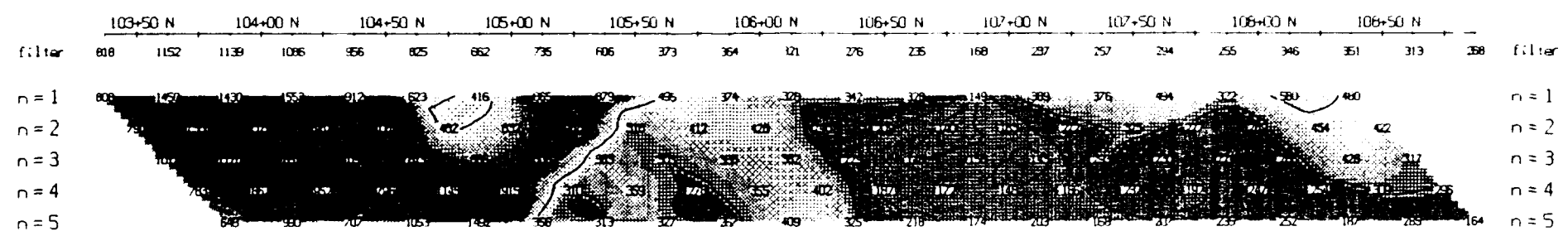
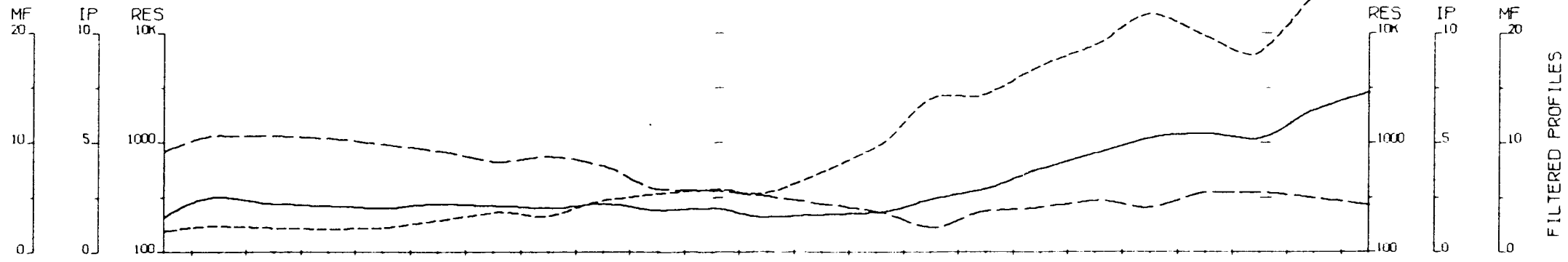
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

Line 9600 E
Yukon

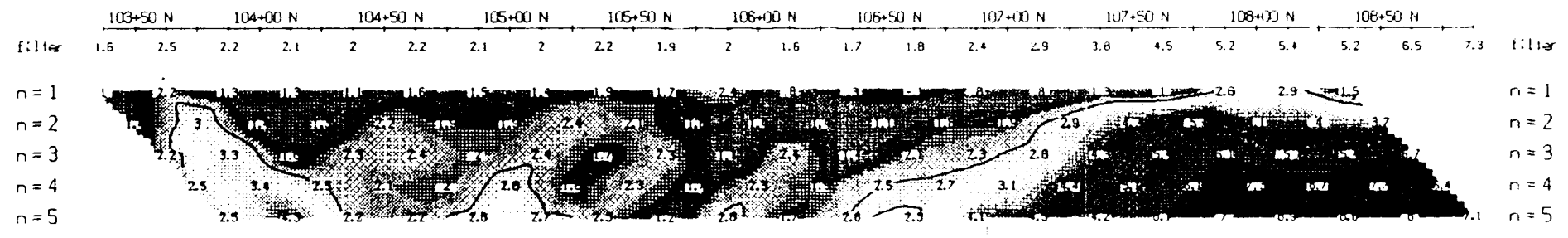
Date: 89/06/15 N.T.S 115/I
Interpretation by: L. Bradish
Scale: 1 : 2500

n o r a n d a

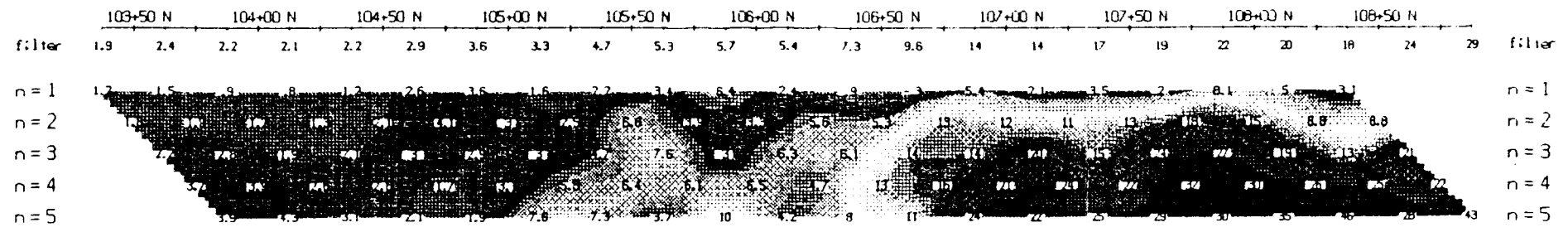


INTERP

RESISTIVITY
(ohm-m)



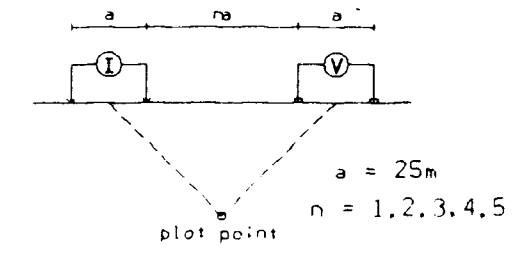
Chargeability
(msec)



METAL FACTOR
(ip/res * 1000)

Line 9700 E

Dipole-Dipole Array



Filtered Profiles

Resistivity filter *

Polarization **

Metal Factor ***

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
Time Base : 2 sec
Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

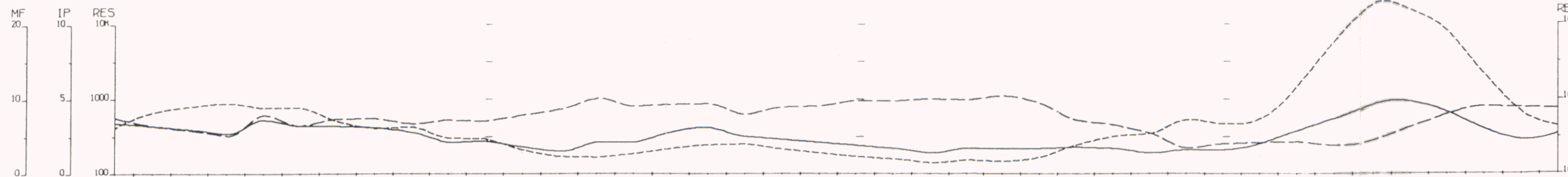
MT. NANSEN PROJECT

INDUCED POLARIZATION SURVEY

Line 9700 E
Yukon

Date: 89/06/15 N.T.S 115/I
Interpretation by: L. Bradish
Scale: 1 : 2500

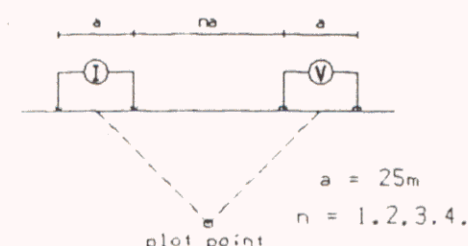
n o r a n d a



FILTERED PROFILES

Line 9800 E

Dipole-Dipole Array



INTERP

Filtered Profiles

Resistivity filter
 Polarization * * *
 Metal Factor * * * *

Logarithmic Contours 1, 3, 5, 7.5, 10, ...

Instrument : EDA IP 6
 Time Base : 2 sec
 Operator : MPH

INTERPRETATION

- Strong increase in polarization
- Moderate increase in polarization
- Pronounced resistivity increase
- Pronounced resistivity decrease

MT. NANSEN PROJECT

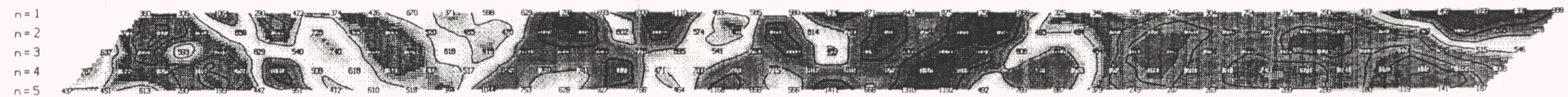
INDUCED POLARIZATION SURVEY

Line 9800 E
 Yukon

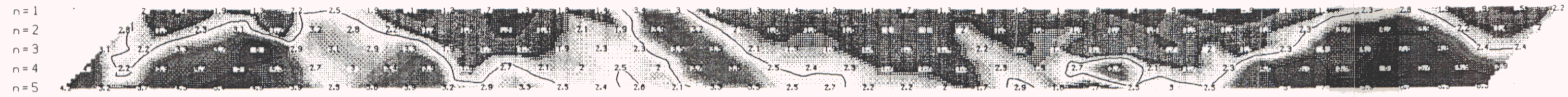
Date: 89/06/16 N.T.S 115/1
 Interpretation by: L. Bradish
 Scale: 1 : 2500

n o r a n d a

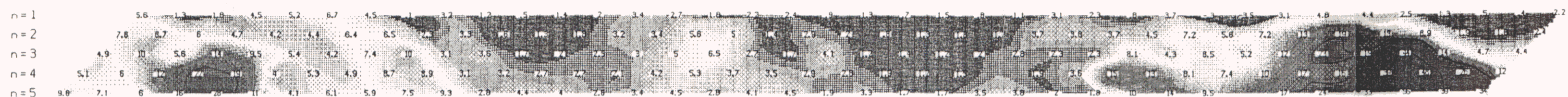
filter 559 441 366 325 608 442 541 550 470 524 506 609 723 1013 795 647 860 626 773 802 941 941 1008 971 1102 880 527 485 363 221 252 261 267 239 277 417 612 785 770 745 filter



filter 3.4 3.2 3 2.7 3.6 3.2 3.2 3.1 2.8 2.1 2.2 1.8 1.5 2.1 2.1 2.8 3.1 2.5 2.3 2.1 1.9 1.7 1.4 1.7 1.7 1.7 1.8 1.7 1.4 1.6 1.6 2 2.9 3.7 4.6 4.8 4.1 3 2.3 2.7 filter



filter 6.2 8.2 9 9.4 8.8 8.8 7 6.1 6.3 4.8 4.7 3.2 2.3 2.2 2.7 3.4 3.9 4 3.3 2.8 2.3 2 1.5 1.8 1.7 2.2 3.9 5 5.4 7.2 6.7 7.3 12 18 29 22 18 13 6.3 6.4 filter



APPENDIX II

DRILL LOGS

| FROM | TO | ROCK TYPE | DESCRIPTION | GEOTECH | | | | | GEOCHEM | | | | | SAMPLING | | |
|-------|-------|-----------|--|---------|------|-------------|--------------|---------|---------------------|-------|-------|------------|--------------|----------|-------|------------|
| | | | | FROM | TO | % RECO-VERY | BREAK-AGE | % SULPH | STRUCTURE ° TO C.A. | FROM | TO | CLAY ALT'N | SILICA ALT'N | FROM | TO | SAMPLE No. |
| 40.25 | 43.5 | | <u>INTRUSIVE DYKE (?)</u> BUFF - LIGHT GREY IN COLOR DISSEMINATED Py ON FRACTURES AND ALONG FOLIATIONS. SOME DISTORTION MINOR APPLE GREEN CLAY | 40.25 | 43.5 | 82% | A | 1-3 | | 40.25 | 43.5 | 2-1 | 3-2 | 39.0 | 40.25 | 12394 DR |
| | | | | 40.25 | | | | | | | | | | 40.25 | 42.0 | 12395 |
| | | | | 40.25 | | | SHEARING | | 60° | | | | | 42.0 | 43.5 | 12396 |
| | | | | | | | | | | | | | | | | |
| | | | | | | | SLICKENSIDES | | 80° | | | | | | | |
| | | | | 41.5 | | | FOLIATION | | 55° | | | | | | | |
| 43.5 | 46.5 | | <u>ZONE (C2)</u> MED - DK GREY IN COLOR FINE GRAINED PYRITIC ZONE MINOR MEDIUM GREY QTZ VEINS | 43.5 | 46.5 | 85% | A-C | 3-5 | | 43.5 | 46.5 | 1-2 | 1 | 43.5 | 45.0 | 12397 |
| | | | | | | | | | | | | | | 45.0 | 46.5 | 12398 |
| 46.5 | 50.8 | | <u>BX ZONE</u> MEDIUM TO DARK GREY PYRITIC MATRIX SUPPORTING ANGULAR FRAGMENTS OF STRONGY CLAY ALT'D PORPH(?) | 46.5 | 51.0 | 92% | C-B | 10-20 | | 46.5 | 51.0 | 1 | 2-1 | 46.5 | 48.0 | 12399 |
| | | | | | | | | | | | | | | 48.0 | 49.5 | 12400 |
| | | | | | | | | | | | | | | 49.5 | 51.0 | 12401 |
| 50.8 | 53.6 | | <u>ZONE</u> SIMILAR TO 'ZONE' FROM 43.5-46.5 | 51.0 | 54.0 | 55% | A | TR-3% | | 51.0 | 53.6 | 2-1 | (1) | 51.0 | 52.5 | 12402 |
| | | | | | | | | | | | | | | 52.5 | 54.0 | 12403 |
| 53.6 | 83.82 | | <u>GNEISS</u> MEDIUM GREY TO GREEN IN COLOR WELL FOLIATED | 54.0 | 72.0 | 95% | B-C | TR | | 53.6 | 83.82 | 1-2 | | 54.0 | 55.5 | 12404 |
| | | | | | | | | | | | | | | 55.5 | 57.0 | 12405 |
| | | | | | | | | | | | | | | 57.0 | 58.5 | 12406 |
| | | | | | | | | | | | | | | 58.5 | 60.0 | 12407 |
| | | | | | | | | | | | | | | 60.0 | 61.5 | 12408 |
| | | | | | | | | | | | | | | 61.5 | 63.0 | 12409 |
| | | | | | | | | | | | | | | 63.0 | 64.5 | 12410 |
| | | | | | | | | | | | | | | 64.5 | 66.0 | 12411 |
| | | | | | | | | | | | | | | 66.0 | 67.5 | 12412 |
| | | | | | | | | | | | | | | 67.5 | 69.0 | 12413 |
| | | | | | | | | | | | | | | 69.0 | 70.5 | 12414 |
| | | | | | | | | | | | | | | 70.5 | 72.0 | 12415 |
| | | | | 72.0 | 84.0 | 97% | B-C | | | | | | | 72.0 | 73.5 | 12416 DR |

