Office of the Supervising Mining Recorder
FEB 16 1979
WHITEHORSE
Yukon Territory

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This report has been examined by the Geological Evaluation Unit and recommended to the Commissioner for acceptance as representation work in the amount of $ 32,000.00

28/2/79

Registered Professional Engineer or Registered Mining Engineer

Considered as representation work under Section 53 (4) Yukon Quartz Mining Act.

B. R. BAXTER
Supervising Mining Recorder

for Commissioner of Yukon Territory

Office of The Supervising Mining Recorder
FEB 16 1979
WHITEHORSE
Yukon Territory

1. INTRODUCTION

The ZAP claim block consists of 292 full sized mineral claims located on the west side of the RACKLA RIVER about six kilometers (4 miles) northeast of KATHLEEN LAKES.

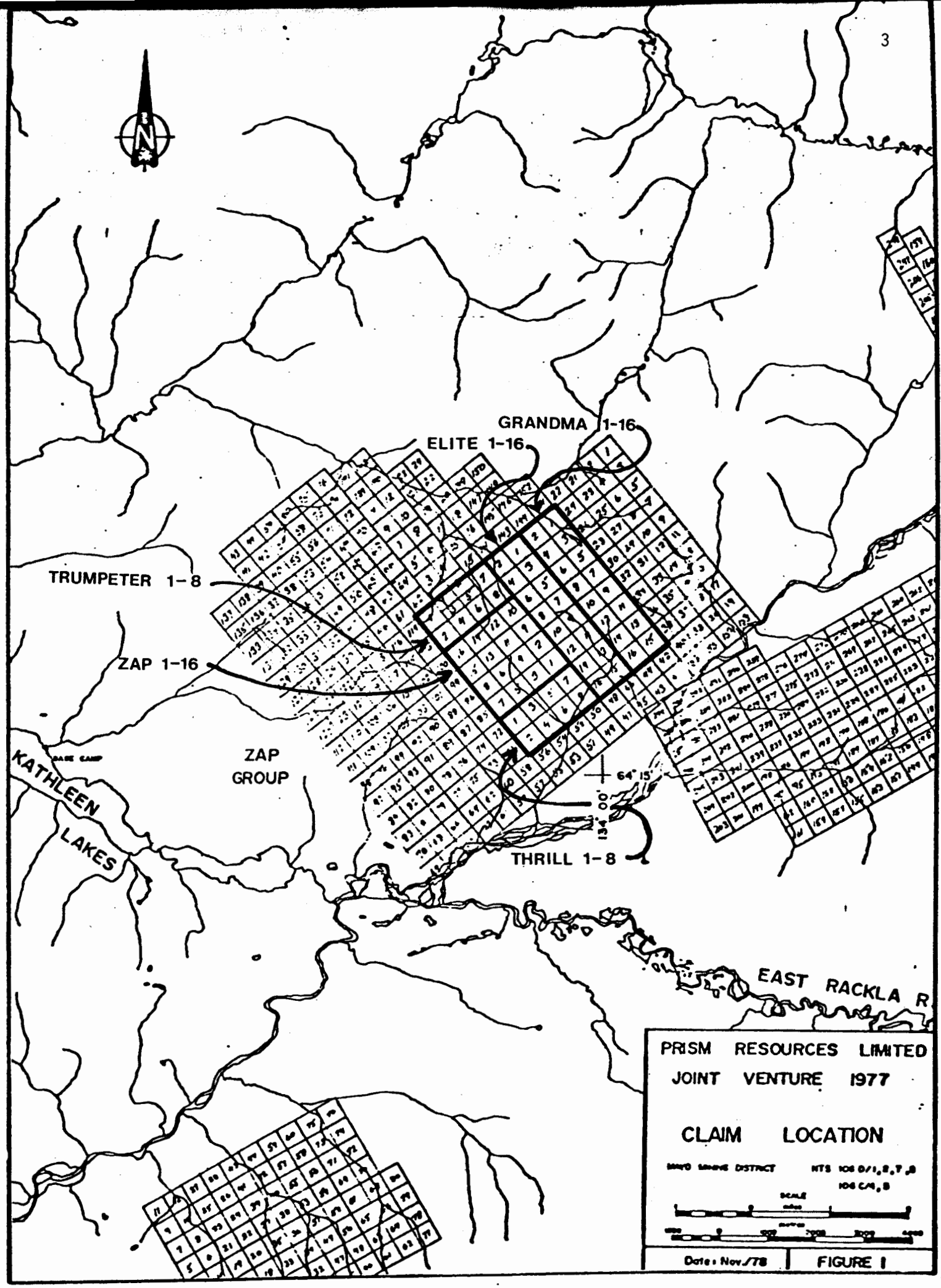
In 1977 the ZAP 1-16 claims were staked to cover lead, zinc, silver mineralization discovered late that summer. Another 48 claims were staked early in the winter to cover high silver values in the streams and soils of the ZAP area. During the early summer of 1978 more mineralization was discovered north of the existing block so 72 PIKA claims were staked. Finally, to cover more anomalies in streams and further zinc lead mineralization, 152 CAROL claims were staked. This report covers the work done on the ZAP, GRANDMA, ELITE, THRILL and TRUMPETER claims, totalling 64 claims.

Work in 1977 consisted of soil sampling, chip sampling, and geological mapping of the main mineralized areas. In 1978, further chip sampling in hand trenches, soil sampling and geological mapping were completed. A 1000 M x 700 M gravity survey was completed by Kenting Exploration along with a 1000 M x 900 M topographic control survey. D.W. Coates Diamond Drilling Company drilled a net 1585 feet of BQ core in 1730 feet of drilling (145 feet of casing) in 5 holes on the central ZAP claim block.

LOCATION AND ACCESS

Figure 1 shows the location of the ZAP group of claims. The eastern border is the RACKLA RIVER and the western boundary is PAN ACHERON'S claim block 7 kilometers (4 miles) northeast of the camp on KATHLEEN LAKES. The claim block is situated between the elevations of 760 meters (2500 feet) and 1700 meters (5500 feet). The block is 130 air kilometers (80 air miles) northeast of MAYO, Y.T., NTS Map Reference 106D-1,106 D-8 and 106 C-5; coordinates of the discovery showings and main work are latitude 64°17' N, longitude 134°02'W.

Access to the property is by a helicopter from a float plane supported camp on KATHLEEN LAKES.


GRANDMA 1-16
ELITE 1-16
TRUMPETER 1-8
ZAP 1-16
ZAP
GROUP
KATHLEEN
LAKES
64° 15'
134°
THRILL 1-8
EAST RACKLA R
PRISM RESOURCES LIMITED
JOINT VENTURE 1977
CLAIM LOCATION
Date: Nov./78
FIGURE 1

CLAIM INFORMATION

The ZAP group of claims lies within the MAYO MINING DISTRICT. All claims are held in the name of PRISM RESOURCES LIMITED. The following table list pertinent information.

TABLE 1

CLAIM	DATE STAKED	STAKER	RECORD NO.	EXPIRY DATE
ZAP 1-8	Sept.9/77	R. Thurston	YA16383-90	Sept. 23/83
" 9-16	"	J. Montgomery	YA16391-98	"
ELITE 1-8	Oct. 24/77	J. Grette	YA17371-78	Nov. 15/83
9-16	"	D. Runkle	YA17379-86	"
THRILL 1-8	"	A. MacDonald	YA17363-70	"
TRUMPETER 1-8	"	R. Forshaw	YA17387-94	"
GRANDMA 1-8	"	E. Graham	YA17347-54	"
9-16	"	D. Brown	YA17355-62	"

4. LOCAL GEOLOGY

The geology of ZAP was mapped on three scales: a 1:1000 scale map was done over the main portion of the grid (Figure 2), BL 10,000 N to BL 9000 N, grid lines 9500 E to 10,400 E; a 1:5000 scale detailed geology map of the ZAP 1-16, THRILL 1-8, TRUMPETER 1-8, ELITE 1-16 and GRANDMA 1-16 (Figure 3); finally, a 1:50,000 scale regional map is being compiled of all the area immediately surrounding the ZAP group, the CAROL claims (Figure 3)

There are 4 main rock units in the ZAP group, each with minor rock divisions. The youngest rock is a well bedded, massive, medium grained ortho-quartzite. On the surface there is approximately 50 m. exposed and there could be up to 500 m. of total thickness in the unit. Within the quartzite are minor beds, up to 5 m. in combined thickness, of orange weathering, laminated, well bedded dolomite. Also, a brown weathering slightly limy shale occurs stratigraphically within the quartzite with an estimated thickness of up to 50 meters (Figure 3).

On the ZAP property a fault separates the quartzite package from the next major unit, a massive, well bedded, medium grained dolomite. Elsewhere in the area away from the ZAP property the quartzite has a conformable contact with the same grey dolomite.

The dolomite weathers in four colors. The

uppermost section of dolomite is an orange weathering variety approximately 50 m.?? thick. Below that is a contact grading into boring grey weathering dolomite that covers most of the south-western portion of the ZAP group. Within this unit is a thin section approximately 10 meters thick of algal dolomite. Dr. Dirk Tempelman-Kluit of the Geological Survey of Canada, an expert on the geology of the Yukon, believes, from the samples shown to him, that the rocks are of Ordovician-Silurian age. Under the grey dolomite is another gradational contact with a black weathering, well bedded, well laminated dolomite, fracture-filled crystal dolomite and load breccias of crystal dolomite. This dolomite occupies most of the N.W. portion of the claim group. The bottom of the dolomite package is a well bedded, well laminated, platey orange weathering variety of the dolomite. It can be found in the N.E. corner of the claim block, traced along the PIKA and CAROL claims.

Under the orange dolomites is either a fault or an unconformable contact with a very thinly bedded, grey fresh surface, brown weathering shale, with greyish brown, silvery grey varicolored hues on the bedding planes. There is no estimate of thickness of these shales. They are found N.E. of the small lake on the N.E. edge of the GRANDMA claims. A greenstone dyke has been injected into the area to the west of the shales subjecting them to some heat and possible deformation.

Within the upper orange dolomites, directly below or faulted against the quartzite is a mineralized unit called the carbonaceous unit. It is a black, barite-rich, chert-rich, often brecciated unit with tetrahedrite and galena within the rock in various locations. The unit is bedded at times and brecciated in other areas. There may be more than one of these units in various stratigraphic positions within the upper portions of the dolomite package. A series of faults through the main showings could have altered their original positions to move them to their present positions. In the drill core of hole #3, the carbonaceous unit shows up in its unweathered form. It is black, fine-grained and interbedded with a green-grey siltstone. The siltstone does not appear on the surface unless it is represented in a weathered form by the black carbonaceous unit with the quartzite. More likely, what has happened to it is the fault between the quartzite and the black carbonaceous unit has cross-cut the siltstone and it is not seen on the surface. On the surface there is visible galena and tetrahedrite, but in the core no mineralization is seen in the siltstone and carbonaceous shale although the rock geochemistry shows up to 0.5 oz/t silver.

Mineralization occurs in four main forms; (1) in the carbonaceous unit, mainly tetrahedrite, barite and galena; (2) in breccias within the

dolomite on the western portions of the grid, predominantly sphalerite and galena with some high silver values; 3) in the shales to the east of the GRANDMA claims, mainly sphalerite with minor galena; 4) and in veins on GRANDMA 1 and 2 claims, predominately solid galena with good silver values (Fig. 3).

In the carbonaceous unit trenches have been dug to expose more bedrock. T-9 and T-10 are both in the unit, most of T-1 never hit bedrock, but parts of it touched the carbonaceous unit. Samples taken from float within trench T-9 assayed up to 102 oz/ton silver. The mineralization in the carbonaceous unit is mainly galena, with some visible tetrahedrite and copper staining. Tetrahedrite mineralization also occurs along fractures and around crystals of barite. The main portion of the mineralization on the surface appears to be restricted to the carbonaceous unit although minor mineralization occurs in the host dolomite. This mineralization in the black carbonaceous unit is probably very closely related to the fault through the main showing that separates the quartzite from the dolomite. The fault may have been the avenue through which the mineralized fluids passed into the porous carbonaceous unit. This fault will be dealt with later in the report.

Mineralization also occurs in a crystal dolomite breccia within the main host grey and orange

dolomites. Crystals of sphalerite are common, along with fracture-filled blebs of sphalerite. Galena is quite common and can be found in most areas of the mineralized breccias.

The third main area of mineralization is in the shales east of the lake and north of the GRANDMA claims. The sphalerite occurs with calcite veining, with galena and in some cases as open space filling of the shales. The secondary mineralization coats nodules of carbonate (or stromatolites??) in galena and sphalerite. Sphalerite in some cases completely infills the carbonate nodules making them almost pure sphalerite. The shales are generally high in zinc geochemically; the intrusion of the greenstone dyke may have provided a heat source to release and reconcentrate the zinc and lead. The dykes in the area are mapped as Cretaceous by Green in G.S.C. memoir 364.

