Project No. 1107
Sunexco Energy Corporation Ltd.
NTS 105K/3

REPORT ON A GRAVITY SURVEY CONDUCTED OVER PUG AND KEY CLAIMS YUKON TERRITORY SUMMER, 1980

for

SUNEXCO ENERGY CORPORATION LTD.

by

CAN-LAKE EXPLORATIONS LTD.

September, 1980
Calgary, Alberta

D.C. Bingham
Geophysicist

CAN-LAKE

This report has been examined by the Geological Evaluation Unit and is recommended to the Commissioner to be considered as representation work to the value of $ 86,262.00

Resident Geologist or
Resident Mining Engineer

Considered as representation work under Section 53 (4), Yukon Quartz Mining Act.

B. R. BAXTER
Supervising Mining Recorder

for Commissioner of Yukon Territory

RESPECTFULLY SUBMITTED

CAN-LAKE EXPLORATIONS LTD.

David Clayton Bingham
Geophysicist

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1. SUMMARY

Approximately 1,350 gravity stations were occupied on the Pug and Key Claim Blocks. The purpose of the survey was to locate lead-zinc deposits similar to those in the area (e.g. Vangorda, Faro, Swim Lakes). The survey was undertaken on an old grid where the lines were recut and a number of new lines were cut.

The geology of the area is complex and a number of anomalies were found. However, the amplitudes of the anomalies are generally small (in the order of 0.6 milligals) and a couple of the anomalies are masked by the presence of faults (A-2 and A-3). Drill targets were established on anomalies considered to be caused by ore deposits.

The final residual gravity bears little resemblance to the previous survey, indicating the importance of terrain corrections and proper densities.

2. INTRODUCTION

2.1 Location

Country: Canada
Province: Yukon Territory
NTS: 105K/3

2.2 Disposition

Holder: Sunexco Energy Corporation Ltd. (under option).
Claims: Key - 1 - 16, Tag #YA24412 to 24427
Pug - 1 - 24, Tag #YA8744 to 8767
Pug - 25 - 52, Tag #YA50971 to 50998.

2.3 General

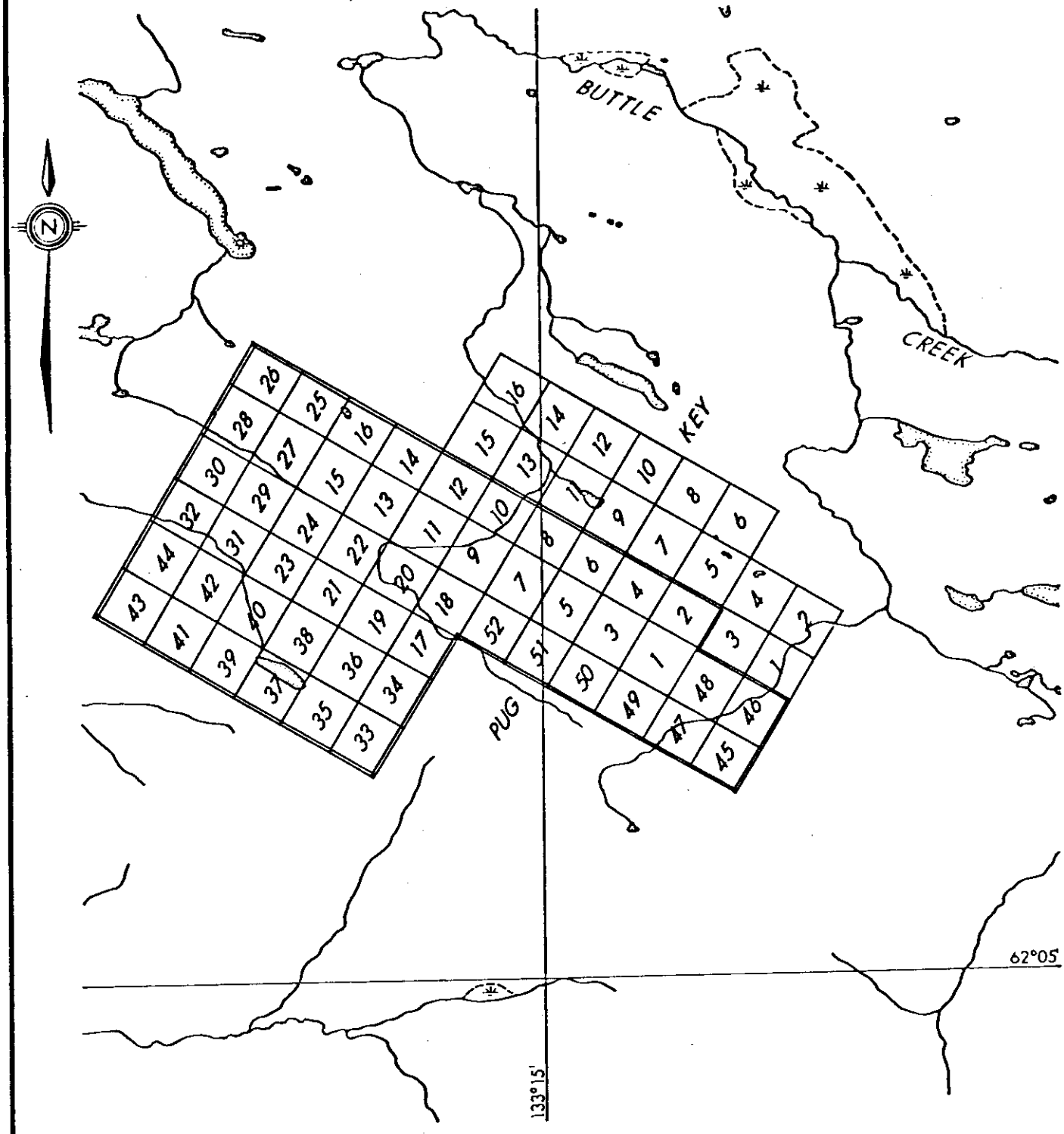
Between the 10th of July, 1980 and the 20th of August, a gravity survey was carried out by Can-Lake Explorations Ltd. for Sunexco Energy Corporation Ltd. The personnel involved in the survey are as follows:

Dave Bingham, Geophysicist	July 10 - August 20, 1980.
Trevor Dundas, Geophysicist	June 27 - June 29, 1980. July 13 - August 20, 1980.
Denny Blanchard, Surveyor	July 10 - August 18, 1980.
Ron Nishimura, Rodman	July 10 - August 18, 1980
Dave Burgess, Cook	July 10 - August 20, 1980

The interpretation, drafting and report compilation was done between the dates August 23, 1980 to September 19, 1980. The personnel involved were:

Interpretation and Report	Dave Bingham
Drafting	Heather Meyers, Merina Barclay

LOCATION MAP
FIGURE #1a



SCALE 1:50,000

1000 0 1000 2000 Metres

SUNEXCO ENERGY CORPORATION

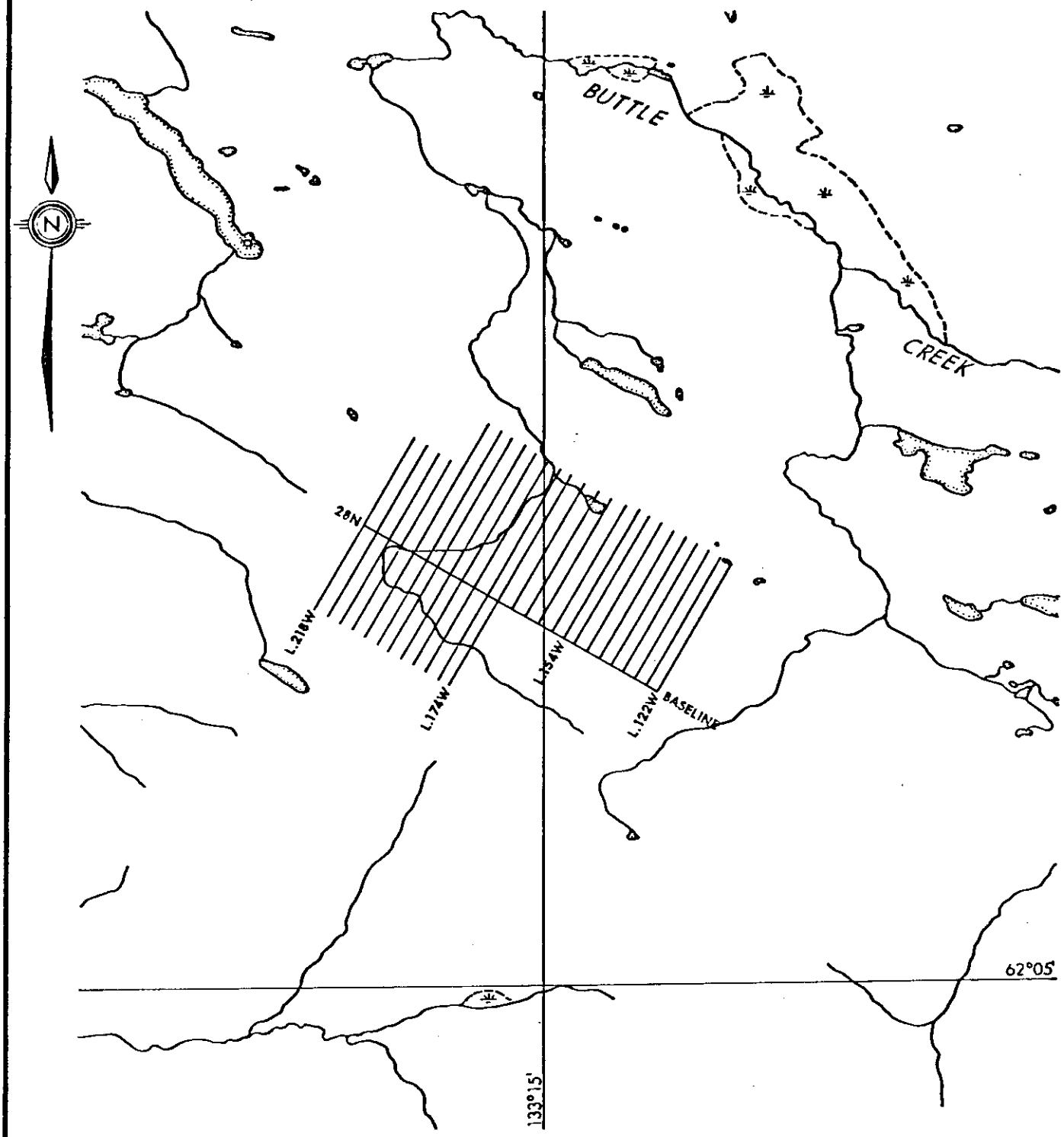
PUG & KEY CLAIMS, YUKON TERRITORY

CLAIM LOCATION MAP

TO ACCOMPANY REPORT BY DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. Calgary Alberta

SCALE: 1:50,000	DATE: SEPT. 1980
PROJECT NO.: 1107	FIGURE NO.: 1b
N.T.S.: 105 K/3	DRAWN BY H. Meyers



SCALE 1:50,000

1000 0 1000 2000 Metres

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY

GRID LOCATION MAP

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. Calgary Alberta	SCALE: 1:50,000	DATE: SEPT. 1980
	PROJECT NO.: 1107	FIGURE NO.: 2
	N.T.S.: 105 K/3	DRAWN BY: H. Meyers

2.4 Objective

The gravity survey was undertaken to redefine anomalies present on a previous gravity survey. No terrain corrections were done on the previous survey and there is some doubt as to the accuracy of the original survey.

The expected targets for the survey to find were massive lead-zinc type deposits such as those in Faro, Vangorda Creek and Swim Lakes.

3. SURVEY SPECIFICATIONS

3.1 Instrumentation

Gravity data was obtained with the use of a LaCoste & Romberg variable damped gravity meter. Two meters were used at separate times during the survey (Serial #'s 333 and 574).

Survey data was obtained with the use of a Sokkisha transit and a K & E Auto Ranger (microwave distance measuring device).

3.2 Parameters

The line interval on the grid is 400 feet between lines with stations at approximately 100 foot intervals. Both station position and elevation were accurately obtained from the survey data. The elevations were surveyed to within 0.1 foot accuracy. The expected accuracy of the gravity data (after all corrections have been applied) is ±0.05 mgals.

4. RESULTS

4.1 Calculations

Both the gravity and elevation calculations were aided by the use of a Hewlett Packard - 85 computer in the field.

(a) Observed Gravity

Meter readings were converted to gravity readings using the constants supplied with the gravity meter. The gravity values were then corrected for instrument drift, tidal variations and the height of the instrument from the ground (free air effect).

Observed Gravity =
Gravity Reading + Instrument Drift + Tide Correction[1] + H.I. Correction
(.09406 mgals/ft)

(b) Bouguer Gravity

Corrections are made for elevation (free air effect = .09406 mgals/ft), the mass below the station (Bouguer effect = .01276 mgals/ft x Density) and latitude (~1.307 x sin (2 x latitude) mgals/mile) to obtain Bouguer gravity.[2]

Bouguer Gravity =
Observed Gravity + Free Air Effect + Bouguer Effect + Latitude Correction

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1 Tide corrections were obtained from Kenting Exploration for:
latitude - 62.1°
longitude - 133.25°

2 Density is discussed in section 4.1 (d).

(c) Final Gravity

A base level of 5660 milligals was taken off the Bouguer gravity to make the numbers more manageable. This is permissible since only the relative difference between gravity stations is important in dealing with local anomalies.

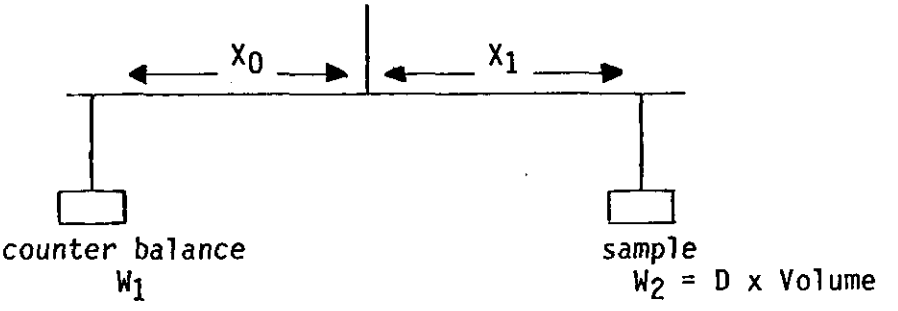
Due to the rough terrain, terrain corrections[3] are necessary.

Gravity =
Bouguer Gravity - 5660 mgals + Terrain Correction

(d) Density

It is necessary to use a correct density in the Bouguer reduction to insure that the topography is not reflected in the gravity data.

Density measurements were made on some core samples which were available. The measurements were done using a suspended lever and immersing the sample in water.



3 Terrain corrections discussed in section 4.1(e).

TABLE 4.1 (d)

Hole 77-1

Depth (ft)	Density (g/cc)
?	2.71
?	2.89
27	2.84
44	2.74
67	2.70
87	2.73
96	2.74
114	2.74
183	2.81
211	2.70
200 + ?	2.67

Random Samples (71-72) (from assorted core)

Description	Density
Phyllite	2.89
Quartz	2.62
Phyllite	2.77
Greenstone?	2.93
Phyllite and Quartz	2.73
Phyllite (brown banded)	2.91
--	2.95
--	2.76
--	2.71
--	2.78
--	2.86
--	2.75
--	3.00
--	2.75
--	2.82
--	2.83
--	2.84
--	2.74
--	2.69
--	2.76
--	2.91
--	2.83
--	2.88
--	2.73
--	2.83
--	2.66

When the sample is immersed in water, buoyant forces effectively decrease the sample's density by the density of water.

balanced dry $W_1X_0 = X_1.D.Vol$

balanced immersed $W_1X_0 = X_2.(D-1).Vol$

Using elementary algebra it easily follows that:

$$D = \frac{X_2}{X_2 - X_1}$$

The results of the density measurements are listed in Table 4.1 (d). The mean density for hole 71 is 2.75 ± .07 and the mean density for the random samples is 2.80 ± .09.

