MAP NO.: 115 I 3

ASSESSMENT REPORT X
PROSPECTUS
CONFIDENTIAL X
OPEN FILE

DOCUMENT NO: 092770
MINING DISTRICT: Whitehorse
TYPE OF WORK: Geophysical, Trenching

REPORT FILED UNDER: Aurchem Exploration Ltd

DATE PERFORMED: 1 June-30 July, 1989

DATE FILED: 4 December, 1989

LOCATION: **LAT.:** 62°05'N

AREA: Mt Nansen

LONG.: 137°10'W

VALUE $: 5675.00

CLAIM NAME & NO.: RAS 1-4 (YA93138-41); MSL (YA95099); BIT 1-5 (YA97733-7); WEDGE 5-10,15 (YA82171-6, YA82181)

WORK DONE BY: M. Langdon

WORK DONE FOR: Aurchem Exploration Ltd

DATE TO GOOD STANDING:

REMARKS: #56 GOULTER

Gold, silver and lead occur in veins associated with north and north-west trending porphyry dykes. Most work in 1989 consisted of bull-dozer and backhoe trenching on the WILLOW CREEK zone. A new zone was identified at ELIZA CREEK where two parallel north-trending veins 11 and 22 m wide are associated with numerous smaller subparallel veins consisting of clays, quartz and manganese and iron oxides.

1989 Exploration Program
Report on Trenching, Geology, Magnetometer
Survey and Soil Geochemical Survey carried out
on Wedge 5, Wedge 6, Wedge 7, Wedge 8, Wedge 9
Wedge 10, Wedge 15, Ras 1, Ras 2, Ras 3, Ras 4
MSL, Bit 1, Bit 2, Bit 3, Bit 4, Bit 5
Claim Sheet 115I/3, 62° 05'N/137° 10W
June 1, 1989 to Sept. 30, 1989

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Mark Langdon
Manager - Geological Projects
November 1989

This report has been examined by the Geological Evaluation Unit under Section 53 (4) Yukon Quartz Mining Act and is allowed as representation work in the amount of $ 5675.00.

for Regional Manager, Exploration and Geological Services for Commissioner of Yukon Territory.

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Introduction

The claims and accompanying Leases have been explored by Aurchem Exploration Ltd. from 1985 to present.

The bulk of our 1989 work program consisted of bulldozer/backhoe trenching in our Willow Creek Zone within the granodiorite host. Past work has been concentrated in this area uncovering a number of interesting veins. The 1989 trenching consisted of follow up on these zones by deepening existing trenches, trenching on drill indicated veins and trenching in on-strike areas. The goal was to attain better geological knowledge of the characteristics of the vein structures along strike in the areas of grade, vein width, the effects of various faults, etc.

Aurchem has developed a theory of post vein emplacement gravity slides. The same vein structure can be exposed on surface in various blocks on the property showing different paleo-elevations of the same vein structure. Based on the belief of this theory, a trenching program was conducted on four other zones outside our main Willow Creek Zone. One of these zones, the Eliza Creek Zone, showed excellent potential for the existence of a mineable ore-body so further follow-up work was done. This consisted of the formation of a surveyed grid being established with 100 foot spaced lines with 50 foot station spacings. A total field magnetometer survey was completed on this grid along with a partial geochemical survey.

Some metallurgical testwork was also done on vein material. This preliminary data helps to direct our exploration efforts by giving us some idea of the material's metallurgical characteristics and thus some idea of the grade/tonnage required.

Minor soil geochemical samples were also taken on parts of the property as on-strike follow up work and on new untested areas.

Location

The claims are located in the valley of Discovery Creek, a tributary of Nansen Creek. Access is from Carmacks by going west on the Mount Nansen Road. The claims are approximately 10 km by road past the Mount Nansen Mine site or 70 km by road west of Carmacks.

Property Claim Maps

Two claim maps can be found in the back folder. The "Discovery Creek" claim map shows the entire property with the claims and leases. This claim map is drawn from ground distances, not horizontal distances.

A second claim map called "Eliza Creek Zone - Claim Map" shows the western and central portions of our ground. This claim map is based on horizontal distances and is much more accurate in locating the claims than the former map.

The Eliza Creek claim map shows that the LGCS 1 and LGCS 3 claims do not contain any ground that was not previously covered by earlier claims. The open space between the Bull claims and our claims shown by the government's claim map does not exist.

Wedge 9 also shows to hold less than 1% of a claim block because of the Bull claims.

On our southern boundary our property adjoins the Joanne Claims. These claims have not yet been located so the existence of Bit claims 3, 4 and 5 and possibly Ras 4 have not yet been verified.

Boundary problems on the north and east sides also exist with Wedge 16 and 17, Dome and TBR claims overlapping with each other and our claims. The now expired ME claims are part of the problem on the east side. The north and east side boundaries do not, at present, pose any problems for our future exploration plans.

General Geology

A simplified geology map is found in the back folder.

Outcrops on the property are rare (5 known outcrops). The bulk of the property is non-glaciated and overburden consists of in-situ weathered rock and/or slumped rocks from nearby. Near Discovery Creek and the lower ends of Willow, Shaw and Eliza Creeks there is some glacial-fluvial overburden of variable thickness up to 50 feet.

Near and within our "Paleocreek trench" is an area studied this summer by the government's glacial geologists. It shows on aerial photographs as an oval shaped mound about 100 feet in diameter. This mound consists of highly cross-bedded layers of sand and highly rounded and manganese coated beds of pebble conglomerate. Beneath the mound (25 feet) is a larger area of green clay up to ten feet thick with some subrounded boulders up to 2 feet in diameter. The lithologies of the zone are composed of rocks foreign to the region.

Our target of exploration is an epithermal vein system that hosts Au, Ag, Pb, and Zn on our property. This system follows a northwest fault zone and can be traced both to the north and south of Aurchem's property for a number of kilometers. The veins strike from N290° to N345° (usually N330°) and dip steeply (75°- 85°) to the west. Any or all lithologies on the property can host the veins.

The western edge of the property host the Precambrian to Cambrian age Yukon Group metasediments and metavolcanics. These rocks are a highly metamorphosed group of shists and gneisses of a usually siliceous nature.

A large block of our property hosts a sub-intrusive hornblende diorite of Jurassic age.

The Casino Granodiorite of early Cretaceous age is our most common lithology. It is found on the east side of the diorite but probably overlaid the diorite and may underlie it at depth.

Andesite dykes and sills intrude the above lithologies and are presumed to belong to the Mount Nansen Volcanic unit. These began in middle Cretaceous time and may have continued until the late Cretaceous where they may be genetically related to the Carmacks Group. Dykes of this group we have found show a porphyrytic texture with large euthedral plagioclase crystals. The dykes also sub-parallel the vein system. All of the above lithologies are then cut by variably altered, porphyry dykes of andesite to rhyolitic composition. These dykes occured before, during and after the epithermal veins, have the same strike as the veins and are probably genetically related to the heat source of the epithermal system. Veins are found within some porphyry dykes and on one occasion a porphyry dyke graded into a vein. A very close relationship is obvious but the implications are not clear. The dykes may have been competing for space in the fault controlled zones that the epithermal system was enlarging and subsequently filling. The porphyry dykes may be a late phase of the Mount Nansen Volcanics implying the source for the Volcanic Group is the same as that for the heat source of the epithermal system.

A megacrystic granite outcrops just above the forks of Eliza Creek. Individual K-spar and quartz crystals are up to 1 cm in size. The outcrop shows a relatively fresh and unaltered appearance to the granite until you go downhill to the junction of the creek branches. Three major faults cross at this junction and the granite becomes sheared and displays "augen" texture quartz eyes. The age of the granite is unknown. It is strongly possible that it may have a direct relationship to the epithermal system. Within the granodiorite (Cretaceous age) there are found hydothermally potassium enriched patches irregular in nature. Also within the granodiorite are found rare K-spar rich dykes of granitic material less than six inches wide. It is possible that the K-spar enriched patches (which pre-date the epithermal alteration overprinted) and these thin dykes may be sourced from the granite thus making the granite one of our youngest lithologies. It is also located very close to where we believe was the centre of the epithermal system.

Model of Mineralization

I will give a brief description of our model here since we use it to guide our exploration efforts. Our model, although it appears a bit "wild" to most continues to hold up through our exploration data and has helped our effort considerably. We will continue to use it or adjust it accordingly as new data dictates. Overall the model's movements, in our opinion, have occured but the number of movements, which block overrides the other or vice-versa, etc., is not clear. Therefore, we follow the model's directives to certain areas but cannot dismiss other areas as our interpretation of the movements and their order may not be correct.

The controlling feature of the epithermal system is a large N310° - N330° fault. This is a regional fault probably produced by plate tectonics. Lithologies within the whole belt generally conform to this direction whether by source or later movement. Along this fault magma chambers rose giving sources of epthermal/hydrothermal situations. We believe one such centre occured as shown below (Fig. 1).

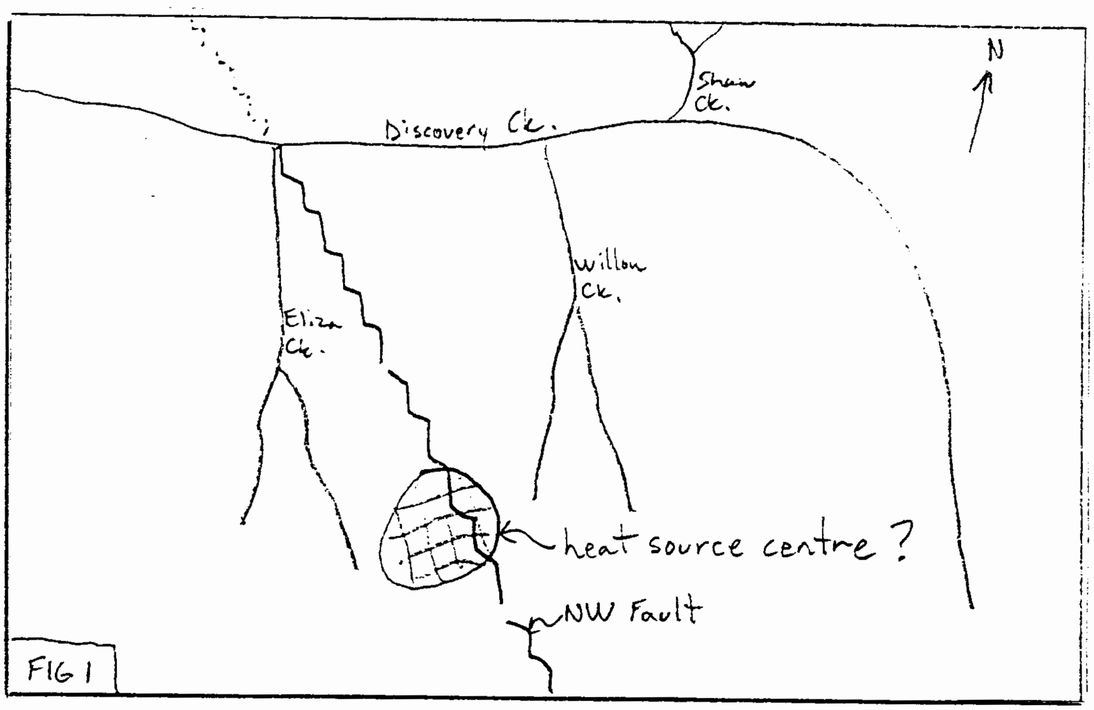


FIG. 1

The magma heat source most likely produces the porphyry dykes and the rhyolitic/dacitic domes in the region. An up-swelling occurs with the intrusion causing a very large and high mountain to occur. The epithermal system occurs throughout this major uplift. The majority of the veins are produced, structurally controlled by the major NW fault system. A silicified cap forms through which rhyolitic domes are produced up through the fault in locations along strike. The upswelling continues forming numerous cross-faulting systems. Finally the upswelling becomes too much and through the network of faults, large blocks of ground slide off the top. The centre of the heat source shown on Fig. 1 is really the point where the gravity slides move in a radial fashion from this point. This point is controlled by the fault system so may not be the actual centre of the heat source or the highest peak.

North and south movements of blocks appear to be dominant at first. North and east of Discovery Creek we appear to be in silicified granodiorite. Northeast of our property the top of the northwest fault can be seen with rhyolitic domes trending along the fault. We feel this may represent the silicified cap of this system.

After north-south block slides, east-west slides from the centre point appear to become dominant.

Each time a block of ground slides off a pressure release is formed causing new telescoping veins possibly to occur through the system. Cooling of the heat source then took place accompanied by collapsing through contraction. Minor veins telescope in collapsing forming some veins in other fault directions.

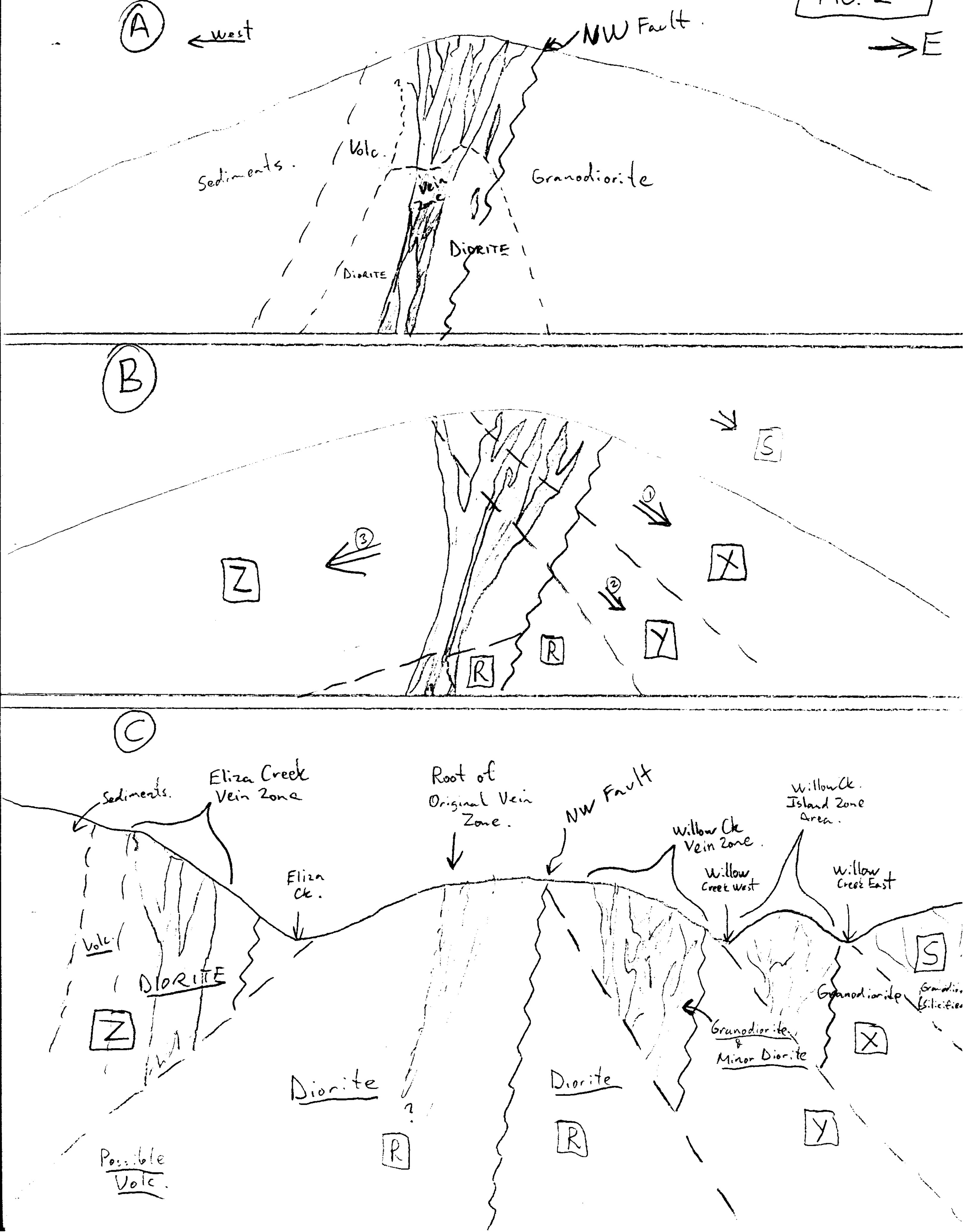
Aurchem's vein zones of Willow Creek and Eliza Creek have been uncovered by north trending block slides. The east-west slides then sub-divided our target vein zone. Fig. 2 on the next page illustrates this theory. After the movements shown in Fig. 2 have occured, collapsing causes cross-fault dip slip movements. A major north trending fault also shows pre-epithermal strike-slip movement and probably post-epithermal dip slip movement.

If the above movements stated are true, it creates a bit of a mess due to intense faulting but the gains may outweigh the negatives. The blocks themselves appear to be quite thick. The Willow Creek block from drilling is at least 450 feet thick. The slides produce a situation where we can look for economic pods at different paleo-elevations of the same vein at surface. This gives a good open pit potential from larger tonnages also.

Lithologies Versus Veins

Lithology of the host obviously plays a strong role in dictating the characteristics of the veins produced. Alteration halos and vein width will show marked differences through different lithologies with the same fault fracture control. Early work on our property and using data from nearby properties tended to confirm a belief for preferred lithologies for economic

FIG. 2



A
west
NW Fault
E
Volc.
Sediments.
Vein Zone
Granodiorite
DIORITE
DIORITE
B
S
X
Y
Z
R
R
R
C
Sediments.
Eliza Creek Vein Zone
Root of Original Vein Zone.
NW Fault
Willow Ck. Island Zone Area.
Willow Ck Vein Zone.
Eliza Ck.
Willow Creek West
Willow Creek East
S
Volc.
DIORITE
Granodiorite
Z
Granodiorite & Minor Diorite
X
Diorite
Diorite
Y
R
R
Possible Volc.

veins. Evidence suggests the granodiorite is by far the best lithology for wide veins. This would be followed by the intermediate volcanics and the diorite/sediments being tied for last place. In our belief of this we have concentrated our efforts within the granodiorite. I now believe we were wrong in this assessment. The lithology host plays a strong role but is only a secondary controlling factor. By far the major controlling factor is the nature of the fault/fracture system controlling the hydrothermal solutions. If a vein does cross lithologies into the granodiorite the vein will expand as the granodiorite may act as a pressure release due to its characteristics. But a vein totally within one of the other lithologies will not have this pressure release?, so although it may be more difficult for the solutions to penetrate the host and create a wider structure, it can occur.

A typical 5 foot wide advanced argillic/vein mixture structure in the granodiorite shows an argillic halo of tens of feet and propylitic halo of 50-100 feet on either side. (i.e. usually hit another vein before propylitic alteration ends). A similar vein/advanced argillic structure in the diorite shows the entire alteration halo usually less than three feet with the argillic measured in inches. But the width of the vein/advanced argillic centre, I now believe, is not controlled by the lithology but by the structure. Our widest advanced argillic/vein zones found to date, are all found within a diorite host. Even with the wider structures the alteration halo into the diorite was again very narrow (<3 feet).

Faulting

Faulting is quite intense on the property with a number of fault trends. Some broad, generalizations can be made for some trends in relation to the veins and the lithologies. The data is taken from what is seen in the Willow Creek Zone.

(a) NW Fault;

The NW fault (N310° - N330°) was described partially in the discussion of the model. It presumably dips the same as the veins at 75° to 80° west. It is difficult to pin-point exactly where the fault is located but it appears to be east of the vein zone and acts something like a footwall. The veins themselves run parallel and sub-parallel to this fault possibly in sub-fractures formed by the fault. In other words there is a zone 300-400 feet wide to the west of the major fault of sub-faults and fractures which the veins occupy.

Movement in the fault is speculative but appears to be left lateral in the order of a couple of hundred feet.

(b) North-South Faults;

These faults strike N345° to N00°, can dip either east or west (usually greater than 60°) and were probably pre-epthermal originally. They are regional faults found commonly within the belt. On our area a left lateral movement of about 300-400 feet pre-epithermal appears to be possible. Post-epithermal movements mostly as dip-slip faults also occur. The relationship of the north faults to the NW faults is confusing. Both faults appear to fault each other to some extent. Possibly the north fault comes in, the NW fault offsets this fault and then later the N fault moves to offset the NW fault. This last movement may have occured during uplift and collapse of the epithermal system.

(c) NE Fault;

This fault at N45 is common on the property. The dip is unknown. It appears to be an early fault that pre-dates the epithermal and is regional in extent. They are possibly regional stress faults related to plate tectonics. Very large lateral movements can take place but is appears that later movement was minimal in most cases after vein emplacement.

(d) N75° Fault

This fault is very similar in all aspects to the NE fault above and may be genetically related. All I can really say about this fault is that left lateral lithology displacements appear to occur.

(e) N110° Collapse Faults;

One large and numerous minor faults occur at N110°/75° south. These appear to be post gravity slides, post epithermal, and are fairly local to this area. They may be best explained as collapse faults. They appear to occur as reverse dip-slip faults. They occur not as a single fault but as a zone of faults. The zone may be 100 feet wide with 10 faults, each with the footwall slipping down a little further than the last one. Many show late one inch wide quartz/galena veins within them. They tend to shear the main veins and cause short vein offsets (less than 10 feet) due to the paleo elevation change and the dip of the vein.

Faults - General;

One peculiar feature about the above faults is that they all try to intersect each other at the same point. Wherever a NW hits a north or NE fault, a N110° fault will also appear. It is common to locate a point and see 4 or 5 different trending faults all converging to this point. The significance of this is unclear.

Mineralization/Veins

The mineralization occurs in two distinct phases with a very minor third phase overprinted.

(a) Third Phase;

The third phase are very late stringers of quartz-galena-minor sphalerite and pyrite that came up the N110° faults. Although silver and gold values can be high they are generally only one inch wide stringer veins. They are generally non-oxidized and their chemistry closely follows that of the second phase veins as small shoots during the final collapsing of the epithermal dome. Economically they are not that significant, but may play a part in up-grading earlier veins where they cross.

(b) First Phase;

The first phase veins strike at N340° - N350° and dip 75° west. They are a brecciated cherty quartz (blue quartz) vein carrying arsenopyrite-pyrite-galena-sphalerite. They display multiple-phase brecciation of a hydrothermal nature. Very late brecciation shows a brecciation infill matrix of Ca-carbonate. The calcite/dolomite matrix carries no precious metal values and tends to just dilute the earlier grade. Earlier brecciation matrix was quartz and does carry mineralization. Many of the breccias commonly display calcite filled vuggs and pits. Precious metal values closely follow the sulphide content with high values showing when the cherty quartz-sulphide becomes very black from sulphides.

Their appearance, their different strike, the presence of Ca-carbonate, Pb/Zn ratios of less then one and their unoxidized nature make these veins easily distinguishable from the later second phase veins.

The widths of the veins vary from 3 feet up to 50 feet. Gold and silver values tends to be low in the .020 oz/ton Au range but sections have run up to 3 feet of .200 oz/ton Au and grab samples up to .400 oz/ton Au and 10 oz/ton Ag. Precious metal values are highly erratic. Intrusions of second phase veins, usually on the hanging and footwalls obscure the true values found in the first phase material.

The first phase vein material has been found almost exclusively on the east side of the N345 fault. Two parallel veins run continuously for at least 2000 feet of strike being within 200 feet (east) of this N345°fault. Their hanging wall sides usually have the best grades. They are surrounded by very large argillic and propylitic alteration halos. The easterly vein generally has better assay values than the western vein.

Paralleling these veins on the footwall of the fault (ie. the hanging wall of the veins) is a sheared fault/vein zone. Veins of "blue mud" (phyllic-carbonate alteration) occur interspearsed with barren zones of highly sheared very fine green clay. The "blue mud" veins are like lenses of vein material along the fault which have been sheared up by late dip slip movement on this fault. The veins can contain up to 25% sulphide mainly as pyrite/arsenopyrite and can be up to 50 feet wide. Higher lead, gold and silver values are found on the hanging wall side of the zone which range up to .200 oz/ton Au over 2 feet. Precious metal values are highly erratic with similar looking material going from .200 to nil oz/ton Au. There is no relationship to Fe-sulphides and precious metals but values show a direct correlation to silicification and visual galena.

Sometimes (rarely) in the brecciated cherty-quartz-sulphide veins, patches or veinlets of white quartz (sulphides, vugs) can be found. Precious metal values increase dramatically in these areas. This white quartz (not cherty quartz) may be related to the second phase mineralization as this type of quartz is the dominant type there.

(c) <u>Second Phase;</u>

The second phase mineralization is distinctly different from the first phase veins and they are definitely later veins. Within the group of second phase veins there can be wide differences in their characteristics due to temperature forming different assemblages but overall they have common characteristics.

The veins have a strike of N310° to N330° and dip westerly generally steep at about 75°. Lower temperature forms are the most common which all display a very strong oxidized form. This oxidation is likely supergene of acid generation and goes to considerable depth. The vein zone itself appears as a white clay mud (almost like plaster) composed of kaolimite clays, quartz, sericite, limonite and possibly alunite. Economic minerals are dominated by gold, silver, lead and variable zinc. Galena as the dominant sulphide has been almost completely replaced by cerussite which can then be coated with a manganese rich carbonate. Silver occurs as native silver but usually (80%) as acanthite (argentite) as rims on galena/cerussite grains. Therefore, the silver values are directly related to the lead values. Zinc, originally as sphalerite, shows an increase in content proportionally to the lead, but at a slower rate of increase. Therefore, Pb/Zn values in the veins are almost always greater then one. Gold is erratic and although grades tend to increase with higher Ag, Pb and Zn values, there is no direct relationship. We have been unable to identify gold's association even with high grade values in thin section. It is possibly as very fine electrum/free gold.

Quartz is found as druzy/vuggy clasts and so far assays show the quartz component to run lower grades than the vein as a whole.

Visually it is very difficult to access silver/gold values in individual veins. The cerussite is very difficult to see in the veins except in very high grade sections, (15-60% Pb) and then only lead silver values can be expected. Within the advanced argillic zone, a centre core of cerussite rich material is usually found. In wider veins, multiple "cores" of cerussite are found. In some veins in the Willow Creek area the oxidation is not complete and a mixture of very fine galena/sphalerite/pyrite shows up as purple/blue streaks within the white veins.

In the 11 South trench a higher temperature form of second phase veining is found. Here an unoxidized central core consists of massive vuggy quartz with 30% coarse euhedral pyrite (10 foot width). This is surrounded on both sides with an advanced argillic (white mud) halo. Other than the visual differences the cental core and halo contains no kaolinite clays (illite) but has sericite, ankerite, ferroan dolomite and arsenopyrite. Tetrathedrite is common (some argentite rims) and minor chalcopyrite and galena are found.

In the Willow Creek area the second phase veins show a network of multiple veins which branch and join in an anastomosing network. Veins vary from 3-30 feet in width. Grades are very erratic. In the Eliza Creek zone veins show considerably greater width and possible continuity (greater than 65 feet wide). It all cases the second phase veins show narrow alteration halos outside of the advanced argillic/vein zones (less than 5 feet) compared to the first phase veins with alteration halos measured in tens of feet.

In the Willow Creek zone the two north faults (N00° and N345°) give a strict control on the N330° veins by post-vein movement on these northerly faults. All veins were found to terminate upon hitting the northerly faults. It is unknown at this time if this will hold true in the Eliza Creek zone also. This movement may be associated with the collapse stage which could act very differently in separate blocks and different lithologies.

It is hard to give general assays of they second phase veins as the range from nil to very high. In the Willow Creek area 5-10 feet of .1 gold equivalent (Au/Ag) and 2% Pb may be typical but high grade patches are common. One sample this year over 1.5 feet of width gave .867 oz/ton Au, 16.8 oz/ton Ag and 17.3% Pb. Grab samples previously gave results as high as .200 oz/ton Au, 90.0 oz/ton Ag and 62.0% Pb.

Geophysics and Soil Geochems - General

Specific details on these aspects will be dealt with under results of work. Here I would like to express general comments.