The fourth area of mineralization is on the GRANDMA claims. Mineralization occurs in veins from 0.15 m. wide to very thin veinlets. The mineralization is found as massive galena and sphalerite with high silver values associated with the veins.

A possible source of this mineralization was proposed by S. Blusson, (G.S.C.) in 1977. A major E-W trending fault named the Dawson thrust fault of approximately Tertiary age has faulted Devonian-Mississippian against Hadrynian rock. Mineralization within the general area occurs along either side of

this fault trace. A northern offshoot or branch of this mineral avenue could have disrupted the rock on ZAP and allowed the porous rock of the breccias and carbonaceous units to be mineralized.

This simple theory becomes more complex when the faulting in the cirque on ZAP is considered. The major fault separating the quartzite and the dolomite trends about 140°, but there is no surfacial indication of dip.

With a northeast dipping fault, mineralization could be found under the quartzite. With a southwest dipping fault, mineralization is restricted to the upper portions of the dolomite. The cirque fault could have some right lateral strike slip, therefore, some mineralization could be found in rocks either north or south from the main showings. A N.E. - S.W. fault below all mineralization forms the southern boundary of the mineralized block, separating the dolomites and quartzites from a fossiliferous dolomite. This fault may have occurred after the mineralization, thus a further mineralized zone could be somewhere along its trend.

Within the main showings or discovery zone, a fault, or a series of faults, between quartzite and the carbonaceous unit trends 100° and is near vertical. This fault could be representative of a horsetail of the main fault that runs at 140° through the cirque. The horsetail faulting could be the

reason for the various positions of the carbonaceous unit within the discovery zone.

The dolomites of ZAP are relatively undeformed. The strike and dip of the unit is usually around 060°/ 30° S throughout the area.

Brecciation is very common in the drill core of all the holes on ZAP. The fragments are coarse angular fragments with a matrix of white carbonate infilling between the fragments. Pyrite in crystalline form is common in the matrix.

The quartzites show a fractured anticlinal system that doesn't continue into the dolomites across the horsetailed faults. The fold axis of the anticline is approximately 100°. At the head of the cirque is a fault that runs about 30°?? that separates the anticline from the head of the cirque. At the top are vertically dipping, 130° striking quartzites that have been faulted upright. To the west of the vertical block about 50 m. is a block that forms the nose of an anticline. It may have been part of the present anticline, but now it appears to be faulted out of place.

A rock talus slope approximately 200 m. by 300 m. fills the bottom of the cirque. Trenches dug in the talus show metal content generally increases with depth. Being very optimistic, this demonstrates that mineralization may be found beneath the talus pile. The rock slide covers the fault between the quartzite and the dolomite. This fault, as mentioned

previously, has a good chance of carrying mineralization. The geochemistry indicates a highly anomalous area over the fault in the cirque. The gravity survey shows a coincident anomaly with the geochemistry and traces of mineralization along the fault demonstrate that there is mineral present.

5. GEOCHEMISTRY

5-1 INTRODUCTION

Two grids were completed on the ZAP claims this summer (Fig. 3). One grid covers the main showing area on ZAP claims 2, 4, 9, 10, 11 and 12. It is a 1500 m. by 700 m. grid with a 50 m. line spacing and 25 m. sample spacing, a total of 1100 samples. The results of this grid are on Fig. 4A , 4B and 4C

Four sample lines were extended from base line 9000 N to the creek below the main showings. A total of 5 lines were run, 90 samples were taken and analyzed for lead, zinc and silver.

The other grid is a smaller one on the GRANDMA 1 and 2 claims (ZAP GRID B). It is a 500 m. x 350 m. grid with 25 m. line spacing and 25 m. sample spacing for a total of 315 samples. It was completed to search for lead-silver veins similar to those already found outcropping in the area.

5-2 RESULTS

The results of the main grid on ZAP are on Fig. 4A , 4B and 4C geochemical plans for lead, zinc and silver respectively.

The lead geochemical plan (Fig. 4A) shows a broad area of anomalous values extending from approximately Line 10,400 E to Line 9850 E and station 9200 N to 9900 N. Anomalous values in zinc and silver were detected over the same area of the grid. The highest values in the grid were 18,100 ppm Lead (1.81% Pb), 10,700 ppm Zinc (1.07% Zn) and 60.0 ppm silver (1.75 oz/t Ag).

The results of ZAP Grid-B are on Fig. 5A . 5B and 5C geochemical plans for lead, zinc and silver respectively. The lead, zinc and silver values show an anomalous area around Line 20,200 E and station 19,900 N. The highest values in that area were 14,000 ppm lead (1.4% Pb), 10,700 ppm zinc (1.07% Zn) and 26 ppm silver (0.75 oz/t Ag).

5-3 INTERPRETATION

Statistical values for contour intervals were determined using cumulative percent curves. The curves were the result of a computer analysis of the ZAP data.

Statistical lead contours were determined to be 2600 ppm, 700 ppm and 200 ppm. Above 2600 ppm 5% of the sample population can be found. Between 2600 and 700 ppm 11% of the samples can be found. From

700 ppm to 200 ppm lie 34% of the samples; the remaining 50% are below the 200 ppm level.

The zinc contours determined statistically are 4500 ppm, 300 ppm and 200 ppm. Above 4500 ppm 3% of the population appears, and these values are considered very anomalous. Between 4500 and 300 ppm 60% of the population is located. From 300 to 200 ppm 10% of the samples occur and below 200 ppm the remaining 27% appear.

The silver contours are 5.0, 3.0 and 2.0 ppm. Above 5.0 ppm, 12% of the samples occur. Between 5.0 and 3.0, 16% of the population is recorded. Between 3.0 ppm and 2.0 ppm 24% of the samples occur and below 2.0 ppm the remainder of the samples occur (48%).

The various contour intervals attempt to represent 4 populations of samples. Values above the highest contours (2600 ppm Pb, 4500 ppm Zn and 5.0 ppm Ag) represent the very anomalous samples. Values between the highest and the next highest contours represent the second population as those between the lowest and second lowest contour interval (200 ppm Pb, 200 ppm Zn and 2.0 ppm Ag) are samples that are considered background values on this grid. The lower values mean little or no metal content in the surface samples.

However, some of the contour intervals are unrealistic. The three contour intervals for lead were workable, but the lowest intervals for zinc (200 ppm) and silver (2 ppm) were not used. These values are too close to the preceeding contour interval, so rather

than contouring values lower than background for the grid and complicating the geochemical plan, they were disregarded.

Since the interval between 4500 ppm and 200 ppm is very broad, two values were selected to help in interpreting the data, 2000 ppm and 1000 ppm. With the silver contour intervals, a value of 10 ppm was chosen to illustrate the higher regions of the grid, higher areas than the statistical interval of 5 ppm.

No statistics were done for the ZAP Grid B. Contour intervals were selected by inspection of the data. The results show high metal content near, but not on, a known Pb, Zn, Ag vein, possibly representing a vein under the surface or a continuation of the known vein.

A large anomaly 500 x 100 meters trends approximately 310^{o}. This anomaly may also represent continuation of the known vein or just transportation of metals along the creek. Mapping and trenching will be subject to interpretation of this anomaly.

6. GEOPHYSICS

A complete report of the gravity survey accompanies this report. (Appendix A)

Further to the interpretation section, conversations with Dr. J. Wyder of E & B Explorations helped in clarification of the gravity results. He suggested the two gravity highs located around Line 9900 E, Station 9500 N and Line 10,100 E, Station 9800 N may be connected by some structure. Mineralization can be found along this approximate trend and further drilling will be needed to evaluate this theory.

7. SUMMARY AND CONCLUSIONS

The mapping, geochemistry and drilling information accumulated during the 1978 field season enable the summary and conclusions to be drawn as follows:

1) Mapping - In the course of regional exploration of the ground surrounding the 1977 borders of the ZAP claim group, four new mineralized showings were discovered. These were subsequently staked (PIKA and CAROL groups). The four new showings are 1) South of the main ZAP grid; a small lead-zinc mineralized breccia 2) East of the GRANDMA claims; lead-zinc in shales 3) On Grandma number 1 and 2 claims; lead-zinc-silver veins, and 4) Northwest of the ZAP group; lead, zinc and silver in a creek bed. The northern PIKA and CAROL claims are covered with overburden and vegetation; the only rock exposures are in the creeks. More geochemical grids are planned and a program of mapping is planned in conjunction with these grids (Fig. 6).

2) Geochemistry - In the geochemistry section (Section 5), a large lead-zinc-silver anomaly was outlined on the main ZAP GRID, as well as on the ZAP B Grid. The anomaly on the main grid will be further tested with more drilling in the 1979 season. The anomaly on the ZAP B Grid will be tested by trenching, followed by drilling if warranted. This area will be expanded to determine the exact boundaries of the anomaly. The extent of other mineralized areas discovered outside the central claim block will be tested

by geochemical surveys.

3) Drilling - The first three holes on ZAP did not encounter significant mineralization. Poor drilling conditions resulted in holes 1, 4 and 5 being abandoned before their targets were intersected. Further drilling is planned on the ZAP grid with a larger capacity drill so better results are expected.

A combination of geological, geochemical and geophysical information has resulted in eight drill targets planned for the ZAP claims. Four holes are planned in the cirque to test the fault for mineralization and four holes are planned to test the mineralized gravity high in the area of DDH 78-4.

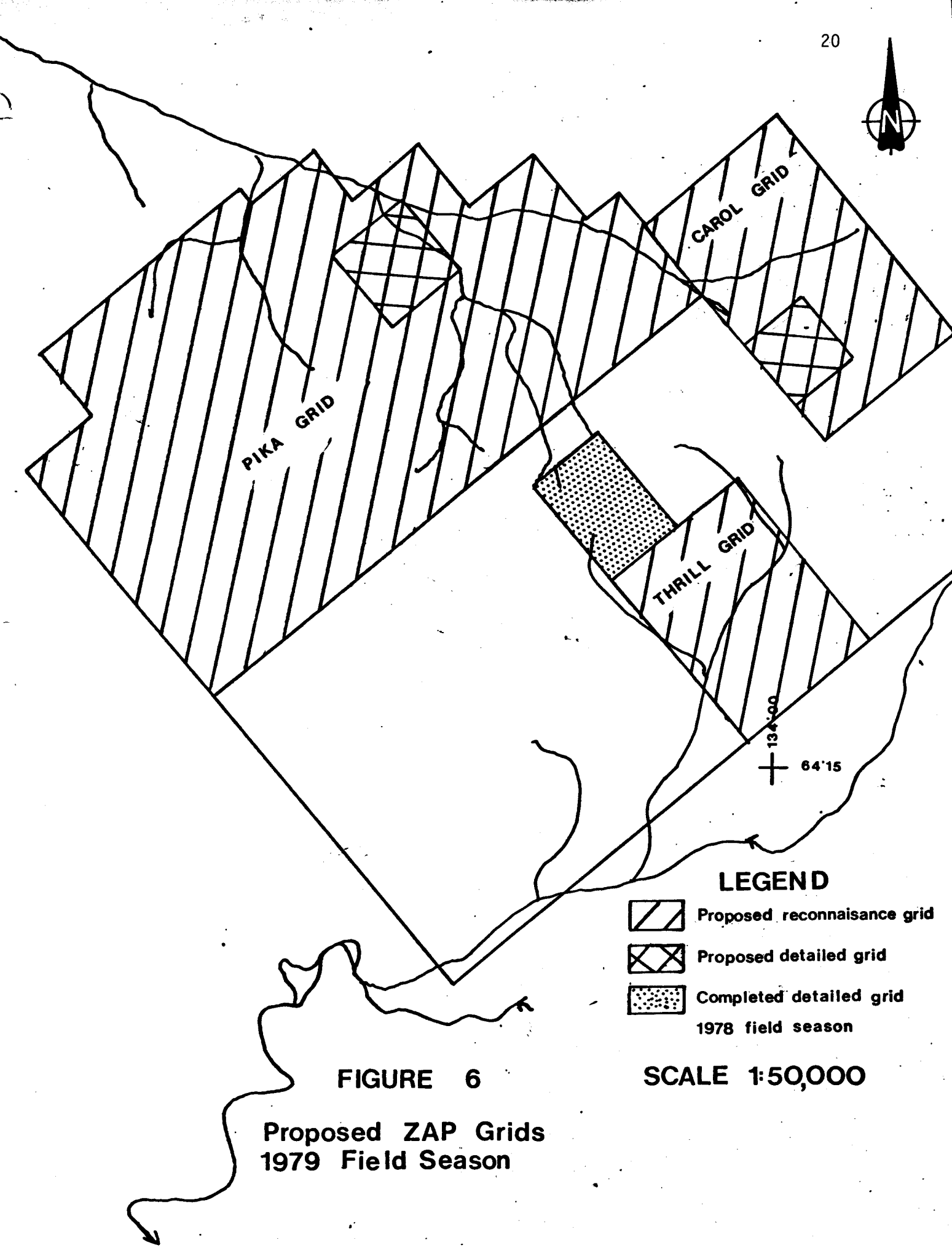


FIGURE 6

Proposed ZAP Grids
1979 Field Season

8. RECOMMENDATIONS

1) Reconnaissance level geochemical sampling should be done over the important areas of PIKA, CAROL and THRILL claims. Approximately 1500 samples or 125 line kilometers should be done on the PIKA claims to test the area north of the present grid. 37 line kilometers (530 samples) should be done on the north-eastern CAROL claims to test the shales for more lead zinc mineralization. Fifty line kilometers (500 samples) should be taken below the main grid on ZAP, on the THRILL claims to test for continuation of mineralization (Fig. 6).