The density used for the Bouguer gravity reduction is 2.75 g/cc.

However there appears to be a change in density on the west side of the grid. Since no core was available for measurement an alternate approach to determine density was used.

The approach to determine the density was to use the gravity and elevation data to find a suitable density. The analytical approach (Parasnis' method[4]) uses the formula:

$$D = \frac{(g - .09406 \times h)}{(.01276 \times h - T)}$$

Where:

D = density

g = difference in observed gravity

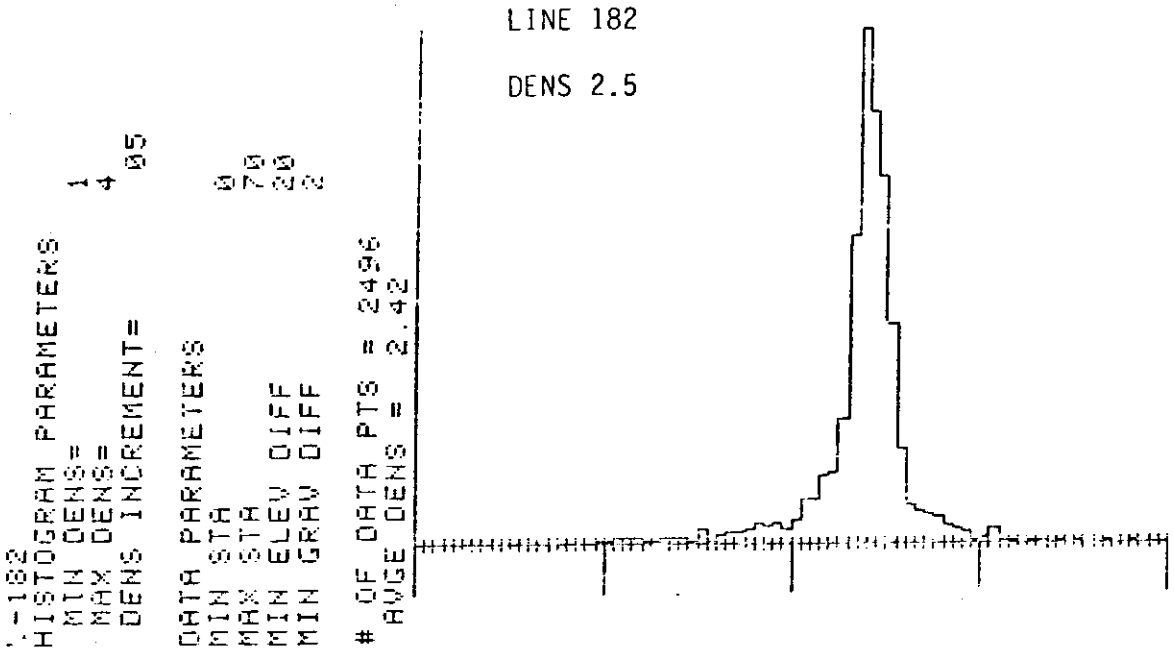
h = difference in elevation

T = difference in Terrain factor

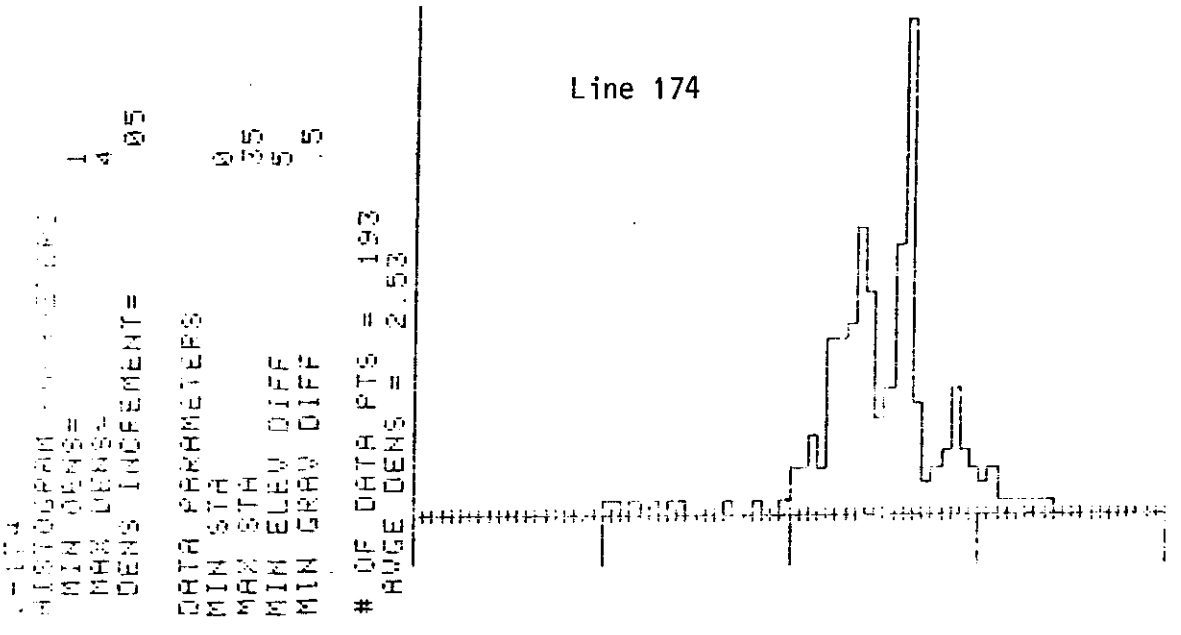
4 APPLIED GEOPHYSICS p. 30.

LINE 182

DENS 2.5

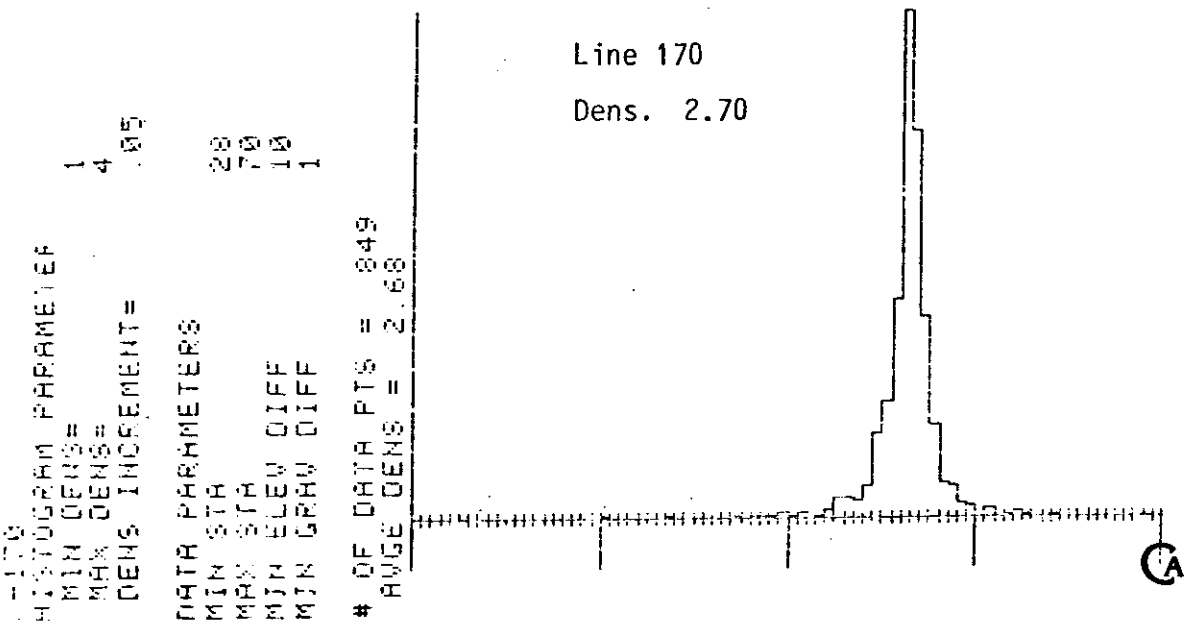


Line 174



Line 170

Dens. 2.70



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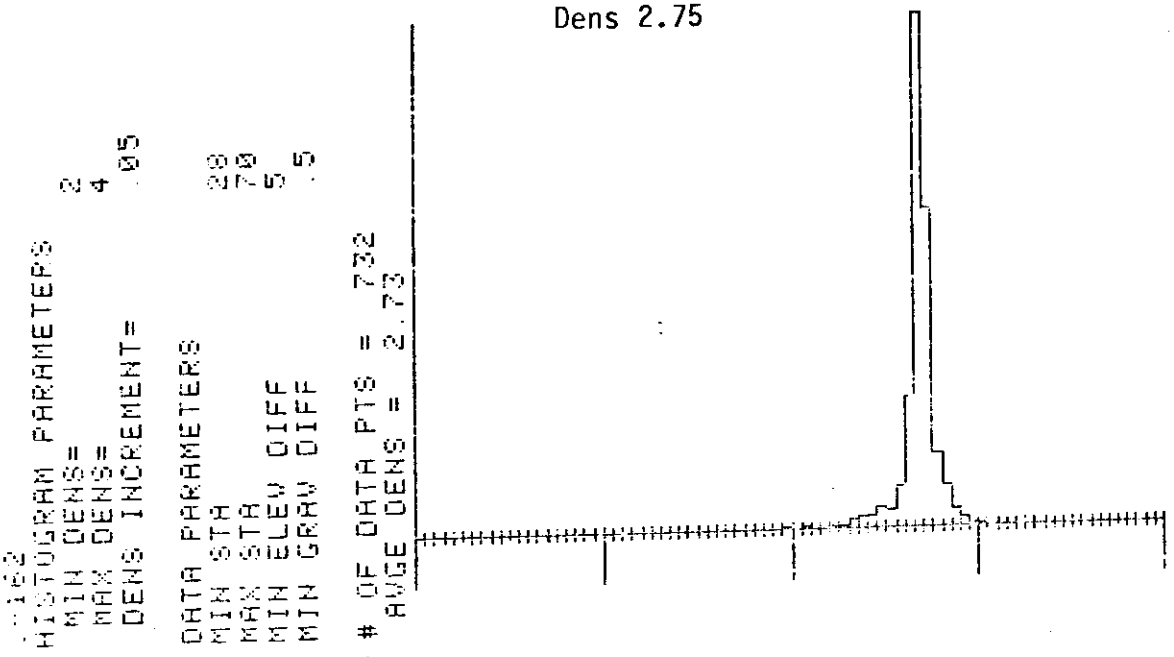
Line 162

Dens 2.75



Line 166

Dens 2.75

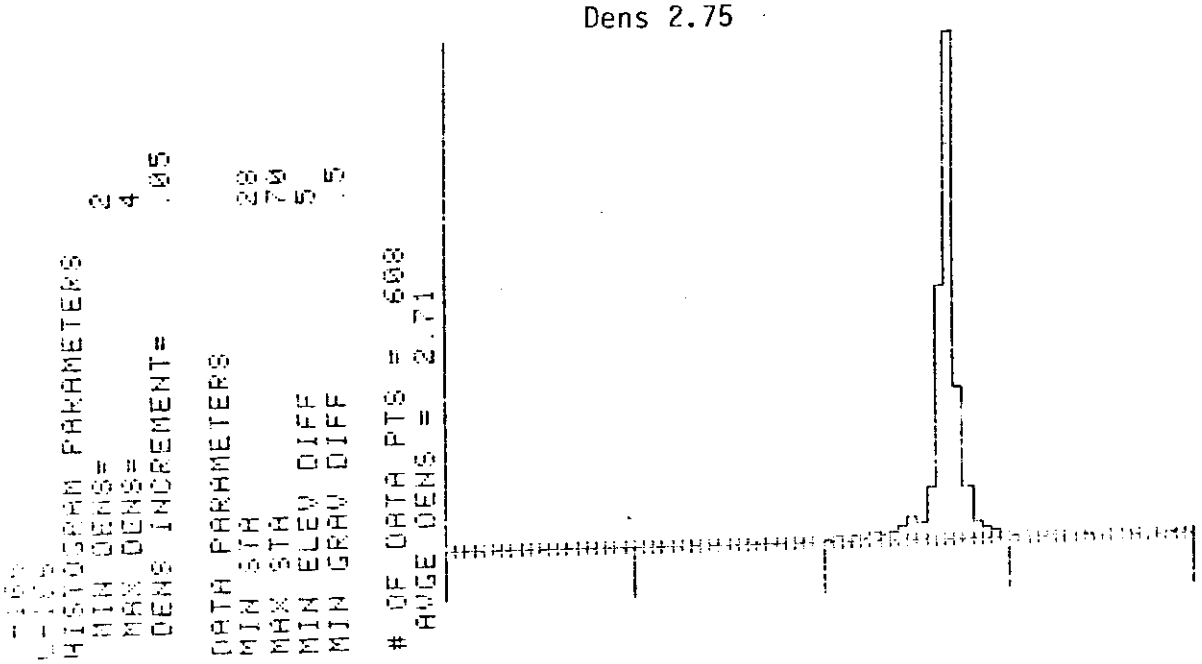


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Figure 4.1(d) - 2

To apply this formula rigorously, the regional gravity effect must be removed, as well as removing anomalies and noise. To facilitate quick calculations only a straight line regional was removed. Some results of this method are shown in Figure 4.1 (d)-1 and Figure 4.1 (d)-2. The densities have been calculated and displayed in a histogram format. On lines 170, 182, 166, and 162 the formula has been applied to all combinations of data points on the line, whereas on line 174 the formula has been limited to data points within 600 feet of each other in order to show the double density peaks indicating a density change. On lines 162 and 166 the analytical density measurement agrees very well with the densities measured in the drill hole samples (i.e. mean density is about 2.75 g/cc).

As such a density of 2.50 g/cc was used for Bouguer reductions to the west of line 170. Due to problems involved in matching Bouguer maps of different densities, separate Bouguer maps have been produced and the residual gravity maps have been matched.

(e) Terrain Corrections

Terrain corrections in the area are quite significant and exceed 2 milligals in places due to the large amount of vertical displacement and steep slopes. Due to the large amount of time involved and possible inaccuracies in using Hammer charts to do corrections, each profile has been assumed to be two-dimensional and the corrections were done with the computer using Talwani's method.[5] While this assumption is very close over most of the grid area, it breaks down and is inaccurate in the vicinity of steep sidehills (especially along the main creek). To overcome this drawback, extra corrections have been done at right angles to the lines in areas where it has been deemed necessary. These extra corrections have been added into the smoothed residual map.

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[5] GRANT & WEST - Interpretation Theory in Applied Geophysics. pp.288-289

Also, the station intervals have been assumed to be constant. This generates small errors in places where the vertical relief is great, and stations are not 100 feet apart (e.g. lines 122, 126 at stations 46 and 47).

4.2 Presentation

In addition to an elevation map (contoured in 50 foot intervals), two Bouguer gravity maps are presented (contoured at 0.2 mgal intervals) at densities of 2.50 g/cc and 2.75 g/cc. Also a residual gravity map and a smoothed residual gravity map (contoured at 0.2 mgal and 0.1 mgal intervals respectively) are included. The interpretation map is based on the smoothed residual gravity map (includes terrain corrections for sidehills).