VLF (EM-16) work was done in previous years and subsequent follow-up work showed it to be of only limited value. The VLF appears to show up the north trending faults as good crossovers with secondary inclination anomalies on the first phase veins. Lithology change from diorite to granodiorite also shows a reaction but this contact is usually faulted in variable amounts which obscures the meaning of the anomaly. The second phase veins appear to have little to no response on the VLF. Most likely they give a small response which is totally obscured by the strong responses I discussed above. This caused our early trenching and drilling to focus on the first phase veins and it was only by chance that we would intercept a second phase vein in our trenches. We therefore switched to magnetometer due to the nature (advanced argillic) of the veins and this method has proved highly effective. A low magnetometer reading is found over the vein and due to the small alteration halos even the width of the vein can sometime be inferred. In order to get useful data from the magnetometer you must do very close station readings. In the Willow Creek area, for example, where numerous narrow veins are found, we were required to use a station spacing of about ten feet. In the Eliza Creek area where the vein widths are much larger, a 25 foot spacing on 100 foot spaced lines was used.

For regional exploration 200 foot spaced lines with 50 feet station readings could be used. Anywhere that a band or zone of anomalous readings are found, you would have to redo these zones in greater detail.

Soil geochemical sampling was done generally on 100 foot spaced lines on 50 foot stations. Elements of Au, Ag, As, Pb, and Zn were assayed. They all correlate very well to each other with Au being a little erratic. They generally "broad band" vein zones but are rarely site specific for veins or their relative grade. Very high anomalies have formed over low grade veins and some high grade veins have been found underlying a soil geochem of little or no anomaly. Too many surface features effect the soil samples to give site specific targets. Cross faulting also appears to strongly effect the soil values. The post vein N110° collapse faults tend to show good anomalies. The contoured geochem maps would suggest that the veins trend at N110° because of this effect but the magnetometer data and surface trenching show this not to be so.

Of all elements, lead appears to be the best indicator because of it's relative stable form in the surface oxidized state and the direct relationship of lead in our second phase veins. Pb/Zn ratios plotted show good correlation with vein zones.

On Aurchem's property the surface ash tuff layer found regionally is almost absent, usually being less than one inch thick. A small area just east of the upper forks of Eliza Creek show it to be about 15 inches thick. Overall the ash layer poses no problems in doing soil geochem work on the property. Surface slumping, depth of overburden, cross-faults, permafrost, minor landslides and vein surface solifluction are the main problems in interpretation of the soil values.

Assays

Assay results of samples taken in trenches are shown in Appendix I. They have been arranged into groups showing assays of each trench. In most cases the widths shown are close to true widths.

The depth of a trench on a vein zone that is required to accurately display the vein is a major problem with using trenching to access veins. The highly erratic values within the veins themselves add to this problem. On some veins the values found are the same at three feet of depth as at 10 or 20 feet. In other cases you get low values for 10 to 15 feet and then an upgrade of 10 or 20 fold by digging an addition two feet deeper. Accessing the proper depth required is almost impossible in most cases. Therefore a "guess" or "feeling" for each trench on whether it was deep enough must also be brought into the interpretation of the results found.

Results of 1989 Exploration and Work Done

The following results have been divided up into six categories based on our geologic model of blocks of ground showing different paleo-elevations. It is done this way since our exploration program was based partly on this model. The Trench Location Map in the back folder will locate individual trench locations and names. General values stated below are sometimes in gold equivalent of Au, Ag, Pb, Zn.

1) Courtland Trench Area

This work encompassed deepening of the existing trench. This is our only trench north of Discovery Creek. This zone represents our highest paleosurface. Our optimism was not very high for this area, but past work indicated a better look was required. The trench was deepened from 10 feet to 22 feet by the use of a backhoe. A second phase vein about 10 feet wide and a first phase vein zone (multiple veins) of about 75 feet was found. The granodiorite host shows signs of silicification.

Assays on the second phase vein were barely anomalous. Within the wider first phase vein zone, the best values were:

6 feet of .061 oz/ton Au equivalent.
7 feet of .020 oz/ton Au equivalent.
4 feet of .063 oz/ton Au equivalent.

Some zinc and arsenic values were strong but on the whole, base metal values were very low. The lead values, our best indicator, are the lowest of anywhere yet looked at on the property (ie. highest value was 439 ppm).

No further work is anticipated in this area in the near future.

2) Willow Creek Island Trench Area

Only the one trench was dug on this block. We believe that this is one "slice" up from the Willow Creek Zone.

The trench was based on two things; (1) four soil geochem samples that gave about 5.0 ppm silver; (2) a verbal report by Mrs. Goulter of having found native silver in the stream there.

A 150 long foot trench was dug to about 10 feet of depth. It uncovered a highly propylitic and argillic granodiorite with a 3 foot wide porphyry dyke. No indication of a vein was seen. A very rusty overburden was shown which probably hosted the high silver geochems. This disappeared with depth. Only weakly analmous values are found in the assay results. No further work is anticipated in this area in the near future.

3) Willow Creek Zone

This zone has seen our main thrust of work done in the past and in 1989. Within the granodiorite, numerous veins had been located. Our objective was to get a better look at these veins by trenching on strike and deepening

existing trenches accompanied with detailed sampling.
Each trench displays a number of veins that in most cases pinch and swell, branch or join other veins, etc. This made vein correlation between trenches difficult. Intense faulting was also observed as discussed earlier.

The high number of veins makes reporting of this area difficult, so I will attempt to report mainly the highlights and generalities.

a) Two South Vein

In the 2 South trench we have one of our main second phase veins. It displays numerous parallel veins both east and west of it. It strikes N310°- N330° and dips steeply west (75 west). To the north (within the 2 South Trench) the vein terminates abruptly on a N00° fault. To the south the vein has been traced for about 600 feet of strike length. Grab samples within this vein have yielded some very high assays;

Au - up to .525 oz/ton
Ag - up to 83.0 oz/ton
Pb - up to 62.0%

In 2 South, four sample channels have been taken across the main vein from a 3 foot to 12 foot depth. Although individual assays have been very erratic, the combined totals across the vein have been very similar. They showed;

11 feet of .114 oz/ton Au equivalent withing 16 feet of .100 oz/ton Au equivalent.

To the south (100 feet on strike) the vein is exposed in the Line 11 trench where we found;

13 feet of .059 oz/ton Au equivalent within 24 feet of .036 oz/ton Au equivalent.

To the south (300 feet on strike) the vein is exposed in the 12E trench where it assays;

7 feet of .161 oz/ton Au equivalent.

Twenty feet further from above the vein swells and assays;

30 feet of .106 oz/ton Au equivalent.

About 600 feet from 2 South on strike is the 14E trench. This shallow trench barely reached the top expression of the vein but assayed;

12 feet of .022 oz/ton Au equivalent.

To the east of the vein in the 2 South trench, a number of parallel veins were found that have not been chased on strike. They are summarized below and are all within 200 feet of the main vein;

1 foot of .036 oz/ton Au equivalent.
6 feet of .275 oz/ton Au equivalent.
3 feet of .018 oz/ton Au equivalent.
8.5 feet of .082 oz/ton Au equivalent.

b) D12 Vein

This vein runs at N330°/75° west and is about 200 feet west of the 2 South vein. In 1987 DDH-87-12 intersected;

4 feet of .313 oz/ton Au equivalent within 12.3 feet of .121 oz/ton Au equivalent (at a 60 foot vertical depth).

Trenching at this location uncovered;

4 feet of .103 oz/ton Au equivalent A surface expression on strike 250 feet south is found in trench 14 east showed 2 veins which gave;

2 feet of .096 oz/ton Au equivalent.
3.5 feet of .070 oz/ton Au equivalent (i.e. trench not deep enough).

c) 11 South Vein

This vein found previously did not see much work in 1989 because of the deep overburden cover in this area. This makes trenching very slow and expensive.

The original showing found at a 15 foot depth gave;

15 feet of .064 oz/ton Au equivalent including 5 feet of .173 oz/ton Au equivalent.

This vein is a higher temperature form of the secondary veins showing a quartz/massive pyrite core containing tetrahedrite. In 1989 we deepened this trench by about 5 feet and got assays of;

11 feet of .110 oz/ton Au equivalent includes 6 feet of .176 oz/ton Au equivalent.

The Ag/Au ratios in this vein are much higher than normal with individuals silver assays over a one foot width reaching 23.2 oz/ton.

To the north this vein likely terminates about 50 feet on strike against the N350° fault. To the south it had been previously located by DDH-88-9 (50 feet south) at a depth of 200 vertical feet. Roughly on strike 400 feet to the south, near the lower end of the D4 trench, a vein was found of very high grade that might be an extension or branch of the 11 South vein. It assayed;

1.5 feet of .867 oz/ton Au
16.8 oz/ton Ag (1.543 oz/ton Au equivalent)
17.3% Pb

In trench 13 we did not locate the 11 South extension as it failed to reach the required depth for the vein. Deepening of the trench in 1990 will likely be done.

d) D4 Vein

DDH-87-4 intersected;

6 feet of .105 oz/ton Au equivalent withing 19 feet of .057 oz/ton Au equivalent (at 50 feet of vertical depth).

This vein also shows massive sulphides with abundant tetrahedrite of a higher temperature source.

A trench was dug over this zone (12 feet deep) and the vein was found but at this depth it was not sulphide rich. Two channel samples gave;

20 feet of .020 oz/ton Au equivalent.
4 feet of .119 oz/ton Au equivalent.

An on strike vein, 300 feet to the north in Trench 13 assayed;

5 feet of .104 oz/ton Au equivalent.

An on strike vein 325 feet to the south in the H4 trench assayed;

19 feet of .020 oz/ton Au equivalent.

It is not known if these strike extensions are really the same vein.

e) D14 Vein

DDH-88-14 intersected a vein right at surface that assayed;

6 feet of .166 oz/ton Au equivalent.

This area was trenched. Then the exposed vein was trenched on strike for 200 feet to the north and 100 feet to the south. Therefore the final trench shows the vein for about 300 feet of strike length. What was found was a system of veins which branch, pinch and swell, join other veins, etc. The best assay of numerous cross-cuts was at the exact location of where the drill hole had intersected. It gave;

7 feet of .105 oz/ton Au equivalent.

Assays of other sections of the vein and it's branches gave;

4.5 feet of .039 oz/ton Au equivalent.
3 feet of .058 oz/ton Au equivalent.
9 feet of .039 oz/ton Au equivalent.

12 feet of .032 oz/ton Au equivalent.
8 feet of .058 oz/ton Au equivalent.

f) <u>D8 Vein</u>

DDH-88-8 had intersected a vein at a 180 feet of vertical depth of;

19 feet of .036 oz/ton Au equivalent including 2 feet of .208 oz/ton Au equivalent.

Trenching over this zone uncovered a vein of;

11 feet of .069 oz/ton Au equivalent.

Onstrike 300 feet to the south a vein in Trench 13 gave;

10 feet of .025 oz/ton Au equivalent.

g) <u>W8 Trench</u>

This existing trench was deepened by about 10 feet and move westward by cut and fill with the backhoe. The aim was to get a look at the secondary veins west of the N350° fault. Two veins were found about 12 feet apart, trending N330°. Both terminate to the south against the N350° fault within the trench. Also seen was a N110° cross-fault (dip slip collapse fault) which had the effect of a left lateral movement of 5 feet on both veins. The two veins, although narrow (less than 3 feet and average 2 feet in width) showed the advanced argillic/vein material with pods of massive sulphides along strike. These pods assayed up to;

.050 oz/ton Au
15.2 oz/ton Ag (.844 oz/ton Au equivalent)
.5% ZN
14.2% Pb

These pods (only 4 feet in length) gave the appearance of being related to the N110° cross-faults. It is unknown if this relationship is true.

h) <u>Paleocreek Trench/L4 Trench</u>

About 125 feet on strike from the veins of W8 (above) we had a soil geochem give us a 1400 ppb Au value. Therefore, we trenched across this location in the hope of finding one of the sulphide pods of W8 in an enlarged form. Unfortunately, the trench never got though the green-clay bottom of the "paleocreek" (discussed earlier) where the vein was projected to be. Due to the Paleocreek's thickness though, it is doubtful that the gold geochem was caused by the underlying vein. About 50 feet west of there a vein was found that assayed;

12 feet of .048 oz/ton Au equivalent.

About 450 feet on strike to this vein to the north, the L4 trench produced two parallel veins which gave;

12 feet of .038 oz/ton Au equivalent.
1.6 feet of .304 oz/ton Au equivalent.

i) <u>First Phase Veins</u>

To the east of the N350° fault a number of sometimes wide but low grade first phase brecciated blue quartz veins occur (N350°/75° west).

Some of the assays of these are as follows;

In the W8 trench;

4 feet of .013 oz/ton Au equivalent.
13 feet of .014 oz/ton Au equivalent.
1.5 feet of .103 oz/ton Au equivalent.
4 feet of .048 oz/ton Au equivalent.
3 feet of .050 oz/ton Au equivalent.

(All of the above veins are within a 100 foot wide zone.)

In the 3 South Trench;

6 feet of .044 oz/ton Au equivalent
2 feet of .117 oz/ton Au equivalent
3 feet of .024 oz/ton Au equivalent

In Trench 13;

22 feet of .022 oz/ton Au equivalent includes 6 feet of .049 oz/ton Au equivalent.

In the H4 Trench;

34 feet of .024 oz/ton Au equivalent.
20 feet of .033 oz/ton Au equivalent.

The H4 trench veins above are separated by 10 feet. West of there (about 100 feet) is where DDH-87-3A showed a first phase vein of;

51 feet of .017 oz/ton Au (gold alone).

The H4 trench being about 225 feet long shows that at least 50% of this is vein material. Although the grades are quite low, this zone does show some encouragement for a larger tonnage heap leach type operation. The zone shows multiple second phase veins intruding up first phase vein boundaries and many 1" wide stringers within the N110°faults. The zone shows a wide area of multiple cross-faulting, making interpretation difficult.

4) Central Diorite Block

Not much work has been done on this block. The block is entirely composed of diorite with some porphyry dyke intrusions (as far as we know).

Although out stated model suggests this to be our deepest block, this may not be true. Another possible model, which also fits well, is that the Central Diorite Block and the Willow Creek Block are really one block. When the Willow Creek zone slides up over the Eliza Creek Zone, this would put the Central Block as originally being west of our main zone overlying an area near the western boundary of our claim groups. The N00° fault displays a wide (up to 50 feet) shear zone of post-vein emplacement but this may be from minor movement during gravity sliding and collapse rather than a thrust block surface. A skematic of this model possibility shown on the next page.

The N00° fault displays a vein(?) along this fault that strikes N00° and is semi-continuous as blocks and pods. It would be my guess that this is not really as it appears and that the vein blocks and pods represent numerous veins that were caught up in the fault. Grab samples of some of these blocks have given very good assays;

2 feet of .916 oz/ton Au equivalent.
2 feet of 1.220 oz/ton Au equivalent.

These blocks also contain As values of 1-10% and contain both first and second phase vein material.

Other veins just west of the N00° fault were found in the western end of the trenches or in the "drains" of trenches that targeted the Willow Creek zone. Some values in this area are;

In the 2 South trench;

1.5 feet of .107 oz/ton Au equivalent.
3 feet of .087 oz/ton Au equivalent.
2 feet of .116 oz/ton Au equivalent.
6 feet of .200 oz/ton Au equivalent.

In the L11 trench;

6 feet of .055 oz/ton Au equivalent.

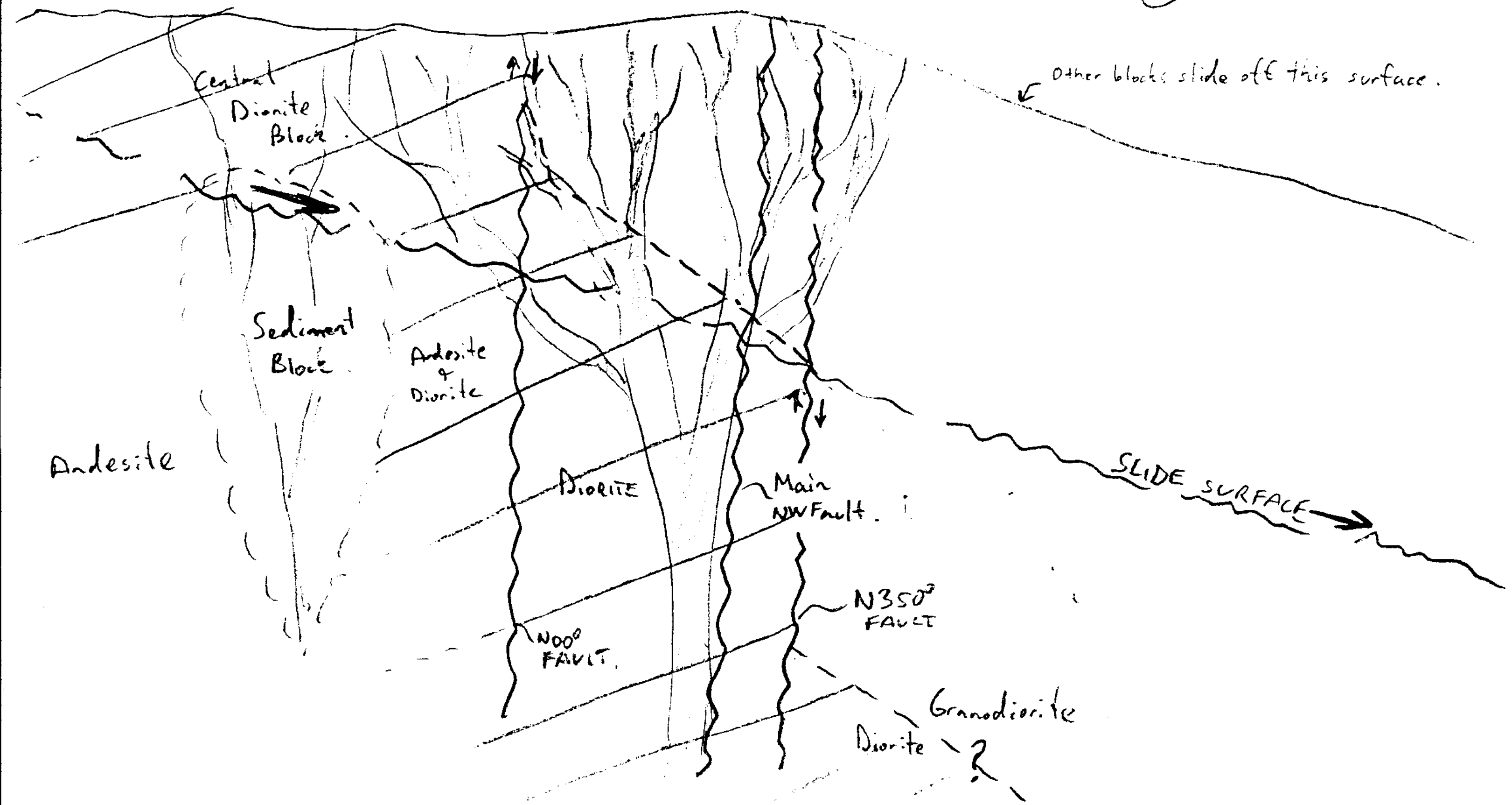
In the D12 trench in the drain (at 4 feet of depth).

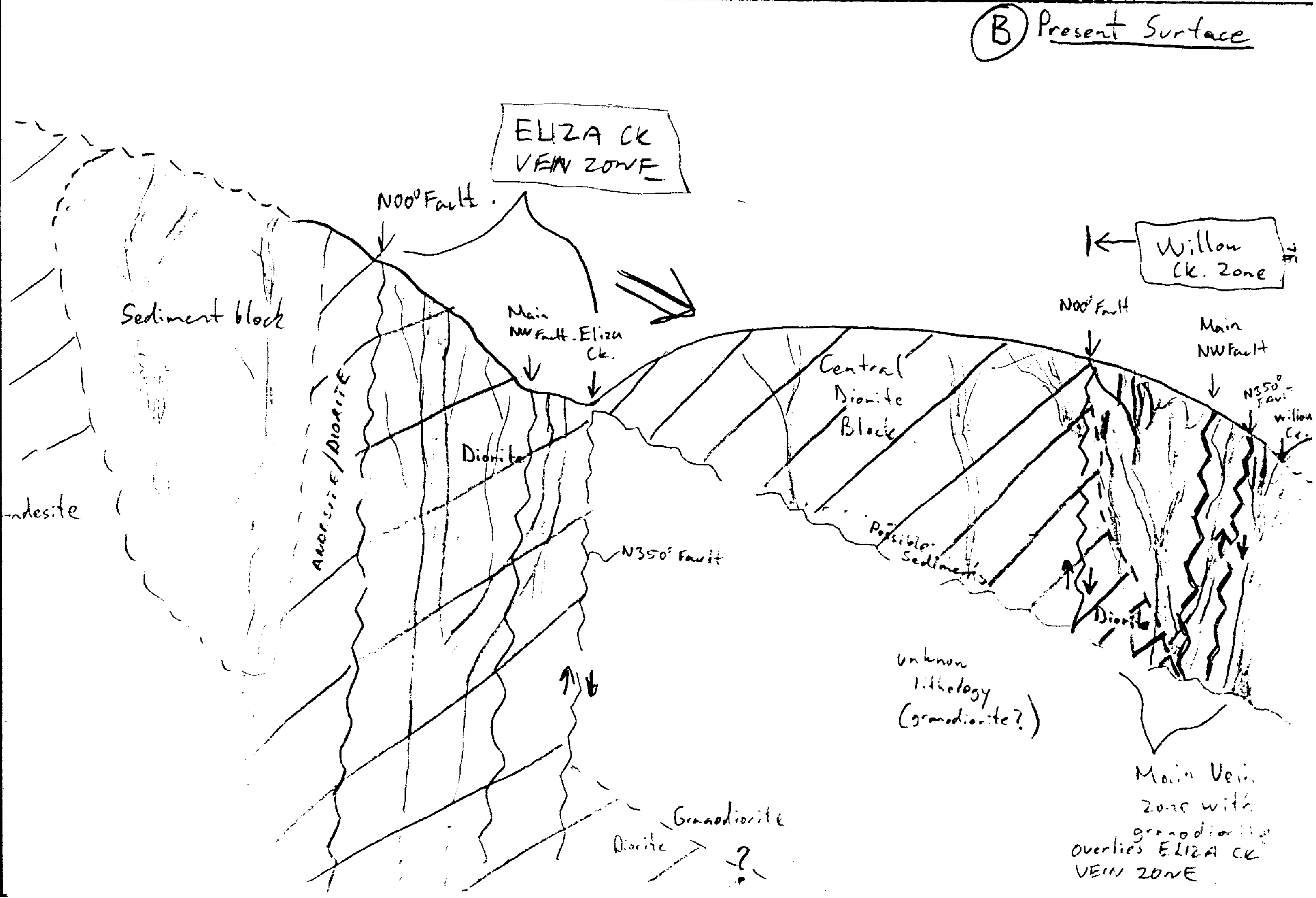
10 feet of .094 oz/ton Au equivalent.

Onstrike to the above vein about 350 feet to the south the L14 west trench showed two veins giving;

12 feet of .064 oz/ton Au equivalent.
2 feet of .344 oz/ton Au equivalent.

OTHER POSSIBLE SLIDE MODEL.





The 8 South trench was deepened by backhoe and uncovered an area with many narrow veins. The N00 fault runs through the centre of the trench and displays post vein and lithology movement. The area shows a number of porphyry dykes up to 50 feet wide which themselves contain narrow (2 feet) veins. One narrow porphyry dyke showed a transformation from dyke to vein along a 5 foot strike length. Some of the assays in the 8 south area are;

2 feet of .374 oz/ton Au equivalent.
2 feet of .184 oz/ton Au equivalent.
2.5 feet of .132 oz/ton Au equivalent.
3 feet of .070 oz/ton Au equivalent.

The bulk of the Central Diorite Block was covered by the magnetometer and soil geochem surveys of the Eliza Creek Zone. A number of targets are shown which future work will investigate, the most obvious being the area near Discovery Creek. This area is also where the Goulter's hand dug adit is located (now caved in) from the early 1900's.

One zone uncovered in 1989 of significance was the H5 trench. I suspect this zone is within the Central Diorite Block but it is uncertain. Therefore I treat it separately below.

5) H5 Trench Results

The lithology host in the trench is diorite. No porphyry dykes were seen. This vein is in a block which either overlays or underlies our Eliza Creek Vein close to the southern end of our property boundary. The trench at present is definitely not deep enough to properly expose the vein (has just reached the top exposure). Some of the rubble piles suggest that we are also very close to the contact of a block of highly altered sediment or carbonate lithologies (strange looking pieces of material that looked almost like a limestone skarn were found). On the original surface many clasts of the Yukon Group Metasediments can be found in the H5 area. These clasts are the same lithology as outcrops found west of our Eliza Creek zone about 1600 feet west-northwest of the H5 area.

A second phase vein was uncovered of considerable width which is very similar in appearance to our Eliza Creek 16 trench zone. The vein at present strikes N330° (dip unknown but likely 75° W) and the western boundary of the vein has not yet been found (ie. vein width open to west). At present the vein is 45 feet wide (true width) which assays;

45 feet of .052 oz/ton Au
.57 oz/ton Ag (.060 oz/ton Au equivalent)
.1% Pb

6) Eliza Creek Zone

Past work in this area (west of Eliza Creek) was limited to geochems, some magnetometer and VLF geophysics and one incomplete drill hole (DDH-87-8). This preliminary data suggested a broad zone of veining similar to that in the

Willow Creek Area but within a diorite host. The diorite as host and the physical factors of the area kept us away from here. Two preliminary trenches dug this year show great encouragement. Because of this a surveyed grid was established on which a total field magnetometer survey and partial soil geochem survey were conducted.

An overview of the data suggests two main veins that appear to be continuous (about 3000 feet of strike length each) within our property boundaries. Our two preliminary trenches show that both main veins have a broad width so a larger tonnage potential was created.

The Elevation Contour Map - Eliza Creek shows the general topographic setting. The generally steep slope on permafrost makes backhoe and cat work difficult and thus more costly. The northeast facing slope gets very little summer sunshine so thawing of the permafrost is very slow. A trench in the Willow Creek area left for 24 hours would generally thaw about six inches of depth. In Eliza Creek we were lucky if we had one inch of thaw.

A) Trench Results in Eliza Creek

i) "S" Trench

This trench is located at Line 800 north/50 east. It was the deepening of an old trench (unknown who originally dug it) at its easterly end. This was the site of a magnetometer anomaly and a minor geochem anomaly. It was also the easiest accessable location in the Eliza Creek area. At the junction of Eliza Creek and Discovery Creek, the overburden (transported) is seen to be 50-80 feet thick. Therefore it was viewed that we should stay away from trenching close to Eliza Creek and move up the slope enough to try to eliminate the overburden thickness. Aerial photographs also show a strong N330° lineament running through the trench location.

The original trench showed a depth of about 6-8 feet and was still in overburden with no veins showing. We basically scraped this off with the cat and then backhoed a trench of 4 feet additional depth (total depth 10 feet). At this point two or three 6 inch rusty streaks appeared and a five foot wide secondary "white mud" vein was found on the east end. The material surrounding this vein was a frozen diorite sand and not bedrock so the ground was re-dug with the cat about two feet deeper than the bottom of the backhoe trench (about 12 feet of depth). At this point, a vein zone of significance could be seen. The red streaks had turned into veins (2-3 feet wide) and the 5 foot vein was now 9 feet wide. Also 8 feet east of this vein was a newly uncovered vein with an 11 foot width. Assays of veins at this stage were (from east to west);

3 feet of .050 oz/ton Au equivalent.
3 feet of .042 oz/ton Au equivalent.
9 feet of .064 oz/ton Au equivalent.
11 feet of .058 oz/ton Au equivalent.

An interesting feature seen there was that the 11 feet wide vein was completely cut off above it by a waterlain, very dark green to black layer of diorite sand (frozen). This layer dips about 20 to the east under which the vein was located. Digging with a hand shovel at the eastern edge of the 11 feet wide vein showed the vein to continue to the east under this "sand" wedge. Therefore, we brought the backhoe in and had a 2 foot deep trench dug over the 9 and 11 foot wide veins.

The 9 foot vein narrowed to 3 feet of width in the backhoe trench. Onstrike 15 feet to the north this vein swelled to about 15 feet of width. The 3 foot section was sampled and assayed;

3 feet of .098 oz/ton Au equivalent.

The 11 foot vein showed considerable width expansion from the removal of the diorite sand overlying it. We uncovered another 10 feet of vein to expose a 21 foot width. This assayed;

21 feet of .060 oz/ton Au equivalent.

