

MAP NO.:	ASSESSMENT REPORT X	DOCUMENT NO:	092635
105 F 15	PROSPECTUS	MINING DISTRICT:	WHITEHORSE, WATSON LAKE
105 K 2	CONFIDENTIAL X	TYPE OF WORK:	GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL
	OPEN FILE		

REPORT FILED UNDER:	Noranda Exploration Co. Ltd.
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DATE PERFORMED:	August 1 - October 7, 1988	DATE FILED:	January 9, 1989
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LOCATION:	LAT.:	62 ⁰⁰ 'N	AREA:	Faro
	LONG.:	132 ⁰⁰ 'W	VALUE \$:	132,000.00

CLAIM NAME & NO.:	RAN 91-146, 153-158, 199-232, 235-304, 307-398, 707-708, 701-794, 796-797, 233-234, 305-306, 475-478, 555-557, 635-636, 795 (YB09068-70, YB12153-8, YB09671-96)
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WORK DONE BY:	G. MacKay
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WORK DONE FOR:	Prime Capital Corporation
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DATE TO GOOD STANDING:	REMARKS: ADJOINS #88 GREW CREEK (ARGO GP)
	Till sampling, surficial and bedrock mapping a ground magnetometer survey were undertaken in 1988. Two areas of anomalous Ag and Hg were found on the west side of the property with values up to 830 ppb Hg, and 1.4 ppm Ag.

GEOLOGICAL, GEOCHEMICAL & GEOPHYSICAL REPORT

on the

ARGO PROJECT

RAN 91-146, 153-158, 199-232, 235-304

307-398, 707-708, 791-794, 796-797

RAN 233-234, 305-306, 475-478, 555-557,

635-636, 795

Whitehorse Mining District

Watson Lake Mining District

N.T.S.: 105 F/15, K/2

Latitude: 62 00'

Longitude: 132 40'



Owned by; Prime Capital Corporation

Operated by; Noranada Exploration Co. Ltd.

(no personal liability)

09 26 35

Gordon MacKay

December, 1988

This report has been examined by
the Geological Evaluation Unit
under Section 53 (4) Yukon Quartz
Mining Act and is allowed as
representation work in the amount
of \$~~59,925.00~~ 132,000.00 *JFB*

J.F. Bremner
for Regional Manager, Exploration and
Geological Services for Commissioner
Yukon Territory.



035832

SUMMARY

Geochemical sampling, geophysics and geological mapping were undertaken over the Argo Project claims in an attempt to discover mineralization similar to that at Grew Creek.

Of the geochemical anomalies discovered, an anomaly in the southeast is most certainly derived from a source well off the property, while two areas of weak mercury/silver anomalies are unexplained.

Geological mapping, though greatly hampered by the extensive overburden, appears to indicate that the property does not lie within the tertiary graben that hosts the Grew Creek deposit.

It is recommended that further work include detailed geochem, prospecting and ground geophysics in the vicinity of, and "Up ice" from, the geochem anomalies. Careful attention should also be paid to the conjugate faults in this area as they are thought to possibly be genetically related to the mineralization at Grew Creek. (Jesse Duke per. com.)

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CHAPTER ONE: INTRODUCTION

1-1: Introductory Statement

The Argo Project lies within the Tintina Trench between Ross River and Grew Creek. The claims were staked in the fall of 1987 to cover ground adjacent to Noranda Exploration/Brenda Mines/ Golden Nevada's Grew Creek Project. In 1988 a program of till sampling, surficial and bedrock mapping and a ground magnetometer survey were conducted.

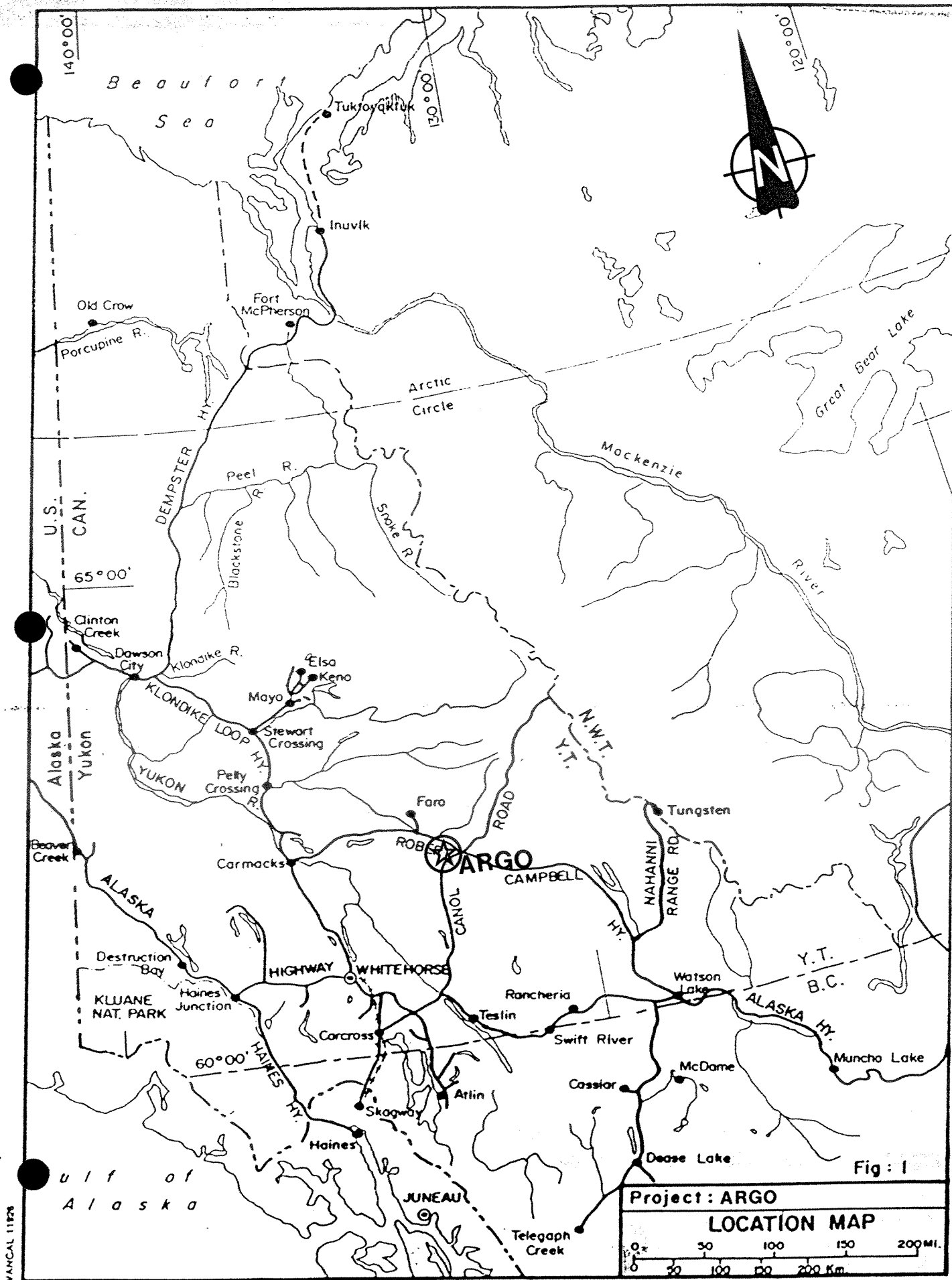
1-2: Location & Access

The property lies southwest of the Robert Campbell Highway and is cut at its southeast end by the South Canal Road 18km from Ross River. The Argo Project encloses the previously staked Grand claims like a large horseshoe that opens to the northwest. Although the property is cut by the South Canal Road and the Robert Campbell Highway, access to the majority of the property is restricted to helicopter. Helicopter access was provided by Trans North Air from Ross River. During work on the property a camp was located on the Lapie River 2km off the Robert Campbell highway.

1-3: Topography & Vegetation

The claims lie along the southwestern edge of the Tintina Trench in the Pelly Mountains. Within the Tintina Trench, topography is characterized by rolling glacial features (drumlins, moraines, etc.) of low relief. Elevation on the property varies between 700 & 975 metres. A fire during the late 1960's destroyed most of the first growth on the claims and the area has been revegetated with poplar, birch and pine. Some mature stands of spruce and pine do remain.

Numerous small pothole lakes cover the property. Drainage by several small creeks is generally to the north into the Pelly River. Major drainages through the claims include Grew, Rat, ^{h-s*} Danger Creek and the Lapie



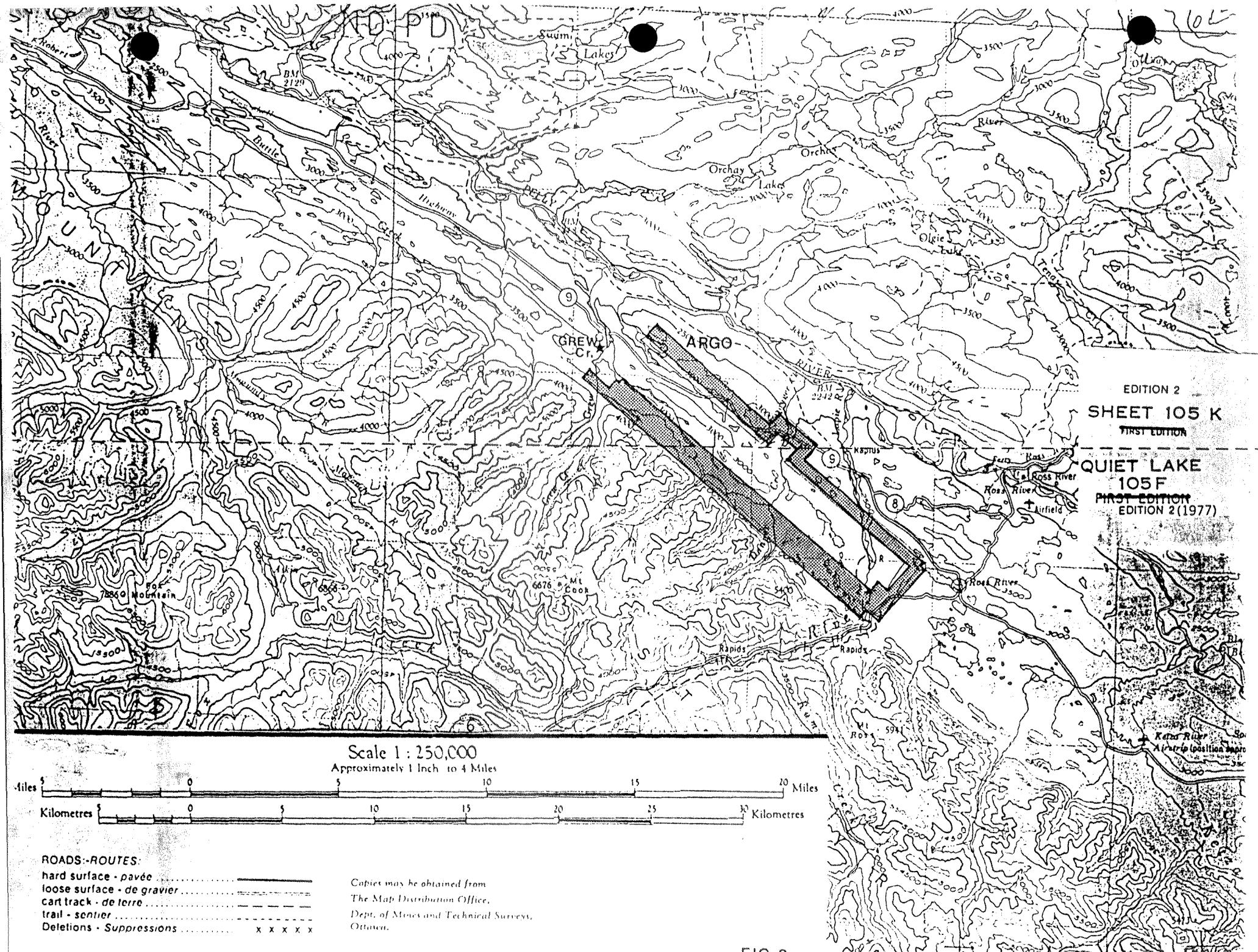


FIG. 2

River.

1-4: History

Exploration in the area was first conducted in the 1800's. Recorded instances of exploration in the area are not known until 1965 when the area east of Grew & Rat Creeks (Tarn Zone) was staked by General Enterprises. EM and IP surveys and three diamond drill holes were completed in that area in subsequent years. Small placer operations have been attempted on Grew Creek proper since the early 1980's.

The first of what is now the Grew Creek property was staked by Whitehorse prospector Al Carlos in June 1983 and optioned to Hudson Bay Exploration and Development later that year. They performed numerous geophysical, geochemical, and geological surveys and diamond drilling (13 holes, 1732 metres), trenching and rotary holes (19 holes, 1660 metres) during the next 3 years. Drilling was concentrated on Grew Creek Main and Tarn zones, whereas other surveys covered the entire property. Hudson Bay dropped the option and it was picked up by Noranda Exploration Company Limited in June 1987.

No recorded instances of work are known for the bulk of the ground now covered by the ARGO project, although some of the claims have been staked in the past.

1-5: Claim Definition

This report covers the following claims;

Whitehorse Mining District

CLAIMS	RECORD NO.s	RECORDED	ANNIVERSARY
RAN 91-146	YB09068-123	Nov. 23, 1988	May 24, 1993
153-158	YB09124-129	Nov. 24, 1988	"
199-232	YB09169-202	Nov. 24, 1988	"
235-304	YB09203-272	Nov. 25, 1988	"
307-398	YB09273-364	"	"
707-708	YB09369-370	"	"
791-794	YB12153-156	"	"
796-797	YB12157-158	"	"

Watson Lake Mining District

CLAIMS	RECORD NO.s	RECORDED	ANNIVERSARY
RAN 233-234	YB09671- 72	Nov. 25, 1987	May 24, 1993
305-306	YB09673- 74	Nov. 25, 1987	"
475-478	YB09973- 76	Nov. 30, 1987	"
555-557	YB09750- 52	Nov. 25, 1987	"
635-636	YB10684 85	Dec. 14, 1987	"
795	YB09896	Nov. 25, 1987	"

Upon acceptance of this report the claims will be in good standing until the anniversary date.

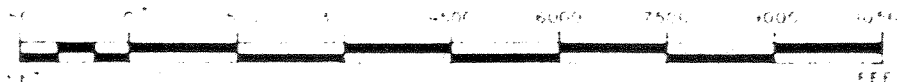
SHEET 105.F-15

QUARTZ & PLACER

LATITUDE 61° 45' to 62° 00'

LONGITUDE 132° 30' to 133° 00'

SCALE 1:31,680



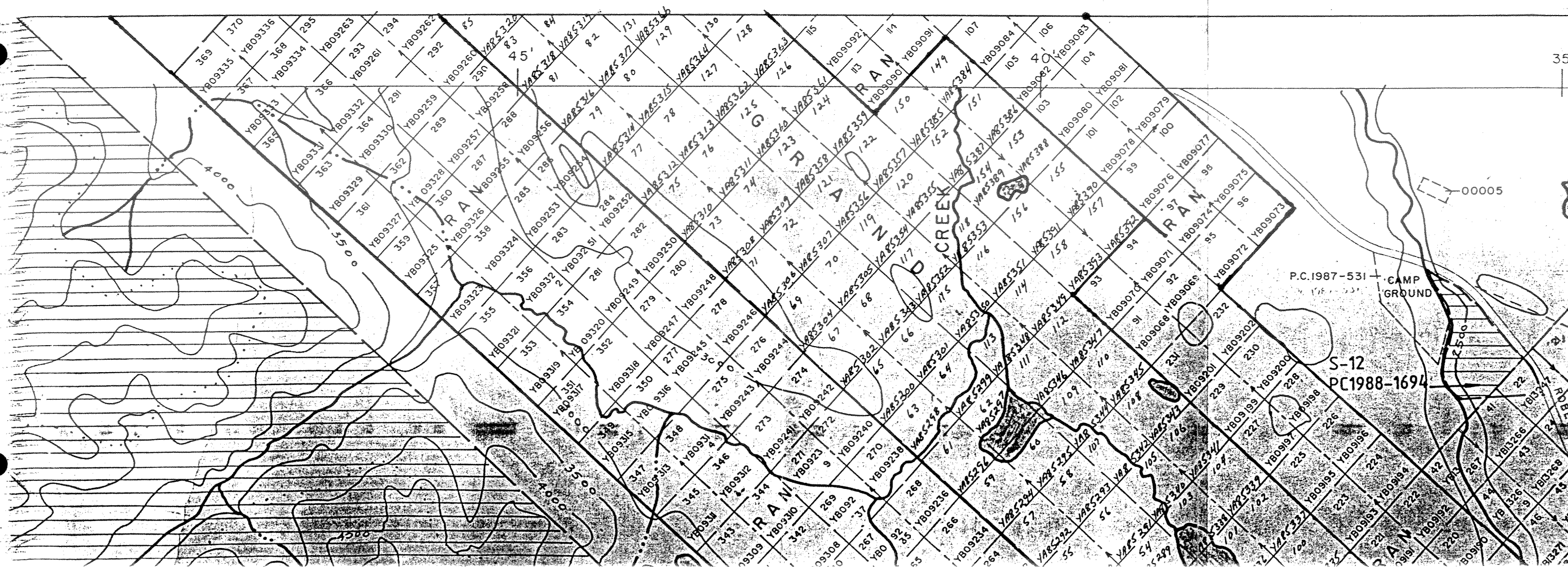
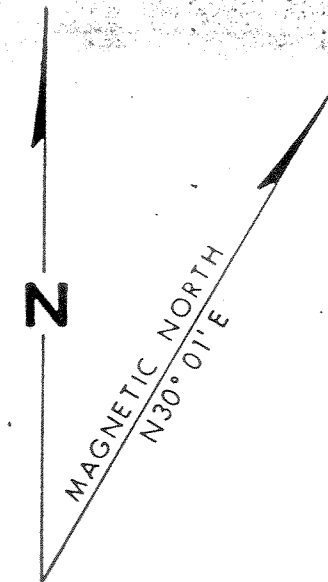
ISSUED UNDER THE AUTHORITY OF THE MINISTER
OF
INDIAN AFFAIRS AND NORTHERN DEVELOPMENT

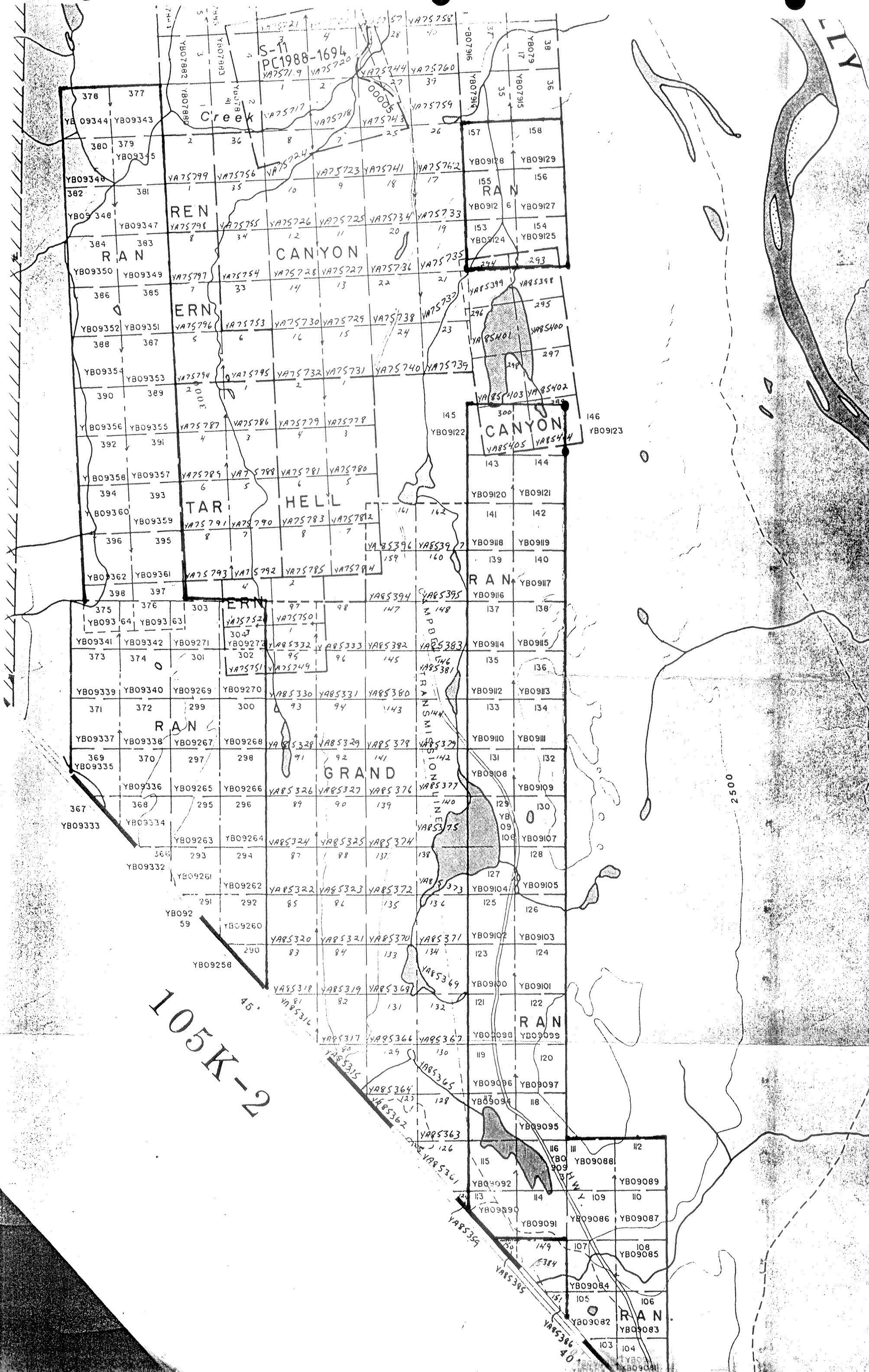
NOTICE

THIS MAP IS ISSUED AS A PRELIMINARY
FOR WHICH THE DEPARTMENT OF INDIAN
AND NORTHERN DEVELOPMENT WILL ACCEPT
RESPONSIBILITY FOR ANY ERRORS, INACCURACIES
OR OMISSIONS WHATSOEVER.

[I.G.] Indian Grave Site

Note: Entry on certain Lands is withdrawn
by P.C. 1988-1694
to facilitate the settlement of Native Land
without prejudice to Existing Surface and
Rights.





S-11
PC1988-1694
YA75719 YA75720

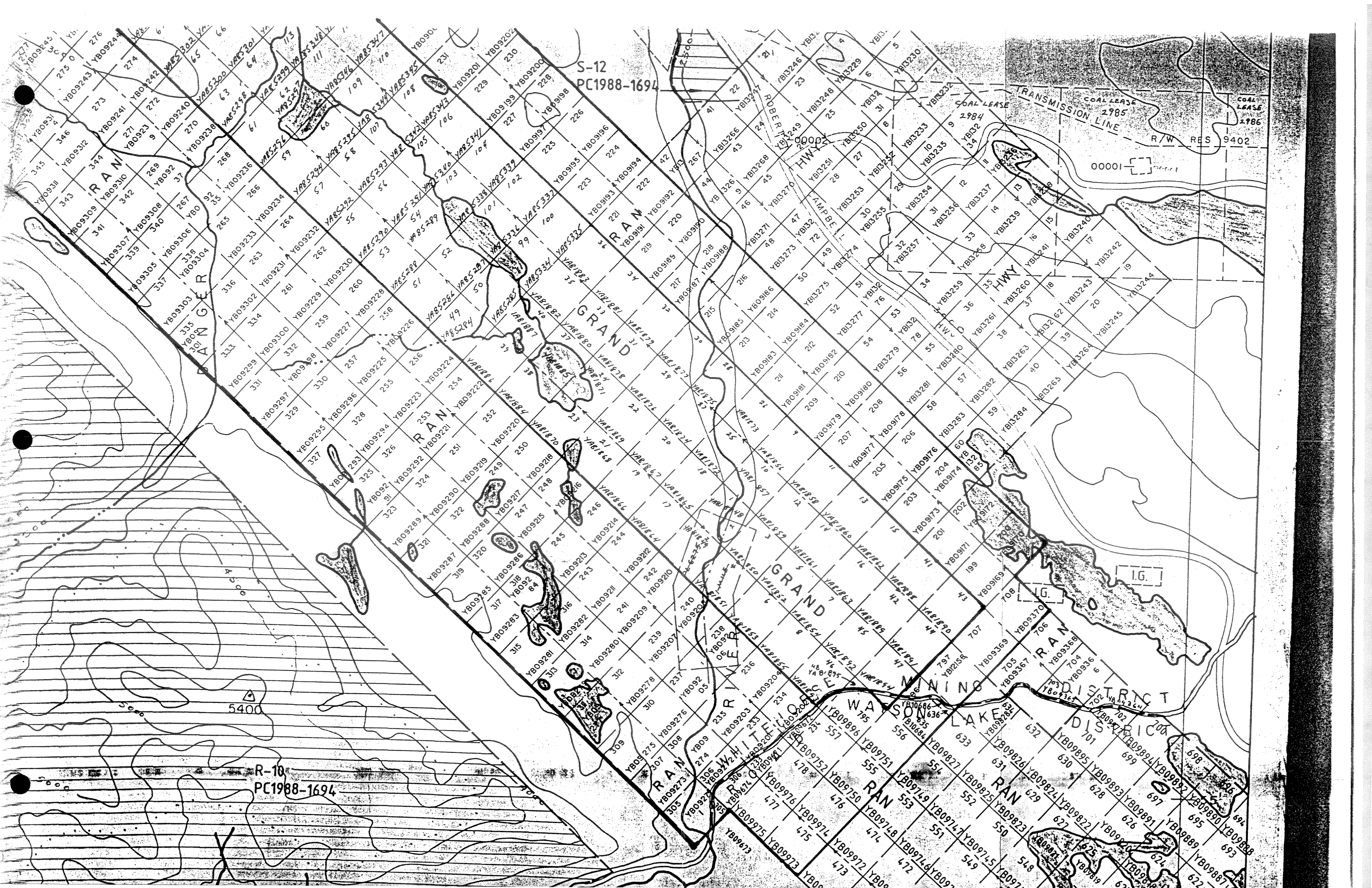
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CANYON

RAN

RAN



1-6: Work Program

In 1988 a program of till, humus and rock sampling (489 samples) surficial and geological mapping, airborne geophysics and ground magnetometer (158 line km) was carried out.

The following personnel were involved;

Gordon MacKay	Geologist
Alain Plouffe	Quaternary Geologist
I. Poliquin	"
S. Reid	Field Geologist
L. Hoover	" Assistant
K. Rogers	" "
S. Keizer	Field Geophysicist
J. Weir	Geophysical Assistant
L. Gagnon	Quaternary Geologist
J. Hoffer	Field Assistant
D. Dempsey	" "
J. Jensen	" "
J. Copland	Cook
M. Tew	Camp Manager
J. O'Rourke	Carpenter

CHAPTER TWO: GEOLOGY

2-1: Regional Geology

The RAN claims lie within the Tintina Trench, a major physiographic feature which reflects the trace of the Tintina fault system. The Tintina fault is a Cretaceous-Tertiary dextral slip transcurrent fault with an estimated horizontal offset of up to 470km.

In the region of the RAN claims the fault separates the tectonic terranes of the Pelly-Cassiar to the southwest from the Anvil Allochthon to the northeast. A Tertiary? extension event along the fault formed a series of grabens northeast of the main fault. These grabens were sites of Eocene? bimodal, volcanic activity. It is these rocks that host the Grew Creek deposit. (Jesse Duke, per. com.).

2-2: Property Geology

2-2-1: Surficial Geology (see fig. 7,8,9) (from Plouffe 1988)

-Till-

Till is the most extensive surficial sediment of the RAN claim blocks. Unleached till in this area is grey, calcareous, silty, and compact. In some profiles where oxidation is predominant, till is reddish to yellowish, non-calcareous, sandy to silty, and less compact. In several localities, especially close to abrupt slopes, till was reworked by processes such as solifluction and slumping. The surficial till throughout the area was deposited during McConnell glaciation.

-Gravel-

Major gravel deposits cover parts of the three properties. These deposits can be subdivided in four categories; (1) modern alluvium, (2) terrace gravel, (3) ice contact stratified drift, and (4) supra-glacial gravel. The texture of these deposits varies tremendously throughout the

Era	Period or Epoch	Formation	Map-unit	Lithology	Thickness
CENOZOIC	Tertiary		15b	Conglomerate, sandstone, shale	unknown
			15a	Basalt	unknown
			14b	Rhyolitic tuff	unknown
			14a	Quartz-feldspar porphyry	
	RELATIONS NOT KNOWN				
	Cretaceous or Tertiary		13	Saundersitized porphyritic hornblende diorite	
	INTRUSIVE INTO UNITS 2, 3 and 11				
	Age unknown		12	Pyroxenitic, hornblende diorite	
	INTRUSIVE INTO UNITS 2 and 3				
MESOZOIC	Cretaceous	Anvil Batholith	11	Porphyritic biotite-quartz monzonite and granodiorite; muscovite-biotite-granodiorite; foliated equivalents	
	INTRUSIVE INTO UNITS 2, 3 and 8				
	Lower or Middle Triassic		10	Conglomerate, shale, sandstone	± 2,000
	UNCONFORMABLE ON UNIT 1				
	Upper Permian or Lower Triassic		9	Serpentinite, peridotite	
	FAULT BOUNDED				
	Upper Permian	Anvil Range Group	8c	Massive resistant recrystallized limestone	± 300
	Lower Permian		8b	Basalt	± 1,500
	Lower Permian and Upper Pennsylvanian		8a	Chert and siliceous tuff	± 2,000
	UNCONFORMABLE ON UNITS 3, 4, 5, 6, 7				
	Upper Devonian and Mississippian		7	Slate, chert, greywacke, conglomerate, limestone	± 10,000
PALEOZOIC	UNCONFORMABLE ON UNITS 3 and 4				
	Middle Devonian		6	Limestone and dolomite	0-100
	Silurian and Devonian		5	Medium-grained ortho-quartzite	50
	CONFORMABLE				
	Ordovician and Silurian		4	Black slate, chert	+400
PROTEROZOIC	UNCONFORMABLE ?				
	Ordovician ?		3	Grey lustrous muscovite phyllite, quartzose phyllite, phyllitic schist, biotite-muscovite schist	4,000?
			3a	Andesitic greenstone, chloritic tuff	
	Cambrian ? and/or Hadrnyian ?	CONFORMABLE ?			
			2	Biotite-muscovite schist, banded quartz-diopside skarn, marble, amphibolite	+2,000?
	BASE NOT SEEN				
	Hadrnyian	'Grit Unit'	1	Muscovite quartzite, graphitic quartzite	?
BASE NOT SEEN					

TABLE 1
Stratigraphic Column of the
Faro - Ross River Area
(Tempelman-Kluit, 1972)

area.

-Glaciolacustrine sediments-

Surficial sediments on certain parts of the property consist of an extensive cover of glaciolacustrine silt and clay. These sediments seem to be confined below 730m a.s.l.. Based on observations made on river bank sections along the Pelly River, they can easily reach a thickness of 10m. Jackson (1986) believes they were deposited in a glacial lake, formed by isostatic downwarping, in front of the retreating McConnell ice. In other areas, isolated pockets of laminated silt and clay are probably related to supraglacial sedimentation.

-Stratigraphy-

The most complete stratigraphic record is exposed along the Lapie and Pelly Rivers.

-Lapie River: The lowest unit exposed at this section is a clast-supported bouldery gravel. It is overlain by a thick till unit defined as pre-McConnell. (Jackson in press). A thick unit of outwash gravels overlies the lower till. An erosional contact separates the outwash gravels from the overlying till which is thought to be of McConnell age. This upper till is overlain by thin cover (1-3m) of outwash gravel.

-Pelly River: The lowest unit at this section is the pre-McConnell till. A sharp contact separates this till unit from the overlying glaciolacustrine sediments. The McConnell till is exposed at this section directly above the outwash gravels from which it is separated by an erosional contact. This upper till is essentially overlain by the same sequence of sediments as the pre-McConnell till (i.e. glaciolacustrine silt and clay, and outwash

gravels). The section is capped by eolian deposits.

Quaternary History

Most of the following is presented in Jackson (in press). The lowest gravel unit exposed along the Lapie River is related to a period of fluvial aggradation prior to the pre-McConnell glaciation. Recession of the pre-McConnell glacier was characterized by the formation of a glacial lake in the Pelly River valley. In other areas, such as the Lapie River valley, the ice front was marked by an open drainage system and the deposition of outwash gravel. Following the isostate rebound, the drainage was reopened in the Pelly River valley prior to the McConnell glaciation. As indicated from the stratigraphic record, the McConnell glaciation was essentially followed by the same events.

Holocene time was marked by the build up of alluvial fans at the foothills of the Pelly Mountains.

-Ice flow patterns-

Ice flow pattern indicators for the pre-McConnell glaciation are limited to till fabrics and pebble counts. Both of these indicators reveal that pre-McConnell ice was flowing west to northwest over the area (Plouffe, in progress).