APPENDIX III
ROCK SAMPLE DESCRIPTIONS

NORANDA EXPLORATION COMPANY, LIMITED

PROPERTY MT. NANSEN - DOWS CLAIMS

N.T.S. 115I-3

DATE JUNE 3/89

ROCK SAMPLE REPORT

PROJECT: 337

| SAMPLE NO. | LOCATION & DESCRIPTION | % SULPHIDES | TYPE | WIDTH | G <input type="checkbox"/> A <input type="checkbox"/> | | | | | | | | SAMPLI BY | |
|------------|--|----------------|---------|-------------------------|---|--|--|--|--|--|--|--|--------------|------|
| | | | | | | | | | | | | | | |
| R48662 | 8325 E, 9175 N FLOAT. - MODERATE TO INTENSELY SILICIFIED RHYOLITE | | GRAB | | | | | | | | | | | R.I. |
| R48663 | 7660 E, 9475 N FLOAT - SUBCROP. INTENSELY SILICIFIED AGGLOMERATE - "VEIN" MATERIAL | | TR GRAB | | | | | | | | | | | |
| R48664 | SAME LOCATION & DESCRIPTION AS 48663. | | TR GRAB | | | | | | | | | | | |
| R48665 | 10,000 N B.L. 6550 E. FLOAT BOULDER. - DARK BLUE GREY SILICA VEIN. RED-MAROON STAINING ON FRACTURE SURFACES. | | TR GRAB | | | | | | | | | | | |
| R48666 | 6525 E, 10,025 N S/C - OUTCROP. LARGE BOULDERS 3-4 FEET ACROSS OF INTENSELY SILICIFIED ROCK "VEIN MATERIAL". (DARK BLUE GREY SILICA) TR ASPY. SAME ROCK AS # 48665. | | TR | CONT. CHIP 1.5 M. | | | | | | | | | | |
| R48667 | 8900 E, 10,325 N WEATHERED QZ. FORM. | | GRAB | | | | | | | | | | | |

G = GEOCHEM A = ASSAY

NORANDA EXPLORATION COMPANY, LIMITED

PROPERTY MT. NANSEN - DOWS CLAIMS

N.T.S. 115 I-3

DATE JUNE 4/88

ROCK SAMPLE REPORT

PROJECT 337

| SAMPLE NO. | LOCATION & DESCRIPTION | % SULPHIDES | TYPE | WIDTH | G <input type="checkbox"/> A <input type="checkbox"/> | | | | | | | | SAMPL BY | |
|------------|--|----------------|-----------------------|-------|---|--|--|--|--|--|--|--|-------------|------|
| | | | | | | | | | | | | | | |
| 48668 | 10840 E, 6730 N / DARK BLUE GREY SILICA VEIN 2-5% SULPHIDES, TR ASPY "SUBCROP" | 2-5% | GRAB | | | | | | | | | | | R.D. |
| 48669 | FLOAT 10840 E, 6650 N WHITE DRUSY QUARTZ VEIN | | GRAB | | | | | | | | | | | |
| 48670 | OUTCROP SILICIFIED QUARTZITE, MODERATE IRON STAINING, MINOR QZ VEINING, 10900 E, 6950 E | | RANDOM CHIP | 2M | | | | | | | | | | |
| 48671 | FLOAT - 8400 E, 10,800 N CHLORITE BIOTITE SCHIST WITH TR PYRRHOTITE, WEAKLY MAGNETIC | | TR GRAB | | | | | | | | | | | |
| 48672 | FLOAT - L87E, 10,975 N LIGHT GREEN STRONGLY SILICIFIED META-SEDIMENTS, VERY CALCAREOUS POSSIBLE SKARN | | GRAB | | | | | | | | | | | |
| 48673 | O/C L8050 E, 8050 N MODERATE SILICIFIED METASEDIMENT WITH TR MAGNETITE | | TR RAN DOM CHIP | .5M | | | | | | | | | | D.K. |

G = GEOCHEM A = ASSAY

NORANDA EXPLORATION COMPANY, LIMITED

PROPERTY MT. NANSEN

N.T.S. 115 I-3

DATE JUNE/10/89

ROCK SAMPLE REPORT

PROJECT 337

| SAMPLE NO. | LOCATION & DESCRIPTION | % SULPHIDES | TYPE | WIDTH | G <input type="checkbox"/> A <input type="checkbox"/> | | | | | | | | SAMPL BY | |
|------------|---|----------------|--------------------|-------|---|--|--|--|--|--|--|--|-------------|-----|
| | | | | | | | | | | | | | | |
| 48674 | L 7775E, 8050N Qtz vein, o/c. UP TO .8M wide, 10M length. No sulphides | | RANDOM CHIP | | | | | | | | | | | D.K |
| 48675 | L 7384E, 9525N Blue grey Qtz vein, Py + Aspy ≈ 3% Subcrop | | Selective chip. | | | | | | | | | | | |
| 52226 | SUBCROP 7930E, 9500N DARK BLUE GREY SILICA (QZ) VEIN WITH 3-5% DISS. PY & ASPY. | 3-5% | GRAB | | | | | | | | | | | |
| 52227 | SUBCROP 7930E, 9500N LIGHT GREY JUGGY DRUSY QZ VEINING. POSSIBLY WALL ROCK OF # 52226. TR PY. | | TR GRAB | | | | | | | | | | | |
| 52228 | FLOAT 10675E, 7500N LIGHT PINK TO WHITE QZ RICH INTRUSIVE WITH TR OF MAGNETITE. | | GRAB | | | | | | | | | | | |
| 52229 | OUTCROP - 10050E, 8100N MODERATELY IRON STAINED, ARGILLICALLY ALTERED QZ RICH INTRUSIVE (GRANITE). | | RANDOM CHIP. | | | | | | | | | | | |

APPENDIX IV

RESULTS

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

Don Cl. Mt. Nansen (K6)

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 2ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN PB SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: Core AU* ANALYSIS BY ACID LEACH/AA FROM 10 CM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: MAY 18 1989 DATE REPORT MAILED: *May 26/89* SIGNED BY: *C. Long* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION CO. LTD. PROJECT 8905-018 337 File # 89-1138 Page 1