From the assays in Appendix I it can be seen that the gold values themselves were quite low and that the bulk of the value came from Ag, Pb, and Zn. The most easterly 4 feet of the vein shows the best gold values. The last sample to the east showed;

2 feet of .040 oz/ton Au
1.56 oz/ton Ag
2.12% Pb
.19% Zn

Once again hand digging on the eastern edge of the vein shows that the vein continues on the east going under the diorite sand wedge. A relatively wide vein zone that is open to the east (where the assays withing the vein are increasing to the east) make this a very promising zone. The detailed magnetometer survey suggest this vein may continue 25-50 feet more in width, after which a broad low then continues for another 200 feet before a definite high is found. Optimism would suggest a series of parallel smaller veins over this 200 feet of width as we find on the west side of the vein. As we go east though, the overburden will get progressively thicker so trenching may not prove a viable method. With an aggressive trenching program on this location I feel we could uncover bedrock for about 50 feet east of our present vein boundary and better expose the true nature of the vein.

ii) <u>Eliza Creek 16 Trench</u>

The "S" Trench showed the eastern main vein. The Eliza Creek 16 Trench attempted to open up both the east and west main veins. It is located near Line 0 from 200 west to 300 east.

On the east vein we failed to penetrate the overburden. We are presently at a ten foot depth in this area and have seen no sign of bedrock or veins as yet.

One feature worth mentioning here is that the overburden suggests that a landslide took place at some earlier time. After scrapping off the black organic layer (3 inches) and then about 5 feet of overburden, we then hit a second organic layer. At this layer old rotten trees and other material was found. If a landslide is the case (along with the diorite sand at the "S" trench) it likely means that soil geochems in the lower areas of the Eliza Creek area are meaningless as they are derived from transported material (ie. landslides and/or fluvial).

Within Eliza 16 trench, west of the base line (LO/STNO) we are finding outcrop. As you go west the overburden thins from about 5 feet to almost nil. To the west of the trench advanced argillic/vein material can be seen in the cat tracks where the track has stripped the organics/moss away.

Once again, this vein is not properly exposed. By trenching a few feet deeper (5 feet?) the character and most likely the assay strength of the zone should improve. At about 3 feet of depth we started to see the main vein as a dirty yellow mud. Within another foot this yellow colour started to disappear to a brighter white colour. Another 6 inches exposed "white" advanced argillic mud with multiple broad bands of intense manganese straining. Bright blood-red pods also started to expose themselves in no clear pattern (hematite mud). It was at this early stage that we sampled the vein zone. It should be noted that in the western-most samples, the last 22 feet were then only at a six inch depth and their lower assay values seem to reflect this. The main vein is open to the west in width and the sediment contact with our diorite host appears to be about 100-150 feet to the west of the trench boundary.

The assays and geology are shown in figure 3 from the base line/line 0 post going west. The widths given are not true widths (true widths are probably about 90% of the given widths).

As in the "S" Trench, the gold values themselves are once again very low. In fact, many of the samples (3 feet each) contain almost no gold. The gold equivalent value is mainly produced by the silver and lead values (and zinc to a lesser extent).

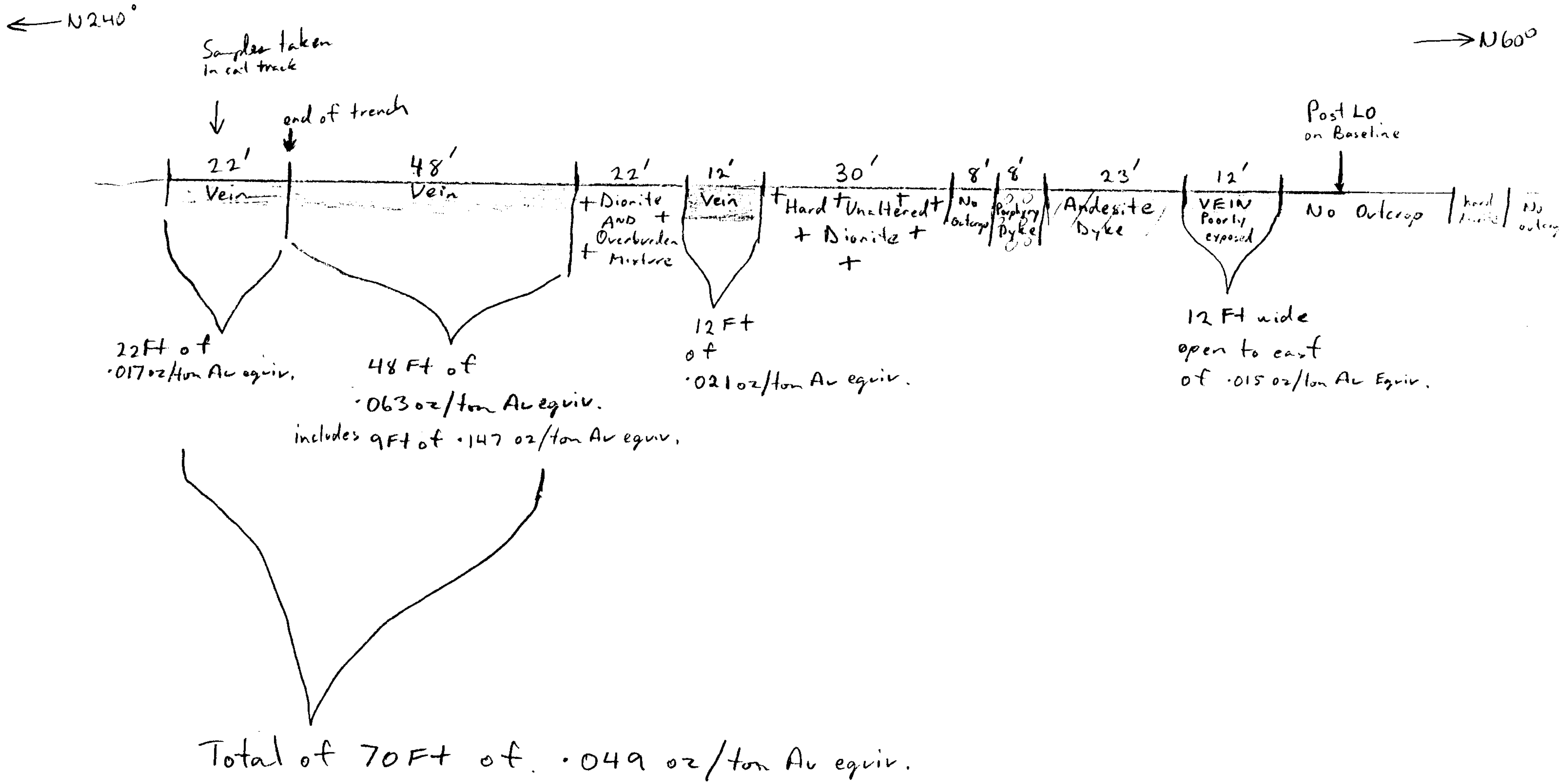
Eliza Creek - Magnetometer Map

A total field magnetometer survey was done on 100 feet spaced line on 25 feet station spaces. This work, the grid and some soil geochems were done for us by Aurum Geological Consultants Inc. of Whitehorse, Yukon. The magnetometer data maps are shown in the back folder. Skewed contour maps were also done on the fault directions. Work is still being done at present to locate faults from this data and to try to anticipate their relevance or disruption in the Eliza Creek Zone. All the major faults previously discussed can be seen in the Eliza Creek area as well as one new fault at N75° . On the aerial photograph the N75° faults can be detected and they "appear" to have a unique feature that at present we have no idea of its possible significance. This is

Scale: 1 inch = 25 ft.

Figure 3

ELIZA 16 TRENCH – WEST VEIN



True width ≅ 90% of width shown.

that this N75° fault is only found west of the centre (NW fault) of the epithermal. No N75° faults can be seen in the east.

The geology which is little known, is difficult to interpret from the magnetometer data. The diorite and the andesites appear to create a similar magnetometer reading. No discernable boundaries of the granite can be seen either. Better interpretation of this may be possible as trenching locates some contacts for us to relate the data to. The metasediments to the west can be easily seen as a strong magnetometer high.

We have a very high magnetometer reading area and an intermediate high magnetometer reading area. Outcrops of sediments have been found in the intermediate high reading area. At Line 100 South/750 West a very high reading is found. Nothing at this surface location indicates the reason for this. A pod of magnetite/pyrrhotite in the sediments is possible.

Indications of veins are shown in the area inferred as metasediments. Some of these will be look at in 1990.

Soil Geochems - Eliza Creek Zone

Soil geochem maps of Au, Ag, Pb, Zn, Pb/Zn as As are included in the back folder. Correlation of anomalies with the magnetometer map is quite good but are not precise in locating vein zones. The western area of the metasediments has had no geochem samples taken. This area is quite flat and has a fairly thin overburden cover so geochems may work quite well to access some of the magnetometer anomalies. Conversely, because of this, trenching would be relatively easy also and may be a better approach to get more direct and relevant data.

Discussion of Results and Recommendations

A basic problem on Aurchem's property is the abundance of veins. Erratic values and widths play havoc in trying to locate the main veins within the zones. The strength and width of the veins appear to be structurally controlled rather than lithology controlled although the lithology also plays a part. The paleo-depth is also a very strong factor but is also obscured by different phases and telescoping veins. Pods formed by vein swelling on strike or dip with elevated precious metal values appears to be the target for economic mineralization at higher paleodepths. These are very difficult to locate without extensive work, especially if they are not at surface.

Through the use of our model of gravity slides we have been attempting to locate the best paleodepth for us to concentrate our work on. Work in all the areas is warranted but is beyond the scope of our abilities. We must continue to do minor work in areas "deemed" less attractive by our model. We will continue to put the majority of our effort in our most promising areas.

By looking at a cross-sectional geologic model of an epithermal system (eg.

Panteleyev and Schroeter, 1985), the characteristics of the system in relation to our gravity sliding block theory continue to fit quite well. The inferred higher sections show regional silicification (siliceous cap?), low base metal values, and although low precious metal values high Au/Ag ratios. At more intermediate depths which I suggest is our Willow Creek zone we are plagued by veins splitting and merging, horsetails, relatively short strike lengths, highly erratic assay values and relatively narrow veins in abundance. We appear in the Eliza Creek zone to be at a greater depth where we should find a wider vein width of "main veins" with less branching, etc. Trenching has shown this to be true and assays show greater Ag/Au ratios and relatively increased base metal values which also fit the model. The magnetometer data suggests fairly good continuity in Eliza Creek of the two main veins across the property. The large vein widths and the indicated continuity suggests large tonnage potential and is the obvious target for our future work. A trenching program in Eliza Creek will be the main thrust of our 1990 work. This will be difficult for reasons stated earlier, especially on the easterly main vein which may be covered with deep overburden. With just the two main veins we have a suggested 6000 feet of strike length to explore which would require a major program in itself. A number of other targets also require trenching in the area. For this reason I firmly believe that our best initial approach in the area would be in the form of an Induced Polarization Survey. This may or may not show surface trenching target sites but it will likely show; 1) a better or stronger position of the continuity of the veins, 2) relative strength and continuity at depth showing tonnage potential, 3) locate drill targets to a much better degree than the magnetometer, 4) locate sulphide zones and possibly indicate a depth to the oxidized zone, 5) may show potential bulges in the vein (pods or lenses) along strike and dip, 6) may show geological knowledge with depth of lithologies and possibly faults.

Basically an I.P. survey will give us a much stronger geological knowledge base on which to target our exploration activities. The cost of the survey will likely be saved in the follow up exploration work being better guided. This assumes favourable results in the I.P. survey in Eliza Creek which at present looks very promising.

The grades in Eliza Creek have been disappointing from a visual expectation but even at the grades found, (which should improve with better trenching) the large widths with strike length produce large tonnages which greatly enhances the possibility of mining lower grade material. Topographically in Eliza Creek, the veins are also ideal for an open pit situation. For these reasons we are very bullish on work in our Eliza Creek area.

Results in the Willow Creek area were good but somewhat discouraging. Selective vein mining in small open pits shows some promise but the grades and widths combined with the small tonnages makes this somewhat impractical. What is needed is a strong main vein to justify the mining whereby selective mining on the Willow Creek veins could then be done to a shallow depth as added feed to the main ore.

The most promising vein in Willow Creek is the 11 South vein in both grade and tonnage potential. Unfortunately, the deep overburden in his area makes trenching unattractive. Therefore I would recommend that a small I.P. survey be done along the strike of this vein when the Eliza Creek survey is done. The high sulphide nature of the vein should give an excellent response. This would probably cost less than the digging of one trench in that area and would probably give us much better information on the vein as to strike, depth and possible strength.

A number of other locations in the Willow Creek zone require some follow up work based on results. Most require minimal work and will be worked accordingly as to their importance.

Some targets shown by the magnetometer and soil surveys in the Central Diorite Block will also be targeted for trenching. This work will also depend on our progress on main targets and their relative importance.

A definite main target for 1990 trenching will be continued work on the H5 trench (a 45 foot wide vein, open to width on the west grading .060 oz/ton Au equivalent). The large width carrying values make this a very attractive target. The existing trench is not deep enough and the western vein boundary has not been identified. Targets along strike may be warranted also.

On a different aspect, one important job that must be done in 1990 is to locate the Joanne claims to the south of us. Their location will enable us to locate our property boundary on the south side. It is very difficult to justify work in an area which may or may not be on our property.

Another possible work proposal would be initial work on the property north of the Eliza Creek grid (ie. Ricoo Lease). We basically have no idea of what potential this block of the property holds. Work on this area should be done by extending the Eliza Creek grid to the north. Line 11 North at Discovery Creek shows the continuation of our main veins to that point. According to our geological model, the Ricoo Block is a separate block from Eliza Creek. If this is true the vein zone should come to a sudden stop at this gravity slide/fault boundary. The boundary if it exists may not be at the creek but up to 500 feet north of Discovery Creek. Therefore, we may be able to increase our strike length of the vein zone. Whatever is true we should extend the baseline at least 800 feet and run magnetometer work on the grid to either verify the vein(s) end or extension.

A trenching program, as discussed would almost certainly need the combined effort of a D8 with ripper and backhoe. In designing the program in the Eliza Creek area, it would probably be of great advantage to us to build a road up through the Eliza Creek area to access the top of the hill. This would not require a great deal of work and would make fuel transport for the backhoe possible even if the transporter was the cat.

The surveyed grid should also be carefully maintained throughout the trenching program. Through trenching and the resulting mud flows, much of the grid could be easily lost. Trenching on the west main vein will also produce quantities of material to flow down the hill over the east vein zone, thus burying this zone even deeper than present. This poses a problem on the eastern vein. It is likely that only three trenches will be dug on the eastern vein because of this and the deeper overburden cover. These will likely be at 1) the "S" trench location, 2) the present Eliza 16 (east end) trench, 3) at the large magnetometer anomaly on Line 700 South. This last area is up higher out of the Eliza Creek valley so trenching might be much easier.

In summary, my 1990 exploration recommendations would be;

1) I.P. survey over the Eliza Creek Zone (also a minor survey possibly over the 11 South vein).

2) Establish a road into the Eliza Creek area to the top of the hill.

3) Major trenching in the Eliza Creek zone with detailed sampling and mapping programs.

4) Trenching, sampling and mapping of the H5 zone and possibly on-strike equivalents.

5) Establish our southern claims boundary by locating the Joanne claims.

6) Extension of the Eliza Creek grid to the north to find the extent of the main veins via the magnetometer.

7) Minor other trench locations and/or geochemical sampling on prospective areas.

Mark Langdon

Mark Langdon
Manager-Geological Projects

AURCHEM EXPLORATION LTD.

List of Expenditures

a) Personnel Expenditures

Mark Langdon	Manager-Geological Projects 511 Hayward Crescent Milton, Ontario Field work; supervision and implementation of trenching program, magnetometer and geochem survey, geological mapping and sampling, interpretation.	
	60 days at $200/day	$12,000.
Rick Mortimer	Geological Assistant General Delivery Carmacks, Yukon Field Work; assistant in all aspects of field program, general duties	
	48 days at $100/day	4,800.
John Schneider	President Aurchem Exploration	
	7 days at $250/day	1,750.
Secretarial Office Costs	$1,000	1,000.
A) Total Personnel Expenditures		$19,550

B) Rental Costs

1 Suburban 4 x 4 truck	$ 3,374.
1 MP-2 Magnetometer Rental	1,730.
Total Rental Costs;	$ 5,104.

C) Miscellaneous Field Expenses

Hotels, meals, supplies, fuel, etc.	$ 5,757.

D) Cost of Flights to Yukon

Cost of all flights	$ 2,976.

E) Trenching Costs

Colt Enterprises - Carmacks, Yukon	$101,547.

F) Assay Expenditures

Cost of all assays by Bondar Clegg and Co. Ltd., Whitehorse/Ottawa. Au, Ag, Cu, Zn, As, Pb, Sb 992 rocks, plus soil geochems	$ 30,033.

G) Geological Consultant Work

Aurum Geological Consultants Inc., Whitehorse	$ 17,459.
MPH Consulting Limited, Toronto	$ 1,015.
Total Geological Consultant Work	$ 18,474.

Summary of Expenditures

A)	Personnel Expenditures	$ 19,550.
B)	Rental Costs	5,104.
C)	Miscellaneous Field Expenses	5,757.
D)	Cost of Flights	2,976.
E)	Trenching Costs	101,547.
F)	Assay Costs	30,033.
G)	Geological Consultant Costs	18,474.
	GRAND TOTAL	$183,441.

For all expenditures, receipts are available on request.

Mark Langdon

Mark Langdon
Manager-Geological Projects

AURCHEM EXPLORATION LTD.

APPENDIX I

Trench Assays

The Au equiv. value was obtained by the formula:

$$\text{Au equiv.} = (\text{Ag} * .014) + \left(\frac{\text{Pb}}{392{,}156}\right) + \left(\frac{\text{Zn}}{202{,}020}\right) + \text{Au}$$

This formula is based on prices of:

Au = $366.00/oz
Ag = $5.20/oz
Pb = $0.42/pound
Zn = $0.82/pound

Sample widths are in feet but may not represent true widths.

Trench Assays

Wedge 8 Trench

Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	PB/ZN	AG/AU	AU/PB/ZN/AG AU EQUIV OPT	Width*Au OPT
SS-89-01	0.5	0.047	15.18	216	44800	1586	348	142200	3.17	322.98	0.844	0.422
SS-89-02	0.5	0.045	10.41	632	7900	5300	227	118300	14.97	231.33	0.532	0.266
SS-89-03	0.5	0.04	8.01	595	6840	3800	171	88300	12.91	200.25	0.411	0.206
SS-89-05	1	0.01	1.98	255	1132	1553	199	4150	3.67	198.00	0.054	0.054
SS-89-06	1	0.003	0.21	64	420	482	23	731	1.74	70.00	0.010	0.010
SS-89-39	2	0.002	0.02	8	85	51	15	83	0.98	10.00	0.003	0.006
SS-89-40	1	0.005	0.12	97	246	307	32	261	1.06	24.00	0.009	0.009
SS-89-41	3	0.002	0.84	16	80	19	24	125	1.56	420.00	0.014	0.043
SS-89-42	5	0.002	0.02	37	69	5	14	89	1.29	10.00	0.003	0.014
SS-89-43	2	0.002	0.06	61	171	32	28	172	1.01	30.00	0.004	0.008
SS-89-44	2	0.008	0.14	66	554	331	24	479	0.86	17.50	0.014	0.028
SS-89-45	1.5	0.007	0.69	150	1647	791	79	1288	0.78	98.57	0.028	0.042
SS-89-46	1.5	0.005	0.46	78	1331	855	61	1614	1.21	92.00	0.022	0.033
SS-89-47	3	0.003	0.08	11	262	61	24	59	0.23	26.67	0.006	0.017
SS-89-48	2.5	0.017	1.29	86	1100	1380	5	10960	9.96	75.88	0.068	0.171
SS-89-49	1	0.025	4.04	33	796	302	5	41800	52.51	161.60	0.192	0.192
SS-89-50	2	0.02	7.09	248	159	5	5	53400	335.85	354.50	0.256	0.512
SS-89-51	2	0.014	0.85	146	456	992	41	3680	8.07	60.71	0.038	0.075
SS-89-52	2	0.046	3.57	855	3700	1800	22	7240	1.96	77.61	0.133	0.266
SS-89-53	3	0.002	0.15	22	234	40	29	179	0.76	75.00	0.006	0.017
SS-89-54	1	0.005	0.27	54	1662	419	23	1023	0.62	54.00	0.020	0.020
SS-89-55	2	0.009	0.49	194	15200	1163	5	3000	0.20	54.44	0.099	0.198
SS-89-56	2	0.012	3.14	33	1220	5	5	28700	23.52	261.67	0.135	0.270
SS-89-57	2	0.033	2.82	304	3550	5	5	27100	7.63	85.45	0.159	0.318
SS-89-58	2	0.021	4.67	390	5150	5	5	49000	9.51	222.38	0.237	0.474
SS-89-59	0.5	0.026	4.05	1160	71400	605	5	41600	0.58	155.77	0.542	0.271
SS-89-60	0.5	0.035	5.25	532	33400	1190	129	47900	1.43	150.00	0.396	0.198
SS-89-61	3	0.003	0.09	56	2213	308	42	1119	0.51	30.00	0.018	0.054
SS-89-62	1	0.02	6.64	122	16600	259	5	59800	3.60	332.00	0.348	0.348
SS-89-63	2	0.007	0.13	39	257	338	31	154	0.60	18.57	0.010	0.021
SS-89-64	1	0.073	0.39	341	222	273	93	183	0.82	5.34	0.080	0.080
SS-89-65	4	0.031	0.5	244	1553	1219	66	840	0.54	16.13	0.048	0.191
SS-89-66	2	0.002	0.15	16	146	151	45	203	1.39	75.00	0.005	0.011
SS-89-67	0.5	0.073	0.46	204	414	3800	5	898	2.17	6.30	0.084	0.042
SS-89-68	1	0.102	0.5	80	731	767	46	261	0.36	4.90	0.113	0.113
SS-89-69	1	0.002	0.14	15	277	157	86	152	0.55	70.00	0.006	0.006
SS-89-70	2	0.002	0.14	10	278	127	28	84	0.30	70.00	0.006	0.011
SS-89-71	1	0.013	0.28	71	418	1123	36	495	1.18	21.54	0.020	0.020
SS-89-72	1	0.002	0.17	19	222	257	19	126	0.57	85.00	0.006	0.006
SS-89-73	2	0.003	0.08	34	398	1374	24	834	2.10	26.67	0.008	0.016
SS-89-74	3	0.011	0.07	5	54	302	5	29	0.54	6.36	0.012	0.037
SS-89-75	3	0.009	0.34	15	74	322	5	106	1.43	37.78	0.014	0.043
SS-89-76	7	0.009	0.29	75	213	446	44	388	1.82	32.22	0.015	0.106
SS-89-77	0.5	0.003	0.14	150	262	559	17	207	0.79	46.67	0.007	0.003
SS-89-78	3	0.002	0.13	34	235	125	14	135	0.57	65.00	0.005	0.016
SS-89-79	2	0.002	0.06	8	128	13	5	127	0.99	30.00	0.004	0.008
SS-89-80	2	0.003	0.1	10	117	269	47	120	1.03	33.33	0.005	0.011
SS-89-81	1	0.002	0.17	91	282	245	43	245	0.87	85.00	0.006	0.006
SS-89-82	1	0.008	0.32	230	447	785	82	248	0.55	40.00	0.015	0.015
SS-89-84	2	0.005	0.22	125	300	443	62	204	0.68	44.00	0.010	0.020
SS-89-086	1	0.002	0.09	10	115	42	22	97	0.84	45.00	0.004	0.004

										Ag/Au	Au equiv	
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	PB/ZN ERR	ERR ERR	ERR ERR	ERR ERR
SS-89-087	3.5	0.002	0.1	17	107	23	26	101	0.94	50.00	0.004	0.015
SS-89-088	1	0.002	0.11	13	476	94	30	159	0.33	55.00	0.006	0.006
SS-89-089	1	0.002	0.11	75	1420	696	5	166	0.12	55.00	0.011	0.011
SS-89-090	1	0.023	1.41	454	399	1010	15	6220	15.59	61.30	0.061	0.061
SS-89-091	1	0.014	0.97	121	673	461	104	1695	2.52	69.29	0.035	0.035
SS-89-092	1	0.002	0.12	246	2611	1446	8	154	0.06	60.00	0.017	0.017
SS-89-093	1.5	0.01	0.59	137	222	439	27	2048	9.23	59.00	0.025	0.037
SS-89-094	2	0.002	0.1	240	964	727	38	416	0.43	50.00	0.009	0.018
SS-89-095	1	0.002	0.24	663	939	829	5	772	0.82	120.00	0.012	0.012
SS-89-096	1	0.002	0.02	351	4115	1828	5	361	0.09	10.00	0.024	0.024
SS-89-097	1	0.018	0.84	71	210	526	57	2220	10.57	46.67	0.036	0.036
SS-89-098	1	0.008	2.17	308	399	1910	393	2870	7.19	271.25	0.048	0.048
SS-89-099	2	0.003	0.42	174	405	475	68	762	1.88	140.00	0.013	0.026
SS-89-100	2	0.002	0.02	399	2514	724	19	271	0.11	10.00	0.015	0.031
SS-89-101	1	0.021	0.96	320	631	1030	5	8620	13.66	45.71	0.060	0.060
SS-89-102	1.5	0.012	0.53	159	857	1587	166	1707	1.99	44.17	0.028	0.042
SS-89-103	1.5	0.002	0.02	269	944	826	34	321	0.34	10.00	0.008	0.012
SS-89-104	1	0.013	0.8	543	936	746	129	2890	3.09	61.54	0.036	0.036
SS-89-105	1	0.018	2.41	299	536	2000	366	7620	14.22	133.89	0.074	0.074
SS-89-106	1	0.005	0.78	170	413	386	87	1034	2.50	156.00	0.021	0.021
SS-89-107	0.7	0.059	0.28	57	967	2000	183	811	0.84	4.75	0.070	0.049
SS-89-108	1	0.002	0.02	36	379	103	15	273	0.72	10.00	0.005	0.005
SS-89-109	1	0.011	0.46	102	359	1321	83	1436	4.00	41.82	0.023	0.023

									Pb/Zn	Ag/Au	Au equiv.	
2 South Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	PB	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
SS-89-04	0.5	0.355	14.14	6080	16610	107400	1400	110200	6.63	39.83	0.916	0.458
S89-237	1	0.002	0.05	21	553	446	17	77	0.14	25.00	0.006	0.006
S89-238	1	0.012	0.74	102	1387	2500	55	2760	1.99	61.67	0.036	0.036
S89-239	1	0.012	2.93	118	806	704	94	40400	50.12	244.17	0.160	0.160
S89-240	2.5	0.022	5.5	182	1322	2900	275	83400	63.09	250.00	0.318	0.796
S89-241	1	0.017	18.6	1070	2268	717	452	150400	66.31	1094.12	0.672	0.672
S89-242	1	0.025	1.66	80	2652	4600	280	12960	4.89	66.40	0.094	0.094
S89-243	1	0.004	0.16	14	545	803	62	248	0.46	40.00	0.010	0.010
S89-244	3	0.002	0.09	6	330	478	40	242	0.73	45.00	0.006	0.017
S89-245	2	0.005	0.23	62	1356	785	43	1656	1.22	46.00	0.019	0.038
S89-246	10	0.002	0.02	7	158	106	11	52	0.33	10.00	0.003	0.032
S89-247	10	0.004	0.02	6	109	255	24	57	0.52	5.00	0.005	0.050
S89-248	3	0.004	0.23	17	1208	567	191	2070	1.71	57.50	0.018	0.055
S89-249	3	0.002	0.02	12	413	367	24	540	1.31	10.00	0.006	0.017
S89-250	3	0.002	0.11	17	1141	771	96	723	0.63	55.00	0.011	0.033
S89-251	3	0.006	0.52	26	4340	2600	369	3890	0.90	86.67	0.045	0.134
S89-252	1	0.004	5.12	28	15480	1419	1620	20100	1.30	1280.00	0.204	0.204
S89-253	2	0.002	0.13	15	85	247	13	567	6.67	65.00	0.006	0.011
S89-254	2	0.002	0.06	13	113	295	10	172	1.52	30.00	0.004	0.008
S89-255	2	0.002	0.02	209	535	450	12	227	0.42	10.00	0.006	0.011
S89-256	2	0.002	0.04	114	152	329	8	227	1.49	20.00	0.004	0.008
S89-257	1	0.002	0.04	36	179	648	20	543	3.03	20.00	0.005	0.005
S89-258	1	0.008	0.18	42	75	355	58	609	8.12	22.50	0.012	0.012
S89-259	1	0.006	0.05	34	113	356	26	332	2.94	8.33	0.008	0.008
S89-260	1	0.009	0.05	29	78	224	46	708	9.08	5.56	0.012	0.012
S89-261	1	0.171	2.3	38	131	3800	50	1576	12.03	13.45	0.208	0.208
S89-262	1	0.451	21.68	181	458	12500	413	181500	396.29	48.07	1.220	1.220
S89-263	1	0.333	1.71	273	2355	51500	409	14290	6.07	5.14	0.405	0.405
S89-264	1	0.626	12.79	2370	6930	61000	2290	78900	11.39	20.43	1.041	1.041
S89-327	1	0.006	0.02	137	2685	1371	24	1236	0.46	3.33	0.023	0.023
S89-328	1	0.005	0.02	114	2904	1144	18	718	0.25	4.00	0.021	0.021
S89-329	2	0.015	0.51	83	809	1485	45	3950	4.88	34.00	0.036	0.072
S89-330	1	0.012	0.54	27	331	701	33	4210	12.72	45.00	0.032	0.032
S89-331	1	0.052	1.07	57	320	1121	40	10380	32.44	20.58	0.095	0.095
S89-332	2	0.012	0.35	87	1121	881	41	2680	2.39	29.17	0.029	0.059
S89-333	1.3	0.009	0.02	49	1571	540	-5	197	0.13	2.22	0.018	0.023
S89-334	1.3	0.005	0.03	15	853	420	8	171	0.20	6.00	0.010	0.013
S89-335	1.3	0.024	0.3	15	542	575	9	1713	3.16	12.50	0.035	0.046
S89-336	1	0.212	1.42	45	550	2100	46	10900	19.82	6.70	0.262	0.262
S89-337	1	0.526	3.34	113	632	4100	140	27000	42.72	6.35	0.645	0.645
S89-338	1	0.043	1.14	39	428	1696	33	9010	21.05	26.51	0.084	0.084
S89-339	1	0.035	1.33	39	643	1414	34	9080	14.12	38.00	0.080	0.080
S89-340	1	0.023	0.78	41	818	1444	29	6500	7.95	33.91	0.055	0.055
S89-341	1	0.005	0.32	105	1298	1790	23	2670	2.06	64.00	0.023	0.023
S89-342	1	0.006	0.3	65	1488	942	28	1786	1.20	50.00	0.022	0.022
S89-343	2	0.002	0.16	59	2940	644	33	206	0.07	80.00	0.019	0.039
S89-344	1	0.002	0.15	49	3890	769	34	159	0.04	75.00	0.024	0.024
S89-345	1	0.002	0.09	78	9660	793	29	285	0.03	45.00	0.052	0.052
S89-346	1	0.006	0.1	38	1547	1298	24	219	0.14	16.67	0.016	0.016
S89-347	1	0.009	0.41	17	888	674	21	3100	3.49	45.56	0.027	0.027
S89-348	1	0.097	3.65	52	561	4800	138	29400	52.41	37.63	0.226	0.226
S89-349	1	0.075	5.35	55	412	5200	97	45000	109.22	71.33	0.267	0.267
S89-350	0.5	0.15	31.13	149	557	12000	587	250400	449.55	207.53	1.227	0.614

Pb/Zn Ag/Au Au equiv.

Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	PB PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-351	1	0.066	3.8	30	270	3600	52	32100	118.89	57.58	0.202	0.202
S89-352	1	0.053	3.68	32	229	3700	59	22600	98.69	69.43	0.163	0.163
S89-353	1	0.008	0.66	21	416	918	8	4510	10.84	82.50	0.031	0.031
S89-354	1	0.008	0.82	56	1253	1227	25	5210	4.16	102.50	0.039	0.039
S89-355	1	0.04	3.25	49	329	3300	54	25000	75.99	81.25	0.151	0.151
S89-356	1	0.018	3.11	61	282	1824	38	31700	112.41	172.78	0.144	0.144
S89-357	1	0.004	0.79	54	534	1256	17	6240	11.69	197.50	0.034	0.034
S89-358	1	0.003	0.39	96	2080	1014	18	1201	0.58	130.00	0.022	0.022
S89-531	2	0.005	0.02	36	1108	929	30	373	0.34	4.00	0.012	0.023
S89-532	1	0.025	0.15	10	917	3300	69	221	0.24	6.00	0.032	0.032
S89-533	1	0.018	1.79	176	1487	4300	122	16490	11.09	99.44	0.092	0.092
S89-534	1	0.006	0.35	110	631	1912	70	757	1.20	58.33	0.016	0.016
S89-535	1	0.126	2.54	220	1670	21500	2	22100	13.23	20.16	0.226	0.226
S89-536	1	0.152	2.34	505	2897	31100	588	17680	6.10	15.39	0.244	0.244
S89-537	3	0.002	0.04	58	255	354	33	256	1.00	20.00	0.004	0.013
S89-538	1	0.121	1.09	220	580	2500	173	9720	16.76	9.01	0.164	0.164
S89-539	1	0.094	6.29	490	1389	23300	476	64000	46.08	66.91	0.352	0.352
S89-540	2	0.042	0.99	74	291	7900	111	1393	4.79	23.57	0.061	0.122
S89-541	1	0.029	1.15	40	103	2500	38	937	9.10	39.66	0.048	0.048
S89-542	1.5	0.045	1.1	510	4372	9100	128	11730	2.68	24.44	0.112	0.168
S89-543	3	0.004	0.18	24	196	1939	37	660	3.37	45.00	0.009	0.028
S89-544	1.5	0.075	0.79	216	9421	3400	75	7680	0.82	10.53	0.152	0.228
S89-545	2.5	0.004	0.09	41	631	410	32	736	1.17	22.50	0.010	0.026
S89-546	2	0.052	0.16	52	493	1191	51	445	0.90	3.08	0.058	0.116
S89-547	2	0.02	0.16	42	308	580	39	323	1.05	8.00	0.025	0.049
S89-548	2	0.002	0.14	6	59	29	13	49	0.83	70.00	0.004	0.009
S89-549	2	0.115	0.06	13	96	167	39	58	0.60	0.52	0.116	0.233
S89-550	1	0.014	0.02	8	123	66	36	76	0.62	1.43	0.015	0.015
S89-551	2	0.026	0.59	132	1577	5500	71	4420	2.80	22.69	0.053	0.107
S89-552	1	0.096	0.36	100	726	6700	66	1990	2.74	3.75	0.110	0.110
S89-553	2	0.003	0.53	49	1130	1964	25	2623	2.32	176.67	0.023	0.045
S89-554	3	0.002	0.2	64	931	1589	31	1777	1.91	100.00	0.014	0.042
S89-555	3	0.002	0.02	37	866	929	23	245	0.28	10.00	0.007	0.022
S89-556	3	0.002	0.08	38	710	334	34	177	0.25	40.00	0.007	0.021
S89-557	5	0.002	0.19	35	854	624	34	354	0.41	95.00	0.010	0.049
S89-558	1	0.037	0.36	45	1137	5100	34	962	0.85	9.73	0.050	0.050
S89-559	2	0.064	1.69	95	1756	13800	84	3760	2.14	26.41	0.106	0.212
S89-560	2	0.051	0.27	51	486	2400	41	1010	2.08	5.29	0.060	0.120
S89-561	1.5	0.073	1.43	66	779	3600	62	3910	5.02	19.59	0.107	0.160

									Pb/Zn	Ag/Au	Au equiv.	
11 South Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
SS-89-07	1	0.048	0.39	68	89	3600	102	1164	13.08	8.13	0.057	0.057
SS-89-135	3	0.014	0.12	66	861	999	5	171	0.20	8.57	0.020	0.061
SS-89-136	1	0.12	1.17	67	426	3400	69	3610	8.47	9.75	0.148	0.148
SS-89-137	4	0.002	0.02	213	1034	221	33	226	0.22	10.00	0.008	0.032
SS-89-138	4	0.002	0.05	247	784	221	38	191	0.24	25.00	0.007	0.028
SS-89-139	3	0.002	0.14	282	633	446	79	734	1.16	70.00	0.009	0.027
SS-89-140	2	0.004	0.06	221	491	1115	113	1251	2.55	15.00	0.010	0.021
SS-89-141	1	0.01	0.28	71	233	915	42	1466	6.29	28.00	0.019	0.019
SS-89-142	1	0.003	0.24	27	101	377	26	372	3.68	80.00	0.008	0.008
SS-89-143	1	0.004	0.13	101	161	1422	30	1197	7.43	32.50	0.010	0.010
SS-89-144	1	0.007	0.38	32	84	952	64	803	9.56	54.29	0.015	0.015
SS-89-145	1	0.006	0.3	104	145	1011	7	1111	7.66	50.00	0.014	0.014
SS-89-146	1	0.042	0.18	190	282	2700	111	2610	9.26	4.29	0.053	0.053
SS-89-147	1	0.011	0.33	140	185	1263	22	1515	8.19	30.00	0.020	0.020
SS-89-148	1	0.003	0.28	31	78	762	45	597	7.65	93.33	0.009	0.009
SS-89-149	1	0.012	0.32	142	209	1834	52	1515	7.25	26.67	0.021	0.021
SS-89-150	1	0.047	0.22	159	242	2000	56	1596	6.60	4.68	0.055	0.055
SS-89-151	1	0.012	0.24	169	200	1994	46	1475	7.38	20.00	0.020	0.020
SS-89-152	1	0.008	0.31	98	102	1264	62	878	8.61	38.75	0.015	0.015
SS-89-153	1	0.014	0.35	173	252	2700	104	1748	6.94	25.00	0.025	0.025
SS-89-154	1	0.008	0.41	30	67	395	35	658	9.82	51.25	0.016	0.016
SS-89-155	1	0.044	0.04	123	109	2000	5	1550	14.22	0.91	0.049	0.049
SS-89-156	1	0.017	0.75	64	98	1059	91	1234	12.59	44.12	0.031	0.031
SS-89-157	1	0.046	0.26	160	127	4900	5	1840	14.49	5.65	0.055	0.055
SS-89-158	1	0.035	0.6	69	105	3000	100	1186	11.30	17.14	0.047	0.047
SS-89-159	1	0.064	0.92	69	1	6300	5	1310	1310.00	14.38	0.080	0.080
SS-89-160	1	0.055	15.15	2470	654	6200	3800	8890	13.59	275.45	0.293	0.293
SS-89-161	1	0.056	0.9	113	40	4700	5	1840	46.00	16.07	0.073	0.073
SS-89-162	1	0.038	23.18	7890	1270	10500	6350	6550	5.16	610.00	0.386	0.386
SS-89-163	1	0.066	5.8	393	482	4700	1260	4330	8.98	87.88	0.161	0.161
SS-89-164	1	0.094	5.94	472	520	3000	1120	3680	7.08	63.19	0.189	0.189
SS-89-165	1	0.088	21.7	5010	988	8700	7070	10570	10.70	246.59	0.424	0.424
SS-89-166	1	0.004	0.61	82	253	495	54	466	1.84	152.50	0.015	0.015
SS-89-167	1	0.065	13.79	893	1340	23300	1610	9450	7.05	212.15	0.289	0.289
SS-89-168	1	0.005	0.48	164	480	839	82	904	1.88	96.00	0.016	0.016
SS-89-169	1	0.007	0.15	57	636	738	38	372	0.58	21.43	0.013	0.013
SS-89-170	1	0.002	0.31	122	596	380	51	1667	2.80	155.00	0.014	0.014
SS-89-171	1	0.006	0.33	48	579	615	55	374	0.65	55.00	0.014	0.014
SS-89-172	1	0.002	0.2	107	712	339	41	993	1.39	100.00	0.011	0.011
SS-89-173	1	0.003	0.09	79	517	423	34	224	0.43	30.00	0.007	0.007
SS-89-174	2	0.002	0.02	29	1004	48	12	201	0.20	10.00	0.008	0.016

									Pb/Zn	Ag/Au	Au equiv.	
Road Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
SS-89-08	1.5	0.002	0.04	6	362	480	12	217	0.60	20.00	0.005	0.007
SS-89-09	1.5	0.002	0.02	7	253	352	7	65	0.26	10.00	0.004	0.006
SS-89-10	1.5	0.002	0.02	18	431	420	33	157	0.36	10.00	0.005	0.007
SS-89-11	1.5	0.002	0.07	22	805	511	11	136	0.17	35.00	0.007	0.011
SS-89-12	1	0.003	0.02	372	4124	996	141	181	0.04	6.67	0.024	0.024
SS-89-13	1.5	0.006	0.18	242	1098	2500	54	646	0.59	30.00	0.016	0.023
SS-89-14	1.5	0.006	0.09	156	1002	1945	16	312	0.31	15.00	0.013	0.020
SS-89-15	3	0.058	3.1	244	472	3200	124	25700	54.45	53.45	0.169	0.508
SS-89-16	3	0.05	3.8	282	564	3400	152	34900	61.88	76.00	0.195	0.585
SS-89-17	3	0.041	7.58	401	558	3500	704	32900	58.96	184.88	0.234	0.701
SS-89-18	1.5	0.005	0.12	49	2078	909	331	722	0.35	24.00	0.019	0.028
SS-89-19	1.5	0.003	0.1	27	933	740	197	495	0.53	33.33	0.010	0.015
SS-89-20	1	0.004	0.07	10	774	760	170	281	0.36	17.50	0.010	0.010
SS-89-21	1	0.007	0.16	13	927	1164	137	762	0.82	22.86	0.016	0.016
SS-89-22	3	0.002	0.02	7	302	232	94	164	0.54	10.00	0.004	0.013
SS-89-23	3	0.002	0.03	5	529	521	51	172	0.33	15.00	0.005	0.016
SS-89-34	2	0.009	0.19	16	741	405	22	221	0.30	21.11	0.016	0.032
SS-89-35	1	0.003	0.1	13	203	211	24	90	0.44	33.33	0.006	0.006
SS-89-36	6	0.002	0.02	30	342	154	23	325	0.95	10.00	0.005	0.029
SS-89-37	4	0.005	0.14	92	287	321	60	278	0.97	28.00	0.009	0.036
SS-89-38	4	0.005	0.15	108	837	720	102	216	0.26	30.00	0.012	0.047

									Pb/Zn	Ag/Au	Au equiv.	
3 South Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
SS-89-110	5	0.002	0.02	7	231	19	21	100	0.43	10.00	0.004	0.018
SS-89-111	5	0.002	0.02	89	390	10	39	105	0.27	10.00	0.004	0.022
SS-89-112	5	0.002	0.08	40	237	122	25	113	0.48	40.00	0.005	0.023
SS-89-113	5	0.002	0.05	22	419	256	19	376	0.90	25.00	0.006	0.029
SS-89-114	5	0.002	0.11	110	1566	508	48	326	0.21	55.00	0.012	0.061
SS-89-115	5	0.002	0.02	7	1084	15	11	71	0.07	10.00	0.008	0.039
SS-89-116	3	0.01	0.41	318	1349	1855	64	632	0.47	41.00	0.024	0.072
SS-89-117	3	0.004	0.02	53	550	166	25	517	0.94	5.00	0.008	0.025
SS-89-118	2	0.109	0.31	64	334	3500	5	874	2.62	2.84	0.117	0.234
SS-89-119	1	0.002	0.05	75	888	500	64	698	0.79	25.00	0.009	0.009
SS-89-120	1	0.008	0.11	61	336	1671	37	779	2.32	13.75	0.013	0.013
SS-89-121	1	0.012	0.07	55	742	1405	15	437	0.59	5.83	0.018	0.018
SS-89-122	1	0.016	0.3	120	764	2000	91	818	1.07	18.75	0.026	0.026
SS-89-123	1	0.119	0.39	322	4230	8600	64	2040	0.48	3.28	0.151	0.151
SS-89-124	1	0.009	0.33	188	558	1930	89	1265	2.27	36.67	0.020	0.020
SS-89-125	1	0.014	0.21	22	136	511	60	294	2.16	15.00	0.018	0.018
SS-89-126	0.5	0.01	0.2	59	641	572	11	432	0.67	20.00	0.017	0.009
SS-89-127	3	0.014	0.12	69	911	2900	31	736	0.81	8.57	0.022	0.066
SS-89-128	2	0.002	0.02	6	1002	90	25	76	0.08	10.00	0.007	0.015
SS-89-129	2	0.002	0.02	8	906	30	57	68	0.08	10.00	0.007	0.014
SS-89-130	2	0.002	0.1	7	238	124	5	160	0.67	50.00	0.005	0.010
SS-89-131	2	0.004	0.17	55	826	362	16	687	0.83	42.50	0.012	0.024
SS-89-132	1.5	0.002	0.05	12	144	117	7	168	1.17	25.00	0.004	0.006
SS-89-133	4	0.011	0.16	56	227	5800	5	205	0.90	14.55	0.015	0.060
SS-89-134	4	0.002	0.09	30	223	277	5	97	0.43	45.00	0.005	0.018
S89-227	1	0.002	0.04	30	523	584	50	204	0.39	20.00	0.006	0.006
S89-228	1	0.038	0.61	165	9260	26500	2130	8910	0.96	16.05	0.115	0.115
S89-229	1	0.029	1.48	564	15500	25200	1250	19300	1.25	51.03	0.176	0.176
S89-230	1	0.048	1.3	370	24000	30000	1910	17500	0.73	27.08	0.230	0.230
S89-231	1	0.004	0.09	316	1101	2300	171	230	0.21	22.50	0.011	0.011
S89-232	1	0.002	0.02	215	320	285	77	159	0.50	10.00	0.004	0.004
S89-233	1	0.003	0.07	368	370	1730	97	152	0.41	23.33	0.006	0.006
S89-234	1	0.002	0.02	83	279	566	34	146	0.52	10.00	0.004	0.004
S89-235	10	0.003	0.02	515	303	284	62	80	0.26	6.67	0.005	0.050
S89-236	1	0.029	0.12	285	663	3100	45	443	0.67	4.14	0.035	0.035

Pb/Zn Ag/Au Au equiv.

8 South Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-175	1	0.051	0.31	26	745	26600	31	1842	2.47	6.08	0.064	0.064
S89-176	1	0.198	0.47	18	1717	80100	116	1642	0.96	2.37	0.217	0.217
S89-177	1	0.131	0.27	15	1678	58900	90	1242	0.74	2.06	0.146	0.146
S89-178	2	0.003	0.26	127	976	1195	36	805	0.82	86.67	0.014	0.027
S89-179	3	0.003	0.18	49	1980	3100	28	1093	0.55	60.00	0.018	0.054
S89-180	3	0.002	0.05	2	221	393	14	61	0.28	25.00	0.004	0.012
S89-181	1.5	0.002	0.08	57	1192	644	79	560	0.47	40.00	0.010	0.016
S89-182	3.5	0.002	0.04	54	390	140	35	57	0.15	20.00	0.005	0.016
S89-183	1	0.208	0.29	29	1185	211	41	551	0.46	1.39	0.219	0.219
S89-184	0.5	0.181	0.55	16	2933	76700	116	1917	0.65	3.04	0.208	0.104
S89-185	1	0.071	1.27	65	7580	5000	76	9000	1.19	17.89	0.149	0.149
S89-186	1	0.002	0.05	35	1662	315	28	274	0.16	25.00	0.012	0.012
S89-187	1	0.002	0.37	131	2379	1205	76	1391	0.58	185.00	0.023	0.023
S89-188	6.5	0.002	0.02	20	1974	509	32	143	0.07	10.00	0.012	0.081
S89-189	2.5	0.103	0.6	81	3029	16100	117	2310	0.76	5.83	0.132	0.331
S89-190	5.5	0.002	0.03	13	1508	332	15	106	0.07	15.00	0.010	0.056
S89-191	3	0.016	0.38	111	2474	10100	102	2220	0.90	23.75	0.039	0.118
S89-192		0.01	0.13	86	1525	4200	96	1321	0.87	13.00	0.023	0.000
S89-193		0.027	0.41	132	2002	14200	232	2760	1.38	15.19	0.050	0.000
S89-194	2	0.002	0.02	16	249	252	51	162	0.65	10.00	0.004	0.008
S89-195	5	0.002	0.04	18	105	152	40	93	0.89	20.00	0.003	0.017
S89-196	1	0.003	0.15	81	1756	4000	33	1946	1.11	50.00	0.019	0.019
S89-197	2	0.161	0.57	38	1545	71300	96	4010	2.60	3.54	0.187	0.374
S89-198	3	0.003	0.08	26	687	363	45	87	0.13	26.67	0.008	0.023
S89-199	1	0.028	1.79	81	2142	3600	63	14630	6.83	63.93	0.101	0.101
S89-200	1	0.005	0.24	32	1298	1128	41	1875	1.44	48.00	0.020	0.020
S89-201	1	0.006	0.12	53	1292	2100	60	824	0.64	20.00	0.016	0.016
S89-202	1	0.002	0.04	23	941	573	39	227	0.24	20.00	0.008	0.008
S89-203	1	0.002	0.15	15	289	409	59	98	0.34	75.00	0.006	0.006
S89-204	1	0.002	0.03	24	151	819	87	103	0.68	15.00	0.003	0.003
S89-205	2	0.006	0.28	48	1353	2100	85	840	0.62	46.67	0.019	0.038
S89-206	2	0.009	0.11	38	2368	3400	65	449	0.19	12.22	0.023	0.047
S89-207	2	0.013	0.14	41	2741	4400	103	727	0.27	10.77	0.030	0.061
S89-208	2	0.012	0.16	18	1277	5800	184	1191	0.93	13.33	0.024	0.047
S89-209	1	0.002	0.02	11	258	1401	52	98	0.38	10.00	0.004	0.004
S89-210	2	0.002	0.07	12	374	204	52	90	0.24	35.00	0.005	0.010
S89-211	2	0.002	0.03	12	472	131	35	95	0.20	15.00	0.005	0.010
S89-212	3	0.018	0.61	119	5730	9100	149	5730	1.00	33.89	0.070	0.209
S89-213	7	0.002	0.07	20	264	298	21	194	0.73	35.00	0.005	0.033
S89-214	8	0.002	0.02	15	269	117	36	89	0.33	10.00	0.004	0.031
S89-215	2	0.002	0.02	11	131	830	38	69	0.53	10.00	0.003	0.006
S89-216	7	0.002	0.02	13	109	40	24	62	0.57	10.00	0.003	0.021
S89-217	8	0.002	0.02	16	297	524	48	93	0.31	10.00	0.004	0.032
S89-218	2	0.003	0.03	18	773	1343	78	326	0.42	10.00	0.008	0.016
S89-219	6	0.002	0.07	20	149	713	58	83	0.56	35.00	0.004	0.024
S89-220	2	0.002	0.02	6	100	1786	114	85	0.85	10.00	0.003	0.006
S89-221	1	0.002	0.02	13	84	229	10	61	0.73	10.00	0.003	0.003
S89-222	1	0.002	0.02	5	168	720	130	168	1.00	10.00	0.004	0.004
S89-223	1	0.349	0.73	42	2210	120000	197	6620	3.00	2.09	0.387	0.387
S89-224	1	0.003	0.16	8	224	1824	156	228	1.02	53.33	0.007	0.007
S89-225	8	0.002	0.05	13	130	184	21	60	0.46	25.00	0.003	0.028
S89-226	1	0.002	0.11	6	130	1844	123	100	0.77	55.00	0.004	0.004

1%/Zn 1%/Au Au equiv.

Drain 2 South Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-265	1	0.021	0.44	52	142	1512	54	3080	21.69	20.95	0.036	0.036
S89-266	1	0.009	0.13	24	63	355	25	649	10.30	14.44	0.013	0.013
S89-267	1	0.004	0.12	52	476	648	28	400	0.84	30.00	0.009	0.009
S89-268	1	0.003	0.02	131	987	1103	19	360	0.36	6.67	0.009	0.009
S89-269	1	0.003	0.2	174	844	395	45	1033	1.22	66.67	0.013	0.013
S89-270	2	0.002	0.02	33	324	241	16	295	0.91	10.00	0.005	0.009
S89-271	2	0.002	0.04	24	136	249	13	228	1.68	20.00	0.004	0.008
S89-272	3	0.002	0.02	20	122	274	6	78	0.64	10.00	0.003	0.009
S89-279	2	0.003	0.39	268	413	825	46	2410	5.84	130.00	0.017	0.033
S89-280	2	0.002	0.17	111	522	425	18	865	1.66	85.00	0.009	0.018
S89-281	2	0.002	0.21	325	1324	685	28	1566	1.18	105.00	0.015	0.031
S89-282	2	0.003	0.15	306	1332	753	51	1270	0.95	50.00	0.015	0.030
S89-283	1	0.002	0.04	461	1288	548	21	268	0.21	20.00	0.010	0.010
S89-284	1	0.002	0.04	92	911	1086	12	358	0.39	20.00	0.008	0.008
S89-285	1	0.002	0.05	92	653	945	16	341	0.52	25.00	0.007	0.007
S89-286	1	0.008	0.64	37	98	801	25	3980	40.61	80.00	0.028	0.028
S89-287	1	0.015	0.61	23	35	909	20	4430	126.57	40.67	0.035	0.035
S89-288	1	0.005	0.29	26	160	487	21	1585	9.91	58.00	0.014	0.014
S89-289	1	0.005	0.24	30	281	618	20	1611	5.73	48.00	0.014	0.014
S89-290	1	0.004	0.22	82	392	986	32	1205	3.07	55.00	0.012	0.012
S89-291	1	0.004	0.29	90	626	1330	23	784	1.25	72.50	0.013	0.013
S89-292	1	0.005	0.34	101	561	1377	58	1812	3.23	68.00	0.017	0.017
S89-293	1	0.004	0.2	53	270	657	21	852	3.16	50.00	0.010	0.010
S89-294	1	0.002	0.02	152	328	1513	5	361	1.10	10.00	0.005	0.005
S89-295	1	0.002	0.02	150	419	415	5	93	0.22	10.00	0.005	0.005
S89-296	2	0.002	0.02	118	456	132	6	83	0.18	10.00	0.005	0.009
S89-297	2	0.002	0.02	27	221	96	5	84	0.38	10.00	0.004	0.007
S89-298	3	0.002	0.02	7	86	117	5	68	0.79	10.00	0.003	0.009
S89-299	3	0.002	0.02	6	71	143	8	84	1.18	10.00	0.003	0.009
S89-300	2	0.002	0.02	171	924	576	15	515	0.56	10.00	0.008	0.016
S89-301	2	0.002	0.09	315	1068	857	28	1084	1.01	45.00	0.011	0.023
S89-302	2	0.002	0.02	262	1219	295	18	87	0.07	10.00	0.009	0.017
S89-303	1	0.006	0.02	112	162	505	36	410	2.53	3.33	0.008	0.008
S89-304	1	0.002	0.08	130	409	909	19	335	0.82	40.00	0.006	0.006
S89-305	1	0.002	0.11	131	475	1369	15	166	0.35	55.00	0.006	0.006
S89-306	1	0.002	0.03	154	535	1232	9	127	0.24	15.00	0.005	0.005
S89-307	2	0.002	0.08	216	337	384	12	412	1.22	40.00	0.006	0.012
S89-308	2	0.002	0.02	92	463	219	5	74	0.16	10.00	0.005	0.010
S89-309	3	0.002	0.02	18	226	174	5	95	0.42	10.00	0.004	0.011
S89-310	2	0.002	0.02	28	323	376	8	165	0.51	10.00	0.004	0.009
S89-311	2	0.002	0.02	27	466	395	5	111	0.24	10.00	0.005	0.010
S89-312	2	0.002	0.08	130	918	599	5	278	0.30	40.00	0.008	0.017
S89-313	2	0.002	0.45	310	843	913	64	1809	2.15	225.00	0.017	0.034
S89-314	2	0.002	0.02	195	922	762	5	283	0.31	10.00	0.008	0.015
S89-315	1	0.012	0.26	74	612	1510	5	676	1.10	21.67	0.020	0.020
S89-316	1	0.004	0.35	53	186	540	22	1851	9.95	87.50	0.015	0.015
S89-317	1	0.008	0.85	25	68	416	58	1972	29.00	106.25	0.025	0.025
S89-318	1	0.006	0.94	37	102	500	59	2910	28.53	156.67	0.027	0.027
S89-319	1	0.004	0.5	47	300	500	41	2201	7.34	125.00	0.018	0.018
S89-320	1	0.002	0.23	101	366	675	21	1161	3.17	115.00	0.010	0.010
S89-321	1	0.003	0.24	46	178	380	23	1325	7.44	80.00	0.011	0.011
S89-322	1	0.004	0.33	96	246	701	42	1372	5.58	82.50	0.013	0.013
S89-323	1	0.006	0.3	103	299	805	40	1089	3.64	50.00	0.014	0.014
S89-324	1	0.004	0.02	126	514	573	13	439	0.85	5.00	0.008	0.008
S89-325	2	0.002	0.02	76	575	295	11	110	0.19	10.00	0.005	0.011
S89-326	2	0.002	0.02	11	238	162	9	82	0.34	10.00	0.004	0.007