2) A bulldozer should be used to test 3 areas by trenching on the ZAP group. Two of these areas are on the main grid, one on the mineralized seep and the other to reach bedrock where the sample assaying 102 oz/t Ag was found (Trench T-9A). The third trenching area would be on the GRANDMA claims where the geo-chemical anomaly and known Pb, Zn, Ag veins are located. A hand-blasted trench will be required on the mineralized shales if the slope is too steep for the bulldozer.

3) 4000 feet of diamond drilling should be done to further test two areas of extreme interest on the ZAP claim block. 4 holes of approximately 500 feet each should be drilled in the cirque in the vicinity of the gravity high, geochemical high and mineralized fault structure.

The other four holes of approximately 500

feet each should be drilled in the area of the gravity high previously tested (DDH 78-4). Encouraging mineralization found in the hole demonstrates that this area requires further drilling to evaluate.

APPENDIX A

REPORT ON

A GRAVITY SURVEY

for

PRISM RESOURCES LIMITED

on

ZAP CLAIMS, YUKON TERRITORY

Latitude: 64° 16' N Longitude: 134° 2' W

June 14 to July 10, 1978

Dennis P. Dorval, P. Geoph.

Trevor R.B. Dundas, P. Geoph.

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EXPLORATION SERVICES LIMITED

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P.E.M. Specifications Appendix B

Principle Gravity Data Appendix C

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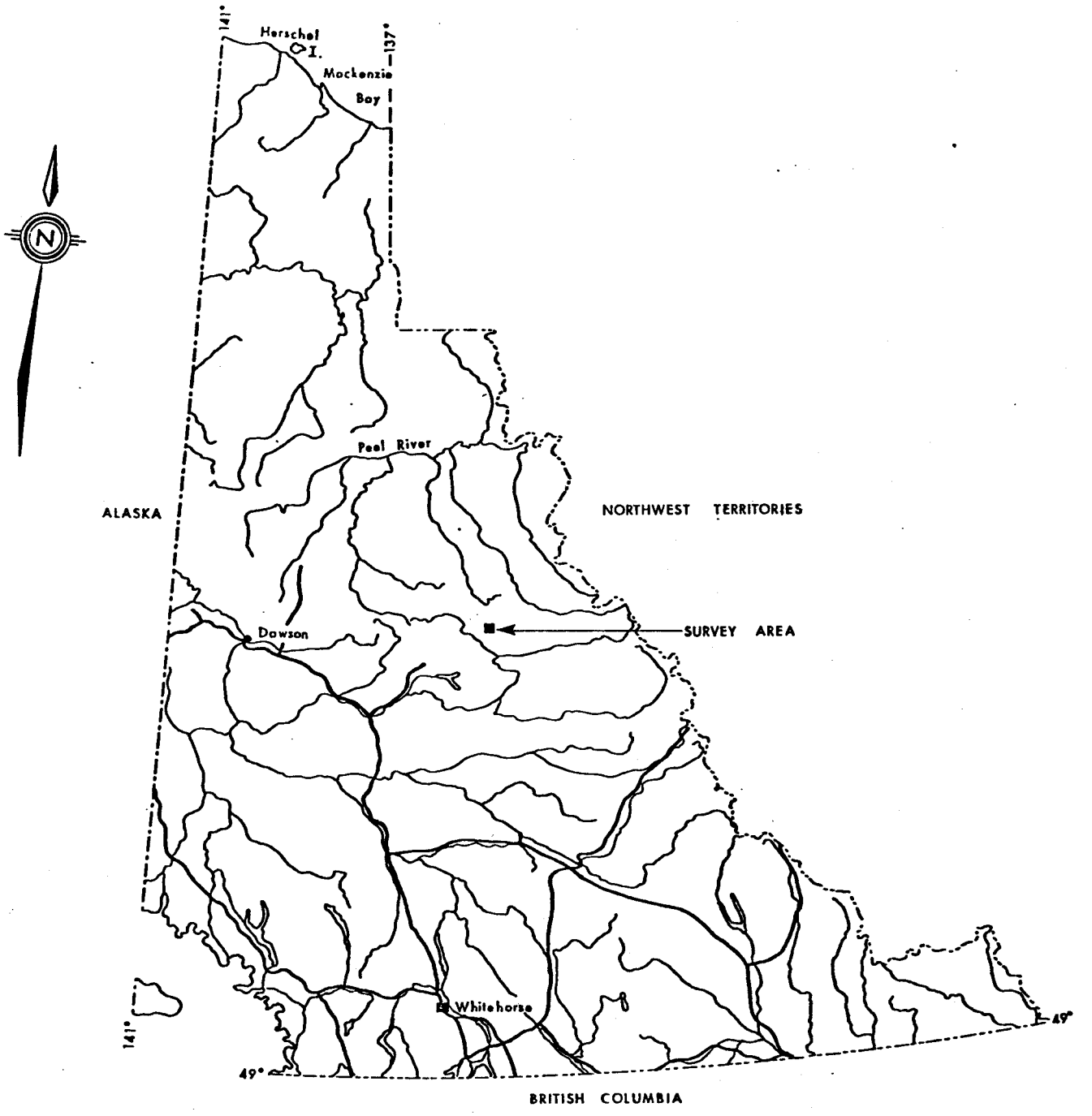
1	Location	1:6,336,00	In Report
2	Claim	1:14,750	In Report
3	PEM Profile 9650 N	1:2,500	In Report
4	PEM Profile 9750 N	1:2,500	In Report
5	Bouguer Gravity	1:2,000	Map Pocket
6	Residual Gravity	1:2,000	Map Pocket
7	Topography	1:2,000	Map Pocket

1. SUMMARY

A gravity survey and a limited amount of P.E.M. was conducted by Kenting Exploration Services Limited on the Zap Claims for Prism Resources Limited. The geophysical work consisted of 542 gravity stations and .85 km. of P.E.M.

Numerous anomalies are apparent on the residual gravity map. No specific drill targets were picked from the gravity map, however all of the positive anomalies have potential and should be evaluated further.

The P.E.M. survey covering only a small portion of the area indicated no conductive response.



LOCATION MAP
Figure 1
Scale 1:6,336,000

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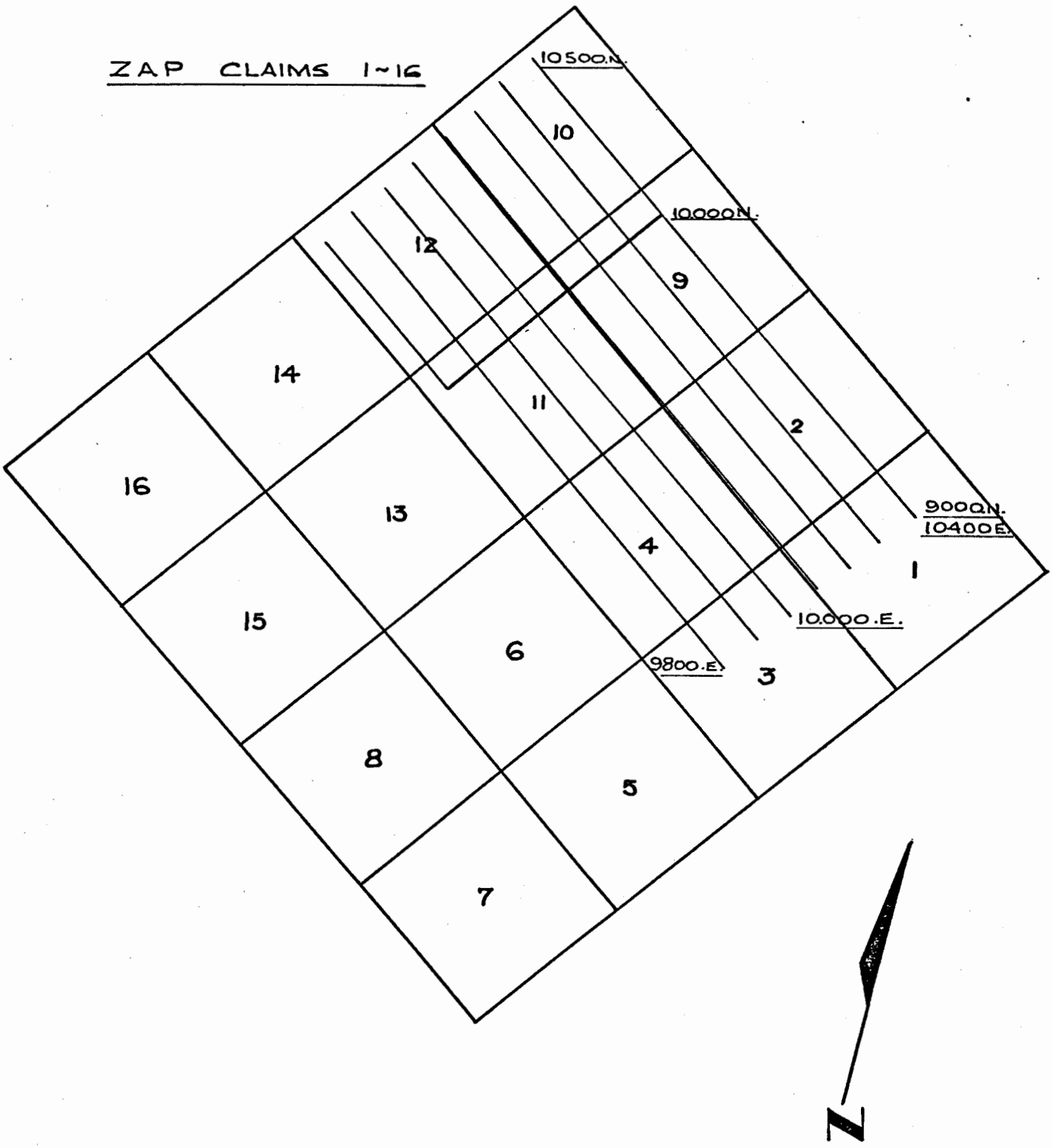

SCALE 1:14,750

CLAIM & LINE LOCATION MAP

FIGURE . 2.

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2. INTRODUCTION

During the period of June 14 to July 10, 1978, geophysical work was conducted by Kenting Exploration Services Limited on the Zap Claim Group. The claims covered are held by Prism Resources Limited. A list of Kenting Personnel involved in the survey is given in Appendix A.

The Zap property is located approximately 80 miles NE of Mayo in the Yukon Territory. The property is located at 64^{o} 16' N latitude and 134^{o} 2' W longitude. NTS map sheet 106 D/8 covers the property. Access was via fixed-wing aircraft from Mayo to nearby Kathleen Lake then via helicopter to the grid.

The geophysical surveying consisted of a gravity survey consisting of a total of 542 stations. In addition, two short lines of EM were run a total of 850 meters.

The gravity survey was conducted to outline any large subsurface bodies of high grade zinc-lead-silver mineralization which occurs in outcrop in the area. Large areas with anomalous geochem results have been mapped on the grid.

The EM surveying was conducted to test for conductivity associated with a known showing. The EM work was terminated on the second day of work when the receiver was damaged during a tumble down a steep slope.

The topography of the survey area is very rugged. Elevations ranged from 1178 m (3865 feet) to 1569 m (5147 feet) over the surveyed part of the grid.

Geological work indicates the local rocks are dolomites, quartzite and shale. Several known and suspected faults occur in the survey area and these appear to have had some effect on the location of mineralization. In several places the dolomite rocks have a large amount of open space within the rock contributing to a lower than normal density. Barite mineralization occurs in several places on the property.

3. SURVEY SPECIFICATIONS

3.1 Survey Grid

The grid was established by chain and compass surveying of lines spaced 50 meters apart. Control was provided by a baseline running along the crest of a ridge at 10,000 N on the grid and a tie line cut at 9000 N. Adjustments for steep slopes were made to the chaining to produce a consistent, horizontal station spacing of 25 meters. Stations were marked with flagged pickets.