At the onset of McConnell glaciation, valley glaciers were emanating from major valleys of the Pelly Mountains. This early stage of valley glaciation is clearly indicated by till fabrics and pebble counts. (Plouffe, in progress)

At the maximum of McConnell glaciation the Selwyn Lobe of the Cordilleran ice sheet flowed west to northwest over the area (Hughes et al. 1969). Ice flow direction is clearly indicated from striations, drumlinoid ridges, till fabrics, and pebble counts. As presented by Jackson (in

press), flow patterns of McConnell glaciation was totally controlled by topography. At the termination of the McConnell glaciation, a glacial lake was dammed at 1040 m a.s.l. up into the Lapie River valley (Jackson, in press). Also, clasts such as the Tertiary rhyolite (Tempelman-Kluit, 1977; Jackson et al., 1986) and the South Fork Volcanics (Gordey, 1988; Gordey and Irwin, 1987) were found in till at about 940 m a.s.l.. These clast are coming from bedrock units to the northeast of the Tintina Fault, and therefore had to be transported by ice into the Lapie River valley. From these observations, it is clear that ice flowed up gradient in the Lapie Valley for an unknown period of time during the downwasting of the Selwyn Lobe.

2-3: Bedrock Geology

Bedrock mapped on the Argo claims belongs to the Anvil Allochthonous assemblage.

There are three main areas of outcrop on the property. In the northwest there are large outcrops of the late Paleozoic fine to crystalline limestone. In the southwest and south central portions of the claim block is an area of scattered outcrops of late Paleozoic thin bedded cherts and foliated siliceous tuffs. The third area of outcrop is in the northeast central part of the property and is made up of Pre-Cambrian schist and quartzites.

Summary of units mapped;

Late Paleozoic

- light grey weathering, massive fine crystalline limestone. Locally recrystalized and silicified.
- thin bedded grey, green and red cherts
- thin bedded foliated grey siliceous tuff
- thin bedded to massive grey to black (hornfels?) (siltstone)

Late Pre-Cambrian

-light to dark grey massive muscovite-quartz schist

-micaceous to graphitic quartzite. Locally with clasts of quartz and feldspar.

The southern arm of the property is sandwiched approximately between the Buttle Creek fault and the Grew Creek fault. The northern arm of the property lies approximately between the Danger Creek and the Lapie River faults. These faults are all parallel splays off the main Tintina fault.

Conjugate faults crisscross the property and can be identified from airphoto linears.

CHAPTER THREE: GEOCHEMISTRY

3-11 Procedures

In 1988 a systematic till sampling program was implemented over the Argo properties. In previous studies, till sampling has been found useful in prospecting for gold in glaciated terrain (e.g. Closs and Dado, 1978; Dilabio, 1982a; Kaszycki and Dilabio, 1986). This technique is based on the fact that till is composed of comminuted substratum debris which was transported by the glacier in the down ice direction. Thus, till reflects the nature and geochemistry of the substratum. Further, any geochemical anomaly defined in till can be traced back to its source in the up ice direction. Gravel deposits were not sampled in this program primarily because they do not represent the composition of the local bedrock, and secondly they are often slightly enriched in gold which is concentrated by physical effects during the deposition of the gravel. Glaciolacustrine sediments were not used in geochemical exploration because they generally have a low gold content. Also, it is practically impossible to define a source area for an anomalous sample of such sediment. Alluvial fans identified on ortho maps were not sampled because they are composed of a mixture of debris emanating from outside the claim blocks area and therefore do not reflect the local bedrock.

Samples of unleached and oxidized till were collected in hand dug pits to depth varying between 30 to 70cm (i.e. below the B-horizon). Till exposed in road cuts and river bank sections were sampled at different depths. All samples were collected at 50m intervals along transect lines (perpendicular to baseline) which are trending 040-220, perpendicular to the major ice flow direction (see below). The spacing between each transect line varies between 300 and 1000m.

Based on previous work by Dilabio (1982B, 1985), gold in the till seems

to be concentrated in the silt fraction. Therefore, the $63\ \mu\text{m}$ fraction was recommended for geochemical analysis. Analysis of bulk samples would be found useless in this case since the coarser fraction would have a diluting effect on gold content. At Acme Laboratory in Vancouver the $63\ \mu\text{m}$ separations are costly and time consuming, however the $75\ \mu\text{m}$ separations are performed on a regular basis and therefore are cheaper and faster. For this reason all analysis were done on the $75\ \mu\text{m}$ fraction. Based on results obtained so far this fraction seems to be satisfactory for gold analysis. (Plouffe 1988). A total of 362 till, 103 humus, and 40 rock samples were taken.

All samples were dried in the field and shipped to Acme Laboratories for preparation and analysis. Rocks and humus were treated using standard (-80 mesh) geochemical procedures. Tills were sieved to -200 mesh ($75\ \mu\text{m}$) as previous work has shown gold to concentrate in the silt fractions of the tills. Samples were analysed for Au, Ag, As, and Hg or a 30 element ICP analysis which includes the above four elements.

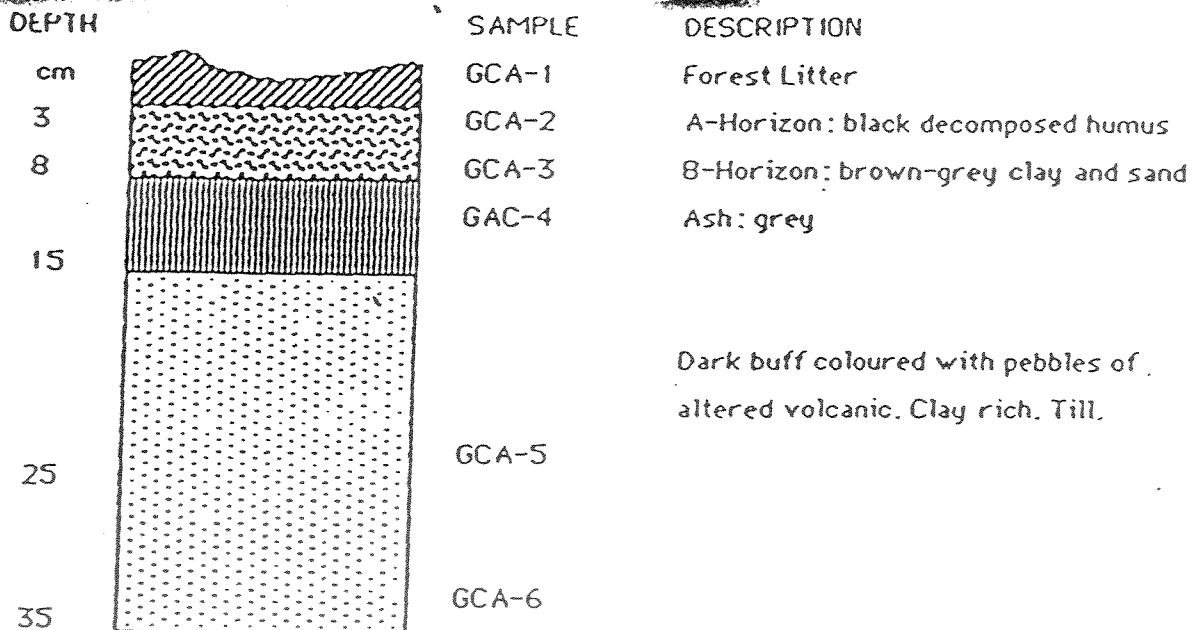
3-2: Results

Extensive soil sampling by Noranda Exploration on nearby properties in the area has given us a standard soil profile for the area summarized on Fig. 14. Mercury and arsenic have traditionally been the best pathfinder elements for Au - Ag mineralization in the area. 1988 results are plotted on figs. 15-30. These are in the form of dot plots showing relative values of each element in till. Complete numerical results have been included in the appendix.

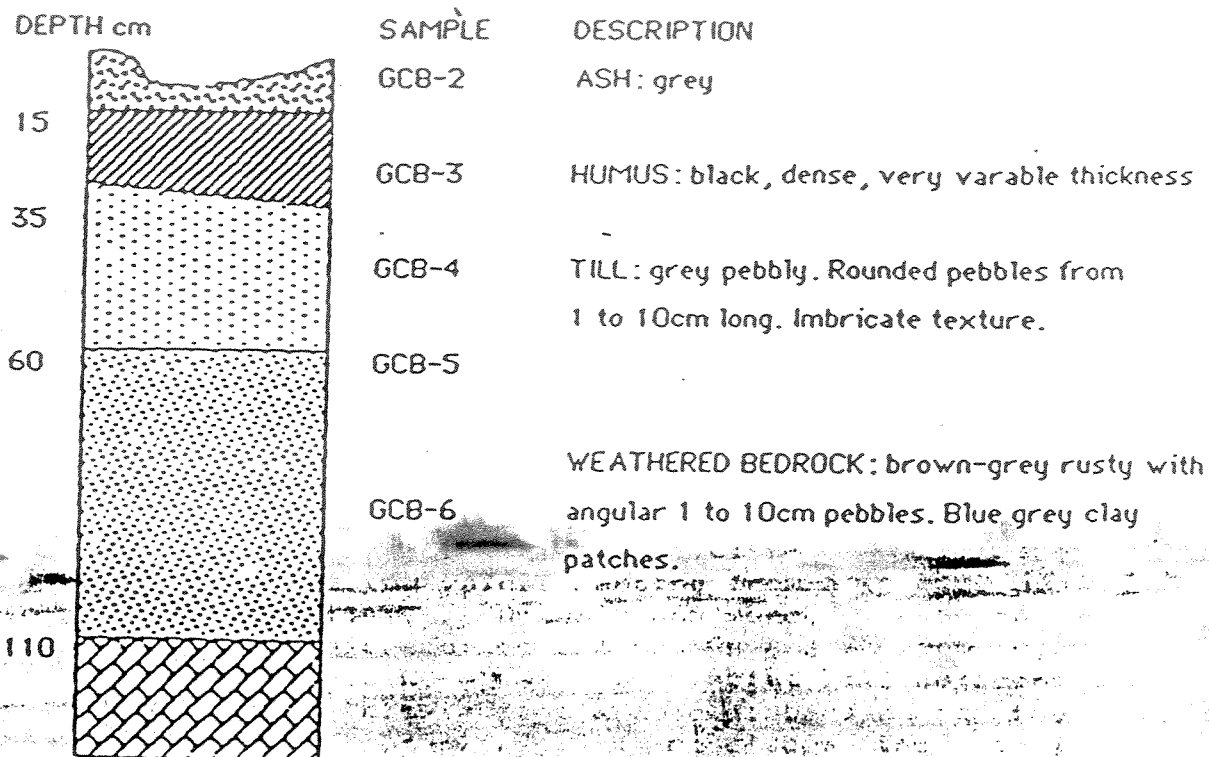
The following suggestions concerning further sampling are from Plouffe 1988.

Gold, silver and arsenic were all quite sporadic. Due to the nature of gold, false anomalies are common in drift prospecting for the element. Most

SAMPLE SITE: GCA SOIL PROFILE



SAMPLE SITE GCB SOIL PROFILE



of these false values can be produced at two levels: (1) in soil profiles as secondary enrichment due to gold mobility, and (2) during analytic procedures where gold particles can get preconcentrated in a subsample because of their high density. Therefore anomalies obtained at the reconnaissance level should be resampled to verify if they are reproducible. As an example, five samples could be collected at and around an anomalous site. During follow-up, this site should be resampled as well as four sites around it, the distance should vary between 10 and 25m depending on the amount of anomalous samples on the same transect line. Typically the angle of spread in the vertical plane of the anomalies is low (5 degrees) and as such would not reach surface for a distance of several 100 metres. Drilling would be necessary to reach the anomaly. In the case of closely spaced anomalies, drilling can be done using either a portable drill or a reverse circulation drill to get deeper unoxidized till samples. Drilling sites should be selected carefully with respect to the ice flow direction and slope orientation. Anomalies defined in till are not likely to be directly over the bedrock source unless the overburden is very thin. It is more likely to find them down-ice with respect to the source. Also, it should be kept in mind that in steep terrain, till was reworked by gravity process such as solifluction and slumping.

Results of geochemical sampling on the Argo claims are initially disappointing. The lack of correlation between gold and its standard pathfinder elements and the overall subtlety of the anomalies are discouraging. However, there does appear to be a good correlation between silver and mercury.

There are two areas of silver mercury anomalies on the property. In the northwest quadrant between L 4000E, 10000N and 2200E 11000N and in the southwest from 9100E to 6400E parallel to the baseline along 50100N. These anomalies are very subtle and the sample intervals are very large in the

along strike (down ice) direction.

The only significant gold anomaly is from samples taken along the Lapie River around 50000N 16600E. Along with the high gold (50 ppb) is more general elevated mercury and silver. The source of this anomaly (up ice) is more difficult to determine because the anomaly occurs in an area where the Lapie River valley glacier enters into the main valley.

Grid Soils Statistics

Grid : Argo

Project : 335

Date : November 17, 1988

 Summary (Note : Reduced avg. excludes all values > 3 S.D.)

	Ag	As	Au	Hg
# samples	362	362	362	362
High	1.4	112	50	832
Low	0.1	2	1	10
Std. Dev.	0.2	8.4	4.2	83.8

Distribution (# of values, n=Avg.)

n + 0-0.5 S.D.	125	250	313	159
n + 0.5-1 S.D.	191	91	21	157
n + 1-2 S.D.	33	15	18	36
n + 2-3 S.D.	9	2	3	6
n + > 3 S.D.	4	4	7	4

Simple Avg.	0.2	12.5	3.0	103.0
Reduced Avg.	0.2	11.6	2.5	97.4

CHAPTER FOUR: GEOPHYSICS

4-11 Magnetometer

A ground geophysics survey was carried out over 158.45 line km on the Argo project on EDA OMNI 4 instrument and base stations were used. The survey was completed on grids with 200m line spacing and 12.5m stations. Data was filtered and plotted by Noranda's Vancouver office.

Contoured magnetometer data is plotted on figures 31, 32 and 33.

Significant magnetic highs in the southeast and northeast map areas may be related to unseen intrusives. The anomaly in the southeast appears to be truncated at both ends by north trending linears.

CHAPTER FIVE: CONCLUSIONS & RECOMMENDATIONS

Geochemical sampling, geophysics and geological mapping were undertaken over the Argo project claims in an attempt to discover mineralization similar to that at Grew Creek.

Of the geochemical anomalies discovered, the anomaly in the southeast is most certainly derived from a source well off the property while the mercury/silver anomalies are unexplained.

Geological mapping, though greatly hampered by the extensive overburden, appears to indicate that the property does not lie within the tertiary graben that hosts the Grew Creek deposit.

It is recommended that further work include detailed geochem, prospecting and ground geophysics in the vicinity of, and "Up ice" from, the geochem anomalies. Careful attention should also be paid to the conjugate faults in this area as they are thought to possibly be genetically related to the mineralization at Grew Creek. (pers. com. Jesse Duke)

Respectfully submitted by;



Gordon MacKay

Geologist

STATEMENT OF COSTS

Labour:	280 man days at \$150/day	\$ 42,000.
Food & Lodging	280 man days at \$60/day	16,800.
Transportation	truck rental & expenses	5,575.
	gas and oil	1,500.
Geochemical Analysis	489 samples @ \$20/sample	9,780.
Magnetometer Survey	158.45 km @ \$125/km	19,806.
Linecutting		27,880.
Report Writing & Drafting		<u>3,200.</u>
	TOTAL	\$138,436.

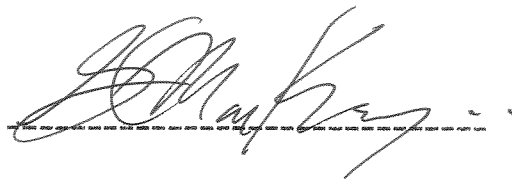
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STATEMENT OF QUALIFICATIONS

I, Gordon MacKay of the City of Whitehorse, Yukon, do hereby certify that:

- 1) I have been an employee of Noranda Exploration Company Limited (NPL) in Whitehorse, Yukon since May, 1988.
- 2) I am a graduate of the University of British Columbia with a B.Sc. in Geology.
- 3) I supervised work on the claims during 1988.



Gordon MacKay

Geologist

APPENDIX 1

Geochem Results

Argo North (SR)

ACME ANALYTICAL LABORATORIES LTD.

DATE RECEIVED: SEP 3 1988

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE(604)253-3158

FAX(604)253-1716

DATE REPORT-MAILED:

Sept. 10/88

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR NG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

ASSAYER: *W. Sefer* D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION PROJECT 8809-013 335 FILE # 88-4207

SAMPLE#	Ag PPM	As PPM	Au* PPB	Hg PPB
R 39747	.1	18	3	810
R 39748	.1	13	1	520
R 39749	.1	5	1	440
R 39750	.2	6	2	130
R 40109	.4	2	4	50
R 40110	.1	3	1	190
R 40111	.1	2	2	60
R 40112	.1	2	1	230
R 40113	.2	2	3	130
R 40114	.1	2	1	190
R 40115	.1	2	1	190
R 40116	.1	2	1	120
R 40117	.1	2	2	460
R 40118	.1	2	1	690
R 40120	.3	4	2	50
R 40121	.1	2	8	50
R 40122	.1	7	1	20
R 40123	.4	49	1	90
R 40124	.5	11	17	150
R 40151	.1	5	1	430
STD C/AU-R	6.9	40	485	1400



NORANDA EXPLORATION PROJECT 8808-086 335 FILE # 88-3799

Page 5

SAMPLE#	Mo	Cu	Pb	Zn	Ag	NI	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	M	Au*	Hg
PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	PPB
R40131	1	6	11	29	.1	9	3	410	2.24	3	5	WD	17	117	1	2	2	4	2.46	.029	25	10	.76	43	.01	2	.36	.02	.21	1	1	5
R40132	7	243	14	36	.4	34	26	179	6.91	7	6	WD	15	12	1	2	3	26	.11	.033	14	35	.46	52	.01	2	.91	.04	.15	1	1	5
R40133	2	11	28	59	.1	18	8	484	2.45	6	5	WD	30	111	1	2	3	4	3.31	.037	25	7	.75	112	.01	6	.34	.02	.23	1	2	5
R40134	1	28	8	50	.1	24	9	377	2.86	6	5	WD	18	7	1	2	2	15	.23	.028	35	22	.42	38	.01	2	.74	.02	.15	2	1	5
R40135	3	20	12	72	.1	23	8	436	3.21	12	5	WD	26	31	1	2	2	26	.31	.013	41	39	1.01	66	.02	2	1.36	.03	.22	1	1	5
R40136	1	42	5	26	.1	4	5	295	2.53	54	5	WD	12	9	1	2	2	12	1.10	.031	14	11	.53	35	.01	2	.89	.03	.10	1	1	5
R40137	3	12	12	26	.1	3	1	58	1.25	156	5	WD	18	15	1	2	3	1	.03	.006	43	8	.01	26	.01	2	.19	.04	.23	1	1	5
R40138	1	23	4	20	1.0	13	5	650	2.69	45	8	WD	6	59	1	2	2	43	14.65	.018	10	25	.24	93	.01	2	.20	.01	.07	1	1	5
R40139	2	54	4	26	.3	34	6	169	2.03	3	5	WD	11	11	1	2	3	30	.42	.021	10	32	.66	125	.04	6	1.09	.03	.49	1	1	5
R40140	4	32	6	33	.5	32	8	303	2.37	20	5	WD	14	8	1	2	2	60	.46	.039	11	65	.82	215	.09	3	1.09	.02	.69	1	1	5
R40141	2	38	27	56	.8	7	6	373	1.76	9	5	WD	19	10	1	2	3	8	.37	.018	28	13	.20	64	.01	2	.38	.03	.20	1	1	5
R40142	1	42	13	95	1.0	58	16	1015	5.07	61	8	WD	11	24	1	2	4	137	3.70	.047	7	137	2.91	233	.10	2	3.39	.02	1.51	1	4	5
R40143	3	16	4	22	.7	25	4	299	1.69	11	5	WD	14	53	1	2	3	24	1.01	.025	14	33	.43	159	.02	5	.51	.01	.35	1	1	5
STD C/AU-R	18	58	38	131	8.2	64	27	936	4.04	38	16	7	40	45	17	15	22	55	.49	.087	39	55	.52	173	.07	34	1.92	.06	.15	12	480	1300

NORANDA EXPLORATION PROJECT 8809-012 335 FILE # 88-4214

Page 3

SAMPLE#	Mo	Cu	Pb	Zn	Ag	NI	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	M	Au*	Hg
PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	PPB
R 40130	1	25	24	57	.1	6	5	390	2.92	5	5	WD	4	24	1	2	7	4	1.20	.011	12	5	.42	29	.01	2	.41	.02	.14	6	1	10
R 40144	1	35	15	99	.1	5	7	581	3.50	2	5	WD	5	34	1	2	2	23	2.48	.108	11	6	1.30	40	.01	2	1.88	.02	.14	1	1	10
R 40145	1	19	13	75	.1	4	4	458	2.74	2	5	WD	3	30	1	2	2	11	3.94	.049	10	5	.82	24	.01	2	1.48	.01	.15	1	1	5
R 40146	1	36	9	70	.1	28	14	388	3.64	2	5	WD	8	19	1	2	2	55	.34	.029	13	39	1.25	178	.13	10	2.33	.05	1.21	1	4	5
R 40147	2	22	11	32	.1	42	12	1878	2.20	39	5	WD	9	5	1	3	2	36	.09	.024	18	25	.57	371	.01	9	.90	.01	.07	2	3	20
R 40148	2	40	12	62	.1	64	23	690	5.90	2	5	WD	4	130	1	2	2	124	4.51	.139	28	156	3.79	125	.17	2	2.87	.12	.37	1	6	5
R 40149	3	42	18	43	.1	4	6	520	2.79	19	5	WD	10	64	1	2	2	10	2.86	.027	20	7	.65	23	.01	2	.94	.02	.16	2	21	5
STD C/AU-R	18	59	42	133	6.9	68	31	1022	4.11	40	18	8	36	47	18	18	23	59	.48	.094	38	57	.97	176	.07	33	2.02	.06	.13	12	480	1300

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR HG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P4 TILL P5 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: AUG 22 1988 DATE REPORT MAILED: Aug 30/88 ASSAYER: D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION PROJECT 8808-086 335 File # 88-3799 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Se PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
ARG 3400 50125	3	5	31	260	.1	34	13	564	3.31	23	5	ND	1	144	1	2	2	48	5.78	.095	20	27	1.24	761	.02	5	1.61	.02	.25	1	5	70
ARG 3400 50200	1	1	14	65	.1	18	6	134	2.69	5	5	ND	6	11	1	3	7	37	.17	.010	25	24	.56	104	.03	3	1.75	.01	.05	1	3	20
ARG 3400 51275	3	3	11	111	.1	37	9	286	2.92	8	5	ND	5	21	1	2	2	47	.27	.035	24	31	.58	437	.02	2	1.51	.01	.12	1	4	40
ARG 3400 51325	2	7	25	130	.2	62	12	420	4.02	14	5	ND	5	29	1	2	2	63	.45	.030	32	42	.78	425	.03	2	1.97	.03	.27	1	9	150
ARG 3400 51375	2	4	19	171	.1	54	11	373	3.39	12	5	ND	4	37	1	2	2	57	.42	.055	25	36	.76	524	.02	8	1.85	.01	.26	1	1	100
ARG 3400 51475	2	5	17	130	.1	56	13	593	4.27	13	5	ND	3	50	1	2	2	62	.70	.038	25	45	1.10	469	.06	10	2.09	.03	.23	1	6	130
ARG 3400 51525	2	4	14	109	.1	52	9	378	3.07	12	5	ND	3	33	1	2	2	53	.52	.053	24	36	.67	621	.03	2	1.56	.01	.13	1	4	150
ARG 4400 50825	4	5	18	184	.1	51	10	588	3.14	14	5	ND	1	94	1	3	2	60	2.71	.109	21	30	1.10	664	.02	6	1.55	.01	.24	1	6	140
ARG 4400 50675	3	5	17	182	.2	47	8	344	2.97	13	5	ND	1	100	1	3	2	58	2.76	.109	19	30	1.06	813	.01	6	1.51	.01	.23	1	1	240
ARG 4400 50500-1	3	4	16	150	.1	45	10	625	3.27	12	5	ND	5	100	1	2	6	42	4.96	.077	22	38	1.15	422	.03	2	1.35	.02	.28	1	2	70
ARG 4400 50300-2	4	5	18	191	.1	50	11	442	3.27	12	5	ND	1	97	1	3	3	56	2.80	.111	20	32	1.13	657	.02	6	1.50	.01	.25	1	1	160
ARG 4400 50300-3	4	6	23	216	.1	55	12	598	3.22	15	5	ND	2	99	2	3	2	64	2.57	.121	20	28	1.05	765	.01	4	1.56	.01	.27	1	1	230
ARG 4400 51025	2	6	15	115	.1	46	8	302	3.13	8	5	ND	4	39	1	2	9	54	.94	.031	24	36	.87	419	.04	5	1.82	.03	.23	1	1	100
ARG 4400 51075	1	20	6	69	.1	30	9	346	2.16	7	5	ND	2	22	1	3	2	35	.34	.033	18	30	.51	339	.03	4	1.26	.01	.13	1	1	50
ARG 4400 51125	2	47	11	114	.4	48	8	479	2.98	14	5	ND	3	58	1	4	2	48	2.48	.049	19	39	.76	450	.03	2	1.45	.02	.19	1	1	120
ARG 4400 51300	2	2	8	98	.1	36	8	271	2.64	11	5	ND	4	44	1	2	8	40	.52	.104	21	31	.63	558	.04	7	1.29	.02	.14	1	3	60
ARG 5400 50275	2	4	12	122	.2	43	9	396	2.80	11	5	ND	2	97	1	2	5	46	3.05	.099	19	34	1.02	735	.03	4	1.54	.02	.21	2	1	160
ARG 5400 50475	2	2	14	103	.2	29	7	231	2.69	12	5	ND	5	27	1	2	2	42	.40	.032	19	29	.58	345	.03	3	1.41	.01	.16	2	1	70
ARG 5400 50575	1	3	12	85	.1	49	9	330	2.75	8	5	ND	1	41	1	2	6	45	.91	.057	23	34	.87	401	.05	2	1.59	.02	.12	1	2	100
ARG 5400 50625	2	1	14	84	.1	29	8	236	2.43	8	13	ND	6	18	1	4	6	40	.27	.032	21	29	.50	491	.02	2	1.55	.01	.06	1	3	30
ARG 5400 50675	1	30	13	74	.1	37	7	510	2.22	9	5	ND	1	90	1	2	2	38	3.74	.064	16	25	.87	572	.03	4	1.14	.02	.11	1	1	70
ARG 5400 50725	2	43	12	71	.2	40	6	331	1.89	6	5	ND	1	105	1	2	2	31	5.92	.087	13	22	.86	595	.02	2	.90	.02	.10	1	4	120
ARG 5400 50775	2	1	12	74	.1	20	7	322	2.38	7	5	ND	4	19	1	2	2	38	.34	.019	16	29	.49	283	.03	2	1.42	.01	.10	1	1	10
ARG 5400 50825	2	2	15	96	.1	34	14	384	4.25	6	5	ND	6	24	1	2	2	51	.45	.033	16	28	.99	527	.15	2	2.63	.04	.41	1	1	20
ARG 5400 51125	2	2	16	76	.1	38	8	273	3.06	12	5	ND	5	23	1	2	6	40	.38	.025	25	34	.53	328	.04	2	1.42	.02	.16	1	1	50
ARG 5400 51225	2	1	8	70	.1	34	9	397	2.32	8	5	ND	3	28	1	2	2	36	.44	.035	21	29	.51	433	.03	8	1.28	.02	.08	1	1	40
ARG 5400 51275	2	3	7	82	.3	41	8	242	2.70	9	5	ND	4	57	1	3	7	44	.71	.031	23	36	.56	491	.04	5	1.97	.05	.13	1	2	120
ARG 6400 50350	5	6	9	223	1.1	54	9	311	2.56	15	5	ND	1	122	1	6	2	48	2.53	.093	18	22	1.00	1084	.01	6	1.08	.02	.21	1	4	150
ARG 6400 50400	2	4	10	98	.4	40	8	281	2.19	20	5	ND	1	65	1	4	7	37	2.06	.097	16	24	.72	498	.02	10	.95	.01	.16	1	1	200
ARG 6400 50450	2	6	19	96	.4	68	14	475	4.15	21	5	ND	5	44	1	3	8	51	.67	.068	24	34	.68	528	.04	2	1.53	.02	.22	1	3	100
ARG 6400 50500	2	4	8	88	.7	37	9	346	2.23	11	5	ND	1	109	1	2	2	37	5.55	.094	14	26	1.08	623	.03	10	1.09	.02	.24	1	1	150
ARG 6400 50550	2	5	14	784	.2	49	10	391	3.56	21	5	ND	1	46	4	2	10	49	.75	.066	21	34	.74	451	.05	2	1.53	.03	.15	1	9	120
ARG 6400 50625	2	5	10	100	.7	38	6	318	2.14	12	5	ND	1	104	1	2	3	36	4.80	.082	14	27	.95	540	.03	7	1.16	.03	.15	1	1	180
ARG 6400 50675	2	4	15	111	.3	42	9	397	2.57	10	5	ND	1	99	1	2	2	46	4.07	.105	18	30	1.09	646	.03	3	1.38	.02	.18	1	1	140
ARG 6400 50750	3	5	14	136	.7	36	11	572	2.72	10	10	ND	5	40	1	2	2	46	.44	.040	20	30	.58	552	.03	2	1.42	.02	.18	1	1	60
ARG 6400 50800	2	4	13	84	.5	44	8	264	2.77	18	5	ND	4	31	1	2	2	44	.59	.044	23	31	.68	490	.03	4	1.38	.02	.12	1	1	120
STD C/AG-S	19	36	132	6.8	67	31	1057	4.19	39	24	8	38	49	18	18	24	59	.48	.091	41	60	.93	181	.07	38	1.95	.06	.17	13	50	1400	

SAMPLE#	PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB	
ARG 6400 50850	2	25	10	98	.2	43	12	567	2.67	10	5	ND	4	45	1	3	2	42	.65	.048	25	29	.63	612	.02	2	1.36	.02	.11	1	2	90
ARG 6400 50900	2	20	9	83	.1	29	12	343	2.47	10	5	ND	4	24	1	3	2	42	.34	.025	20	23	.51	502	.02	2	1.36	.01	.09	1	1	40
ARG 6400 50950	1	41	9	102	.2	35	7	401	2.38	13	5	ND	5	101	1	2	5	41	3.88	.085	18	25	1.05	609	.03	5	1.15	.02	.11	1	1	150
ARG 6400 51000	1	26	12	89	.3	33	12	304	2.38	11	5	ND	2	29	1	3	2	40	.45	.047	20	29	.53	584	.03	6	1.42	.02	.08	1	1	60
ARG 6400 51050	2	55	14	125	.2	53	11	491	2.94	14	5	ND	5	33	1	2	5	50	.72	.051	24	33	.75	714	.03	4	1.56	.01	.13	1	1	140
ARG 6400 51100	2	49	12	118	.6	44	9	384	2.71	13	5	ND	4	62	1	2	2	48	1.52	.090	21	29	.81	623	.02	7	1.43	.02	.13	1	1	200
ARG 6400 51150	2	42	8	166	.2	43	10	439	2.76	14	5	ND	6	72	1	3	2	48	2.04	.093	20	29	1.09	700	.03	8	1.35	.02	.16	1	1	100
ARG 6400 51200	1	24	10	84	.3	29	8	526	2.29	9	5	ND	3	34	1	2	4	39	.75	.062	20	26	.60	472	.04	5	1.11	.32	.08	1	1	50
ARG 6400 51250	2	37	13	126	.2	35	7	401	2.38	12	5	ND	5	96	1	2	2	41	2.89	.089	18	25	.96	634	.03	4	1.12	.02	.12	1	1	90
ARG 6400 51350	2	33	17	164	.3	46	11	429	3.06	15	5	ND	6	55	1	2	4	53	1.20	.098	22	33	.91	455	.03	10	1.55	.02	.16	1	1	60
ARG 6400 51400	1	16	11	140	.2	25	10	381	2.11	7	5	ND	2	45	1	2	2	35	.79	.068	15	24	.53	325	.03	8	1.07	.02	.09	1	1	140
ARG 7200 50350	1	31	14	76	.3	31	6	338	2.02	12	5	ND	3	85	1	2	3	32	3.00	.061	16	23	1.04	582	.03	4	.99	.02	.09	1	1	100
ARG 7200 50400	2	24	10	82	.1	30	11	304	2.37	11	5	ND	4	22	1	2	2	40	.35	.026	22	27	.51	482	.03	4	1.30	.01	.09	1	1	30
ARG 7200 50450	2	35	11	80	.2	41	9	305	2.52	11	5	ND	4	35	1	2	3	41	.75	.055	24	26	.66	468	.03	6	1.30	.02	.11	1	1	90
ARG 7200 50500	2	31	13	84	.4	39	10	385	2.71	12	5	ND	5	36	1	2	6	41	.71	.035	25	30	.79	484	.04	6	1.32	.02	.11	1	1	80
ARG 7200 50550	2	41	11	90	.4	39	8	323	2.56	14	5	ND	3	52	1	3	4	40	1.29	.085	20	27	.87	496	.03	7	1.21	.02	.12	1	1	110
ARG 7200 50600	2	37	8	91	.4	39	8	282	2.73	18	5	ND	5	37	1	2	2	46	.77	.051	24	30	.62	502	.03	7	1.42	.01	.11	1	1	120
ARG 7200 50650	2	28	12	90	.1	35	11	304	2.86	17	5	ND	7	23	1	2	3	39	.32	.039	27	32	.57	340	.04	14	1.20	.01	.11	1	1	30
ARG 7200 50700	3	37	12	102	.2	39	10	280	2.78	13	5	ND	5	25	1	2	5	45	.48	.032	25	27	.56	415	.03	3	1.25	.01	.16	1	1	80
ARG 7200 50750	3	42	15	121	.4	49	10	391	3.15	19	5	ND	5	31	1	2	4	56	.47	.068	24	32	.62	472	.02	8	1.52	.01	.18	1	1	100
ARG 7200 50800	3	38	19	125	.2	45	11	339	3.28	20	5	ND	7	23	1	4	4	55	.32	.044	28	31	.56	538	.02	7	1.58	.01	.18	1	1	60
ARG 7200 50875	2	28	12	119	.2	35	11	288	2.53	12	5	ND	3	29	1	2	4	41	.49	.052	23	26	.52	517	.02	5	1.24	.01	.09	1	3	70
ARG 7200 50925	2	35	10	103	.3	31	7	224	2.76	11	5	ND	5	23	1	2	4	74	.44	.037	24	38	1.18	477	.05	11	1.80	.01	.12	1	1	90
ARG 7200 50975	2	18	13	92	.1	28	10	187	2.51	13	5	ND	4	22	1	3	2	35	.33	.034	20	25	.50	300	.03	4	1.16	.01	.11	1	1	20
ARG 7200 51025	3	32	12	105	.2	36	10	262	3.00	14	5	ND	5	26	1	3	2	50	.39	.039	25	31	.58	466	.02	8	1.47	.01	.14	1	1	100
ARG 7200 51100	2	26	9	88	.2	34	10	244	2.49	12	5	ND	5	23	1	3	2	43	.36	.038	23	28	.48	514	.02	4	1.37	.01	.10	1	1	70
ARG 7200 51150	2	24	14	97	.4	31	11	256	2.71	11	5	ND	6	27	1	2	2	48	.44	.033	22	30	.64	421	.02	8	1.38	.01	.13	1	1	90
ARG 7200 51200	2	43	14	125	.4	44	7	371	2.48	16	5	ND	5	95	1	2	6	47	3.64	.086	17	27	1.14	677	.03	9	1.30	.02	.15	1	1	130
ARG 7200 51250	3	43	16	151	.3	39	10	602	2.61	20	5	ND	6	91	1	2	2	44	2.73	.067	21	24	1.03	645	.01	7	1.19	.01	.17	1	1	100
ARG 7200 51425	3	25	15	137	.3	31	9	252	3.02	13	5	ND	6	42	1	2	2	47	.64	.084	23	30	.71	444	.03	14	1.37	.01	.14	1	1	70
ARG 8200 50075-1	3	41	12	157	.3	36	8	383	2.55	17	5	ND	6	115	1	3	2	43	3.21	.090	18	25	1.34	755	.03	6	1.10	.02	.14	1	1	110
ARG 8200 50075-2	3	35	10	150	.7	33	7	377	2.31	13	5	ND	6	128	1	2	2	45	3.74	.087	16	26	1.27	837	.03	5	1.15	.02	.17	1	1	260
ARG 8200 50075-3	3	41	10	163	.4	36	7	407	2.45	14	5	ND	6	117	1	2	4	47	3.73	.086	17	24	1.23	828	.03	6	1.18	.02	.18	1	1	130
ARG 8200 50125	5	48	13	206	.4	48	8	370	2.39	16	5	ND	4	108	2	4	2	51	3.49	.082	19	21	.90	1027	.01	7	1.13	.01	.15	1	1	90
ARG 8200 50175	7	56	13	355	.6	64	8	328	2.97	18	5	ND	6	76	2	3	2	47	2.40	.087	22	21	1.06	877	.02	3	1.17	.01	.16	1	1	80
ARG 8200 50425	1	27	10	54	.2	24	6	241	1.78	11	5	ND	5	187	1	2	2	16	11.57	.064	13	14	1.44	801	.02	4	.77	.02	.06	1	1	60
STD C/AU-S	18	55	38	133	6.7	67	28	1081	4.09	44	16	7	37	47	18	16	20	58	.48	.081	40	57	.92	176	.06	33	1.95	.06	.13	12	47	1300