									Pb/Zn	Ag/Au	Au equiv.	
D4 Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-273	0.5	0.155	2.07	628	214	57000	87	1542	7.21	13.35	0.189	0.094
S89-710	3	0.007	0.52	206	293	817	150	1394	4.76	74.29	0.019	0.058
S89-711	0.5	0.002	0.03	10	34	43	5	26	0.76	15.00	0.003	0.001
S89-712	2.5	0.002	0.07	12	44	86	5	79	1.80	35.00	0.003	0.008
S89-713	2	0.002	0.02	9	60	41	5	54	0.90	10.00	0.003	0.005
S89-714	2	0.011	0.12	13	69	41	5	73	1.06	10.91	0.013	0.026
S89-715	2	0.002	0.16	56	234	704	7	474	2.03	80.00	0.007	0.013
S89-716	2	0.134	0.7	52	200	5800	35	1484	7.42	5.22	0.149	0.297
S89-717	2	0.08	0.5	108	171	18400	39	636	3.72	6.25	0.089	0.179
S89-718	2	0.005	0.21	198	334	1048	119	329	0.99	42.00	0.010	0.021
S89-719	2	0.002	0.21	67	225	687	5	266	1.18	105.00	0.007	0.013
S89-720	2	0.002	0.29	14	175	330	5	1196	6.83	145.00	0.010	0.020
S89-721	2	0.002	0.25	39	285	609	5	993	3.48	125.00	0.009	0.019
S89-722	2	0.007	0.21	109	464	2400	25	952	2.05	30.00	0.015	0.029
S89-723	2	0.002	0.02	125	515	1182	5	449	0.87	10.00	0.006	0.012
S89-724	2	0.003	0.02	78	729	182	5	730	1.00	6.67	0.009	0.018
S89-725	2	0.009	0.23	54	414	987	13	656	1.58	25.56	0.016	0.032
S89-726	2	0.006	0.23	55	481	799	7	1067	2.22	38.33	0.014	0.029
S89-727	2	0.058	0.41	121	820	17800	41	405	0.49	7.07	0.069	0.138
S89-728	2	0.009	0.19	183	1253	1231	215	328	0.26	21.11	0.019	0.037
S89-729	2	0.013	0.13	362	1251	4500	118	512	0.41	10.00	0.022	0.045
S89-730	1	0.017	0.02	9	80	255	14	862	10.78	1.18	0.020	0.020
S89-731	1	0.026	0.34	15	195	783	46	1195	6.13	13.08	0.035	0.035
S89-732	2	0.007	0.04	40	115	441	9	105	0.91	5.71	0.008	0.017
S89-733	1.5	0.007	0.08	22	167	396	9	138	0.83	11.43	0.009	0.014
S89-734	1	0.006	0.06	8	29	163	15	129	4.45	10.00	0.007	0.007
S89-735	2	0.002	0.02	15	143	264	5	65	0.45	10.00	0.003	0.006
S89-736	1	0.002	0.02	17	49	80	5	42	0.86	10.00	0.003	0.003
S89-737	2	0.01	0.41	32	466	1176	14	2202	4.73	41.00	0.024	0.047
S89-738	2	0.018	0.15	206	1084	304	18	211	0.19	8.33	0.026	0.052
S89-739	1	0.025	0.94	37	992	3000	20	5310	5.35	37.60	0.057	0.057
S89-740	12	0.004	0.02	4	197	37	19	136	0.69	5.00	0.006	0.067
S89-741	1.5	0.867	16.81	93	811	3500	252	~~1730000~~ 173000	~~2133.17~~ 213.3	19.39	~~5.510~~ 1.543	~~[illegible]~~
S89-742	6	0.025	0.42	49	632	83	24	5750	9.10	16.80	0.049	0.292
S89-743	16	0.007	0.04	121	454	24	22	1044	2.30	5.71	0.012	0.200
S89-744	17	0.005	0.02	132	561	5	43	203	0.36	4.00	0.009	0.146

Pb/Zn Ag/Au Avequiv.

S Trench / Eliza Creek									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-274	1	0.002	0.02	22	5295	615	93	70	0.01	10.00	0.029	0.029
S89-275	1	0.02	0.24	19	1187	1185	33	1740	1.47	12.00	0.034	0.034
S89-276	2	0.017	0.54	151	14550	5500	181	5320	0.37	31.76	0.110	0.220
S89-277	2	0.013	0.13	53	5180	532	130	996	0.19	10.00	0.043	0.086
S89-278	1	0.002	0.62	124	4140	405	48	12500	3.02	310.00	0.063	0.063
S89-359		0.002	0.02	30	1169	656	39	459	0.39	10.00	0.009	0.000
S89-562	1	0.01	0.88	43	738	1971	39	8520	11.54	88.00	0.048	0.048
S89-563	1	0.013	0.72	43	1315	1900	30	7970	6.06	55.38	0.050	0.050
S89-607	2	0.002	0.12	5	150	151	5	29	0.19	60.00	0.004	0.009
S89-608	2	0.002	0.12	6	118	98	10	22	0.19	60.00	0.004	0.009
S89-609	4	0.002	0.07	8	232	242	35	104	0.45	35.00	0.004	0.018
S89-610	3	0.002	0.09	14	241	97	16	139	0.58	45.00	0.005	0.014
S89-611	3.5	0.007	0.02	32	1431	534	25	1738	1.21	2.86	0.019	0.066
S89-612	3	0.014	0.47	57	2246	1262	37	7210	3.21	33.57	0.050	0.150
S89-613	3	0.002	0.02	16	171	52	11	128	0.75	10.00	0.003	0.010
S89-614	1	0.013	0.35	30	1492	1591	29	4660	3.12	26.92	0.037	0.037
S89-615	1	0.032	0.63	22	1844	2100	37	6320	3.43	19.69	0.066	0.066
S89-616	1	0.007	0.26	22	1256	1472	19	2147	1.71	37.14	0.022	0.022
S89-617	5	0.002	0.03	34	2418	563	36	412	0.17	15.00	0.015	0.077
S89-618	5	0.002	0.09	79	1576	495	47	1144	0.73	45.00	0.014	0.070
S89-619	6	0.037	0.03	28	801	361	32	226	0.28	0.81	0.042	0.252
S89-620	1	0.018	1.28	142	12880	3700	90	9870	0.77	71.11	0.125	0.125
S89-621	1	0.021	0.79	98	3710	2600	68	6040	1.63	37.62	0.066	0.066
S89-622	1	0.003	0.26	297	6320	1493	34	3150	0.50	86.67	0.046	0.046
S89-623	1	0.045	0.71	50	1308	1891	50	6600	5.05	15.78	0.078	0.078
S89-624	1	0.039	0.58	24	568	1670	36	5830	10.26	14.87	0.065	0.065
S89-625	1	0.016	0.59	32	1342	1519	39	6740	5.02	36.88	0.048	0.048
S89-626	1	0.011	0.69	31	971	1385	32	9490	9.77	62.73	0.050	0.050
S89-627	1	0.002	0.17	212	6450	1050	28	2710	0.42	85.00	0.043	0.043
S89-628	1	0.002	0.4	166	6680	832	45	5760	0.86	200.00	0.055	0.055
S89-629	8	0.003	0.17	95	6970	489	41	1446	0.21	56.67	0.044	0.349
S89-630	1	0.011	0.96	112	2318	4000	62	10240	4.42	87.27	0.062	0.062
S89-631	1	0.02	1.01	54	900	3200	54	8390	9.32	50.50	0.060	0.060
S89-632	1	0.015	1.07	39	748	2400	55	9290	12.42	71.33	0.057	0.057
S89-633	1	0.007	0.55	59	1258	2400	39	4560	3.62	78.57	0.033	0.033
S89-634	1	0.003	0.37	144	3127	3000	37	2162	0.69	123.33	0.029	0.029
S89-635	1	0.014	0.43	122	3039	2600	41	3840	1.26	30.71	0.045	0.045
S89-636	1	0.011	0.71	160	2116	2500	40	6960	3.29	64.55	0.049	0.049
S89-637	1	0.012	1.04	109	1880	2700	58	11310	6.02	86.67	0.065	0.065
S89-638	1	0.019	1.16	113	1384	3100	66	15250	11.02	61.05	0.081	0.081
S89-639	1	0.027	1.4	116	1286	4300	69	15890	12.36	51.85	0.093	0.093
S89-640	1	0.012	1.05	117	2048	2400	53	10870	5.31	87.50	0.065	0.065
S89-941	3	0.022	1.358	89	2058	2400	69	18510	8.99	61.73	0.098	0.295
S89-942	1	0.014	0.856	86	1710	2800	63	8670	5.07	61.14	0.057	0.057
S89-943	2	0.013	0.922	99	1672	3000	47	14720	8.80	70.92	0.072	0.143
S89-944	2	0.02	1.653	178	1495	5000	85	22200	14.85	82.65	0.107	0.214
S89-945	2	0.003	0.25	224	1415	2200	39	3990	2.82	83.33	0.024	0.047
S89-946	2	0.002	0.163	276	1664	1600	32	2242	1.35	81.50	0.018	0.036
S89-947	1	0.002	0.052	259	1399	1300	19	844	0.60	26.00	0.012	0.012
S89-948	2	0.015	0.702	337	3157	2100	65	14260	4.52	46.80	0.077	0.154
S89-949	2	0.007	0.561	198	1880	1923	50	7130	3.79	80.14	0.042	0.085
S89-950	2	0.017	0.868	106	1698	2600	56	8725	5.14	51.06	0.060	0.120
S89-951	2	0.011	0.746	127	1541	2100	45	8160	5.30	67.82	0.050	0.100

Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	Pb/Zn ERR ERR	Ag/Au ERR ERR	Au equiv. ERR ERR	ERR ERR
S89-952	2	0.021	1.159	162	1940	3000	78	11280	5.81	55.19	0.076	0.151
S89-953	2	0.04	1.564	209	1884	2000	86	21200	11.25	39.10	0.125	0.251
S89-954		0.002	0.06	19	187	136	9	401	2.14	30.00	0.005	ERR

Pb/Zn Ag/Au Au equiv.

Courtland									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-360	8	0.002	0.02	34	27	5	5	55	2.04	10.00	0.003	0.020
S89-361	5	0.002	0.02	44	42	5	5	37	0.88	10.00	0.003	0.013
S89-362	5	0.002	0.02	45	48	10	5	27	0.56	10.00	0.003	0.013
S89-363	5	0.002	0.02	31	42	5	5	30	0.71	10.00	0.003	0.013
S89-364	5	0.002	0.05	53	36	5	5	40	1.11	25.00	0.003	0.015
S89-365	5	0.002	0.02	46	27	7	14	39	1.44	10.00	0.003	0.013
S89-366	3	0.002	0.02	30	20	5	9	39	1.95	10.00	0.002	0.007
S89-367	3	0.002	0.02	105	31	5	9	41	1.32	10.00	0.003	0.008
S89-368	3	0.002	0.02	53	19	42	5	61	3.21	10.00	0.003	0.008
S89-369	3	0.002	0.02	120	39	28	9	90	2.31	10.00	0.003	0.008
S89-370	2	0.002	0.02	18	18	23	5	45	2.50	10.00	0.002	0.005
S89-371	2	0.002	0.02	5	4	11	5	13	3.25	10.00	0.002	0.005
S89-372	2	0.002	0.02	3	4	6	5	5	1.25	10.00	0.002	0.005
S89-373	2	0.002	0.02	18	9	14	5	20	2.22	10.00	0.002	0.005
S89-374	2	0.003	0.02	164	24	54	5	123	5.13	6.67	0.004	0.007
S89-375	2	0.002	0.02	158	54	72	5	75	1.39	10.00	0.003	0.005
S89-376	5	0.002	0.02	5	4	22	5	10	2.50	10.00	0.002	0.012
S89-377	4	0.002	0.02	45	17	25	5	44	2.59	10.00	0.002	0.010
S89-378	5	0.002	0.02	70	21	22	5	30	1.43	10.00	0.002	0.012
S89-379	5	0.002	0.03	123	60	34	7	38	0.63	15.00	0.003	0.014
S89-380	3	0.002	0.02	109	76	10	11	57	0.75	10.00	0.003	0.008
S89-381	4	0.063	0.09	102	117	36	12	100	0.85	1.43	0.065	0.260
S89-382	10	0.002	0.02	61	89	16	5	60	0.67	10.00	0.003	0.029
S89-383	8	0.002	0.02	40	36	15	7	52	1.44	10.00	0.003	0.021
S89-384	3	0.005	0.02	100	36	151	10	84	2.33	4.00	0.006	0.017
S89-385	4	0.002	0.02	63	64	22	13	50	0.78	10.00	0.003	0.011
S89-386	3	0.014	0.02	21	385	2600	14	144	0.37	1.43	0.017	0.050
S89-387	2	0.008	0.09	27	2068	1231	16	193	0.09	11.25	0.020	0.040
S89-388	2	0.012	0.02	37	2242	2400	14	241	0.11	1.67	0.024	0.048
S89-389	3	0.004	0.02	17	959	624	22	166	0.17	5.00	0.009	0.028
S89-390	2	0.002	0.02	9	1428	61	18	91	0.06	10.00	0.010	0.019
S89-391	2	0.003	0.02	5	993	177	13	95	0.10	6.67	0.008	0.017
S89-392	6	0.022	0.02	57	7560	2400	31	428	0.06	0.91	0.061	0.365
S89-393	3	0.002	0.02	4	134	52	14	44	0.33	10.00	0.003	0.009
S89-394	4	0.002	0.02	3	102	15	17	50	0.49	10.00	0.003	0.012
S89-395	3	0.002	0.19	4	104	5	16	55	0.53	95.00	0.005	0.016
S89-396	1	0.006	0.33	11	148	1563	5	439	2.97	55.00	0.012	0.012
S89-397	4	0.002	0.22	3	189	111	25	353	1.87	110.00	0.007	0.028
S89-398	3	0.002	0.11	15	626	34	11	352	0.56	55.00	0.008	0.023
S89-399	13	0.002	0.02	9	85	57	15	88	1.04	10.00	0.003	0.038
S89-400	13	0.002	0.02	4	137	34	19	127	0.93	10.00	0.003	0.043
S89-401	3	0.002	0.12	4	1658	485	14	72	0.04	60.00	0.012	0.036
S89-402	8	0.004	0.07	52	641	284	11	180	0.28	17.50	0.009	0.069
S89-403	4	0.002	0.05	82	50	40	5	76	1.52	25.00	0.003	0.013
S89-404	4	0.002	0.05	33	35	63	5	63	1.80	25.00	0.003	0.012
S89-405	4	0.002	0.02	45	17	30	12	56	3.29	10.00	0.003	0.010
S89-406	4	0.002	0.02	87	14	26	12	48	3.43	10.00	0.002	0.010
S89-407	16	0.002	0.02	71	28	21	8	47	1.68	10.00	0.003	0.041

									Pb/Zn	Ag/Au		Au equiv.
Trench H4									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-408	4	0.017	0.08	86	597	1627	12	269	0.45	4.71	0.022	0.087
S89-409	1	0.009	0.22	163	529	823	75	734	1.39	24.44	0.017	0.017
S89-410	6	0.006	0.16	334	1103	1046	146	1054	0.96	26.67	0.016	0.098
S89-411	2	0.029	0.72	197	648	987	241	2680	4.14	24.83	0.049	0.098
S89-412	3	0.002	0.02	195	1235	648	86	567	0.46	10.00	0.010	0.030
S89-413	3	0.006	0.05	183	1215	1811	125	463	0.38	8.33	0.014	0.042
S89-414	2	0.002	0.02	28	441	134	19	110	0.25	10.00	0.005	0.009
S89-415	2	0.002	0.05	7	477	114	17	59	0.12	25.00	0.005	0.010
S89-416	2	0.002	0.02	22	640	270	62	107	0.17	10.00	0.006	0.011
S89-417	2	0.002	0.02	29	247	341	54	100	0.40	10.00	0.004	0.008
S89-418	2	0.002	0.07	22	90	95	14	97	1.08	35.00	0.004	0.007
S89-419	2	0.002	0.07	130	156	229	31	311	1.99	35.00	0.005	0.009
S89-420	2	0.002	0.27	535	174	267	131	501	2.88	135.00	0.008	0.016
S89-421	2	0.002	0.07	21	310	770	42	575	1.85	35.00	0.006	0.012
S89-422	2	0.002	0.06	22	89	526	30	72	0.81	30.00	0.003	0.007
S89-423	2	0.002	0.04	7	117	519	31	59	0.50	20.00	0.003	0.007
S89-424	2	0.002	0.05	417	83	687	79	116	1.40	25.00	0.003	0.007
S89-425	0.5	0.035	0.42	3160	180	1016	505	363	2.02	12.00	0.043	0.021
S89-426	2	0.005	0.13	54	142	1105	84	105	0.74	26.00	0.008	0.016
S89-427	2	0.002	0.09	15	174	83	19	89	0.51	45.00	0.004	0.009
S89-428	2	0.002	0.08	74	249	237	20	52	0.21	40.00	0.004	0.009
S89-429	3	0.002	0.03	77	277	1053	30	224	0.81	15.00	0.004	0.013
S89-430	3	0.002	0.03	17	271	173	11	65	0.24	15.00	0.004	0.012
S89-431	3	0.002	0.02	323	173	74	6	122	0.71	10.00	0.003	0.010
S89-432	3	0.002	0.1	163	176	134	15	59	0.34	50.00	0.004	0.013
S89-433	3	0.002	0.34	222	221	161	71	574	2.60	170.00	0.009	0.028
S89-434	3	0.002	0.21	161	199	317	57	238	1.20	105.00	0.007	0.020
S89-435	4	0.002	0.09	59	153	191	24	89	0.58	45.00	0.004	0.017
S89-436	2	0.003	0.48	108	135	268	50	601	4.45	160.00	0.012	0.024
S89-437	1	0.006	0.32	21	20	99	15	535	26.75	53.33	0.012	0.012
S89-438	1	0.005	0.26	22	29	91	29	330	11.38	52.00	0.010	0.010
S89-439	2	0.022	0.44	22	50	127	13	372	7.44	20.00	0.029	0.059
S89-440	2	0.002	0.22	200	480	163	14	485	1.01	110.00	0.009	0.017
S89-441	6	0.002	0.16	173	554	148	14	406	0.73	80.00	0.008	0.048
S89-442	6	0.002	3	91	309	71	5	104	0.34	1500.00	0.046	0.275
S89-443	2	0.005	0.48	119	114	201	12	267	2.34	96.00	0.013	0.026
S89-444	2	0.012	2.01	196	160	529	24	296	1.85	167.50	0.042	0.083
S89-445	5	0.002	0.09	203	174	236	10	104	0.60	45.00	0.004	0.022
S89-446	5	0.033	0.85	98	256	481	17	944	3.69	25.76	0.049	0.243
S89-447	2	0.002	0.11	104	158	75	5	142	0.90	55.00	0.005	0.009
S89-448	2	0.006	0.32	127	294	308	13	233	0.79	53.33	0.013	0.025
S89-449	3	0.002	0.14	10	367	98	13	65	0.18	70.00	0.006	0.018
S89-450	3	0.002	0.02	11	339	36	9	127	0.37	10.00	0.004	0.013
S89-451	3	0.002	0.02	66	655	57	16	317	0.48	10.00	0.006	0.019
S89-452	3	0.002	0.02	16	166	50	20	71	0.43	10.00	0.003	0.010
S89-453	3	0.002	0.09	88	511	133	14	755	1.48	45.00	0.008	0.023
S89-454	4	0.002	0.22	241	2644	133	34	1023	0.39	110.00	0.021	0.083
S89-455	3	0.002	0.07	143	430	224	25	448	1.04	35.00	0.006	0.019
S89-456	7	0.002	0.02	6	224	51	16	59	0.26	10.00	0.004	0.025
S89-457	2	0.002	0.02	51	752	115	20	188	0.25	10.00	0.006	0.013
S89-458	1	0.025	0.38	49	221	704	38	3610	16.33	15.20	0.041	0.041
S89-459	2	0.016	0.33	90	483	822	27	3620	7.49	20.63	0.032	0.064
S89-460	2	0.018	0.41	78	825	1044	30	3620	4.39	22.78	0.037	0.074
S89-461	2	0.019	0.32	112	761	970	45	3030	3.98	16.84	0.035	0.070

									Pb/Zn	Ag/Au	Au equiv.	
Line 14 West Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-462	1.5	0.004	0.03	16	348	1340	58	228	0.66	7.50	0.007	0.010
S89-463	2	0.002	0.02	14	186	431	50	113	0.61	10.00	0.003	0.007
S89-464	2	0.002	0.02	10	172	120	30	99	0.58	10.00	0.003	0.007
S89-465	1	0.003	0.02	37	374	558	50	267	0.71	6.67	0.006	0.006
S89-466	1	0.004	0.07	67	642	1134	153	597	0.93	17.50	0.010	0.010
S89-467	2.5	0.002	0.02	14	177	75	16	73	0.41	10.00	0.003	0.008
S89-468	1	0.002	0.02	19	130	236	20	77	0.59	10.00	0.003	0.003
S89-469	1.5	0.002	0.02	14	93	74	13	68	0.73	10.00	0.003	0.004
S89-470	1.5	0.002	0.02	21	103	71	13	78	0.76	10.00	0.003	0.004
S89-471	1	0.006	0.03	36	550	3600	298	189	0.34	5.00	0.010	0.010
S89-472	1	0.002	0.02	8	57	25	81	49	0.86	10.00	0.003	0.003
S89-473	5	0.002	0.02	7	122	34	28	58	0.48	10.00	0.003	0.015
S89-474	4	0.002	0.02	9	185	34	13	62	0.34	10.00	0.003	0.013
S89-475	3	0.002	0.05	11	365	146	17	102	0.28	25.00	0.005	0.014
S89-476	1	0.002	0.02	11	1005	612	17	69	0.07	10.00	0.007	0.007
S89-477	3	0.002	0.03	25	1247	714	66	127	0.10	15.00	0.009	0.027
S89-478	2	0.02	8.55	2130	4604	8300	574	71200	15.46	427.50	0.344	0.688
S89-519	2	0.002	0.02	30	3767	549	67	81	0.02	10.00	0.021	0.042
S89-520	1	0.002	0.02	255	5210	1983	15	132	0.03	10.00	0.028	0.028
S89-521	1	0.004	0.04	153	2047	5100	14	294	0.14	10.00	0.015	0.015
S89-522	1	0.002	0.04	77	681	3300	10	178	0.26	20.00	0.006	0.006
S89-523	1	0.022	0.22	37	417	5600	15	691	1.66	10.00	0.029	0.029
S89-524	1	0.014	0.07	67	727	7200	12	434	0.60	5.00	0.020	0.020
S89-525	1	0.006	0.14	73	1369	2200	11	490	0.36	23.33	0.016	0.016
S89-526	1	0.028	0.35	25	408	1432	10	1160	2.84	12.50	0.038	0.038
S89-527	1	0.133	0.8	39	386	11500	33	5100	13.21	6.02	0.159	0.159
S89-528	1	0.274	1.6	60	627	6600	99	4910	7.83	5.84	0.312	0.312
S89-529	1	0.082	0.54	75	1530	5000	31	1625	1.06	6.59	0.101	0.101
S89-530	1	0.002	0	44	2110	928	37	87	0.04	0.00	0.013	0.013

Pb/Zn Ag/Au Au equiv.

Line 14 East Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-479	2	0.003	0.2	94	1029	420	25	1319	1.28	66.67	0.014	0.029
S89-480	1	0.002	0.11	55	1334	721	116	457	0.34	55.00	0.011	0.011
S89-481	1	0.002	0.28	75	13910	867	489	3680	0.26	140.00	0.084	0.084
S89-482	3	0.002	0.18	109	1706	377	23	442	0.26	90.00	0.014	0.042
S89-483	2	0.005	0.42	195	1605	941	37	1836	1.14	84.00	0.024	0.047
S89-484	1	0.006	0.46	228	704	999	27	1846	2.62	76.67	0.021	0.021
S89-485	1	0.004	0.33	279	995	906	5	896	0.90	82.50	0.016	0.016
S89-486	1	0.002	0.26	131	1393	190	5	408	0.29	130.00	0.014	0.014
S89-487	1	0.002	0.08	108	1043	51	5	52	0.05	40.00	0.008	0.008
S89-488	1.5	0.002	0.14	17	176	61	5	66	0.38	70.00	0.005	0.007
S89-489	2	0.002	0.03	5	132	60	5	64	0.48	15.00	0.003	0.006
S89-490	1	0.002	0.06	7	157	36	5	198	1.26	30.00	0.004	0.004
S89-491	4.5	0.002	0.11	71	697	387	21	1540	2.21	55.00	0.011	0.049
S89-492	4	0.002	0.1	20	87	100	13	97	1.11	50.00	0.004	0.016
S89-493	2	0.002	0.24	194	369	923	39	715	1.94	120.00	0.009	0.018
S89-494	2	0.002	0.14	194	257	752	13	146	0.57	70.00	0.006	0.011
S89-495	2	0.003	0.16	97	9310	2100	208	323	0.03	53.33	0.052	0.104
S89-496	1.5	0.053	1.1	206	552	5400	565	8580	15.54	20.75	0.093	0.140
S89-497	1.5	0.009	0.44	78	348	1386	52	2860	8.22	48.89	0.024	0.036
S89-498	1.5	0.002	0.15	56	2931	1108	95	390	0.13	75.00	0.020	0.029
S89-499	2.5	0.002	0.02	42	353	362	10	71	0.20	10.00	0.004	0.011
S89-500	2	0.002	0.02	53	521	452	5	62	0.12	10.00	0.005	0.010
S89-501	2	0.06	1.15	79	228	2900	44	7550	33.11	19.17	0.096	0.193
S89-502	2	0.034	1.02	37	161	3000	43	8400	52.17	30.00	0.070	0.141
S89-503	1.5	0.002	0.06	118	623	1225	11	557	0.89	30.00	0.007	0.011
S89-504	8	0.002	0.08	4	37	38	7	28	0.76	40.00	0.003	0.027
S89-505	8	0.002	0.02	6	34	73	6	68	2.00	10.00	0.003	0.021
S89-506	4	0.004	0.02	16	222	189	22	87	0.39	5.00	0.006	0.022
S89-507	2	0.002	0.07	12	395	229	11	465	1.18	35.00	0.006	0.012
S89-508	2	0.1	0.55	48	605	8000	33	2159	3.57	5.50	0.116	0.232
S89-509	4	0.002	0.02	27	163	211	21	80	0.49	10.00	0.003	0.013
S89-510	2	0.005	0.09	48	519	936	24	576	1.11	18.00	0.010	0.021
S89-511	1	0.007	0.08	36	275	1135	22	579	2.11	11.43	0.011	0.011
S89-512	1	0.003	0.05	39	680	884	23	351	0.52	16.67	0.008	0.008
S89-513	1	0.002	0.12	42	333	992	20	537	1.61	60.00	0.007	0.007
S89-514	8	0.005	0.02	16	250	269	10	50	0.20	4.00	0.007	0.053
S89-515	5	0.002	0.03	28	202	171	14	58	0.29	15.00	0.004	0.018
S89-516	5	0.003	0.02	40	812	491	19	238	0.29	6.67	0.008	0.040
S89-517	7	0.006	0.02	54	989	843	15	491	0.50	3.33	0.012	0.087
S89-518		0.002	0.02	32	329	200	5	184	0.56	10.00	0.004	0.000