5. INTERPRETATION

5.1 Geology

The geological information available in the grid area is from the KERR-ADDISON MINES composite geology plan (1971). The geological setting of the grid area is on the south side of the Tintina Fault, across from the Anvil, Grum and Swim Lakes ore deposits. The rocks are divided into four main groups as follows:

A - Gneiss
B - mainly Quartz Biotite Schist along contact with A and C
C - Limestone and Limy rocks
D - mainly shales, phyllites, also limestone schists, graphitic shales and limy rocks.

Mineralized showings occur in the limestone unit (c).

As well as some geology, geochemical maps are available for lead and zinc content.

Since both the geology and geochemistry were done on traverses, the actual location is somewhat uncertain with respect to the gravity survey.

5.2 Gravity

5.2 (a) Regional-Residual Separation.

Due to the density change (discussed previously) regional trends were separated from two different Bouguer maps. The regional trend removed in both cases was a planar trend (see Table 5.2-1). While this trend may not be a true regional, any regional effects present in the residual map are easily identified.

TABLE 5.2 (a)-1

REGIONAL GRAVITY (By Line)

A Density = 2.75 g/cc

Line	RegionalBase Level (at Base Line 28N)	Regional Gradient (per 100 ft)
122	6.12	.03467
126	6.23	.034
130	6.34	.03633
134	6.45	.03367
138	6.55	.0345
142	6.65	.035
146	6.76	.034
150	6.87	.0325
154	7.00	.032
158	7.10	.03325
162	7.22	.0345
166	7.33	.03325
170	7.45	.035

B Density = 2.50 g/cc

Line	Regional Base Level (at Station ON)	Regional Gradient (per 100 ft)
174	17.22	.0796
178	17.28	.078
182	17.48	.0802
186	17.58	.0804
190	17.70	.0802
194	17.80	.079
198	17.92	.07886
202	18.00	.0794
206	18.10	.0786
210	18.20	.079
214	18.35	.08
218	18.45	.08

* Note - Gradients unequal due to divergence of lines.

Figure 5.2-2 shows two-dimensional terrain corrections calculated at right angles to the line. Lines A[1], A, B, C, D, and E were used to calculate supplemental corrections for the sidehill and main creek vicinity, while lines F, G, and H were used to calculate corrections in the vicinity of a steep washout on a minor creek.

5.2 (b) Interpretation

The interpretation is shown on the interpretation map as faults, structural highs, anomalies, and gravity lows.

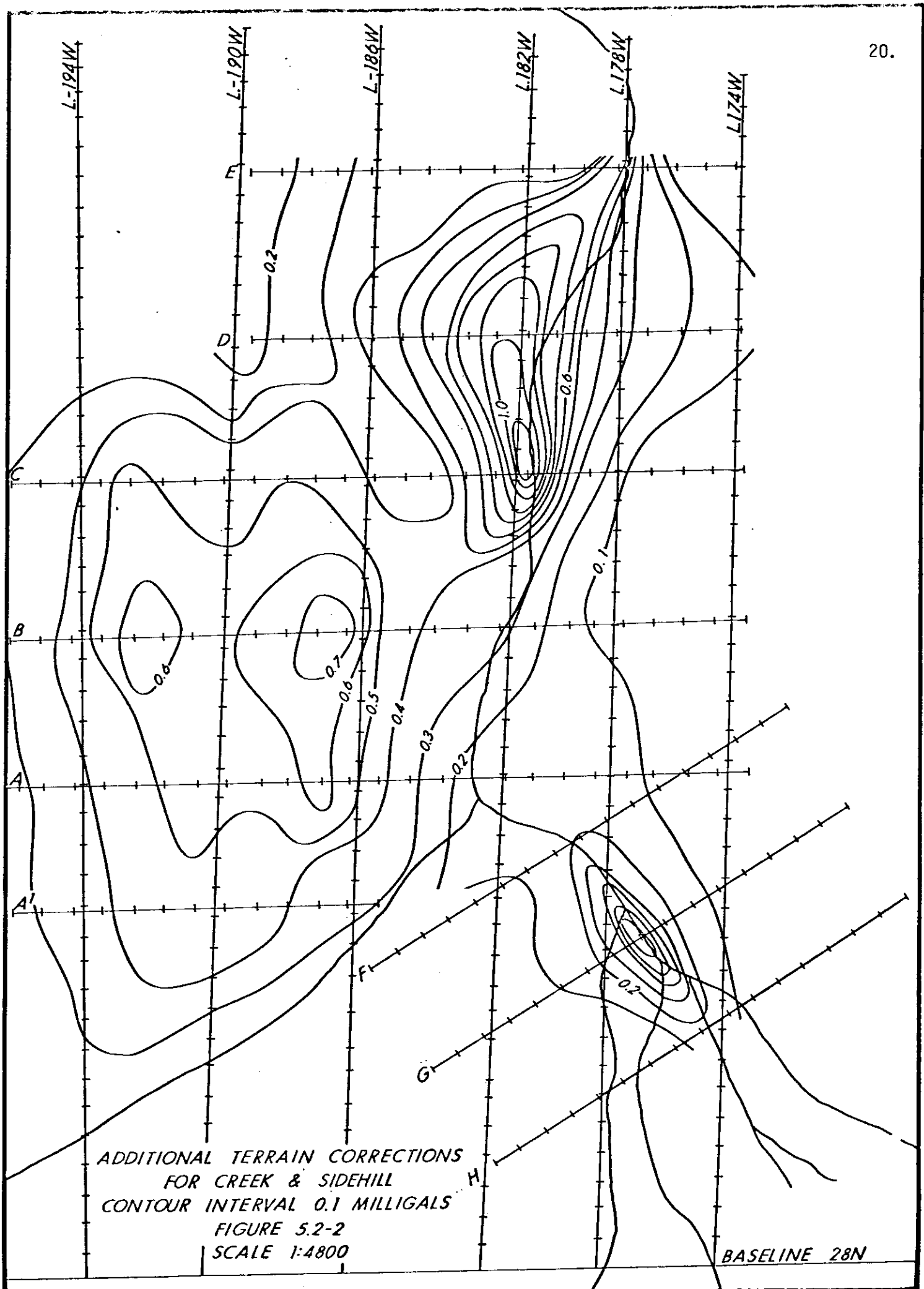
The faults are classed in probable and possible categories. The probable faults are based on major gradients in the gravity data. On some of the probable faults (especially F1 and F2), the actual location is obscure due to the fault being parallel to the survey lines. The possible faults are based on small gradients and trends in the gravity data and may be helpful in determining contacts.

The structural highs are anomalies which are considered to arise from structure or rock type charge, rather than from an orebody. Certain characteristics and locations tend to this conclusion about some of these highs.

S-1 to S-6. These highs are closely related to probable faults and seem to be related from evidence gathered in the OVERLAND GRAVITY SURVEY.[6]

S-2. This high coincides with a geological contact on lines 122 - 134. The gneiss unit gives rise to the gravity high. This high can be used to extend the contact from line 134 to line 170 at the north end of the grid.

6. GALESKI REPORT for KERR-ADDISON 1971 - certain areas of the data can be related (no terrain corrections were done).



ADDITIONAL TERRAIN CORRECTIONS
FOR CREEK & SIDEHILL
CONTOUR INTERVAL 0.1 MILLIGALS
FIGURE 5.2-2
SCALE 1:4800

S-3, S-4, and S-5. The character of these highs are similar and they are probably related, although separated by faults. Due to the broad nature of these highs it is difficult to model a source for them. The source may be a small density change in rock type near surface or a larger change in depth.

The remaining anomalies are considered to be the prime targets for drilling and/or further detail work. The anomalies are numbered in order of importance.

A-1. This anomaly has a good coincidence with previous lead geochemical results, and is considered as the prime target. The anomaly is not easily modelled due to effects from side structures. However parameters for a ribbon model[7] yield a depth of about 40 feet on Line 122. Figure 5.2-1 shows some attempts at two-dimensional modelling of the anomaly on Line 122. Very rough calculations gives rise to about one million tons of ore (about 7%Pb, 7%Zn). This assumes the orebody is 250' x 300' x 1000' with a density contrast of 0.4 g/cc.

A-2 and A-3. These anomalies are quite subtle due to their proximity to a probable fault. Rough depth calculations on A-2 (see footnote 7) suggest a depth of about 80 feet. Anomaly A-3 is very obscure, but is rated in importance due to its coincidence with a lead geochemical anomaly.

A-4. This anomaly is quite distinct, but is located in the gneiss unit. Less emphasis is placed on this feature due to it being in the gneiss unit and its close proximity to cliffs, but it cannot be totally ignored.

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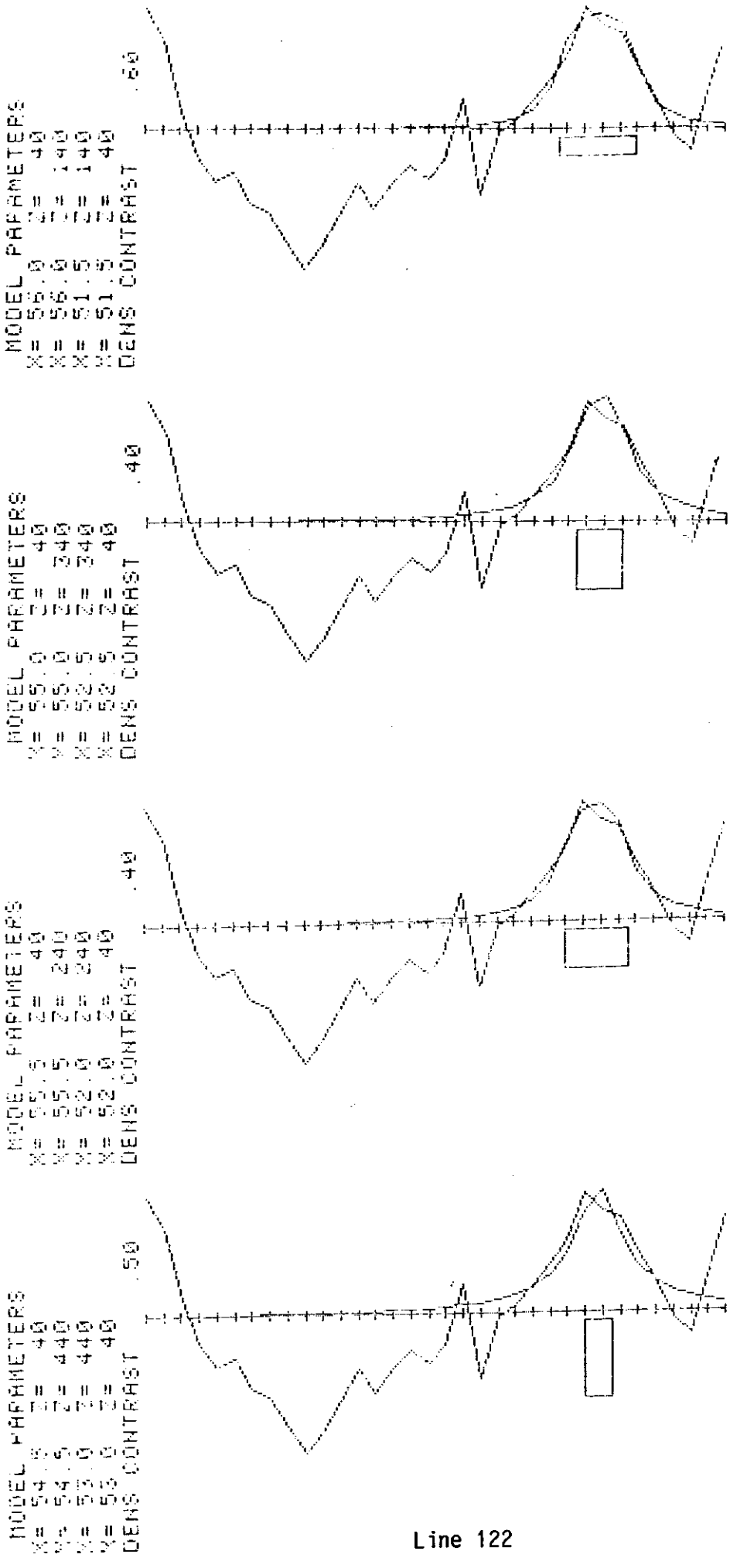
[7] GRANT & WEST - Interpretation Theory in Applied Geophysics. pp. 273-280.



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Line 122

FIG. 5.2.1

A-5. This anomaly is quite small (0.3 mgals), but it is given credence because it is located about 400 feet east of some minor lead geochemistry. It may also be partially masked by a gravity low (possible creek overburden).

Many of the gravity lows on the interpretation map may be due to overburden, but they may be useful in outlining geologic contacts.

5.3 Recommendations

On the basis of the interpretation, drill targets can be established. The drill targets (in order of importance) are:

L 122	Station 53 N	(A-1)
L 178	Station 35 N	(A-2)
L 182	Station 22 N	(A-3)
L 134	Station 63 N	(A-4)
L 174	Station 26 N	(A-5)

Also, detailed geochemistry is suggested in the vicinities of A-1 and A-3 to re-affirm the geochemical response present.

There is the possibility that the gravity features classed as structural highs may also be stratiform ore deposits. There is no way to distinguish the difference with gravity. Some type of electromagnetic method may be of use, particularly the C.E.M. shoot-back (due to its relative ease of operation and independence of topography).

CERTIFICATE

I, David Clayton Bingham, hereby certify that:

1. I am a geophysicist employed by Can-Lake Explorations Ltd. of #1, 4001 - 19th Street N.E., in the city of Calgary, in the Province of Alberta.

2. I currently reside at 724 - 86th Avenue S.W. in the city of Calgary, Province of Alberta and the postal code of the said address is T2V 0V9.

3. I obtained a Bachelor of Science degree in geophysics in 1978 from the University of British Columbia, Vancouver, B.C.

4. I have been practising my profession since 1978.

5. I hold no direct or indirect interest in nor expect to receive any other benefits from the mineral properties.

Date 22 Sept 80
Calgary, Alberta

Dave Bingham
David Clayton Bingham, B.Sc.
Can-Lake Explorations Ltd.