SAMPLE#		Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Si	Z	W	Au*	Hg	
		PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPB	PPB		
ARG 8200 50550	2	4	7	113	.3	56	9	462	2.12	17	5	ND	2	39	1	2	2	51	.80	.053	23	34	.85	557	.03	11	1.50	.02	.14	1	7	150
ARG 8200 50653	2	10	16	116	.5	55	3	441	3.46	15	5	ND	3	57	1	2	2	56	.76	.058	29	45	.37	689	.06	2	1.34	.02	.14	1	1	170
ARG 8200 53700	2	13	14	83	.4	43	10	410	2.67	18	5	ND	4	28	1	4	2	44	.62	.027	27	31	.63	427	.03	8	1.28	.02	.10	1	1	100
ARG 8200 50800	1	14	8	79	.5	33	7	290	2.10	11	5	ND	1	158	1	2	2	29	9.02	.077	11	21	1.27	737	.02	5	.89	.02	.08	1	1	150
ARG 8200 50850	1	14	12	78	.6	35	6	301	1.39	9	5	ND	2	174	1	4	2	30	8.32	.062	11	21	1.65	767	.02	2	.96	.02	.11	1	3	220
ARG 8200 50950	1	13	6	94	.4	34	7	365	2.26	11	5	ND	1	80	1	2	2	36	3.28	.032	17	24	1.05	573	.03	4	1.11	.02	.10	1	1	120
ARG 8200 51000	1	17	14	88	.7	35	6	277	2.34	9	5	ND	1	139	1	2	2	35	5.15	.059	12	23	1.38	856	.02	9	1.11	.02	.14	1	2	160
ARG 8200 51175	2	40	11	116	.7	44	7	341	2.96	15	5	ND	3	61	1	2	2	52	1.36	.046	23	31	.91	614	.03	2	1.59	.02	.13	1	1	100
ARG 8200 51225	2	60	17	146	.6	53	11	455	3.09	18	5	ND	2	64	1	2	2	60	2.06	.081	21	33	.89	641	.01	7	1.58	.01	.17	1	2	150
ARG 8200 51275	2	37	15	126	.6	46	10	379	3.30	14	5	ND	4	43	1	2	2	57	.52	.053	25	35	.74	671	.02	6	1.70	.01	.14	1	1	90
ARG 9075 50875-1	3	11	8	156	.5	38	8	458	2.45	12	5	ND	4	120	2	2	5	43	4.66	.036	15	21	1.32	712	.02	5	1.05	.01	.13	1	1	100
ARG 9075 50875-2	2	12	12	145	.4	40	8	510	2.50	12	5	ND	5	115	1	3	3	40	4.91	.077	16	22	1.50	605	.02	6	1.13	.01	.18	1	1	80
ARG 9075 50900	3	11	14	157	.5	39	8	556	2.49	39	5	ND	4	131	2	2	2	42	5.03	.036	12	21	1.56	246	.02	6	1.07	.01	.19	1	1	70
ARG 9075 50925	3	13	14	156	.6	55	10	504	2.44	30	5	ND	4	126	1	2	2	41	5.25	.079	14	23	1.46	556	.02	4	1.05	.01	.18	1	2	100
ARG 9075 50975	2	15	11	126	.4	35	5	440	2.31	26	5	ND	4	123	1	2	2	35	5.63	.075	14	22	1.37	492	.03	6	.99	.01	.16	1	1	60
ARG 9100 51050	2	14	12	126	1.4	34	6	419	2.45	14	5	ND	4	129	1	2	2	42	5.41	.078	13	23	1.57	673	.02	2	1.12	.02	.15	1	3	300
ARG 9100 51075	2	14	14	122	.4	30	7	425	2.11	8	5	ND	4	111	1	2	4	35	4.46	.079	15	19	1.53	557	.02	7	.93	.01	.15	1	9	80
ARG 9100 51150-1	5	45	14	187	.7	45	7	420	2.67	10	5	ND	4	116	1	2	2	50	3.66	.034	13	26	1.46	188	.03	4	1.24	.03	.20	1	1	110
ARG 9100 51150-2	4	10	12	178	.5	44	10	529	2.53	14	5	ND	4	116	2	3	4	45	3.89	.065	15	22	1.20	687	.02	4	1.01	.01	.16	1	1	120
ARG 9100 51150-3	3	19	11	164	.5	37	7	476	2.65	13	5	ND	4	129	1	4	3	43	4.81	.085	15	23	1.42	693	.02	4	1.04	.01	.18	1	1	100
ARG 9100 51175	4	11	15	178	.6	36	7	338	2.52	13	5	ND	4	123	1	3	2	47	4.23	.089	12	22	1.29	346	.02	10	1.07	.02	.19	1	3	120
ARG 9100 51225	4	12	18	175	.5	40	8	405	2.57	13	5	ND	4	116	1	3	3	48	3.87	.091	14	23	1.29	639	.02	7	1.11	.02	.19	1	1	110
ARG 9100 51300	3	18	11	159	.5	34	7	417	2.40	11	5	ND	4	131	1	2	6	42	4.86	.084	12	22	1.70	383	.02	2	1.06	.02	.19	1	1	120
ARG 9125 51000-1	3	17	10	140	.5	39	8	465	2.38	12	5	ND	4	124	1	2	2	39	4.94	.082	12	21	1.64	202	.02	9	1.06	.01	.17	1	1	90
ARG 9125 51000-2	3	10	8	150	.4	38	7	488	2.54	15	5	ND	4	125	1	2	2	39	4.82	.084	14	23	1.56	558	.02	12	1.07	.01	.13	1	4	80
ARG 9200 50800	2	10	10	127	.2	32	6	457	2.29	12	5	ND	4	124	1	2	2	34	5.82	.074	15	21	1.73	579	.02	4	1.03	.01	.16	1	1	70
ARG 9200 50850-1	3	10	15	146	.4	38	8	502	2.43	8	5	ND	4	131	1	2	2	42	4.98	.086	12	21	1.62	325	.02	9	1.08	.02	.19	1	1	90
ARG 9200 50850-2	2	11	8	122	.5	38	8	502	2.30	12	5	ND	4	123	1	2	2	35	5.48	.076	15	27	1.66	587	.02	9	1.02	.01	.16	1	1	90
ARG 9200 50850-3	1	12	9	110	.2	31	8	373	2.11	21	5	ND	3	93	1	2	2	30	3.70	.081	14	22	1.14	510	.03	3	.83	.01	.19	1	1	60
ARG 12200 49800	2	15	17	91	.4	41	11	285	2.74	11	5	ND	3	29	1	4	2	48	.61	.034	23	31	.64	460	.02	4	1.48	.02	.10	1	1	100
ARG 12200 49875	2	15	17	166	.7	49	10	412	3.36	14	5	ND	2	37	1	3	3	51	.63	.065	22	28	1.06	545	.05	5	1.67	.01	.12	1	1	120
ARG 12200 50000-1	2	16	16	136	.8	55	10	463	2.86	17	5	ND	3	62	1	4	2	50	1.80	.061	21	36	.80	677	.02	7	1.57	.01	.20	1	2	70
ARG 12200 50000-2	2	14	14	139	.5	37	9	377	2.45	15	5	ND	4	184	2	3	2	48	6.76	.081	15	29	1.33	640	.02	5	1.34	.01	.15	1	1	210
ARG 12800 50400	2	10	10	99	.2	45	11	503	3.25	17	5	ND	5	27	1	2	5	55	.43	.022	27	37	.61	616	.03	2	1.72	.01	.16	1	3	90
ARG 12800 50500	2	10	12	100	.5	64	10	607	3.31	17	5	ND	3	42	1	2	4	52	1.47	.057	34	38	1.06	722	.03	9	1.67	.02	.14	1	2	200
ARG 12800 50800	2	10	20	134	.4	54	10	444	3.02	14	5	ND	2	39	1	2	3	47	1.20	.044	23	32	.98	554	.03	6	1.57	.02	.14	1	1	130
STD C/AJ-S	18	15	39	133	6.6	72	29	1081	4.20	42	18	8	27	47	18	18	20	57	.48	.086	39	57	.93	174	.06	36	1.95	.06	.14	12	51	1400

SAMPLE#	PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	V PPM	Au* PPM	Hg PPM		
ARG 12800 50853	2	37	16	103	.3	49	11	417	2.81	15	5	NC	4	66	1	2	2	51	2.47	.069	22	33	.95	602	.03	12	1.65	.02	.16	1	5	130
ARG 12800 50925	2	40	14	85	.5	39	7	303	2.41	13	5	ND	2	96	1	2	2	43	5.33	.063	18	27	1.14	610	.03	10	1.47	.03	.13	1	3	160
ARG 12800 51025	2	41	17	120	.5	55	10	504	3.14	16	5	ND	5	56	1	3	2	60	1.35	.091	30	39	.98	634	.03	6	1.81	.02	.19	1	1	210
ARG 13800 50125	2	41	16	102	.3	40	9	402	2.38	13	5	ND	5	131	1	2	2	47	4.90	.085	18	28	1.15	730	.03	19	1.53	.02	.18	1	2	150
ARG 13800 50250	2	35	12	110	.3	39	10	563	2.83	15	5	ND	5	52	1	2	2	54	1.05	.079	25	34	.83	520	.04	5	1.65	.01	.19	1	1	170
ARG 13800 50300	2	36	15	108	.3	51	11	429	2.95	16	5	ND	2	54	1	2	5	46	1.37	.083	23	32	.91	375	.03	4	1.47	.02	.16	1	3	120
ARG 15600 50000-1	2	40	12	150	.2	48	10	487	2.94	13	5	NC	6	121	1	3	2	55	3.22	.102	21	34	1.34	732	.04	23	1.66	.03	.25	1	2	140
ARG 15600 50000-2	3	41	15	146	.2	49	10	508	2.87	14	5	NC	6	121	1	4	2	57	3.30	.104	20	39	1.38	761	.04	8	1.63	.02	.25	1	1	150
STD C/AU-S	19	59	39	133	6.7	67	28	1090	4.13	42	17	6	37	48	18	17	24	60	.45	.094	41	59	.92	182	.07	34	2.07	.06	.15	12	49	1400

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: TILL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

-200 MESH

DATE RECEIVED: SEP 23 1988 DATE REPORT MAILED: Sept 29/88 ASSAYER: C. Leong, D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

NORANDA EXPLORATION PROJECT 8809-076 335 File # 88-4750 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	F %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
9200 10500	2	59	18	89	.3	39	8	353	2.68	10	5	ND	3	31	1	2	2	34	.59	.025	26	25	.66	479	.01	3	1.14	.01	.10	1	3	160
9200 10550	2	38	15	92	.2	37	9	293	3.08	14	5	ND	5	27	1	2	3	40	.46	.023	22	28	.56	761	.01	2	1.45	.01	.09	1	2	60
9200 10600	2	53	14	105	.3	44	10	334	2.94	12	5	ND	4	53	1	2	2	37	1.47	.061	22	27	.75	465	.01	4	1.32	.01	.13	1	7	130
9200 10650	2	53	18	111	.3	48	11	567	3.20	13	5	ND	6	30	1	2	2	42	.55	.051	25	32	.66	548	.02	4	1.39	.01	.12	1	1	120
9200 10800	2	38	21	165	.3	36	10	341	2.92	14	5	ND	5	62	1	2	3	32	1.26	.083	20	26	.63	726	.02	5	1.11	.01	.09	1	3	40
9200 10850	2	42	19	91	.1	39	3	525	2.84	11	5	ND	4	21	1	2	2	37	.56	.019	23	26	.52	505	.01	3	1.17	.01	.08	1	1	100
9200 10900	2	19	16	73	.1	25	8	236	2.79	12	5	ND	6	16	1	2	2	35	.23	.026	19	24	.41	362	.02	3	1.17	.01	.06	1	1	30
9200 10950	1	50	11	79	.6	29	7	284	2.12	11	5	ND	1	136	1	2	2	17	1.76	.064	10	19	.96	628	.01	2	.87	.01	.08	1	1	150
9200 11000	2	39	15	111	.2	35	9	435	2.47	10	5	ND	4	110	1	2	2	35	3.93	.076	12	22	1.15	549	.02	4	1.08	.02	.13	1	1	90
9200 11125	1	37	14	85	.1	36	10	373	2.71	12	5	ND	4	31	1	2	2	34	.62	.022	18	27	.63	376	.02	2	1.27	.01	.13	2	2	60
9200 11175	2	34	12	84	.1	38	10	332	3.18	16	5	ND	6	19	1	2	2	42	.32	.021	22	34	.60	493	.02	2	1.58	.01	.12	2	1	70
9200 11275	2	21	17	101	.1	35	11	361	3.13	10	5	ND	6	27	1	2	2	40	.38	.044	24	33	.75	511	.02	2	1.56	.01	.11	1	1	40
9200 11325	1	35	8	63	.3	26	6	223	2.06	10	5	ND	1	60	1	2	2	26	3.03	.042	14	23	.67	384	.01	4	.95	.01	.07	2	2	130
9200 11375	1	12	11	97	.1	19	7	164	2.21	6	5	ND	3	19	1	2	3	31	.52	.054	12	25	.55	207	.02	2	1.11	.01	.09	1	6	60
9200 11425	2	21	15	78	.1	38	10	325	3.02	10	5	ND	6	17	1	2	2	39	.29	.025	25	31	.54	359	.02	2	1.44	.01	.09	1	1	120
9600 11250-2	2	43	11	122	.2	34	9	416	2.62	12	5	ND	5	104	1	2	2	33	4.70	.076	14	26	1.14	497	.02	3	1.10	.01	.15	2	7	110
10200 10475	2	27	16	84	.1	36	11	407	2.93	13	5	ND	4	41	1	2	3	38	1.36	.039	21	26	.76	753	.02	4	1.46	.01	.09	1	1	70
10200 10575	1	28	13	76	.1	31	9	348	2.84	13	5	ND	5	21	1	2	2	38	.30	.018	26	27	.56	479	.02	3	1.43	.01	.09	2	1	70
10200 10625	2	21	18	80	.1	30	9	233	2.97	19	5	ND	7	16	1	2	2	37	.21	.022	24	28	.52	379	.03	2	1.33	.01	.08	2	2	30
10200 10675	1	16	11	54	.1	14	6	342	1.69	7	5	ND	2	14	1	2	2	23	.20	.023	10	15	.28	315	.02	4	.78	.01	.07	1	1	20
10200 10775	2	61	18	92	.1	49	12	410	3.47	16	5	ND	5	26	1	2	3	45	.52	.039	25	35	.76	481	.02	3	1.58	.01	.16	1	2	140
10200 10825	2	51	16	86	.2	39	9	374	2.48	12	5	ND	2	44	1	2	3	36	1.56	.041	20	24	.77	415	.02	6	1.09	.01	.10	1	5	150
10200 10875	2	40	9	92	.3	32	8	492	2.03	9	5	ND	2	103	1	2	2	31	4.09	.071	13	19	1.10	608	.02	4	.93	.02	.12	1	1	80
10200 10925	2	33	8	51	.2	27	7	351	2.05	10	5	ND	2	96	1	2	2	31	3.65	.063	12	20	.92	549	.02	2	.95	.01	.11	1	1	60
10200 10975	2	41	9	78	.3	31	8	279	2.25	8	5	ND	2	73	1	2	2	35	2.97	.040	15	23	.78	559	.01	2	1.17	.01	.10	2	1	90
10200 11075	2	19	14	81	.1	29	9	205	3.05	16	5	ND	5	17	1	2	2	35	.26	.029	21	30	.67	259	.03	2	1.35	.01	.10	2	2	30
10200 11175	2	33	22	94	.1	21	10	405	2.85	20	5	ND	5	76	1	2	3	30	3.38	.092	20	24	1.06	627	.02	3	.97	.01	.07	1	3	50
10200 11225	1	27	15	79	.2	27	9	364	2.51	16	5	ND	2	95	1	2	2	27	3.33	.065	14	20	.87	520	.02	2	.95	.01	.05	1	1	40
10200 11250	2	34	14	107	.2	29	8	414	2.41	11	5	ND	4	111	1	2	2	30	4.97	.074	11	24	1.15	279	.02	3	1.00	.01	.15	1	1	80
10200 11275	1	31	11	53	.1	26	6	285	2.29	13	5	ND	3	38	1	2	2	33	1.59	.035	16	23	.73	336	.02	2	.99	.01	.06	1	2	100
10200 11325	1	17	10	57	.1	26	8	224	2.28	10	5	ND	2	30	1	2	3	27	.50	.029	14	22	.53	1648	.02	3	.94	.01	.05	1	1	50
10200 11475	2	50	18	81	.1	40	12	492	1.36	14	5	ND	5	21	1	3	2	33	.53	.026	26	32	.66	415	.01	2	1.59	.01	.10	2	27	200
11000 11500-1	2	47	15	120	.2	48	14	556	2.93	13	5	ND	4	82	1	2	2	32	3.61	.068	17	30	.90	442	.02	5	1.09	.01	.14	2	5	320
11000 11500-2	2	50	16	126	.3	51	14	568	3.15	14	5	ND	4	89	1	2	2	36	4.06	.090	16	34	.98	464	.02	2	1.23	.01	.15	1	3	530
11200 9600	2	33	14	90	.1	35	10	345	3.03	16	5	ND	6	20	1	2	2	36	.32	.030	30	26	.50	441	.02	3	1.28	.01	.07	1	1	80
11200 9650	2	59	13	102	.6	37	9	323	2.47	14	5	ND	1	59	1	2	2	36	2.13	.056	16	24	.74	462	.01	6	1.16	.01	.07	1	1	210
STD C/AU-S	18	60	36	132	6.8	67	21	1028	4.30	38	16	8	28	49	16	16	20	61	.49	.093	40	56	.93	162	.07	33	2.07	.06	.13	12	51	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	B1 PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Es PPM	Ti %	E PPM	Al %	Na %	K %	N PPM	Au PPE	Hg PPE	
11200 9700	2	19	8	70	.2	27	9	439	2.30	10	5	ND	4	25	1	2	2	30	.36	.033	21	24	.41	329	.02	2	.91	.01	.08	1	1	40
11200 9750	1	25	11	75	.1	32	8	324	2.73	15	5	ND	5	22	1	2	2	41	.47	.023	26	25	.54	494	.02	2	1.29	.01	.10	1	1	60
11200 9800	1	21	12	86	.1	28	7	415	2.25	10	5	ND	3	21	1	2	2	35	.48	.021	25	19	.44	411	.02	3	.99	.01	.07	1	1	80
11200 9900	2	35	16	92	.1	38	10	358	3.10	14	5	ND	7	24	1	2	2	50	.36	.020	27	30	.60	533	.03	2	1.48	.01	.17	1	3	90
11200 9950	2	28	25	130	.1	30	5	392	2.75	15	5	ND	5	20	1	2	2	40	.34	.034	23	24	.49	365	.02	5	1.18	.01	.12	1	1	70
11200 10000	1	13	12	66	.2	22	8	189	2.33	9	5	ND	6	15	1	2	2	34	.21	.029	20	26	.50	262	.03	2	1.11	.01	.09	1	1	20
11200 10050	1	22	20	79	.1	30	12	287	3.05	17	5	ND	6	16	1	2	2	41	.22	.018	21	35	.70	413	.02	2	1.53	.01	.10	1	1	50
11200 10100	1	19	13	82	.1	27	8	204	2.78	17	5	ND	6	20	1	2	2	37	.28	.022	24	27	.51	445	.03	3	1.28	.01	.08	1	28	40
11200 10150	1	16	8	63	.1	23	8	200	2.36	12	5	ND	4	17	1	2	2	33	.23	.022	19	24	.43	402	.03	2	1.06	.01	.08	1	2	20
11200 10200	1	15	6	61	.1	20	7	189	2.11	10	5	ND	4	20	1	2	2	33	.35	.022	20	22	.43	396	.03	2	1.05	.02	.07	1	1	20
11200 10250	1	13	14	71	.2	23	8	239	2.67	11	5	ND	2	29	1	2	2	39	.52	.038	19	26	.67	426	.02	2	1.43	.01	.07	1	1	60
11200 10350	2	23	12	69	.1	23	7	228	2.45	12	5	ND	5	21	1	2	3	34	.26	.024	19	21	.43	331	.02	2	1.08	.01	.14	1	1	20
11200 10400	2	22	17	89	.1	33	10	323	2.86	15	5	ND	6	21	1	2	2	47	.30	.021	22	37	.54	416	.03	3	1.44	.01	.12	1	1	30
11200 10475	1	51	6	59	.5	39	9	477	2.40	12	5	ND	3	71	1	2	2	28	3.52	.050	18	25	.77	466	.02	2	1.24	.02	.11	1	5	190
11200 10500	2	24	17	58	.1	30	10	349	2.93	10	5	ND	8	19	1	2	2	45	.28	.020	26	29	.60	475	.04	3	1.42	.01	.14	1	1	30
11200 10550	1	16	10	64	.1	23	8	232	2.54	11	5	ND	5	20	1	2	2	40	.29	.021	20	26	.45	445	.03	2	1.43	.01	.12	1	1	20
11200 10600	1	29	15	68	.3	31	9	240	2.47	15	5	ND	4	29	1	2	2	35	.66	.045	24	22	.60	460	.02	2	1.04	.01	.10	1	2	70
11200 10650	1	19	7	59	.3	22	6	221	2.25	10	5	ND	3	32	1	2	2	32	.47	.022	15	22	.51	438	.03	2	1.27	.02	.10	1	2	30
11200 10700	1	24	15	76	.1	28	8	499	2.55	14	5	ND	2	49	1	3	2	38	.77	.037	19	31	.76	515	.04	2	1.45	.04	.09	2	1	40
11200 10750	1	11	10	54	.1	19	7	321	2.02	7	5	ND	4	19	1	2	2	30	.30	.021	16	21	.45	307	.03	2	.99	.01	.08	1	2	30
11200 11050	1	38	11	74	.1	40	10	327	3.04	14	5	ND	7	28	1	2	2	43	.33	.010	23	34	.77	457	.03	2	1.47	.01	.12	1	1	70
11200 11100	1	41	12	80	.1	49	13	547	3.36	14	5	ND	8	21	1	2	2	46	.33	.025	30	46	.72	419	.04	2	1.56	.01	.16	1	2	80
11200 11150	1	45	14	86	.1	47	12	467	3.46	14	5	ND	7	21	1	2	3	49	.33	.025	29	38	.68	529	.03	3	1.69	.01	.18	1	6	80
11200 11200	1	27	39	71	.1	32	11	445	2.79	10	5	ND	6	15	1	2	2	40	.23	.015	20	32	.56	412	.03	2	1.41	.01	.14	1	1	50
11200 11250	1	39	11	77	.1	41	10	445	2.79	12	5	ND	5	22	1	2	2	37	.36	.030	24	32	.55	397	.02	2	1.16	.01	.11	1	1	110
11200 11300	1	44	12	89	.1	43	9	339	3.34	17	5	ND	5	22	1	2	2	49	.44	.027	28	36	.65	518	.02	2	1.64	.01	.16	1	1	120
11200 11350	1	46	11	132	.3	45	9	360	3.22	15	5	ND	4	62	1	2	2	48	1.89	.077	21	35	.91	443	.03	4	1.47	.01	.21	1	1	140
11200 11425	1	23	9	87	.3	29	9	373	2.45	8	5	ND	2	40	1	2	2	34	1.02	.077	17	27	.71	320	.02	7	1.08	.02	.14	1	4	120
11200 9500	1	38	20	117	.5	39	13	408	3.23	5	5	ND	5	55	1	2	2	47	.72	.043	23	34	.62	851	.01	2	2.01	.01	.11	1	2	40
11200 9600	1	35	19	62	.1	38	12	491	3.50	13	5	ND	8	34	1	2	2	36	.72	.045	33	19	.81	497	.01	2	1.60	.01	.12	1	3	140
11200 9550	1	34	12	89	.2	38	9	375	2.68	11	5	ND	3	36	1	2	2	39	.63	.039	22	31	.70	475	.02	2	1.20	.01	.10	1	4	200
11200 9700	2	36	24	110	.1	42	12	569	3.61	13	5	ND	7	27	1	2	2	48	.36	.022	30	43	.33	511	.02	2	1.79	.01	.15	1	2	80
11200 9750	1	16	7	54	.2	19	5	208	1.60	8	5	ND	2	38	1	2	2	25	.56	.066	14	19	.48	343	.02	3	.76	.03	.08	1	2	30
11200 9800	1	21	13	72	.1	27	8	315	2.69	16	5	ND	6	20	1	2	2	41	.24	.041	21	26	.49	354	.03	4	1.26	.01	.11	1	1	40
11200 9850	1	24	11	75	.1	28	8	286	2.66	11	5	ND	6	19	1	2	2	40	.24	.033	20	26	.47	328	.04	2	1.20	.01	.13	1	7	30
11200 9900	1	19	7	68	.1	25	3	305	2.38	10	5	ND	5	17	1	2	2	36	.23	.027	18	25	.45	345	.03	2	1.15	.01	.10	1	1	20
STD C/AJ-S	18	60	42	132	5.8	66	30	1032	4.26	40	19	7	39	45	19	17	19	60	.49	.094	40	55	.54	180	.07	32	1.91	.05	.13	12	50	1400