Eliza Creek L16 Trench									Pb/Zn	Ag/Au	Avequiv.	
									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-564	8	0.005	0.23	24	888	7400	67	812	0.91	46.00	0.015	0.117
S89-565	5	0.005	0.15	34	1181	1784	59	817	0.69	30.00	0.015	0.075
S89-566	3	0.006	0.35	32	1191	1363	61	1092	0.92	58.33	0.020	0.059
S89-567	3	0.005	0.27	30	1602	1617	61	861	0.54	54.00	0.019	0.057
S89-568	3	0.005	0.31	27	985	1632	50	1620	1.64	62.00	0.018	0.055
S89-569	3	0.014	0.73	73	2026	7300	87	2218	1.09	52.14	0.040	0.120
S89-570	3	0.026	0.88	84	1060	5300	138	5070	4.78	33.85	0.056	0.169
S89-571	3	0.039	1.24	108	4271	3300	116	4080	0.96	31.79	0.088	0.264
S89-572	3	0.005	0.42	108	4821	1964	112	1838	0.38	84.00	0.039	0.118
S89-573	1	0.005	0.28	44	1322	950	44	1160	0.88	56.00	0.018	0.018
S89-574	3	0.015	0.43	73	735	1823	54	1413	1.92	28.67	0.028	0.085
S89-575	3	0.034	5.49	220	2838	2000	289	12030	4.24	161.47	0.156	0.467
S89-576	3	0.003	0.52	53	3980	1359	105	1261	0.32	173.33	0.033	0.100
S89-577	3	0.005	0.36	40	1220	1008	50	1480	1.21	72.00	0.020	0.060
S89-578	3	0.002	0.14	76	3031	362	64	925	0.31	70.00	0.021	0.064
S89-579	3	0.002	0.02	29	1813	376	34	406	0.22	10.00	0.012	0.037
S89-580	3	0.002	0.02	29	1902	423	52	365	0.19	10.00	0.013	0.038
S89-581	3	0.002	1.41	133	2979	1393	96	1796	0.60	705.00	0.041	0.123
S89-582	3	0.004	0.4	25	750	988	51	1714	2.29	100.00	0.018	0.053
S89-583	3	0.006	4.59	144	14650	1191	468	13010	0.89	765.00	0.176	0.528
S89-584	3	0.009	8.79	420	9320	3100	1170	11680	1.25	976.67	0.208	0.624
S89-585	3	0.003	1.18	169	3104	1001	148	8460	2.73	393.33	0.056	0.169
S89-586	5	0.002	0.03	25	877	214	13	279	0.32	15.00	0.007	0.037
S89-587	10	0.002	0.43	45	1259	461	44	1552	1.23	215.00	0.018	0.182
S89-588	7	0.002	0.02	33	832	268	24	570	0.69	10.00	0.008	0.055
S89-589	3	0.002	0.09	17	610	303	40	296	0.49	45.00	0.007	0.021
S89-590	3	0.011	0.24	11	530	859	17	327	0.62	21.82	0.018	0.053
S89-591	3	0.027	0.36	13	920	1824	160	1392	1.51	13.33	0.040	0.120
S89-592	3	0.013	0.22	14	563	1470	37	506	0.90	16.92	0.020	0.060
S89-593	4	0.002	0.1	30	379	257	18	511	1.35	50.00	0.007	0.026
S89-594	3	0.002	0.07	15	167	92	19	181	1.08	35.00	0.004	0.013
S89-595	4	0.002	0.09	17	121	56	12	97	0.80	45.00	0.004	0.016
S89-596	4	0.002	0.11	11	122	34	15	146	1.20	55.00	0.005	0.018
S89-597	10	0.002	0.11	36	269	39	23	222	0.83	55.00	0.005	0.054
S89-598	13	0.002	0.11	14	377	39	27	139	0.37	55.00	0.006	0.075
S89-599	5	0.011	0.17	38	488	1271	73	382	0.78	15.45	0.017	0.084
S89-600	2	0.015	0.21	29	970	1488	70	657	0.68	14.00	0.024	0.049
S89-601	3	0.009	0.14	20	317	526	63	139	0.44	15.56	0.013	0.039
S89-602	2	0.002	0.07	44	430	1053	64	182	0.42	35.00	0.006	0.011
S89-603	5	0.003	0.02	20	367	669	46	121	0.33	6.67	0.005	0.027
S89-604	3	0.003	0.02	17	123	138	13	74	0.60	6.67	0.004	0.012
S89-605	3	0.002	0.09	14	83	36	8	62	0.75	45.00	0.004	0.011
S89-606	4	0.002	0.12	17	106	64	15	106	1.00	60.00	0.004	0.018

									Pb/Zn	Ag/Au	Au eqiv.	
Line 11 Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-641	1	0.003	0.11	554	2141	2400	19	713	0.33	36.67	0.017	0.017
S89-642	1	0.005	0.11	656	2486	4100	64	2630	1.06	22.00	0.026	0.026
S89-643	1	0.003	0.13	325	1503	1720	65	1129	0.75	43.33	0.015	0.015
S89-644	4	0.002	0.02	13	146	97	8	134	0.92	10.00	0.003	0.013
S89-645	2	0.037	0.88	310	2694	4300	105	8370	3.11	23.78	0.084	0.168
S89-646	1	0.021	0.81	110	1965	1179	95	8430	4.29	38.57	0.064	0.064
S89-647	1	0.014	0.82	48	834	647	56	10390	12.46	58.57	0.056	0.056
S89-648	1	0.014	0.72	36	378	627	35	10040	26.56	51.43	0.052	0.052
S89-649	1	0.009	0.8	76	679	722	68	2740	4.04	88.89	0.031	0.031
S89-650	1	0.01	0.65	106	661	559	73	8130	12.30	65.00	0.043	0.043
S89-651	1	0.002	0.13	107	2915	674	8	243	0.08	65.00	0.019	0.019
S89-652	2	0.002	0.42	165	7950	759	27	846	0.11	210.00	0.049	0.099
S89-653	2	0.002	0.18	111	1801	328	9	171	0.09	90.00	0.014	0.028
S89-654	1	0.094	1.34	85	952	2500	52	8060	8.47	14.26	0.138	0.138
S89-655	1	0.056	2.22	179	1236	3200	106	1660	1.34	39.64	0.097	0.097
S89-656	1	0.013	1.28	68	847	1670	37	8880	10.48	98.46	0.058	0.058
S89-657	1	0.033	1.38	28	437	1839	35	10770	24.65	41.82	0.082	0.082
S89-658	1	0.012	0.89	26	437	1106	21	6650	15.22	74.17	0.044	0.044
S89-659	1	0.008	0.82	19	387	1106	10	6200	16.02	102.50	0.037	0.037
S89-660	1	0.021	1.91	36	454	2100	51	15500	34.14	90.95	0.090	0.090
S89-661	1	0.012	1.21	24	439	1324	15	10000	22.78	100.83	0.057	0.057
S89-662	1	0.005	0.61	57	1600	1215	16	5200	3.25	122.00	0.035	0.035
S89-663	2	0.002	0.06	88	2687	494	5	230	0.09	30.00	0.017	0.033
S89-664	5	0.002	0.07	7	857	238	5	105	0.12	35.00	0.007	0.037
S89-665	4	0.002	0.07	16	798	574	9	130	0.16	35.00	0.007	0.029
S89-666	1	0.002	0.11	23	888	913	16	229	0.26	55.00	0.009	0.009
S89-667	2	0.006	0.19	21	1176	2400	70	977	0.83	31.67	0.017	0.034
S89-668	1	0.002	0.04	18	314	402	18	241	0.77	20.00	0.005	0.005
S89-669	27	0.002	0.23	48	1842	740	28	1183	0.64	115.00	0.017	0.469
S89-670	27	0.003	0.12	19	395	197	21	580	1.47	40.00	0.008	0.219
S89-671	2	0.003	0.12	74	559	1773	27	471	0.84	40.00	0.009	0.017
S89-672	3	0.03	0.35	56	475	8300	17	1521	3.20	11.67	0.041	0.123
S89-673	3	0.048	0.55	90	864	16000	38	3390	3.92	11.46	0.069	0.206
S89-674	2	0.002	0.07	5	157	325	11	90	0.57	35.00	0.004	0.008
S89-675	2	0.002	0.02	23	762	169	25	607	0.80	10.00	0.008	0.015
S89-676	3	0.002	0.09	27	336	98	5	257	0.76	45.00	0.006	0.017

Pb/Zn Ag/Au Au equiv.

L4+16 Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-677	4	0.002	0.18	23	293	90	5	62	0.21	90.00	0.006	0.025
S89-678	1	0.003	0.12	368	2083	2100	79	194	0.09	40.00	0.015	0.015
S89-679	1	0.002	0.18	142	417	1244	15	514	1.23	90.00	0.008	0.008
S89-680	1	0.004	0.33	73	156	1375	25	712	4.56	82.50	0.011	0.011
S89-681	1	0.106	0.89	213	107	7600	137	8810	82.34	8.40	0.141	0.141
S89-682	1	0.018	0.09	31	41	163	5	492	12.00	5.00	0.021	0.021
S89-683	1	0.074	0.34	10	30	160	35	554	18.47	4.59	0.080	0.080
S89-684	1	0.053	0.31	6	28	79	8	376	13.43	5.85	0.058	0.058
S89-685	1	0.003	0.14	22	70	288	5	186	2.66	46.67	0.006	0.006
S89-686	1	0.009	0.53	66	176	1218	115	925	5.26	58.89	0.020	0.020
S89-687	1	0.007	0.32	32	129	751	48	480	3.72	45.71	0.013	0.013
S89-688	2	0.002	0.09	75	675	845	5	51	0.08	45.00	0.007	0.013
S89-689	3	0.022	0.69	11	20	132	60	1125	56.25	31.36	0.035	0.104
S89-690	2	0.002	0.1	262	1168	2900	14	100	0.09	50.00	0.009	0.019
S89-691	2	0.023	0.89	84	152	1034	52	1308	8.61	38.70	0.040	0.079
S89-692	2	0.002	0.07	56	253	555	7	53	0.21	35.00	0.004	0.009
S89-693	3.5	0.002	0.02	4	51	51	7	22	0.43	10.00	0.003	0.009
S89-694	1.6	0.197	2.36	59	5270	12200	92	18890	3.58	11.98	0.304	0.487
S89-695	4	0.015	0.68	84	288	648	96	952	3.31	45.33	0.028	0.113
S89-696	2	0.002	0.06	103	238	457	14	202	0.85	30.00	0.005	0.009
S89-697	2	0.002	0.04	61	231	515	16	121	0.52	20.00	0.004	0.008
S89-698	2	0.002	0.04	31	99	270	10	62	0.63	20.00	0.003	0.006
S89-699	2	0.002	0.02	43	198	268	5	71	0.36	10.00	0.003	0.007
S89-700	2	0.002	0.02	35	127	286	5	45	0.35	10.00	0.003	0.006
S89-701	2	0.002	0.02	75	237	629	12	79	0.33	10.00	0.004	0.007
S89-702	1	0.002	0.06	72	231	823	18	142	0.61	30.00	0.004	0.004
S89-703	1	0.002	0.15	26	71	597	18	211	2.97	75.00	0.005	0.005
S89-704	1	0.027	1.01	16	67	543	189	1329	19.84	37.41	0.045	0.045
S89-705	1	0.016	0.54	6	48	137	139	387	8.06	33.75	0.025	0.025
S89-706	1	0.002	0.02	19	98	295	9	496	5.06	10.00	0.004	0.004
S89-707	1	0.002	0.06	110	667	864	7	118	0.18	30.00	0.006	0.006
S89-708	1.5	0.002	0.03	21	229	171	11	156	0.68	15.00	0.004	0.006
S89-709	3	0.025	0.85	53	125	757	93	1048	8.38	34.00	0.040	0.121

									Pb/Zn	Ag/Au	Au equiv.	
D12 Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-745	1.5	0.005	0.07	41	5400	97	93	229	0.04	14.00	0.033	0.050
S89-746	2.5	0.006	0.1	30	410	401	6	239	0.58	16.67	0.010	0.025
S89-747	1	0.013	0.12	41	376	723	24	1548	4.12	9.23	0.020	0.020
S89-748	1	0.002	0.17	38	542	985	11	235	0.43	85.00	0.008	0.008
S89-749	1	0.095	1.03	73	185	1916	43	6640	35.89	10.84	0.127	0.127
S89-750	1	0.114	5.19	74	158	3300	99	50400	318.99	45.53	0.316	0.316
S89-751	1	0.011	0.34	16	151	430	11	1079	7.15	30.91	0.019	0.019
S89-752	1	0.018	0.36	17	262	397	12	1393	5.32	20.00	0.028	0.028
S89-753	1.4	0.004	0.02	28	459	726	15	758	1.65	5.00	0.008	0.012
S89-754	1.6	0.002	0.14	37	1751	345	41	141	0.08	70.00	0.013	0.021
S89-755	1	0.125	1.24	22	114	4900	23	4820	42.28	9.92	0.155	0.155
S89-756	5	0.002	0.1	50	95	41	19	100	1.05	50.00	0.004	0.021
S89-757	13	0.002	0.29	102	493	278	28	2230	4.52	145.00	0.014	0.184
S89-758	3	0.045	0.29	115	3488	2800	57	1772	0.51	6.44	0.071	0.213
S89-759	3	0.074	1.56	202	3930	4600	93	20000	5.09	21.08	0.166	0.499
S89-760	4	0.013	0.7	109	2163	1227	40	9260	4.28	53.85	0.057	0.228

									Pb/Zn	Ag/Au	Au equiv.	
NW MAG. Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-761	2	0.006	0.02	62	281	117	6	354	1.26	3.33	0.009	0.017
S89-762	3	0.007	0.1	13	227	74	11	157	0.69	14.29	0.010	0.030
S89-763	1	0.025	0.1	71	631	1238	15	644	1.02	4.00	0.031	0.031
S89-764	1	0.004	0.02	42	963	84	20	231	0.24	5.00	0.010	0.010
S89-765	1	0.014	0.02	130	531	215	5	488	0.92	1.43	0.018	0.018
S89-766	1	0.016	0.42	68	530	645	18	1214	2.29	26.25	0.028	0.028
S89-767	1	0.052	0.14	61	411	513	13	783	1.91	2.69	0.058	0.058
S89-768	1	0.007	0.14	76	215	551	10	356	1.66	20.00	0.011	0.011
S89-769	1	0.013	0.17	53	108	582	20	313	2.90	13.08	0.017	0.017
S89-770	1	0.002	0.02	174	539	177	20	117	0.22	10.00	0.005	0.005
S89-771	5	0.002	0.02	29	120	66	5	45	0.38	10.00	0.003	0.015
S89-772	5	0.002	0.02	28	72	47	18	54	0.75	10.00	0.003	0.014
S89-773	1	0.004	0.05	41	574	218	5	997	1.74	12.50	0.010	0.010
S89-774	2	0.002	0.02	91	1966	371	38	80	0.04	10.00	0.012	0.024
S89-775	1	0.008	0.39	141	1080	3000	43	4360	4.04	48.75	0.030	0.030
S89-776	1	0.021	0.56	104	916	4800	56	6490	7.09	26.67	0.050	0.050
S89-777	1	0.024	0.32	102	936	5900	50	3520	3.76	13.33	0.042	0.042
S89-778	1	0.002	0.02	91	1020	4400	12	214	0.21	10.00	0.008	0.008
S89-779	2	0.008	0.02	80	1158	343	14	362	0.31	2.50	0.015	0.030
S89-780	3	0.012	0.02	134	812	1530	21	875	1.08	1.67	0.019	0.056
S89-781	1	0.002	0.02	110	171	79	18	66	0.39	10.00	0.003	0.003
S89-782	1	0.014	0.76	265	220	3900	149	531	2.41	54.29	0.027	0.027
S89-783	3	0.002	0.02	171	513	192	17	596	1.16	10.00	0.006	0.019
S89-784	3	0.002	0.02	420	206	113	15	81	0.39	10.00	0.004	0.011
S89-785	3	0.002	0.24	443	204	97	19	76	0.37	120.00	0.007	0.020
S89-786	5	0.002	0.16	1390	447	214	28	109	0.24	80.00	0.007	0.034
S89-787	6	0.002	0.05	1680	361	272	50	91	0.25	25.00	0.005	0.028

Pb/Zn Ag/Au Au equiv.

D12 East Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-788	5	0.002	0.18	55	1060	379	215	983	0.93	90.00	0.012	0.061
S89-789	7	0.008	0.09	83	636	609	21	605	0.95	11.25	0.014	0.098
S89-790	5	0.002	0.39	42	231	104	46	174	0.75	195.00	0.009	0.045
S89-791	1	0.005	1.26	1950	283	195	45	1435	5.07	252.00	0.028	0.028
S89-792	2	0.079	1.49	98	216	1258	26	3310	15.32	18.86	0.109	0.219
S89-793	1	0.231	1.62	209	403	1677	50	3830	9.50	7.01	0.265	0.265
S89-794	2	0.03	0.69	71	197	766	13	1429	7.25	23.00	0.044	0.089
S89-795	2	0.037	0.96	113	224	1464	5	6970	31.12	25.95	0.069	0.139
S89-796	2	0.042	0.67	264	490	2400	33	3690	7.53	15.95	0.063	0.126
S89-797	2	0.108	2.34	136	241	3200	61	14880	61.74	21.67	0.180	0.360
S89-798	2	0.018	0.51	119	464	1339	21	3920	8.45	28.33	0.037	0.075
S89-799	2	0.074	1.16	77	222	1308	29	4000	18.02	15.68	0.102	0.203
S89-800	2	0.154	2.34	118	311	1950	39	5730	18.42	15.19	0.203	0.406
S89-801	2	0.017	0.49	76	352	1318	24	1649	4.68	28.82	0.030	0.060
S89-802	1	0.069	0.86	83	549	1771	48	1786	3.25	12.46	0.088	0.088
S89-803	1	0.099	1.36	57	215	1201	38	2770	12.88	13.74	0.126	0.126
S89-804	1	0.672	6.2	81	314	3400	94	10480	33.38	9.23	0.787	0.787
S89-805	1	0.051	0.92	32	209	953	24	1815	8.68	18.04	0.070	0.070
S89-806	1	0.013	0.49	23	152	487	14	848	5.58	37.69	0.023	0.023
S89-807	1	0.014	0.44	25	130	648	24	1038	7.98	31.43	0.023	0.023
S89-808	1	0.01	0.27	36	191	1073	22	1428	7.48	27.00	0.018	0.018
S89-809	1	0.013	0.32	49	301	821	14	1678	5.57	24.62	0.023	0.023
S89-810	1	0.013	0.29	69	542	845	19	1485	2.74	22.31	0.024	0.024
S89-811	1	0.012	0.22	75	831	1174	16	1587	1.91	18.33	0.023	0.023
S89-812	1	0.005	0.09	270	2561	1775	35	536	0.21	18.00	0.020	0.020
S89-813	1	0.009	0.22	915	1737	892	74	304	0.18	24.44	0.021	0.021
S89-814	1	0.005	0.14	280	1025	1883	26	262	0.26	28.00	0.013	0.013
S89-815	1	0.005	0.59	248	508	3200	105	984	1.94	118.00	0.018	0.018
S89-816	1	0.014	0.89	164	224	1479	247	2150	9.60	63.57	0.033	0.033
S89-817	1	0.312	36.36	148	198	2600	1380	27500	138.89	116.54	0.892	0.892
S89-818	1	0.026	6	141	199	1702	226	9920	49.85	230.77	0.136	0.136
S89-819	1	0.006	1	237	829	1731	88	3110	3.75	166.67	0.032	0.032
S89-820	1	0.002	0.26	443	614	773	26	680	1.11	130.00	0.010	0.010

Pb/Zn Ag/Au Au equiv.

D14/DB Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-821	4	0.013	0.39	12	637	1196	16	1124	1.76	30.00	0.024	0.098
S89-822	3	0.002	0.07	28	747	450	20	112	0.15	35.00	0.007	0.021
S89-823	4	0.034	2.72	128	532	1665	88	6270	11.79	80.00	0.091	0.363
S89-824	1	0.006	0.22	9	117	397	5	369	3.15	36.67	0.011	0.011
S89-825	1	0.012	0.26	11	112	451	5	420	3.75	21.67	0.017	0.017
S89-826	1	0.035	0.44	23	146	980	17	999	6.84	12.57	0.044	0.044
S89-827	1	0.007	0.57	29	105	609	25	674	6.42	81.43	0.017	0.017
S89-828	1	0.005	0.34	25	147	679	8	600	4.08	68.00	0.012	0.012
S89-829	1	0.002	0.19	117	1476	709	56	335	0.23	95.00	0.013	0.013
S89-830	1	0.004	0.1	6	127	387	5	393	3.09	25.00	0.007	0.007
S89-831	1	0.021	0.21	10	198	831	11	1314	6.64	10.00	0.028	0.028
S89-832	1	0.014	0.28	5	56	432	5	542	9.68	20.00	0.020	0.020
S89-833	1	0.014	0.47	21	359	1266	34	343	0.96	33.57	0.023	0.023
S89-834	1	0.075	2.44	91	719	2700	70	10410	14.48	32.53	0.139	0.139
S89-835	1	0.007	0.91	133	1145	1548	36	4070	3.55	130.00	0.036	0.036
S89-836	3	0.02	0.2	21	176	1113	9	588	3.34	10.00	0.025	0.076
S89-837	3	0.002	0.02	41	818	884	5	121	0.15	10.00	0.007	0.020
S89-838	3	0.074	0.15	14	138	930	10	599	4.34	2.03	0.078	0.235
S89-839	3	0.008	0.19	132	907	1281	23	690	0.76	23.75	0.017	0.051
S89-840	1	0.047	0.33	12	91	1788	17	778	8.55	7.02	0.054	0.054
S89-841	1	0.447	1.57	33	116	14600	190	7480	64.48	3.51	0.489	0.489
S89-842	1	0.045	0.36	13	112	7600	42	1658	14.80	8.00	0.055	0.055
S89-843	1	0.011	0.05	57	913	2900	43	667	0.73	4.55	0.018	0.018
S89-844	1	0.002	0.08	107	1914	1500	12	210	0.11	40.00	0.013	0.013
S89-845	1	0.008	0.27	41	676	1535	19	2061	3.05	33.75	0.020	0.020
S89-846	1	0.074	0.54	15	94	2000	53	1800	19.15	7.30	0.087	0.087
S89-847	1.3	0.017	0.1	18	204	1392	22	620	3.04	5.88	0.021	0.027
S89-848	2.5	0.002	0.1	110	990	864	13	257	0.26	50.00	0.009	0.022
S89-849	3	0.019	0.49	35	203	2200	22	2850	14.04	25.79	0.034	0.102
S89-850	1	0.003	0.06	52	260	292	12	249	0.96	20.00	0.006	0.006
S89-851	6	0.002	0.1	135	971	1045	12	178	0.18	50.00	0.009	0.052
S89-852	2	0.005	0.1	44	480	951	22	792	1.65	20.00	0.011	0.022
S89-853	2	0.004	0.12	36	449	1179	17	632	1.41	30.00	0.010	0.019
S89-854	1	0.007	0.23	20	314	623	7	382	1.22	32.86	0.013	0.013
S89-855	1	0.022	0.38	61	332	4600	29	620	1.87	17.27	0.031	0.031
S89-856	1	0.01	0.22	58	427	817	15	680	1.59	22.00	0.017	0.017
S89-857	5	0.002	0.02	115	724	720	17	226	0.31	10.00	0.006	0.032
S89-858	3	0.002	0.32	162	2761	1407	69	968	0.35	160.00	0.023	0.068
S89-859	1.5	0.006	0.22	120	806	1404	32	1107	1.37	36.67	0.016	0.024
S89-860	1.5	0.002	0.14	60	539	1589	25	531	0.99	70.00	0.008	0.012
S89-861	1	0.013	0.63	145	1058	6200	104	4910	4.64	48.46	0.040	0.040
S89-862	1	0.058	1.46	795	2703	11300	390	11910	4.41	25.17	0.122	0.122
S89-863	1	0.023	0.28	811	10720	10000	363	1441	0.13	12.17	0.084	0.084
S89-864	1	0.058	1.8	132	753	7100	310	13250	17.60	31.03	0.121	0.121
S89-865	1	0.008	0.22	90	1532	1698	168	1237	0.81	27.50	0.022	0.022
S89-866	1	0.021	0.02	33	4530	3500	1450	4600	1.02	0.95	0.055	0.055
S89-867	1	0.037	0.04	47	2433	3900	315	2960	1.22	1.08	0.057	0.057
S89-868	1	0.002	0.26	62	2849	1566	128	414	0.15	130.00	0.021	0.021
S89-869	1	0.005	0.13	86	6010	2900	358	3350	0.56	26.00	0.045	0.045
S89-870	1	0.034	0.3	25	547	2600	42	2700	4.94	8.82	0.048	0.048
S89-871	1	0.012	0.45	11	516	2400	38	1405	2.72	37.50	0.024	0.024
S89-872	1	0.106	0.36	117	11200	6900	725	5040	0.45	3.40	0.179	0.179
S89-873	1	0.174	1.61	30	1499	26500	115	7890	5.26	9.25	0.224	0.224

Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR (Pb/Zn)	ERR (Ag/Au)	ERR (Au equiv.)	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-874	1	0.023	0.42	6	269	1553	17	2011	7.48	18.26	0.035	0.035
S89-875	1	0.036	0.41	13	410	2700	13	2099	5.12	11.39	0.049	0.049
S89-876	1	0.005	0.09	14	424	985	5	592	1.40	18.00	0.010	0.010
S89-877	1	0.002	0.03	19	403	671	5	216	0.54	15.00	0.005	0.005
S89-878	5	0.002	0.02	30	157	61	5	39	0.25	10.00	0.003	0.016
S89-879	8	0.002	0.02	28	37	21	5	30	0.81	10.00	0.003	0.020
S89-880	5	0.002	0.07	33	434	316	20	474	1.09	35.00	0.006	0.032
S89-881	2	0.002	0.07	65	329	699	10	591	1.80	35.00	0.006	0.012
S89-882	2	0.016	0.17	34	92	282	13	743	8.08	10.63	0.021	0.041
S89-883	3	0.011	0.28	247	1064	3000	74	2620	2.46	25.45	0.027	0.081
S89-884	3	0.021	1.09	127	697	4100	102	7050	10.11	51.90	0.058	0.173
S89-885	2	0.009	0.61	35	291	467	16	2790	9.59	67.78	0.026	0.052
S89-886	2.5	0.017	0.86	20	173	369	22	7850	45.38	50.59	0.050	0.125
S89-887	2	0.015	0.78	88	1542	1435	34	10270	6.66	52.00	0.060	0.119
S89-888	22	0.003	0.2	22	267	857	14	612	2.29	66.67	0.009	0.191

Pb/Zn Ag/Au Au equiv.

D13 Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-889	2.5	0.002	0.03	29	808	1809	63	214	0.26	15.00	0.007	0.017
S89-890	1	0.002	0.13	41	790	1499	17	812	1.03	65.00	0.010	0.010
S89-891	1	0.008	0.17	7	129	358	9	1341	10.40	21.25	0.014	0.014
S89-892	1	0.005	0.13	7	85	384	9	774	9.11	26.00	0.009	0.009
S89-893	1	0.015	0.35	23	325	1754	32	1301	4.00	23.33	0.025	0.025
S89-894	1	0.025	0.7	69	792	4200	55	3470	4.38	28.00	0.048	0.048
S89-895	1	0.018	0.53	34	419	1917	33	2520	6.01	29.44	0.034	0.034
S89-896	1	0.012	0.44	30	215	1250	28	2050	9.53	36.67	0.024	0.024
S89-897	1	0.022	0.73	79	385	2000	63	3750	9.74	33.18	0.044	0.044
S89-898	1	0.014	0.43	59	547	1756	36	2930	5.36	30.71	0.030	0.030
S89-899	0.5	0.01	0.45	88	997	1832	36	2750	2.76	45.00	0.028	0.014
S89-900	3	0.007	0.37	8	77	662	12	897	11.65	52.86	0.015	0.045
S89-901	1.5	0.002	0.08	34	183	419	5	239	1.31	40.00	0.005	0.007
S89-902	1.5	0.002	0.17	48	871	578	17	294	0.34	85.00	0.009	0.014
S89-903	3	0.029	0.23	145	404	11400	26	792	1.96	7.93	0.036	0.109
S89-904	3	0.053	0.19	69	335	692	13	356	1.06	3.58	0.058	0.175
S89-905	2	0.15	1.35	133	142	13700	25	1142	8.04	9.00	0.173	0.345
S89-906	1.5	0.008	0.14	54	176	392	5	301	1.71	17.50	0.012	0.017
S89-907	3	0.005	0.02	40	197	480	33	123	0.62	4.00	0.007	0.020
S89-908	2	0.004	0.02	22	125	1823	57	61	0.49	5.00	0.005	0.010
S89-909	2	0.005	0.02	43	168	5100	98	88	0.52	4.00	0.006	0.013
S89-910	2	0.002	0.02	28	97	922	23	48	0.49	10.00	0.003	0.006
S89-911	2	0.002	0.02	29	269	651	51	34	0.13	10.00	0.004	0.007
S89-912	2	0.002	0.02	15	95	234	29	53	0.56	10.00	0.003	0.006
S89-913	2	0.002	0.02	127	319	748	30	47	0.15	10.00	0.004	0.008
S89-914	2	0.021	0.03	71	441	581	100	591	1.34	1.43	0.025	0.050
S89-915	1	0.002	0.05	66	211	877	22	80	0.38	25.00	0.004	0.004
S89-916	1	0.022	0.6	63	243	811	87	851	3.50	27.27	0.034	0.034
S89-917	1	0.007	0.27	30	76	167	41	689	9.07	38.57	0.013	0.013
S89-918	1	0.012	0.58	31	114	385	123	783	6.87	48.33	0.023	0.023
S89-919	1	0.002	0.21	129	336	427	30	192	0.57	105.00	0.007	0.007
S89-920	1	0.002	0.11	224	513	180	12	183	0.36	55.00	0.007	0.007
S89-921	5	0.002	0.12	136	932	140	12	196	0.21	60.00	0.009	0.044
S89-922	5	0.002	0.15	123	974	153	40	363	0.37	75.00	0.010	0.049
S89-923	5	0.002	0.02	18	1071	121	9	51	0.05	10.00	0.008	0.039
S89-924	1	0.005	0.1	46	805	63	28	500	0.62	20.00	0.012	0.012

Pb/Zn Ag/Au Au equiv.