3.2 Gravity Surveying

Gravity readings were taken with a LaCoste and Romberg gravity meter serial number G - 324. Readings were taken using the galvonometer output and have an accuracy of about 0.01 milligals. Gravity meter readings were corrected for instrument drift by running loops closed from base stations established in the area. The height of the meter above the ground surface at each reading location was recorded to enable a free - air correction to be applied. Estimates of the elevation differences for the four, Zone B Hammer Chart compartments were made by the gravity - meter operator at each station.

3.3 Elevation Surveying

Vertical control required for gravity data processing was provided by surveying the grid with a Sokisha automatic theodolite and a stadia rod. The elevation accuracy was checked by surveying in closed loops. The loop misclosures varied from .20 to 2.02 feet. Elevations along the baseline were prorated for misclosure and then used for tie points for the surveying of each line. The elevation survey was tied to a nearby NTS topo control bench mark number G - 5564 having an elevation of 5492 feet. Elevations were determined in units of feet to enable a fit to be made between the grid and published government topographic maps.

3.4 EM Surveying

The EM survey was conducted with a Pulse EM (PEM) unit manufactured by Crone Geophysics Limited of Mississauga, Ontario. The PEM unit is a time domain system measuring the decaying secondary magnetic field over eight integrating periods (channels). Technical specifications of the instrumentation is included in Appendix B. The method of surveying used is essentially free from geometrical problems that affect most EM methods in rugged terrain. The coil separation used was 50 meters and readings were taken every 25 meters.

4. RESULTS

4.1 Gravity Data Reduction

The gravity meter readings were processed with a Hewlett-Packard 9825 computer which performed all of the necessary data reduction and automatically plotted profiles of Bouguer gravity and elevation values for each line. The computer recorded all data on magnetic tape which allowed reprocessing of the data for various Bouguer density values.

Terrain corrections were based on the standard Hammer chart. Terrain corrections for Zone B were derived from elevation estimates made by the gravity operator at each station. Corrections for Zones C and D were made later using the topographic map produced from the elevation survey of the grid.

The Bouguer gravity values were based on an assumed local rock density of 2.1 gms/cc. This rather low density was picked after comparing Bouguer gravity and elevation profiles over a range of densities.

In the steeper areas of the grid a considerable amount of error is expected due to inaccurate terrain corrections. The inaccuracy results from the fact that the Hammer chart method gives an approximate correction which becomes more inaccurate with increasing ruggedness of the nearby terrain. The error expected in steepest areas may be as high as 0.5 milligals.

4.2 Regional Trend Removal

A regional trend with a 7 milligal change over the grid was removed from the Bouguer gravity to produce a residual map. The regional removal was done to enhance local anomalies in areas of steep, regional - scale anomaly gradients.

4.3 Data Presentation

The Bouguer, regional and residual gravity data are presented as contoured maps at a scale of 1:1000 in Figures 5, 6, and 7. A list of principle data is included in Appendix C.

The EM survey results are presented as profiles which run across the grid lines at 9750 N. These are bound in the report as Figures 3 and 4.

5. INTERPRETATION

The residual gravity map shows numerous high and low gravity anomalies. Several of the low-gravity anomalies occur where local terrain is very steep and are probably due to insufficient terrain corrections. The broader lows are probably due to a highly porous rock or possibly a thick overburden cover.

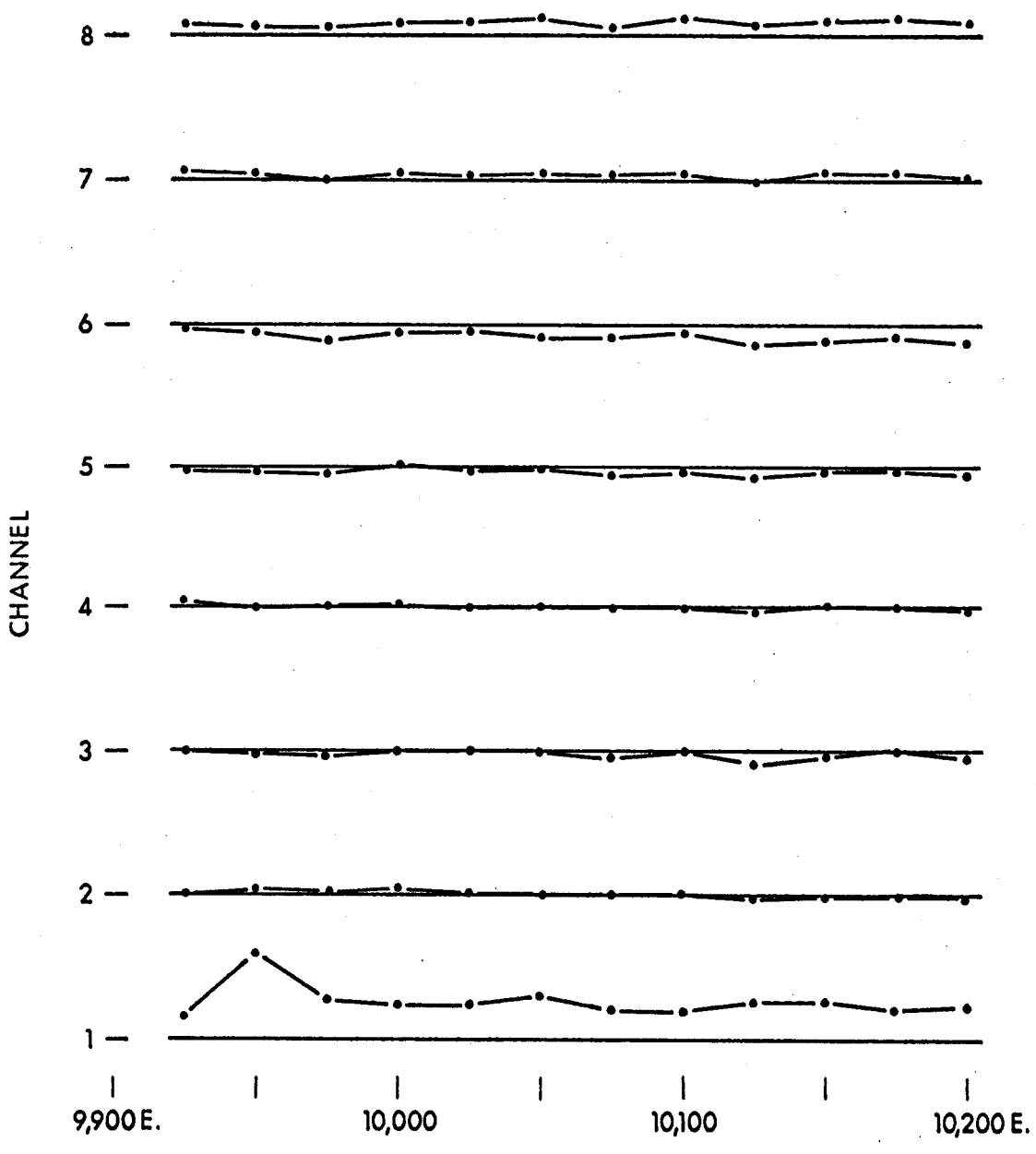
The numerous high-gravity anomalies all warrant further attention. It must be noted however, that because of the relatively low Bouguer density used (2.1 gms/cc) these may be due to rock with a more normal density for dolomites and quartzite (2.4 to 2.7 gms/cc). It is difficult to assign priorities for the evaluation of these anomalies except to say that the best targets would be those with the highest amplitude. Gravity anomaly targets should be picked only if there is either geochemical or geological support.

The pattern of highs and lows on the residual map suggests the occurance of several faults with a significant displacement. Of the two most obvious, one runs coincidently with line 10050 E and the second runs from about 9600 N on line 10400 E to 10500 N on line 9700 E. These faults are interpreted based on an assumption of a density contrast between the adjacent rocks. The apparent variation in density within a rock unit makes any further interpretation difficult until more is known of the geology in this area.

6. RECOMMENDATIONS

The high-gravity anomalies should be evaluated in terms of geochemical and geological information. If there is support for an anomaly it should be drilled to identify its source.

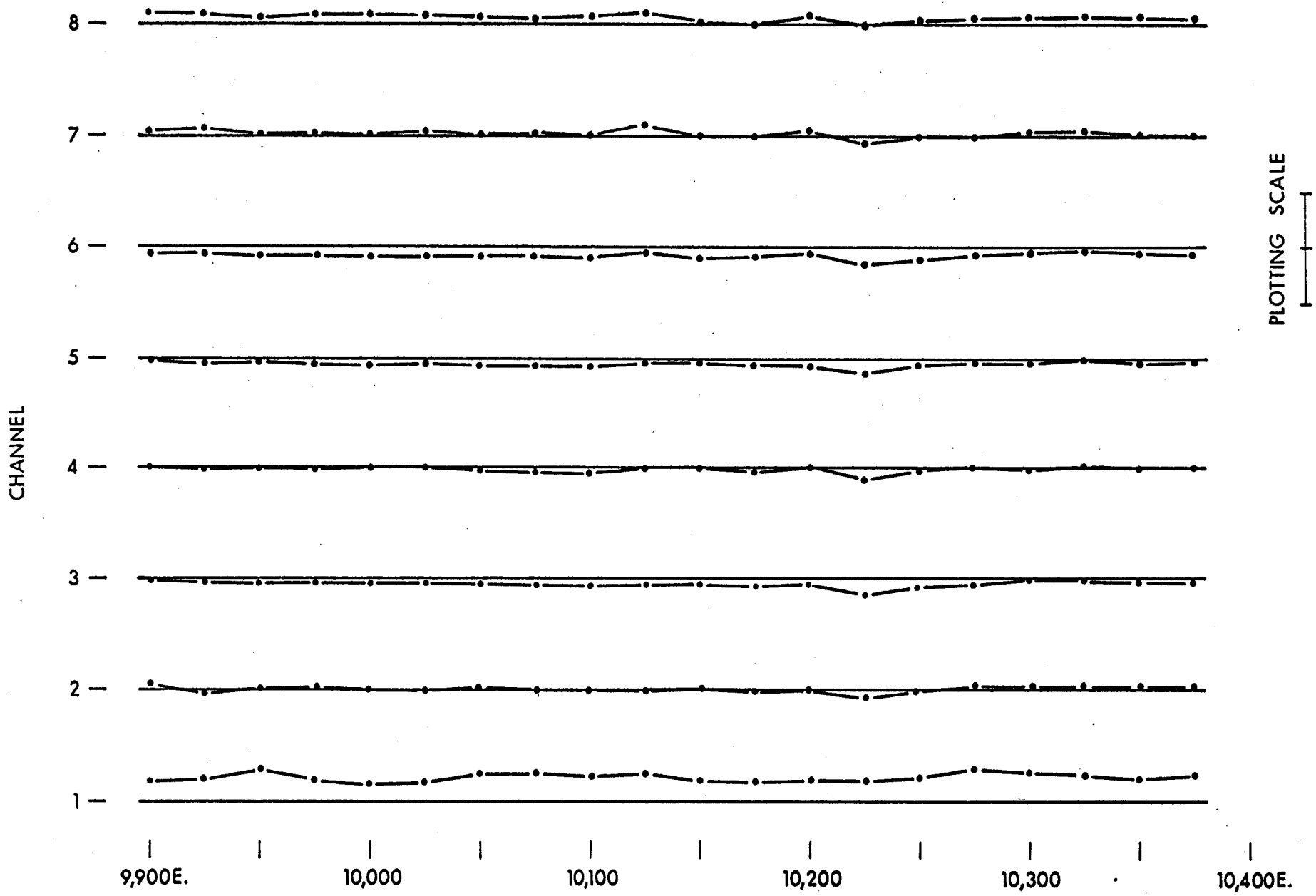
An IP survey could be conducted after testing to ensure responses over the known showings. The showing tested with EM may show a chargeability anomaly which would guide drilling and extended exploration in the area.