SAMP	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Au PPM	Hg PPM	
12200 9950	1	22	10	69	.1	25	7	199	2.18	4	5	ND	3	16	1	2	2	30	.27	.028	16	24	.47	380	.02	2	1.15	.01	.07	1	1	30
12200 10000	1	19	12	53	.2	24	6	224	1.91	6	5	ND	2	22	1	2	2	26	.39	.026	15	20	.42	348	.02	2	.92	.02	.07	1	1	50
12200 10125	1	36	15	89	.2	31	9	354	2.59	12	5	ND	3	57	1	2	2	31	1.58	.080	17	25	.85	446	.02	3	1.07	.01	.10	1	6	80
12200 10175	2	19	16	62	.1	24	9	251	2.54	10	5	ND	5	14	1	2	2	33	.19	.019	17	21	.37	354	.02	2	1.22	.01	.07	1	1	20
12200 10250	2	17	15	66	.1	26	8	218	2.79	9	5	ND	7	18	1	2	2	31	.27	.028	22	26	.62	439	.02	2	1.50	.01	.06	2	1	30
12200 10300	2	52	17	104	.2	45	10	397	3.04	13	5	ND	4	36	1	2	2	44	.80	.054	23	28	.71	479	.02	4	1.51	.01	.15	1	1	120
12200 10350	2	30	16	78	.1	37	10	350	2.88	13	5	ND	7	19	1	3	2	38	.25	.031	23	27	.52	363	.02	2	1.33	.01	.11	1	1	60
12200 10400	2	18	15	84	.1	25	9	220	2.74	12	5	ND	6	14	1	2	2	36	.19	.033	19	27	.52	324	.03	2	1.31	.01	.08	1	2	20
12200 10450	2	31	19	82	.1	34	10	320	2.90	12	5	ND	5	19	1	2	2	39	.29	.031	27	30	.56	447	.02	2	1.49	.01	.11	1	2	80
12200 10500	1	19	12	80	.1	26	7	211	2.35	7	5	ND	5	15	1	2	2	31	.24	.031	19	24	.51	341	.02	2	1.20	.01	.08	1	1	20
13200 9450	1	21	14	73	.1	34	8	220	2.64	12	5	ND	6	17	1	2	2	34	.27	.020	22	25	.46	451	.02	2	1.32	.01	.06	1	1	40
13200 9500	1	27	15	71	.2	28	8	271	2.46	13	5	ND	1	36	1	2	2	36	.67	.041	16	25	.79	401	.02	2	1.20	.02	.06	1	1	100
13200 9550	1	18	4	68	.1	23	7	177	2.27	10	5	ND	4	16	1	2	2	35	.22	.013	19	21	.37	474	.02	2	1.14	.01	.05	1	2	20
13200 9600	2	38	16	96	.1	36	9	250	2.80	13	5	ND	4	52	1	2	2	38	1.61	.036	23	28	.81	455	.02	7	1.34	.02	.10	1	1	110
13200 9650	1	14	7	63	.1	19	6	161	1.93	2	5	ND	4	13	1	2	2	26	.20	.017	14	21	.43	300	.02	2	1.04	.01	.07	1	1	10
13200 9700	2	20	35	69	.1	25	7	196	2.24	7	5	ND	4	15	1	2	2	25	.21	.017	16	26	.44	315	.01	2	1.02	.01	.07	1	1	20
13200 9850	2	36	13	78	.1	37	10	307	2.56	8	5	ND	6	17	1	2	2	25	.17	.031	21	24	.38	266	.02	2	.96	.01	.10	1	2	40
13200 9900	1	37	19	74	.1	46	11	355	3.12	8	5	ND	4	21	1	2	2	40	.30	.027	23	46	.79	357	.04	2	1.57	.01	.08	1	3	50
13200 9950	2	47	10	109	.4	38	9	359	2.64	12	5	ND	3	94	1	2	2	29	3.45	.078	15	21	.72	416	.02	10	.96	.01	.09	1	1	130
13200 10000	2	33	12	113	.1	38	10	324	2.66	11	5	ND	4	73	1	2	2	32	2.69	.093	19	28	.85	600	.03	2	.94	.01	.07	1	4	80
13200 10100	1	39	13	95	.1	36	8	357	2.42	6	5	ND	3	75	1	2	2	28	2.68	.082	19	26	.87	425	.02	2	.98	.01	.08	1	4	90
13200 10150	1	27	12	93	.1	31	8	257	2.40	7	5	ND	2	62	1	2	2	29	1.92	.073	18	25	.76	316	.02	2	1.00	.02	.07	1	2	70
13200 10300	1	49	19	93	.5	35	10	387	2.58	9	5	ND	2	71	1	2	2	33	2.11	.071	19	25	.82	534	.03	4	1.14	.02	.09	1	9	60
14000 9350	2	16	17	118	.1	25	9	369	3.08	13	5	ND	5	20	1	2	2	49	.43	.029	17	26	.52	634	.02	2	1.69	.01	.07	1	1	20
14000 9400	2	47	16	134	.5	44	9	346	2.68	13	5	ND	2	104	1	2	2	42	2.74	.092	16	26	1.10	609	.02	2	1.38	.01	.12	1	5	230
14000 9450	2	27	21	117	.1	35	9	254	3.07	15	5	ND	4	25	1	2	2	39	.47	.047	25	27	.57	486	.02	2	1.48	.01	.10	1	1	50
14000 9500	1	19	15	97	.1	26	8	232	2.76	8	5	ND	4	16	1	2	2	31	.23	.034	21	33	.74	251	.02	2	1.45	.01	.10	1	2	30
14000 9550	1	11	10	53	.1	19	6	167	2.04	7	5	ND	3	11	1	2	2	28	.16	.021	14	22	.38	357	.02	6	1.09	.01	.05	1	8	10
14000 9600	1	47	16	130	.8	36	9	256	2.82	10	5	ND	3	73	1	2	2	42	.87	.096	20	31	.68	1597	.02	3	1.83	.01	.07	1	3	40
14000 9650	2	22	12	77	.1	22	8	296	2.51	7	5	ND	4	18	1	2	2	30	.25	.029	17	21	.41	390	.02	2	1.17	.01	.11	1	1	30
14000 9700	1	14	14	66	.1	18	8	246	2.22	6	5	ND	2	44	1	2	2	35	.49	.017	13	24	.61	435	.02	3	1.39	.01	.05	1	1	50
14000 9750	1	10	10	48	.1	14	5	165	1.74	4	5	ND	1	15	1	2	6	26	.25	.020	12	19	.36	386	.01	2	1.02	.01	.05	2	2	10
14000 9800	1	13	14	59	.1	15	9	161	2.30	11	5	ND	4	13	1	2	3	33	.16	.013	16	25	.46	434	.02	2	1.32	.01	.06	1	1	20
14000 9850	1	11	10	56	.1	19	6	155	2.16	8	5	ND	4	12	1	2	2	27	.18	.020	17	23	.49	279	.02	2	1.03	.01	.05	1	2	20
14000 9900	2	21	14	85	.1	27	8	247	2.94	13	5	ND	5	23	1	2	2	36	.33	.020	23	30	.57	513	.03	2	1.54	.01	.11	1	1	40
14000 10000	1	14	15	67	.1	23	8	232	2.62	12	5	ND	4	17	1	3	2	34	.24	.029	17	26	.49	432	.02	2	1.36	.01	.10	1	1	30
STD C/AU-S	18	58	41	132	6.7	69	30	1022	4.23	39	18	7	28	48	19	21	22	59	.45	.096	40	57	.92	179	.07	32	1.96	.06	.13	12	53	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ea PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PFB	Hg PFB	
14000 10050	2	31	20	66	.2	30	8	235	2.70	9	5	ND	6	18	1	3	2	.23	.019	21	24	.45	352	.02	3	1.28	.01	.12	1	2	20	
14000 10100	1	14	20	52	.2	20	6	169	1.85	7	5	ND	5	13	1	2	2	.17	.016	15	19	.36	375	.02	2	1.07	.01	.58	1	2	10	
14000 10150	1	27	23	84	.2	36	8	281	2.77	13	5	ND	6	29	1	2	2	.45	.019	27	30	.65	411	.02	2	1.50	.01	.11	1	12	50	
14000 10200	2	41	9	109	.4	39	7	325	2.43	10	5	ND	4	81	1	2	3	2.99	.072	18	25	.93	490	.02	11	1.19	.01	.17	1	2	100	
14000 10300	2	43	15	119	.5	37	7	369	2.42	12	5	ND	4	97	1	2	3	3.55	.079	17	23	.98	535	.02	10	1.14	.01	.16	1	3	120	
15600 10050	2	28	16	157	.3	28	9	458	2.62	10	5	ND	5	25	1	2	2	.37	.070	16	23	.43	352	.03	4	1.11	.01	.15	1	1	30	
15600 10100	1	43	24	127	.4	38	10	496	2.73	14	5	ND	2	58	1	2	2	2.19	.075	18	25	.65	469	.03	3	1.23	.01	.15	1	1	40	
15600 10150	2	34	13	93	.4	32	6	377	2.30	10	5	ND	5	216	1	2	2	5.74	.086	16	21	1.54	541	.03	8	1.07	.02	.14	1	1	120	
15600 10350	1	19	19	67	.1	26	8	243	2.52	9	5	ND	6	21	1	2	2	.36	.038	21	25	.59	389	.03	2	1.18	.01	.10	1	4	20	
17600 9425	2	29	25	213	.2	36	10	512	3.20	14	5	ND	4	32	1	5	2	.42	.056	22	31	.55	501	.03	4	1.56	.01	.19	1	1	30	
17600 9475	2	38	20	136	.4	38	9	513	2.65	12	5	ND	3	66	1	3	2	1.54	.084	17	25	.80	452	.02	4	1.38	.02	.20	1	1	30	
17600 9525	2	20	20	82	.1	27	9	266	2.53	11	5	ND	6	16	1	2	2	.21	.039	19	26	.44	358	.03	5	1.15	.01	.09	1	1	10	
17600 9575	1	11	11	56	.1	19	7	197	2.15	5	5	ND	5	13	1	2	2	.18	.023	19	22	.54	295	.02	5	1.12	.01	.08	1	2	10	
17600 9625	1	15	21	69	.1	23	9	226	2.73	9	5	ND	5	18	1	2	2	.25	.026	19	23	.74	407	.03	2	1.59	.01	.05	1	1	30	
17600 9675	1	28	21	83	.1	37	8	307	3.12	16	5	ND	5	24	1	2	3	.33	.071	27	30	.59	395	.03	6	1.44	.01	.14	1	1	40	
17600 9725	1	30	13	113	.2	28	8	324	2.61	11	5	ND	2	50	1	2	2	1.08	.072	16	25	.60	461	.02	4	1.26	.02	.13	1	1	50	
17600 9775	1	48	22	106	.4	40	9	491	2.71	11	5	ND	4	68	1	2	2	2.16	.076	20	27	.81	461	.02	4	1.35	.02	.14	1	3	160	
17600 9825	1	33	19	96	.2	30	7	173	2.27	5	5	ND	3	50	1	2	2	1.02	.078	15	26	.73	258	.03	10	1.21	.02	.15	1	1	50	
18600 9575	2	17	16	62	.1	26	8	191	2.60	13	5	ND	6	17	1	2	2	.26	.029	17	27	.46	419	.02	2	1.32	.01	.07	1	1	20	
18600 9675	1	27	23	78	.2	25	8	348	2.48	27	5	ND	5	117	1	2	2	6.14	.103	19	16	1.58	595	.02	2	.86	.01	.05	1	1	60	
18600 9725	1	14	18	65	.1	17	6	184	2.47	8	5	ND	4	14	1	2	2	.20	.022	16	23	.54	412	.01	2	1.37	.01	.07	1	1	10	
18600 9825	1	12	20	67	.1	21	8	195	2.59	9	5	ND	5	17	1	2	2	.22	.011	18	26	.57	220	.02	12	1.33	.01	.07	1	1	10	
18600 9875	2	21	29	81	.1	30	10	320	3.21	25	5	ND	8	17	1	3	3	.24	.029	25	26	.54	403	.02	7	1.39	.02	.07	1	1	30	
18600 9925	1	19	16	71	.1	28	8	227	1.72	12	5	ND	7	19	1	2	2	.26	.032	23	27	.52	407	.03	7	1.35	.01	.07	1	1	40	
18600 9975	1	16	16	74	.1	26	8	244	2.53	10	5	ND	6	19	1	2	2	.26	.033	21	24	.49	419	.02	2	1.33	.01	.06	1	6	30	
STD C/AU-R	19	59	36	132	6.9	67	31	1027	4.22	39	20	8	38	49	19	16	22	61	.46	.033	40	53	.90	161	.07	32	1.06	.06	.13	13	520	1300

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P2 TILL -200 MKSH P3 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 2 1980 DATE REPORT MAILED: *Sept 13/88* ASSAYER: *C. Leong*, D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
ARG 1400 49875	2	23	21	62	.1	22	9	297	3.49	16	5	ND	4	8	1	2	3	24	.04	.015	21	13	.33	116	.01	2	1.58	.01	.05	1	5	40
ARG 1400 49925	4	46	23	127	.1	54	16	468	5.41	72	5	ND	17	17	1	2	2	61	.24	.014	43	33	1.07	206	.02	2	2.71	.01	.15	1	8	30
ARG 1400 49975	6	42	18	93	.1	50	15	274	4.67	82	5	ND	4	14	1	2	2	58	.11	.042	16	29	.48	292	.01	3	1.98	.01	.07	1	3	30
ARG 1400 50300	1	34	17	69	.1	50	15	406	3.95	34	5	ND	6	21	1	2	2	61	.32	.009	14	61	1.19	281	.11	4	2.83	.02	.37	1	1	40
ARG 1400 50450	1	35	26	82	.1	53	13	514	4.35	25	5	ND	9	24	1	2	2	51	.29	.014	26	52	.89	277	.05	2	2.52	.02	.12	1	1	20
ARG 1400 50500	1	41	8	51	.1	113	9	332	2.85	112	5	ND	1	35	1	2	2	53	.83	.063	12	134	1.17	303	.10	4	2.00	.07	.13	1	1	30
ARG 1400 50950	2	26	11	113	.1	32	8	344	2.23	11	5	ND	1	39	1	2	2	43	.67	.077	18	30	.46	369	.02	4	1.20	.01	.14	1	3	80
ARG 1400 51050	2	49	11	157	.3	52	10	323	2.79	12	5	ND	2	54	1	2	2	50	1.11	.093	20	32	.76	643	.03	5	1.41	.01	.13	1	1	90
ARG 1400 51200	2	45	11	131	.7	46	9	409	2.73	14	5	ND	2	43	1	2	2	47	.72	.078	22	29	.51	602	.02	3	1.30	.01	.16	1	1	200
ARG 2400 49950	2	18	13	76	.1	23	6	199	2.16	12	5	ND	2	11	1	2	2	32	.09	.023	16	20	.32	201	.01	3	1.07	.01	.06	1	1	20
ARG 2400 50150	2	33	9	82	.1	46	12	286	3.40	25	5	ND	3	18	1	2	2	50	.24	.011	16	38	.72	246	.03	2	1.99	.01	.07	1	2	20
ARG 2400 50500	1	25	13	74	.1	30	9	212	2.61	15	5	ND	3	13	1	2	2	43	.12	.012	13	33	.49	371	.04	2	1.68	.01	.13	1	1	30
ARG 15350 50350-1	3	49	16	232	.2	71	14	892	3.46	25	5	ND	1	113	1	2	2	39	2.72	.091	14	31	1.41	465	.05	9	1.20	.02	.13	1	3	160
ARG 15350 50350-2	3	43	15	161	.2	61	12	997	2.76	28	5	ND	3	129	1	3	2	28	5.95	.075	15	22	2.35	420	.03	4	1.01	.01	.13	1	2	120
ARG 15350 50350-3	2	48	25	142	.5	42	9	541	3.19	16	5	ND	3	95	1	2	2	40	2.81	.080	18	31	1.14	492	.02	3	1.41	.01	.20	1	8	200
ARG 16300 50450-1	2	42	18	141	.3	41	9	511	2.76	16	5	ND	2	106	1	2	3	41	3.48	.090	14	28	1.20	542	.03	9	1.10	.02	.15	1	5	140
ARG 16300 50450-2	2	37	11	132	.2	41	8	488	2.62	13	5	ND	2	106	1	2	2	39	3.66	.088	17	26	1.19	553	.03	4	1.14	.02	.13	1	13	170
ARG 16300 50450-1	2	36	20	131	.1	36	8	458	2.54	13	5	ND	1	101	1	2	2	39	3.52	.089	12	27	1.13	265	.03	6	1.06	.02	.15	1	8	130
ARG 16475 50225-1	2	41	20	144	.3	57	13	712	2.79	19	5	ND	1	103	1	2	2	43	3.15	.100	15	28	1.14	606	.03	10	1.14	.02	.15	1	21	150
ARG 16475 50225-2	2	37	16	134	.4	45	7	497	2.49	16	5	ND	1	122	1	2	2	40	4.25	.088	11	26	1.31	311	.03	5	1.00	.02	.17	1	1	130
ARG 16500 50175	2	46	22	177	.3	44	8	428	2.95	17	5	ND	2	100	1	2	2	46	2.99	.101	17	27	1.14	536	.02	11	1.17	.02	.16	1	5	170
ARG 16500 50200	2	38	18	132	.4	45	8	516	2.46	16	5	ND	1	132	1	3	2	40	4.64	.086	11	24	1.36	407	.03	5	.99	.02	.17	1	1	130
ARG 16520 50215-1	2	44	16	145	.4	49	9	526	2.66	18	5	ND	1	127	1	2	2	42	4.49	.092	10	28	1.46	186	.03	8	1.06	.02	.18	1	3	150
ARG 16520 50215-2	3	38	14	133	.2	46	9	555	2.51	15	5	ND	1	129	1	2	2	42	4.38	.085	11	26	1.55	267	.03	7	1.03	.03	.19	1	50	130
ARG 16560 50100-1	4	33	25	178	.2	38	10	586	2.87	11	5	ND	4	128	1	2	2	31	5.75	.076	14	23	2.20	315	.03	10	1.24	.02	.18	1	1	110
ARG 16560 50100-2	3	49	20	180	.3	53	11	544	3.02	20	5	ND	2	94	2	2	2	45	2.80	.100	15	27	1.16	474	.02	4	1.11	.01	.15	1	16	180
ARG 16600 50025-1	2	41	21	184	.2	41	11	456	3.39	18	5	ND	5	116	1	2	2	33	5.26	.075	18	25	1.96	244	.04	4	1.59	.02	.21	2	1	110
ARG 16600 50025-2	3	45	21	168	.3	48	11	516	2.80	19	5	ND	2	90	1	3	2	43	2.39	.095	15	27	1.13	508	.02	8	1.07	.01	.15	1	13	140
ARG 16600 50025-3	2	40	12	143	.2	43	8	442	2.71	16	5	ND	2	101	1	2	2	44	3.04	.093	15	30	1.23	476	.03	3	1.19	.04	.18	1	1	140
ARG 16600 50075	3	46	77	167	.6	44	10	490	2.80	17	5	ND	2	113	1	2	2	44	3.34	.096	15	24	1.27	550	.02	7	1.01	.02	.15	1	22	230
ARG 16650 50000-1	2	41	14	150	.4	46	8	447	2.79	16	5	ND	1	110	1	2	2	44	3.52	.097	12	29	1.42	186	.03	10	1.13	.03	.18	2	4	190
ARG 16650 50000-2	3	44	28	188	.3	49	14	968	3.59	18	5	ND	5	129	1	2	2	38	4.89	.071	14	27	2.03	307	.04	4	1.88	.04	.27	1	3	110
ARG 16700 49975-1	3	50	21	177	.4	47	10	457	2.97	20	5	ND	2	93	1	2	2	45	2.86	.102	15	28	1.09	517	.02	6	1.11	.01	.15	1	7	160
ARG 16700 49975-2	3	46	18	153	.3	43	9	472	2.85	15	5	ND	2	104	1	3	2	44	3.29	.098	13	30	1.37	201	.03	6	1.13	.02	.18	1	7	150
ARG 16725 49875-1	2	41	14	144	.2	46	8	505	2.87	16	5	ND	1	95	1	2	2	43	3.07	.096	15	29	1.02	514	.03	7	1.16	.02	.17	1	2	170
ARG 16725 49875-2	2	40	9	141	.4	41	8	490	2.80	16	5	ND	2	99	1	2	2	43	2.99	.092	16	28	1.06	573	.03	6	1.15	.02	.17	1	1	180
ARG 16725 49975-3	1	31	8	70	.3	33	7	353	2.35	12	5	ND	2	19	1	2	2	31	.48	.021	20	22	.46	300	.02	3	.97	.01	.08	1	6	210
STD C/AO-S	18	62	35	132	6.9	73	30	1091	4.21	40	18	8	35	48	18	16	20	59	.47	.090	39	59	.89	181	.07	32	1.96	.06	.14	13	49	1400

8/8/88 HCS

SAMPLE	ELEMENTS																															
	PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
ARG 3000 10000	1	46	12	46	.3	26	5	210	1.25	7	5	ND	1	142	1	2	2	17	12.22	.060	8	12	.86	663	.02	3	.53	.01	.06	2	3	160
ARG 3000 10050	1	31	10	63	.3	27	7	373	1.83	9	5	ND	1	87	1	2	2	24	7.29	.078	13	16	.83	463	.01	3	.32	.01	.07	1	5	130
ARG 3000 10100	2	28	17	63	.4	28	8	425	2.11	11	5	ND	1	29	1	2	3	27	1.68	.067	20	19	.52	321	.01	4	.89	.01	.06	1	9	70
ARG 3000 10200	2	33	17	83	.2	35	11	183	3.05	21	5	ND	3	23	1	2	2	36	.86	.072	23	24	.55	359	.02	3	1.14	.01	.06	3	1	30
ARG 3000 10400	1	36	11	49	.3	26	6	180	2.15	11	5	ND	1	24	1	2	2	30	.95	.062	18	22	.50	363	.01	4	1.06	.01	.04	1	5	120
ARG 3000 10450	1	37	11	56	.5	30	6	186	1.77	3	5	ND	1	53	1	3	2	23	4.44	.071	14	18	.53	275	.01	3	.85	.02	.06	1	10	170
ARG 3000 10500	1	30	17	63	.3	26	6	207	2.23	11	5	ND	3	70	1	2	2	27	3.39	.093	17	19	.93	384	.02	2	.91	.01	.04	1	2	70
ARG 3000 10600	1	59	14	72	.7	44	8	282	2.13	6	5	ND	2	93	1	2	8	31	6.64	.088	14	32	.86	417	.02	4	.97	.01	.10	1	9	230
ARG 3000 10750	2	36	22	90	.2	46	9	417	2.96	13	5	ND	3	37	1	2	2	39	1.76	.064	22	37	.83	418	.03	2	1.32	.01	.10	1	2	130
ARG 3000 10800	2	45	16	39	.6	35	8	306	2.16	9	5	ND	2	52	1	2	2	32	1.61	.070	14	19	.59	413	.01	2	.58	.02	.19	1	1	140
ARG 4000 10000	2	50	18	99	.3	44	11	382	3.11	12	5	ND	5	21	1	3	2	44	.41	.051	26	28	.66	423	.03	3	1.52	.01	.21	1	3	130
ARG 4000 10050	1	79	16	65	.8	37	6	255	1.94	8	5	ND	1	89	1	2	2	28	7.69	.087	12	19	.74	533	.01	3	.88	.01	.10	1	6	300
ARG 4000 10100	1	54	13	77	.7	35	6	241	2.05	9	5	ND	1	55	1	2	2	28	4.00	.070	14	20	.61	397	.01	3	.92	.01	.13	1	4	180
ARG 4000 10625	1	37	14	81	.1	39	9	417	2.58	11	5	ND	1	42	1	2	2	37	1.52	.070	19	25	.63	467	.01	2	1.34	.01	.08	1	1	200
ARG 4000 10675	2	35	24	87	.2	37	9	311	3.05	14	5	ND	4	20	1	3	2	40	.52	.028	31	27	.55	402	.02	2	1.33	.01	.10	1	2	100
STD C/AU-S	19	62	43	132	6.8	65	30	1025	4.18	39	17	8	36	48	18	19	23	60	.49	.092	38	56	.94	182	.07	33	2.04	.06	.13	11	51	1300

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR NG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: TILLS AU* ANALYSIS BY ACID LEACH/AA FROM 10 GR SAMPLE. HG ANALYSIS BY PLASMALSS AA.

DATE RECEIVED: SEP 9 1988 DATE REPORT MAILED: Sept 15/88 ASSAYER: C. Leong D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ea	Ti	B	Al	Na	K	W	Au*	Hg
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	PPB
ARG 1200 10050	1	40	9	61	.5	54	9	326	1.70	7	5	ND	1	116	1	2	2	21	8.36	.084	13	17	.92	462	.01	3	.65	.01	.09	1	7	160
ARG 1200 10100	1	35	10	75	.2	57	11	438	2.12	6	5	ND	1	88	1	2	2	28	6.00	.092	16	22	.90	486	.02	3	.91	.01	.09	1	5	150
ARG 1200 10225	1	27	8	81	.2	53	12	451	2.53	8	5	ND	2	83	1	2	3	34	5.21	.112	20	40	1.11	270	.04	8	1.06	.01	.10	1	3	170
ARG 1200 10275	1	34	8	77	.2	75	15	422	2.38	8	5	ND	2	115	1	2	2	32	6.05	.115	18	53	1.32	426	.07	2	.89	.01	.08	1	6	150
ARG 1200 10300	1	38	10	66	.3	53	11	381	1.92	7	5	ND	1	92	1	2	2	26	9.15	.083	13	25	.96	435	.02	6	.80	.01	.08	1	4	250
ARG 1200 10400	1	25	11	65	.3	45	9	330	1.86	6	5	ND	1	90	1	2	2	24	4.59	.092	13	22	.92	344	.02	3	.61	.01	.06	1	5	150
ARG 1200 10500	1	36	13	91	.2	62	14	363	2.80	9	5	ND	2	71	1	2	2	36	4.06	.097	19	40	1.14	395	.04	4	1.27	.01	.11	2	9	160
ARG 1200 10600	1	34	10	87	.1	52	11	434	2.46	8	5	ND	2	97	1	2	2	33	8.13	.098	17	38	1.14	415	.04	4	1.07	.01	.11	1	3	190
ARG 1200 10850	1	26	17	56	.1	17	12	354	3.35	5	5	ND	1	107	1	2	2	21	8.85	.050	33	13	1.73	325	.01	2	2.01	.01	.11	1	4	240
ARG 1200 10900	1	52	7	67	.3	48	12	355	2.54	8	5	ND	1	76	1	2	4	29	5.40	.062	17	29	.94	318	.01	3	1.24	.01	.12	1	5	230
ARG 1200 10950	1	43	5	46	.1	43	10	261	1.87	3	5	ND	1	73	1	2	2	23	8.60	.071	12	30	.74	224	.02	2	.91	.01	.07	1	1	260
ARG 2000 10050	1	35	11	58	.2	35	9	224	2.12	10	5	ND	1	52	1	2	2	27	3.81	.057	19	21	.67	347	.02	2	.89	.01	.07	2	2	130
ARG 2200 10150	1	11	10	39	.1	18	4	107	1.66	2	5	ND	1	22	1	2	3	22	1.04	.066	17	17	.40	263	.02	10	.79	.02	.08	2	1	90
ARG 2200 10400	1	31	5	50	.1	47	10	258	1.85	6	5	ND	1	86	1	2	3	28	13.09	.092	15	38	.95	265	.02	4	.98	.01	.06	2	4	300
ARG 2200 10500	1	35	12	79	.1	78	14	469	2.82	8	5	ND	1	98	1	2	2	39	6.71	.105	21	65	1.52	371	.06	5	1.43	.01	.10	1	3	190
ARG 2200 10600	1	34	9	65	.3	35	9	259	2.18	6	5	ND	1	66	1	2	3	29	3.95	.092	20	24	.81	433	.02	3	1.02	.01	.08	1	5	180
ARG 2200 10650	1	35	10	92	.1	50	12	417	2.45	9	5	ND	2	81	1	2	2	32	4.77	.097	17	30	1.01	507	.03	3	.90	.01	.10	1	2	210
ARG 2200 10700	1	29	15	62	.1	41	11	198	2.68	7	5	ND	3	21	1	2	2	31	1.19	.048	21	27	.66	357	.02	4	1.15	.01	.09	1	1	170
ARG 2200 10800	1	38	9	89	.2	64	15	469	2.86	6	5	ND	2	88	1	2	2	40	8.81	.137	19	52	1.12	282	.06	3	1.21	.01	.13	1	2	400
ARG 2200 10850	1	46	7	91	.2	89	16	709	3.22	7	5	ND	1	95	1	2	2	42	11.03	.158	20	67	1.20	265	.06	3	1.32	.01	.13	1	2	680
ARG 2200 10900	1	45	10	89	.1	79	15	691	3.07	6	5	ND	1	82	1	2	2	40	8.98	.139	19	59	1.10	282	.05	11	1.25	.01	.13	1	1	830
ARG 2200 10950	1	34	10	100	.1	66	15	467	3.08	7	5	ND	1	87	1	2	4	42	9.44	.140	19	54	1.11	238	.06	5	1.24	.01	.15	1	1	350
ARG 2200 11000	1	26	10	106	.2	69	17	468	3.28	7	5	ND	2	77	1	2	2	45	7.02	.148	20	59	1.19	218	.06	11	1.36	.01	.15	2	3	330
ARG 4800 10075	1	29	12	86	.1	27	10	364	2.13	7	5	ND	2	110	1	2	2	25	3.99	.084	16	14	1.07	459	.02	7	.70	.01	.09	1	2	80
ARG 4800 10175	1	23	12	72	.1	27	9	285	1.98	10	5	ND	2	147	1	2	2	25	5.15	.073	15	15	1.22	569	.02	5	.73	.01	.10	1	1	40
ARG 4800 10225	1	39	8	48	.4	31	6	215	1.36	6	5	ND	1	135	1	2	2	18	10.03	.063	9	11	.54	837	.01	4	.55	.05	.07	1	2	110
ARG 4800 10400	1	26	16	77	.3	29	6	173	2.29	16	5	ND	1	82	1	2	3	27	4.60	.115	17	18	1.00	462	.01	11	.77	.01	.08	1	4	100
ARG 4800 10450	1	56	15	96	.3	43	11	375	2.92	13	5	ND	3	39	1	3	2	40	1.35	.058	22	23	.65	484	.02	2	1.38	.01	.13	1	5	170
ARG 4800 10550	1	33	20	111	.1	37	10	454	2.88	12	5	ND	3	21	1	2	2	38	.72	.037	22	20	.46	432	.02	2	1.18	.01	.14	1	2	90
ARG 4800 10650	1	33	16	82	.1	41	12	404	2.73	10	5	ND	1	43	1	2	2	37	2.06	.060	21	23	.66	601	.01	2	1.29	.01	.11	1	4	150
ARG 5800 9950	1	22	11	59	.1	23	7	257	2.26	9	5	ND	6	14	1	2	2	27	.20	.039	23	14	.32	313	.02	2	.77	.01	.06	1	3	40
ARG 5800 10000	1	46	15	87	.1	43	10	320	3.10	10	5	ND	3	38	1	2	4	43	.72	.054	22	23	.74	558	.02	3	1.44	.02	.12	1	4	100
ARG 5800 10075	1	22	10	65	.1	31	7	214	2.44	7	5	ND	4	37	1	2	2	33	.77	.024	21	20	.53	467	.02	6	1.50	.03	.09	1	2	70
ARG 5800 10150	1	35	15	77	.2	37	8	302	2.96	10	5	ND	4	27	1	2	2	38	.43	.019	23	20	.63	416	.02	3	1.28	.01	.12	1	1	80
ARG 5800 10200	1	36	17	81	.1	37	10	501	2.74	8	5	ND	3	24	1	2	2	34	.60	.029	28	19	.65	521	.01	6	1.22	.01	.10	1	3	90
ARG 5800 10250	1	33	15	110	.1	37	10	435	2.73	11	5	ND	3	51	1	2	2	35	1.52	.087	21	19	.95	492	.02	3	1.13	.01	.14	1	2	70
STD C/AU-5	18	59	36	132	7.1	69	31	1024	4.10	42	19	8	37	48	18	17	15	59	.48	.091	39	53	.92	163	.06	33	1.94	.06	.15	13	53	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	Pb PPM	As PPM	Hg PPM	
ARG 5800 10300	2	22	15	95	.4	27	8	386	2.57	9	5	ND	4	32	1	2	3	33	.59	.062	19	19	.60	305	.02	6	1.06	.01	.10	1	1	50
ARG 5800 10475	2	38	9	114	.2	29	8	368	2.33	12	5	ND	5	123	1	2	2	37	4.04	.091	14	16	1.14	491	.02	5	.90	.01	.12	1	4	130
ARG 5800 10500	1	39	17	103	.2	31	9	345	2.10	13	5	ND	5	152	1	3	4	31	8.03	.084	13	14	1.09	842	.01	5	.78	.01	.10	2	4	120
ARG 5800 10550	2	45	14	112	.2	49	11	549	3.02	13	5	ND	4	38	1	2	3	49	.82	.076	26	22	.66	541	.01	2	1.33	.01	.13	1	7	150
ARG 5800 10600	2	31	21	69	.2	36	9	270	2.84	14	5	ND	6	18	1	2	2	40	.35	.016	24	26	.50	407	.02	3	1.25	.01	.11	1	2	80
ARG 5800 10650	2	40	12	118	.2	39	8	450	2.47	14	5	ND	5	73	1	2	2	38	3.55	.096	17	18	.82	447	.02	3	.99	.01	.11	1	5	130
ARG 5800 10700	1	18	10	132	.1	30	9	366	2.40	8	5	ND	2	46	1	2	2	38	1.34	.085	18	19	.72	382	.02	4	1.03	.01	.11	1	1	110
ARG 5800 10750	1	24	17	106	.3	30	9	303	2.45	10	5	ND	3	61	1	2	5	41	2.32	.078	17	19	.80	460	.01	4	1.12	.01	.13	1	7	100
ARG 5800 10800	2	16	14	85	.1	27	8	233	2.90	14	5	ND	4	29	1	2	2	33	.76	.079	23	19	.60	294	.02	2	1.04	.01	.07	2	1	70
ARG 5800 10900	2	29	14	89	.1	38	9	371	3.04	11	5	ND	5	20	1	2	3	46	.39	.024	25	25	.60	423	.02	2	1.39	.01	.11	1	1	80
ARG 5800 10950	1	35	15	77	.4	30	8	277	2.41	9	5	ND	3	45	1	2	3	45	1.47	.077	19	21	.78	449	.02	2	1.20	.01	.13	1	2	120
ARG 6000 10175-1	2	43	24	126	.3	34	9	443	2.74	11	5	ND	6	99	1	3	3	37	3.24	.083	18	19	1.17	594	.02	4	1.13	.01	.18	1	2	110
ARG 6000 10175-2	2	41	17	124	.2	34	10	466	2.72	12	5	ND	6	98	1	2	2	36	3.16	.084	18	19	1.16	532	.02	3	1.11	.01	.18	2	3	100
ARG 6000 10175-3	2	43	18	119	.2	33	11	457	2.71	12	5	ND	6	96	1	2	2	34	3.05	.085	18	18	1.13	519	.02	4	1.01	.01	.15	1	1	110
ARG 6000 10175-4	2	40	15	124	.3	33	11	493	2.71	10	5	ND	5	97	1	2	2	35	3.10	.080	18	19	1.19	521	.02	2	1.09	.01	.16	1	3	130
ARG 6800 9875	1	15	12	59	.1	21	5	192	1.88	7	5	ND	2	15	1	2	2	24	.25	.026	15	13	.35	226	.02	2	.74	.01	.07	1	3	30
ARG 6800 9975	2	37	12	117	.2	33	9	438	2.51	10	5	ND	6	104	1	2	2	38	3.40	.085	17	17	1.23	537	.02	9	1.02	.01	.13	1	7	120
ARG 6800 10050	1	37	11	69	.2	30	7	288	2.23	8	5	ND	2	40	1	2	5	29	1.24	.064	22	15	.66	440	.01	4	.92	.01	.10	1	12	130
ARG 6800 10100	1	31	13	80	.1	31	9	320	2.56	9	5	ND	5	15	1	2	2	32	.23	.027	21	18	.43	253	.02	3	.99	.01	.14	1	8	50
ARG 6800 10150	1	25	13	70	.2	27	8	366	2.47	8	5	ND	4	16	1	2	2	32	.28	.027	20	17	.47	266	.02	2	1.12	.01	.12	1	3	70
ARG 6800 10200	1	17	11	74	.1	20	7	362	2.11	5	5	ND	4	14	1	2	2	30	.20	.024	17	15	.40	278	.02	2	.90	.01	.13	1	1	30
ARG 6800 10300	1	30	13	97	.2	31	10	479	2.70	10	5	ND	5	19	1	2	4	36	.31	.036	20	19	.47	333	.02	2	1.13	.01	.16	1	1	40
ARG 6800 10450	1	22	20	139	.1	29	8	408	2.95	10	5	ND	5	14	1	2	3	37	.31	.026	21	18	.44	365	.02	4	1.29	.01	.20	1	2	20
ARG 6800 10500	2	23	20	100	.1	30	8	333	2.88	14	5	ND	4	15	1	2	2	35	.34	.026	22	19	.45	309	.03	4	1.01	.01	.13	2	1	30
ARG 6800 10550	2	22	19	79	.2	29	9	347	3.13	12	5	ND	6	16	1	2	2	39	.31	.024	21	20	.50	358	.02	2	1.30	.01	.11	1	2	40
ARG 6800 10650	2	37	22	496	.5	36	10	594	4.03	14	5	ND	2	67	2	2	2	39	1.68	.060	37	20	1.01	562	.01	3	1.31	.01	.11	1	17	190
ARG 7800 10400	1	35	14	96	.4	32	7	343	2.17	10	5	ND	3	123	1	2	3	29	3.72	.084	14	14	1.22	445	.02	3	.82	.01	.19	1	14	150
ARG 7800 10450	1	24	14	72	.2	27	8	354	2.36	9	5	ND	4	20	1	2	4	29	.35	.052	21	16	.43	228	.02	3	.89	.01	.14	1	3	40
ARG 7800 10500	2	55	8	103	.6	52	9	451	3.23	12	5	ND	5	31	1	2	2	45	.42	.066	23	22	.72	495	.02	4	1.40	.01	.27	1	7	140
ARG 7800 10550	1	31	15	83	.1	37	9	342	2.71	12	5	ND	5	21	1	2	2	37	.28	.058	24	20	.47	332	.03	2	1.22	.01	.22	1	1	50
ARG 7800 10600	1	48	12	81	.5	33	10	314	2.29	12	5	ND	4	174	1	2	2	31	7.92	.081	13	17	1.17	742	.02	3	.99	.01	.19	1	2	130
ARG 7825 10350-1	2	36	17	135	.3	44	15	593	2.75	11	5	ND	6	114	1	2	2	43	3.83	.087	16	20	1.34	594	.02	3	1.19	.01	.20	2	3	110
ARG 7825 10350-2	2	37	13	138	.3	36	11	494	2.86	10	5	ND	6	112	1	2	2	42	3.82	.083	18	26	1.37	569	.02	3	1.19	.01	.18	1	1	100
ARG 7825 10350-3	2	43	17	124	.4	41	13	525	2.81	10	5	ND	5	92	1	2	4	38	2.76	.082	15	20	1.44	420	.02	3	1.17	.01	.17	1	6	120
ARG 8000 9600	1	31	10	108	.3	36	9	326	2.44	7	5	ND	4	49	1	2	2	31	1.43	.051	19	17	.61	401	.01	2	.98	.01	.10	1	2	110
ARG 8000 9650	1	40	19	139	.2	51	11	373	2.91	11	5	ND	7	49	1	2	5	35	.96	.073	22	20	.75	479	.02	4	1.14	.01	.12	1	1	140
STD C/AC-S	18	57	38	132	6.6	67	30	1021	4.21	39	22	8	36	48	17	16	23	57	.48	.088	38	52	.93	172	.06	32	1.90	.06	.14	13	53	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Y PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	Pb PPM	Hg PPB	
ARG 8000 9700	1	36	24	108	.1	42	10	288	2.53	10	5	ND	5	29	1	2	2	37	.43	.026	26	30	.46	450	.01	2	1.24	.01	.09	1	5	120
ARG 8000 9750	1	24	23	110	.1	35	11	329	2.64	14	5	ND	5	30	1	2	2	37	.44	.042	24	28	.49	348	.01	2	1.17	.01	.11	1	1	80
ARG 8000 9900	1	27	13	62	.1	24	6	274	1.44	9	5	ND	2	179	1	2	3	19	12.51	.067	9	21	1.14	716	.01	3	.63	.01	.08	2	1	110
ARG 8000 9950	1	41	16	82	.2	36	8	414	2.10	14	5	ND	4	79	1	2	2	30	3.43	.081	17	23	.79	486	.02	2	.92	.01	.11	1	8	100
ARG 8000 10025	1	35	22	77	.1	40	9	467	2.25	12	5	ND	3	40	1	2	2	34	1.04	.082	21	23	.70	433	.02	2	1.01	.01	.12	1	1	90
ARG 8000 10075	1	34	21	70	.1	37	9	398	2.16	13	5	ND	2	44	1	2	3	32	1.66	.057	24	27	.86	440	.02	2	.98	.01	.09	1	4	120
ARG 8000 10300	2	27	16	84	.1	27	7	376	1.83	10	5	ND	4	86	1	2	2	26	2.76	.074	14	20	.65	463	.02	2	.68	.01	.11	1	19	60
ARG 8000 10450	2	38	14	110	.1	36	8	408	2.18	11	5	ND	4	105	1	2	2	33	3.07	.083	17	25	1.07	536	.02	2	.93	.02	.18	1	9	110
ARG 8000 10650	2	36	19	84	.1	42	9	440	2.66	13	5	ND	7	24	1	2	3	40	.33	.051	24	30	.49	524	.03	3	1.31	.01	.22	2	1	70
ARG 8000 10700	1	33	19	80	.1	38	9	395	2.47	13	5	ND	6	23	1	2	2	38	.23	.052	21	27	.49	362	.03	4	1.22	.01	.20	1	1	50
ARG 8000 10750	1	42	12	80	.3	33	8	349	2.10	10	5	ND	4	72	1	2	2	33	2.62	.078	17	25	.79	433	.02	2	1.05	.01	.20	1	10	120
ARG 8000 10800	1	41	19	82	.1	44	10	403	2.60	11	5	ND	7	25	1	2	2	42	.30	.067	24	28	.50	380	.03	3	1.33	.01	.23	1	3	130
ARG 8000 10850	1	33	17	101	.3	35	10	432	2.72	10	6	ND	9	20	1	2	2	41	.22	.041	26	30	.59	392	.03	2	1.36	.01	.27	2	1	70
ARG 8000 10900	2	41	9	97	.6	33	7	326	1.72	11	5	ND	3	148	2	2	2	34	6.36	.086	11	23	1.07	599	.01	7	.80	.02	.20	1	1	180
ARG 8000 11050	1	25	25	74	.1	30	8	268	2.50	18	5	ND	5	18	1	2	2	33	.63	.060	24	26	.44	640	.02	3	1.08	.01	.06	1	1	80
ARG 8000 11125	1	32	16	59	.1	28	7	307	1.71	9	5	ND	2	48	1	2	2	27	4.00	.076	15	21	.51	411	.01	2	.88	.01	.08	1	5	140
ARG 8000 11225	1	30	10	54	.2	24	6	337	1.60	8	5	ND	4	70	1	2	2	25	8.27	.072	11	21	.56	319	.02	2	.78	.01	.09	1	1	130
ARG 8000 11400	1	37	14	63	.4	28	6	247	1.74	9	5	ND	4	69	2	2	2	26	4.73	.082	13	22	.59	369	.02	4	.84	.01	.09	1	3	150
ARG 9000 10850	1	32	12	82	.2	26	8	370	1.85	9	5	ND	4	91	1	2	2	29	3.40	.077	15	21	.86	468	.03	3	.76	.01	.10	1	5	80
STD C/AU-S	17	57	40	132	6.5	66	29	1035	3.82	38	22	7	38	47	19	17	18	57	.46	.094	39	56	.85	175	.06	32	1.82	.06	.14	12	53	1300