H5 Trench									ERR	ERR	0.000	0.000
Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR	ERR ERR	ERR ERR	ERR ERR
S89-925	4	0.004	0.89	296	2762	2200	66	3370	1.22	222.50	0.039	0.155
S89-926	6	0.048	0.2	25	329	1961	48	471	1.43	4.17	0.054	0.322
S89-927	5	0.038	0.13	44	479	2800	79	462	0.96	3.42	0.043	0.217
S89-928	5	0.114	0.12	18	184	2500	107	838	4.55	1.05	0.119	0.594
S89-929	5	0.049	0.16	29	406	5000	94	473	1.17	3.27	0.054	0.272
S89-930	10	0.063	0.28	70	552	9900	93	732	1.33	4.44	0.072	0.715
S89-931	10	0.033	0.19	96	751	640	107	829	1.10	5.76	0.041	0.415
S89-932	5	0.002	0.04	17	265	425	46	85	0.32	20.00	0.004	0.020
S89-933	10	0.034	0.59	176	911	4600	135	941	1.03	17.35	0.049	0.492
S89-934	14	0.056	1.64	276	1114	4500	224	1651	1.48	29.29	0.089	1.242
S89-935		0.007	0.25	105	638	1186	126	644	1.01	35.71	0.015	0.000
S89-936	10	0.003	1.19	481	1691	1274	103	6120	3.62	396.67	0.044	0.436
S89-937	5	0.083	2	617	1918	11800	479	3550	1.85	24.10	0.130	0.648
S89-938	5	0.019	1.01	509	2275	5500	344	1363	0.60	53.16	0.048	0.239
S89-939	5	0.017	0.02	95	693	2400	176	1347	1.94	1.18	0.024	0.121
S89-940	5	0.045	0.02	115	954	3500	188	632	0.66	0.44	0.052	0.258

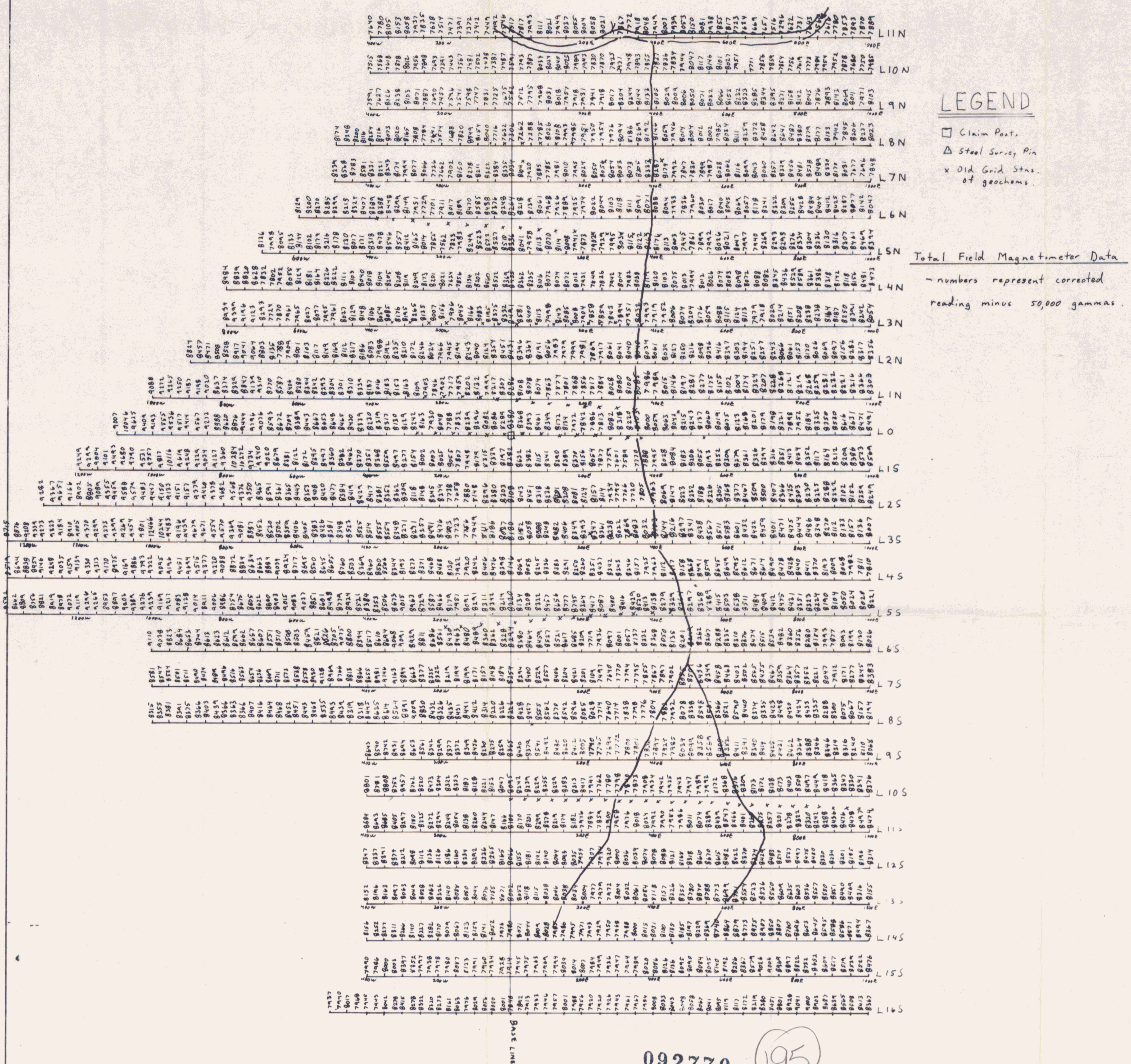
Pb/Zn Ag/Au Au equiv.

Paleo Trench									ERR	ERR	0.000	0.000
Sample	Sample	Au	Ag	Cu	Zn	As	Sb	Pb	ERR	ERR	ERR	ERR
Number	Width	Opt	Opt	PPM	PPM	PPM	PPM	PPM	ERR	ERR	ERR	ERR
S89-955	21	0.005	0.02	24	523	974	15	587	1.12	4.00	0.009	0.197
S89-956	1	0.008	0.02	32	1764	646	36	693	0.39	2.50	0.019	0.019
S89-957	2	0.002	0.02	101	449	800	11	121	0.27	10.00	0.005	0.010
S89-958	1	0.003	0.02	86	363	1156	31	145	0.40	6.67	0.005	0.005
S89-959	1	0.002	0.02	40	324	609	18	208	0.64	10.00	0.004	0.004
S89-960	1	0.002	0.02	46	355	585	26	249	0.70	10.00	0.005	0.005
S89-961	1	0.016	0.69	49	158	553	48	669	4.23	43.13	0.028	0.028
S89-962	1	0.014	0.29	49	191	358	35	290	1.52	20.71	0.020	0.020
S89-963	1	0.009	0.1	37	149	427	34	289	1.94	11.11	0.012	0.012
S89-964	1	0.02	0.02	29	130	395	35	262	2.02	1.00	0.022	0.022
S89-965	1	0.033	0.06	29	76	595	25	280	3.68	1.82	0.035	0.035
S89-966	1	0.011	0.1	22	100	465	17	254	2.54	9.09	0.014	0.014
S89-967	1	0.007	0.05	23	121	434	23	333	2.75	7.14	0.009	0.009
S89-968	1	0.01	0.02	22	114	716	27	253	2.22	2.00	0.011	0.011
S89-969	1	0.01	0.17	23	209	606	50	319	1.53	17.00	0.014	0.014
S89-970	1	0.002	0.04	51	430	1609	29	337	0.78	20.00	0.006	0.006
S89-971	1	0.007	0.08	40	504	1432	31	687	1.36	11.43	0.012	0.012
S89-972	1	0.017	0.16	13	95	741	17	634	6.67	9.41	0.021	0.021
S89-973	1	0.007	0.12	20	162	748	19	458	2.83	17.14	0.011	0.011
S89-974	11	0.006	0.16	19	103	467	22	416	4.04	26.67	0.010	0.108
S89-975	1	0.006	0.03	21	138	651	21	324	2.35	5.00	0.008	0.008
S89-976	1	0.006	0.03	32	182	553	14	300	1.65	5.00	0.008	0.008
S89-977	1	0.007	0.02	42	294	700	12	267	0.91	2.86	0.009	0.009
S89-978	1	0.003	0.02	81	484	894	8	242	0.50	6.67	0.006	0.006
S89-979	6	0.029	0.09	53	376	1983	137	1223	3.25	3.10	0.035	0.211
S89-980	6	0.044	0.93	16	78	579	24	967	12.40	21.14	0.060	0.359
S89-981	1	0.002	0.29	105	459	582	9	96	0.21	145.00	0.009	0.009
S89-982	1	0.022	0.79	30	115	2900	15	1144	9.95	35.91	0.037	0.037
S89-983	1	0.003	0.29	31	237	573	13	176	0.74	96.67	0.009	0.009
S89-984	1	0.002	0.13	55	394	845	12	136	0.35	65.00	0.006	0.006
S89-985	1	0.003	0.15	67	357	681	10	149	0.42	50.00	0.007	0.007
S89-986	3	0.002	0.05	12	237	247	13	146	0.62	25.00	0.004	0.013
S89-987	4	0.002	0.09	128	462	1080	41	258	0.56	45.00	0.006	0.025

Pb/Zn As/Au Au equiv.

Island Trench

Sample Number	Sample Width	Au Opt	Ag Opt	Cu PPM	Zn PPM	As PPM	Sb PPM	Pb PPM	ERR ERR ERR	ERR ERR ERR	0.000 ERR ERR	0.000 ERR ERR
S89-988	3	0.005	0.1	137	56	482	56	87	1.55	20.00	0.007	0.021
S89-989	5	0.002	0.02	38	45	59	11	31	0.69	10.00	0.003	0.013
S89-990	2	0.002	0.06	34	78	223	13	38	0.49	30.00	0.003	0.007
S89-991	5	0.007	0.02	164	101	92	20	66	0.65	2.86	0.008	0.040

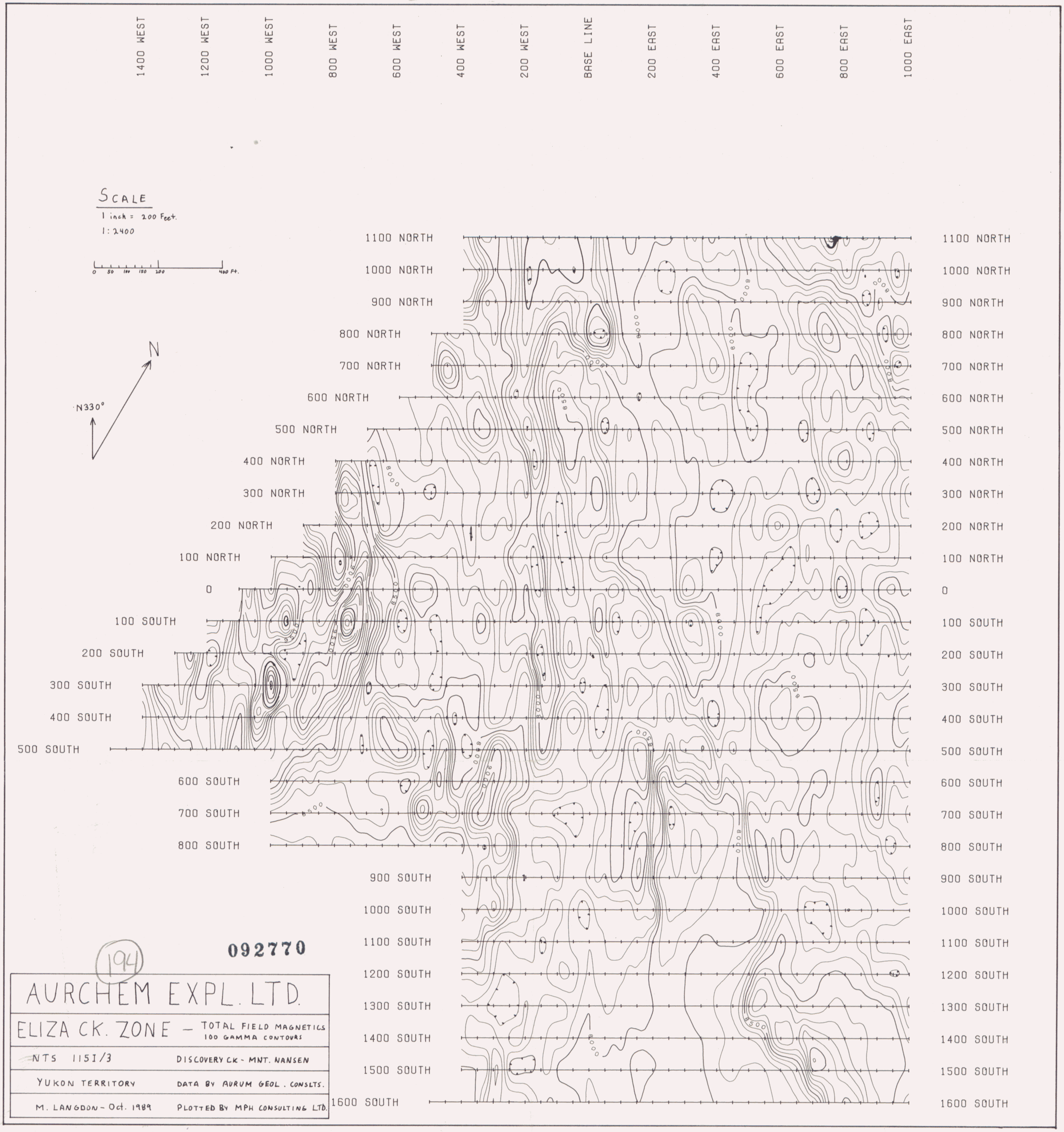


092770 (195)

Scale 1" = 200 Ft.

AURCHEM EXPL. LTD.	
ELIZA CK. ZONE — MAGNETOMETER DATA	
NTS 115I/3	DISCOVERY CK. - MNT. NANSEN
YUKON TERRITORY	Oct. 27, 1989
FIGURE 1	DRAWN BY M. LANGDON

DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



AURCHEM EXPL. LTD.

ELIZA CK. ZONE – TOTAL FIELD MAGNETICS 100 GAMMA CONTOURS

NTS 115I/3 — DISCOVERY CK - MNT. NANSEN

YUKON TERRITORY — DATA BY AURUM GEOL. CONSLTS.

M. LANGDON - Oct. 1989 — PLOTTED BY MPH CONSULTING LTD.

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KEY

— — —	Claim and Lease Boundaries
———	Outer Boundary of Aurchem claims
■	Stakes Located by Aurchem
□	Stakes not yet located by Aurchem

Locations marked by ground distance, not horizontal distance.

092770

AURCHEM EXPL. LTD.

LEASE AND CLAIM BOUNDARIES

NTS.	115 I/3	REGION	Mnt. Nansen
PROV.	YUKON	DATE	June 3, 1988
DATA BY	R. Schneider	DRAWN BY	R. Schneider & K. Ross

Scale

0 200 400 600
FEET
1 INCH = 200 FEET

196

092770

AURCHEM EXPL. LTD.	
ELIZA CK ZONE - CLAIM MAP	
NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	MAP # 3
M. LANGDON	NOV. 1989

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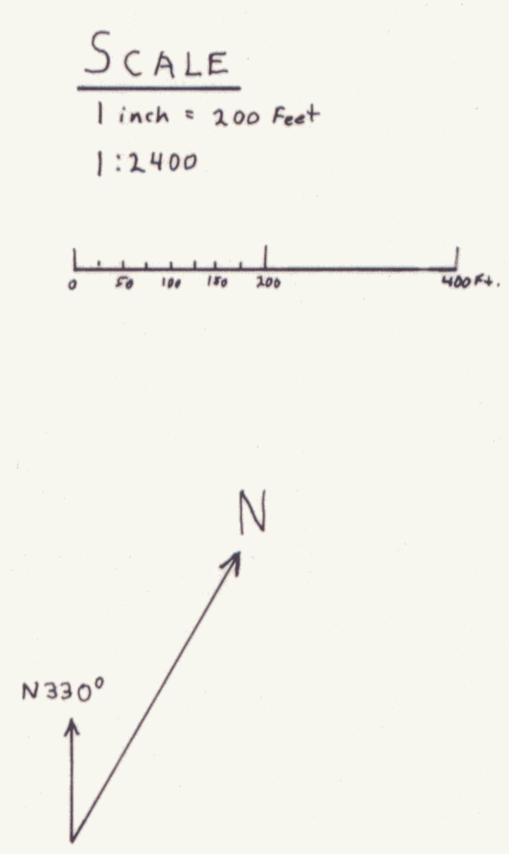
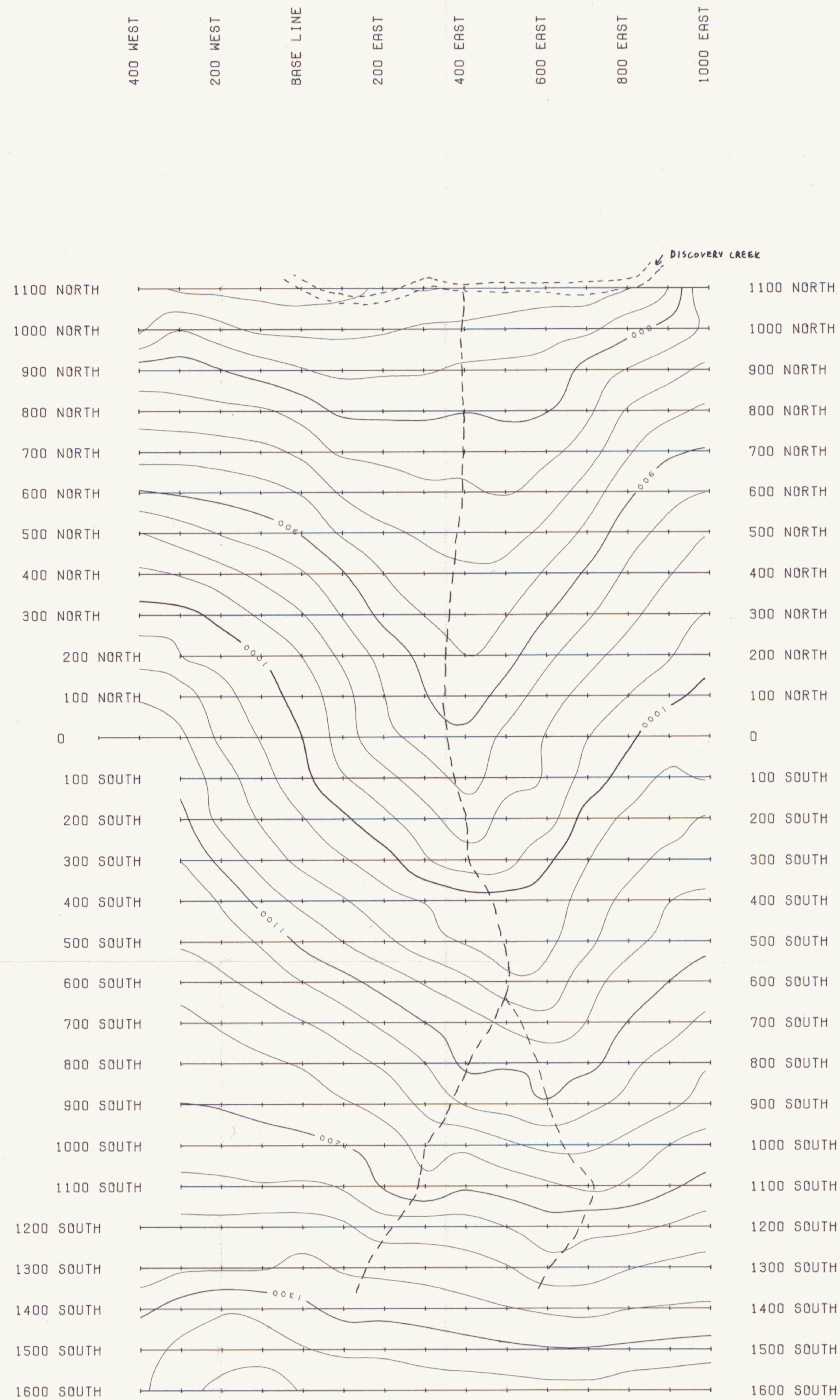
092770

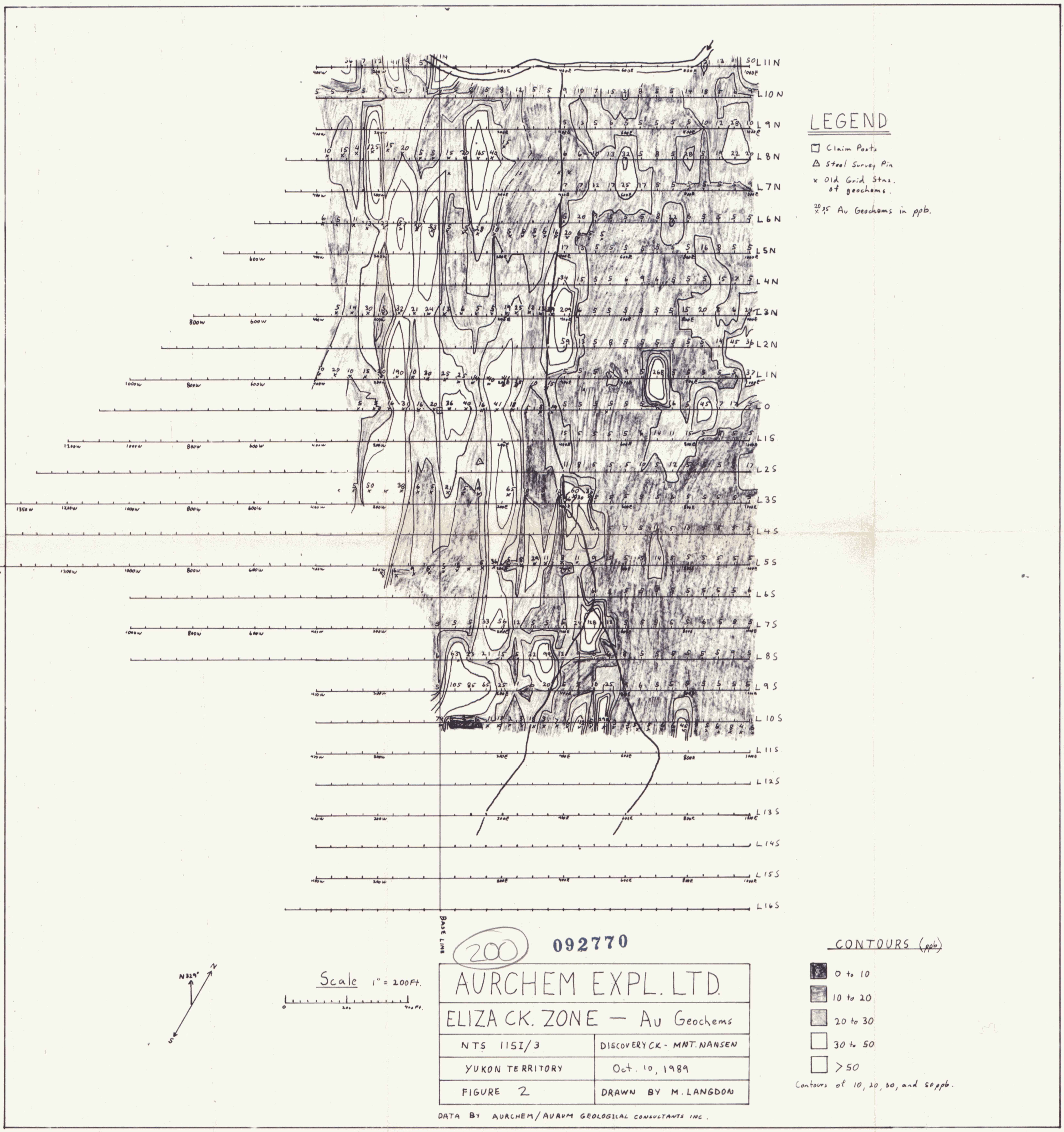
AURCHEM EXPL. LTD.

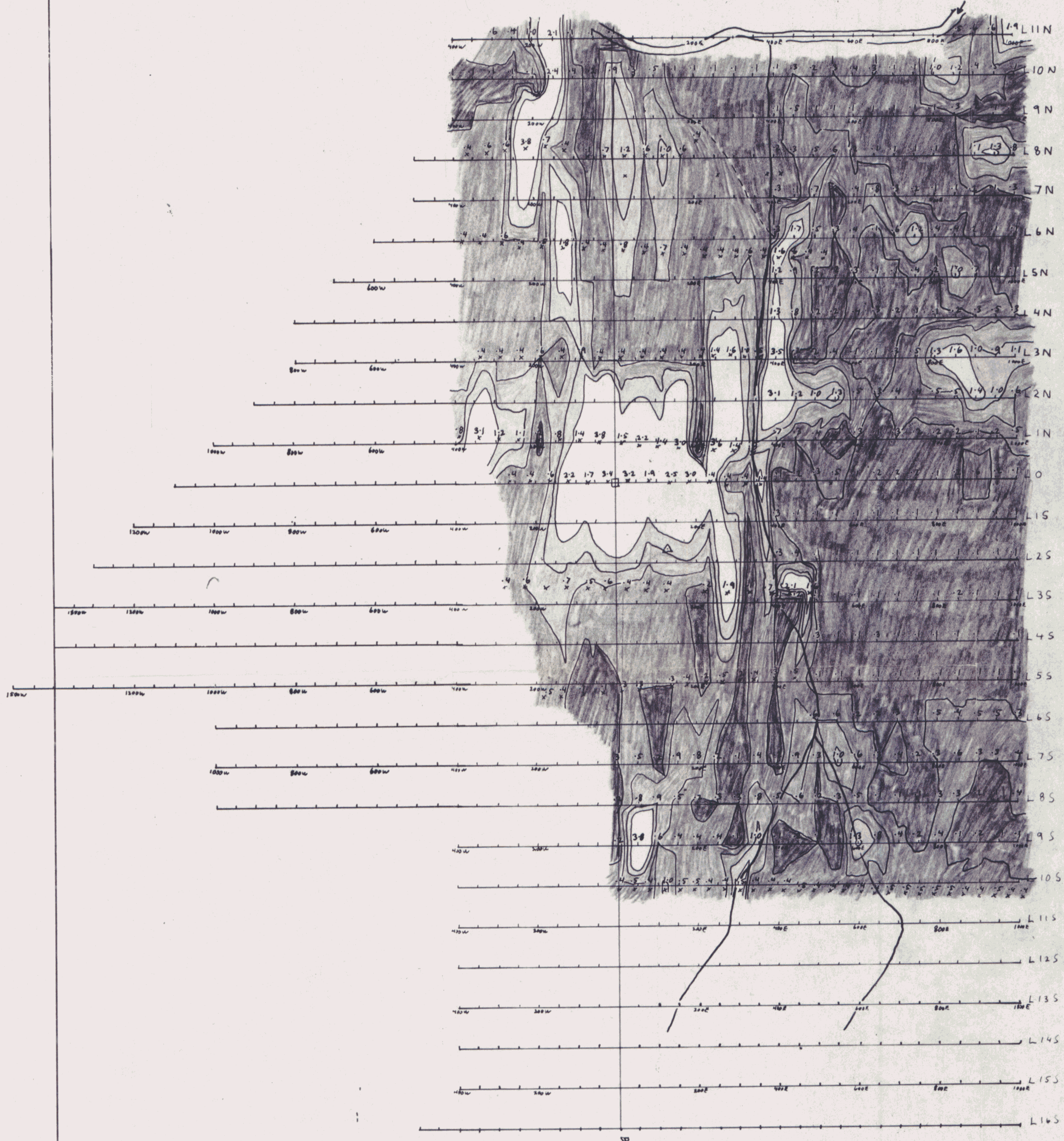
ELIZA CK. ZONE — RELATIVE ELEVATION

NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	DATA BY AURUM GEOL. CONSLTS.
M. LANGDON - Oct. 1989	PLOTTED BY MPH CONSULTING LTD.