| SAMPLE# | MC | CU | PB | CR | AG | NI | CO | MO | FE | AS | U | AM | TR | SR | CG | SB | BI | V | CR | P | LA | CR | MG | BA | TI | B | W | NA | K | AL | SI | PPM | AU* | HG |
|------------|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|-------|------|-----|----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | % | PPM | PPM | % | PPM | % | % | PPM | % | % | % | PPM | PPM | PPM | |
| 12371 DR | 0 | 165 | 13 | 254 | .1 | 13 | 29 | 5370 | 4.98 | 11 | 16 | ND | 1 | 70 | 1 | 2 | 4 | 89 | 2.54 | .104 | 15 | 10 | .24 | 25 | .01 | 2 | .35 | .01 | .10 | 1 | 2 | 70 | | |
| 12372 DR | 1 | 174 | 10 | 34 | .0 | 7 | 12 | 875 | 3.39 | 3 | 6 | ND | 1 | 31 | 1 | 2 | 2 | 92 | 3.96 | .074 | 11 | 12 | .42 | 31 | .02 | 3 | .77 | .01 | .24 | 1 | 2 | 50 | | |
| 12373 DR | 1 | 26 | 7 | 92 | .1 | 9 | 17 | 2976 | 5.20 | 2 | 5 | ND | 1 | 78 | 1 | 2 | 2 | 112 | 1.45 | .059 | 8 | 20 | .44 | 41 | .03 | 3 | .72 | .01 | .26 | 1 | 1 | 40 | | |
| 12374 DR | 1 | 27 | 5 | 63 | .1 | 5 | 15 | 1666 | 4.76 | 4 | 5 | ND | 1 | 114 | 1 | 2 | 2 | 138 | 5.91 | .069 | 9 | 22 | .64 | 40 | .03 | 3 | .69 | .01 | .24 | 1 | 1 | 20 | | |
| 12375 DR | 1 | 24 | 9 | 64 | .1 | 5 | 10 | 1505 | 4.99 | 5 | 5 | ND | 3 | 81 | 1 | 2 | 2 | 113 | 2.53 | .049 | 5 | 20 | .37 | 27 | .02 | 2 | .69 | .01 | .20 | 1 | 2 | 40 | | |
| 12376 DR | 1 | 22 | 9 | 62 | .1 | 3 | 9 | 312 | 5.03 | 2 | 5 | ND | 2 | 70 | 1 | 2 | 4 | 95 | 1.71 | .055 | 6 | 14 | .39 | 26 | .01 | 2 | .66 | .01 | .22 | 1 | 3 | 30 | | |
| 12377 DR | 4 | 72 | 20 | 56 | .1 | 4 | 10 | 2324 | 3.66 | 19 | 24 | ND | 3 | 49 | 1 | 2 | 2 | 51 | .87 | .046 | 6 | 7 | .28 | 34 | .01 | 4 | .55 | .01 | .18 | 1 | 2 | 400 | | |
| 12378 DR | 40 | 92 | 13 | 92 | .1 | 10 | 13 | 2525 | 5.09 | 56 | 46 | ND | 9 | 51 | 1 | 8 | 2 | 54 | .44 | .015 | 4 | 5 | .26 | 19 | .01 | 2 | .45 | .01 | .11 | 1 | 3 | 1100 | | |
| 12379 DR | 3 | 111 | 14 | 151 | .1 | 18 | 17 | 4067 | 7.39 | 71 | 27 | ND | 2 | 75 | 1 | 14 | 2 | 92 | .67 | .027 | 5 | 13 | .30 | 35 | .01 | 2 | .48 | .01 | .15 | 1 | 2 | 1100 | | |
| 12380 DR | 21 | 50 | 10 | 113 | .1 | 7 | 3 | 935 | 2.83 | 25 | 9 | ND | 1 | 80 | 1 | 5 | 2 | 33 | .28 | .029 | 6 | 4 | .12 | 160 | .01 | 2 | .49 | .01 | .10 | 1 | 2 | 1300 | | |
| 12381 DR | 31 | 254 | 22 | 214 | .1 | 10 | 15 | 679 | 7.78 | 394 | 56 | ND | 3 | 75 | 1 | 25 | 2 | 53 | .16 | .021 | 4 | 6 | .06 | 58 | .01 | 3 | .67 | .01 | .16 | 1 | 1 | 1600 | | |
| 12382 DR | 13 | 66 | 24 | 30 | .1 | 6 | 5 | 299 | 4.22 | 123 | 37 | ND | 2 | 46 | 1 | 8 | 2 | 27 | .12 | .029 | 4 | 6 | .03 | 91 | .01 | 3 | .67 | .01 | .16 | 1 | 1 | 1600 | | |
| 12383 DR | 7 | 183 | 10 | 110 | .1 | 21 | 20 | 2423 | 3.22 | 76 | 93 | ND | 3 | 52 | 1 | 7 | 2 | 75 | .37 | .111 | 7 | 10 | .07 | 26 | .01 | 6 | .56 | .01 | .03 | 1 | 1 | 980 | | |
| 12384 DR | 4 | 240 | 12 | 36 | .1 | 31 | 53 | 5306 | 2.69 | 31 | 106 | ND | 3 | 73 | 1 | 8 | 2 | 116 | 1.37 | .094 | 8 | 11 | .26 | 47 | .01 | 2 | .63 | .01 | .10 | 1 | 1 | 900 | | |
| 12385 DR | 1 | 516 | 7 | 102 | .7 | 12 | 22 | 1387 | 4.87 | 20 | 40 | ND | 3 | 107 | 1 | 7 | 2 | 150 | 2.23 | .085 | 7 | 31 | .42 | 31 | .02 | 2 | .65 | .01 | .20 | 1 | 1 | 200 | | |
| 12386 DR | 1 | 98 | 6 | 63 | .1 | 11 | 18 | 1092 | 5.23 | 20 | 52 | ND | 2 | 98 | 1 | 6 | 2 | 165 | 3.52 | .063 | 11 | 20 | .26 | 345 | .02 | 2 | .67 | .01 | .20 | 1 | 4 | 220 | | |
| 12387 DR | 1 | 120 | 5 | 67 | .1 | 3 | 14 | 1715 | 3.52 | 13 | 15 | ND | 3 | 112 | 1 | 2 | 2 | 81 | 4.89 | .070 | 9 | 17 | .42 | 310 | .02 | 2 | .70 | .01 | .25 | 1 | 2 | 40 | | |
| 12388 DR | 1 | 113 | 7 | 52 | .1 | 11 | 13 | 1613 | 4.51 | 14 | 5 | ND | 2 | 155 | 1 | 2 | 2 | 108 | 5.64 | .059 | 9 | 14 | .66 | 547 | .01 | 2 | .59 | .01 | .14 | 1 | 3 | 70 | | |
| 12389 DR | 1 | 167 | 7 | 48 | .1 | 12 | 20 | 2736 | 3.26 | 9 | 3 | ND | 1 | 119 | 1 | 2 | 2 | 92 | 5.24 | .092 | 11 | 10 | .54 | 357 | .01 | 6 | .60 | .01 | .12 | 1 | 2 | 170 | | |
| 12390 DR | 1 | 164 | 5 | 82 | .1 | 19 | 31 | 3925 | 4.16 | 32 | 5 | ND | 1 | 97 | 1 | 11 | 2 | 79 | 4.00 | .074 | 9 | 9 | .46 | 111 | .01 | 2 | .60 | .01 | .16 | 1 | 2 | 240 | | |
| 12391 DR | 2 | 168 | 7 | 206 | .1 | 33 | 47 | 7320 | 5.19 | 95 | 15 | ND | 1 | 38 | 1 | 7 | 2 | 62 | .92 | .043 | 5 | 7 | .09 | 80 | .01 | 4 | .60 | .01 | .10 | 1 | 2 | 650 | | |
| 12392 DR | 5 | 129 | 8 | 116 | .1 | 14 | 24 | 595 | 5.74 | 85 | 37 | ND | 2 | 105 | 1 | 12 | 2 | 56 | 1.74 | .079 | 8 | 4 | .05 | 21 | .01 | 5 | .64 | .01 | .16 | 1 | 1 | 500 | | |
| 12393 DR | 5 | 184 | 10 | 153 | .1 | 13 | 21 | 612 | 7.62 | 180 | 60 | ND | 2 | 59 | 1 | 26 | 2 | 56 | .89 | .074 | 2 | 6 | .05 | 16 | .01 | 4 | .67 | .01 | .17 | 1 | 3 | 920 | | |
| 12394 DR | 1 | 154 | 9 | 193 | .1 | 19 | 13 | 2930 | 3.47 | 120 | 5 | ND | 1 | 72 | 1 | 15 | 2 | 67 | .61 | .065 | 4 | 6 | .07 | 34 | .01 | 5 | 1.02 | .01 | .17 | 1 | 1 | 300 | | |
| 12395 DR | 2 | 178 | 9 | 15 | .1 | 16 | 14 | 46 | 2.39 | 40 | 9 | ND | 1 | 143 | 1 | 51 | 2 | 20 | .09 | .060 | 4 | 6 | .01 | 20 | .01 | 2 | .62 | .01 | .08 | 1 | 4 | 1050 | | |
| 12396 DR | 3 | 163 | 12 | 9 | .1 | 10 | 6 | 67 | 1.35 | 34 | 9 | ND | 1 | 96 | 1 | 39 | 2 | 17 | .07 | .022 | 3 | 11 | .01 | 53 | .01 | 5 | .48 | .01 | .08 | 1 | 2 | 1300 | | |
| 12397 DR | 4 | 252 | 11 | 24 | .2 | 52 | 14 | 30 | 1.65 | 90 | 22 | ND | 1 | 62 | 1 | 68 | 2 | 17 | .06 | .018 | 2 | 25 | .01 | 49 | .01 | 5 | .42 | .01 | .10 | 2 | 20 | 1600 | | |
| 12398 DR | 3 | 86 | 9 | 6 | .1 | 10 | 1 | 27 | .80 | 32 | 5 | ND | 1 | 40 | 1 | 39 | 2 | 10 | .85 | .010 | 2 | 18 | .01 | 108 | .01 | 2 | .26 | .01 | .07 | 1 | 27 | 310 | | |
| 12399 DR | 4 | 76 | 53 | 46 | 1.7 | 31 | 23 | 20 | 6.92 | 229 | 5 | ND | 1 | 94 | 1 | 229 | 2 | 13 | .15 | .041 | 2 | 9 | .04 | 16 | .01 | 4 | .61 | .01 | .13 | 1 | 1180 | 4300 | | |
| 12400 DR | 5 | 64 | 36 | 96 | 3.2 | 25 | 21 | 20 | 3.49 | 126 | 36 | ND | 1 | 53 | 7 | 169 | 2 | 13 | .21 | .052 | 2 | 7 | .06 | 22 | .01 | 7 | .64 | .01 | .16 | 1 | 550 | 1700 | | |
| 12401 DR | 5 | 81 | 50 | 153 | 25.1 | 52 | 23 | 17 | 2.69 | 4726 | 38 | 11 | 1 | 52 | 3 | 420 | 2 | 10 | .11 | .023 | 2 | 17 | .03 | 10 | .01 | 6 | .37 | .01 | .12 | 1 | 10150 | 2900 | | |
| 12402 DR | 6 | 36 | 28 | 136 | 2.5 | 21 | 14 | 52 | 2.72 | 168 | 9 | ND | 1 | 203 | 1 | 61 | 2 | 12 | .20 | .046 | 3 | 8 | .07 | 16 | .01 | 9 | .63 | .01 | .16 | 1 | 155 | 1800 | | |
| 12403 DR | 1 | 11 | 12 | 139 | .4 | 19 | 16 | 1210 | 4.85 | 55 | 5 | ND | 3 | 41 | 1 | 13 | 2 | 9 | .62 | .042 | 8 | 2 | .34 | 36 | .01 | 9 | .47 | .01 | .15 | 1 | 138 | 210 | | |
| 12404 DR | 1 | 27 | 7 | 69 | .1 | 12 | 12 | 879 | 2.96 | 11 | 5 | ND | 3 | 109 | 1 | 2 | 2 | 32 | 2.53 | .038 | 12 | 5 | 1.43 | 84 | .02 | 7 | .61 | .01 | .11 | 1 | 2 | 230 | | |
| 12405 DR | 1 | 17 | 11 | 62 | .1 | 7 | 9 | 730 | 2.97 | 10 | 5 | ND | 2 | 108 | 1 | 2 | 2 | 32 | 2.65 | .052 | 12 | 5 | 1.47 | 198 | .03 | 12 | .97 | .01 | .50 | 1 | 11 | 200 | | |
| 12406 DR | 1 | 5 | 10 | 61 | .1 | 11 | 9 | 592 | 2.06 | 2 | 5 | ND | 2 | 100 | 1 | 2 | 2 | 27 | 2.63 | .041 | 11 | 15 | 1.59 | 168 | .04 | 5 | 1.08 | .01 | .59 | 1 | 2 | 20 | | |
| STD C/AU-B | 17 | 60 | 40 | 102 | 7.1 | 70 | 21 | 940 | 3.67 | 35 | 16 | 7 | 36 | 49 | 17 | 15 | 20 | 57 | .45 | .066 | 37 | 53 | .82 | 172 | .07 | 34 | 1.74 | .89 | .55 | 969 | 6466 | | | |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Hg | Co | Mn | Fe | As | U | Au | Th | Sr | Cr | SS | Bt | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au* | Hg |
|------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|------|-----|-----|------|-----|------|-----|-----|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPB | PPB |
| 12407 DR | 1 | 6 | 6 | 54 | .2 | 9 | 10 | 527 | 2.17 | 7 | 5 | ND | 5 | 90 | 1 | 2 | 3 | 27 | 2.41 | .045 | 11 | 6 | 1.29 | 143 | .03 | 9 | 1.06 | .01 | .53 | 1 | 11 | 170 |
| 12408 DR | 1 | 40 | 10 | 77 | .2 | 11 | 14 | 845 | 3.34 | 5 | 5 | ND | 4 | 94 | 1 | 2 | 2 | 66 | 1.99 | .075 | 9 | 12 | 2.01 | 597 | .12 | 5 | 2.09 | .03 | 1.28 | 1 | 3 | 30 |
| 12409 DR | 1 | 134 | 9 | 87 | .1 | 12 | 10 | 650 | 3.41 | 17 | 5 | ND | 2 | 155 | 1 | 3 | 3 | 41 | 2.51 | .072 | 5 | 11 | 1.27 | 101 | .03 | 2 | .95 | .01 | .49 | 1 | 4 | 380 |
| 12410 DR | 1 | 59 | 4 | 112 | .3 | 9 | 14 | 1183 | 1.49 | 15 | 5 | ND | 3 | 117 | 1 | 2 | 4 | 39 | 1.51 | .085 | 10 | 4 | 1.16 | 47 | .01 | 10 | .30 | .02 | .32 | 1 | 5 | 160 |
| 12411 DR | 1 | 26 | 5 | 53 | .1 | 7 | 7 | 465 | 2.41 | 9 | 5 | ND | 3 | 53 | 1 | 2 | 2 | 33 | .72 | .051 | 6 | 5 | .62 | 124 | .05 | 13 | .68 | .02 | .37 | 1 | 9 | 130 |
| 12412 DR | 1 | 39 | 10 | 87 | .1 | 17 | 13 | 1005 | 4.07 | 18 | 5 | ND | 3 | 170 | 1 | 2 | 3 | 49 | 2.16 | .053 | 6 | 11 | 1.62 | 57 | .02 | 11 | .60 | .01 | .40 | 1 | 2 | 170 |
| 12413 DR | 1 | 14 | 2 | 50 | .1 | 17 | 14 | 669 | 4.19 | 18 | 5 | ND | 4 | 50 | 1 | 2 | 5 | 34 | .71 | .077 | 11 | 14 | .86 | 40 | .04 | 10 | .76 | .02 | .39 | 1 | 1 | 230 |
| 12414 DR | 1 | 14 | 9 | 70 | .2 | 5 | 5 | 409 | 1.37 | 8 | 6 | ND | 2 | 91 | 1 | 2 | 2 | 13 | .99 | .050 | 5 | 6 | .31 | 136 | .01 | 16 | .40 | .02 | .19 | 1 | 1 | 150 |
| 12415 DR | 1 | 44 | 10 | 82 | .1 | 30 | 22 | 1019 | 4.34 | 5 | 5 | ND | 3 | 143 | 1 | 2 | 2 | 91 | 2.66 | .038 | 6 | 43 | 2.32 | 363 | .15 | 4 | 2.20 | .02 | 1.41 | 1 | 2 | 60 |
| 12415 DR | 1 | 222 | 7 | 58 | .7 | 25 | 19 | 1217 | 4.41 | 7 | 5 | ND | 4 | 234 | 1 | 2 | 5 | 120 | 4.72 | .051 | 5 | 33 | 2.42 | 305 | .09 | 7 | 1.45 | .02 | 1.01 | 1 | 3 | 20 |
| 12417 DR | 1 | 56 | 7 | 77 | .1 | 7 | 12 | 791 | 2.95 | 7 | 5 | ND | 2 | 97 | 1 | 2 | 3 | 45 | 2.15 | .069 | 3 | 7 | 1.26 | 220 | .10 | 2 | .99 | .02 | .67 | 1 | 3 | 80 |
| 12418 DR | 1 | 46 | 2 | 40 | .2 | 5 | 5 | 395 | 1.25 | 5 | 5 | ND | 2 | 52 | 1 | 2 | 2 | 20 | .68 | .030 | 4 | 5 | .36 | 193 | .04 | 13 | .42 | .05 | .25 | 2 | 2 | 20 |
| 12419 DR | 1 | 11 | 2 | 56 | .1 | 7 | 5 | 565 | 1.06 | 9 | 5 | ND | 4 | 65 | 1 | 2 | 3 | 37 | 1.19 | .078 | 9 | 8 | .53 | 56 | .09 | 10 | .52 | .03 | .35 | 1 | 1 | 10 |
| 12420 DR | 1 | 7 | 2 | 57 | .1 | 8 | 13 | 333 | 3.03 | 8 | 5 | ND | 3 | 46 | 1 | 2 | 2 | 67 | .75 | .062 | 3 | 17 | 1.42 | 238 | .15 | 2 | 1.36 | .05 | 1.11 | 1 | 2 | 10 |
| 12421 DR | 1 | 20 | 7 | 76 | .1 | 30 | 16 | 812 | 3.25 | 2 | 5 | ND | 2 | 75 | 1 | 2 | 2 | 71 | 1.10 | .047 | 7 | 50 | 1.85 | 369 | .17 | 5 | 1.62 | .03 | 1.41 | 1 | 3 | 50 |
| 12422 DR | 1 | 30 | 9 | 45 | .1 | 12 | 10 | 559 | 2.86 | 9 | 5 | ND | 3 | 125 | 1 | 2 | 2 | 40 | 2.14 | .067 | 6 | 10 | .86 | 39 | .01 | 2 | .59 | .01 | .29 | 1 | 4 | 30 |
| 12423 DR | 1 | 8 | 7 | 22 | .1 | 7 | 5 | 230 | 2.65 | 12 | 5 | ND | 3 | 26 | 1 | 2 | 2 | 15 | .27 | .067 | 4 | 5 | .11 | 55 | .01 | 4 | .26 | .01 | .17 | 2 | 2 | 130 |
| 12424 DR | 1 | 24 | 5 | 23 | .1 | 4 | 2 | 242 | 1.71 | 3 | 5 | ND | 1 | 46 | 1 | 2 | 4 | 4 | .58 | .006 | 2 | 3 | .08 | 26 | .01 | 4 | .40 | .01 | .11 | 1 | 1 | 40 |
| 12425 DR | 1 | 30 | 2 | 18 | .1 | 5 | 1 | 160 | .57 | 3 | 5 | ND | 1 | 72 | 1 | 2 | 2 | 2 | .32 | .005 | 2 | 4 | .11 | 41 | .01 | 4 | .20 | .04 | .07 | 2 | 1 | 50 |
| 12425 DR | 1 | 40 | 14 | 90 | .2 | 13 | 16 | 1021 | 3.83 | 9 | 5 | ND | 2 | 146 | 1 | 2 | 2 | 69 | 1.22 | .056 | 3 | 9 | 1.16 | 124 | .06 | 5 | 1.15 | .01 | .63 | 1 | 2 | 170 |
| 12427 DR | 1 | 27 | 6 | 83 | .1 | 6 | 10 | 560 | 2.42 | 2 | 5 | ND | 3 | 100 | 1 | 2 | 2 | 53 | 1.84 | .069 | 7 | 7 | 1.01 | 170 | .07 | 13 | .99 | .02 | .61 | 1 | 2 | 20 |
| 12428 DR | 1 | 129 | 5 | 86 | .5 | 5 | 11 | 524 | 2.05 | 2 | 5 | ND | 1 | 123 | 1 | 2 | 3 | 57 | 1.12 | .055 | 6 | 4 | .91 | 1709 | .10 | 7 | 1.00 | .03 | .69 | 1 | 7 | 10 |
| 12429 DR | 1 | 46 | 11 | 97 | .2 | 6 | 10 | 571 | 2.01 | 2 | 5 | ND | 1 | 102 | 1 | 2 | 2 | 46 | 1.41 | .057 | 4 | 6 | .88 | 134 | .09 | 10 | 1.02 | .03 | .67 | 1 | 3 | 10 |
| 12430 DR | 1 | 18 | 7 | 107 | .1 | 8 | 16 | 873 | 3.11 | 3 | 5 | ND | 1 | 103 | 1 | 2 | 2 | 71 | 1.41 | .056 | 5 | 9 | 1.64 | 336 | .15 | 2 | 1.77 | .03 | 1.29 | 1 | 2 | 5 |
| 12431 DR | 1 | 54 | 5 | 104 | .2 | 6 | 11 | 610 | 2.25 | 4 | 5 | ND | 2 | 88 | 1 | 2 | 4 | 58 | 1.22 | .069 | 5 | 6 | 1.11 | 155 | .11 | 3 | 1.17 | .02 | .85 | 1 | 4 | 5 |
| 12432 DR | 1 | 25 | 5 | 88 | .1 | 7 | 12 | 684 | 2.47 | 5 | 5 | ND | 2 | 100 | 1 | 2 | 2 | 62 | 1.31 | .046 | 5 | 7 | 1.19 | 342 | .12 | 2 | 1.41 | .03 | .96 | 1 | 5 | 5 |
| 12433 DR | 1 | 15 | 6 | 94 | .3 | 6 | 13 | 853 | 2.59 | 2 | 5 | ND | 2 | 118 | 1 | 2 | 2 | 57 | 2.29 | .055 | 5 | 9 | 1.16 | 456 | .11 | 6 | 1.21 | .03 | .86 | 1 | 1 | 10 |
| 12434 DR | 1 | 74 | 5 | 94 | .4 | 11 | 15 | 754 | 3.13 | 3 | 5 | ND | 1 | 102 | 1 | 2 | 2 | 64 | 1.54 | .042 | 4 | 9 | 1.38 | 360 | .15 | 3 | 1.69 | .03 | 1.20 | 1 | 6 | 5 |
| 12435 DR | 1 | 10 | 11 | 67 | .3 | 4 | 12 | 810 | 1.67 | 4 | 5 | ND | 2 | 194 | 1 | 2 | 2 | 39 | 2.83 | .053 | 7 | 3 | .92 | 801 | .04 | 6 | .85 | .02 | .50 | 1 | 2 | 50 |
| 12436 DR | 1 | 58 | 7 | 112 | .2 | 6 | 17 | 1108 | 4.25 | 4 | 5 | ND | 2 | 161 | 1 | 2 | 4 | 103 | 2.56 | .048 | 5 | 7 | 1.40 | 736 | .09 | 4 | 1.09 | .02 | .78 | 1 | 4 | 60 |