APPENDIX I

Data Listing
By Line and Density

Station
Elevation
Observed Gravity
Terrain Correction
Latitude Correction
Final Gravity

LINE L-122

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2968	5491.66	.09	.05	6.73
29	2982	5490.69	.08	.06	6.54
30	2991	5489.80	.08	.08	6.18
31	2997	5489.18	.09	.10	5.88
32	2997	5488.94	.14	.12	5.72
33	2980	5489.98	.15	.13	5.72
34	2971	5490.36	.17	.15	5.55
35	2964	5490.60	.21	.16	5.47
36	2960	5490.59	.31	.18	5.28
37	2953	5490.70	.49	.20	5.11
38	2928	5492.00	.71	.22	5.17
39	2879	5495.04	.74	.23	5.31
40	2868	5495.79	.75	.24	5.43
41	2842	5497.02	.93	.26	5.27
42	2802	5499.38	1.04	.28	5.36
43	2769	5501.37	1.08	.30	5.42
44	2751	5502.15	1.24	.32	5.31
45	2718	5503.86	1.54	.33	5.37
46	2662	5507.32	1.68	.34	5.65
47	2613	5509.81	1.60	.36	5.12
48	2593	5511.15	1.71	.37	5.41
49	2536	5514.36	1.89	.39	5.43
50	2482	5517.65	1.91	.40	5.49
51	2424	5521.30	1.79	.42	5.59
52	2376	5524.44	1.52	.43	5.65
53	2348	5526.66	1.22	.44	5.87
53	2348	5526.65	1.22	.44	5.87
54	2328	5527.88	1.04	.46	5.74
55	2310	5528.94	1.01	.48	5.57
56	2287	5529.92	1.15	.49	5.46
57	2235	5532.77	1.24	.51	5.26
58	2182	5535.81	1.11	.52	5.05
59	2147	5538.00	.88	.54	4.93
60	2151	5538.22	.67	.55	5.18
61	2176	5536.54	1.18	.57	5.46

LINE L-126

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2979	5490.88	.09	.08	6.56
29	2967	5491.58	.09	.10	6.55
30	2972	5491.21	.11	.12	6.43
31	2960	5491.95	.12	.14	6.47
32	2949	5492.39	.12	.15	6.23
33	2942	5492.64	.12	.17	6.06
34	2936	5492.69	.14	.18	5.81
35	2930	5492.92	.18	.20	5.66
36	2921	5493.25	.24	.22	5.53
37	2909	5493.75	.35	.24	5.40
38	2883	5495.30	.39	.26	5.43
39	2870	5496.03	.45	.27	5.46
40	2855	5496.61	.60	.29	5.28
41	2824	5498.45	.72	.30	5.41
42	2806	5499.38	.86	.32	5.37
43	2779	5500.72	1.09	.34	5.35
44	2744	5502.49	1.35	.36	5.29
45	2692	5505.73	1.44	.37	5.54
46	2668	5507.25	1.51	.39	5.72
47	2636	5508.51	1.83	.40	5.37
48	2577	5511.98	2.08	.42	5.60
49	2510	5516.16	2.09	.43	5.83
50	2456	5519.25	1.93	.44	5.59
51	2407	5522.48	1.74	.46	5.71
52	2368	5525.03	1.52	.47	5.69
53	2333	5527.32	1.31	.49	5.72
54	2303	5529.34	1.11	.51	5.73
54	2303	5529.34	1.11	.51	5.74
55	2281	5530.19	.98	.52	5.74
56	2273	5531.03	1.06	.54	5.56
57	2233	5533.32	1.18	.56	5.58
58	2178	5536.33	1.15	.57	5.35
59	2134	5539.15	.95	.59	5.35
60	2113	5540.61	.71	.60	5.30
61	2092	5541.81	.56	.62	5.10
62	2082	5542.37	.43	.64	4.95
63	2083	5542.82	.39	.65	5.37
64	2069	5543.48	.47	.67	5.31
65	2035	5545.37	.54	.68	5.21
66	1986	5548.22	.53	.70	5.15
67	1982	5548.97	.25	.72	5.40
68	1975	5549.36	.18	.73	5.30
69	1973	5549.67	.12	.75	5.38
	1970	5550.06	.09	.76	5.5[illegible]

LINE L-130

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	3015	5488.36	.50	.12	6.54
29	2982	5490.30	.54	.14	6.55
30	2945	5492.72	.49	.15	6.74
31	2935	5493.39	.34	.17	6.61
32	2929	5493.68	.28	.18	6.50
33	2919	5494.15	.28	.20	6.37
34	2903	5494.96	.29	.22	6.24
35	2885	5495.84	.29	.24	6.03
36	2870	5496.76	.27	.25	6.04
37	2861	5497.11	.28	.27	5.83
38	2849	5497.76	.32	.29	5.77
39	2837	5498.25	.41	.30	5.68
40	2816	5499.35	.51	.32	5.58
41	2795	5500.50	.61	.34	5.61
42	2781	5501.05	.82	.36	5.52
43	2748	5502.87	1.04	.37	5.59
44	2709	5505.14	1.17	.39	5.67
45	2676	5507.07	1.27	.40	5.71
46	2650	5508.35	1.48	.42	5.65
47	2606	5510.68	1.71	.43	5.64
48	2560	5513.25	1.94	.44	5.70
49	2494	5517.01	2.01	.46	5.64
50	2439	5520.27	1.89	.47	5.52
51	2386	5523.66	1.68	.48	5.59
52	2350	5526.40	1.39	.50	5.87
53	2331	5527.59	1.25	.52	5.77
54	2288	5530.21	1.13	.54	5.73
55	2277	5531.09	.98	.55	5.78
56	2246	5532.78	.99	.56	5.67
57	2208	5535.06	.94	.58	5.61
58	2181	5536.65	.91	.60	5.56
59	2138	5538.89	.89	.61	5.22
60	2098	5541.35	.75	.63	5.19
61	2080	5542.36	.54	.64	4.94
61	2080	5542.39	.54	.64	4.97
62	2078	5542.99	.40	.66	5.28
63	2092	5542.38	.38	.68	5.46
64	2093	5542.18	.60	.69	5.49
65	2041	5545.04	.68	.71	5.35
66	1986	5548.23	.61	.72	5.25
67	1982	5548.89	.29	.74	5.29
68	1972	5549.52	.21	.75	5.28
69	1967	5550.15	.15	.77	5.5
70	1964	5550.42	.11	.79	5.

LINE L-134

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	3028	5487.26	.40	.16	6.07
29	3003	5488.73	.46	.17	6.12
30	2979	5490.21	.49	.19	6.16
31	2958	5491.38	.54	.21	6.13
32	2935	5492.92	.56	.22	6.32
33	2913	5494.12	.59	.24	6.24
34	2891	5495.43	.66	.26	6.28
35	2852	5497.80	.64	.28	6.37
36	2837	5498.54	.60	.29	6.14
37	2804	5500.56	.59	.31	6.21
38	2780	5502.17	.52	.33	6.29
39	2764	5503.05	.46	.34	6.13
40	2750	5503.78	.45	.36	6.02
41	2735	5504.57	.50	.38	5.95
42	2716	5505.46	.58	.40	5.83
43	2698	5506.35	.70	.41	5.75
44	2678	5507.34	.87	.43	5.72
45	2658	5508.23	1.17	.45	5.67
46	2611	5510.80	1.33	.46	5.66
47	2586	5512.10	1.55	.48	5.65
48	2538	5514.61	1.83	.50	5.59
49	2482	5517.96	2.04	.51	5.83
50	2411	5521.47	2.01	.52	5.15
51	2361	5525.18	1.79	.54	5.68
52	2317	5528.37	1.55	.55	6.00
53	2285	5530.56	1.28	.57	5.98
54	2264	5531.93	1.10	.58	5.98
54	2264	5531.89	1.10	.58	5.93
55	2230	5534.00	.97	.60	5.85
56	2222	5534.47	.93	.62	5.80
57	2183	5536.69	.97	.64	5.72
58	2140	5539.21	.93	.66	5.69
59	3099	5541.32	.81	.67	5.23
60	2070	5543.11	.65	.69	5.14
61	2075	5543.31	.49	.70	5.46
62	2103	5541.82	.58	.72	5.6'
63	2109	5541.04	1.21	.74	5.'

LINE L-138

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	3022	5487.72	.50	.19	6.26
29	2995	5489.33	.63	.21	6.34
30	2959	5491.48	.68	.23	6.43
31	2930	5493.10	.68	.24	6.39
32	2905	5494.51	.67	.26	6.33
33	2885	5495.75	.72	.28	6.32
34	2852	5497.92	.75	.30	6.53
35	2823	5499.65	.72	.32	6.52
36	2795	5501.23	.68	.33	6.42
37	2772	5502.53	.66	.35	6.32
38	2739	5503.90	.62	.36	5.69
39	2725	5505.40	.54	.38	6.26
40	2707	5506.48	.56	.40	6.27
41	2687	5507.50	.61	.42	6.11
42	2671	5508.37	.70	.43	6.14
43	2649	5509.44	.84	.45	6.06
44	2629	5510.35	1.05	.46	5.96
45	2596	5512.07	1.26	.48	5.96
46	2561	5513.85	1.50	.50	5.86
47	2513	5516.59	1.69	.52	5.98
48	2465	5519.12	1.87	.54	5.81
49	2397	5522.09	1.90	.55	5.79
50	2338	5526.74	1.70	.56	5.77
51	2292	5529.67	1.38	.58	5.65
52	2269	5531.62	1.02	.59	5.88
53	2267	5532.01	.85	.61	5.93
54	2235	5533.91	.78	.62	5.88
55	2210	5535.50	.66	.64	5.82
56	2210	5535.38	.66	.64	5.70
56	2216	5535.22	.60	.66	5.83
57	2206	5535.50	.85	.68	5.78
58	2157	5538.11	.97	.70	5.58
59	2101	5541.26	.93	.71	5.39
60	2059	5543.93	.76	.72	5.37
61	2051	5544.38	.50	.73	5.07
62	2068	5543.60	.38	.75	5.18
63	2069	5543.30	.55	.77	5.09
64	2022	5546.09	.54	.78	5.05
65	1985	5548.57	.43	.80	5.25
66	1978	5549.16	.23	.81	5.21
67	1973	5549.55	.15	.83	5.23
68	1970	5549.89	.10	.84	5.34
69	1967	5550.24	.08	.86	5.4
70	1969	5550.31	.07	.88	5

LINE L-142

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2997	5489.62	.38	.23	6.52
29	2982	5490.12	.56	.24	6.30
30	2949	5492.16	.69	.26	6.48
31	2905	5494.97	.68	.28	6.69
32	2889	5496.00	.62	.30	6.65
33	2864	5497.28	.65	.31	6.51
34	2839	5498.69	.67	.33	6.46
35	2813	5500.41	.68	.35	6.60
36	2787	5501.71	.68	.36	6.40
37	2762	5503.20	.68	.38	6.35
38	2736	5504.73	.69	.40	6.36
39	2710	5506.13	.70	.42	6.24
40	2685	5507.69	.72	.44	6.28
41	2661	5509.20	.75	.45	6.40
42	2642	5510.25	.82	.47	6.36
43	2620	5511.34	.95	.48	6.31
44	2596	5512.53	1.16	.50	6.28
45	2562	5514.16	1.43	.52	6.12
46	2507	5517.25	1.53	.54	6.10
47	2465	5519.80	1.54	.56	6.14
48	2420	5522.36	1.59	.57	6.06
49	2364	5525.56	1.51	.59	5.86
50	2324	5528.20	1.31	.60	5.95
51	2289	5530.31	1.15	.61	5.84
52	2251	5532.61	.98	.63	5.72
53	2235	5533.82	.75	.64	5.74
54	2220	5534.84	.63	.66	5.74
55	2212	5535.54	.58	.68	5.88
56	2210	5535.72	.68	.69	6.04
56	2210	5535.69	.68	.69	6.00
57	2192	5536.40	.95	.71	5.89
58	2140	5539.16	1.09	.73	5.73
59	2082	5542.54	1.00	.74	5.57
60	2050	5544.68	.75	.76	5.59
61	2029	5545.94	.61	.77	5.45
62	2000	5547.50	.52	.79	5.16
63	1993	5548.21	.33	.81	5.25
64	1989	5548.60	.23	.82	5.31
65	1983	5549.06	.16	.84	5.24
66	1980	5549.39	.10	.86	5.38
67	1978	5549.58	.05	.88	5.40
68	1977	5549.71	.03	.90	5.43
69	1975	5549.96	.04	.91	5.55
?	1974	5550.12	.04	.93	5.65

LINE L-146

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2944	5492.99	.44	.26	6.75
29	2926	5493.99	.42	.28	6.68
30	2908	5495.20	.41	.30	6.80
31	2893	5495.82	.43	.32	6.53
32	2876	5496.54	.46	.34	6.34
33	2858	5497.65	.52	.35	6.35
34	2835	5499.17	.58	.37	6.54
35	2809	5500.62	.64	.38	6.55
36	2779	5502.46	.66	.40	6.57
37	2756	5503.62	.68	.41	6.42
38	2726	5505.34	.72	.43	6.38
39	2697	5507.07	.73	.45	6.41
40	2670	5508.69	.72	.47	6.40
41	2654	5509.50	.75	.48	6.27
42	2633	5510.74	.84	.50	6.34
43	2608	5512.12	.97	.52	6.38
44	2584	5513.38	1.16	.55	6.36
45	2546	5515.32	1.37	.55	6.28
46	2500	5517.86	1.52	.56	6.26
47	2449	5520.84	1.57	.58	6.26
48	2397	5523.90	1.48	.60	6.15
49	2357	5526.47	1.31	.61	6.17
50	2324	5528.57	1.16	.62	6.16
51	2292	5530.57	1.06	.64	6.16
52	2258	5532.49	.95	.66	5.95
53	2228	5534.39	.79	.68	5.89
54	2216	5535.29	.62	.69	5.92
55	2204	5536.26	.58	.71	6.11
56	2193	5536.93	.62	.73	6.11
57	2171	5538.07	.75	.74	6.07
58	2132	5540.13	.82	.76	5.92
59	2088	5542.67	.77	.78	5.79
60	2060	5544.35	.63	.80	5.65
61	2034	5545.76	.52	.81	5.41
62	2017	5546.56	.40	.83	5.04
63	2003	5547.73	.30	.85	5.27
64	1996	5548.23	.21	.86	5.30
65	1988	5548.83	.15	.88	5.35
66	1984	5549.40	.10	.90	5.60
67	1983	5549.38	.07	.91	5.46
68	1981	5549.63	.05	.93	5.56
69	1980	5549.78	.04	.95	5.64
70	1980	5550.02	.04	.96	5.88

LINE L-150

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2915	5494.77	.32	.20	6.66
29	2902	5495.23	.33	.32	6.40
30	2888	5496.06	.38	.24	6.51
31	2869	5497.29	.42	.35	6.51
32	2851	5498.26	.47	.37	6.46
33	2830	5499.58	.53	.39	6.58
34	2805	5501.03	.57	.40	6.62
35	2783	5502.19	.61	.42	6.49
36	2761	5503.57	.68	.44	6.62
37	2736	5504.92	.76	.46	6.54
38	2710	5506.26	.90	.47	6.48
39	2666	5508.82	.95	.49	6.51
40	2636	5510.76	.91	.50	6.61
41	2607	5512.52	.89	.52	6.64
42	2588	5513.53	.92	.54	6.53
43	2566	5514.66	1.07	.56	6.50
44	2526	5516.93	1.17	.58	6.45
45	2491	5518.82	1.26	.59	6.39
46	2442	5521.72	1.25	.61	6.35
47	2407	5523.83	1.16	.62	6.30
48	2368	5526.16	1.10	.64	6.27
49	2332	5528.39	.99	.66	6.24
50	2306	5530.01	.86	.68	6.18
51	2281	5531.64	.79	.70	6.26
52	2254	5533.10	.73	.71	6.03
53	2232	5534.12	.64	.72	5.64
54	2220	5535.04	.59	.74	5.83
55	2214	5535.68	.71	.76	6.18
56	2182	5537.41	.84	.78	6.12
57	2141	5539.83	.88	.80	6.15
58	2098	5542.00	.82	.81	5.70
59	2068	5544.13	.69	.83	5.94
60	2038	5545.86	.57	.84	5.80
61	2017	5546.97	.43	.86	5.50
62	2015	5547.06	.27	.88	5.28
63	2008	5547.71	.20	.90	5.40
64	2003	5548.13	.14	.92	5.48
65	1997	5548.58	.10	.94	5.52
66	1995	5548.81	.07	.96	5.55
67	1994	5549.07	.07	.97	5.73
68	1996	5549.17	.09	.99	5.97
69	2011	5548.37	.10	1.01	6.03
3	2017	5548.00	.12	1.02	6.04