PLOTTING SCALE
+10
0
-10

P.E.M.
LINE 9650N.
Coil spacing 50 m.
Figure 3

KENTING
EXPLORATION SERVICES LIMITED

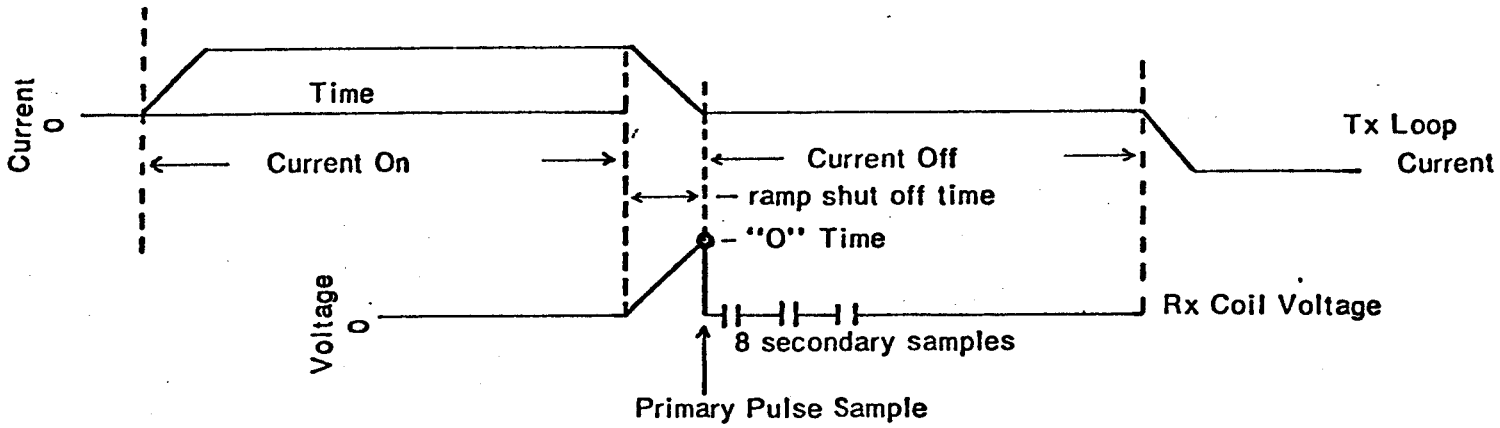


P.E.M.
LINE 9750N.
Coil spacing 50 m. Figure 4

KENTING
EXPLORATION SERVICES LIMITED

APPENDIX B

PEM SPECIFICATIONS



Current Off time: 9.4 ms
Current on time: 10.8 ms
Current shut off (ramp) time: 1.4 ms
Sample times (zero to centre of sample): .15ms, .45ms, .85ms, 1.45ms, 2.45ms, 3.75ms, 5.85ms, 8.85ms.

Sample width: 100 μs
Zero time set at drop off point of primary pulse

TRANSMITTER — Transmitter power and loop size may be increased to obtain increased penetration. Weight, portability and power capabilities of the control instrument are the limiting factors. The standard transmitter i designed to be carried by two men.

Loop diameter	— minimum 4 meters (13 feet)
Loop current	— 15 to 20 amps
Loop applied voltage	— 24 volts
Loop output	— minimum 4500 amps x meter ^{2}
Loop weight	— 11.8 kilos (26 lb)
Control unit weight	— 10 kilos (22 lb)
Control unit dimensions	— 20.5cm x 25.5cm x 36.5cm (8" x 10" x 14.5")
Battery supply weight	— 18.1 kilos (40 lb)
Battery supply	— 2 of 12 volt, 14 to 20 ampere hour

Timing control by radio synchronization

RECEIVER

- Receive coil dimensions: 55cm x 15cm (22" x 6")
- Receive coil weight: 4.5 kilos (10 lb)
- Preamplifier in coil
- Preamplifier batteries: 2 of 9 volt
- Receive coil tripod mounted
- Receiver measuring instrument dimensions: 28cm x 18cm x 21.5cm (11" x 7" x 9")
- Receiver measuring instrument weight: 6.3 kilos (14 lb)
- Timing control by radio synchronization
- Primary sample width: 100 μs
- Primary sample can be swept through primary pulse by means of a time calibrated pot
- Zero time set at primary pulse drop-off
- Secondary samples (eight of them) width: 100 μs
- Secondary samples time (zero to middle of sample): (1) .15ms (2) .45ms (3) .85ms (4) 1.45ms (5) 2.45ms (6) 3.75ms (7) 5.85ms (8) 8.85ms
- Automatic sampling for 5 seconds then all samples automatically stored
- Sample read out by means of meter
- Continuous sampling possible by switching function switch to "Continuous"
- Noise can be monitored by switching function switch to "Noise"
- Battery supply: 24 volt rechargeable, 2 of 12 volt Gel GC 12-15