| 12437 DR | 1 | 18 | 9 | 120 | .1 | 8 | 16 | 1172 | 1.19 | 7 | 5 | ND | 1 | 147 | 1 | 2 | 2 | 113 | 2.23 | .055 | 6 | 15 | 1.69 | 551 | .12 | 2 | 1.59 | .03 | 1.18 | 1 | 1 | 10 |
| 12438 DR | 1 | 27 | 8 | 86 | .1 | 5 | 5 | 403 | 1.67 | 2 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 38 | .60 | .047 | 9 | 10 | .50 | 176 | .05 | 11 | .72 | .03 | .50 | 1 | 1 | 20 |
| 12439 DR | 1 | 10 | 5 | 77 | .1 | 3 | 5 | 587 | 1.56 | 5 | 5 | ND | 2 | 75 | 1 | 2 | 3 | 26 | 1.12 | .048 | 7 | 18 | .35 | 151 | .03 | 7 | .52 | .03 | .31 | 1 | 6 | 100 |
| 12440 DR | 1 | 8 | 9 | 96 | .1 | 7 | 5 | 445 | 1.61 | 5 | 5 | ND | 2 | 67 | 1 | 2 | 2 | 27 | .48 | .049 | 6 | 21 | .45 | 40 | .04 | 6 | .59 | .04 | .35 | 1 | 3 | 80 |
| 12441 DR | 1 | 25 | 25 | 79 | .1 | 5 | 7 | 587 | 1.70 | 24 | 5 | ND | 11 | 224 | 1 | 2 | 2 | 8 | 1.14 | .031 | 5 | 8 | .38 | 36 | .01 | 9 | .50 | .01 | .20 | 2 | 14 | 330 |
| 12442 DR | 1 | 21 | 17 | 42 | .1 | 1 | 2 | 259 | .74 | 8 | 5 | ND | 2 | 109 | 1 | 2 | 2 | 9 | .86 | .017 | 4 | 3 | .29 | 13 | .01 | 2 | .41 | .01 | .07 | 2 | 1 | 60 |
| STD C/AU-2 | 18 | 61 | 39 | 131 | 7.0 | 72 | 29 | 984 | 3.78 | 36 | 22 | 6 | 36 | 47 | 17 | 18 | 18 | 55 | .43 | .083 | 35 | 56 | .79 | 173 | .06 | 32 | 1.79 | .06 | .14 | 11 | 510 | 1400 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au* | Hg |
|------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|----|------|------|-----|----|------|-----|-----|----|------|-----|-----|-----|-----|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPB | PPB | |
| 12443 DR | 1 | 22 | 28 | 69 | .1 | 4 | 4 | 537 | 1.62 | 17 | 5 | ND | 9 | 250 | 1 | 2 | 2 | 16 | 1.75 | .631 | 6 | 4 | .57 | 12 | .01 | 6 | .36 | .01 | .14 | 1 | 5 | 120 |
| 12444 DR | 1 | 5 | 10 | 79 | .1 | 3 | 3 | 322 | 1.23 | 1 | 5 | ND | 1 | 95 | 1 | 2 | 2 | 12 | 1.35 | .039 | 5 | 1 | .29 | 24 | .01 | 2 | .27 | .02 | .03 | 1 | 1 | 310 |
| 12445 DR | 1 | 7 | 7 | 93 | .2 | 4 | 9 | 680 | 1.00 | 7 | 5 | ND | 1 | 189 | 1 | 2 | 1 | 72 | 2.33 | .033 | 5 | 5 | .96 | 364 | .06 | 2 | .85 | .02 | .51 | 1 | 2 | 140 |
| 12446 DR | 1 | 5 | 11 | 76 | .1 | 2 | 4 | 373 | 1.40 | 5 | 5 | ND | 2 | 141 | 1 | 2 | 2 | 27 | 2.05 | .055 | 11 | 2 | .41 | 156 | .03 | 5 | .52 | .02 | .25 | 1 | 1 | 230 |
| 12447 DR | 1 | 14 | 11 | 79 | .1 | 5 | 9 | 667 | 2.49 | 10 | 5 | ND | 1 | 211 | 1 | 2 | 2 | 51 | 2.39 | .049 | 6 | 4 | .73 | 329 | .02 | 3 | .66 | .02 | .32 | 1 | 2 | 150 |
| 12448 DR | 1 | 9 | 11 | 73 | .2 | 4 | 7 | 533 | 1.95 | 10 | 5 | ND | 3 | 170 | 1 | 2 | 2 | 24 | 2.00 | .034 | 5 | 1 | .62 | 125 | .01 | 3 | .40 | .01 | .23 | 1 | 3 | 130 |
| 12449 DR | 7 | 107 | 21 | 103 | .3 | 8 | 10 | 791 | 3.97 | 21 | 5 | ND | 1 | 109 | 1 | 2 | 2 | 33 | .99 | .042 | 6 | 7 | .46 | 19 | .01 | 4 | .42 | .01 | .14 | 1 | 2 | 390 |
| 12450 DR | 3 | 16 | 39 | 72 | .1 | 9 | 7 | 466 | 1.95 | 16 | 5 | ND | 1 | 66 | 1 | 2 | 2 | 18 | .56 | .035 | 6 | 3 | .23 | 27 | .01 | 2 | .35 | .02 | .11 | 1 | 2 | 630 |
| 12451 DR | 1 | 101 | 15 | 111 | .2 | 15 | 14 | 1017 | 4.27 | 20 | 5 | ND | 1 | 191 | 1 | 2 | 2 | 58 | 1.89 | .055 | 5 | 7 | .86 | 57 | .01 | 9 | .50 | .02 | .12 | 1 | 5 | 510 |
| 12452 DR | 2 | 62 | 12 | 70 | .1 | 3 | 9 | 725 | 2.81 | 13 | 5 | ND | 1 | 115 | 1 | 2 | 2 | 37 | 1.31 | .040 | 5 | 5 | .51 | 44 | .01 | 3 | .41 | .02 | .13 | 1 | 4 | 320 |
| 12453 DR | 1 | 45 | 9 | 70 | .1 | 5 | 8 | 751 | 1.71 | 16 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 23 | .73 | .041 | 8 | 7 | .39 | 14 | .01 | 2 | .46 | .02 | .18 | 1 | 1 | 580 |
| 12454 DR | 3 | 95 | 19 | 101 | .2 | 13 | 15 | 796 | 3.66 | 14 | 5 | ND | 1 | 201 | 1 | 2 | 2 | 56 | 1.97 | .050 | 8 | 25 | .65 | 48 | .01 | 17 | .55 | .02 | .21 | 1 | 2 | 230 |
| 12455 DR | 1 | 44 | 14 | 77 | .1 | 9 | 12 | 713 | 2.65 | 11 | 5 | ND | 2 | 187 | 1 | 2 | 2 | 51 | 2.20 | .054 | 7 | 14 | 1.06 | 251 | .06 | 6 | 1.30 | .01 | .79 | 1 | 3 | 420 |
| 12456 DR | 1 | 51 | 9 | 96 | .2 | 14 | 17 | 945 | 3.90 | 6 | 5 | ND | 2 | 166 | 1 | 2 | 2 | 69 | 2.15 | .028 | 8 | 19 | 1.45 | 391 | .11 | 4 | 1.48 | .02 | .99 | 1 | 4 | 130 |
| 12457 DR | 1 | 59 | 6 | 89 | .1 | 10 | 18 | 1223 | 4.44 | 5 | 5 | ND | 1 | 212 | 1 | 2 | 2 | 68 | 3.44 | .033 | 6 | 13 | 1.37 | 474 | .05 | 10 | .86 | .01 | .55 | 1 | 4 | 140 |
| 12458 DR | 1 | 19 | 8 | 106 | .1 | 14 | 19 | 1258 | 4.23 | 26 | 5 | ND | 2 | 249 | 1 | 4 | 2 | 77 | 3.89 | .038 | 7 | 14 | 1.37 | 214 | .04 | 4 | .84 | .01 | .53 | 1 | 5 | 300 |
| 12459 DR | 1 | 77 | 12 | 74 | .1 | 9 | 10 | 726 | 2.66 | 56 | 5 | ND | 1 | 184 | 1 | 2 | 2 | 31 | 2.58 | .033 | 10 | 10 | .75 | 148 | .02 | 8 | .61 | .01 | .32 | 1 | 3 | 130 |
| 12460 DR | 1 | 19 | 7 | 31 | .1 | 15 | 15 | 734 | 3.61 | 5 | 5 | ND | 2 | 108 | 1 | 2 | 2 | 73 | 1.21 | .027 | 10 | 21 | 1.17 | 614 | .12 | 2 | 1.18 | .02 | .94 | 1 | 4 | 40 |
| 12461 DR | 1 | 33 | 19 | 79 | .2 | 10 | 10 | 907 | 3.46 | 14 | 5 | ND | 6 | 321 | 1 | 2 | 2 | 18 | 4.12 | .024 | 6 | 5 | .89 | 137 | .01 | 5 | .34 | .01 | .16 | 1 | 4 | 90 |
| 12462 DR | 1 | 72 | 14 | 73 | .1 | 27 | 14 | 567 | 3.25 | 43 | 5 | ND | 1 | 238 | 1 | 6 | 2 | 36 | 3.75 | .060 | 6 | 27 | .98 | 224 | .01 | 6 | .41 | .01 | .23 | 1 | 4 | 170 |
| 12463 DR | 1 | 17 | 19 | 124 | .1 | 16 | 14 | 1198 | 3.17 | 204 | 5 | ND | 3 | 209 | 1 | 5 | 2 | 22 | 2.43 | .031 | 5 | 8 | .81 | 61 | .01 | 6 | .41 | .01 | .18 | 1 | 7 | 210 |
| 12464 DR | 2 | 29 | 36 | 77 | .1 | 3 | 3 | 641 | 1.31 | 87 | 5 | ND | 7 | 216 | 1 | 9 | 2 | 11 | 1.71 | .023 | 4 | 4 | .48 | 26 | .01 | 5 | .37 | .01 | .15 | 1 | 10 | 200 |
| 12465 DR | 3 | 13 | 41 | 85 | .1 | 9 | 6 | 572 | 1.58 | 23 | 5 | ND | 8 | 235 | 1 | 2 | 2 | 12 | 1.89 | .019 | 5 | 5 | .60 | 99 | .01 | 4 | .34 | .01 | .16 | 1 | 9 | 210 |
| 12466 DR | 2 | 33 | 25 | 83 | .1 | 11 | 7 | 763 | 2.06 | 34 | 5 | ND | 5 | 197 | 1 | 2 | 2 | 15 | 2.48 | .021 | 6 | 4 | .72 | 90 | .01 | 9 | .32 | .01 | .15 | 1 | 8 | 230 |
| 12467 DR | 1 | 35 | 15 | 80 | .1 | 12 | 12 | 960 | 3.10 | 35 | 5 | ND | 3 | 290 | 1 | 2 | 2 | 40 | 3.89 | .041 | 7 | 18 | 1.15 | 147 | .01 | 10 | .34 | .01 | .18 | 1 | 4 | 440 |
| 12468 DR | 2 | 40 | 26 | 95 | .1 | 10 | 10 | 820 | 2.43 | 44 | 5 | ND | 4 | 248 | 1 | 6 | 2 | 13 | 2.71 | .031 | 5 | 3 | .63 | 88 | .01 | 5 | .31 | .01 | .17 | 1 | 13 | 600 |
| 12469 DR | 1 | 35 | 88 | 129 | .6 | 14 | 13 | 868 | 3.96 | 104 | 5 | ND | 5 | 418 | 2 | 19 | 2 | 13 | 3.25 | .029 | 3 | 6 | .63 | 26 | .01 | 7 | .33 | .01 | .18 | 1 | 61 | 510 |
| 12470 DR | 1 | 25 | 29 | 95 | .1 | 8 | 6 | 812 | 1.84 | 24 | 5 | ND | 4 | 300 | 1 | 2 | 2 | 11 | 3.20 | .021 | 3 | 2 | .65 | 59 | .01 | 2 | .33 | .01 | .16 | 1 | 12 | 350 |
| 12471 DR | 1 | 34 | 13 | 69 | .1 | 5 | 9 | 896 | 1.52 | 26 | 5 | ND | 2 | 208 | 1 | 2 | 2 | 16 | 3.52 | .019 | 10 | 6 | .99 | 150 | .01 | 5 | .31 | .01 | .21 | 1 | 3 | 270 |
| 12472 DR | 1 | 31 | 12 | 78 | .1 | 7 | 10 | 922 | 3.23 | 30 | 5 | ND | 1 | 211 | 1 | 2 | 2 | 18 | 2.67 | .020 | 9 | 2 | .83 | 161 | .01 | 4 | .35 | .01 | .21 | 1 | 2 | 720 |
| 12473 DR | 1 | 20 | 30 | 106 | .1 | 3 | 6 | 912 | 2.02 | 52 | 5 | ND | 7 | 231 | 1 | 5 | 2 | 6 | 1.62 | .017 | 5 | 4 | .49 | 24 | .01 | 4 | .37 | .01 | .18 | 1 | 12 | 430 |
| 12474 DR | 1 | 16 | 39 | 97 | .2 | 6 | 5 | 1323 | 1.95 | 40 | 5 | ND | 9 | 232 | 1 | 2 | 2 | 4 | 1.64 | .010 | 3 | 2 | .47 | 44 | .01 | 4 | .34 | .01 | .15 | 1 | 16 | 480 |
| 12475 DR | 4 | 14 | 31 | 125 | .1 | 8 | 5 | 710 | 1.26 | 145 | 5 | ND | 10 | 211 | 1 | 4 | 2 | 4 | .98 | .013 | 4 | 5 | .27 | 63 | .01 | 4 | .40 | .01 | .19 | 1 | 11 | 1400 |
| 12476 DR | 3 | 7 | 25 | 205 | .1 | 9 | 6 | 1018 | 1.36 | 92 | 5 | ND | 7 | 210 | 1 | 4 | 2 | 7 | 2.11 | .014 | 5 | 3 | .53 | 107 | .01 | 7 | .40 | .01 | .20 | 1 | 10 | 1200 |
| 12477 DR | 2 | 22 | 29 | 101 | .1 | 9 | 6 | 994 | 1.66 | 24 | 5 | ND | 8 | 255 | 1 | 2 | 2 | 11 | 2.33 | .017 | 5 | 5 | .69 | 78 | .01 | 3 | .38 | .01 | .17 | 1 | 8 | 430 |
| 12478 DR | 1 | 44 | 37 | 97 | .1 | 10 | 8 | 1105 | 2.10 | 39 | 5 | ND | 6 | 286 | 1 | 2 | 2 | 21 | 2.95 | .023 | 5 | 5 | .91 | 116 | .01 | 4 | .43 | .01 | .20 | 1 | 6 | 980 |
| STD C/AU-R | 17 | 59 | 39 | 132 | 7.1 | 73 | 20 | 935 | 3.66 | 39 | 17 | 5 | 36 | 19 | 17 | 15 | 19 | 57 | .50 | .084 | 37 | 55 | .83 | 176 | .07 | 33 | 1.79 | .06 | .14 | 11 | 525 | 1300 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | U | Cd | Sb | Bi | V | Ca | P | La | Ce | Mg | Ba | Ti | S | Al | Na | K | W | Au* | Hg |
|------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPM | PPM | |
| 12475 DR | 1 | 25 | 31 | 66 | .2 | 7 | 7 | 1155 | 2.20 | 565 | 5 | ND | 8 | 229 | 1 | 13 | 2 | 13 | 2.64 | .029 | 5 | 7 | .61 | 54 | .01 | 7 | .49 | .01 | .20 | 1 | 1 | 300 |
| 12460 DR | 11 | 66 | 180 | 717 | .5 | 12 | 6 | 1213 | 2.27 | 119 | 5 | ND | 4 | 132 | 18 | 4 | 2 | 15 | 3.49 | .038 | 8 | 4 | 1.07 | 137 | .01 | 5 | .34 | .01 | .17 | 1 | 8 | 180 |
| 12481 DR | 11 | 48 | 92 | 292 | .2 | 13 | 7 | 1276 | 2.32 | 53 | 5 | ND | 3 | 222 | 5 | 2 | 2 | 22 | 3.32 | .044 | 8 | 9 | 1.15 | 177 | .01 | 4 | .36 | .01 | .16 | 1 | 1 | 160 |
| 12482 DR | 3 | 25 | 32 | 113 | .1 | 13 | 7 | 1331 | 2.09 | 36 | 5 | ND | 6 | 273 | 1 | 2 | 2 | 19 | 3.13 | .030 | 8 | 7 | 1.16 | 25 | .01 | 5 | .29 | .01 | .19 | 1 | 3 | 152 |
| 12463 DR | 1 | 22 | 28 | 76 | .2 | 10 | 7 | 1366 | 2.12 | 35 | 5 | ND | 9 | 206 | 1 | 4 | 2 | 17 | 2.05 | .025 | 7 | 7 | .81 | 119 | .01 | 7 | .37 | .01 | .16 | 1 | 16 | 270 |
| 12484 DR | 1 | 9 | 24 | 51 | .1 | 5 | 3 | 1110 | 1.09 | 73 | 5 | ND | 14 | 130 | 1 | 2 | 3 | 10 | .95 | .012 | 7 | 3 | .35 | 23 | .01 | 5 | .31 | .02 | .14 | 1 | 2 | 452 |
| 12465 DR | 1 | 1 | 40 | 35 | .1 | 1 | 1 | 147 | .16 | 62 | 5 | ND | 19 | 143 | 1 | 2 | 2 | 1 | .27 | .001 | 8 | 4 | .10 | 99 | .01 | 6 | .35 | .01 | .14 | 2 | 1 | 322 |
| 12466 DR | 1 | 5 | 43 | 73 | .1 | 3 | 1 | 605 | .44 | 66 | 8 | ND | 17 | 121 | 1 | 2 | 2 | 2 | .55 | .003 | 8 | 2 | .19 | 88 | .01 | 7 | .34 | .01 | .14 | 1 | 1 | 372 |
| 12487 DR | 1 | 1 | 44 | 34 | .1 | 1 | 1 | 564 | .45 | 22 | 5 | ND | 17 | 146 | 1 | 2 | 2 | 1 | 1.40 | .001 | 7 | 7 | .22 | 360 | .01 | 5 | .34 | .01 | .14 | 1 | 1 | 160 |
| 12459 DR | 4 | 38 | 32 | 238 | .5 | 15 | 7 | 724 | 2.61 | 32 | 5 | ND | 5 | 195 | 2 | 3 | 4 | 23 | 2.62 | .061 | 9 | 5 | 1.09 | 106 | .01 | 9 | .44 | .01 | .20 | 1 | 1 | 150 |
| 12489 DR | 1 | 43 | 20 | 97 | .4 | 15 | 9 | 699 | 2.46 | 11 | 5 | ND | 5 | 202 | 1 | 2 | 3 | 36 | 2.58 | .035 | 7 | 17 | 1.15 | 186 | .01 | 7 | .51 | .01 | .26 | 1 | 7 | 70 |
| 12490 DR | 4 | 55 | 35 | 132 | .3 | 13 | 10 | 812 | 2.93 | 11 | 5 | ND | 4 | 196 | 1 | 2 | 2 | 37 | 2.71 | .039 | 10 | 8 | 1.21 | 211 | .01 | 5 | .60 | .01 | .29 | 1 | 2 | 90 |
| 12491 DR | 5 | 76 | 29 | 102 | .1 | 17 | 11 | 685 | 2.58 | 10 | 5 | ND | 2 | 200 | 1 | 2 | 2 | 35 | 2.75 | .035 | 8 | 15 | 1.22 | 182 | .01 | 7 | .54 | .01 | .27 | 1 | 1 | 80 |
| 12492 DR | 1 | 46 | 27 | 123 | .2 | 27 | 12 | 636 | 3.13 | 19 | 5 | ND | 3 | 202 | 2 | 2 | 2 | 38 | 3.23 | .049 | 6 | 15 | 1.59 | 70 | .01 | 10 | .46 | .01 | .22 | 1 | 3 | 110 |
| 12453 DR | 1 | 82 | 16 | 107 | .2 | 16 | 19 | 1258 | 4.57 | 36 | 5 | ND | 3 | 276 | 1 | 2 | 2 | 60 | 4.31 | .054 | 7 | 8 | 1.54 | 59 | .01 | 6 | .53 | .01 | .22 | 1 | 3 | 420 |
| 12494 DR | 1 | 59 | 3 | 95 | .1 | 10 | 13 | 1117 | 4.76 | 11 | 5 | ND | 1 | 174 | 1 | 2 | 2 | 109 | 1.95 | .073 | 3 | 11 | 1.65 | 275 | .10 | 4 | 1.19 | .03 | .69 | 1 | 1 | 160 |
| 12495 DR | 1 | 20 | 17 | 79 | .3 | 9 | 12 | 940 | 2.96 | 3 | 5 | ND | 3 | 114 | 1 | 2 | 2 | 62 | 2.04 | .025 | 5 | 17 | 1.31 | 393 | .06 | 4 | .79 | .03 | .52 | 1 | 1 | 20 |
| 12496 DR | 1 | 19 | 5 | 94 | .1 | 5 | 16 | 335 | 4.04 | 2 | 5 | ND | 1 | 102 | 1 | 2 | 2 | 35 | 1.50 | .041 | 4 | 8 | 1.51 | 397 | .12 | 2 | 1.41 | .04 | .77 | 1 | 1 | 20 |
| 12497 DR | 1 | 24 | 6 | 75 | .2 | 7 | 11 | 1972 | 2.74 | 1403 | 5 | ND | 1 | 106 | 1 | 15 | 2 | 46 | 2.55 | .037 | 4 | 13 | 1.41 | 211 | .54 | 6 | .84 | .02 | .48 | 1 | 50 | 210 |
| 12498 DR | 1 | 54 | 7 | 70 | .1 | 3 | 10 | 1262 | 2.61 | 2072 | 5 | ND | 1 | 135 | 1 | 23 | 2 | 35 | 3.45 | .042 | 9 | 5 | 1.28 | 24 | .01 | 10 | .39 | .01 | .17 | 1 | 3 | 310 |
| 12499 DR | 1 | 121 | 14 | 74 | .1 | 7 | 15 | 1367 | 4.07 | 216 | 5 | ND | 1 | 169 | 1 | 16 | 2 | 34 | 4.55 | .035 | 4 | 3 | 1.63 | 102 | .01 | 4 | .42 | .01 | .27 | 1 | 5 | 160 |
| 46918 | 2 | 12 | 6 | 32 | .1 | 4 | 4 | 440 | .55 | 30 | 5 | ND | 10 | 10 | 1 | 2 | 2 | 8 | .09 | .008 | 4 | 3 | .07 | 84 | .01 | 2 | .32 | .02 | .14 | 1 | 4 | 40 |
| 46919 | 3 | 32 | 24 | 21 | .1 | 7 | 2 | 24 | 2.75 | 846 | 5 | ND | 12 | 20 | 1 | 39 | 2 | 55 | .03 | .141 | 15 | 25 | .01 | 23 | .01 | 12 | .66 | .01 | .04 | 1 | 10 | 210 |
| 46920 | 3 | 4 | 22 | 10 | .1 | 5 | 1 | 35 | .29 | 2 | 5 | ND | 15 | 3 | 1 | 2 | 2 | 5 | .06 | .004 | 7 | 6 | .04 | 77 | .01 | 9 | .32 | .01 | .21 | 1 | 3 | 90 |
| 46921 | 31 | 43 | 22 | 10 | 5.2 | 2 | 2 | 66 | .92 | 3597 | 19 | 6 | 1 | 24 | 1 | 371 | 2 | 8 | .04 | .010 | 2 | 41 | .01 | 242 | .01 | 3 | .13 | .01 | .05 | 1 | 5650 | 2600 |
| STD C/AU-R | 15 | 62 | 42 | 132 | 6.7 | 75 | 31 | 1034 | 3.81 | 35 | 16 | 7 | 40 | 52 | 18 | 17 | 21 | 61 | .48 | .095 | 40 | 52 | .30 | 180 | .07 | 15 | 1.56 | .06 | .14 | 12 | 435 | 1300 |