LINE L-154

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2896	5495.89	.46	.34	6.78
29	2874	5496.95	.50	.36	6.59
30	2849	5498.48	.52	.37	6.64
31	2827	5499.84	.54	.39	6.69
32	2799	5501.53	.53	.41	6.73
33	2782	5502.62	.51	.43	6.74
34	2761	5503.85	.53	.45	6.73
35	2743	5504.84	.55	.46	6.72
36	2726	5505.84	.63	.48	6.74
37	2703	5507.07	.73	.50	6.70
38	2681	5508.15	.92	.52	6.65
39	2637	5510.74	1.00	.54	6.72
40	2607	5512.51	1.01	.55	6.73
41	2577	5514.37	1.05	.57	6.81
42	2553	5515.65	1.18	.59	6.78
43	2513	5517.76	1.37	.60	6.73
44	2458	5520.98	1.38	.62	6.66
45	2417	5523.44	1.24	.63	6.58
46	2384	5525.62	1.10	.65	6.63
47	2355	5527.34	1.00	.67	6.56
48	2325	5529.15	.92	.69	6.51
49	2300	5530.90	.84	.70	6.66
50	2277	5532.03	.81	.72	6.41
51	2250	5533.52	.85	.74	6.29
52	2204	5536.13	.78	.75	6.12
53	2191	5537.03	.58	.77	6.04
54	2177	5538.08	.56	.79	6.24
55	2153	5539.48	.57	.81	6.33
56	2125	5541.08	.55	.82	6.09
57	2105	5542.07	.55	.84	5.94
58	2061	5544.64	.53	.86	5.87
59	2058	5544.97	.30	.87	5.75
60	2051	5545.55	.23	.89	5.80
61	2045	5546.00	.20	.91	5.85
62	2029	5546.86	.19	.92	5.78
63	2014	5547.74	.16	.94	5.70
64	2007	5548.13	.11	.96	5.61
65	2002	5548.44	.09	.98	5.61
66	1999	5548.64	.09	1.00	5.58
67	1998	5549.01	.10	1.01	5.90
68	1996	5549.19	.12	1.03	6.00
69	1996	5549.17	.15	1.05	5.9

LINE L-158

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2854	5498.58	.40	.38	6.87
29	2824	5500.40	.43	.39	6.97
30	2804	5501.57	.42	.41	6.93
31	2780	5503.03	.44	.43	6.98
32	2757	5504.29	.42	.44	6.86
33	2742	5505.31	.40	.46	6.94
34	2728	5506.09	.42	.48	6.92
35	2717	5506.71	.49	.50	6.89
36	2699	5507.62	.57	.52	6.85
37	2685	5508.15	.73	.53	6.66
38	2656	5509.70	.90	.55	6.66
39	2619	5511.81	1.05	.56	6.74
40	2574	5514.51	1.07	.58	6.76
41	2547	5516.03	1.10	.60	6.70
42	2503	5518.49	1.14	.61	6.60
43	2461	5521.27	1.05	.63	6.84
44	2440	5522.63	.95	.65	6.83
45	2411	5524.32	.92	.66	6.78
46	2388	5525.70	.92	.68	6.74
47	2355	5527.50	.94	.70	6.64
48	2315	5529.92	.86	.72	6.58
49	2297	5531.39	.72	.74	6.82
50	2287	5531.65	.82	.75	6.58
51	2242	5533.90	.90	.77	6.25
52	2195	5536.63	.81	.78	6.08
53	2165	5538.62	.61	.80	6.10
54	2154	5539.55	.41	.81	6.16
55	2147	5540.15	.30	.83	6.22
56	2149	5540.14	.23	.85	6.25
57	2152	5539.91	.28	.87	6.20
58	2130	5541.12	.29	.89	6.13
59	2110	5542.33	.26	.90	6.12
60	2109	5542.38	.30	.92	6.13
61	2087	5543.55	.35	.94	6.04
62	2060	5545.08	.37	.95	5.95
63	2034	5546.65	.33	.97	5.94
64	2014	5547.90	.28	.99	5.92
65	2000	5548.71	.23	1.01	5.88
66	1998	5548.76	.17	1.02	5.71
67	1996	5548.95	.16	1.04	5.80
68	1996	5548.99	.18	1.06	5.82
69	1997	5548.89	.24	1.08	5.79

LINE L-162

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2795	5502.41	.34	.41	7.15
29	2775	5503.60	.36	.42	7.16
30	2752	5505.04	.35	.44	7.25
31	2733	5506.11	.32	.46	7.14
32	2724	5506.63	.29	.48	7.06
33	2715	5507.05	.33	.50	6.96
34	2702	5507.76	.39	.51	6.99
35	2686	5508.57	.48	.53	6.89
36	2668	5509.46	.60	.55	6.85
37	2638	5511.09	.68	.56	6.80
38	2617	5512.33	.76	.58	6.82
39	2593	5513.66	.91	.60	6.88
40	2561	5515.15	1.09	.62	6.66
41	2515	5517.77	1.20	.63	6.68
42	2467	5520.70	1.15	.65	6.70
43	2434	5522.85	1.02	.67	6.72
44	2410	5524.33	.95	.68	6.71
45	2377	5526.29	.93	.70	6.70
46	2343	5528.33	.83	.72	6.60
47	2319	5529.71	.69	.74	6.42
48	2305	5530.63	.59	.75	6.40
49	2290	5531.44	.61	.76	6.31
50	2257	5533.40	.63	.78	6.33
51	2221	5535.54	.59	.80	6.29
52	2190	5537.22	.47	.81	6.05
53	2180	5537.92	.31	.83	5.97
54	2175	5538.70	.24	.84	6.33
55	2187	5538.15	.19	.86	6.42
56	2187	5538.20	.21	.88	6.48
57	2174	5538.85	.27	.90	6.44
57	2174	5538.80	.27	.90	6.39
58	2153	5540.01	.28	.91	6.32
59	2136	5540.80	.27	.93	6.10
60	2131	5541.30	.29	.95	6.30
61	2126	5541.49	.46	.96	6.37
62	2090	5543.26	.56	.98	6.11
63	2047	5545.92	.52	.99	6.18
64	2028	5547.18	.40	1.01	6.13
65	2003	5548.62	.36	1.03	6.09
66	1999	5548.73	.25	1.04	5.84
67	2001	5548.65	.20	1.06	5.80
68	1999	5548.81	.21	1.08	5.85
69	1999	5548.92	.27	1.09	5.9
	2002	5548.91	.45	1.11	6.3

LINE L-166

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2747	5505.25	.21	.45	7.01
29	2729	5506.49	.21	.46	7.18
30	2719	5507.08	.22	.48	7.17
31	2706	5507.96	.24	.50	7.24
32	2698	5508.36	.27	.52	7.20
33	2691	5508.69	.35	.54	7.17
34	2678	5509.27	.46	.56	7.07
35	2662	5510.01	.64	.57	7.03
36	2623	5512.17	.70	.59	6.97
37	2600	5513.54	.74	.61	6.99
38	2573	5514.98	.86	.63	6.95
39	2535	5517.27	.96	.64	7.06
40	2492	5519.81	.95	.66	7.06
41	2459	5521.91	.85	.68	7.09
42	2434	5523.50	.74	.70	7.07
43	2437	5523.19	.73	.72	6.94
44	2414	5524.52	.83	.74	6.94
45	2381	5526.36	.95	.75	6.95
46	2333	5529.03	.96	.77	6.80
47	2289	5531.79	.80	.78	6.78
48	2274	5532.85	.58	.80	6.71
49	2251	5534.18	.53	.82	6.60
50	2219	5535.97	.47	.84	6.43
51	2212	5536.32	.29	.86	6.17
52	2208	5536.79	.20	.88	6.32
53	2209	5537.02	.15	.89	6.57
54	2218	5536.56	.15	.91	6.58
55	2236	5535.41	.19	.93	6.54
56	2250	5534.50	.33	.94	6.55
57	2232	5535.54	.39	.96	6.58
57	2232	5535.49	.39	.96	6.53
58	2197	5537.61	.38	.98	6.56
59	2184	5538.45	.36	.99	6.58
60	2184	5538.33	.48	1.01	6.60
61	2176	5538.40	.83	1.03	6.51
62	2118	5541.73	.87	1.05	6.43
63	2078	5544.18	.79	1.06	6.45
64	2040	5546.41	.73	1.08	6.33
65	2006	5548.51	.62	1.10	6.29
66	1999	5549.03	.39	1.12	6.15
	1996	5549.24	.30	1.14	6.0

LINE L-170

DENSITY= 2.75

ST	ELEV	OBS G	TERR	LATT	GRAV
28	2718	5506.80	.35	.49	6.96
29	2702	5507.73	.35	.51	6.93
30	2687	5508.63	.37	.52	6.90
31	2673	5509.30	.40	.54	6.78
32	2654	5510.44	.46	.56	6.85
33	2630	5511.80	.49	.58	6.81
34	2607	5513.41	.49	.60	7.02
35	2588	5514.38	.49	.61	6.88
36	2570	5515.38	.57	.63	6.85
37	2534	5517.45	.59	.65	6.82
38	2509	5519.19	.54	.66	7.02
39	2487	5520.65	.50	.68	7.10
40	2470	5521.62	.46	.70	7.04
41	2462	5522.07	.47	.72	7.02
42	2456	5522.27	.61	.74	6.99
43	2427	5523.94	.73	.76	7.00
44	2391	5525.96	.76	.77	6.92
45	2358	5527.94	.71	.79	6.93
46	2340	5529.00	.73	.80	6.93
47	2301	5530.95	.79	.82	6.59
48	2257	5533.66	.74	.84	6.63
49	2224	5535.67	.59	.86	6.56
50	2231	5536.00	.34	.87	6.42
51	2221	5536.20	.22	.89	6.50
52	2225	5536.10	.16	.91	6.57
53	2237	5535.38	.13	.93	6.52
54	2246	5534.91	.15	.95	6.57
55	2238	5535.36	.17	.96	6.54
56	2219	5536.53	.18	.98	6.56
57	2209	5537.01	.17	1.00	6.45
58	2208	5537.17	.22	1.02	6.59
59	2206	5537.00	.38	1.03	6.46
60	2188	5537.84	.56	1.05	6.38
61	2149	5540.35	.61	1.07	6.59
62	2119	5542.04	.59	1.08	6.51
63	2089	5543.82	.55	1.10	6.44
64	2063	5545.25	.48	1.12	6.24
65	2045	5546.55	.39	1.14	6.38
66	2033	5547.10	.34	1.15	6.17
67	2012	5548.24	.33	1.17	6.04
68	1985	5549.85	.31	1.18	6.05
[illegible]	1985	5549.94	.19	1.20	5.
	1995	5549.55	.12	1.22	6.

LINE L-174

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2996	5492.57	.11	.05	18.84
1	3005	5491.84	.16	.07	18.70
2	3007	5592.77	.25	.08	.11
3	2993	5492.27	.33	.10	18.55
4	2969	5493.64	.40	.12	18.47
5	2938	5495.41	.43	.14	18.33
6	2907	5497.33	.41	.15	18.29
7	2879	5498.86	.36	.17	18.03
8	2860	5500.12	.29	.19	17.98
9	2849	5500.88	.21	.20	18.00
10	2844	5501.26	.15	.22	17.96
11	2842	5501.44	.11	.24	17.95
12	2839	5501.63	.08	.26	17.89
13	2842	5501.25	.06	.27	17.67
14	2844	5501.10	.05	.29	17.63
15	2847	5500.76	.06	.31	17.50
16	2844	5500.86	.07	.32	17.39
17	2835	5501.33	.08	.34	17.28
18	2825	5501.77	.09	.36	17.10
19	2816	5502.06	.10	.38	16.81
20	2815	5502.09	.11	.40	16.75
21	2808	5502.27	.15	.41	16.54
22	2798	5502.67	.19	.43	16.36
23	2783	5503.45	.24	.44	16.21
24	2764	5504.56	.26	.46	16.19
25	2748	5505.48	.29	.48	16.12
26	2731	5506.48	.32	.50	16.08
27	2713	5507.50	.35	.52	15.97
28	2695	5508.47	.38	.53	15.87
28	2695	5508.47	.38	.53	15.87
29	2679	5509.26	.43	.55	15.66
30	2659	5510.34	.49	.56	15.55
31	2632	5511.84	.53	.58	15.37
32	2606	5513.28	.54	.60	15.18
33	2576	5514.95	.53	.62	15.01
34	2553	5516.22	.51	.63	14.79
35	2527	5517.79	.49	.65	14.70
36	2502	5519.19	.45	.67	14.46
37	2477	5520.61	.39	.68	14.31
38	2480	5520.42	.32	.70	14.19
39	2467	5521.29	.34	.72	14.24
40	2452	5522.23	.38	.74	14.29
41	2435	5523.39	.44	.76	14.40
42	2412	5524.76	.49	.77	14.41
43	2385	5526.43	.51	.79	14.39
44	2362	5527.89	.51	.80	14.43
45	2339	5529.21	.55	.82	14.36
46	2305	5531.12	.59	.84	14.16
	266	5533.32	.55	.86	13.8
	238	5534.91	.44	.87	13.5
	32	5535.40	.27	.89	13.4
	30	5535.76	.19	.90	13
	37	5535.40	.12	.92	13.
52	2247	5534.90	.10	.94	13. .
53	2250	5534.76	.10	.96	13.74
54	2247	5534.89	.15	.97	13.72
55	2227	5536.02	.15	.98	13.60
56	2219	5536.41	.15	1.00	13.48
57	2216	5536.60	.20	1.02	13.53
58	2210	5536.79	.31	1.04	13.44
59	2190	5537.85	.40	1.05	13.33
60	2164	5539.39	.48	1.07	13.32
61	2134	5541.07	.51	1.09	13.13
62	2106	5542.72	.49	1.10	12.99
63	2081	5544.18	.44	1.12	12.83
64	2061	5545.30	.38	1.14	12.68
65	2047	5546.11	.37	1.16	12.53
66	2022	5547.43	.37	1.17	12.32
67	1996	5548.97	.34	1.18	12.21
68	1970	5550.60	.33	1.20	12.19
69	1977	5550.36	.18	1.22	12.19
70	1991	5550.18	.11	1.24	12.78
71	1998	5549.57	.09	1.26	12.56

LINE L-178

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2979	5493.45	.21	.10	18.73
1	2980	5493.26	.26	.12	18.64
2	2959	5494.41	.30	.14	18.50
3	2939	5495.62	.33	.15	18.4
4	2910	5497.39	.32	.17	18.4
5	2894	5498.32	.31	.18	18.3
6	2868	5499.89	.30	.20	18.2
7	2849	5500.99	.25	.22	18.08
8	2835	5501.82	.20	.23	18.02
9	2826	5502.49	.15	.25	18.03
10	2822	5502.63	.11	.27	17.86
11	2820	5502.56	.08	.28	17.67
12	2821	5502.56	.06	.30	17.68
13	2827	5502.13	.06	.32	17.62
14	2828	5501.99	.06	.34	17.49
15	2826	5501.94	.08	.35	17.33
16	2817	5502.29	.10	.37	17.15
17	2803	5503.12	.10	.39	17.04
18	2802	5503.16	.10	.40	17.01
19	2796	5503.27	.14	.42	16.78
20	2778	5504.24	.16	.44	16.65
20	2778	5504.23	.16	.44	16.64
21	2769	5504.62	.18	.46	16.46
22	2750	5505.64	.19	.48	16.32
23	2744	5505.90	.19	.50	16.17
24	2737	5506.24	.24	.51	16.10
25	2724	5506.92	.32	.52	16.02
26	2696	5508.68	.35	.54	16.06
27	2677	5509.91	.33	.56	16.05
28	2666	5510.49	.36	.57	15.98
28	2666	5510.49	.36	.57	15.98
29	2648	5511.42	.42	.59	15.82
30	2625	5512.64	.48	.60	15.68
31	2597	5514.34	.51	.62	15.66
32	2570	5515.99	.51	.64	15.63
33	2547	5517.41	.49	.65	15.58
34	2532	5518.24	.48	.67	15.45
35	2512	5519.42	.51	.69	15.39
36	2490	5520.63	.57	.70	15.30
37	2455	5522.43	.56	.72	14.87
38	2442	5522.95	.51	.74	14.49
39	2422	5524.79	.61	.75	15.22
40	2381	5527.19	.66	.77	15.10
41	2338	5529.67	.59	.78	14.82
42	2317	5530.77	.44	.80	14.46
43	2336	5529.55	.29	.82	14.20
44	2322	5530.28	.26	.84	14.02
45	2302	5531.72	.24	.85	14.21
46	2284	5532.92	.21	.87	14.22
47	2271	5533.66	.16	.88	14.11
	2260	5534.36	.13	.90	14.06
	253	5534.85	.10	.92	14.09
	51	5535.03	.08	.94	
51	2248	5535.02	.09	.96	
52	2244	5535.11	.10	.98	13.73
53	2238	5535.34	.13	.99	13.56
54	2233	5535.67	.18	1.01	13.62
55	2228	5535.94	.25	1.03	13.67
56	2219	5536.39	.38	1.04	13.66
57	2196	5537.27	.46	1.06	13.20
58	2177	5538.50	.58	1.07	13.33
59	2146	5540.24	.69	1.09	13.25
60	2110	5542.25	.74	1.10	13.06
61	2074	5544.44	.74	1.12	12.96
62	2035	5546.71	.68	1.14	12.72
63	2010	5547.85	.54	1.15	12.16
64	1990	5548.93	.43	1.16	11.92
65	1973	5550.05	.34	1.18	11.84
66	1962	5550.89	.24	1.20	11.86
67	1954	5551.47	.17	1.22	11.88
68	1945	5552.11	.13	1.24	11.93
69	1937	5552.64	.11	1.25	11.90
70	1940	5552.47	.08	1.27	11.89