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10200E	10000N	5092.9	329.70	672.38	2.10
10200E	9950N	5097.0	328.94	672.20	2.10
10200E	9900N	5073.8	330.12	672.25	2.10
10200E	9850N	4941.1	340.82	674.00	2.10
10200E	9800N	4881.6	344.91	674.03	2.10
10200E	9750N	4830.2	348.24	673.78	2.10
10200E	9700N	4766.2	352.83	674.10	2.10
10200E	9650N	4730.2	354.57	673.61	2.10
10200E	9600N	4626.7	361.33	673.44	2.10
10200E	9550N	4527.8	367.82	673.28	2.10
10200E	9500N	4472.7	371.32	672.86	2.10
10200E	9450N	4434.9	373.62	672.45	2.10
10200E	9450N	4434.9	373.55	672.40	2.10
10200E	9400N	4367.4	377.66	671.96	2.10
10200E	9350N	4330.4	379.83	671.60	2.10
10200E	9300N	4276.4	383.26	671.33	2.10
10200E	9250N	4215.9	387.28	671.27	2.10
10200E	9200N	4187.1	388.99	670.97	2.10
10200E	9150N	4143.4	391.53	670.65	2.10
10200E	9100N	4088.4	394.93	670.51	2.10
10200E	9050N	4021.5	398.99	670.18	2.10
10200E	9000N	3946.5	403.52	669.74	2.10
10150E	9000N	4015.4	399.65	670.15	2.10
10150E	9050N	4083.2	395.52	670.46	2.10
10150E	9100N	4085.6	395.65	670.86	2.10
10150E	9150N	4121.6	393.26	671.28	2.10
10150E	9200N	4218.9	387.36	671.72	2.10
10150E	9250N	4253.9	384.84	671.48	2.10
10150E	9300N	4313.5	380.89	671.56	2.10
10150E	9350N	4376.6	376.91	671.69	2.10
10150E	9400N	4415.2	374.71	672.02	2.10
10150E	9450N	4457.4	372.23	672.37	2.10
10150E	9500N	4489.1	370.44	672.75	2.10
10150E	9550N	4532.7	367.70	673.15	2.10
10150E	9600N	4600.4	363.44	673.55	2.10
10150E	9650N	4691.2	357.58	673.73	2.10
10150E	9700N	4727.2	355.64	674.09	2.10
10150E	9750N	4755.2	353.99	674.35	2.10
10150E	9800N	4821.4	349.63	674.74	2.10
10150E	9850N	4899.9	344.12	674.60	2.10
10150E	9900N	4988.5	337.69	674.06	2.10
10150E	9950N	5098.3	329.42	673.16	2.10
10150E	10000N	5082.5	331.28	673.62	2.10
10300E	10000N	4905.3	344.72	675.13	2.10
10300E	9950N	4916.9	343.23	674.20	2.10
10300E	9900N	4917.8	342.74	673.77	2.10
10300E	9850N	4890.4	344.58	673.78	2.10
10300E	9800N	4847.4	347.61	673.89	2.10
10300E	9750N	4813.3	349.92	673.88	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10300E	9700N	4793.7	351.02	673.66	2.10
10300E	9650N	4829.1	346.90	672.09	2.10
10300E	9600N	4795.5	348.29	671.61	2.10
10300E	9550N	4696.2	355.34	672.40	2.10
10300E	9500N	4591.7	362.62	672.83	2.10
10300E	9450N	4474.0	370.35	672.65	2.10
10300E	9400N	4365.7	377.46	672.54	2.10
10300E	9350N	4280.0	383.13	671.97	2.10
10300E	9300N	4224.5	386.64	671.55	2.10
10300E	9250N	4162.4	390.56	671.19	2.10
10300E	9200N	4100.1	394.42	670.93	2.10
10300E	9150N	4049.7	397.43	670.49	2.10
10300E	9100N	3987.0	400.78	669.54	2.10
10300E	9050N	3929.9	404.14	669.01	2.10
10300E	9000N	3865.4	408.42	669.05	2.10
10250E	9000N	3902.7	405.99	669.43	2.10
10250E	9050N	4046.2	398.05	670.99	2.10
10250E	9100N	4069.7	395.75	670.12	2.10
10250E	9150N	4118.0	392.78	670.13	2.10
10250E	9200N	4144.7	391.56	670.67	2.10
10250E	9250N	4178.9	389.60	671.05	2.10
10250E	9300N	4238.0	385.80	671.30	2.10
10250E	9350N	4284.0	383.08	671.80	2.10
10250E	9400N	4335.6	379.91	672.19	2.10
10250E	9450N	4390.5	376.34	672.52	2.10
10250E	9500N	4487.5	370.06	673.11	2.10
10250E	9550N	4595.9	362.92	673.37	2.10
10250E	9600N	4719.5	354.09	672.75	2.10
10250E	9650N	4821.6	347.23	672.36	2.10
10250E	9700N	4824.7	348.47	673.34	2.10
10250E	9750N	4857.3	346.41	673.40	2.10
10250E	9800N	4891.2	344.26	673.58	2.10
10250E	9850N	4938.5	340.83	673.36	2.10
10250E	9900N	4991.9	336.82	672.93	2.10
10250E	9950N	5016.7	335.19	672.84	2.10
10100E	9975N	5077.8	331.97	673.78	2.10
10100E	9950N	5083.5	331.21	673.60	2.10
10100E	9925N	5076.1	331.27	673.37	2.10
10100E	9900N	5036.5	334.02	673.51	2.10
10100E	9875N	4983.0	338.06	674.08	2.10
10100E	9850N	4930.3	341.83	674.38	2.10
10100E	9825N	4877.0	345.63	674.59	2.10
10100E	9800N	4862.2	346.55	674.45	2.10
10100E	9775N	4826.6	348.94	674.38	2.10
10100E	9750N	4788.9	351.41	674.24	2.10
10100E	9725N	4766.5	352.73	673.98	2.10
10100E	9700N	4745.7	353.95	673.80	2.10
10100E	9675N	4720.4	355.54	673.78	2.10
10100E	9650N	4682.0	358.01	673.63	2.10
10100E	9625N	4650.0	360.09	673.44	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10100E	9600N	4622.3	361.84	673.31	2.10
10100E	9575N	4598.4	363.36	673.20	2.10
10100E	9550N	4566.1	365.35	673.03	2.10
10100E	9525N	4543.1	366.89	672.92	2.10
10100E	9500N	4530.6	367.59	672.74	2.10
10100E	9475N	4521.2	368.00	672.62	2.10
10100E	9450N	4494.2	369.61	672.50	2.10
10100E	9425N	4456.4	372.10	672.57	2.10
10100E	9400N	4421.7	374.31	672.43	2.10
10100E	9375N	4381.9	376.82	672.32	2.10
10100E	9350N	4350.8	378.86	672.34	2.10
10100E	9325N	4319.7	380.74	672.05	2.10
10100E	9300N	4271.5	383.83	671.85	2.10
10100E	9275N	4230.5	386.55	671.69	2.10
10100E	9250N	4201.5	388.31	671.41	2.10
10100E	9225N	4184.6	389.49	671.34	2.10
10100E	9200N	4164.6	390.81	671.18	2.10
10100E	9175N	4160.2	391.16	671.16	2.10
10100E	9150N	4152.3	391.62	671.02	2.10
10100E	9125N	4146.6	392.00	671.04	2.10
10100E	9100N	4159.2	390.99	670.96	2.10
10100E	9075N	4166.1	390.29	670.76	2.10
10100E	9050N	4151.6	391.19	670.67	2.10
10100E	9025N	4132.8	392.26	670.45	2.10
10100E	9000N	4114.7	393.16	670.17	2.10
10050E	9000N	4129.8	392.12	670.39	2.10
10050E	9025N	4169.5	389.99	670.94	2.10
10050E	9050N	4194.3	388.49	671.00	2.10
10050E	9075N	4216.7	386.95	670.95	2.10
10050E	9100N	4234.6	385.87	671.04	2.10
10050E	9125N	4239.2	385.66	671.06	2.10
10050E	9150N	4248.0	385.34	671.32	2.10
10050E	9175N	4252.7	385.12	671.41	2.10
10050E	9200N	4262.9	384.25	671.38	2.10
10050E	9225N	4285.0	383.01	671.75	2.10
10050E	9250N	4308.4	381.40	671.85	2.10
10050E	9275N	4326.2	380.22	672.03	2.10
10050E	9300N	4370.3	377.41	672.32	2.10
10050E	9325N	4421.8	373.97	672.38	2.10
10050E	9350N	4454.2	371.85	672.46	2.10
10050E	9375N	4490.6	369.45	672.48	2.10
10050E	9400N	4531.0	367.13	672.91	2.10
10050E	9425N	4570.5	364.09	672.40	2.10
10050E	9450N	4605.5	361.73	672.29	2.10
10050E	9475N	4642.1	359.21	672.26	2.10
10050E	9500N	4655.5	358.72	672.48	2.10
10050E	9525N	4676.1	357.41	672.55	2.10
10050E	9550N	4701.7	355.78	672.68	2.10
10050E	9600N	4764.4	351.65	672.75	2.10
10050E	9625N	4778.6	350.83	672.83	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10050E	9650N	4806.1	349.13	673.01	2.10
10050E	9675N	4844.1	346.74	673.17	2.10
10050E	9700N	4895.1	342.79	672.79	2.10
10050E	9725N	4895.0	343.57	673.33	2.10
10050E	9750N	4901.7	343.16	673.48	2.10
10050E	9825N	4997.9	334.41	671.23	2.10
10050E	9850N	5032.4	334.02	673.21	2.10
10050E	9875N	5068.7	331.41	673.09	2.10
10050E	9900N	5104.9	328.64	672.60	2.10
10050E	9925N	5121.9	327.73	672.90	2.10
10050E	9950N	5114.4	328.75	673.27	2.10
10050E	9975N	5099.4	330.33	673.84	2.10
10050E	10000N	5081.5	331.95	674.13	2.10
10000E	10000N	5129.0	327.54	672.82	2.10
10000E	9975N	5147.5	325.95	672.44	2.10
10000E	9950N	5149.5	325.75	672.37	2.10
10000E	9925N	5141.8	326.25	672.29	2.10
10000E	9900N	5123.1	327.58	672.35	2.10
10000E	9875N	5105.1	328.63	672.27	2.10
10000E	9850N	5072.0	330.89	672.42	2.10
10000E	9825N	5061.2	331.45	672.27	2.10
10000E	9800N	5043.6	332.63	672.38	2.10
10000E	9775N	5015.5	334.50	672.46	2.10
10000E	9750N	4992.3	335.97	672.37	2.10
10000E	9725N	4960.0	338.13	672.35	2.10
10000E	9700N	4929.5	339.97	672.25	2.10
10000E	9675N	4885.7	343.21	672.67	2.10
10000E	9650N	4841.5	346.56	673.05	2.10
10000E	9625N	4813.4	348.36	672.90	2.10
10000E	9600N	4786.6	349.96	672.68	2.10
10000E	9575N	4754.6	351.90	672.60	2.10
10000E	9550N	4706.5	355.40	672.81	2.10
10000E	9525N	4661.4	358.48	672.83	2.10
10000E	9500N	4631.8	360.44	672.76	2.10
10000E	9475N	4600.8	362.47	672.67	2.10
10000E	9450N	4564.6	364.76	672.53	2.10
10000E	9425N	4547.2	365.73	672.24	2.10
10000E	9400N	4520.1	367.30	672.01	2.10
10000E	9375N	4491.1	369.37	672.12	2.10
10000E	9350N	4455.1	371.83	672.14	2.10
10000E	9325N	4426.5	373.66	672.01	2.10
10000E	9300N	4388.5	376.19	671.96	2.10
10000E	9275N	4358.1	378.08	671.75	2.10
10000E	9250N	4339.4	379.21	671.53	2.10
10000E	9225N	4316.7	380.62	671.39	2.10
10000E	9200N	4296.1	382.00	671.37	2.10
10000E	9175N	4275.6	383.30	671.25	2.10
10000E	9150N	4254.2	384.71	671.27	2.10
10000E	9125N	4233.3	386.05	671.17	2.10
10000E	9100N	4207.0	387.58	670.92	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10000E	9075N	4187.3	388.87	670.98	2.10
10000E	9050N	4158.3	390.58	670.70	2.10
10000E	9025N	4131.6	392.23	670.56	2.10
10000E	9000N	4102.4	393.95	670.35	2.10
9950E	9000N	4053.0	397.10	670.86	2.10
9950E	9025N	4148.6	391.43	671.28	2.10
9950E	9050N	4180.0	389.45	671.35	2.10
9950E	9075N	4202.8	388.03	671.35	2.10
9950E	9100N	4221.6	386.85	671.47	2.10
9950E	9125N	4239.1	385.95	671.59	2.10
9950E	9150N	4255.3	384.87	671.54	2.10
9950E	9175N	4275.9	383.58	671.68	2.10
9950E	9200N	4301.1	381.91	671.73	2.10
9950E	9225N	4323.3	380.58	671.99	2.10
9950E	9250N	4350.0	378.90	672.15	2.10
9950E	9275N	4383.4	376.71	672.20	2.10
9950E	9300N	4408.2	375.10	672.25	2.10
9950E	9325N	4442.0	372.87	672.24	2.10
9950E	9350N	4463.6	371.71	672.41	2.10
9950E	9375N	4474.0	371.06	672.56	2.10
9950E	9400N	4491.7	369.96	672.73	2.10
9950E	9425N	4532.1	367.44	673.00	2.10
9950E	9450N	4546.9	366.40	673.01	2.10
9950E	9475N	4577.1	364.52	673.31	2.10
9950E	9500N	4624.7	361.67	673.71	2.10
9950E	9525N	4655.6	359.22	673.47	2.10
9950E	9550N	4701.0	356.21	673.50	2.10
9950E	9575N	4744.8	353.19	673.46	2.10
9950E	9600N	4797.7	349.53	673.33	2.10
9950E	9625N	4836.9	346.87	673.26	2.10
9950E	9650N	4880.2	343.75	672.98	2.10
9950E	9675N	4908.1	341.89	672.88	2.10
9950E	9700N	4944.1	339.19	672.46	2.10
9950E	10000N	5123.3	328.14	673.23	2.10
9950E	9975N	5146.6	326.25	672.90	2.10
9950E	9950N	5145.5	326.31	672.77	2.10
9950E	9925N	5134.5	327.06	672.63	2.10
9950E	9900N	5113.9	328.59	672.80	2.10
9950E	9875N	5088.3	330.41	672.93	2.10
9950E	9850N	5058.5	332.63	673.17	2.10
9950E	9825N	5039.4	333.90	673.15	2.10
9950E	9800N	5029.6	334.36	673.06	2.10
9950E	9775N	5027.2	333.78	672.33	2.10
9950E	9750N	5004.2	335.29	672.41	2.10
9950E	9725N	4979.0	336.94	672.41	2.10
9950E	9700N	4944.1	339.40	672.66	2.10
9950E	9675N	4908.1	341.78	672.67	2.10
9900E	9675N	4849.9	346.28	673.08	2.10
9900E	9700N	4877.4	344.51	673.07	2.10
9900E	9725N	4897.3	343.34	673.14	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
9900E	9750N	4907.1	342.96	673.46	2.10
9900E	9775N	4923.7	342.13	673.80	2.10
9900E	9800N	4930.4	341.83	674.10	2.10
9900E	9825N	4957.3	340.00	674.13	2.10
9900E	9850N	4997.9	337.27	674.21	2.10
9900E	9875N	5043.2	334.02	673.85	2.10
9900E	9900N	5091.9	330.14	673.36	2.10
9900E	9925N	5118.1	328.39	673.48	2.10
9900E	9950N	5125.7	328.01	673.52	2.10
9900E	9975N	5106.0	329.74	673.78	2.10
9900E	9650N	4827.1	347.80	673.19	2.10
9900E	9625N	4800.6	349.46	673.22	2.10
9900E	9600N	4768.3	351.63	673.32	2.10
9900E	9575N	4717.3	355.20	673.58	2.10
9900E	9550N	4669.2	358.53	673.79	2.10
9900E	9525N	4617.2	361.93	673.79	2.10
9900E	9500N	4565.3	365.35	673.80	2.10
9900E	9475N	4517.0	368.58	673.70	2.10
9900E	9450N	4467.2	371.75	673.43	2.10
9900E	9425N	4423.6	374.55	673.28	2.10
9900E	9400N	4371.5	377.87	672.93	2.10
9900E	9375N	4319.2	381.00	672.51	2.10
9900E	9350N	4300.6	382.22	672.23	2.10
9900E	9325N	4286.1	383.04	672.02	2.10
9900E	9300N	4264.6	384.36	671.87	2.10
9900E	9275N	4241.4	385.75	671.68	2.10
9900E	9250N	4210.6	387.65	671.46	2.10
9900E	9225N	4180.4	389.67	671.45	2.10
9900E	9200N	4154.8	391.23	671.25	2.10
9900E	9175N	4131.6	392.86	671.28	2.10
9900E	9150N	4107.2	394.27	671.03	2.10
9900E	9125N	4096.2	394.93	670.85	2.10
9900E	9100N	4079.0	395.90	670.68	2.10
9900E	9075N	4066.9	396.66	670.66	2.10
9900E	9050N	4055.0	397.33	670.56	2.10
9900E	9025N	4030.1	398.72	670.30	2.10
9900E	9000N	4007.2	400.11	670.20	2.10
9850E	9025N	3955.4	403.23	669.64	2.10
9850E	9050N	3970.6	402.32	669.78	2.10
9850E	9075N	3981.4	401.76	669.96	2.10
9850E	9100N	3995.5	400.89	670.04	2.10
9850E	9125N	4008.9	400.02	670.11	2.10
9850E	9150N	4027.3	398.71	670.08	2.10
9850E	9175N	4066.7	396.46	670.58	2.10
9850E	9200N	4080.7	395.48	670.63	2.10
9850E	9225N	4097.6	394.31	670.68	2.10
9850E	9250N	4126.1	392.92	671.36	2.10
9850E	9275N	4159.9	390.80	671.69	2.10
9850E	9300N	4209.4	387.81	672.06	2.10
9850E	9325N	4262.2	384.65	672.59	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
9850E	9350N	4302.7	382.19	672.86	2.10
9850E	9375N	4355.8	378.95	673.27	2.10
9850E	9400N	4397.0	376.26	673.38	2.10
9850E	9425N	4461.9	371.99	673.36	2.10
9850E	9450N	4505.8	369.21	673.52	2.10
9850E	9475N	4544.4	366.80	673.66	2.10
9850E	9500N	4586.9	363.86	673.51	2.10
9850E	9525N	4636.9	360.46	673.37	2.10
9850E	9550N	4682.0	357.51	673.36	2.10
9850E	9575N	4716.7	355.18	673.21	2.10
9850E	9600N	4740.4	353.71	673.21	2.10
9850E	9625N	4758.4	352.68	673.28	2.10
9850E	9650N	4778.2	351.37	673.23	2.10
9850E	9675N	4796.3	350.31	673.27	2.10
9850E	9700N	4818.2	348.84	673.32	2.10
9850E	9725N	4821.9	348.95	673.70	2.10
9850E	9750N	4833.6	348.20	673.68	2.10
9850E	9775N	4841.3	347.87	674.15	2.10
9850E	9800N	4873.8	345.73	674.34	2.10
9850E	9825N	4916.5	342.91	674.41	2.10
9850E	9850N	4955.6	340.19	674.34	2.10
9850E	9875N	5009.6	336.38	674.07	2.10
9850E	9900N	5057.6	332.82	673.80	2.10
9850E	9925N	5091.9	330.31	673.63	2.10
9850E	9950N	5108.0	329.24	673.60	2.10
9850E	9975N	5092.2	330.77	674.19	2.10
9800E	9975N	5069.6	332.78	674.35	2.10
9800E	9950N	5063.4	333.01	674.30	2.10
9800E	9925N	5039.8	334.53	674.39	2.10
9800E	9900N	5005.8	336.80	674.42	2.10
9800E	9850N	4898.3	344.20	674.91	2.10
9800E	9825N	4834.5	348.60	674.94	2.10
9800E	9800N	4794.7	351.06	674.59	2.10
9800E	9750N	4710.1	356.59	674.31	2.10
9800E	9725N	4685.5	358.21	673.99	2.10
9800E	9700N	4692.8	357.62	673.76	2.10
9800E	9675N	4664.8	359.32	673.56	2.10
9800E	9650N	4660.1	359.49	673.26	2.10
9800E	9625N	4648.8	360.25	673.22	2.10
9800E	9600N	4637.5	360.92	673.17	2.10
9800E	9575N	4627.8	361.33	672.97	2.10
9750E	9000N	3909.5	406.10	670.14	2.10
9750E	9050N	4007.1	400.04	670.65	2.10
9750E	9100N	4085.9	395.40	671.16	2.10
9750E	9150N	4142.5	392.13	671.57	2.10
9750E	9200N	4193.4	388.91	671.73	2.10
9750E	9250N	4242.9	385.92	672.15	2.10
9750E	9300N	4326.5	380.51	672.46	2.10
9750E	9350N	4401.5	375.48	672.41	2.10
9750E	9400N	4486.1	369.88	672.37	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
9750E	9450N	4528.1	367.49	672.52	2.10
9750E	9500N	4534.8	367.49	672.83	2.10
9750E	9550N	4537.8	367.56	673.01	2.10
9750E	9600N	4550.7	366.74	673.09	2.10
9750E	9650N	4543.5	367.23	673.36	2.10
9750E	9700N	4576.3	365.24	673.84	2.10
9750E	9750N	4670.6	359.48	674.75	2.10
9750E	9800N	4780.1	352.30	675.18	2.10
9750E	9850N	4861.1	346.80	675.01	2.10
9750E	9900N	4951.4	340.82	674.85	2.10
9750E	9950N	5031.1	335.44	674.58	2.10
9750E	10000N	5059.5	333.54	674.48	2.10
9800E	9025N	3904.7	406.41	669.95	2.10
9800E	9050N	3935.8	404.49	669.92	2.10
9800E	9075N	3983.7	401.58	670.41	2.10
9800E	9100N	4026.4	399.24	670.85	2.10
9800E	9125N	4042.5	398.31	671.06	2.10
9800E	9150N	4070.5	396.62	671.24	2.10
9800E	9175N	4095.4	395.18	671.56	2.10
9800E	9200N	4129.1	393.24	671.82	2.10
9800E	9225N	4153.2	391.75	672.02	2.10
9800E	9250N	4190.3	389.37	672.18	2.10
9800E	9275N	4234.1	386.43	672.25	2.10
9800E	9300N	4285.0	383.17	672.56	2.10
9800E	9350N	4347.3	379.19	672.67	2.10
9800E	9375N	4385.4	376.80	672.78	2.10
9800E	9400N	4429.8	373.96	672.89	2.10
9800E	9425N	4472.2	371.24	672.91	2.10
9800E	9450N	4511.9	368.71	673.00	2.10
9800E	9475N	4550.0	366.11	672.89	2.10
9800E	9500N	4586.7	363.52	672.66	2.10
9800E	9525N	4605.2	362.65	672.84	2.10
9800E	9550N	4614.3	362.19	672.90	2.10
9700E	10000N	5041.7	334.85	674.76	2.10
9700E	10050N	4965.3	341.03	675.68	2.10
9700E	10100N	4906.4	345.38	676.40	2.10
9700E	10150N	4824.5	351.11	676.91	2.10
9700E	10200N	4726.4	358.00	677.24	2.10
9700E	10250N	4648.3	363.55	677.33	2.10
9700E	10300N	4573.7	368.71	677.44	2.10
9700E	10350N	4505.5	373.14	677.20	2.10
9700E	10400N	4422.8	378.10	676.50	2.10
9700E	10450N	4405.0	379.08	676.18	2.10
9700E	10500N	4452.2	376.71	676.98	2.10
9750E	10500N	4370.8	381.77	676.36	2.10
9750E	10450N	4390.4	380.03	675.96	2.10
9750E	10400N	4467.6	375.58	676.85	2.10
9750E	10350N	4540.5	370.89	677.08	2.10
9750E	10300N	4602.6	366.75	677.25	2.10
9750E	10250N	4673.4	361.95	677.26	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
9750E	10200N	4754.3	356.06	677.03	2.10
9750E	10150N	4855.2	348.97	676.66	2.10
9750E	10100N	4947.8	342.23	675.92	2.10
9750E	10050N	5000.6	338.27	675.19	2.10
9800E	10000N	5058.1	333.66	674.38	2.10
9850E	10000N	5051.4	334.42	674.59	2.10
9850E	10050N	5023.5	336.84	675.37	2.10
9850E	10100N	4940.1	342.95	676.17	2.10
9850E	10150N	4839.3	350.28	676.82	2.10
9850E	10200N	4747.4	356.62	676.89	2.10
9850E	10250N	4669.3	362.03	676.86	2.10
9850E	10300N	4612.7	365.71	676.43	2.10
9850E	10350N	4570.9	368.69	676.48	2.10
9850E	10400N	4537.2	370.98	676.46	2.10
9850E	10450N	4505.7	372.99	676.32	2.10
9850E	10500N	4453.0	376.27	676.16	2.10
9800E	10500N	4360.1	381.85	675.55	2.10
9800E	10450N	4379.8	380.39	675.44	2.10
9800E	10400N	4444.4	376.59	676.17	2.10
9800E	10350N	4517.3	372.14	676.86	2.10
9800E	10050N	4997.2	338.93	675.57	2.10
9800E	10100N	4930.5	343.98	676.48	2.10
9800E	10150N	4850.0	349.61	676.89	2.10
9800E	10200N	4753.7	356.24	677.11	2.10
9800E	10250N	4673.3	361.96	677.23	2.10
9800E	10300N	4590.5	367.32	676.90	2.10
9900E	10500N	4518.3	371.99	676.59	2.10
9900E	10450N	4576.5	368.40	676.64	2.10
9900E	10400N	4618.8	365.72	676.76	2.10
9900E	10350N	4644.0	364.10	676.85	2.10
9900E	10300N	4686.2	361.14	676.79	2.10
9900E	10250N	4744.7	357.11	676.77	2.10
9900E	10200N	4797.6	353.32	676.67	2.10
9900E	10150N	4839.3	348.32	674.68	2.10
9900E	10100N	4959.3	341.50	676.02	2.10
9900E	10050N	5035.3	335.73	675.07	2.10
9900E	10000N	5078.1	332.30	674.23	2.10
10000E	10050N	5058.5	333.82	674.42	2.10
10000E	10100N	5001.6	338.59	675.46	2.10
10000E	10150N	4971.4	340.78	675.53	2.10
10000E	10200N	4935.2	343.13	675.56	2.10
10000E	10250N	4858.4	349.11	676.35	2.10
10000E	10300N	4809.6	352.96	676.99	2.10
10000E	10350N	4809.5	352.59	676.34	2.10
10000E	10400N	4761.2	356.03	676.61	2.10
10000E	10450N	4723.6	358.40	676.40	2.10
10000E	10500N	4679.8	361.24	676.52	2.10
9950E	10500N	4584.9	367.85	676.97	2.10
9950E	10450N	4656.0	363.12	676.97	2.10
9950E	10400N	4717.7	358.99	676.77	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
9950E	10350N	4763.9	355.92	676.71	2.10
9950E	10300N	4772.4	355.51	676.84	2.10
9950E	10250N	4823.9	351.60	676.55	2.10
9950E	10200N	4888.8	346.75	676.04	2.10
9950E	10150N	4927.9	344.16	676.11	2.10
9950E	10100N	4971.8	340.69	675.78	2.10
9950E	10050N	5036.9	335.52	674.83	2.10
10100E	10000N	5071.4	332.69	674.18	2.10
10100E	10050N	5058.6	333.67	674.36	2.10
10100E	10100N	5000.0	338.24	675.25	2.10
10100E	10150N	4903.6	345.49	676.11	2.10
10100E	10200N	4840.5	350.35	676.66	2.10
10100E	10250N	4779.6	354.57	676.60	2.10
10100E	10300N	4730.4	358.17	676.68	2.10
10100E	10350N	4714.6	359.21	676.56	2.10
10100E	10400N	4711.1	359.24	676.44	2.10
10100E	10450N	4668.3	362.08	676.54	2.10
10100E	10500N	4613.3	365.85	676.58	2.10
10050E	10500N	4668.1	361.86	676.37	2.10
10050E	10450N	4736.9	357.03	676.07	2.10
10050E	10400N	4795.9	352.82	675.85	2.10
10050E	10350N	4791.8	353.73	676.23	2.10
10050E	10300N	4801.5	353.34	676.59	2.10
10050E	10250N	4843.1	350.04	676.13	2.10
10050E	10200N	4898.8	346.01	676.12	2.10
10050E	10150N	4964.5	341.00	675.44	2.10
10050E	10100N	5030.2	335.77	674.65	2.10
10050E	10050N	5050.0	334.41	674.43	2.10
10200E	10050N	5036.0	334.67	673.95	2.10
10200E	10100N	4973.9	339.92	675.27	2.10
10200E	10150N	4882.6	346.89	676.50	2.10
10200E	10200N	4796.0	353.52	677.15	2.10
10200E	10250N	4708.9	359.41	677.12	2.10
10200E	10300N	4629.2	364.87	676.96	2.10
10200E	10350N	4552.2	369.76	676.49	2.10
10200E	10400N	4525.3	371.58	676.34	2.10
10200E	10450N	4505.3	372.91	676.28	2.10
10200E	10500N	4464.9	375.44	676.04	2.10
10150E	10500N	4541.4	370.67	676.46	2.10
10150E	10450N	4587.1	367.68	676.44	2.10
10150E	10400N	4619.4	365.48	676.48	2.10
10150E	10350N	4624.9	365.18	676.52	2.10
10150E	10300N	4649.1	363.49	676.67	2.10
10150E	10250N	4713.9	359.14	676.84	2.10
10150E	10200N	4797.8	353.36	676.96	2.10
10150E	10150N	4878.3	347.44	676.48	2.10
10150E	10100N	4952.0	342.00	675.88	2.10
10150E	10050N	5045.3	334.28	674.29	2.10
10250E	10050N	4963.1	340.30	674.54	2.10
10250E	10100N	4910.5	344.94	675.82	2.10