Bondar-Clegg & Company Ltd.
 130 Penikese Ave.
 North Vancouver, B.C.
 V7P 2R5
 (604) 85-0681 Telex 04-352667



Geochemical Lab Report

REPORT: V88-07492.0 (COMPLETE)

Argo (AP)

REFERENCE INFO: LAB CODE #8809-035

CLIENT: NORANDA EXPLORATION CO. LTD.
 PROJECT: 335

SUBMITTED BY: UNKNOWN
 DATE PRINTED: 25-OCT-88

ORDER	ELEMENT		NUMBER OF ANALYSES	LOWER DETECTION LIMIT	EXTRACTION	METHOD
1	Au	Gold	29	1 PPM		INST. NEUTRON ACTIV.
2	Ag	Silver	29	2 PPM		INST. NEUTRON ACTIV.
3	As	Arsenic	29	0.5 PPM		INST. NEUTRON ACTIV.
4	Ba	Barium	29	100 PPM		INST. NEUTRON ACTIV.
5	Br	Bromine	29	1 PPM		INST. NEUTRON ACTIV.
6	Cd	Cadmium	29	2 PPM		INST. NEUTRON ACTIV.
7	Co	Cobalt	29	2 PPM		INST. NEUTRON ACTIV.
8	Cr	Chromium	29	10 PPM		INST. NEUTRON ACTIV.
9	Ir	Iridium	29	20 PPM		INST. NEUTRON ACTIV.
10	Mo	Molybdenum	29	0.5 PPM		INST. NEUTRON ACTIV.
11	Ni	Nickel	29	10 PPM		INST. NEUTRON ACTIV.
12	Sb	Antimony	29	0.1 PPM		INST. NEUTRON ACTIV.
13	Se	Selenium	29	5 PPM		INST. NEUTRON ACTIV.
14	Ta	Tantalum	29	0.5 PPM		INST. NEUTRON ACTIV.
15	Th	Thorium	29	0.5 PPM		INST. NEUTRON ACTIV.
16	U	Uranium	29	0.1 PPM		INST. NEUTRON ACTIV.
17	W	Tungsten	29	1 PPM		INST. NEUTRON ACTIV.
18	Zn	Zinc	29	20 PPM		INST. NEUTRON ACTIV.

SAMPLE TYPES	NUMBER	SIZE FRACTIONS	NUMBER	SAMPLE PREPARATIONS	NUMBER
H HUMUS	29	1 - 80	29	DRY, SIEVE - 80	29

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REPORT: V88-07492.0

PROJECT: 335

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SAMPLE NUMBER	ELEMNT UNITS	Au PPB	Ag PPM	As PPM	Ba PPM	Br PPM	Cd PPM	Co PPM	Cr PPM	Ir PPB	Mo PPM	Ni PPM
H1 1200 10450		2	<2	4.3	640	4	<2	6	66	<20	1.0	41
H1 2200 10100		<1	<2	2.0	400	4	<2	3	13	<20	1.5	<10
H1 2200 10200		2	<2	4.9	670	13	<2	3	40	<20	1.3	17
H1 2200 10250		<1	<2	1.6	320	4	<2	2	11	<20	1.1	<10
H1 2200 10300		<1	<2	3.7	710	5	<2	3	22	<20	1.4	11
H1 2200 10350		<1	<2	1.4	620	6	<2	4	14	<20	1.0	<10
H1 2200 10450		<1	<2	4.7	570	8	<2	4	31	<20	0.6	<10
H1 2200 10550		<1	<2	1.6	610	5	<2	4	11	<20	2.3	<10
H1 5000 10700		<1	<2	0.6	110	4	<2	<2	<10	<20	1.9	<10
H1 5000 10750		<1	<2	1.1	360	8	2	<2	<10	<20	2.0	<10
H1 6800 10350		2	<2	2.7	690	3	<2	3	23	<20	2.4	<10
H1 6800 10750		1	<2	1.8	590	6	<2	3	<10	<20	1.9	<10
H1 8000 10950		2	<2	3.6	790	18	<2	5	56	<20	1.0	12
H1 8000 11000		<1	<2	2.1	920	5	<2	4	19	<20	1.2	<10
H1 8000 11100		2	<2	1.6	780	7	<2	7	15	<20	1.0	<10
H1 8000 11175		<1	<2	1.7	760	7	<2	5	<10	<20	1.5	<10
H1 8000 11275		<1	<2	1.5	600	10	2	4	12	<20	0.8	<10
H1 8000 11325		2	<2	1.8	520	6	<2	3	<10	<20	1.8	<10
H1 8000 11375		<1	<2	1.7	790	6	<2	4	14	<20	1.3	<10
H1 12001 10550		<1	<2	1.2	590	5	<2	3	<10	<20	1.4	<10
H1 12001 10800		2	<2	2.2	610	4	<2	3	17	<20	0.8	<10
H1 12001 11000		2	<2	4.1	730	5	<2	8	47	<20	1.0	31
H1 48001 10125		<1	<2	2.9	700	6	<2	4	17	<20	1.5	12
H1 48001 10350		<1	<2	2.2	710	7	<2	4	12	<20	1.4	11
H1 48001 10500		1	<2	4.5	840	6	<2	5	31	<20	1.7	17
H1 48001 10600		<1	<2	1.4	650	5	<2	3	23	<20	1.3	14
H1 50001 10650		2	<2	<0.5	120	4	<2	<2	<10	<20	2.4	<10
H1 68001 10700		<1	<2	3.8	760	6	2	4	23	<20	1.3	17
H1 68001 10800		2	<2	1.5	640	7	<2	4	12	<20	1.5	<10

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SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Se PPM	Ta PPM	Th PPM	U PPM	W PPM	Zn PPM
H1 1200 10450		0.8	<5	<0.5	3.2	1.3	<1	<50
H1 2200 10100		0.4	<5	<0.5	1.6	0.6	<1	94
H1 2200 10200		0.9	<5	<0.5	3.1	1.1	<1	<50
H1 2200 10250		0.3	<5	<0.5	0.9	0.5	<1	69
H1 2200 10300		1.0	<5	<0.5	2.4	1.0	<1	78
H1 2200 10350		0.3	<5	<0.5	2.4	0.9	<1	77
H1 2200 10450		0.8	<5	<0.5	2.8	1.4	<1	67
H1 2200 10550		0.3	<5	<0.5	3.1	1.3	<1	69
H1 5000 10700		0.2	<5	<0.5	<0.5	0.1	<1	<50
H1 5000 10750		0.4	<5	<0.5	1.2	0.5	<1	140
H1 6800 10350		0.5	<5	<0.5	2.1	0.7	<1	120
H1 6800 10750		0.4	<5	<0.5	2.5	0.9	<1	77
H1 8000 10950		0.9	<5	<0.5	2.7	1.2	<1	91
H1 8000 11000		0.5	<5	<0.5	3.7	1.2	<1	110
H1 8000 11100		0.5	<5	<0.5	3.2	1.3	<1	<50
H1 8000 11175		0.4	<5	<0.5	3.4	1.3	<1	<50
H1 8000 11275		0.5	<5	<0.5	2.1	0.9	<1	95
H1 8000 11325		0.5	<5	<0.5	1.9	1.0	<1	<50
H1 8000 11375		0.4	<5	<0.5	3.1	1.2	<1	91
H1 12001 10550		0.3	<5	<0.5	2.3	0.8	<1	60
H1 12001 10800		1.3	<5	<0.5	2.2	1.2	<1	62
H1 12001 11000		0.8	<5	0.7	4.2	1.5	1	61
H1 48001 10125		0.6	<5	<0.5	4.1	1.6	<1	63
H1 48001 10350		0.4	<5	<0.5	3.5	1.3	<1	51
H1 48001 10500		0.8	<5	<0.5	4.4	1.5	<1	91
H1 48001 10600		0.4	<5	<0.5	2.4	0.9	<1	130
H1 50001 10650		<0.1	<5	<0.5	<0.5	<0.1	<1	64
H1 68001 10700		0.8	<5	<0.5	3.6	1.3	<1	66
H1 68001 10800		0.4	<5	<0.5	3.3	1.3	<1	<50

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Geochemical Lab Report

REPORT: V88-067711.11 (COMPLETE)

Argo (AP)

REFERENCE INFO: LAB CODE #88118-1186

CITIENT: NORANDA EXPLORATION CO. LTD.
PROJECT: 335

SUBMITTED BY: UNKNOWN
DATE PRINTED: 30-SEP-88

ORDER	ELEMENT		NUMBER OF ANALYSES	LOWER DETECTION LIMIT	EXTRACTION	METHOD
1	Au	Gold	22	1 PPM		INST. NEUTRON ACTIV.
2	Ag	Silver	22	2 PPM		INST. NEUTRON ACTIV.
3	As	Arsenic	22	0.5 PPM		INST. NEUTRON ACTIV.
4	Ba	Barium	22	100 PPM		INST. NEUTRON ACTIV.
5	Br	Bromine	22	1 PPM		INST. NEUTRON ACTIV.
6	Cd	Cadmium	22	2 PPM		INST. NEUTRON ACTIV.
7	Co	Cobalt	22	2 PPM		INST. NEUTRON ACTIV.
8	Cr	Chromium	22	10 PPM		INST. NEUTRON ACTIV.
9	Ir	Iridium	22	20 PPM		INST. NEUTRON ACTIV.
10	Mo	Molybdenum	22	0.5 PPM		INST. NEUTRON ACTIV.
11	Ni	Nickel	22	10 PPM		INST. NEUTRON ACTIV.
12	Sb	Antimony	22	0.1 PPM		INST. NEUTRON ACTIV.
13	Se	Selenium	22	5 PPM		INST. NEUTRON ACTIV.
14	Ta	Tantalum	22	0.5 PPM		INST. NEUTRON ACTIV.
15	Th	Thorium	22	0.5 PPM		INST. NEUTRON ACTIV.
16	U	Uranium	22	0.1 PPM		INST. NEUTRON ACTIV.
17	W	Tungsten	22	1 PPM		INST. NEUTRON ACTIV.
18	Zn	Zinc	22	20 PPM		INST. NEUTRON ACTIV.

SAMPLE TYPES	NUMBER	STZF FRACTIONS	NUMBER	SAMPLE PREPARATIONS	NUMBER
0 ORGANIC OR HUMUS	22	0 -20	22	STEF -20	22

REMARKS: SAMPLE ARG 44111 51175 REPEAT = 53 PPM Zn.

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PROJECT: 335

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SAMPLE NUMBER	ELEMENT UNITS	Au PPM	Ag PPM	As PPM	Ba PPM	Br PPM	Cd PPM	Co PPM	Cr PPM	Ir PPM	Mo PPM	Ni PPM
00 ARG 3400 S11551		6	<2	15.0	630	5	2	9	29	<20	2.6	32
00 ARG 3400 S11151		<1	<2	11.0	630	4	<2	8	26	<20	2.2	<10
00 ARG 3400 S11251		2	<2	2.5	160	5	<2	6	<10	<20	11.7	<10
00 ARG 4300 S11325		<1	<2	1.1	180	4	<2	<2	12	<20	1.5	<10
00 ARG 3400 S11375		2	<2	2.3	250	6	<2	3	20	<20	1.0	<10
00 ARG 3400 S11425		1	<2	1.2	150	5	<2	<2	<10	<20	1.4	<10
00 ARG 3400 S11475		2	<2	2.8	440	6	<2	7	<10	<20	1.7	<10
00 ARG 4400 S11100		<1	<2	2.3	410	5	<2	2	12	<20	11.9	<10
00 ARG 4400 S11150		<1	<2	165.0	640	7	<2	8	12	<20	1.4	14
00 ARG 4400 S11110		<1	<2	12.0	340	4	<2	5	17	<20	3.0	<10
00 ARG 4400 S11200		3	<2	1.4	180	3	<2	<2	<10	<20	1.1	<10
00 ARG 4400 S11250		<1	<2	1.3	120	3	<2	<2	<10	<20	11.5	<10
00 ARG 4400 S11300		1	<2	1.7	200	4	<2	<2	<10	<20	1.4	<10
00 ARG 4400 S11350		2	<2	1.2	130	5	<2	<2	<10	<20	11.7	<10
00 ARG 4400 S11175		<1	<2	1.7	610	5	3	5	15	<20	1.7	<10
00 ARG 4400 S11225		2	<2	3.6	490	4	<2	5	18	<20	1.8	<10
00 ARG 5400 S11375		2	<2	6.4	520	4	<2	3	10	<20	4.7	<10
00 ARG 5400 S11875		<1	<2	2.3	870	4	<2	3	24	<20	2.3	<10
00 ARG 5400 S11925		<1	<2	1.2	450	7	<2	3	<10	<20	1.7	<10
00 ARG 5400 S11975		3	<2	11.8	210	4	<2	<2	<10	<20	1.2	<10
00 ARG 5400 S11350		<1	<2	11.0	440	6	<2	9	24	<20	1.2	11
00 ARG 8200 S11100		<1	<2	11.7	320	4	<2	<2	<10	<20	1.1	<10

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Geochemical Lab Report

REPORT: U88-06770.0

PROJECT: 335

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SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Se PPM	Ta PPM	Th PPM	U PPM	W PPM	Zn PPM
00 ARG 3400 S11150		0.8	<5	<0.5	3.8	4.6	<1	140
00 ARG 3400 S11150		0.7	<5	<0.5	4.5	1.4	<1	67
00 ARG 3400 S11250		0.3	<5	<0.5	0.8	0.2	<1	<50
00 ARG 4300 S11325		0.1	<5	<0.5	0.9	0.3	<1	<50
00 ARG 3400 S11375		0.4	<5	<0.5	2.8	0.8	<1	71
00 ARG 3400 S11425		0.2	<5	<0.5	0.7	0.3	<1	<50
00 ARG 3400 S11475		0.3	<5	<0.5	4.1	1.6	<1	92
00 ARG 4400 S11000		0.3	<5	<0.5	2.7	0.7	<1	77
00 ARG 4400 S11150		0.5	<5	<0.5	6.7	1.6	<1	150
00 ARG 4400 S11100		0.2	<5	<0.5	4.5	1.4	<1	150
00 ARG 4400 S11200		0.2	<5	<0.5	0.5	0.2	<1	70
00 ARG 4400 S11250		0.1	<5	<0.5	<0.5	0.1	<1	<50
00 ARG 4400 S11300		0.2	<5	<0.5	1.1	0.4	<1	85
00 ARG 4400 S11350		0.1	<5	<0.5	0.6	0.2	<1	150
00 ARG 4400 S11175		0.4	<5	<0.5	2.9	1.1	<1	75
00 ARG 4400 S1225		0.5	<5	<0.5	3.5	1.1	<1	56
00 ARG 5400 S11375		0.3	<5	<0.5	3.2	1.0	1	100
00 ARG 5400 S11875		0.6	<5	<0.5	2.9	1.1	<1	100
00 ARG 5400 S11925		0.3	<5	<0.5	2.4	4.4	<1	<50
00 ARG 5400 S11975		0.3	<5	<0.5	0.6	0.3	<1	140
00 ARG 5400 S11350		0.9	<5	<0.5	5.9	1.5	<1	100
00 ARG 8200 S1100		0.1	<5	<0.5	1.3	0.2	<1	<50

Bondar-Clegg & Company Ltd.
 130 Pemberton Ave.
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Geochemical Lab Report

REPORT: V88-07424.0 (COMPLETE)

Argo (AP)

REFERENCE INFO: LAB CODE #88 09-012

CLIENT: NORANDA EXPLORATION CO. LTD.
 PROJECT: 335

SUBMITTED BY: UNKNOWN
 DATE PRINTED: 3-OCT-88

ORDER	ELEMENT		NUMBER OF ANALYSES	LOWER DETECTION LIMIT	EXTRACTION	METHOD
1	Au	Gold	52	1 PPM		INST. NEUTRON ACTIV.
2	Ag	Silver	52	2 PPM		INST. NEUTRON ACTIV.
3	As	Arsenic	52	0.5 PPM		INST. NEUTRON ACTIV.
4	Ba	Barium	52	100 PPM		INST. NEUTRON ACTIV.
5	Br	Bromine	52	1 PPM		INST. NEUTRON ACTIV.
6	Cd	Cadmium	52	2 PPM		INST. NEUTRON ACTIV.
7	Co	Cobalt	52	2 PPM		INST. NEUTRON ACTIV.
8	Cr	Chromium	52	10 PPM		INST. NEUTRON ACTIV.
9	Ir	Iridium	52	20 PPM		INST. NEUTRON ACTIV.
10	Mo	Molybdenum	52	0.5 PPM		INST. NEUTRON ACTIV.
11	Ni	Nickel	52	10 PPM		INST. NEUTRON ACTIV.
12	Sb	Antimony	52	0.1 PPM		INST. NEUTRON ACTIV.
13	Se	Selenium	52	5 PPM		INST. NEUTRON ACTIV.
14	Ta	Tantalum	52	0.5 PPM		INST. NEUTRON ACTIV.
15	Th	Thorium	52	0.5 PPM		INST. NEUTRON ACTIV.
16	U	Uranium	52	0.1 PPM		INST. NEUTRON ACTIV.
17	W	Tungsten	52	1 PPM		INST. NEUTRON ACTIV.
18	Zn	Zinc	52	20 PPM		INST. NEUTRON ACTIV.

SAMPLE TYPES	NUMBER	SIZE FRACTIONS	NUMBER	SAMPLE PREPARATIONS	NUMBER
0 ORGANIC OR MINUS	52	0 -20	52	SIFV -20	52

REMARKS: SAMPLE 1400 51225 REPEAT = 37 PPB Au

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PROJECT: 335

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SAMPLE NUMBER	ELEMENT UNITS	Au PPM	Ag PPM	As PPM	Ba PPM	Br PPM	Cd PPM	Co PPM	Cr PPM	Ir PPM	Mn PPM	Ni PPM
00 1400 49825		1	<2	11.8	2611	3	<2	<2	<111	<211	1.4	<10
00 1400 501175		<1	<2	1.3	4511	5	<2	<2	<111	<211	1.1	<10
00 1400 50125		<1	<2	64.2	6311	3	<2	4	49	<211	2.2	<10
00 1400 50175		2	<2	23.11	4711	7	3	11	12	<211	2.5	10
00 1400 502511		<1	<2	9.4	6111	13	<2	14	15	<211	1.11	17
00 1400 503511		2	<2	31.11	5211	7	<2	17	37	<211	1.7	31
00 1400 504011		<1	<2	11.7	3911	4	<2	<2	<111	<211	<11.5	<10
00 1400 50525		1	<2	1.2	2811	4	<2	2	<111	<211	1.1	<10
00 1400 50575		<1	<2	8.3	5911	7	<2	7	17	<211	2.11	<10
00 1400 50625		<1	<2	1.1	2111	7	<2	<2	<111	<211	3.1	<10
00 1400 50675		<1	<2	11.6	4311	3	<2	<2	<111	<211	11.8	<10
00 1400 50725		<1	<2	1.8	5711	4	<2	111	26	<211	2.11	<10
00 1400 50775		1	<2	11.8	2711	5	<2	<2	<111	<211	1.6	<10
00 1400 50825		2	<2	1.3	2211	8	<2	<2	<111	<211	2.3	<10
00 1400 51225		7	<2	7.7	9811	3	<2	8	51	<211	2.8	11
00 2000 1011111		<1	<2	2.1	6111	6	<2	4	<111	<211	1.7	<10
00 2200 106511		<1	<2	2.1	6911	6	<2	4	<111	<211	1.7	<10
00 2200 107511		2	<2	5.3	6211	5	<2	7	72	<211	1.11	33
00 2400 5011111		<1	<2	4.8	5811	7	<2	9	18	<211	1.6	<10
00 2400 5111511		<1	<2	11.7	1311	5	<2	<2	<111	<211	<11.5	<10
00 2400 502111		<1	<2	1.5	5111	7	2	4	111	<211	1.4	<10
00 2400 503511		1	<2	3.9	2511	3	<2	2	<111	<211	11.7	<10
00 2400 504011		1	<2	2.11	1811	5	<2	2	<111	<211	11.8	<10
00 2400 504511		<1	<2	4.8	3211	9	<2	8	<111	<211	1.11	<10
00 2400 50625		<1	<2	11.7	1411	4	<2	<2	<111	<211	11.6	<10
00 2400 50675		<1	<2	<11.5	<1111	3	<2	<2	<111	<211	<11.5	<10
00 2400 50725		1	<2	1.2	1311	4	<2	<2	<111	<211	1.1	<10
00 2400 50775		<1	<2	3.5	<1111	5	<2	6	<111	<211	11.8	<10
00 2400 50825		1	<2	11.8	1611	5	<2	2	<111	<211	11.8	<10
00 2400 50875		<1	<2	4.11	6411	6	<2	13	311	<211	2.3	22
00 2400 509311		2	<2	2.5	3911	6	<2	6	13	<211	3.3	12
00 3000 101511		<1	<2	2.1	5611	4	<2	4	13	<211	2.3	<10
00 3000 102511		<1	<2	1.9	5711	5	<2	2	13	<211	1.9	<10
00 3000 103111		2	<2	2.7	6711	7	<2	4	19	<211	1.6	<10
00 3000 103511		<1	<2	1.3	9911	5	3	4	<111	<211	2.2	<10
00 3000 105511		<1	<2	1.8	6311	7	<2	4	<111	<211	2.11	<10
00 3000 106511		<1	<2	1.9	8211	6	<2	6	13	<211	1.6	<10
00 3000 107111		<1	<2	2.8	7311	8	<2	7	41	<211	1.9	17
00 3000 108511		<1	<2	2.11	6711	4	<2	6	27	<211	1.8	21
00 3000 109111		<1	<2	1.7	6911	5	<2	4	22	<211	1.6	15

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PROJECT: 335

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SAMPLE NUMBER	FLUX UNITS	Sb PPM	Se PPM	Ta PPM	Th PPM	U PPM	W PPM	Zn PPM
00 1400 49825		11.2	<5	<11.5	11.6	11.3	<1	56
00 1400 501175		11.1	<5	<11.5	11.6	11.2	<1	73
00 1400 50125		1.1	<5	11.6	4.11	1.6	2	71
00 1400 50175		11.9	<5	<11.5	16.11	1.8	<1	290
00 1400 502511		11.4	<5	<11.5	2.2	11.8	<1	67
00 1400 503511		1.5	<5	<11.5	3.4	1.2	<1	1411
00 1400 504111		11.1	<5	<11.5	<11.5	11.2	<1	1311
00 1400 50525		11.3	<5	<11.5	1.2	11.5	<1	<50
00 1400 50575		11.5	<5	<11.5	6.3	1.8	<1	611
00 1400 50625		11.2	<5	<11.5	1.11	11.4	<1	<50
00 14111 50675		11.1	<5	<11.5	11.6	11.2	<1	63
00 14111 50725		11.4	<5	<11.5	3.3	1.4	<1	62
00 14111 50775		11.2	<5	<11.5	11.9	11.4	<1	71
00 14111 50825		11.3	<5	<11.5	1.11	11.6	<1	52
00 14111 51225		1.4	<5	11.6	6.5	1.8	<1	1111
00 20111 1111111		11.3	<5	<11.5	3.5	1.4	<1	<50
00 22111 1116511		11.3	<5	<11.5	3.4	1.4	<1	64
00 22111 1117511		11.8	<5	11.8	4.5	1.3	<1	68
00 24111 5111111		11.5	<5	<11.5	4.8	1.6	<1	94
00 24111 5111511		11.1	<5	<11.5	11.5	11.2	<1	56
00 24111 5112111		11.3	<5	<11.5	1.6	11.5	<1	1311
00 24111 5113511		11.3	<5	<11.5	<11.5	11.2	<1	<50
00 24111 5114111		11.2	<5	<11.5	1.5	11.3	<1	71
00 24111 5114511		11.3	<5	<11.5	3.1	11.9	<1	83
00 24111 511625		<11.1	<5	<11.5	<11.5	11.1	<1	61
00 24111 511675		<11.1	<5	<11.5	<11.5	<11.1	<1	<50
00 24111 511725		11.2	<5	<11.5	1.11	11.3	<1	1411
00 24111 511775		11.2	<5	<11.5	1.8	11.3	<1	2311
00 24111 511825		11.1	<5	<11.5	11.7	11.2	<1	53
00 24111 511875		11.7	<5	11.7	11.11	2.3	<1	1311
00 24111 5119311		11.5	<5	<11.5	3.1	11.8	<1	<50
00 30111 1111511		11.8	<5	<11.5	2.1	11.8	<1	<50
00 30111 1112511		11.4	<5	<11.5	1.4	11.6	<1	1411
00 30111 1113111		11.6	<5	<11.5	2.7	11.11	<1	98
00 30111 1113511		11.3	<5	<11.5	2.5	11.9	<1	1611
00 30111 1115511		11.3	<5	<11.5	3.3	11.3	<1	511
00 30111 1116511		11.4	<5	<11.5	3.11	11.5	<1	96
00 30111 1117111		11.2	<5	<11.5	3.1	11.6	<1	711
00 30111 1118511		11.5	<5	<11.5	3.7	11.5	<1	<50
00 30111 1119111		11.6	<5	<11.5	1.7	11.6	<1	611

REPORT: V88-117474.N

PROJECT: 335

PAGE 2A

SAMPLE NUMBER	ELEMENT UNITS	Au PPM	Ag PPM	As PPM	Ba PPM	Br PPM	Cd PPM	Co PPM	Cr PPM	Tr PPM	Mo PPM	Ni PPM
00 3000 10950		1	<2	1.8	610	7	<2	5	30	<20	1.2	12
00 3000 11000		<1	<2	1.2	680	5	<2	4	21	<20	1.8	<10
00 4000 10225		<1	<2	1.2	540	5	<2	<2	11	<20	1.0	<10
00 4000 10275		1	<2	4.9	870	7	<2	7	15	<20	1.5	26
00 4000 10325		<1	<2	2.9	840	5	<2	4	25	<20	1.3	13
00 4000 10375		<1	<2	1.4	610	6	<2	3	19	<20	1.3	<10
00 4000 10425		2	<2	1.6	370	9	<2	5	15	<20	1.2	<10
00 4000 10475		<1	<2	1.9	1100	4	<2	4	20	<20	2.0	<10
00 4000 10525		<1	<2	3.3	690	5	<2	3	28	<20	1.3	14
00 4000 10575		<1	<2	11.9	150	4	<2	<2	11	<20	2.9	<10
00 4000 10725		24	<2	2.8	390	4	<2	3	16	<20	1.6	<10
00 4000 10775		2	<2	2.4	620	6	<2	7	77	<20	1.7	33



REPORT: U88-117424.11

PROJECT: 335

PAGE 2B

SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Se PPM	Ta PPM	Th PPM	U PPM	W PPM	Zn PPM
00 3000 1095H		11.5	<5	<11.5	3.2	1.6	1	55
00 3000 1100H		11.4	<5	<11.5	2.3	1.9	1	270
00 4000 10225		11.4	<5	<11.5	1.2	1.1	<1	73
00 4000 10275		5.2	<5	<11.5	2.1	1.3	<1	67
00 4000 10325		11.7	<5	<11.5	2.9	1.1	<1	150
00 4000 10375		11.4	<5	<11.5	1.9	1.7	<1	91
00 4000 10425		11.4	<5	<11.5	2.1	1.9	<1	58
00 4000 10475		11.5	<5	<11.5	3.3	1.1	<1	57
00 4000 10525		11.6	<5	11.5	3.7	1.2	<1	<50
00 4000 10575		11.3	<5	<11.5	11.6	11.3	<1	<50
00 4000 10725		11.7	<5	<11.5	1.7	11.6	<1	<50
00 4000 10775		11.7	<5	11.7	2.9	1.2	<1	<50

APPENDIX 2

Rock Sample Descriptions

PROPERTY Argo South

N.T.S.