Mt. Nansen / Box C. (R3)

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR NG BA TI B V AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: ROCK AU ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: MAY 24 1989

DATE REPORT MAILED: June 2/89

SIGNED BY: C. Long, D. TOYE, C. LEONG, J. WANG: CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION CO. LTD. PROJECT 8905-022 337 File # 89-1188

| SAMPLE# | VC | CU | PB | ZN | AG | MO | CO | MN | FE | AS | U | AU | TH | SR | CS | SB | BI | V | CR | P | LA | CR | MG | BA | TI | B | AL | NA | K | W | AU* | Hg |
|---------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPB | PPB |
| R 46922 | 2 | 27 | 20 | 11 | .1 | 7 | 1 | 50 | .27 | 71 | 5 | ND | 1 | 6 | 1 | 20 | 1 | 2 | .02 | .002 | 2 | 4 | .01 | 15 | .01 | 5 | .11 | .03 | .05 | 1 | 1 | 50 |
| R 46923 | 3 | 59 | 15 | 62 | .1 | 50 | 23 | 1202 | 2.90 | 71 | 5 | ND | 1 | 30 | 1 | 57 | 2 | 56 | 17.52 | .035 | 3 | 141 | 2.80 | 98 | .01 | 2 | .18 | .01 | .07 | 1 | 2 | 400 |
| R 46924 | 7 | 22 | 26 | 54 | .1 | 15 | 3 | 590 | 1.25 | 60 | 5 | ND | 1 | 11 | 2 | 12 | 2 | 26 | 2.67 | .273 | 3 | 22 | .05 | 25 | .01 | 4 | .17 | .01 | .07 | 1 | 3 | 638 |
| R 46957 | 2 | 23 | 13 | 51 | .5 | 15 | 6 | 3807 | 1.55 | 184 | 5 | ND | 1 | 21 | 1 | 25 | 2 | 19 | 1.42 | .021 | 4 | 9 | .10 | 122 | .01 | 2 | .14 | .01 | .08 | 1 | 10 | 410 |

RECEIVED ICP
 JUN 1 1989
 ANALYST: HJ

A&ME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

Mt. Nansen (RD)

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B V AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: MAY 31 1989

DATE REPORT MAILED: *June 2/89.*

SIGNED BY: *C. Long* D. TOIB, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION CO. LTD. PROJECT 8906-011 File # 89-1278

| SAMPLE# | KO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SE | CD | SB | BI | V | CA | P | LA | CR | MG | BA | TI | B | AL | NA | K | V | AU* |
|------------|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|-----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPM |
| R 48658 | 3 | 54 | 21 | 24 | .1 | 7 | 2 | 67 | .85 | 16 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 17 | .03 | .002 | 2 | 6 | .13 | 28 | .02 | 7 | .23 | .04 | .07 | 1 | 3 |
| R 48659 | 2 | 15 | 19 | 28 | .1 | 8 | 3 | 149 | 1.83 | 95 | 5 | ND | 1 | 15 | 1 | 28 | 2 | 10 | .08 | .042 | 6 | 5 | .01 | 1072 | .01 | 2 | .38 | .01 | .03 | 2 | 12 |
| R 48650 | 2 | 5 | 4 | 40 | .1 | 8 | 2 | 108 | .74 | 185 | 5 | ND | 1 | 5 | 1 | 10 | 2 | 5 | .02 | .005 | 2 | 9 | .01 | 106 | .01 | 2 | .15 | .01 | .05 | 1 | 1 |
| STD C/AU-2 | 17 | 63 | 44 | 132 | 7.1 | 70 | 31 | 947 | 3.77 | 42 | 18 | 7 | 37 | 50 | 18 | 17 | 22 | 58 | .45 | .088 | 37 | 55 | .85 | 172 | .07 | 34 | 1.82 | .06 | .14 | 11 | 520 |

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE (604) 253-3158 FAX (604) 253-1716

Don C. M. Nausen (RD)

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR NG BA TI S W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1 ROCK P2-P3 SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GN SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUN 7 1989 DATE REPORT MAILED: *June 9/89* SIGNED BY: *C. Long* D. TOYE, C. LEONG, J. WANG: CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION CO. LTD. PROJECT 8906-032 337 File # 89-1374 Page 1