LINE	STN	ELEV.	OBS.GRAV.	BOUG.GRAV.	B.DENSITY
10250E	10150N	4840.6	350.36	676.76	2.10
10250E	10200N	4768.7	355.57	677.06	2.10
10250E	10250N	4693.1	360.72	677.18	2.10
10250E	10300N	4623.4	365.43	677.18	2.10
10250E	10350N	4549.2	370.05	676.74	2.10
10250E	10400N	4471.0	374.75	676.01	2.10
10250E	10450N	4425.9	377.46	675.54	2.10
10250E	10500N	4386.1	379.89	675.22	2.10
10300E	10050N	4872.9	347.72	675.73	2.10
10300E	10100N	4842.8	350.33	676.40	2.10
10300E	10150N	4790.6	354.22	676.89	2.10
10300E	10200N	4735.1	358.12	677.12	2.10
10300E	10250N	4681.1	361.76	677.15	2.10
10300E	10300N	4618.5	365.71	676.89	2.10
10300E	10350N	4551.1	369.51	676.09	2.10
10300E	10400N	4528.0	371.07	676.01	2.10
10300E	10450N	4484.3	373.86	675.85	2.10
10300E	10500N	4454.2	376.26	676.27	2.10
10400E	10500N	4661.2	361.93	675.90	2.10
10400E	10450N	4688.5	360.21	676.06	2.10
10400E	10400N	4759.9	355.23	675.78	2.10
10400E	10350N	4793.0	353.10	675.76	2.10
10400E	10250N	4792.4	353.87	676.37	2.10
10400E	10200N	4763.5	356.30	676.82	2.10
10400E	10150N	4750.1	357.52	677.12	2.10
10400E	10100N	4779.4	355.29	676.83	2.10
10400E	10050N	4773.9	355.19	676.39	2.10
10400E	10000N	4749.8	356.54	676.09	2.10
10400E	9950N	4732.0	357.24	675.64	2.10
10400E	9900N	4729.8	356.87	675.15	2.10
10400E	9850N	4717.8	357.34	674.76	2.10
10400E	9800N	4687.7	359.26	674.67	2.10
10400E	9750N	4690.6	358.87	674.40	2.10
10400E	9700N	4701.0	357.86	674.11	2.10
10400E	9650N	4698.8	357.32	673.59	2.10
10400E	9600N	4674.2	358.23	673.08	2.10
10400E	9550N	4617.0	361.72	672.92	2.10
10400E	9500N	4548.0	365.87	672.69	2.10
10400E	9450N	4466.3	371.27	672.70	2.10
10400E	9400N	4378.9	376.90	672.49	2.10
10400E	9350N	4288.5	382.79	672.34	2.10
10400E	9300N	4212.3	387.40	671.71	2.10
10400E	9250N	4121.1	393.28	671.25	2.10
10400E	9200N	4075.3	395.98	670.55	2.10
10400E	9150N	4039.6	398.22	670.32	2.10
10400E	9100N	3988.8	401.33	670.00	2.10
10400E	9050N	3930.3	404.77	669.59	2.10

APPENDIX B

VANGEOCHEM LAB LTD. 1521 PEMBERTON AVE., NORTH VANCOUVER, B.C., CANADA 604 986-5211 XXXXXXX
V7P 2S3

January 20, 1978

TO: Prism Resources Ltd.,
214 - 850 West Hastings Street,
Vancouver, B. C. V6C 1E1

FROM: Vangeochem Lab Ltd.,
1521 Pemberton Avenue,
North Vancouver, B. C. V7P 2S3

SUBJECT: Analytical procedure used to determine hot acid soluble Mo, Cu, Pb, Zn, Ag, and Cd in geochemical silt and soil samples.

1. Sample Preparation

(a) Geochemical soil or silt samples were received in the laboratory in wet-strength $3\frac{1}{2}$ x $6\frac{1}{2}$ Kraft paper bags.

(b) The wet samples were dried in a ventilated oven.