DATE 18th August

ROCK SAMPLE REPORT

PROJECT 335.

AMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G	A	G	A	G	A	G	A	G	A	G	A	SAMPLED BY
					☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	
R-40130	L 2600 E Δ 50750N well-jointed chert, slightly altered	1-2	Grab														A.P.
R-40131	L 9100 E Δ 51075N well-jointed chert silicified (?)	1%	Grab														A.P.
R-40132	L 9100 E Δ 51075N well-jointed chert silicified	2%	Grab														A.P.
R-40133	L 9100 E Δ 51075N clay alteration collected on chert	-	Grab														A.P.
R-40134	L 6325 E Δ 50450N well-jointed chert oxidized with minor pyrite	2%	Grab														A.P.

G = GEOCHEM

A = ASSAY

PROPERTY

Argo South

N.T.S.

DATE

18th August

PROJECT

335

ROCK SAMPLE REPORT

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
R-40135	Crystal tuff, moderately altered (silica + carbonate alteration observed). Very minor pyrite L 5500 E Δ 50900 N	tr.	grab									A.P.
R-40136	L 4175 E Δ 50230 N silicified chert slightly altered minor pyrite	1%	grab									A.P.
R-40137	L 4450 E Δ 50075 N silicified chert slightly altered oxidized	tr.	grab									A.P.
R-40138	L 3425 E Δ 50075 N fault breccia, carbonatized minor clay alteration no sulphides observed	—	grab									
R-40139	L 3375 E Δ 50075 N oxidized chert	1%	grab									A.P.

G = GEOCHEM

A = ASSAY

PROPERTY Argo SouthN.T.S. 18th August
DATE
PROJECT 335

ROCK SAMPLE REPORT

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
R-40140	L 3350 E Δ 50075 N oxidized chert	1%	grab									A. P.
R-40141	L 5800 E Δ 50525 N silicified chert minor alteration very minor sulphides	tr.	grab									A. P.
R-40142	L 3500 E Δ 50075 N oxidized chert with minor sulphides	2%	grab									I. P.
R-40143	L 3650 E Δ 50075 N chert with minor silica alteration	—	grab									I. P.
R-40144	L 2125 E Δ 51000 N carbonate alteration in hornfels. (minor alteration) traces of sulphides	tr.	grab.									I. P.

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A = ASSAY

PROPERTY

Argo South

N.T.S.

DATE

18th August

PROJECT

335.

ROCK SAMPLE REPORT

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G	A	G	A	G	A	G	A	G	A	G	A	SAMPLED BY
R-40145	L2125 E Δ 51000 N carbonate alteration in hornfels (minor alteration traces of sulphides)	tr.	grab														A.P.
R-40146	L 2115 2225 E Δ 50800 N Carbonate staining on crystal tuff.	1%	grab														A.P.
R-40147	L 2380 E Δ 50050 N altered chert (silica alteration) disseminated sulphides	1%	grab														A.P.
R-40148	L 1475 E Δ 50375 N acid volcanic (non foliated crystal tuff) No alteration	2%	grab														A.P.
R-40149	L 1775 E Δ 50575 N Carbonate alteration in chert (no sulphides observed).	—	grab														A.P.

G = GEOCHEM

A = ASSAY

PROPERTY ARGO NORTH

N.T.S. _____

DATE AUGUST 24 198

ROCK SAMPLE REPORT

PROJECT 335

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G	A	G	A	G	A	G	A	G	A	G	A	SAMPLED BY
					☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	
39747	L 1+00E Δ 10525N Coarse white limestone with grey sugary carbonate blobs. Massive, grey to rusty weathering.	>1%	Grab														S.E.R.
39748	L 1+500E Δ 10000N Massive grey recrystallized limestone with white crystallized veins (<2mm)	>1%	Grab														S.E.R.
39749	L 2+250E Δ 10225N Massive grey carbonate with large white carbonate veins	>1%	Grab														S.E.R.
39750	L 2+500E Δ 10125N Green intermediate intrusive dyke? Up to 10% sulfides, very carbonate rich	10%	Grab														S.E.R.

G = GEOCHEM

A = ASSAY

N.T.S. _____

PROPERTY ARGO NORTHDATE AUGUST 24/88

ROCK SAMPLE REPORT

PROJECT 335

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
2-40109	L 2+750 E Δ 10175 N Dark green intermediate intrusive dyke? Up to 10% sulphides, very carbonate rich	10%	Grab									S.E.R.
2-40110	L 3+250 E Δ 10125 N Grey fine phaneritic limestone with white crystalline randomly orientated veinlets	>1%	Grab									S.E.R.
2-40111	L 3+000 E Δ 10800 N Pale green foliated limestone. (Marble) Weathers white-tan, no visible sulphides.	>1%	Grab									S.E.R.
2-40112	L 3+000 E Δ 10750 N Pale green to tan foliated carbonate. White to grey, rusty coloured.	>1%	Grab									S.E.R.

G = GEOCHEM

A = ASSAY

N.T.S. _____

PROPERTY ARGO NORTHDATE AUGUST 24/88

ROCK SAMPLE REPORT

PROJECT 335

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
2-40113	L 2+300 E Δ 10425N Grey recrystallized limestone with white carbonate veins No visible sulfides.	>1%	Arch									S.E.R.
2-40114	L 3+800 E Δ 10125N White chalk colour limestone interbedded with grey recrystallized limestone w/ calcite veins. Sample taken across fault.	>1%	Arch									S.E.R.
2-40115	L 3+810 E Δ 10130N Grey recrystallized limestone and interbedded white/ chalk limestone.	>1%	Arch									S.E.R.
2-40116	L 4+200 E Δ 10300N Grey recrystallized limestone. Numerous calcite veins 11 to strike - Local faulting	>1%	Arch									S.E.R.

G = GEOCHEM

A = ASSAY

N.T.S. _____

PROPERTY ARGO NORTHDATE AUGUST 24/88

ROCK SAMPLE REPORT

PROJECT 335

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G	A	G	A	G	A	G	A	G	A	G	A	SAMPLED BY
-40117	L 5+000E Δ 10675N Grey recrystallized limestone with calcite veins randomly orientated	>1%	Grdb														S.E.R.
-40118	L 5+200E Δ 10525N Rusty coloured, grey recrystallized limestone with with white calcite veins.	>1%	Grdb														S.E.R.
-40120	L 14+500E Δ 10300N Grey to silver, rusty, micaceous quartzite. Well lenseated / folded. up to 1% sulphides.	1%	Grdb														S.E.R.
-40121	L 14+500E Δ 10310N Grey to silver, rusty, micaceous quartzite. Well lenseated. up to 1% sulphides.	1%	Grdb														S.E.R.

G = GEOCHEM

A = ASSAY

N.T.S. _____

PROPERTY ARGO NORTHDATE AUGUST 24 1988

ROCK SAMPLE REPORT

PROJECT 335

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
2-40122	L 14+300 E Δ 10350 N Grey to silver, rusty micaceous quartzite. mm size quartz veinlets 11 to strike. up to 5% sulphides.	5%	Grab									S.E.R.
2-40123	L 14+275 E Δ 10600 N Rusty, grey to silver, silicified quartzite. up to 10-15% sulphides. Sulphides soft, weathered out. Visible quartz veins.	10-15%	Grab									S.E.R.
2-40124	L 14+275 E Δ 10625 N Rusty, grey to silver, silicified quartzite. up to 10-15% sulphides. Sulphides, weathered out. Visible quartz veins.	10-15%	Grab									S.E.R.

G = GEOCHEM

A = ASSAY

N.T.S.

PROPERTY ARGO NORTH

DATE AUGUST 24/88

ROCK SAMPLE REPORT

PROJECT 335

[illegible]

G = GEOCHEM

A = ASSAY

N.T.S. _____

PROPERTY Hemlo ExplorationDATE August 28/88

ROCK SAMPLE REPORT

PROJECT 334

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	G ☐ A ☐	SAMPLED BY
2-40152	L 11000 E Δ 49900 N Rusky, light green- apple green jasper chert. Weakly to moderately silicified up to 7% sulphides	7%	Grub									S.E.R.
2-40153	L 11200 E Δ 49860 N Rusky mafic to intermediate volcanic with carbonate veins. up to 1% sulphides	1%	Grub									S.E.R.
2-40154	L 11400 E Δ 50200 N Intermediate volcanic with chert Carbonate rich. 2% sulphides	2%	Grub									S.E.R.
40155	L 11400 E Δ 49900 N Apple green massive chert. Less than 1% sulphides.	>1%	Grub									S.E.R.

G = GEOCHEM

A = ASSAY

PROPERTY Hemlo Exploration

N.T.S. _____

DATE August 28/88

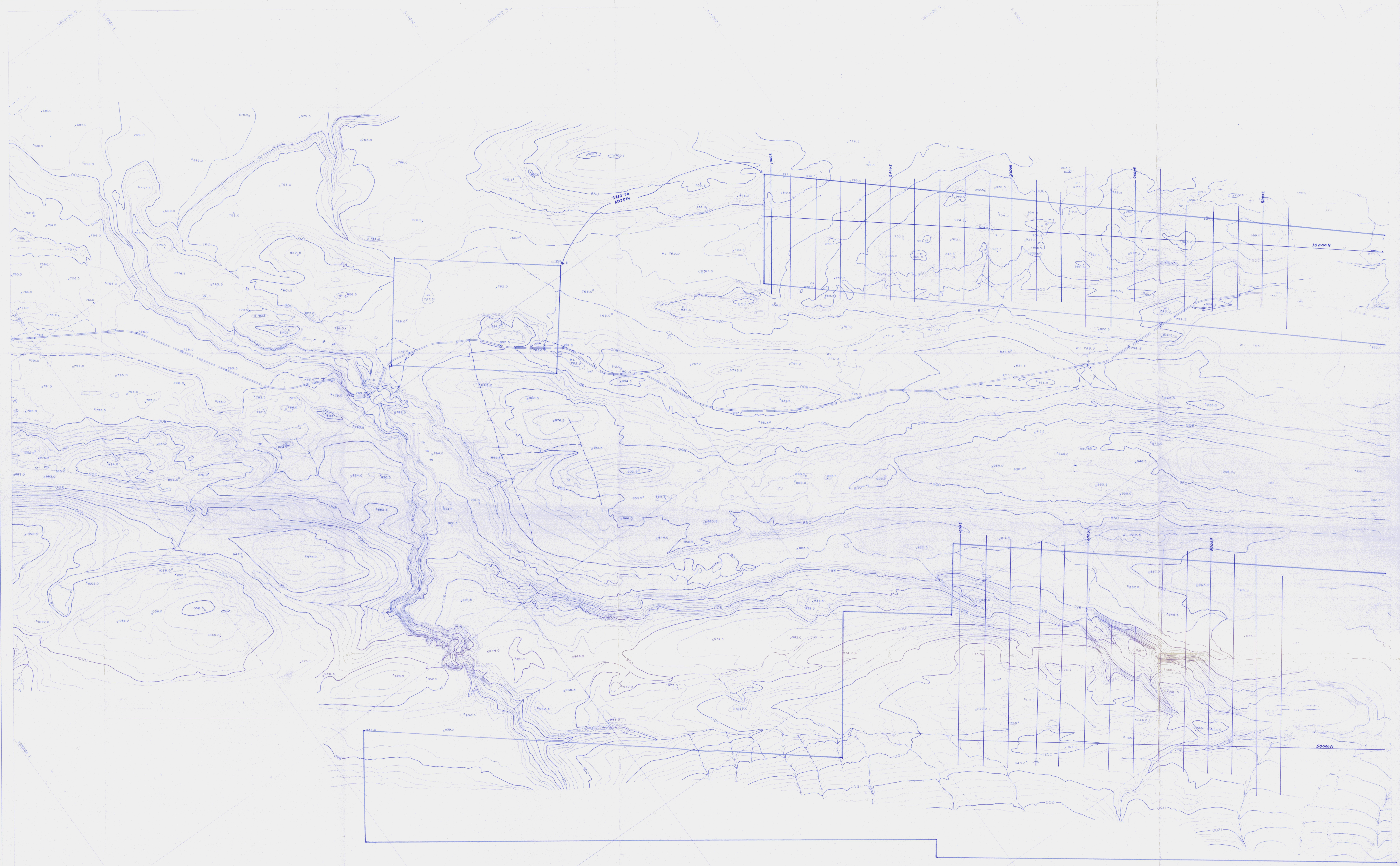
ROCK SAMPLE REPORT

PROJECT 334

SAMPLE NO.	LOCATION & DESCRIPTION	% SULPHIDES	TYPE	WIDTH	G	A	G	A	G	A	G	A	G	A	G	A	SAMPLED BY
					☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	☐	
2-40156	L 11600E Δ 49900N Light green - apple green chert with hematite. Up to 2% sulphides	2%															S.E.R.
2-40157	L 11600E Δ 50250N Apple green chert (volcanics) hematite moderate carbonate alteration. No visible sulphides	>1%															S.E.R.
2-40158	L 11900E Δ 50300N Light green chert and inter- mediate volcanics. No visible sulphides	>1%															S.E.R.
2-40159	L 12000E Δ 50125N Light green to grey chert with hematite. No visible sulphides.	>1%															S.E.R.

G = GEOCHEM

A = ASSAY



092635

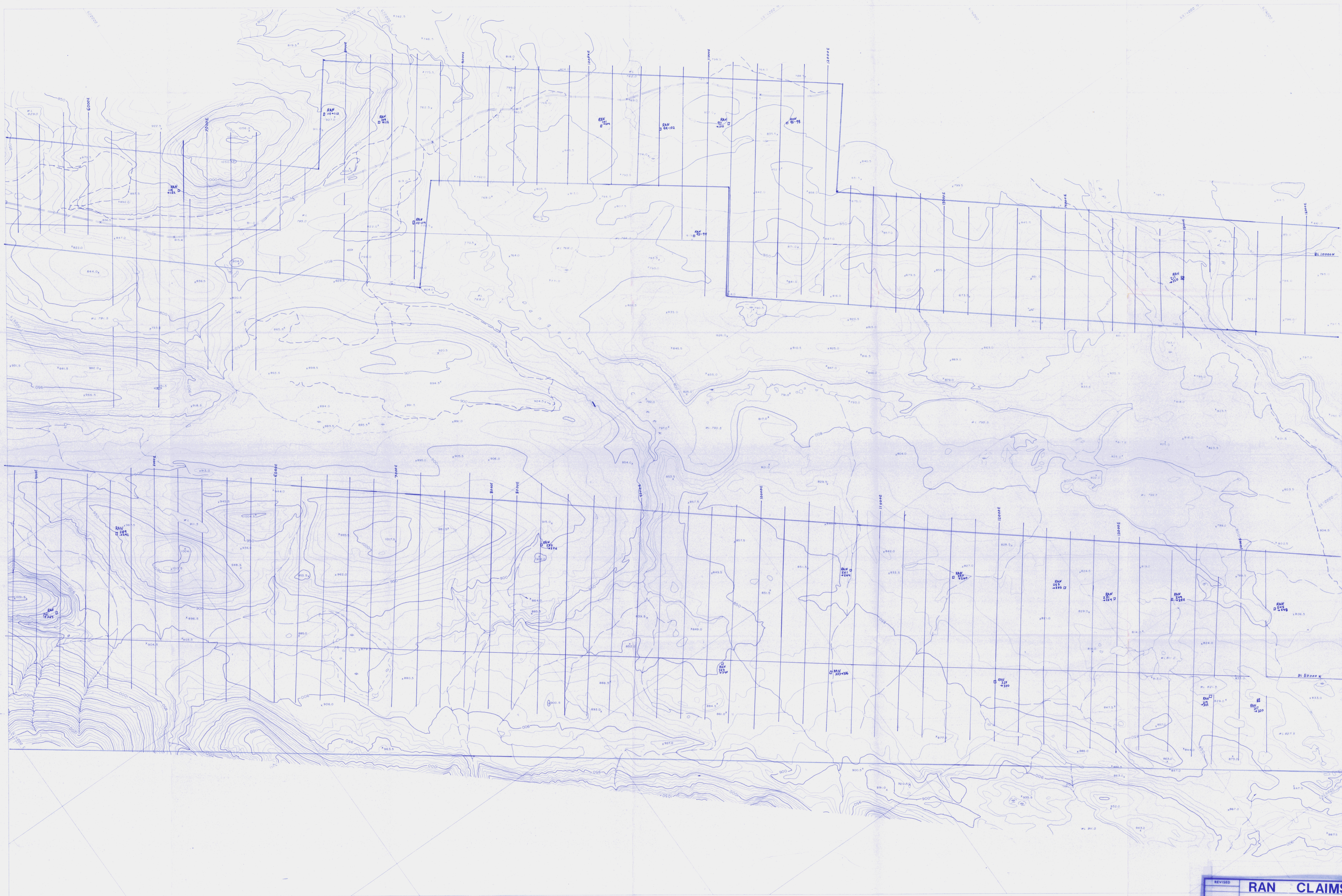
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THE METRO-TECH GROUP LTD.
100-100 ALBERT STREET, VANCOUVER, B.C. V6A 1G1
COMPILED FROM DEPT. PHOTOGRAPHY TAKEN IN 1961
AT AN AIRBORNE PHOTO SCALE OF 1:50,000
DATE COMPLETED: MARCH 1988
SHEET NUMBER: 7 OF 8



THE METRO-TECH GROUP LTD.
100-100 ALBERT STREET, VANCOUVER, B.C. V6A 1G1
COMPILED FROM DEPT. PHOTOGRAPHY TAKEN IN 1961
AT AN AIRBORNE PHOTO SCALE OF 1:50,000
DATE COMPLETED: MARCH 1988
SHEET NUMBER: 7 OF 8

REVISED	RAN CLAIMS WEST	
PROJ. NO. 325	SURVEY BY	DATE Dec/88
ALTA 05 015 K/2	DRAWN BY	
7	NORANDA EXPLORATION	
	OFFICE KASE	



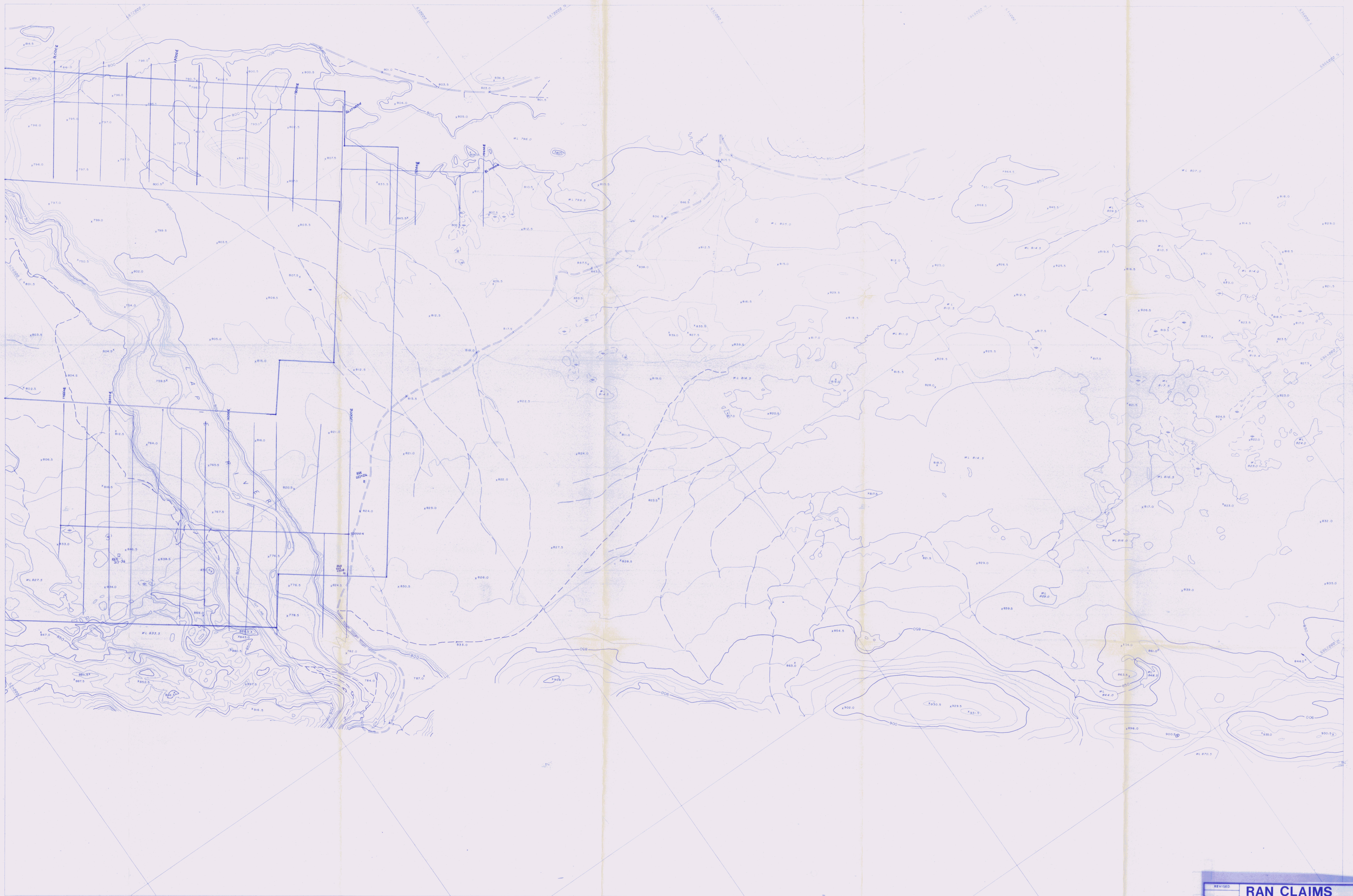
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SHEET INDEX



THE MCLENNAN GROUP LTD.
200-1166 ALBERTA STREET, VANCOUVER, B.C. V6C 1G4
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
AT AN APPROXIMATE SCALE OF 1:50000
MAP SCALE 1:10,000
DATE COMPILED 10-MARCH-1968
CONTOUR INTERVAL 10 METRE
SHEET NUMBER 3 OF 8

REVISED	RAN CLAIMS	
	CENTRAL	
	092635 9/10	
PROJ. NO.	SURVEY BY	DATE
N.T.S.	DRAWN BY	SCALE
TRANS. NO.	NORANDA EXPLORATION	
8	OFFICE	



8	7	6	5	4	3	2	1
SHEET INDEX							

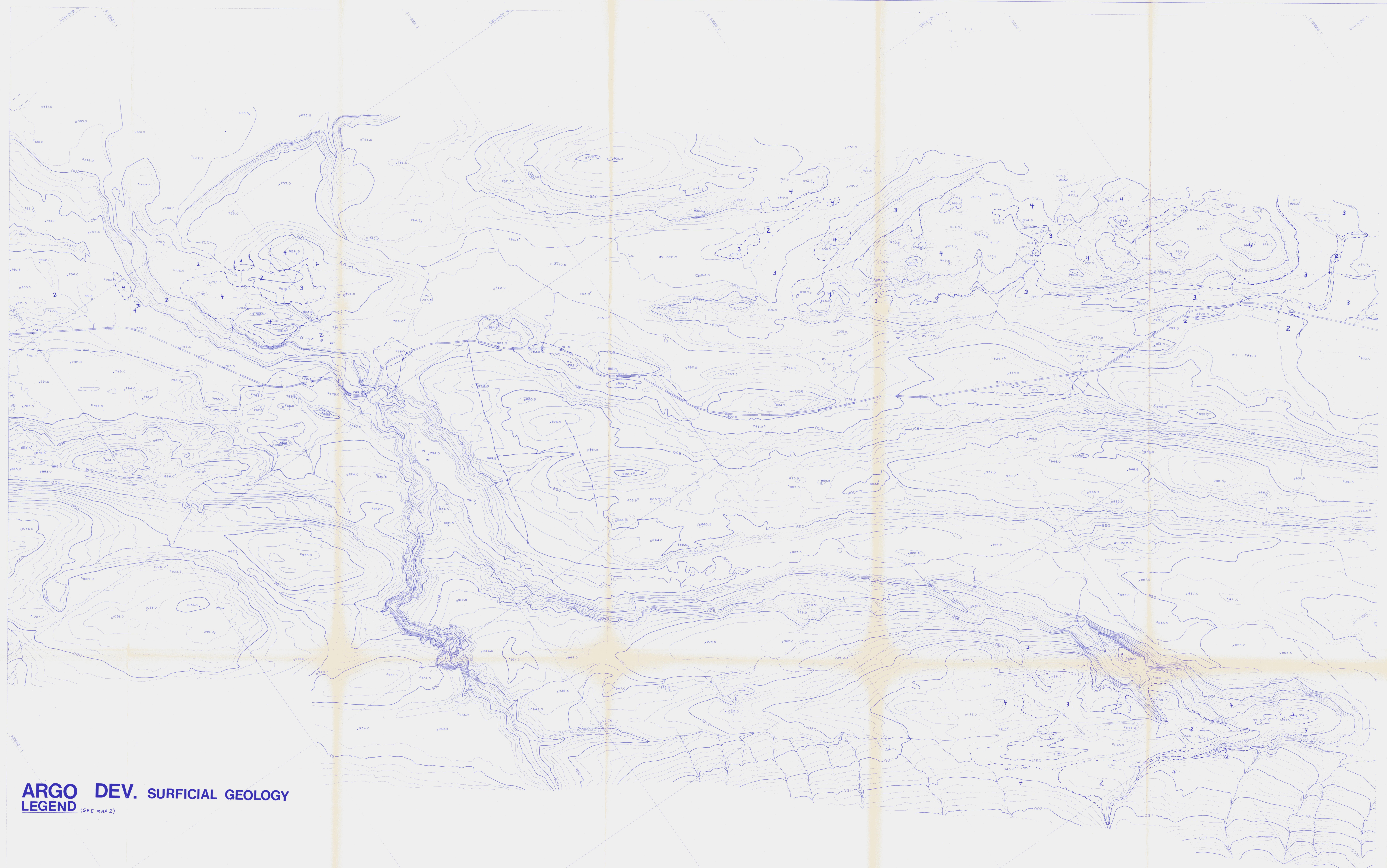
PRELIMINARY RECONNAISSANCE TYPE MAPPING
SCALE AND ELEVATION DATUM BASED ON LIMITED GROUND CONTROL
RESULTING IN GOOD RELATIVE BUT UNCERTAIN MAP ACCURACY.



THE MCELHANEY GROUP LTD.
200-1166 ALBERNI STREET, VANCOUVER, B.C. (604) 683-8521
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
AT AN APPROXIMATE SCALE OF 1:155000

MAP SCALE	1:10,000
CONTOUR INTERVAL	10 METRE
DATE COMPILED	10-MARCH 1988
SHEET NUMBER	2 OF 8

REVISED	RAN CLAIMS	
	EAST	
	092635 917	
MAP No.	SHEET No.	DATE
9		
NORANDA EXPLORATION		
OFFICE		



ARGO DEV. SURFICIAL GEOLOGY
LEGEND (SEE MAP 2)

8 7 6 5 4 3 2 1
SHEET INDEX



THE McELVANEY GROUP LTD.
220-1186 ALBERT STREET, VANCOUVER, B.C. V6A 4G9
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
AT AN APPROXIMATE SCALE OF 1:50,000
MAP SCALE 1:10,000
DATE 1978
COMPILED 10 MARCH 1988
CONTOUR INTERVAL 10 Meters
SHEET NUMBER 4 OF 5
REF. NO. 11582

REVISED	RAN CLAIMS WEST	
NO. 336	Surveyed by AP, IP	DATE Dec/88
INTL 1:250,000	092635 918	
DWG. NO. 10	NORANDA EXPLORATION	
	OFFICE	



ARGO DEV. SURFICIAL GEOLOGY (map 2)

- 2 SAND AND GRAVEL**
Includes modern alluvium, fluvial terraces, alluvial fan and proglacial outwash. Gravelly to well stratified sand and gravel with laminated sandy layers. Variable thickness (2m to 2m).
- 3 MCCONNELL TILL**
Compact to loose, grey, locally calcareous, pebbly to cobbly till, silty and locally sandy where returned. Variable thickness (10 to 15m).
- 4 BEDROCK**
Closely spaced outcrops and bedrock covered by less than 0.5m of unconsolidated sediments (usually till); includes colluvium and crushed bedrock.

SHEET INDEX
8 7 6 5 4 3 2 1

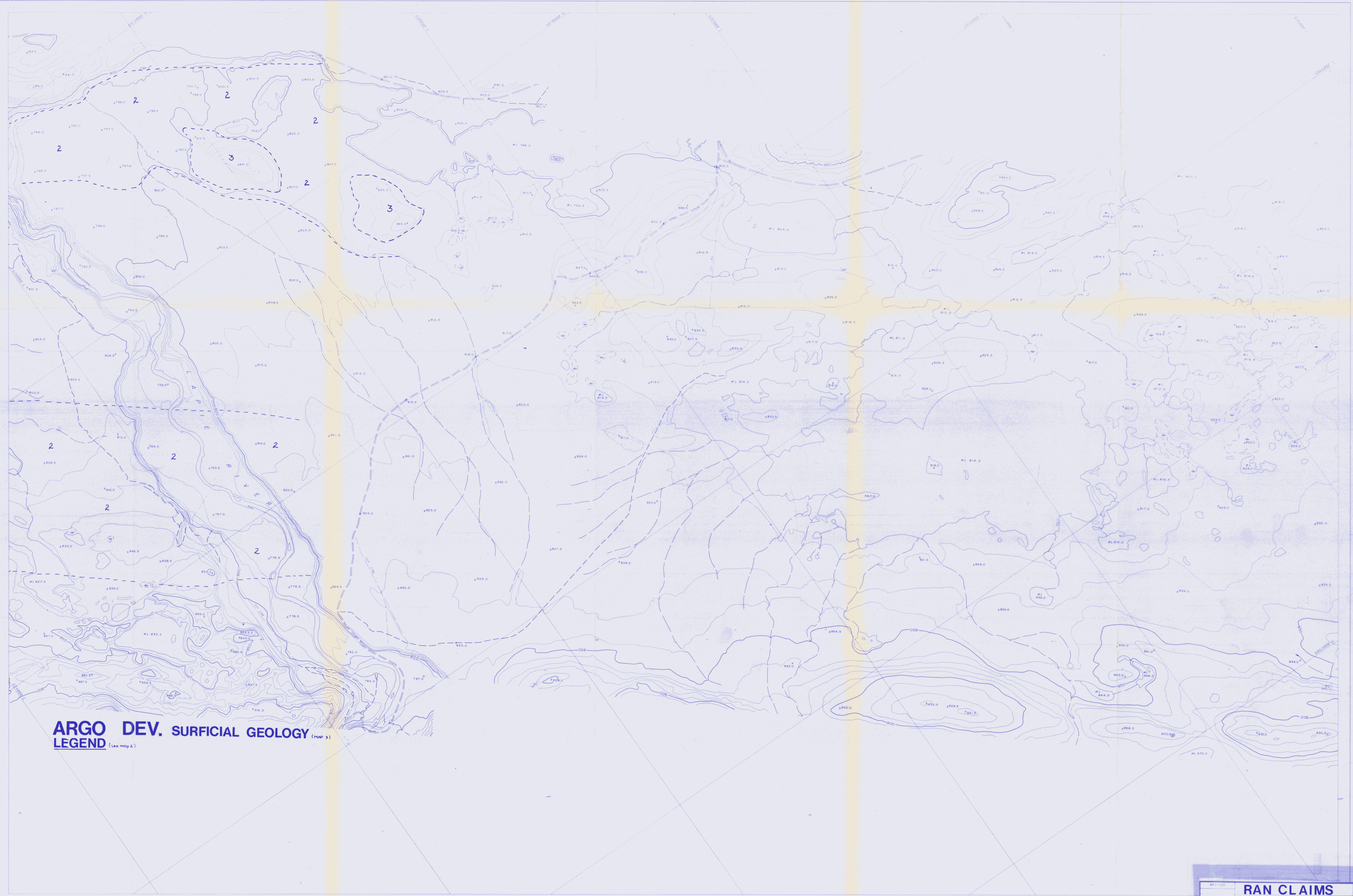
PRELIMINARY RECONNAISSANCE TYPE MAPPING
SCALE AND ELEVATION DATA BASED ON LIMITED GROUND CONTROL
RESULTING IN GOOD RELATIVE BUT UNCERTAIN MAP ACCURACY.