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mg | Fe | Ac | U | Au | Th | St | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | S | Al | Na | K | W | Au* | Hg |
|------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | .PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | PPM | PPM | PPM | |
| 18661 | 5 | 74 | 11 | 92 | .1 | 24 | 19 | 1464 | 5.66 | 12 | 5 | ND | 3 | 7 | 1 | 12 | 2 | 99 | .12 | .026 | 6 | 23 | .03 | 199 | .01 | 2 | .45 | .01 | .06 | 1 | 19 | 160 |
| 18662 | 2 | 24 | 8 | 20 | .2 | 12 | 16 | 97 | 2.32 | 236 | 5 | ND | 1 | 11 | 1 | 31 | 2 | 21 | .07 | .019 | 6 | 9 | .03 | 157 | .01 | 2 | .26 | .02 | .03 | 1 | 14 | 280 |
| 18663 | 3 | 44 | 16 | 35 | .3 | 8 | 5 | 228 | 1.45 | 99 | 5 | ND | 2 | 9 | 1 | 32 | 2 | 21 | .04 | .016 | 5 | 7 | .01 | 102 | .01 | 2 | .28 | .01 | .04 | 2 | 51 | 920 |
| 18664 | 2 | 14 | 6 | 28 | .1 | 13 | 3 | 96 | .58 | 96 | 5 | ND | 3 | 9 | 1 | 5 | 2 | 7 | .03 | .012 | 9 | 11 | .01 | 57 | .01 | 5 | .26 | .01 | .03 | 1 | 21 | 320 |
| 18665 | 7 | 9 | 14 | 11 | .2 | 9 | 1 | 39 | .74 | 171 | 5 | ND | 1 | 9 | 1 | 12 | 2 | 3 | .03 | .005 | 2 | 10 | .01 | 44 | .01 | 6 | .07 | .01 | .02 | 1 | 1 | 940 |
| 18666 | 5 | 10 | 7 | 12 | .1 | 9 | 1 | 70 | .73 | 141 | 5 | ND | 1 | 13 | 1 | 14 | 2 | 4 | .03 | .012 | 2 | 12 | .01 | 39 | .01 | 2 | .08 | .01 | .02 | 1 | 14 | 710 |
| 18667 | 2 | 39 | 13 | 49 | .1 | 54 | 22 | 1447 | 1.90 | 572 | 5 | ND | 13 | 79 | 1 | 34 | 2 | 27 | .19 | .062 | 21 | 20 | .01 | 79 | .01 | 7 | .69 | .01 | .11 | 1 | 60 | 90 |
| 18668 | 4 | 13 | 22 | 15 | .1 | 17 | 5 | 36 | 2.11 | 788 | 5 | ND | 2 | 11 | 1 | 11 | 3 | 4 | .03 | .017 | 4 | 13 | .01 | 75 | .01 | 5 | .26 | .01 | .06 | 2 | 1 | 1900 |
| 18669 | 3 | 5 | 6 | 6 | .1 | 5 | 1 | 34 | .24 | 10 | 5 | ND | 1 | 6 | 1 | 2 | 2 | 2 | .03 | .001 | 2 | 4 | .01 | 65 | .01 | 7 | .12 | .04 | .05 | 1 | 1 | 20 |
| 18670 | 16 | 16 | 9 | 49 | .1 | 10 | 4 | 49 | 2.93 | 381 | 5 | ND | 4 | 17 | 1 | 32 | 2 | 3 | .01 | .027 | 8 | 9 | .01 | 145 | .01 | 2 | .26 | .01 | .09 | 1 | 22 | 2400 |
| STD C/AU-2 | 17 | 62 | 40 | 132 | 7.1 | 73 | 31 | 949 | 3.81 | 36 | 19 | 6 | 37 | 50 | 19 | 16 | 23 | 57 | .47 | .085 | 37 | 55 | .66 | 172 | .07 | 31 | 1.96 | .06 | .12 | 12 | 510 | 1400 |

1866

NORANDA EXPLORATION CO. LTD. PROJECT 8906-032 337 FILE # 89-1374

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | As PPM | W PPM | Co PPM | Ni PPM | Fe % | Ag PPM | U PPM | Au PPM | Th PPM | Pt PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Cr % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Mn % | K % | W PPM | Au* PPM | Hg PPM |
|-------------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|-----------|
| L65Z 10250W | 1 | 21 | 7 | 46 | .1 | 12 | 7 | 205 | 3.03 | 8 | 5 | ND | 5 | 17 | 1 | 2 | 3 | 65 | .38 | .049 | 18 | 24 | .31 | 156 | .07 | 2 | .93 | .01 | .07 | 1 | 16 | 30 |
| L65Z 10225W | 1 | 15 | 9 | 56 | .1 | 12 | 8 | 193 | 4.47 | 6 | 5 | ND | 7 | 19 | 1 | 2 | 2 | 100 | .32 | .049 | 23 | 32 | .34 | 133 | .09 | 2 | .92 | .01 | .09 | 1 | 17 | 5 |
| L65Z 10200W | 1 | 17 | 10 | 47 | .1 | 12 | 7 | 156 | 4.06 | 8 | 5 | ND | 9 | 15 | 1 | 2 | 4 | 90 | .31 | .065 | 21 | 29 | .25 | 77 | .07 | 4 | .85 | .01 | .06 | 1 | 1 | 5 |
| L65Z 10175W | 1 | 17 | 9 | 43 | .1 | 11 | 6 | 136 | 2.98 | 11 | 5 | ND | 8 | 18 | 1 | 2 | 2 | 66 | .24 | .029 | 19 | 22 | .27 | 95 | .07 | 2 | .92 | .01 | .06 | 1 | 44 | 5 |
| L65Z 10150W | 1 | 11 | 7 | 44 | .1 | 10 | 6 | 153 | 3.96 | 7 | 5 | ND | 8 | 18 | 1 | 2 | 4 | 65 | .33 | .056 | 23 | 22 | .28 | 96 | .07 | 2 | .81 | .01 | .05 | 1 | 1 | 5 |
| L65Z 10125W | 1 | 17 | 10 | 51 | .1 | 12 | 7 | 152 | 3.13 | 4 | 5 | ND | 6 | 19 | 1 | 2 | 3 | 71 | .29 | .043 | 15 | 26 | .35 | 142 | .08 | 2 | 1.27 | .01 | .06 | 1 | 14 | 10 |
| L65Z 10100W | 1 | 16 | 8 | 51 | .1 | 14 | 8 | 200 | 2.85 | 11 | 5 | ND | 5 | 21 | 1 | 2 | 2 | 62 | .35 | .061 | 17 | 24 | .33 | 133 | .07 | 2 | 1.14 | .01 | .06 | 1 | 57 | 5 |
| L65Z 10075W | 1 | 14 | 2 | 43 | .1 | 11 | 7 | 163 | 3.95 | 3 | 5 | ND | 5 | 17 | 1 | 2 | 5 | 39 | .37 | .063 | 27 | 27 | .24 | 97 | .07 | 6 | .76 | .01 | .05 | 1 | 2 | 20 |
| L65Z 10050W | 1 | 16 | 7 | 56 | .1 | 10 | 8 | 220 | 3.65 | 16 | 5 | ND | 5 | 16 | 1 | 2 | 2 | 61 | .36 | .047 | 20 | 29 | .29 | 155 | .07 | 2 | .92 | .01 | .05 | 1 | 1 | 20 |
| L65Z 10025W | 1 | 16 | 4 | 51 | .1 | 10 | 7 | 222 | 3.00 | 3 | 5 | ND | 3 | 18 | 1 | 2 | 1 | 59 | .33 | .026 | 14 | 24 | .32 | 134 | .06 | 2 | 1.05 | .01 | .05 | 1 | 1 | 10 |
| L65Z 10000W | 1 | 20 | 5 | 57 | .1 | 10 | 7 | 209 | 3.10 | 24 | 5 | ND | 3 | 22 | 1 | 3 | 4 | 70 | .35 | .043 | 21 | 20 | .23 | 98 | .06 | 2 | .87 | .02 | .06 | 1 | 1 | 80 |
| L65Z 9975W | 1 | 19 | 6 | 51 | .1 | 10 | 8 | 201 | 3.59 | 3 | 5 | ND | 3 | 17 | 1 | 2 | 2 | 91 | .32 | .036 | 19 | 30 | .34 | 142 | .06 | 3 | 1.09 | .01 | .10 | 1 | 1 | 10 |
| L65Z 9950W | 1 | 20 | 9 | 58 | .1 | 10 | 9 | 199 | 5.15 | 5 | 5 | ND | 9 | 18 | 1 | 2 | 2 | 114 | .38 | .057 | 26 | 36 | .35 | 111 | .09 | 2 | 1.09 | .01 | .09 | 1 | 1 | 5 |
| L65Z 9925W | 1 | 19 | 4 | 56 | .1 | 14 | 10 | 247 | 6.75 | 3 | 5 | ND | 11 | 18 | 1 | 2 | 3 | 153 | .42 | .083 | 27 | 44 | .24 | 39 | .08 | 2 | .68 | .01 | .07 | 1 | 62 | 10 |
| L65Z 9900W | 1 | 20 | 8 | 47 | .1 | 10 | 7 | 195 | 3.70 | 2 | 5 | ND | 5 | 17 | 1 | 2 | 2 | 83 | .34 | .056 | 27 | 27 | .28 | 147 | .07 | 2 | .81 | .01 | .08 | 1 | 24 | 5 |
| L65Z 9875W | 1 | 20 | 3 | 49 | .1 | 14 | 7 | 189 | 3.23 | 4 | 5 | ND | 6 | 18 | 1 | 2 | 2 | 71 | .31 | .044 | 20 | 26 | .31 | 156 | .08 | 2 | 1.04 | .01 | .10 | 1 | 1 | 5 |
| L65Z 9850W | 1 | 19 | 6 | 54 | .1 | 11 | 8 | 206 | 3.28 | 7 | 5 | ND | 8 | 16 | 1 | 2 | 4 | 97 | .30 | .050 | 25 | 33 | .34 | 133 | .09 | 2 | .76 | .01 | .09 | 1 | 3 | 5 |
| L65Z 9825W | 1 | 28 | 11 | 50 | .1 | 13 | 9 | 229 | 2.55 | 7 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 56 | .32 | .043 | 13 | 27 | .53 | 138 | .09 | 2 | 1.72 | .02 | .10 | 1 | 3 | 10 |
| L65Z 9800W | 1 | 20 | 10 | 55 | .1 | 11 | 8 | 207 | 4.43 | 5 | 5 | ND | 8 | 17 | 1 | 2 | 3 | 99 | .33 | .059 | 22 | 29 | .32 | 108 | .08 | 8 | .93 | .01 | .07 | 1 | 64 | 5 |
| L65Z 9775W | 1 | 29 | 3 | 53 | .1 | 11 | 9 | 222 | 4.70 | 6 | 5 | ND | 6 | 17 | 1 | 2 | 2 | 109 | .21 | .059 | 20 | 31 | .29 | 111 | .08 | 9 | .33 | .01 | .07 | 1 | 1 | 5 |
| L65Z 9750W | 1 | 16 | 5 | 37 | .1 | 10 | 5 | 143 | 2.18 | 2 | 5 | ND | 5 | 16 | 1 | 2 | 2 | 50 | .31 | .047 | 17 | 18 | .27 | 92 | .06 | 2 | .63 | .01 | .06 | 1 | 1 | 5 |
| L65Z 9725W | 1 | 19 | 9 | 46 | .1 | 11 | 8 | 179 | 4.06 | 6 | 5 | ND | 7 | 17 | 1 | 2 | 3 | 91 | .34 | .066 | 24 | 28 | .27 | 96 | .07 | 2 | .77 | .01 | .07 | 2 | 19 | 5 |
| L65Z 9700W | 1 | 28 | 8 | 50 | .1 | 12 | 7 | 224 | 3.84 | 5 | 5 | ND | 8 | 18 | 1 | 2 | 2 | 90 | .36 | .074 | 21 | 27 | .36 | 118 | .08 | 7 | .89 | .01 | .09 | 1 | 97 | 5 |
| L65Z 9675W | 1 | 16 | 10 | 50 | .1 | 10 | 7 | 187 | 2.91 | 3 | 5 | ND | 6 | 17 | 1 | 2 | 2 | 64 | .31 | .056 | 19 | 24 | .35 | 132 | .08 | 2 | 1.00 | .01 | .08 | 1 | 95 | 5 |
| L65Z 9650W | 1 | 21 | 9 | 47 | .1 | 13 | 7 | 195 | 3.43 | 4 | 5 | ND | 7 | 18 | 1 | 2 | 2 | 79 | .40 | .079 | 22 | 25 | .32 | 100 | .08 | 4 | .79 | .01 | .08 | 1 | 131 | 5 |
| L65Z 9625W | 1 | 15 | 8 | 44 | .1 | 12 | 6 | 164 | 2.98 | 8 | 5 | ND | 7 | 17 | 1 | 2 | 2 | 65 | .35 | .075 | 21 | 23 | .29 | 89 | .07 | 2 | .77 | .01 | .06 | 1 | 10 | 5 |
| L65Z 9600W | 1 | 25 | 8 | 51 | .1 | 16 | 8 | 173 | 3.22 | 3 | 5 | ND | 5 | 15 | 1 | 2 | 2 | 72 | .27 | .041 | 18 | 24 | .34 | 142 | .08 | 2 | 1.01 | .01 | .09 | 1 | 1 | 5 |
| L65Z 9575W | 1 | 12 | 8 | 39 | .1 | 11 | 5 | 157 | 2.26 | 2 | 5 | ND | 7 | 17 | 1 | 2 | 2 | 50 | .35 | .063 | 21 | 19 | .27 | 77 | .06 | 14 | .66 | .01 | .06 | 1 | 1 | 5 |
| L65Z 9550W | 1 | 10 | 7 | 36 | .1 | 11 | 5 | 148 | 2.16 | 2 | 5 | ND | 5 | 17 | 1 | 2 | 2 | 47 | .37 | .068 | 25 | 17 | .24 | 63 | .06 | 14 | .59 | .01 | .05 | 1 | 1 | 5 |
| L65Z 9525W | 1 | 24 | 11 | 62 | .1 | 15 | 11 | 242 | 4.51 | 5 | 5 | ND | 7 | 18 | 1 | 2 | 2 | 101 | .33 | .049 | 22 | 31 | .48 | 151 | .10 | 2 | 1.16 | .01 | .10 | 1 | 1 | 10 |
| L65Z 9500W | 1 | 36 | 9 | 82 | .1 | 16 | 11 | 272 | 3.14 | 4 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 75 | .32 | .038 | 14 | 29 | .66 | 217 | .11 | 4 | 1.70 | .02 | .14 | 1 | 1 | 10 |
| STD C/AD-S | 17 | 62 | 29 | 132 | 7.1 | 73 | 31 | 925 | 3.77 | 39 | 18 | 5 | 36 | 49 | 17 | 15 | 22 | 56 | .47 | .086 | 36 | 55 | .86 | 174 | .07 | 31 | 1.80 | .06 | .13 | 11 | 49 | 1300 |