LINE L-182

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2940	5495.62	.57	.13	18.78
1	2924	5496.69	.40	.15	18.70
2	2924	5496.61	.28	.17	18.47
3	2922	5496.71	.26	.18	18.40
4	2915	5496.95	.30	.20	18.23
5	2899	5497.85	.40	.22	18.19
6	2858	5500.39	.39	.23	18.19
7	2835	5501.87	.28	.25	18.12
8	2823	5502.63	.20	.27	18.06
9	2813	5503.25	.16	.28	17.97
10	2808	5503.60	.12	.30	17.93
11	2805	5503.60	.09	.32	17.74
12	2800	5503.87	.08	.33	17.67
13	2794	5504.18	.07	.35	17.58
14	2802	5503.53	.07	.37	17.37
15	2797	5503.62	.07	.39	17.18
16	2786	5504.21	.07	.40	17.08
17	2782	5504.48	.07	.42	17.03
18	2788	5504.71	.13	.44	17.72
19	2770	5504.91	.13	.45	16.80
20	2759	5505.37	.15	.47	16.53
21	2736	5506.74	.16	.49	16.51
22	2727	5507.09	.14	.50	16.26
23	2731	5507.02	.15	.52	16.38
24	2741	5505.79	.23	.54	15.83
25	2736	5505.87	.35	.56	15.71
26	2714	5506.99	.46	.57	15.61
27	2686	5508.77	.56	.59	15.72
28	2648	5511.03	.56	.61	15.55
28	2648	5511.13	.56	.61	15.66
29	2626	5512.24	.53	.62	15.41
30	2605	5513.57	.58	.64	15.43
31	2576	5515.30	.62	.65	15.40
32	2549	5516.92	.63	.67	15.30
33	2521	5518.64	.61	.69	15.26
34	2498	5520.11	.57	.71	15.24
35	2486	5520.74	.60	.72	15.12
36	2456	5522.41	.63	.74	14.98
37	2433	5523.73	.64	.76	14.82
38	2407	5525.13	.71	.77	14.66
39	2363	5527.60	.69	.78	14.39
40	2337	5529.09	.58	.80	14.12
41	2313	5530.33	.51	.82	13.81
42	2287	5531.73	.46	.84	13.49
43	2262	5533.07	.37	.85	13.22
44	2259	5533.33	.23	.87	13.10
45	2262	5533.13	.18	.89	13.02
46	2254	5533.74	.17	.90	13.12
[illegible]	2254	5533.73	.17	.90	13.11
[illegible]	2242	5534.48	.16	.92	13.07
[illegible]	2228	5535.35	.17	.94	13.[illegible]
[illegible]	2213	5536.24	.19	.96	13.[illegible]
[illegible]	2187	5537.78	.20	.97	1
[illegible]	2196	5537.35	.11	.99	1
[illegible]	2199	5537.24	.12	1.00	13.04
[illegible]	2202	5536.99	.16	1.02	12.99
54	2192	5537.61	.24	1.04	13.07
55	2161	5539.20	.26	1.06	12.72
56	2136	5540.43	.23	1.07	12.34
57	2119	5541.26	.18	1.09	12.05
58	2112	5541.70	.14	1.10	11.99
59	2110	5541.85	.12	1.12	12.02
60	2106	5542.11	.21	1.14	12.07
61	2136	5540.35	.26	1.15	12.25
62	2157	5539.03	.39	1.16	12.33
63	2140	5540.03	.41	1.18	12.30
64	2118	5541.33	.48	1.20	12.27
65	2098	5542.31	.59	1.21	12.10
66	2069	5543.95	.74	1.23	12.08
67	2024	5546.60	.77	1.35	11.82
68	1985	5548.95	.74	1.27	11.79
69	1949	5551.04	.68	1.29	11.61
70	1916	5553.16	.59	1.30	11.57
71	1898	5554.25	.44	1.32	11.35

LINE L-186

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2909	5496.65	.93	.18	18.25
1	2879	5498.64	.73	.20	18.11
2	2857	5500.18	.58	.21	18.12
3	2843	5500.96	.51	.23	17.97
4	2806	5503.26	.47	.24	17.88
5	2799	5503.62	.27	.26	17.61
6	2792	5504.10	.19	.28	17.56
7	2787	5504.36	.13	.29	17.44
8	2786	5504.41	.08	.31	17.39
9	2788	5504.22	.06	.33	17.26
10	2787	5504.25	.05	.34	17.22
11	2787	5504.25	.06	.36	17.18
12	2782	5504.43	.08	.38	17.07
13	2771	5505.02	.11	.40	16.94
14	2748	5506.45	.12	.42	16.94
15	2752	5506.08	.07	.43	16.77
16	2759	5505.51	.07	.46	16.62
17	2757	5505.50	.08	.47	16.45
18	2755	5505.53	.11	.49	16.42
19	2748	5505.68	.17	.50	16.15
20	2727	5506.92	.21	.52	16.10
21	2700	5508.70	.21	.54	16.20
22	2690	5509.18	.18	.56	16.00
23	2700	5508.35	.19	.57	15.80
23	2700	5508.37	.19	.57	15.82
24	2706	5507.77	.32	.59	15.68
25	2687	5508.79	.43	.60	15.63
26	2654	5510.80	.49	.62	15.65
27	2626	5512.37	.50	.64	15.48
28	2603	5513.79	.50	.66	15.41
28	2603	5513.84	.50	.66	15.46
29	2591	5514.48	.58	.68	15.43
30	2558	5516.55	.65	.68	15.50
31	2528	5518.22	.65	.70	15.31
32	2506	5519.54	.67	.71	15.25
33	2474	5521.57	.68	.73	15.31
34	2445	5523.14	.66	.75	15.06
35	2410	5525.04	.59	.77	14.70
36	2392	5526.01	.49	.78	14.38
37	2370	5527.19	.46	.80	14.16
38	2340	5529.08	.43	.82	14.13
39	2312	5530.81	.39	.84	14.04
40	2322	5530.32	.18	.86	13.98
41	2327	5530.10	.11	.87	14.01
41	2327	5530.09	.11	.87	14.00
42	2330	5529.91	.08	.89	13.94
43	2331	5529.85	.07	.91	13.94
44	2324	5530.15	.07	.93	13.76
45	2317	5530.65	.07	.95	13.77
46	2306	5531.24	.06	.96	13.6
	2302	5531.40	.05	.98	13.5
	2298	5531.56	.05	.99	13.4
	2293	5531.92	.05	1.01	13.4
	2289	5532.14	.05	1.03	
	2286	5532.23	.05	1.05	.. ..
52	2284	5532.48	.04	1.06	12.41
53	2283	5532.48	.05	1.08	13.33
54	2275	5532.97	.05	1.10	13.35
55	2270	5533.24	.05	1.12	13.26
56	2267	5533.41	.05	1.13	13.25
57	2267	5533.39	.06	1.15	13.24
58	2262	5533.62	.08	1.16	13.15
59	2257	5533.86	.10	1.18	13.07
60	2253	5534.00	.16	1.20	12.99
61	2246	5534.33	.23	1.21	12.98
62	2240	5534.65	.35	1.23	13.00
63	2232	5534.92	.50	1.25	12.90
64	2219	5535.41	.63	1.26	12.73
65	2189	5536.81	.84	1.28	12.46
66	2150	5538.88	.99	1.30	12.22
67	2096	5541.98	1.14	1.31	12.13
68	2038	5545.46	1.14	1.33	11.96
69	1996	5547.98	1.03	1.34	11.72
70	1947	5550.83	.93	1.36	

LINE L-190

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2929	5495.15	.92	.24	17.89
1	2892	5497.55	.84	.25	17.88
2	2868	5499.27	.74	.26	18.04
3	2839	5501.14	.70	.28	18.05
4	2805	5502.27	.61	.31	16.92
5	2783	5504.51	.47	.32	17.64
6	2765	5505.48	.36	.33	17.37
7	2749	5506.57	.27	.35	17.39
8	2742	5507.05	.16	.36	17.30
9	2743	5506.85	.11	.38	17.09
10	2732	5507.42	.10	.40	16.97
11	2730	5507.45	.08	.41	16.83
12	2728	5507.54	.07	.43	16.73
13	2724	5507.68	.07	.45	16.64
14	2725	5507.63	.07	.47	16.60
15	2721	5507.71	.10	.49	16.47
16	2714	5508.06	.15	.50	16.40
17	2687	5509.66	.16	.52	16.35
18	2669	5510.80	.14	.53	16.34
19	2675	5510.30	.09	.55	16.15
20	2665	5510.85	.10	.57	16.06
21	2658	5511.30	.14	.59	16.04
23	2684	5509.39	.22	.63	15.83
24	2690	5508.75	.42	.64	15.74
25	2656	5510.98	.41	.66	15.81
26	2639	5511.97	.48	.67	15.80
27	2610	5513.51	.54	.68	15.62
28	2589	5514.80	.64	.70	15.65
28	2589	5514.84	.64	.70	15.69
29	2551	5517.14	.69	.72	15.67
30	2519	5519.04	.66	.74	15.52
31	2491	5520.81	.62	.75	15.52
32	2463	5522.20	.55	.76	15.11
33	2435	5523.88	.48	.78	14.96
34	2413	5525.04	.41	.80	14.66
35	2389	5526.54	.37	.82	14.59
36	2386	5526.87	.29	.83	14.65
37	2408	5525.70	.16	.85	14.71
38	2418	5525.19	.11	.87	14.71
39	2426	5524.68	.08	.88	14.70
40	2435	5524.11	.07	.90	14.66
41	2442	5523.64	.06	.92	14.57
42	2443	5523.53	.06	.94	14.54
43	2450	5523.04	.07	.95	14.46
44	2460	5522.34	.09	.97	14.38
45	2466	5521.86	.13	.98	14.27
46	2453	5522.41	.16	1.00	14.03
47	2420	5524.29	.16	1.02	13.8
	5	5524.62	.12	1.04	13.8
	16	5523.20	.11	1.05	13.6
	2434	5523.25	.13	1.07	
	2413	5524.59	.12	1.08	13.5
52	2408	5524.89	.10	1.10	13.59
53	2404	5525.21	.12	1.12	13.63
54	2395	5525.53	.18	1.14	13.42
55	2369	5527.00	.18	1.15	13.29
56	2356	5527.78	.15	1.17	13.22
57	2351	5528.19	.13	1.18	13.27
58	2348	5528.37	.14	1.20	13.26
59	2342	5528.69	.18	1.22	13.23
60	2329	5529.36	.24	1.24	13.16
61	2314	5530.20	.32	1.26	13.10
62	2295	5531.36	.38	1.27	13.11
63	2281	5532.05	.47	1.29	12.99
64	2268	5532.65	.60	1.30	12.90
65	2254	5533.10	.83	1.32	12.74
66	2230	5534.21	1.16	1.34	12.64
67	2181	5536.80	1.42	1.35	12.45
68	2122	5540.31	1.50	1.37	12.32
69	2066	5543.61	1.41	1.3	
	2026	5546.08	1.26	1.4	

LINE L-194

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2929	5495.16	.76	.25	17.72
1	2887	5497.90	.75	.26	17.83
2	2869	5499.16	.65	.28	17.84
3	2843	5500.82	.61	.30	17.83
4	2826	5501.71	.66	.32	17.73
5	2779	5503.51	.62	.34	16.56
6	2771	5505.06	.44	.35	17.41
7	2758	5506.09	.47	.37	17.60
8	2719	5508.38	.44	.39	17.43
9	2699	5509.41	.31	.40	17.11
10	2692	5509.82	.21	.42	16.96
11	2684	5510.30	.16	.44	16.88
12	2677	5510.70	.12	.46	16.78
13	2669	5511.07	.10	.47	16.62
14	2666	5511.11	.07	.49	16.43
15	2665	5511.19	.06	.51	16.39
16	2666	5511.02	.06	.52	16.28
17	2662	5511.11	.07	.54	16.12
18	2650	5511.95	.11	.56	16.19
19	2631	5513.17	.22	.58	16.37
20	2655	5511.47	.21	.60	16.12
21	2684	5509.60	.27	.61	16.12
22	2704	5507.90	.42	.63	15.78
23	2686	5509.07	.43	.65	15.80
24	2658	5510.82	.47	.66	15.85
25	2629	5512.67	.50	.68	15.89
26	2603	5514.21	.53	.70	15.83
27	2575	5515.81	.56	.72	15.72
28	2541	5517.91	.54	.74	15.63
28	2541	5517.96	.54	.74	15.69
29	2519	5519.21	.49	.75	15.54
30	2492	5520.74	.46	.77	15.34
31	2472	5521.94	.41	.78	15.21
32	2445	5523.57	.41	.80	15.14
33	2422	5525.00	.47	.82	15.18
34	2441	5524.03	.30	.84	15.23
34	2441	5523.95	.30	.84	15.16
35	2463	5522.81	.24	.85	15.28
36	2483	5521.61	.21	.87	15.29
37	2500	5520.56	.19	.88	15.29
38	2519	5519.42	.17	.90	15.28
39	2527	5518.91	.13	.92	15.20
40	2532	5518.58	.13	.93	15.13
41	2544	5517.71	.12	.95	15.02
42	2551	5517.17	.09	.97	14.88
43	2553	5516.94	.08	.98	14.76
44	2565	5516.16	.08	1.00	14.67
45	2568	5515.88	.06	1.02	14.55
46	2574	5515.38	.06	1.04	14.40
47	2579	5514.95	.07	1.06	14.29
	2574	5515.09	.07	1.08	14.11
	2567	5515.43	.08	1.09	13.96
	2564	5515.46	.10	1.11	13.
	2557	5515.56	.14	1.13	13.54
	2547	5516.30	.18	1.15	13.61
53	2538	5516.77	.22	1.16	13.57
54	2531	5516.87	.34	1.18	13.37
55	2503	5518.64	.39	1.20	13.40
56	2481	5520.00	.42	1.21	13.39
57	2456	5521.51	.44	1.23	13.39
58	2435	5522.74	.47	1.25	13.30
59	2406	5524.50	.48	1.26	13.30
60	2381	5526.09	.46	1.28	13.28
61	2364	5527.23	.45	1.30	13.35
62	2348	5528.09	.48	1.32	13.19
63	2334	5528.83	.54	1.33	13.14
64	2325	5529.05	.70	1.35	12.90
65	2308	5529.64	.98	1.37	12.69
66	2267	5531.89	1.19	1.38	12.64
67	2228	5534.14	1.39	1.40	12.64
68	2177	5537.00	1.53	1.42	12.44
69	2126	5540.02	1.55	1.43	12
	2078	5543.02	1.52	1.44	.