THE MCELHENNY GROUP LTD.
200-1166 ALBERTA STREET, VANCOUVER, B.C. V6C 4G3
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
DT ON APPROXIMATE SCALE OF 1:50,000
MAP SCALE 1:10,000
DATE COMPILED 10 MARCH 1988
CONTOUR INTERVAL 10 METERS
SHEET NUMBER 3 OF 8

REF. NO. 11530

REVISED	RAN CLAIMS
	092635
	CENTRAL 919
PROJ. NO. 335	SURVEY BY: AP I P
DATE: DEC/88	SCALE
REVISIONS: 1/15/82	DRAWN BY: KR
11	NORANDA EXPLORATION
	OFFICE



ARGO DEV. SURFICIAL GEOLOGY (MVP 3)
LEGEND (see map 2)



8	7	6	5	4	3	2	1
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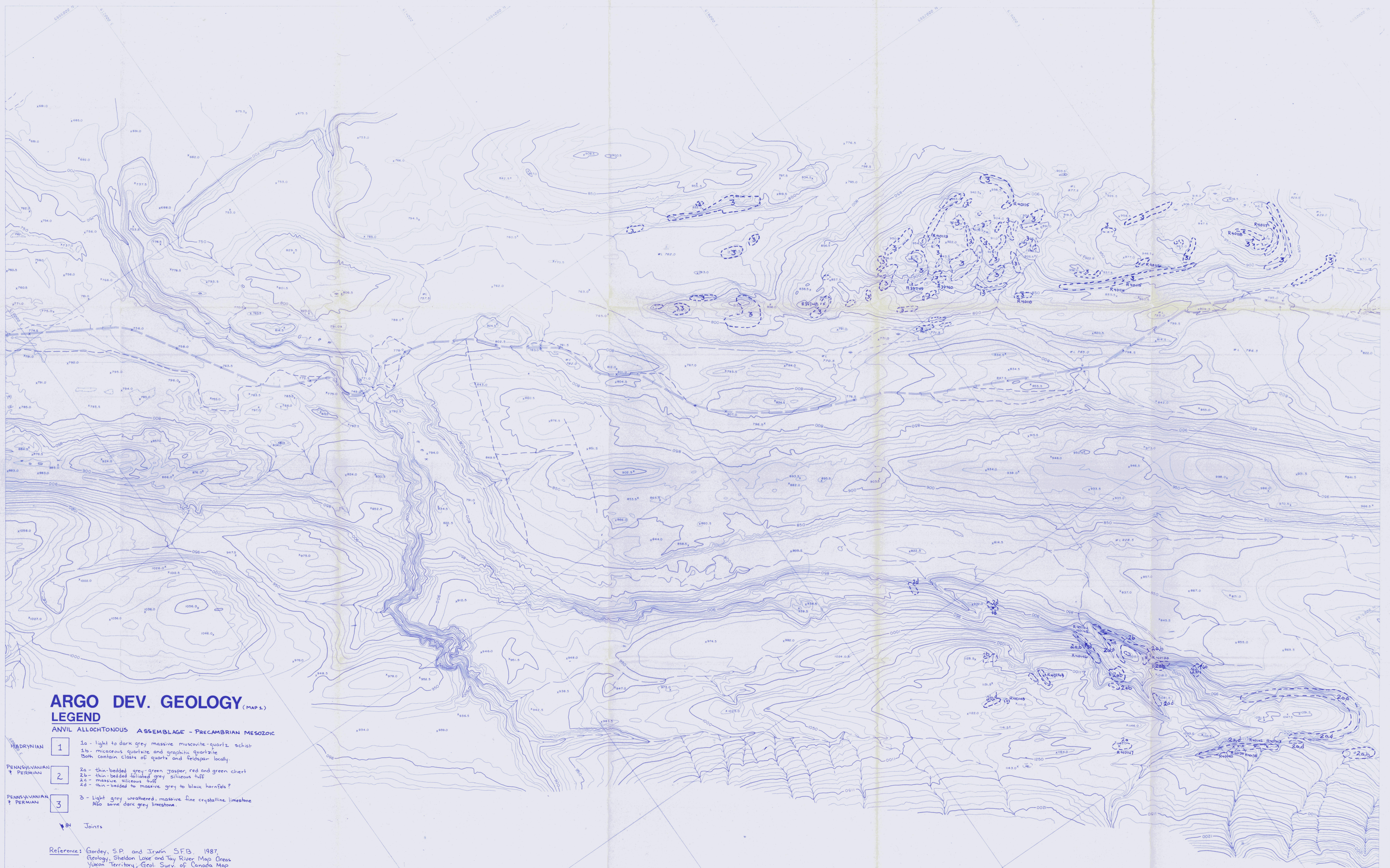
SHEET INDEX



THE MCELHANEY GROUP LTD.
200-1165 ALBERNI STREET, VANCOUVER, B.C. (604) 683-9581
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
AT AN APPROXIMATE SCALE OF 1:55,000
MAP SCALE 1:10,000
DATE COMPILED 10-MARCH 1988
SHEET NUMBER 2 OF 8
CONTOUR INTERVAL 10 METRE

PRELIMINARY RECONNAISSANCE TYPE MAPPING
SCALE AND ELEVATION DATUM BASED ON LIMITED GROUND CONTROL
RESULTING IN GOOD RELATIVE BUT UNCERTAIN MAP ACCURACY.
REF. NO. 11538-

REVISED	RAN CLAIMS EAST		930
	092635		
MAP NO. 935	SURVEY BY AP TP	DATE Dec/88	
1:105,000	KR		
DWG. NO.	NORANDA EXPLORATION		
12	DEVELOP		



ARGO DEV. GEOLOGY (MAP 1) LEGEND

ANIL ALLOCHTHONOUS ASSEMBLAGE - PRECAMBRIAN MESOZOIC

- 1a - light to dark grey massive muscovite-quartz schist
1b - micaceous quartzite and graphitic quartzite
Both contain clasts of quartz and feldspar locally.
- 2a - thin-bedded grey-green Jasper, red and green chert
2b - thin-bedded foliated grey siliceous tuff
2c - massive siliceous tuff
2d - thin-bedded to massive grey to black hornfels?
- 3 - light grey weathered, massive fine crystalline limestone
Also some dark grey limestone.

Joint

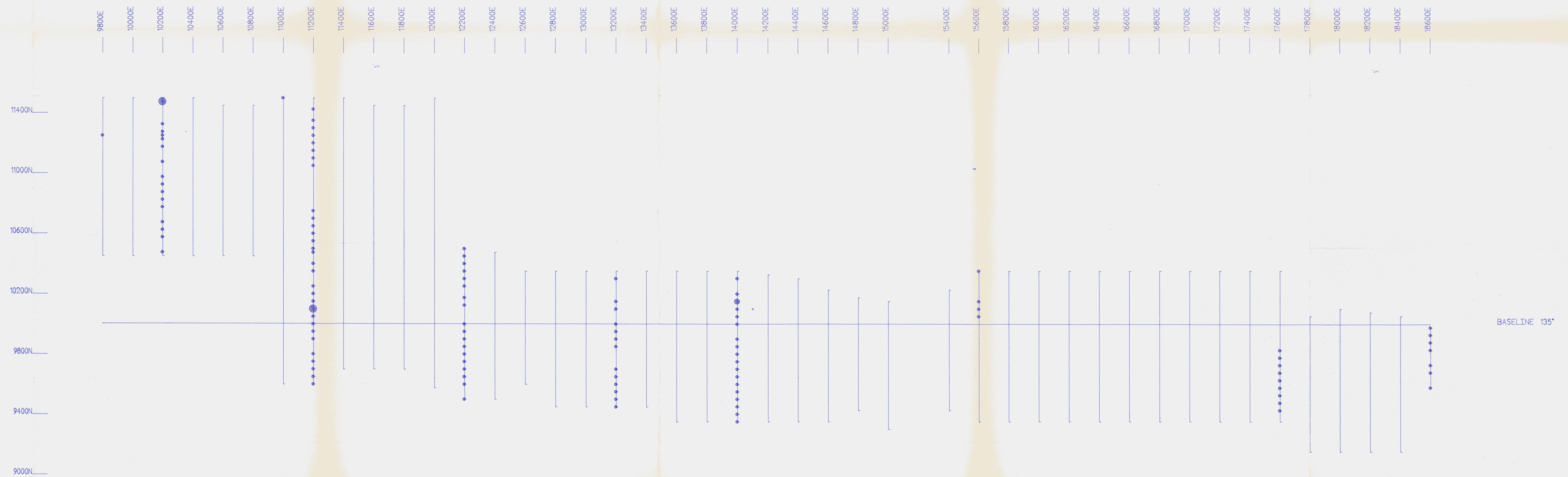
Reference: Gordon, S.P. and Irwin, S.F.B. 1987,
Geology, Sheldon Lake and Tay River Map Areas
Yukon Territory, Geol. Surv. of Canada Map
19-1987 3 Sheets scale 1:250,000.

8 7 6 5 4 3 2 1
SHEET INDEX



THE MCELLENNAN GROUP LTD.
200-1166 ALBERTA STREET, VANCOUVER, B.C. (604) 683-8521
COMPILED FROM AERIAL PHOTOGRAPHY TAKEN IN 1967
AT AN APPROXIMATE SCALE OF 1:50,000
MAP SCALE 1:100,000
DATE COMPILED 18-MARCH 1988
CONTOUR INTERVAL 10 METRE
SHEET NUMBER 4 OF 8

REVISED	RAN CLAIMS	
	WEST 092435	
PROJ. NO. 933	SURVEY BY SR, AP, LP	DATE Dec/88
W. 105 615K2	DRAWN BY KR	SCALE 1:100,000
13	NORANDA EXPLORATION	
	OFFICE	



Contour Interval : 1

200m 100m 0m 200m 400m

15

923

ARGO (NORTHEAST)

GEOCHEMICAL SURVEY

PPB Au **092635**

PROJECT: ARGO PROJECT # : 335

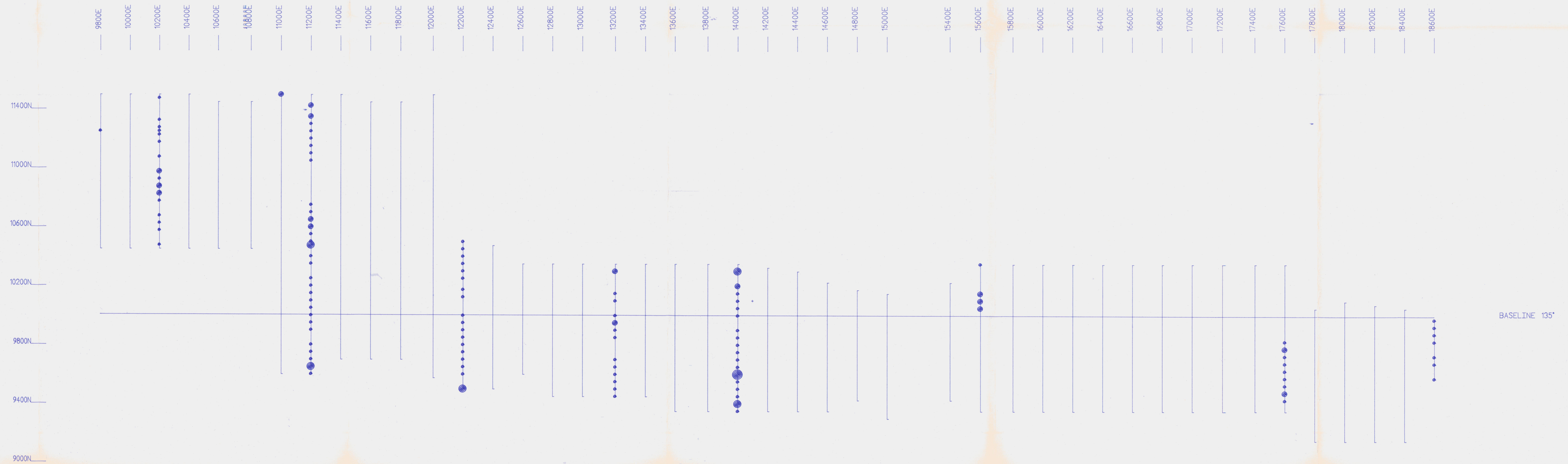
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGN

NORANDA EXPLORATION



Contour Interval :

20m 50m 1m 200m 400m

924

•	•	•	•	•	•	•
>0	>0.30	>0.50	>0.70	>0.90	>1.1	>1.3
<0.30	<0.50	<0.70	<0.90	<1.1	<1.3	
PPM Ag						

ARGO (NORTHEAST)

GEOCHEMICAL SURVEY

PPM Ag

PROJECT: ARGO PROJECT # : 335

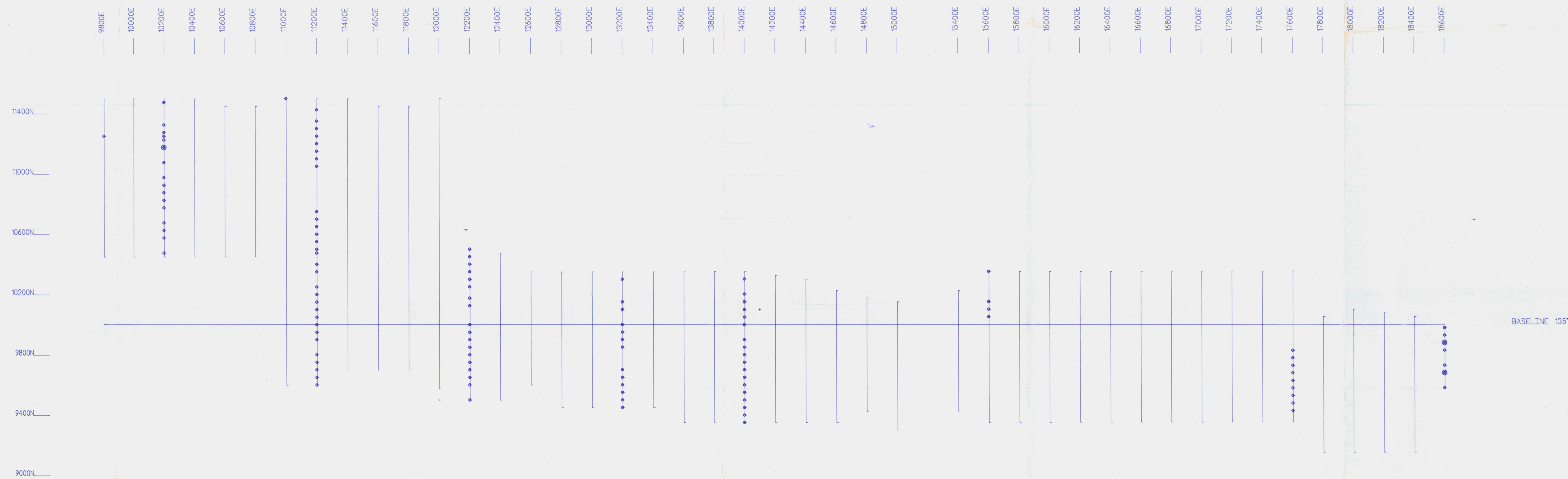
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGN

NORANDA EXPLORATION



Contour Interval :
1

200m 100m 50m 200m 400m

18

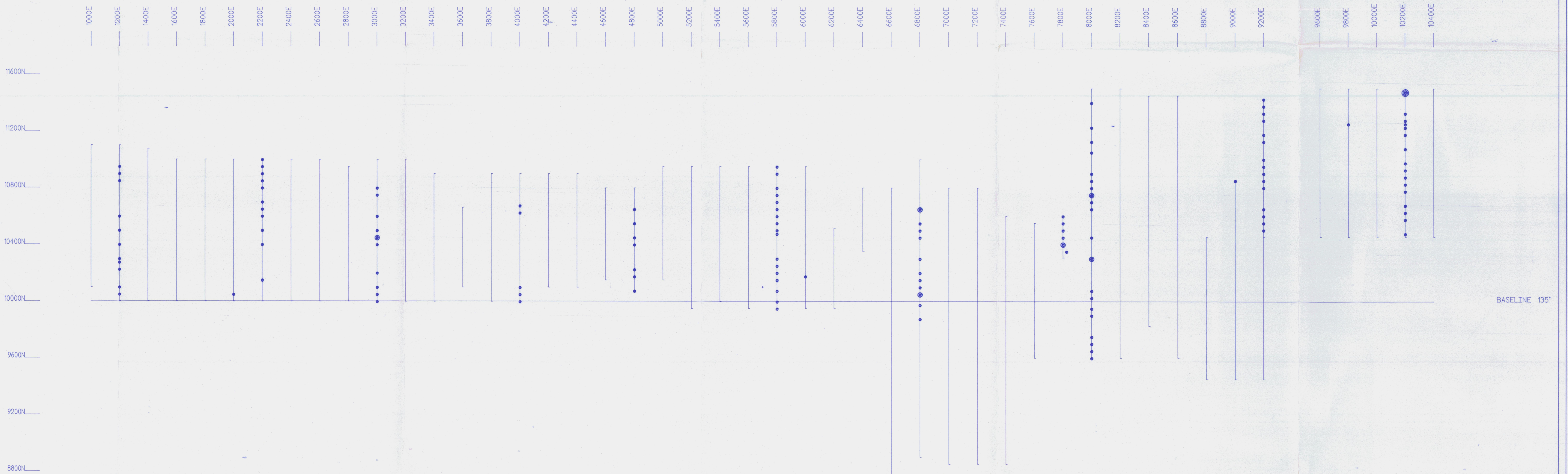
926

ARGO (NORTHEAST)

GEOCHEMICAL SURVEY
PPM As

PROJECT: ARGO PROJECT # : 335
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88
SURVEY BY : AP NTS :
FILE: C335ARGN
NORANDA EXPLORATION



Contour Interval :

200m 100m 0m 200m 400m

10 10 20 30 40 50
<10 <20 <30 <40 <50
100 200 300 400 500

ARGO (NORTHWEST)

GEOCHEMICAL SURVEY

PPB AU

PROJECT: ARGO PROJECT # : **3092635**

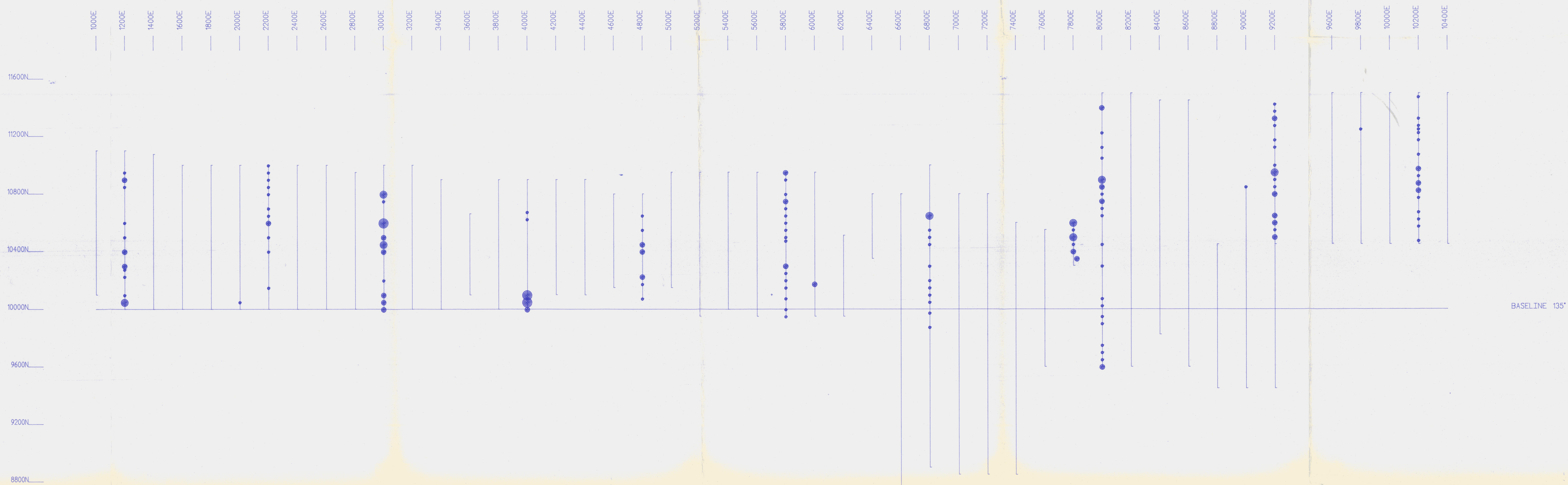
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGN

NORANDA EXPLORATION



Contour Interval :
:

20m 10m 5m 20m 40m

•

>0.30
<0.50

•

>0.50
<0.70

•

>0.70
<0.90

•

>0.90
<1.1

•

>1.1
<1.3

•

>1.3

PPM Ag

928

ARGO (NORTHWEST)

GEOCHEMICAL SURVEY

PPM Ag

PROJECT: ARGO PROJECT # : 33092635

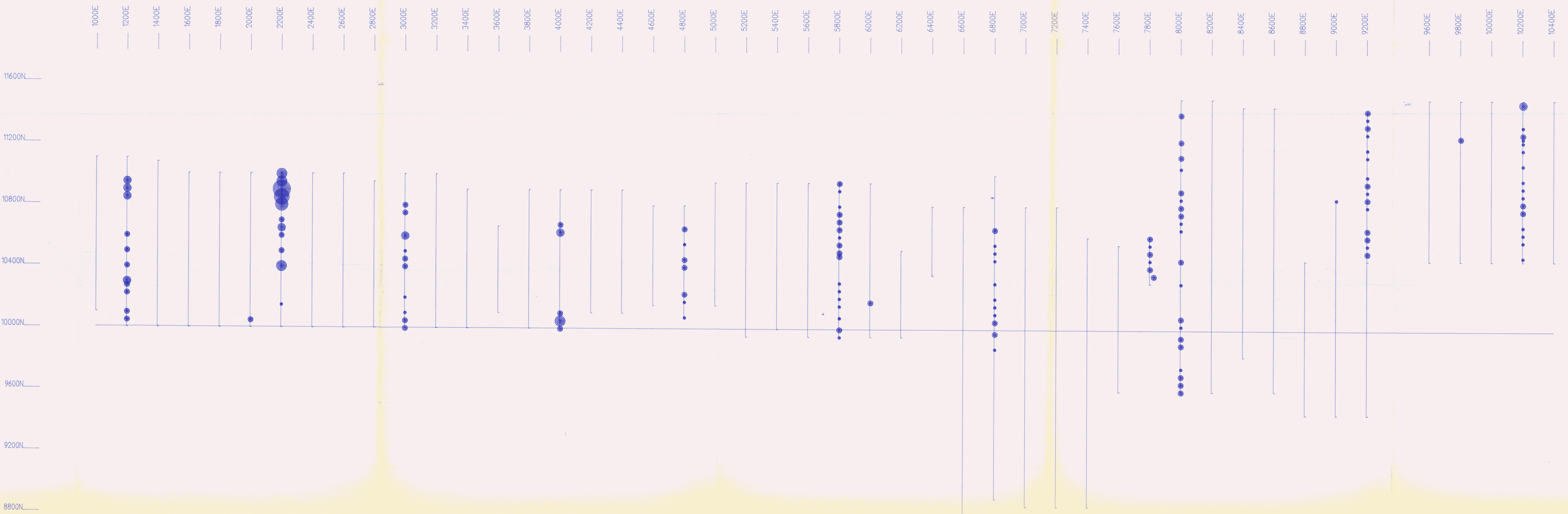
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGN

NORANDA EXPLORATION



Contour Interval :
200m 100m 50m 200m 400m

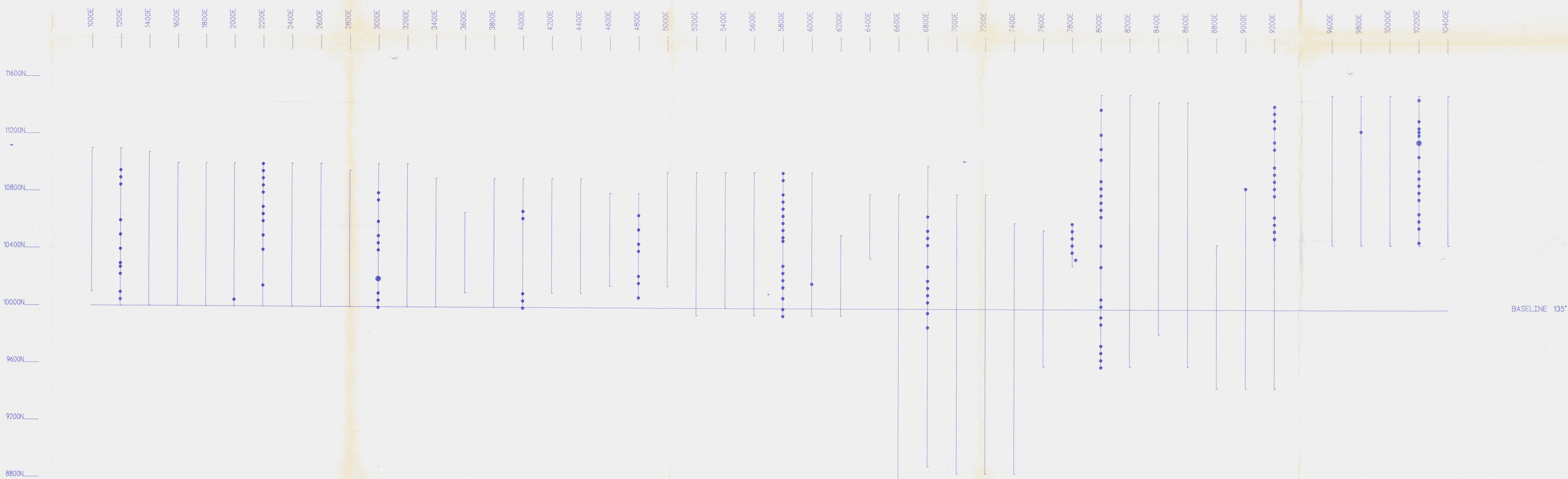
21

• • • • •
100 200 300 400 500 750
100 200 300 400 500 750
PPB Hg

ARGO (NORTHWEST)
GEOCHEMICAL SURVEY
PPB Hg
PROJECT: ARGO PROJECT # : 335
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88
SURVEY BY : AP NTS :
FILE: C335ARGN
NORANDA EXPLORATION

929



Contour Interval : 1

200m 100m 50m 200m 400m

22

930

ARGO (NORTHWEST)

GEOCHEMICAL SURVEY

PPM As

PROJECT: ARGO PROJECT # : 33992635

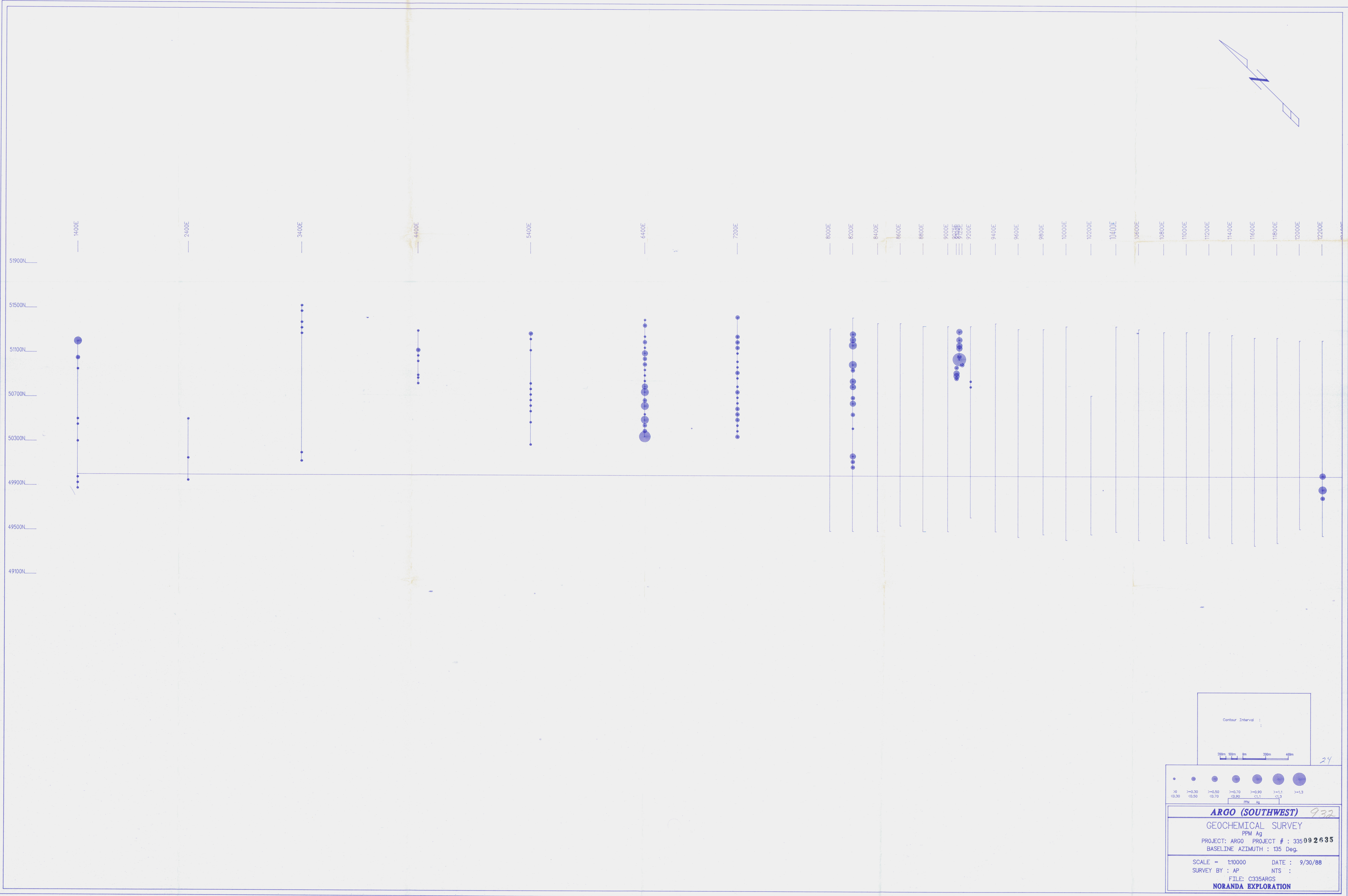
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGN

NORANDA EXPLORATION



Contour Interval :

200m 100m 0m 200m 400m

24

•	•	•	•	•	•	•
<0.30	>=0.30 <0.50	>=0.50 <0.70	>=0.70 <0.90	>=0.90 <1.1	>=1.1 <1.3	>=1.3
PPM Ag						