NORANDA EXPLORATION CO. LTD. PROJECT 8906-032 337 FILE # 89-1374

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Tb | Sr | Cd | Sb | Bi | V | Cr | P | Li | Cl | Mg | Ba | Zr | Y | Al | Na | K | W | Mo | Hf | U | Th |
|-------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | PPM | % | % | % | PPM | PPM | PPM | PPM | PPM |
| 1632 10500M | 1 | 5 | 7 | 31 | .1 | 7 | 1 | 144 | 1.64 | 4 | 5 | ND | 6 | 14 | 1 | 2 | 4 | 37 | .29 | .061 | 17 | 16 | .22 | 71 | .05 | 3 | .65 | .01 | .05 | 1 | 1 | 5 | | |
| 1632 10475M | 1 | 3 | 7 | 29 | .2 | 10 | 5 | 126 | 1.59 | 2 | 5 | ND | 4 | 13 | 1 | 2 | 2 | 34 | .21 | .049 | 12 | 17 | .29 | 57 | .05 | 4 | .94 | .01 | .05 | 1 | 1 | 10 | | |
| 1632 10450M | 1 | 16 | 9 | 52 | .2 | 12 | 7 | 131 | 2.52 | 4 | 5 | ND | 4 | 14 | 1 | 2 | 4 | 56 | .16 | .026 | 13 | 25 | .30 | 74 | .06 | 2 | 1.39 | .01 | .04 | 1 | 1 | 10 | | |
| 1632 10425M | 1 | 14 | 7 | 42 | .1 | 12 | 7 | 159 | 2.53 | 2 | 5 | ND | 5 | 14 | 1 | 2 | 2 | 58 | .26 | .058 | 19 | 22 | .33 | 71 | .07 | 3 | 1.03 | .01 | .07 | 1 | 1 | 10 | | |
| 1632 10400M | 1 | 7 | 5 | 30 | .1 | 6 | 4 | 125 | 1.10 | 2 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 22 | .26 | .050 | 12 | 12 | .22 | 74 | .04 | 4 | .58 | .01 | .06 | 1 | 1 | 5 | | |
| 1632 10375M | 1 | 3 | 5 | 26 | .2 | 11 | 5 | 154 | 2.03 | 4 | 5 | ND | 3 | 16 | 1 | 2 | 2 | 47 | .31 | .065 | 20 | 19 | .26 | 65 | .06 | 2 | .78 | .01 | .05 | 1 | 1 | 10 | | |
| 1632 10350M | 1 | 20 | 7 | 45 | .1 | 16 | 3 | 142 | 2.57 | 3 | 5 | ND | 5 | 16 | 1 | 2 | 3 | 57 | .28 | .051 | 20 | 25 | .31 | 96 | .07 | 3 | 1.16 | .01 | .06 | 1 | 1 | 10 | | |
| 1632 10325M | 1 | 31 | 7 | 51 | .3 | 17 | 3 | 157 | 2.30 | 11 | 5 | ND | 5 | 15 | 1 | 2 | 3 | 50 | .22 | .039 | 16 | 26 | .42 | 66 | .08 | 2 | 1.65 | .01 | .07 | 1 | 4 | 20 | | |
| 1632 10300M | 1 | 6 | 5 | 33 | .2 | 7 | 4 | 166 | 1.19 | 5 | 5 | ND | 5 | 15 | 1 | 2 | 2 | 33 | .33 | .070 | 18 | 16 | .25 | 73 | .05 | 2 | .68 | .01 | .06 | 1 | 1 | 5 | | |
| 1632 10275M | 1 | 11 | 9 | 27 | .1 | 10 | 5 | 163 | 1.92 | 2 | 5 | ND | 5 | 16 | 1 | 2 | 2 | 44 | .29 | .064 | 17 | 19 | .28 | 67 | .06 | 4 | .83 | .01 | .06 | 1 | 1 | 10 | | |
| 1632 10250M | 1 | 37 | 7 | 83 | .1 | 13 | 7 | 155 | 2.90 | 3 | 5 | ND | 5 | 18 | 1 | 2 | 2 | 57 | .22 | .033 | 22 | 24 | .30 | 144 | .04 | 2 | 1.33 | .01 | .06 | 1 | 1 | 10 | | |
| 1632 10225M | 1 | 23 | 7 | 52 | .1 | 13 | 3 | 189 | 2.53 | 5 | 5 | ND | 6 | 18 | 1 | 2 | 2 | 56 | .28 | .060 | 18 | 25 | .35 | 113 | .06 | 2 | 1.38 | .01 | .08 | 1 | 1 | 5 | | |
| 1632 10200M | 1 | 9 | 9 | 40 | .2 | 12 | 5 | 142 | 1.80 | 2 | 5 | ND | 5 | 17 | 1 | 2 | 2 | 39 | .27 | .060 | 15 | 18 | .28 | 87 | .05 | 2 | 1.05 | .01 | .05 | 1 | 1 | 5 | | |
| 1632 10175M | 1 | 11 | 4 | 38 | .1 | 9 | 5 | 138 | 1.91 | 2 | 5 | ND | 3 | 16 | 1 | 2 | 2 | 43 | .27 | .057 | 14 | 19 | .27 | 76 | .06 | 6 | .90 | .01 | .05 | 1 | 1 | 10 | | |
| 1632 10150M | 1 | 17 | 3 | 41 | .2 | 12 | 5 | 168 | 2.32 | 6 | 5 | ND | 5 | 18 | 1 | 2 | 3 | 52 | .30 | .062 | 18 | 22 | .30 | 79 | .06 | 2 | 1.02 | .01 | .07 | 1 | 1 | 5 | | |
| 1632 10125M | 1 | 14 | 5 | 40 | .1 | 11 | 5 | 177 | 1.98 | 5 | 5 | ND | 5 | 17 | 1 | 2 | 5 | 45 | .30 | .067 | 18 | 20 | .32 | 92 | .06 | 2 | .92 | .01 | .08 | 1 | 1 | 5 | | |
| 1632 10100M | 1 | 22 | 7 | 71 | .2 | 19 | 13 | 190 | 3.70 | 32 | 5 | ND | 3 | 27 | 1 | 2 | 4 | 95 | .28 | .026 | 12 | 31 | .64 | 147 | .11 | 2 | 2.95 | .02 | .19 | 1 | 14 | 5 | | |
| 1632 10075M | 1 | 13 | 5 | 29 | .2 | 9 | 5 | 176 | 1.92 | 6 | 5 | ND | 6 | 17 | 1 | 2 | 2 | 43 | .30 | .059 | 17 | 21 | .32 | 72 | .06 | 4 | .92 | .01 | .08 | 1 | 2 | 5 | | |
| 1632 10050M | 1 | 19 | 5 | 39 | .1 | 14 | 7 | 136 | 1.78 | 11 | 5 | ND | 3 | 16 | 1 | 2 | 2 | 39 | .24 | .045 | 10 | 18 | .33 | 86 | .06 | 2 | 1.15 | .01 | .08 | 1 | 9 | 5 | | |
| 1632 10025M | 1 | 9 | 5 | 33 | .1 | 10 | 4 | 132 | 1.47 | 5 | 5 | ND | 3 | 16 | 1 | 2 | 2 | 32 | .29 | .059 | 13 | 15 | .27 | 66 | .05 | 3 | .81 | .01 | .06 | 1 | 2 | 5 | | |
| 1632 10000M | 1 | 37 | 10 | 85 | .2 | 13 | 3 | 310 | 3.01 | 46 | 5 | ND | 3 | 19 | 1 | 3 | 5 | 57 | .35 | .047 | 19 | 26 | .33 | 151 | .04 | 5 | 1.05 | .01 | .12 | 1 | 19 | 110 | | |
| 1632 9975M | 1 | 5 | 4 | 29 | .1 | 11 | 5 | 196 | 1.42 | 5 | 5 | ND | 4 | 15 | 1 | 2 | 2 | 30 | .30 | .064 | 15 | 19 | .25 | 81 | .05 | 2 | .70 | .01 | .05 | 1 | 3 | 5 | | |
| 1632 9950M | 1 | 26 | 4 | 61 | .3 | 24 | 11 | 253 | 2.38 | 3 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 72 | .21 | .034 | 14 | 47 | .73 | 100 | .07 | 4 | 1.27 | .01 | .16 | 1 | 1 | 10 | | |
| 1632 9925M | 1 | 9 | 5 | 34 | .1 | 8 | 5 | 173 | 1.67 | 6 | 5 | ND | 4 | 15 | 1 | 2 | 2 | 38 | .28 | .064 | 15 | 17 | .25 | 55 | .05 | 2 | .75 | .01 | .06 | 1 | 3 | 5 | | |
| 1632 9900M | 1 | 6 | 3 | 30 | .1 | 6 | 4 | 150 | 1.27 | 4 | 5 | ND | 5 | 14 | 1 | 2 | 2 | 28 | .27 | .056 | 15 | 13 | .22 | 48 | .04 | 11 | .59 | .01 | .05 | 1 | 22 | 5 | | |
| 1632 9875M | 1 | 3 | 6 | 30 | .2 | 9 | 4 | 167 | 1.57 | 2 | 5 | ND | 5 | 15 | 1 | 2 | 2 | 34 | .31 | .068 | 19 | 15 | .23 | 64 | .05 | 7 | .62 | .01 | .05 | 1 | 16 | 5 | | |
| 1632 9850M | 1 | 9 | 4 | 30 | .1 | 9 | 4 | 109 | 1.52 | 4 | 5 | ND | 4 | 13 | 1 | 2 | 2 | 33 | .23 | .045 | 16 | 16 | .22 | 73 | .05 | 6 | .82 | .01 | .04 | 1 | 1 | 5 | | |
| 1652 10500M | 1 | 37 | 7 | 53 | .1 | 14 | 9 | 306 | 2.79 | 4 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 59 | .31 | .049 | 16 | 27 | .48 | 157 | .07 | 11 | 1.50 | .01 | .07 | 1 | 14 | 20 | | |
| 1652 10475M | 1 | 31 | 4 | 57 | .1 | 10 | 9 | 252 | 2.52 | 3 | 5 | ND | 4 | 24 | 1 | 2 | 2 | 55 | .37 | .055 | 22 | 24 | .45 | 180 | .07 | 2 | 1.11 | .01 | .10 | 1 | 18 | 30 | | |
| 1652 10450M | 1 | 14 | 5 | 39 | .1 | 10 | 7 | 226 | 2.53 | 6 | 5 | ND | 5 | 18 | 1 | 2 | 2 | 57 | .27 | .059 | 18 | 22 | .28 | 95 | .06 | 3 | .92 | .01 | .06 | 2 | 9 | 5 | | |
| 1652 10425M | 1 | 36 | 12 | 55 | .2 | 18 | 3 | 193 | 2.73 | 13 | 5 | ND | 4 | 20 | 1 | 2 | 2 | 57 | .27 | .050 | 17 | 29 | .46 | 152 | .07 | 2 | 1.87 | .01 | .09 | 1 | 3 | 20 | | |
| 1652 10400M | 1 | 20 | 10 | 55 | .1 | 13 | 7 | 210 | 2.62 | 9 | 5 | ND | 7 | 17 | 1 | 2 | 2 | 58 | .26 | .046 | 15 | 24 | .31 | 135 | .06 | 2 | 1.25 | .01 | .07 | 1 | 2 | 10 | | |
| 1652 10375M | 1 | 29 | 3 | 95 | .1 | 10 | 9 | 304 | 3.11 | 9 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 62 | .32 | .032 | 11 | 18 | .66 | 176 | .09 | 2 | 1.84 | .01 | .14 | 1 | 42 | 20 | | |
| 1652 10325M | 1 | 24 | 7 | 51 | .1 | 11 | 7 | 182 | 2.33 | 14 | 5 | ND | 4 | 22 | 1 | 2 | 2 | 51 | .31 | .042 | 18 | 23 | .42 | 149 | .07 | 3 | 1.08 | .01 | .08 | 1 | 14 | 40 | | |
| 1652 10300M | 1 | 14 | 7 | 47 | .1 | 10 | 5 | 207 | 2.62 | 3 | 5 | ND | 3 | 19 | 1 | 2 | 2 | 61 | .25 | .040 | 16 | 23 | .30 | 152 | .07 | 2 | 1.00 | .01 | .08 | 1 | 9 | 10 | | |
| 1652 10275M | 1 | 3 | 3 | 38 | .2 | 9 | 5 | 253 | 1.90 | 5 | 5 | ND | 5 | 15 | 1 | 2 | 2 | 47 | .29 | .049 | 19 | 18 | .26 | 113 | .05 | 3 | .71 | .01 | .06 | 1 | 8 | 5 | | |
| STD C/AU-5 | 19 | 62 | 39 | 132 | 6.8 | 73 | 31 | 1018 | 3.85 | 42 | 20 | 7 | 37 | 51 | 18 | 15 | 16 | 59 | .47 | .090 | 38 | 56 | .87 | 177 | .07 | 35 | 1.84 | .05 | .13 | 12 | 49 | 1308 | | |

Mr. Hanson (RD)