LINE L-198

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2941	5494.73	.60	.29	17.85
1	2922	5495.96	.65	.31	17.92
2	2892	5497.69	.70	.33	17.82
3	2864	5499.52	.72	.34	17.90
4	2830	5501.53	.71	.36	17.76
5	2805	5502.84	.68	.38	17.50
6	2775	5504.86	.65	.39	17.61
7	2749	5506.51	.60	.41	17.56
8	2726	5507.88	.56	.43	17.46
9	2698	5509.24	.52	.44	17.04
10	2672	5510.90	.44	.46	16.97
11	2653	5512.02	.35	.48	16.77
12	2635	5513.05	.28	.50	16.60
13	2624	5513.68	.20	.51	16.45
14	2617	5514.07	.14	.53	16.33
15	2618	5513.89	.09	.55	16.15
16	2621	5513.59	.07	.56	16.04
17	2614	5514.04	.09	.58	16.05
18	2596	5515.08	.16	.60	16.02
19	2616	5513.79	.11	.62	15.88
20	2630	5512.78	.12	.63	15.78
21	2641	5511.97	.17	.65	15.66
22	2645	5511.63	.26	.67	15.63
23	2627	5512.70	.29	.68	15.60
24	2608	5513.97	.34	.70	15.71
25	2582	5515.55	.35	.72	15.65
26	2561	5516.80	.37	.74	15.65
27	2553	5518.55	.38	.75	15.64
28	2509	5520.07	.36	.77	15.61
28	2509	5520.05	.36	.77	15.59
29	2485	5521.67	.36	.79	15.70
30	2457	5523.28	.39	.80	15.58
31	2462	5522.99	.26	.82	15.45
32	2471	5522.48	.23	.84	15.49
33	2486	5521.56	.23	.86	15.47
34	2505	5520.39	.23	.87	15.49
35	2521	5519.56	.24	.89	15.61
36	2542	5518.23	.24	.90	15.55
37	2557	5517.29	.23	.92	15.53
38	2572	5516.31	.23	.94	15.50
39	2585	5515.42	.23	.96	15.37
40	2606	5514.04	.22	.98	15.23
41	2624	5512.79	.18	.99	15.07
42	2630	5512.31	.13	1.00	14.93
43	2640	5511.62	.12	1.02	14.80
44	2631	5512.10	.07	1.04	14.69
45	2629	5512.19	.05	1.06	14.58
46	2632	5511.86	.05	1.08	14.45
[illegible]	2634	5511.54	.05	1.09	14.25
[illegible]	2636	5511.27	.06	1.11	14.0[illegible]
[illegible]	2634	5511.36	.09	1.13	14.0[illegible]

	2630	5511.42	.13	1.14	13
	2619	5511.95	.17	1.16	13
52	2608	5512.49	.22	1.18	13
53	2601	5512.74	.32	1.19	13
54	2584	5513.70	.40	1.21	13.50
55	2570	5514.31	.54	1.23	13.35
56	2537	5516.24	.63	1.24	13.35
57	2506	5518.10	.68	1.26	13.31
58	2473	5520.06	.72	1.28	13.18
59	2438	5522.42	.73	1.30	13.37
60	2400	5524.63	.69	1.31	13.17
61	2370	5526.62	.59	1.33	13.17
62	2361	5527.27	.46	1.35	13.11
63	2361	5527.12	.46	1.36	13.00
64	2361	5526.72	.60	1.38	12.71
65	2349	5526.85	.90	1.40	12.34
66	2304	5529.42	1.08	1.41	12.33
67	2260	5532.16	1.17	1.42	12.37
68	2219	5534.68	1.22	1.44	12.38
[illegible]	2184	5536.61	1.31	1.46	12.2[illegible]
	2143	5539.01	1.43	1.47	12.[illegible]

LINE L-202

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2950	5494.70	.46	.33	18.18
1	2941	5495.23	.52	.35	18.20
2	2922	5496.20	.67	.36	18.11
3	2881	5498.69	.74	.38	18.10
4	2843	5501.01	.71	.40	18.02
5	2813	5502.77	.63	.41	17.88
6	2791	5504.22	.57	.43	17.85
7	2773	5505.35	.52	.44	17.81
8	2766	5505.68	.59	.46	17.73
9	2734	5507.38	.64	.48	17.51
10	2704	5509.08	.61	.50	17.29
11	2677	5510.68	.62	.51	17.21
12	2639	5512.69	.60	.53	16.82
13	2607	5514.63	.49	.55	16.62
14	2593	5515.51	.35	.56	16.45
15	2580	5516.19	.26	.58	16.27
16	2569	5516.78	.21	.60	16.09
17	2558	5517.45	.17	.62	15.99
18	2566	5516.91	.10	.63	15.86
19	2566	5516.86	.07	.65	15.77
20	2569	5516.60	.07	.67	15.67
21	2573	5516.34	.09	.68	15.65
22	2573	5516.32	.12	.70	15.67
23	2564	5516.89	.16	.72	15.68
24	2546	5517.97	.19	.74	15.65
25	2522	5519.41	.19	.76	15.63
26	2503	5520.56	.17	.77	15.56
27	2492	5521.37	.17	.79	15.62
28	2472	5521.68	.25	.81	14.77
28	2472	5521.67	.25	.81	14.76
29	2487	5521.68	.16	.82	15.60
30	2495	5521.24	.16	.84	15.65
31	2508	5520.42	.17	.86	15.61
32	2517	5519.89	.21	.88	15.66
33	2531	5519.03	.27	.90	15.73
34	2557	5517.84	.30	.91	16.19
35	2576	5516.20	.28	.93	15.70
36	2595	5515.09	.26	.95	15.71
37	2604	5514.53	.23	.96	15.68
38	2613	5513.87	.25	.98	15.59
39	2631	5512.67	.29	1.00	15.51
40	2657	5510.90	.29	1.01	15.37
41	2682	5509.28	.25	1.03	15.20
42	2694	5508.38	.18	1.05	14.98
43	2690	5508.71	.11	1.07	14.95
44	2689	5508.69	.09	1.08	14.82
45	2693	5508.24	.10	1.10	14.66
[illegible]	2708	5507.06	.12	1.12	14.40
	2722	5505.81	.16	1.14	14.05
	2717	5506.04	.17	1.16	13.96
	2700	5507.05	.18	1.17	13.89
	2683	5508.04	.19	1.19	13.8
	2670	5508.75	.22	1.20	13.7
52	2658	5509.32	.28	1.22	13.6
53	2640	5510.36	.35	1.24	13.5[illegible]
54	2622	5511.41	.41	1.26	13.54
55	2610	5511.98	.48	1.28	13.41
56	2602	5512.06	.64	1.30	13.15
57	2582	5512.88	.92	1.31	12.97
58	2534	5515.74	1.09	1.32	12.99
59	2481	5519.15	1.13	1.34	13.19
60	2434	5522.10	1.07	1.36	13.12
61	2396	5524.61	.95	1.37	13.13
62	2360	5526.86	.83	1.39	12.98
63	2356	5527.13	.64	1.41	12.80
64	2355	5527.14	.70	1.43	12.82
65	2346	5527.22	1.03	1.44	12.67
66	2291	5530.38	1.16	1.46	12.50
67	2243	5533.46	1.13	1.47	12.56
68	2215	5535.35	1.09	1.49	12.63
69	2194	5536.51	1.24	1.51	12.
[illegible]	2153	5538.89	1.28	1.52	12.

LINE L-206

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
1	2950	5494.92	.62	.38	18.56
2	2937	5495.51	.71	.39	18.36
3	2896	5497.92	.74	.41	18.27
4	2860	5500.16	.66	.43	18.16
5	2833	5501.91	.53	.45	18.08
6	2821	5502.69	.42	.46	17.99
7	2810	5503.32	.39	.48	17.91
8	2795	5504.27	.41	.50	17.90
9	2780	5504.95	.48	.52	17.72
10	2747	5506.89	.50	.53	17.62
11	2726	5508.23	.46	.55	17.58
12	2711	5509.10	.46	.57	17.53
13	2695	5509.88	.57	.58	17.37
14	2655	5511.94	.59	.60	16.94
15	2626	5513.62	.52	.63	16.73
16	2605	5515.07	.47	.64	16.85
17	2575	5516.69	.42	.65	16.52
18	2559	5517.37	.30	.67	16.09
19	2553	5517.57	.22	.69	15.80
20	2544	5518.11	.19	.71	15.70
21	2532	5518.78	.16	.73	15.61
22	2521	5519.40	.13	.74	15.48
23	2514	5519.80	.10	.76	15.40
24	2510	5519.99	.09	.78	15.33
25	2507	5520.34	.10	.80	15.45
26	2501	5520.75	.13	.82	15.55
27	2499	5520.91	.18	.83	15.60
28	2500	5520.88	.29	.85	15.75
28	2500	5520.95	.29	.85	15.82
29	2521	5519.59	.40	.87	15.82
30	2562	5517.25	.39	.88	15.99
31	2585	5515.84	.34	.90	15.93
32	2610	5514.32	.31	.92	15.94
33	2633	5512.89	.26	.94	15.85
34	2645	5512.12	.23	.95	15.80
35	2638	5512.62	.14	.97	15.77
36	2631	5513.04	.11	.98	15.73
37	2631	5512.99	.10	1.00	15.64
38	2635	5512.68	.12	1.02	15.57
39	2646	5512.04	.14	1.04	15.61
40	2660	5511.07	.15	1.06	15.49
41	2675	5509.96	.15	1.08	15.29
42	2686	5509.19	.14	1.09	15.22
43	2700	5508.24	.15	1.11	15.09
44	2718	5506.91	.15	1.13	14.86
45	2727	5506.18	.12	1.15	14.68
46	2734	5505.57	.12	1.16	14.49
47	2731	5505.70	.10	1.18	14.36
48	2733	5505.34	.13	1.20	14.16
49	2729	5505.37	.18	1.22	13.95
50	2722	5505.58	.28	1.23	13.82
51	2700	5506.77	.36	1.25	13.70
52	2673	5508.47	.42	1.27	13.76
53	2654	5509.65	.46	1.28	13.79
54	2642	5510.22	.55	1.30	13.68
55	2632	5510.47	.75	1.32	13.47
56	2604	5511.83	1.00	1.34	13.37

LINE L-210

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2954	5596.18	.53	.40	.11
1	2940	5495.74	.43	.42	18.47
2	2929	5496.14	.52	.44	18.31
3	2888	5498.68	.52	.46	18.24
4	2859	5500.45	.42	.47	18.12
5	2843	5501.67	.32	.49	18.22
6	2829	5502.49	.27	.51	18.08
7	2823	5502.64	.25	.52	17.85
8	2813	5503.40	.30	.54	18.02
9	2789	5504.78	.31	.56	17.92
10	2772	5505.79	.29	.57	17.81
11	2759	5506.57	.28	.59	17.79
12	2748	5507.12	.31	.61	17.66
13	2733	5507.79	.40	.63	17.45
14	2705	5509.25	.44	.64	17.21
15	2679	5510.78	.44	.66	17.11
16	2656	5512.24	.42	.67	17.05
17	2638	5513.22	.37	.69	16.89
18	2636	5513.24	.40	.71	16.78
19	2616	5514.17	.50	.73	16.57
20	2580	5516.13	.55	.75	16.28
21	2539	5518.41	.51	.76	15.99
22	2512	5520.07	.40	.78	15.82
23	2508	5520.25	.25	.80	15.62
24	2507	5520.33	.21	.82	15.55
25	2506	5520.55	.22	.83	15.71
26	2508	5520.67	.26	.85	16.00
27	2519	5520.07	.32	.87	16.09
28	2536	5518.89	.39	.89	16.04
28	2536	5518.87	.39	.89	16.02
29	2560	5517.34	.48	.90	16.06
30	2594	5515.25	.52	.92	16.08
31	2626	5513.14	.57	.94	16.00
32	2674	5510.20	.55	.95	15.99
33	2686	5509.59	.34	.97	15.92
34	2689	5509.45	.22	.99	15.80
35	2685	5509.73	.15	1.00	15.80
36	2677	5510.21	.10	1.02	15.66
37	2671	5510.52	.07	1.04	15.59
38	2672	5510.69	.06	1.06	15.77
39	2662	5511.11	.06	1.08	15.56
40	2661	5510.97	.06	1.09	15.32
41	2663	5510.84	.06	1.11	15.31
42	2670	5510.39	.07	1.13	15.27
43	2679	5509.74	.07	1.15	15.15
44	2688	5509.00	.07	1.16	15.02
45	2698	5508.30	.08	1.18	14.89
46	2707	5507.57	.08	1.20	14.69
47	2711	5507.16	.09	1.22	14.53
48	2709	5507.09	.12	1.23	14.35
49	2702	5507.35	.16	1.25	14.22
50	2689	5508.06	.21	1.27	14.12
51	2672	5509.06	.26	1.29	14.10
52	2660	5509.56	.33	1.31	13.93
53	2644	5510.33	.42	1.32	13.80
54	2629	5511.04	.54	1.34	13.65
55	2613	5511.75	.73	1.36	13.53
56	2582	5513.54	.92	1.38	13.56