ARGO (SOUTHWEST) 932

GEOCHEMICAL SURVEY

PPM Ag

PROJECT: ARGO PROJECT # : 335092635

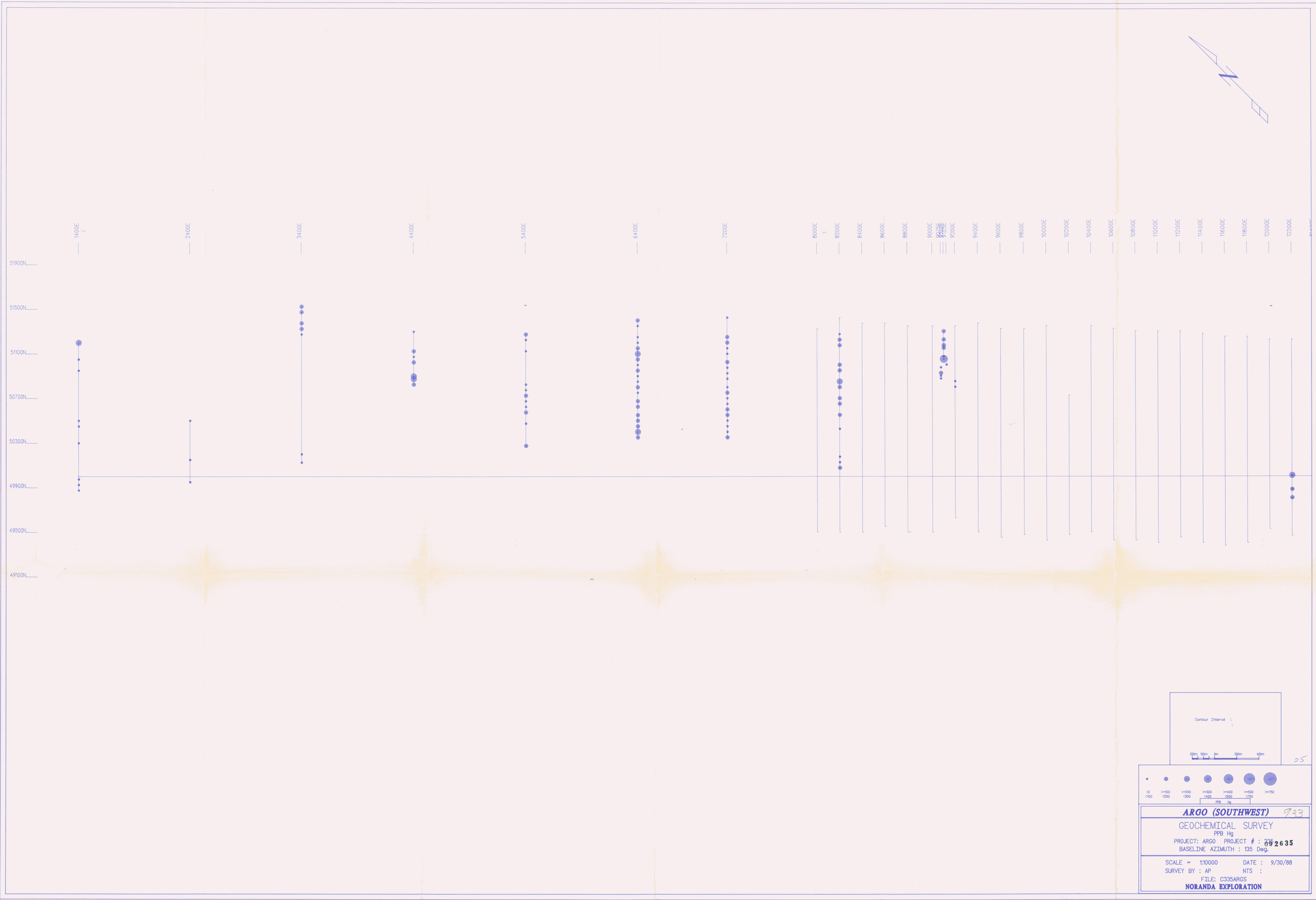
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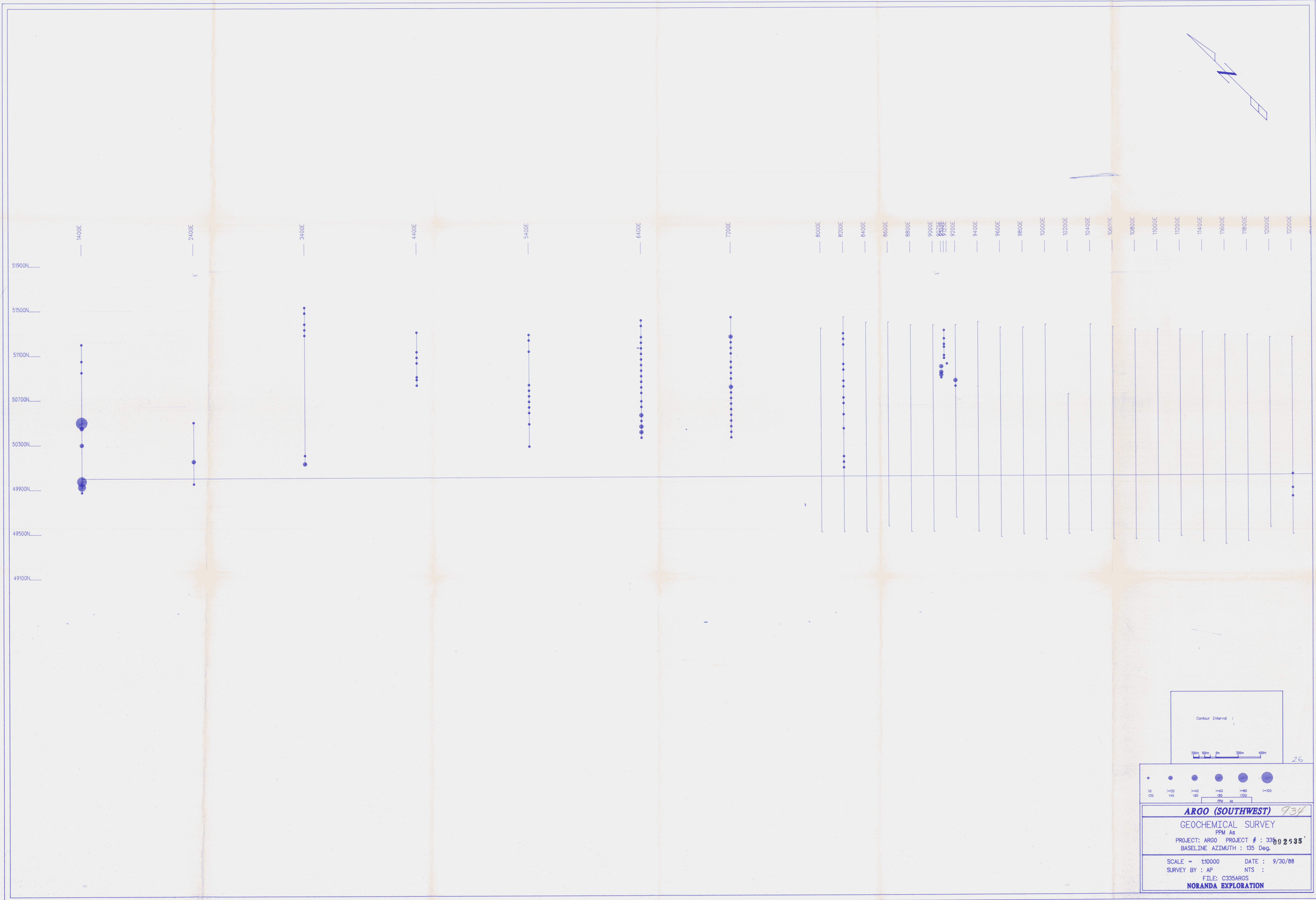
SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGS

NORANDA EXPLORATION





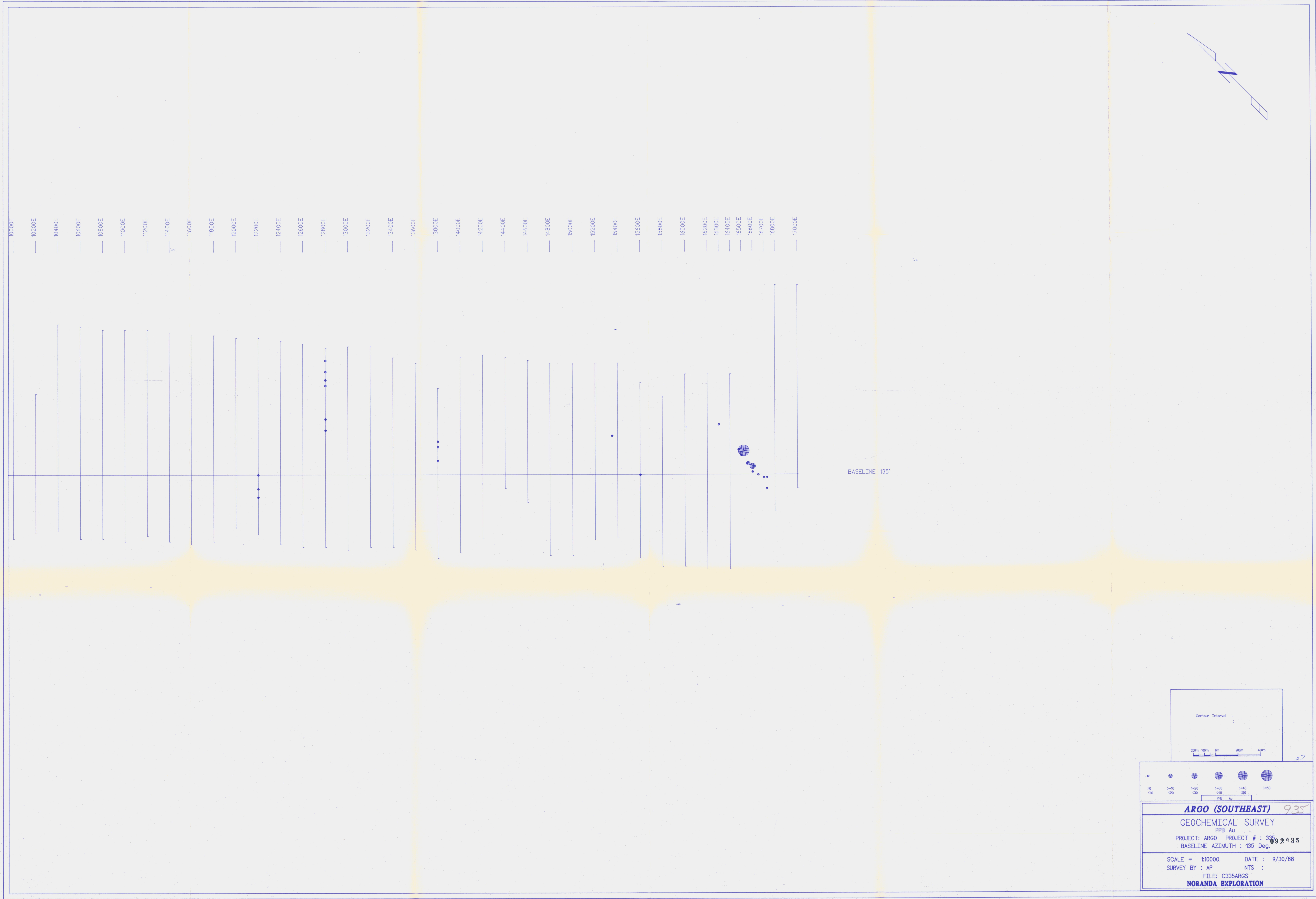
Contour Interval :
200m 100m 50m 200m 400m

26

• • • • •
10 20 40 60 80 100
120 140 160 180 200 220

ARGO (SOUTHWEST) 934
GEOCHEMICAL SURVEY
PPM As
PROJECT: ARGO PROJECT # : 335
BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000 DATE : 9/30/88
SURVEY BY : AP NTS :
FILE: C335ARGS
NORANDA EXPLORATION



Contour Interval :

200m 100m 50m 250m 400m

• >10 >20 >30 >40 >50

PPB Au

ARGO (SOUTHEAST) 935

GEOCHEMICAL SURVEY

PPB Au

PROJECT: ARGO PROJECT # : 335

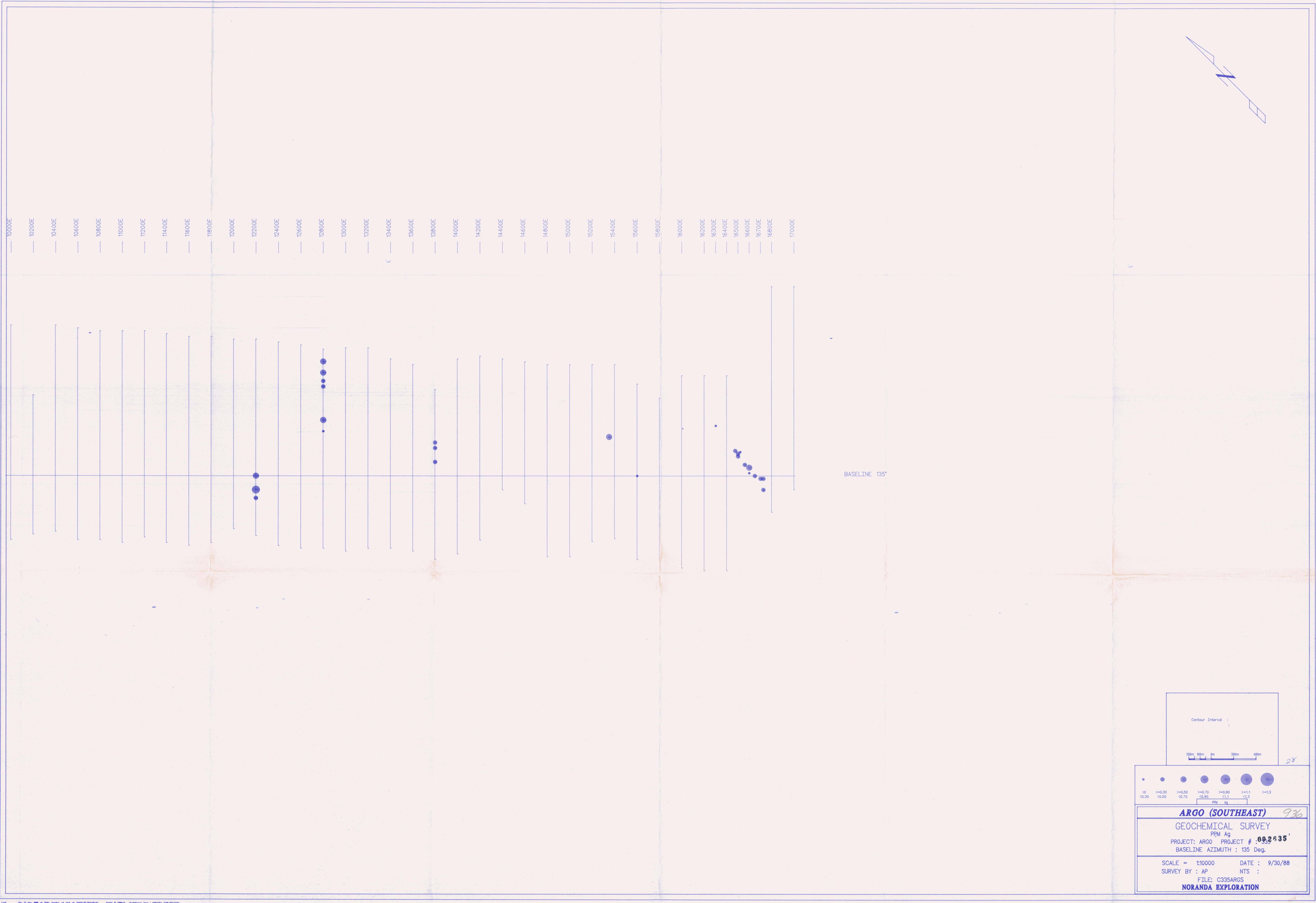
BASELINE AZIMUTH : 135 Deg

SCALE = 1:10000 DATE : 9/30/88

SURVEY BY : AP NTS :

FILE: C335ARGS

NORANDA EXPLORATION



Contour Interval :

200m100m50m200m400m

<0.30

>=0.30

<0.50

>=0.50

<0.70

>=0.70

<0.90

>=0.90

<1.1

>=1.1

<1.3

>=1.3

PPM Ag

ARGO (SOUTHEAST)

GEOCHEMICAL SURVEY

PPM Ag

PROJECT: ARGO PROJECT # : 092635

BASELINE AZIMUTH : 135 Deg.

SCALE = 1:10000

DATE : 9/30/88

SURVEY BY : AP

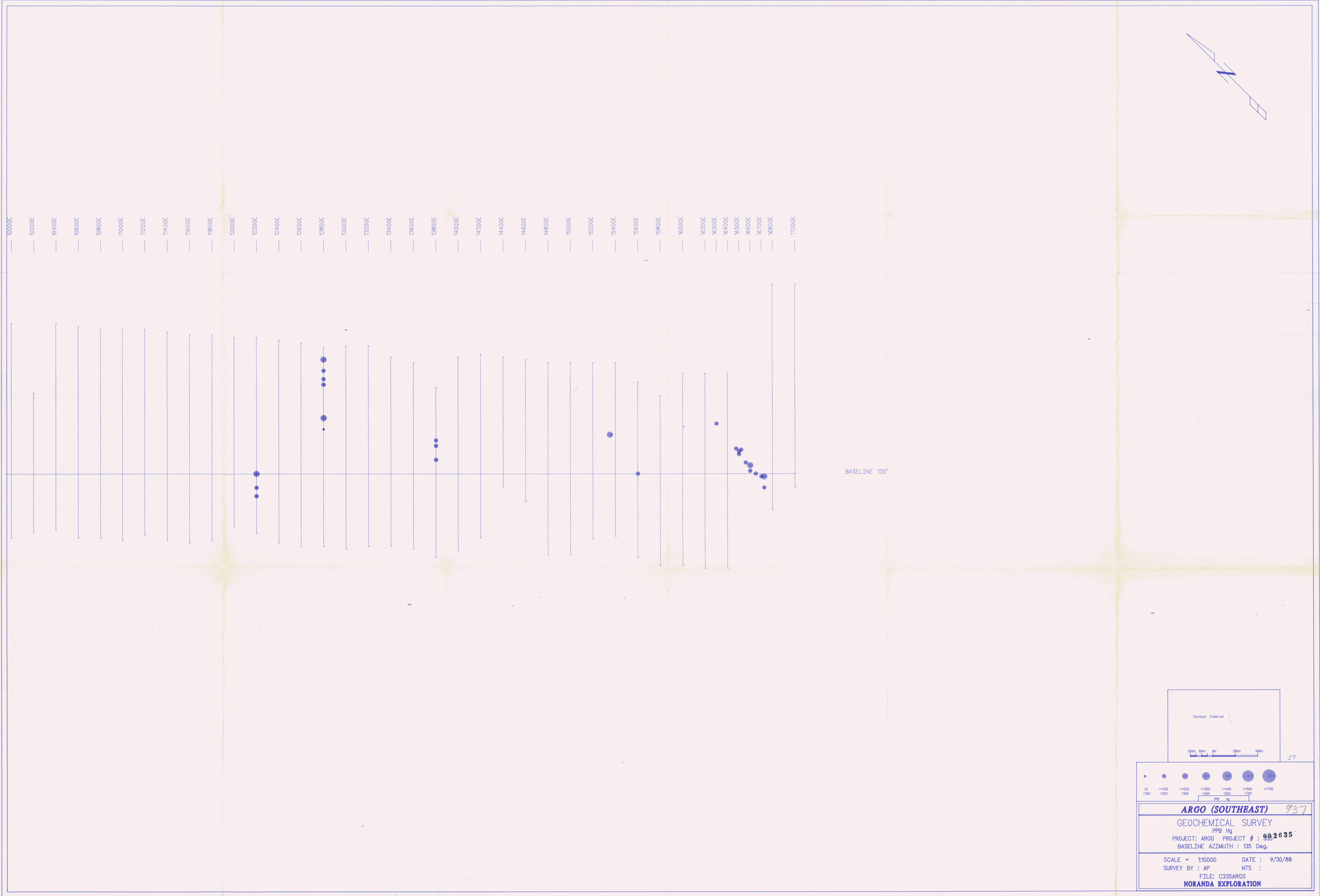
NTS :

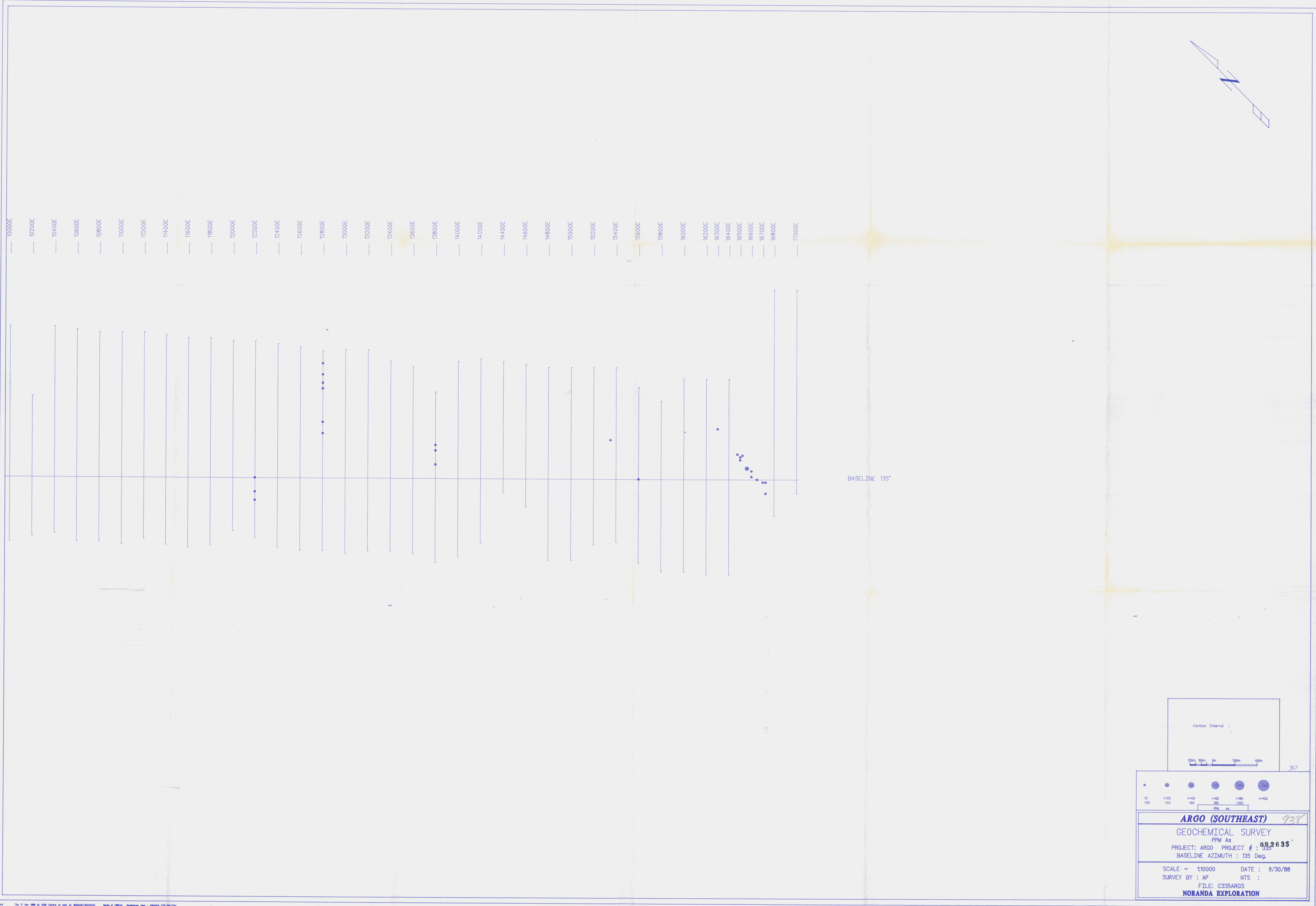
FILE: C335ARGS

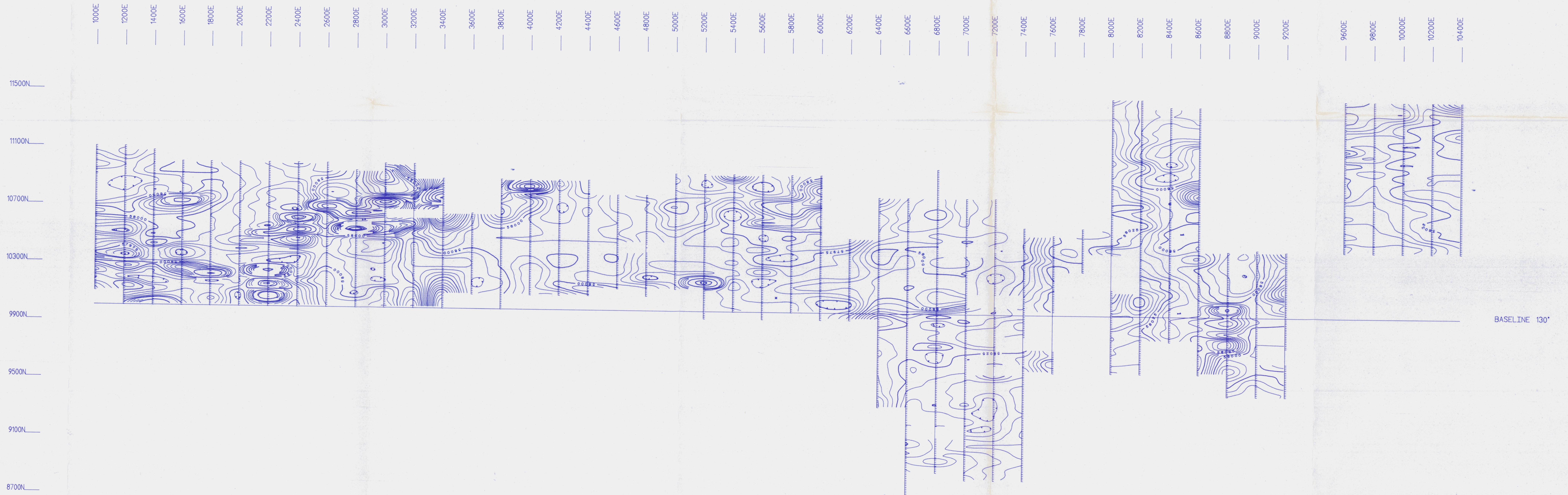
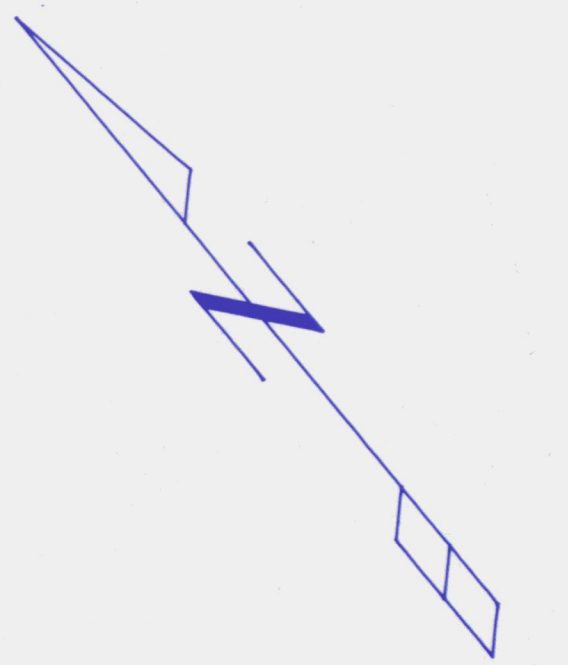
NORANDA EXPLORATION

936

Ver. 5.00 The IT Rev 988 of 024 Centre of plot of 80000E/20400N Serial # 08600 Registered User : NORANDA EXPLORATION



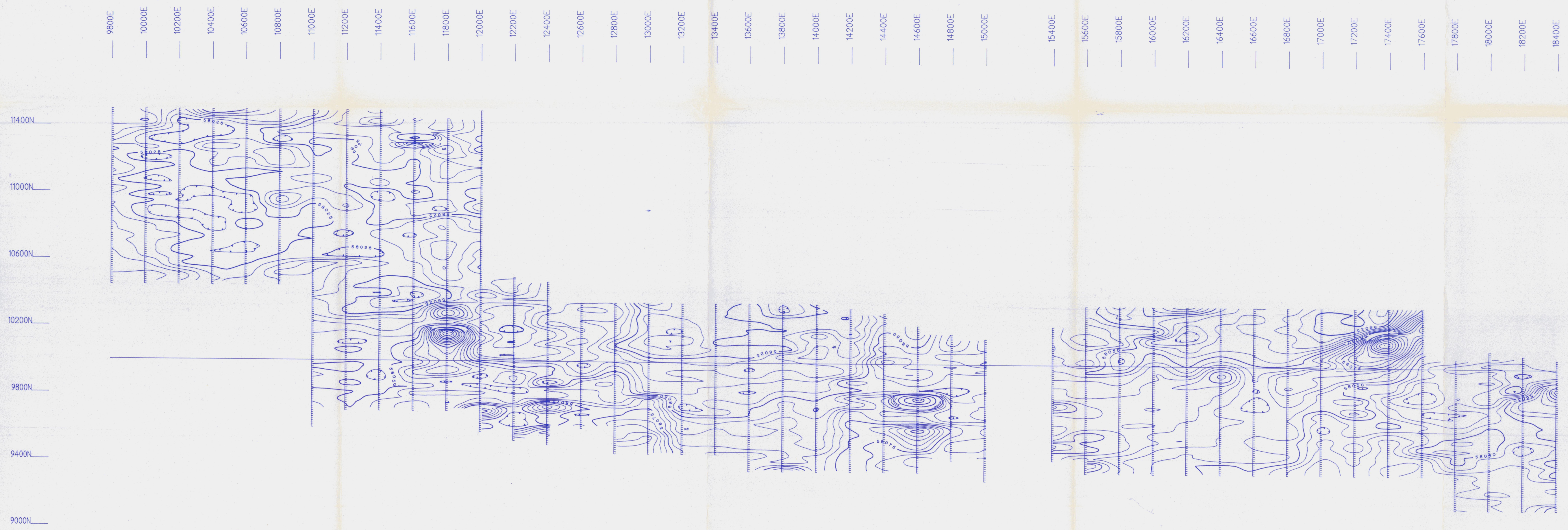
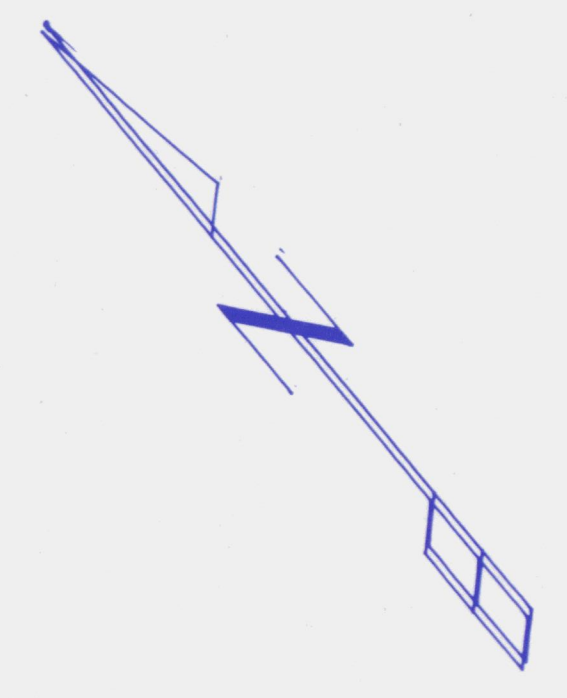




Instrument	: EDI MAG
Field	: TOTAL
Datum	: 0.0 nT
Contour Interval	: 5.0 nT
Conductor Axis	:
Scale	: 1:10000

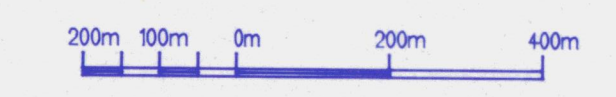
ARGO NORTH(WEST)	
MAGNETOMETER SURVEY	
PROJECT: ARGO	PROJECT # : 335
BASELINE AZIMUTH : 130 Deg.	
SCALE = 1 :10000	DATE : 9/10/88
SURVEY BY : S.K./J.D.W. NTS	
FILE: Margwst	
NORANDA EXPLORATION	

31



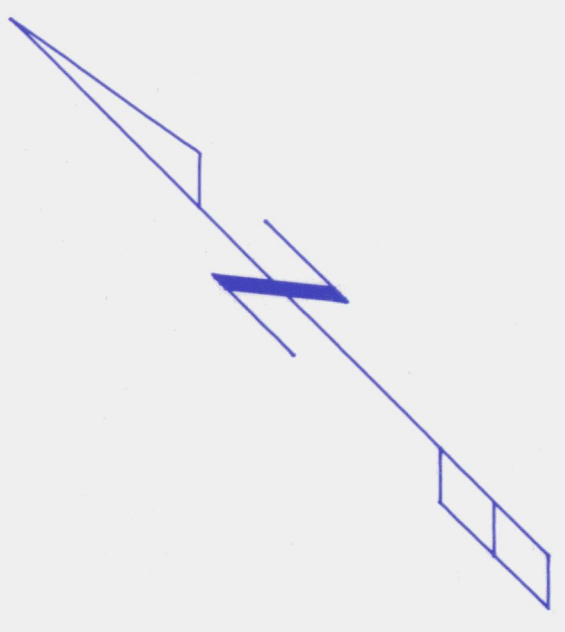
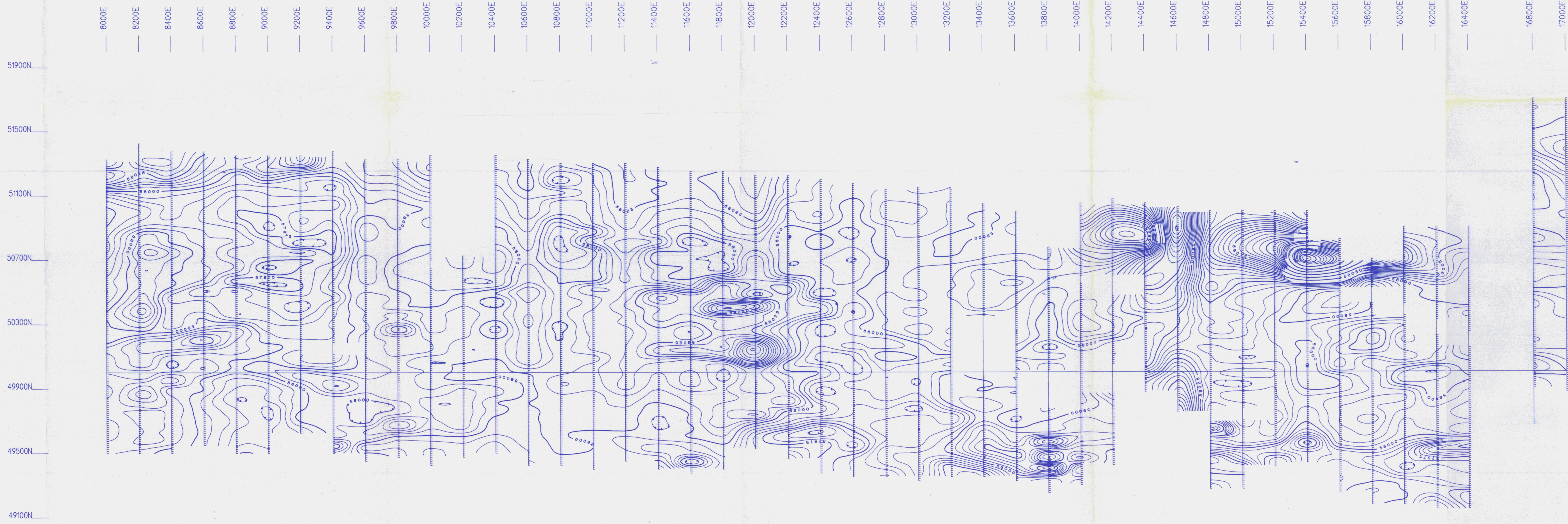
BASELINE 130°

Instrument	: EDX MAG
Field	: TOTAL
Datum	: 0.0 nT
Contour Interval	: 5.0 nT
Conductor Axis	:



ARGO NORTH(EAST)	
MAGNETOMETER SURVEY	
PROJECT: ARGO 092635	PROJECT # : 335
BASELINE AZIMUTH : 130 Deg.	
SCALE = 1 :10000	DATE : 9/10/88
SURVEY BY : S.K./J.D.W. NTS	
FILE: MARGEST	
NORANDA EXPLORATION	

32



Instrument : EDX MAG
Field : TOTAL
Datum : 0.0 nT
Contour Interval : 5.0 nT
Conductor Axis :
200m 100m 0m 100m 200m 400m

ARGO SOUTH GRID 092635 941

MAGNETOMETER SURVEY

PROJECT: ARGO PROJECT # : 335
BASELINE AZIMUTH : 135 Deg.

SCALE = 1 :10000 DATE : 9/23/88
SURVEY BY : S.K.\J.D.W.NTS :
FILE: M335COR
NORANDA EXPLORATION