LEGEND
Claim Posts
Steel Survey Pin
x Old Grid Stns. of geochems.
Au Geochems in ppb.
BASE LINE
Scale 1" = 200Ft.
CONTOURS (ppb)
0 to 10
10 to 20
20 to 30
30 to 50
> 50
Contours of 10, 20, 30, and 50 ppb.
200
092770
AURCHEM EXPL. LTD.
ELIZA CK. ZONE — Au Geochems
NTS 115I/3
DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY
Oct. 10, 1989
FIGURE 2
DRAWN BY M. LANGDON
DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



LEGEND

- □ Claim Posts
- △ Steel Survey Pin
- x Old Grid Stns. of geochems

Contours - ppm

- < .3
- .3 to .6
- .6 to .9
- .9 to 1.2
- > 1.2

Scale 1" = 200 Ft.

0 200 400 Ft.

N32° N S

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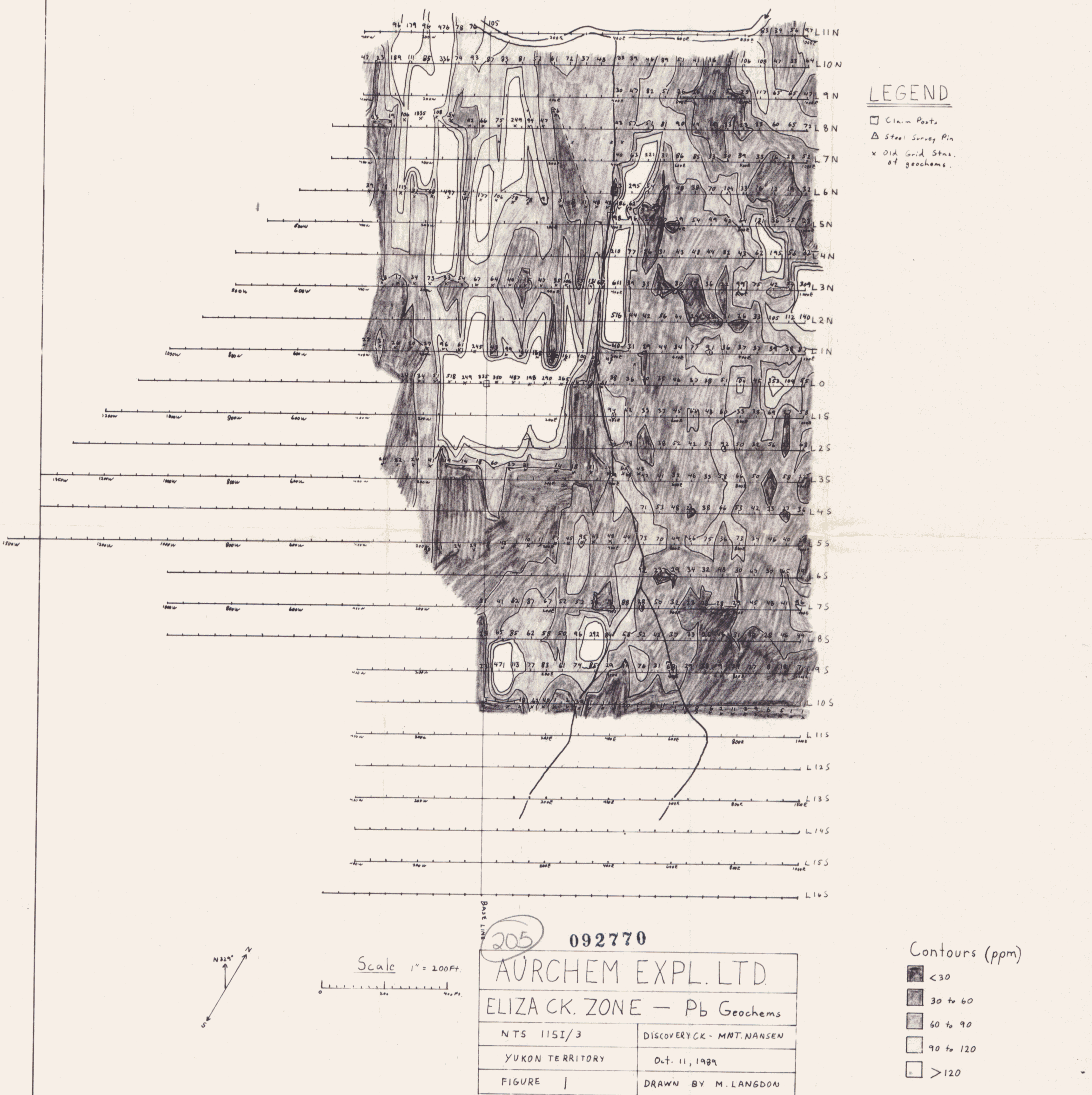
092770

AURCHEM EXPL. LTD.	
ELIZA CK. ZONE — Ag Geochems	
NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	Oct. 12, 1989
FIGURE	DRAWN BY M. LANGDON

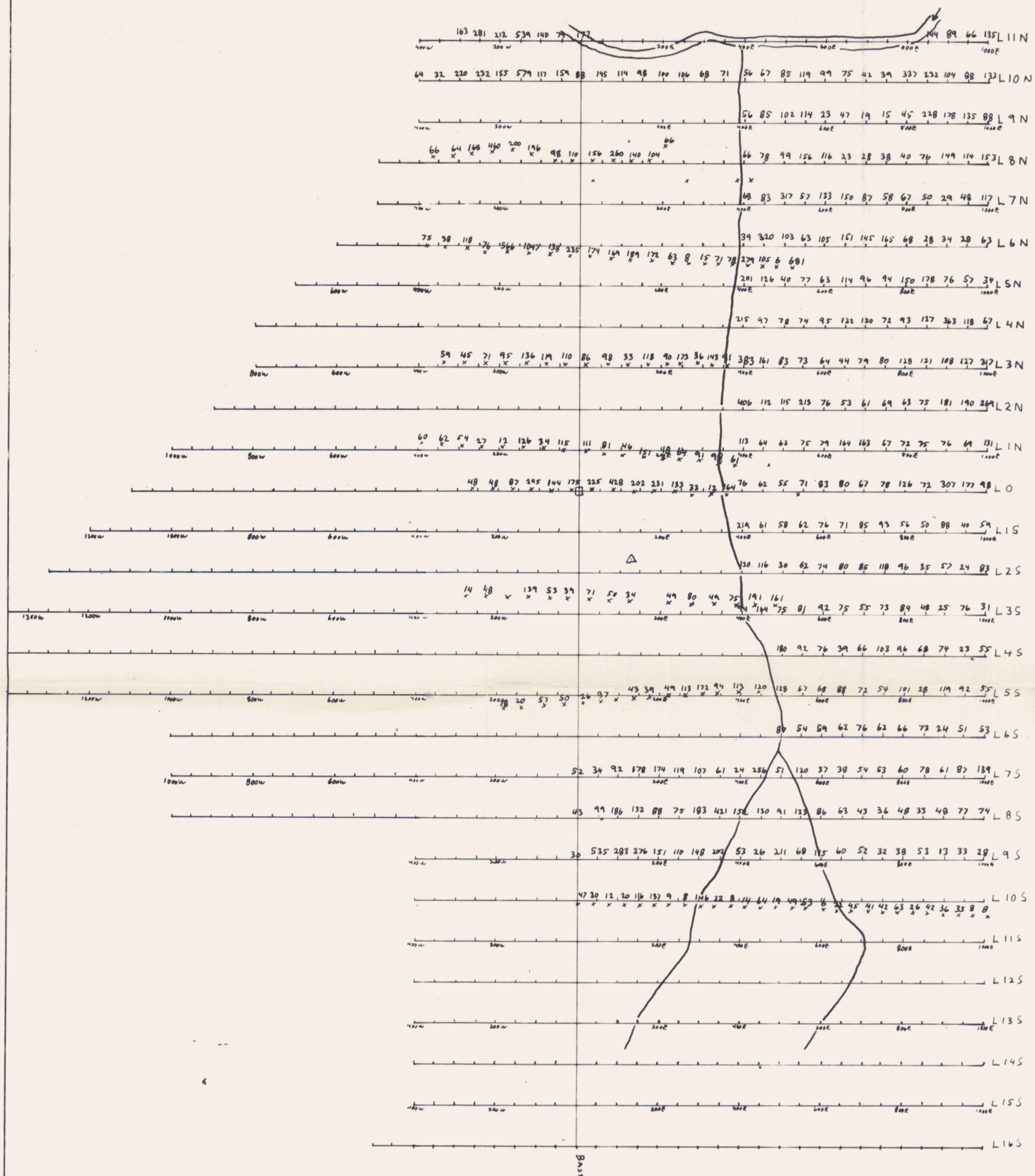
DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



(205) 092770

AURCHEM EXPL. LTD.	
ELIZA CK. ZONE — Pb Geochems	
NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	Oct. 11, 1989
FIGURE 1	DRAWN BY M. LANGDON

DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



LEGEND

- ☐ Claim Posts
- △ Steel Survey Pin
- x Old Grid Stns. of geochems

Scale 1" = 200 Ft.

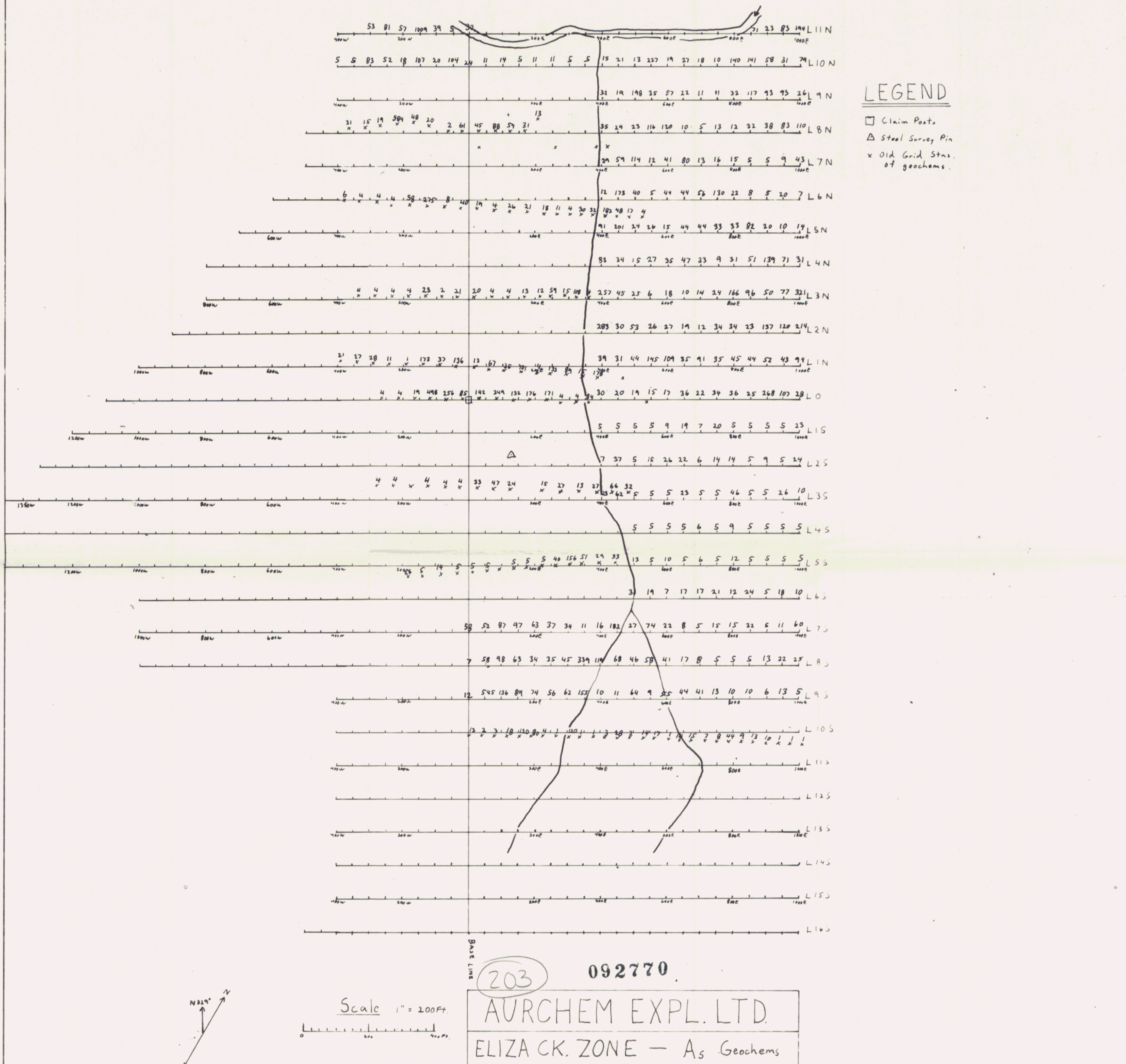
0 200 400 Ft.

N32° N S

(201) 092770

AURCHEM EXPL. LTD.	
ELIZA CK. ZONE — Zn Geochems	
NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	Oct. 12, 1989
FIGURE	DRAWN BY M. LANGDON

DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



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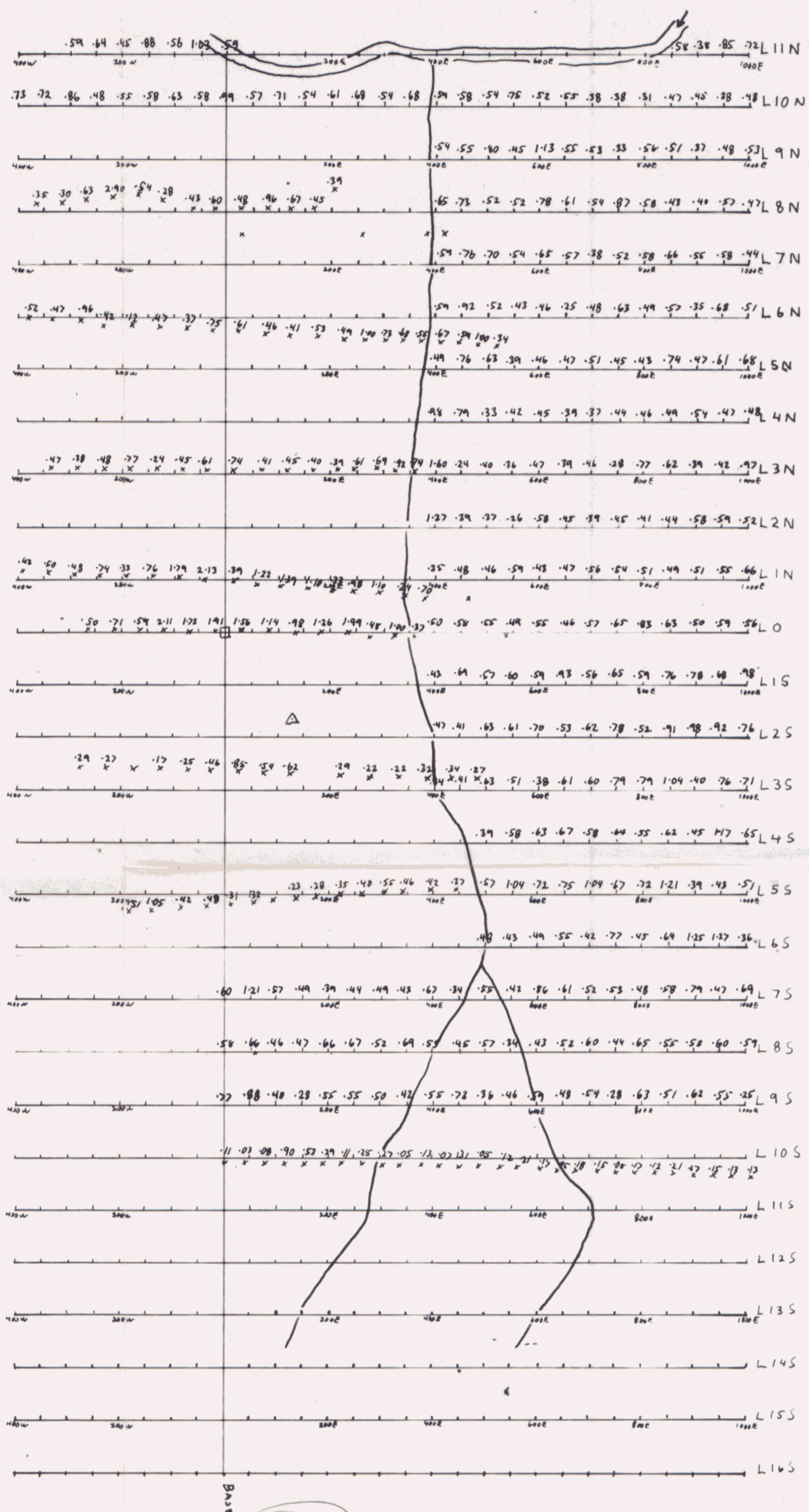
092770

AURCHEM EXPL. LTD.

ELIZA CK. ZONE — As Geochems

NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	Oct. 13, 1989
FIGURE	DRAWN BY M. LANGDON

DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



LEGEND

- ☐ Claim Posts
- △ Steel Survey Pin
- x Old Grid Stns. of geochems.

N329°

Scale 1" = 200 Ft

0 200 400 Ft

202

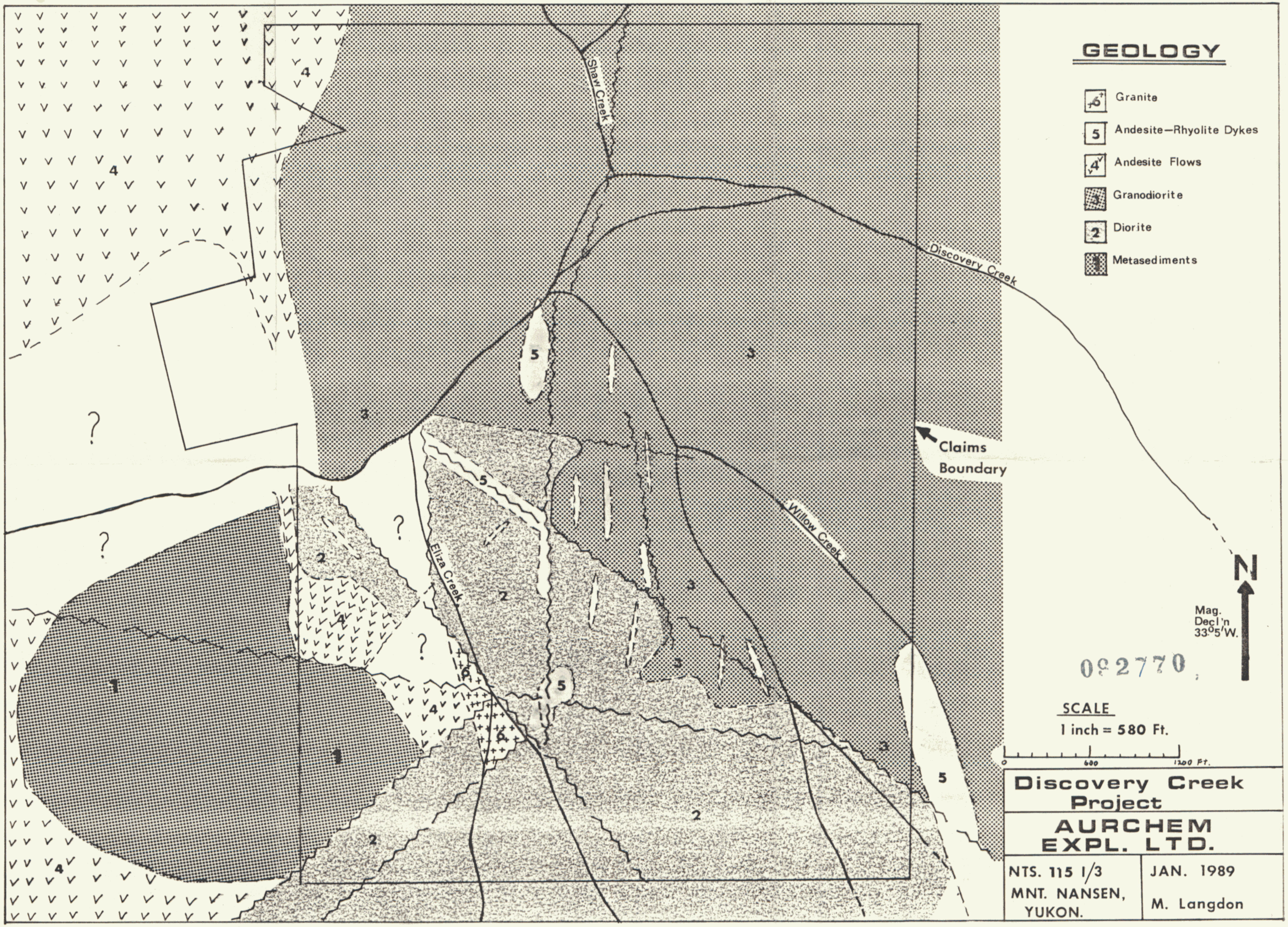
092770

AURCHEM EXPL. LTD.

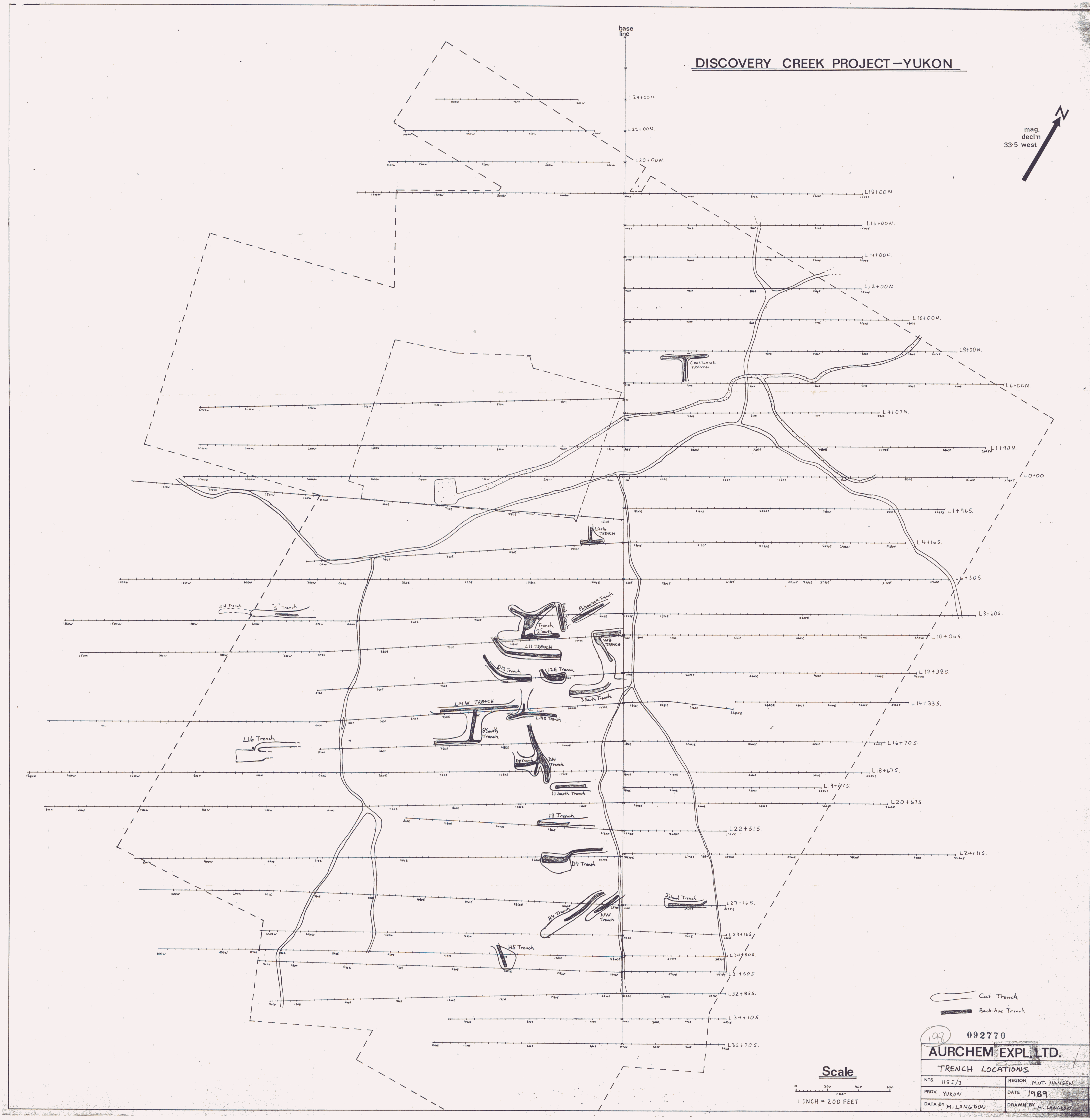
ELIZA CK. ZONE — Pb/Zn Ratio - Geochems

NTS 115I/3	DISCOVERY CK - MNT. NANSEN
YUKON TERRITORY	Oct. 13, 1989
FIGURE	DRAWN BY M. LANGDON

DATA BY AURCHEM/AURUM GEOLOGICAL CONSULTANTS INC.



GEOLOGY
6 Granite
5 Andesite—Rhyolite Dykes
4 Andesite Flows
3 Granodiorite
2 Diorite
1 Metasediments
Shaw Creek
Discovery Creek
Willow Creek
Eliza Creek
Claims Boundary
N
Mag. Decl'n 33°5'W.
SCALE
1 inch = 580 Ft.
0 600 1200 Ft.
Discovery Creek Project
AURCHEM EXPL. LTD.
NTS. 115 I/3
MNT. NANSEN, YUKON.
JAN. 1989
M. Langdon


DISCOVERY CREEK PROJECT—YUKON
base line
mag. decl'n 33·5 west
N
L24+00N.
L22+00N.
L20+00N.
L18+00N
L16+00N
L14+00N
L12+00N
L10+00N.
L8+00N.
L6+00N.
L4+07N.
L1+90N.
L0+00
L1+96S.
L4+16S.
L6+50S.
L8+60S.
L10+06S.
L12+38S.
L14+33S.
L16+70S.
L18+67S.
L19+67S.
L20+67S.
L22+51S.
L24+11S.
L27+16S.
L29+16S.
L30+50S.
L31+50S.
L32+85S.
L34+10S.
L35+70S.
COURTLAND TRENCH
L4+16 TRENCH
Old Trench
"S" Trench
Trench 2 South
Palecreek Trench
W8 TRENCH
L11 TRENCH
D12 Trench
12E Trench
3 South Trench
L14 W TRENCH
L14E Trench
8 South Trench
L16 Trench
D8 Trench
D14 Trench
11 South Trench
13 Trench
D4 Trench
Island Trench
H4 Trench
NW Trench
H5 Trench
Cat Trench
Back-hoe Trench
Scale
1 INCH = 200 FEET
198
092770
AURCHEM EXPL. LTD.
TRENCH LOCATIONS
NTS. 115 I/3
REGION MNT. NANSEN
PROV. YUKON
DATE 1989
DATA BY M. LANGDON
DRAWN BY M. LANGDON