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE (604)253-3158 FAX (604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR NH PE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: ROCK AD* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUN 16 1989 DATE REPORT MAILED: June 22/89 SIGNED BY: C. Hanson, D. TOYE, C. LIONG, J. WANG; CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION CO. LTD. PROJECT 8906-061 337 / File # 89-1556

| SAMPLE# | Ni | Cu | Pb | Zn | Ag | Mn | Co | Mo | Fe | As | U | Au | Tb | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | V | Au* | Hg |
|------------|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|-----|------|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | % | % | PPM | PPM | % | PPM | % | % | % | % | PPM | PPM | PPM | |
| 48671 | 1 | 67 | 4 | 44 | .1 | 9 | 12 | 360 | 3.20 | 2 | 5 | ND | 1 | 380 | 1 | 2 | 2 | 84 | 3.94 | .143 | 2 | 13 | 1.15 | 161 | .09 | 2 | 5.03 | .41 | .16 | 1 | 1 | 10 |
| 48672 | 1 | 18 | 2 | 61 | .1 | 6 | 4 | 333 | .88 | 7 | 5 | ND | 1 | 245 | 1 | 2 | 2 | 13 | 28.28 | .022 | 2 | 11 | 1.03 | 51 | .01 | 2 | .36 | .01 | .01 | 1 | 2 | 10 |
| 48673 | 1 | 19 | 2 | 21 | .5 | 4 | 2 | 116 | 1.09 | 2 | 5 | ND | 4 | 13 | 1 | 2 | 2 | 7 | .13 | .009 | 8 | 21 | .14 | 26 | .02 | 19 | .32 | .04 | .03 | 1 | 1 | 5 |
| 48674 | 2 | 2 | 4 | 4 | .1 | 9 | 1 | 44 | .41 | 2 | 5 | ND | 1 | 2 | 1 | 2 | 2 | 3 | .05 | .004 | 2 | 6 | .03 | 1 | .01 | 2 | .09 | .01 | .01 | 1 | 3 | 10 |
| 48675 | 3 | 30 | 13 | 21 | .1 | 11 | 3 | 31 | 1.47 | 189 | 5 | ND | 1 | 17 | 1 | 29 | 2 | 8 | .04 | .009 | 5 | 11 | .01 | 91 | .01 | 10 | .36 | .01 | .05 | 1 | 23 | 1600 |
| 52226 | 3 | 24 | 15 | 33 | .2 | 12 | 4 | 49 | 1.69 | 362 | 5 | ND | 1 | 22 | 1 | 24 | 2 | 10 | .42 | .015 | 3 | 9 | .02 | 107 | .01 | 11 | .31 | .01 | .04 | 1 | 21 | 1800 |
| 52227 | 2 | 39 | 13 | 26 | .1 | 14 | 6 | 57 | 2.25 | 367 | 5 | ND | 2 | 28 | 1 | 29 | 2 | 14 | .03 | .021 | 5 | 33 | .01 | 421 | .01 | 3 | .37 | .01 | .06 | 1 | 22 | 1900 |
| 52228 | 1 | 4 | 4 | 9 | .1 | 4 | 1 | 72 | .58 | 2 | 5 | ND | 1 | 2 | 1 | 2 | 2 | 4 | .04 | .001 | 3 | 3 | .03 | 11 | .01 | 4 | .16 | .03 | .05 | 1 | 3 | 20 |
| 52229 | 1 | 2 | 4 | 16 | .2 | 5 | 1 | 30 | .37 | 11 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 8 | .11 | .009 | 5 | 6 | .04 | 33 | .01 | 2 | .36 | .02 | .03 | 1 | 1 | 170 |
| 52230 | 2 | 25 | 10 | 14 | .2 | 8 | 2 | 22 | .92 | 211 | 5 | ND | 2 | 20 | 1 | 34 | 2 | 10 | .03 | .008 | 5 | 10 | .01 | 352 | .01 | 5 | .43 | .01 | .07 | 1 | 26 | 1000 |
| STD C/AU-1 | 10 | 63 | 40 | 132 | 6.5 | 69 | 31 | 951 | 4.17 | 40 | 18 | 6 | 37 | 49 | 18 | 15 | 19 | 59 | .52 | .089 | 38 | 56 | .91 | 175 | .07 | 36 | 2.00 | .06 | .13 | 12 | 515 | 1400 |

NORANDA VANCOUVER LABORATORY

PROPERTY/LOCATION: MT. NANSEN

CODE : 8906-061

Project No. : 337

Sheet: 1 of 4

Date rec'd: JUN 16

Material : 173 SDILS

Geol.: R.D.

Date compl: JUL 04

Remarks :

Values in PPM, except where noted.

| T. T. No. | SAMPLE No. | Ag | As | PPB Au |
|--------------|---------------|-----|----|-----------|
| 54 | 6100E-9500N | 0.2 | 1 | 40 |
| 55 | 9550 | 0.1 | 1 | 5 |
| 56 | 9600 | 0.2 | 1 | 5 |
| 57 | 9650 | 0.4 | 1 | 5 |
| 58 | 9700 | 0.3 | 1 | 20 |
| 59 | 9750 | 0.2 | 1 | 5 |
| 60 | 9800 | 0.1 | 1 | 5 |
| 61 | 9850 | 0.2 | 1 | 5 |
| 62 | 9900 | 0.2 | 2 | 5 |
| 63 | 9950 | 0.2 | 2 | 5 |
| 64 | 10000 | 0.2 | 4 | 5 |
| 65 | 10050 | 0.2 | 6 | 5 |
| 66 | 10100 | 0.3 | 1 | 5 |
| 67 | 10150 | 0.1 | 1 | 5 |
| 68 | 10200 | 0.2 | 1 | 5 |
| 69 | 10250 | 0.1 | 1 | 5 |
| 70 | 10300 | 0.1 | 1 | 5 |
| 71 | 10350 | 0.1 | 1 | 5 |
| 72 | 10400 | 0.1 | 1 | 5 |
| 73 | 10450 | 0.2 | 1 | 5 |
| 74 | 6100E-10500N | 0.3 | 1 | 5 |
| 75 | 6300E-9500N | 0.1 | 1 | 5 |
| 76 | 9525 | 0.2 | 1 | 5 |
| 77 | 9550 | 0.1 | 4 | 5 |
| 78 | 9575 | 0.1 | 1 | 5 |
| 79 | 9600 | 0.2 | 4 | 5 |
| 80 | 9625 | 0.3 | 2 | 5 |
| 81 | 9650 | 0.2 | 2 | 5 |
| 82 | 9675 | 0.3 | 4 | 5 |
| 83 | 9700 | 0.1 | 46 | 5 |
| 84 | 9725 | 0.1 | 4 | 5 |
| 85 | 9750 | 0.1 | 6 | 5 |
| 86 | 9775 | 0.2 | 1 | 5 |
| 87 | 9800 | 0.1 | 1 | 5 |
| 88 | 6300E-9825N | 0.2 | 4 | 5 |
| 89 | 6700E-9675N | 0.4 | 6 | 5 |
| 90 | 9700 | 0.1 | 2 | 5 |
| 91 | 6725 | 0.2 | 4 | 35 |
| 92 | 6750 | 0.2 | 2 | 5 |
| 93 | 9825 | 0.3 | 1 | 5 |
| 94 | 9850 | 0.2 | 6 | 5 |
| 95 | 9875 | 0.3 | 1 | 5 |
| 96 | 9900 | 0.1 | 1 | 5 |
| 97 | 9925 | 0.2 | 1 | 5 |
| 98 | 9950 | 0.2 | 2 | 5 |
| 99 | 9975 | 0.3 | 10 | 5 |
| 100 | CHECK NL-6 | 1.1 | 90 | 5 |
| 101 | 6700E-10000N | 0.3 | 1 | 5 |

22. 10. 11

| T. T. No. | SAMPLE No. | Ag | As | PPB Au |
|--------------|---------------|-----|-----|-----------|
| 102 | 6700E-10025N | 0.2 | 6 | 5 |
| 103 | 10075 | 0.2 | 1 | 5 |
| 104 | 10100 | 0.5 | 260 | 5 |
| 105 | 10125 | 0.2 | 54 | 5 |
| 106 | 10150 | 0.3 | 18 | 5 |
| 107 | 10175 | 0.3 | 8 | 5 |
| 108 | 10200 | 0.3 | 12 | 5 |
| 109 | 10225 | 0.3 | 6 | 5 |
| 110 | 10250 | 0.2 | 4 | 5 |
| 111 | 10275 | 0.2 | 1 | 5 |
| 112 | 10300 | 0.4 | 10 | 5 |
| 113 | 10400 | 0.2 | 1 | 5 |
| 114 | 10500 | 0.4 | 1 | 5 |
| 115 | 6700E-14750N | 0.3 | 4 | 15 |
| 116 | 6900E-9500N | 0.2 | 10 | 5 |
| 117 | 9525 | 0.2 | 4 | 5 |
| 118 | 9550 | 0.3 | 10 | 5 |
| 119 | 9575 | 0.2 | 1 | 5 |
| 120 | 9600 | 0.2 | 1 | 5 |
| 121 | 9625 | 0.2 | 1 | 5 |
| 122 | 9650 | 0.2 | 8 | 5 |
| 123 | 9675 | 0.1 | 6 | 5 |
| 124 | 9700 | 0.1 | 14 | 5 |
| 125 | 9725 | 0.1 | 12 | 5 |
| 126 | 10150 | 0.2 | 8 | 5 |
| 127 | 10225 | 0.1 | 4 | 5 |
| 128 | 10250 | 0.1 | 1 | 5 |
| 129 | 10275 | 0.2 | 6 | 5 |
| 130 | 10300 | 0.2 | 10 | 5 |
| 131 | 10325 | 0.2 | 4 | 5 |
| 132 | 10350 | 0.2 | 10 | 5 |
| 133 | 10450 | 0.3 | 12 | 90 |
| 134 | 10500 | 0.2 | 10 | 5 |
| 135 | 10575 | 0.2 | 4 | 5 |
| 136 | 10625 | 0.4 | 10 | 5 |
| 137 | 10650 | 0.1 | 2 | 5 |
| 138 | 10725 | 0.1 | 4 | 5 |
| 139 | 10800 | 0.1 | 4 | 5 |
| 140 | 10850 | 0.1 | 4 | 5 |
| 141 | 10875 | 0.1 | 4 | 5 |
| 142 | 11050 | 0.1 | 6 | 5 |
| 143 | 11075 | 0.1 | 1 | 5 |
| 144 | 11100 | 0.2 | 1 | 5 |
| 145 | 11125 | 0.1 | 1 | 5 |
| 146 | 11150 | 0.2 | 1 | 5 |
| 147 | 11175 | 0.3 | 16 | 5 |
| 148 | 11200 | 0.2 | 10 | 5 |
| 149 | 11225 | 0.1 | 6 | 5 |
| 150 | CHECK NL-6 | 1.1 | 80 | 1 |
| 2 | 6900E-11250N | 0.1 | 2 | 5 |
| 3 | 11275 | 0.1 | 8 | 5 |
| 4 | 11300 | 0.2 | 1 | 5 |
| 5 | 11325 | 0.1 | 6 | 5 |
| 6 | 11350 | 0.1 | 4 | 5 |
| 7 | 11375 | 0.1 | 8 | 5 |
| 8 | 6900E-11400N | 0.2 | 8 | 5 |
| 9 | 7300E-9000N | 0.1 | 4 | 5 |

T. T.
No.SAMPLE
No.

Ag

As

PPB
Au8906-061
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| T. T. No. | SAMPLE No. | Ag | As | PPB Au |
|-----------|--------------|-----|----|--------|
| 10 | 7300E-9050N | 0.1 | 4 | 5 |
| 11 | 9100 | 0.1 | 10 | 5 |
| 12 | 9150 | 0.1 | 2 | 5 |
| 13 | 9300 | 0.2 | 1 | 5 |
| 14 | 9350 | 0.1 | 1 | 10 |
| 15 | 9550 | 0.1 | 4 | 5 |
| 16 | 9600 | 0.1 | 1 | 5 |
| 17 | 9650 | 0.1 | 1 | 5 |
| 18 | 9700 | 0.1 | 6 | 5 |
| 19 | 9850 | 0.3 | 1 | 5 |
| 20 | 9900 | 0.3 | 16 | 5 |
| 21 | 9950 | 0.2 | 1 | 5 |
| 22 | 7300E-10000N | 0.2 | 8 | 5 |
| 23 | 7500E-9200N | 0.1 | 1 | 5 |
| 24 | 9250 | 0.2 | 1 | 5 |
| 25 | 7500E-9850N | 0.3 | 1 | 5 |
| 26 | 10700E-6500N | 0.4 | 1 | 20 |
| 27 | 6550 | 0.5 | 2 | 5 |
| 28 | 6600 | 0.4 | 4 | 5 |
| 29 | 6650 | 0.4 | 1 | 5 |
| 30 | 6700 | 0.3 | 1 | 5 |
| 31 | 6750 | 0.3 | 4 | 5 |
| 32 | 6800 | 0.2 | 6 | 5 |
| 33 | 6850 | 0.3 | 2 | 5 |
| 34 | 6900 | 0.2 | 1 | 5 |
| 35 | 6950 | 0.2 | 1 | 5 |
| 36 | 7050 | 0.2 | 8 | 5 |
| 37 | 7100 | 0.2 | 1 | 10 |
| 38 | 7150 | 0.3 | 2 | 5 |
| 39 | 7200 | 0.2 | 1 | 5 |
| 40 | 7250 | 0.3 | 1 | 5 |
| 41 | 7300 | 0.2 | 1 | 5 |
| 42 | 7350 | 0.2 | 4 | 5 |
| 43 | 7400 | 0.2 | 4 | 5 |
| 44 | 7450 | 0.2 | 2 | 5 |
| 45 | 10700E-7500N | 0.4 | 1 | 5 |
| 46 | 10900E-6500N | 1.1 | 36 | 5 |
| 47 | 6550 | 0.2 | 2 | 100 |
| 48 | 6600 | 0.3 | 6 | 5 |
| 49 | 6650 | 0.2 | 1 | 5 |
| 50 | 6700 | 0.2 | 1 | 5 |
| 51 | 6750 | 0.3 | 1 | 5 |
| 52 | 6800 | 0.3 | 1 | 5 |
| 53 | 6850 | 0.2 | 1 | 5 |
| 54 | 6900 | 0.3 | 1 | 5 |
| 55 | 7000 | 0.3 | 1 | 5 |
| 56 | 7050 | 0.4 | 1 | 5 |
| 57 | 7100 | 0.5 | 6 | 5 |
| 58 | 7150 | 0.3 | 12 | 5 |
| 59 | 7200 | 0.4 | 4 | 5 |
| 60 | 7300 | 0.2 | 1 | 5 |
| 61 | 7350 | 0.2 | 2 | 5 |
| 62 | 10900E-7450N | 0.2 | 2 | 35 |
| 63 | 11100E-6500N | 0.3 | 2 | 5 |
| 64 | 6550 | 0.3 | 18 | 400 |
| 65 | 6600 | 0.2 | 20 | 5 |
| 66 | 11100E-6650N | 0.2 | 1 | 5 |

T. T.
No.

SAMPLE
No.

Ag

As

PPB
Au

8906-061
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| | | | | |
|----|--------------|-----|---|----|
| 67 | 11100E-6700N | 0.3 | 1 | 5 |
| 68 | 6750 | 0.2 | 1 | 5 |
| 69 | 6800 | 0.3 | 1 | 5 |
| 70 | 6850 | 0.3 | 1 | 5 |
| 71 | 6900 | 0.3 | 1 | 5 |
| 72 | 6950 | 0.2 | 1 | 5 |
| 73 | 7000 | 0.3 | 1 | 5 |
| 74 | 7050 | 0.1 | 1 | 5 |
| 75 | 7200 | 0.2 | 1 | 25 |
| 76 | 7300 | 0.2 | 1 | 5 |
| 77 | 7350 | 0.2 | 4 | 5 |
| 78 | 11100E-7400N | 0.2 | 1 | 5 |