LINE L-214

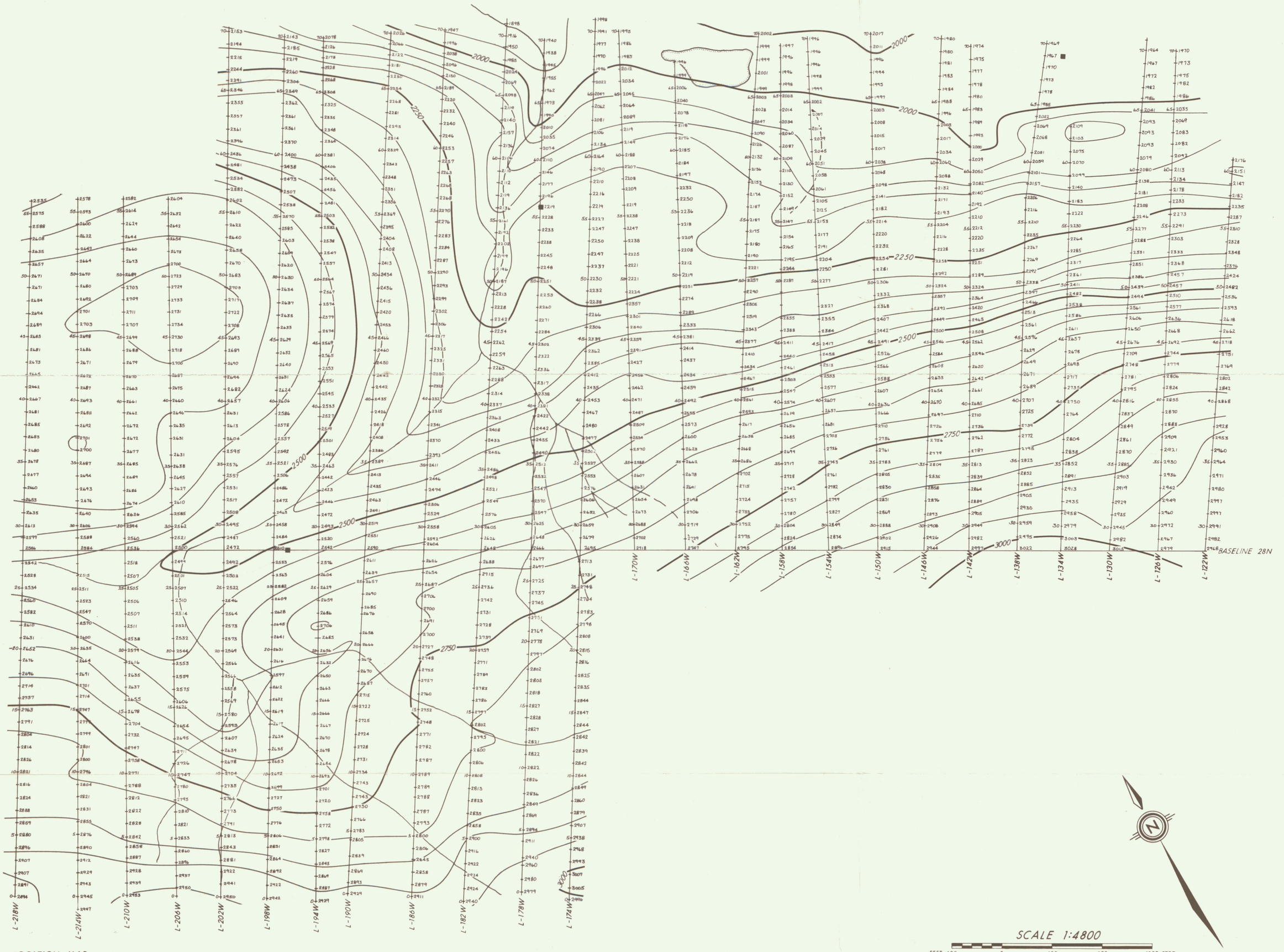
DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
-1	2947	5495.31	.44	.42	18.49
0	2945	5495.59	.32	.44	18.53
1	2943	5495.69	.30	.46	18.47
2	2929	5496.53	.31	.48	18.41
3	2912	5497.52	.31	.49	18.37
4	2890	5498.86	.29	.51	18.26
5	2876	5499.68	.27	.53	18.22
6	2855	5500.97	.28	.54	18.20
7	2831	5502.41	.26	.56	18.10
8	2821	5503.05	.22	.58	18.06
9	2804	5504.11	.20	.60	17.99
10	2796	5504.61	.16	.62	17.97
11	2799	5504.32	.15	.63	17.85
12	2801	5504.07	.21	.65	17.75
13	2799	5504.01	.27	.67	17.59
14	2779	5505.12	.40	.68	17.59
15	2747	5506.87	.47	.70	17.38
16	2714	5508.92	.45	.72	17.32
17	2701	5509.72	.41	.74	17.27
18	2690	5510.24	.48	.75	17.20
19	2664	5511.68	.55	.77	17.08
20	2633	5513.45	.58	.79	16.90
21	2600	5515.27	.56	.80	16.65
22	2569	5517.16	.50	.82	16.52
23	2546	5518.41	.43	.84	16.27
24	2522	5519.68	.42	.85	16.03
25	2511	5520.20	.41	.87	15.83
26	2515	5520.04	.47	.89	15.96
27	2549	5518.27	.42	.90	16.25
28	2584	5516.25	.34	.92	16.26
28	2584	5516.20	.34	.92	16.21
28	2584	5516.16	.34	.92	16.18
29	2588	5515.93	.31	.94	16.15
30	2606	5514.75	.40	.96	16.17
31	2640	5512.49	.45	.67	16.38
32	2676	5510.29	.41	.99	16.06
33	2693	5509.31	.29	1.01	15.98
34	2694	5509.30	.18	1.03	15.88
35	2687	5509.66	.13	1.04	15.74
36	2700	5508.83	.10	1.06	15.69
37	2701	5508.73	.08	1.08	15.64
38	2692	5509.28	.06	1.10	15.57
39	2688	5509.51	.05	1.11	15.55
40	2693	5509.02	.05	1.13	15.36
41	2687	5509.38	.06	1.15	15.30
42	2672	5510.15	.07	1.17	15.17
43	2671	5510.21	.08	1.18	15.13
44	2686	5509.16	.08	1.20	15.01
45	2698	5508.18	.08	1.22	14.77
46	2703	5507.76	.08	1.24	14.61
47	2701	5507.75	.10	1.25	14.50
48	2692	5508.19	.12	1.27	14.38
49	2680	5508.84	.14	1.29	14.26
50	2670	5509.31	.18	1.31	14.16
51	2664	5509.45	.26	1.32	14.00
52	2647	5510.35	.36	1.34	13.90
53	2622	5511.80	.43	1.36	13.85
54	2600	5512.96	.48	1.38	13.67
55	2593	5513.23	.59	1.39	13.63
56	2578	5513.77	.83	1.41	13.46

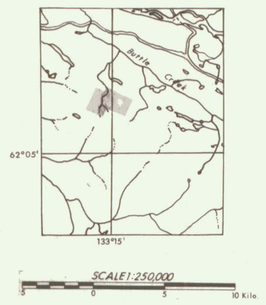
LINE L-218

DENSITY= 2.5

ST	ELEV	OBS G	TERR	LATT	GRAV
0	2894	5498.34	.46	.49	18.19
1	2891	5498.79	.28	.51	18.29
2	2907	5497.82	.23	.52	18.25
3	2907	5497.92	.20	.54	18.25
4	2896	5498.55	.20	.56	18.19
5	2880	5499.46	.21	.57	18.14
6	2859	5500.78	.21	.59	18.10
7	2838	5502.08	.19	.61	18.08
8	2824	5502.87	.16	.62	17.96
9	2816	5503.35	.14	.64	17.89
10	2821	5503.34	.13	.66	18.17
11	2826	5502.60	.17	.67	17.78
12	2814	5503.31	.20	.69	17.73
13	2804	5503.85	.26	.71	17.68
14	2791	5504.36	.36	.72	17.50
15	2763	5506.09	.41	.74	17.48
16	2737	5507.62	.42	.76	17.39
17	2714	5509.03	.42	.78	17.37
18	2696	5510.02	.43	.79	17.23
19	2676	5511.16	.44	.81	17.12
20	2652	5512.58	.43	.83	17.03
21	2631	5513.68	.41	.85	16.79
22	2610	5514.88	.40	.86	16.66
23	2582	5516.40	.39	.88	16.38
24	2560	5517.76	.37	.90	16.34
25	2534	5519.08	.39	.92	16.04
26	2528	5519.21	.39	.93	15.78
27	2542	5518.43	.43	.95	15.93
28	2586	5516.03	.33	.97	16.16
28	2586	5515.98	.33	.97	16.11
29	2599	5515.40	.23	.98	16.18
30	2613	5514.46	.24	1.00	16.12
31	2635	5513.06	.24	1.02	16.05
32	2653	5512.00	.22	1.04	16.09
33	2666	5511.10	.18	1.05	15.96
34	2677	5510.43	.14	1.07	15.92
35	2678	5510.25	.09	1.09	15.72
36	2680	5510.11	.07	1.10	15.67
37	2683	5509.85	.06	1.12	15.53
38	2685	5509.67	.06	1.14	15.47
39	2681	5509.92	.06	1.16	15.44
40	2667	5510.76	.06	1.17	15.41
41	2662	5510.95	.06	1.19	15.26
42	2665	5510.64	.05	1.21	15.17
43	2673	5510.02	.05	1.22	15.02
44	2681	5509.48	.05	1.24	14.92
45	2685	5509.04	.06	1.26	14.74
46	2689	5508.71	.07	1.28	14.66
47	2694	5508.22	.11	1.30	14.46
48	2684	5508.65	.14	1.31	14.34
49	2671	5509.42	.16	1.33	14.29
50	2671	5509.24	.24	1.34	14.15
51	2657	5509.80	.34	1.36	13.95
52	2635	5511.13	.45	1.38	14.00
53	2608	5512.72	.51	1.40	13.94
54	2588	5513.80	.58	1.41	13.82
55	2575	5514.31	.77	1.43	13.68
56	2535	5516.70	.91	1.45	13.74



LOCATION MAP



SCALE 1:250,000
5 0 5 10 Kilo.

LEGEND

LOCATED CLAIM POST ■

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY
SURFACE ELEVATION MAP
CONTOUR INTERVAL 50 FEET

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO: 1107	FIGURE NO.: 3
N.T.S.: 105 K/3	DRAWN BY: H. Meyers

L-218W L-214W L-210W L-206W L-202W L-198W L-194W L-190W L-186W L-182W L-178W L-174W

L-170W L-166W L-162W L-158W L-154W L-150W L-146W L-142W L-138W L-134W L-130W L-126W L-122W

BASELINE 28N

LOCATION MAP

SCALE 1:250,000

5 0 5 10 Kilo.

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY
BOUGUER GRAVITY SURVEY
DENSITY 2.75 GRAMS PER CUBIC CENTIMETRE
CONTOUR INTERVAL 0.2 MILLIGALS

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

Dave Bingham

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO.: 1107	FIGURE NO.: 4A
N.T.S.: 105 K/3	DRAWN BY: H. Meyers

L-218W L-214W L-210W L-206W L-202W L-198W L-194W L-190W L-186W L-182W L-178W L-174W

L-170W L-166W L-162W L-158W L-154W L-150W L-146W L-142W L-138W L-134W L-130W L-126W L-122W

BASELINE 28N

LOCATION MAP

SCALE 1:250,000

5 0 5 10 Kilo.

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

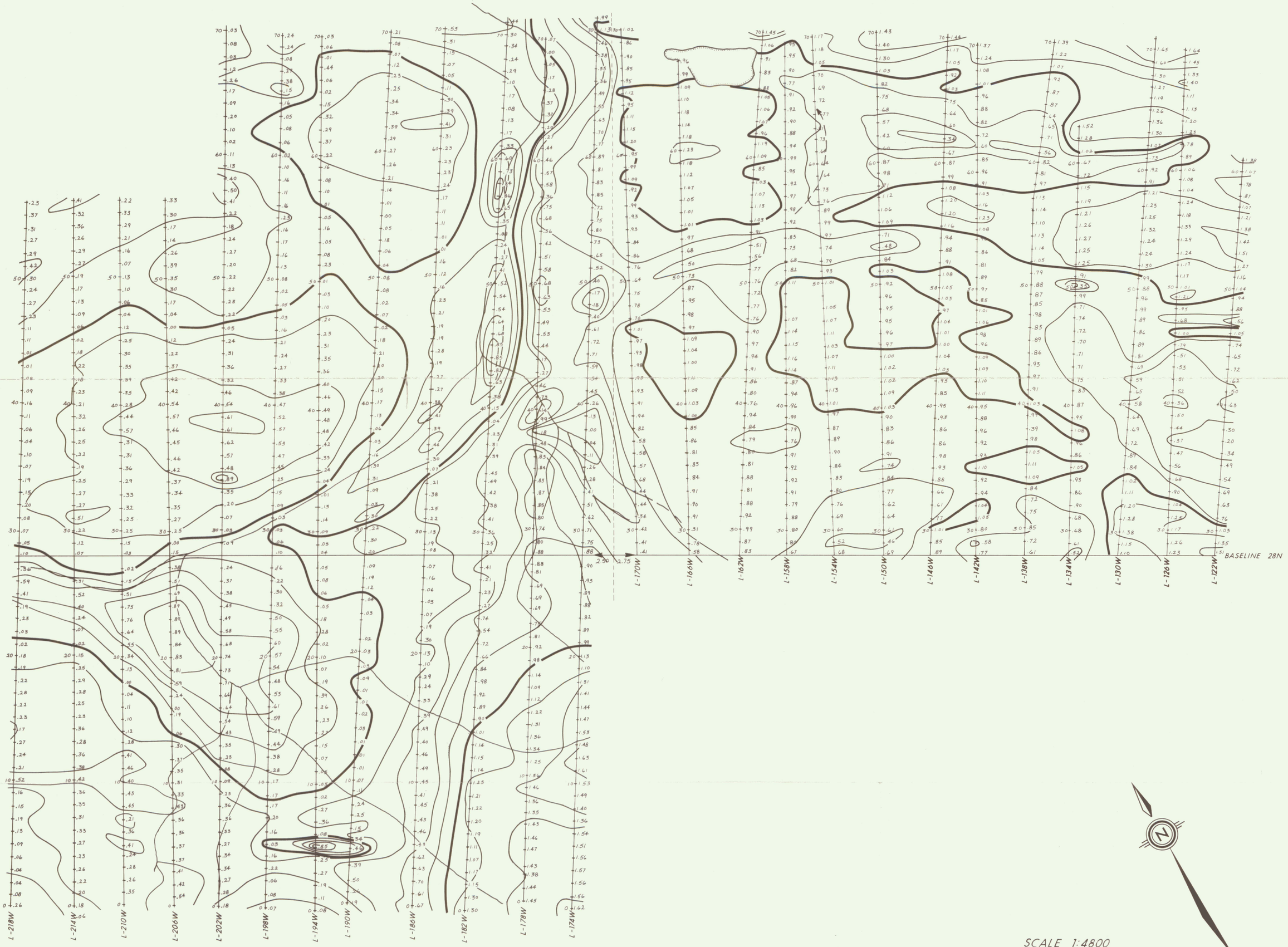
SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY
BOUGUER GRAVITY SURVEY
DENSITY 2.50 GRAMS PER CUBIC CENTIMETRE
CONTOUR INTERVAL 0.2 MILLIGALS

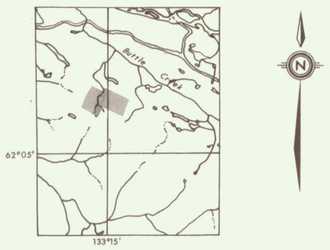
TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO: 1107	FIGURE NO.: 4 B
N.T.S.: 105 K/3	DRAWN BY: M. BARCLAY



LOCATION MAP



SCALE 1:250,000

5 0 5 10 Kilo.

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY
RESIDUAL GRAVITY SURVEY
DENSITY 2.50 & 2.75 GRAMS PER CUBIC CENTIMETER

CONTOUR INTERVAL 0.2 MILLIGALS

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

Dave Bingham

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO: 1107	FIGURE NO.: 5A
N.T.S.: 105 K/3	DRAWN BY: M. Barclay

LOCATION MAP

SCALE 1:250,000

5 0 5 10 Kilo.

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY
SMOOTHED RESIDUAL GRAVITY SURVEY
DENSITY 2.50 & 2.75 GRAMS PER CUBIC CENTIMETER

CONTOUR INTERVAL 0.1 MILLIGALS

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO: 1107	FIGURE NO: 5 B
N.T.S.: 105 K/3	DRAWN BY: M. Barclay

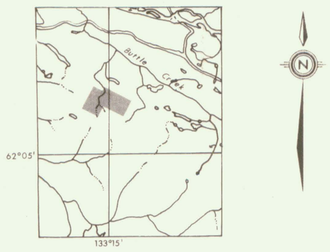
LEGEND

ANOMALIES
STRUCTURAL HIGHS
FAULTS : POSSIBLE
PROBABLE
GRAVITY LOWS
RECOMMENDED DRILL TARGETS ⊠
DIAMOND DRILL HOLE ⊗

SCALE 1:4800

FEET 400 0 400 800 1200 FEET

LOCATION MAP



SCALE 1:250,000
5 0 5 10 Kilo.

SUNEXCO ENERGY CORPORATION

PUG & KEY CLAIMS, YUKON TERRITORY

INTERPRETATION MAP

TO ACCOMPANY REPORT BY: DAVID C. BINGHAM

CAN-LAKE EXPLORATIONS LTD. CALGARY ALBERTA

SCALE: 1 : 4800	DATE: SEPT. 1980
PROJECT NO: 1107	FIGURE NO: 6
N.T.S.: 105 K/3	DRAWN BY: H. Meyers