(c) The dried soil and silt samples were sifted by using a shaking machine with 80-mesh stainless steel sieves. The plus 80-mesh fraction was rejected and the minus 80-mesh fraction was transferred into a new bag for analysis later.

2. Methods of Digestion

(a) 0.50 gram of the minus 80-mesh samples was used. Samples were weighed out by using a top-loading balance.

(b) Samples were heated in a sand bath with nitric and perchloric acids (15% to 85% by volume of the concentrated acids respectively).

(c) The digested samples were diluted with demineralized water to a fixed volume and shaken.

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3. Method of Analysis

Mo, Cu, Pb, Zn, Ag, and Cd analyses were determined by using a Techtron Atomic Absorption Spectrophotometer Model AA4 or Model AA5 with their respective hollow cathode lamps. The digested samples were aspirated directly into an air and acetylene flame. The results, in parts per million, were calculated by comparing a set of standards to calibrate the atomic absorption unit.

4. The analyses were supervised or determined by Mr. Conway Chun and the laboratory staff.

Eddie Tang

Eddie Tang
VANGEOCHEM LAB LTD.

ET:mb

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PRISM JOINT VENTURE 1977 – 2

ZAP GRID

MAYO MINING DISTRICT, YUKON TERRITORY. NTS : 106 D-8

Outcrop Geology Map

DATE : Nov 78 FIGURE No : 2 DRAWN BY : G.C. SCALE : 1:2000

ZAP
GRID - B

TRUMPETER

ELITE

GRANDMA

THRILL

ZAP

5492

4000

4500

5000

3500

LEGEND

- 4 — Greenstone dyke
- 3 — Orthoquartzite, a) limy shaley, b) dolomite
- 2 — Grey dolomite, a) orange dolomite, b) black fossiliferous dolomite c) platey orange dolomite d) shale
- 1 — Shale

- geological contact
- fault contact
- 4000 — contour line
- creek
- geochemical grid area
- area of detailed mapping
- ⊙4 drill hole
- gn X mineral occurance
- gn galena
- sp sphalerite
- tt tetrahedrite
- ba barite
- Ⓕ fossil location

134°00'

64°15'

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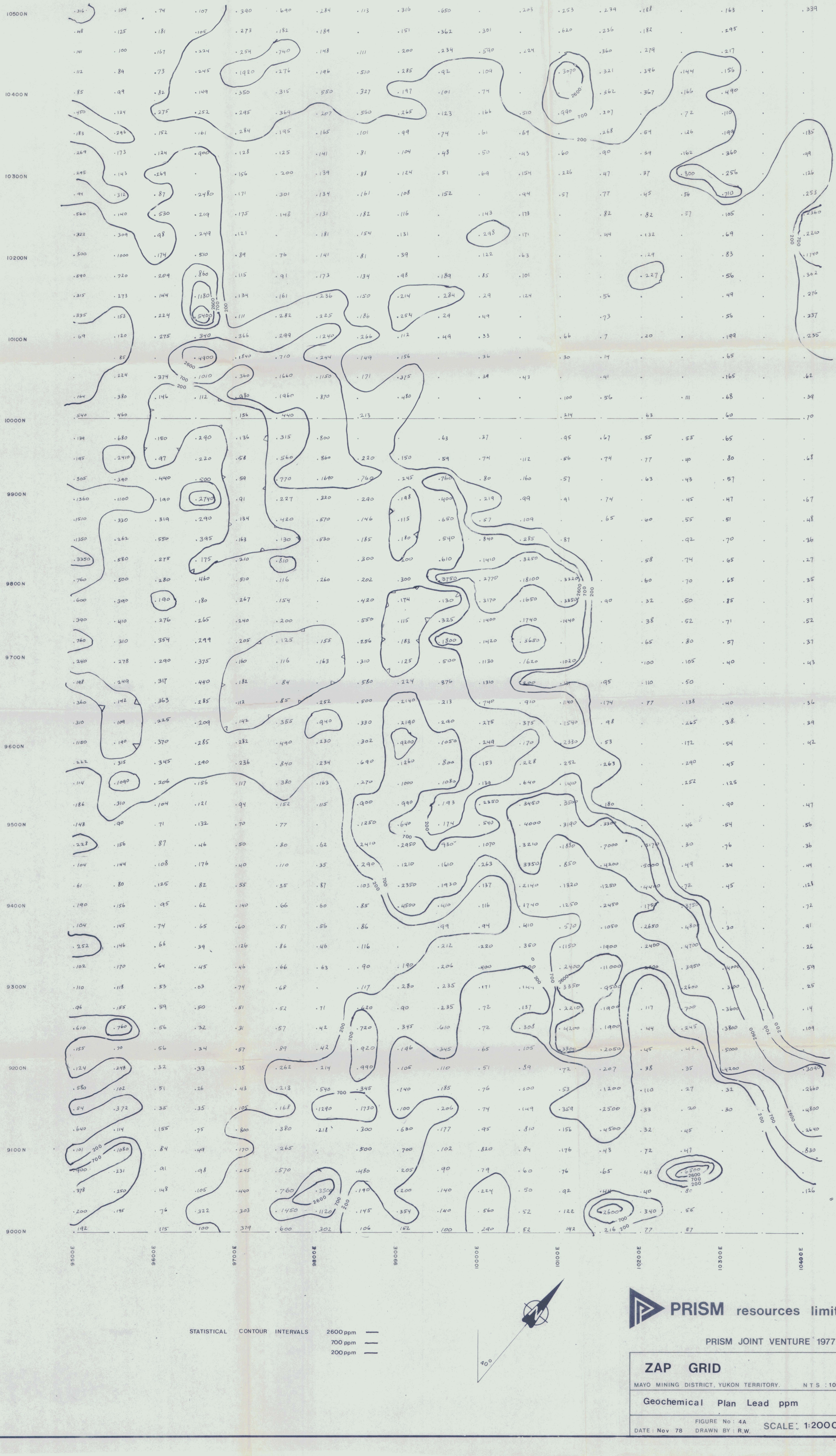
PRISM JOINT VENTURE 1977 - 2

ZAP GROUP

MAYO MINING DISTRICT, YUKON TERRITORY. N.T.S. : 106 D-8

Geology Map

DATE : Nov 78 FIGURE No : 3 DRAWN BY : G.C. SCALE : 1:10,000


10500N
10400N
10300N
10200N
10100N
10000N
9900N
9800N
9700N
9600N
9500N
9400N
9300N
9200N
9100N
9000N
9500E
9600E
9700E
9800E
9900E
10000E
10100E
10200E
10300E
10400E
2600
700
200
STATISTICAL CONTOUR INTERVALS
2600 ppm
700 ppm
200 ppm
40°
PRISM resources limited
PRISM JOINT VENTURE 1977 - 2
ZAP GRID
MAYO MINING DISTRICT, YUKON TERRITORY. NTS : 106-8
Geochemical Plan Lead ppm
FIGURE No : 4A
DATE : Nov 78
DRAWN BY : R.W.
SCALE : 1:2000

10500N
10400N
10300N
10200N
10100N
10000N
9900N
9800N
9700N
9600N
9500N
9400N
9300N
9200N
9100N
9000N
9500E
9600E
9700E
9800E
9900E
10000E
10100E
10200E
10300E
10400E
1000
2000
4500
300
CONTOUR INTERVALS
4500 ppm
2000 ppm
1000 ppm
300 ppm
statistically determined contour interval
40°
PRISM resources limited
PRISM JOINT VENTURE 1977 - 2
ZAP GRID
MAYO MINING DISTRICT, YUKON TERRITORY.
NTS : 106-8
Geochemical Plan Zinc ppm
FIGURE No : 4B
DATE : Nov 78
DRAWN BY : R.W.
SCALE : 1:2000

10500N
10400N
10300N
10200N
10100N
10000N
9900N
9800N
9700N
9600N
9500N
9400N
9300N
9200N
9100N
9000N
9500E
9600E
9700E
9800E
9900E
10000E
10100E
10200E
10300E
10400E
CONTOUR INTERVALS
10.0 ppm
5.0 ppm
3.0 ppm
statistically determined contour interval
40°
PRISM resources limited
PRISM JOINT VENTURE 1977 - 2
ZAP GRID
MAYO MINING DISTRICT, YUKON TERRITORY.
NTS : 106-8
Geochemical Plan Silver ppm
FIGURE No : 4C
DATE : Nov 78
DRAWN BY : R.W.
SCALE : 1:2000

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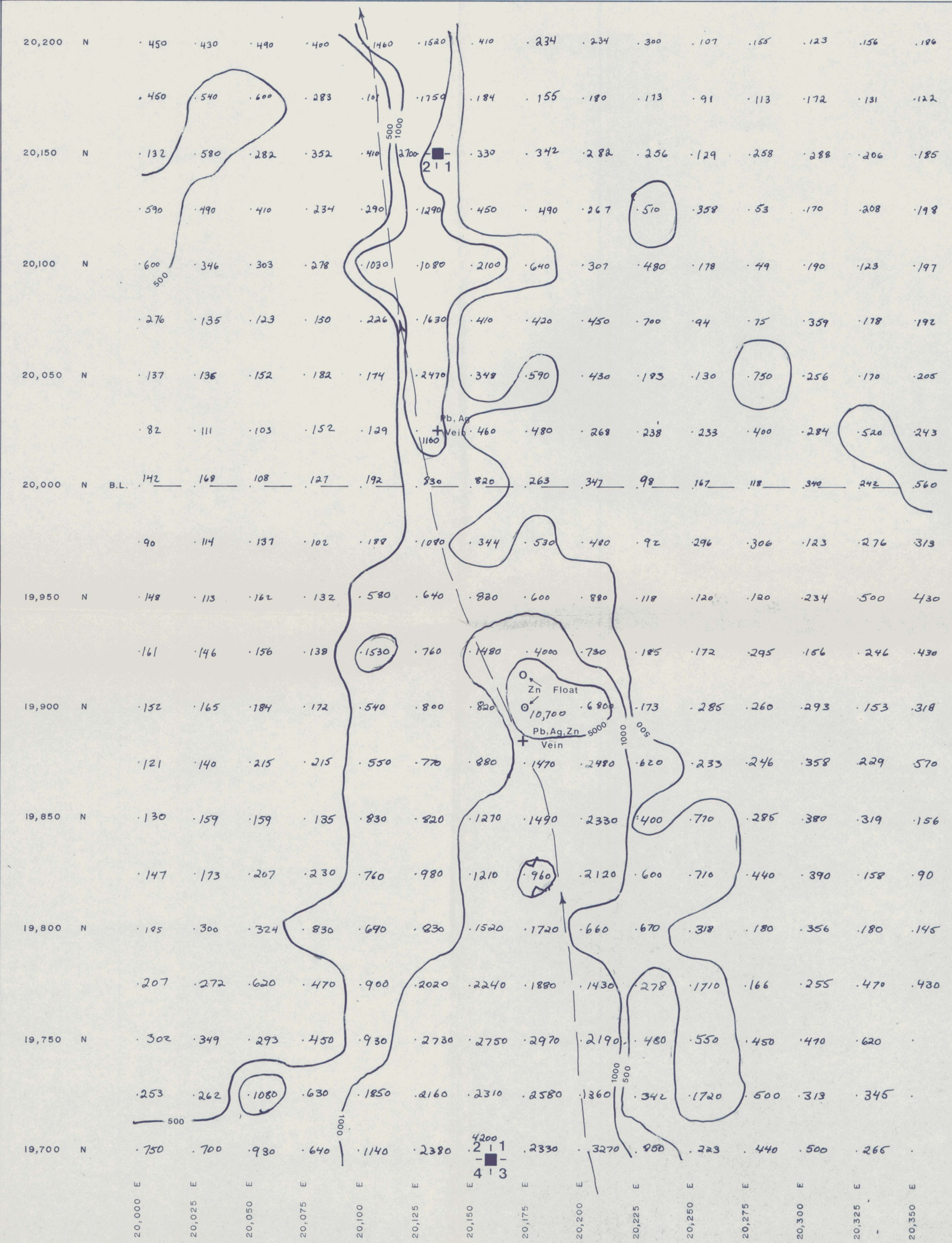

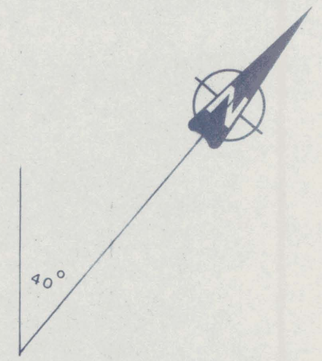

CONTOUR INTERVALS
5000 ppm
1000 ppm
500 ppm

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PRISM JOINT VENTURE 1977 - 2

ZAP B Grid

MAYO MINING DISTRICT, YUKON TERRITORY. NTS : 106D/8

Geochemical Plan ZINC ppm

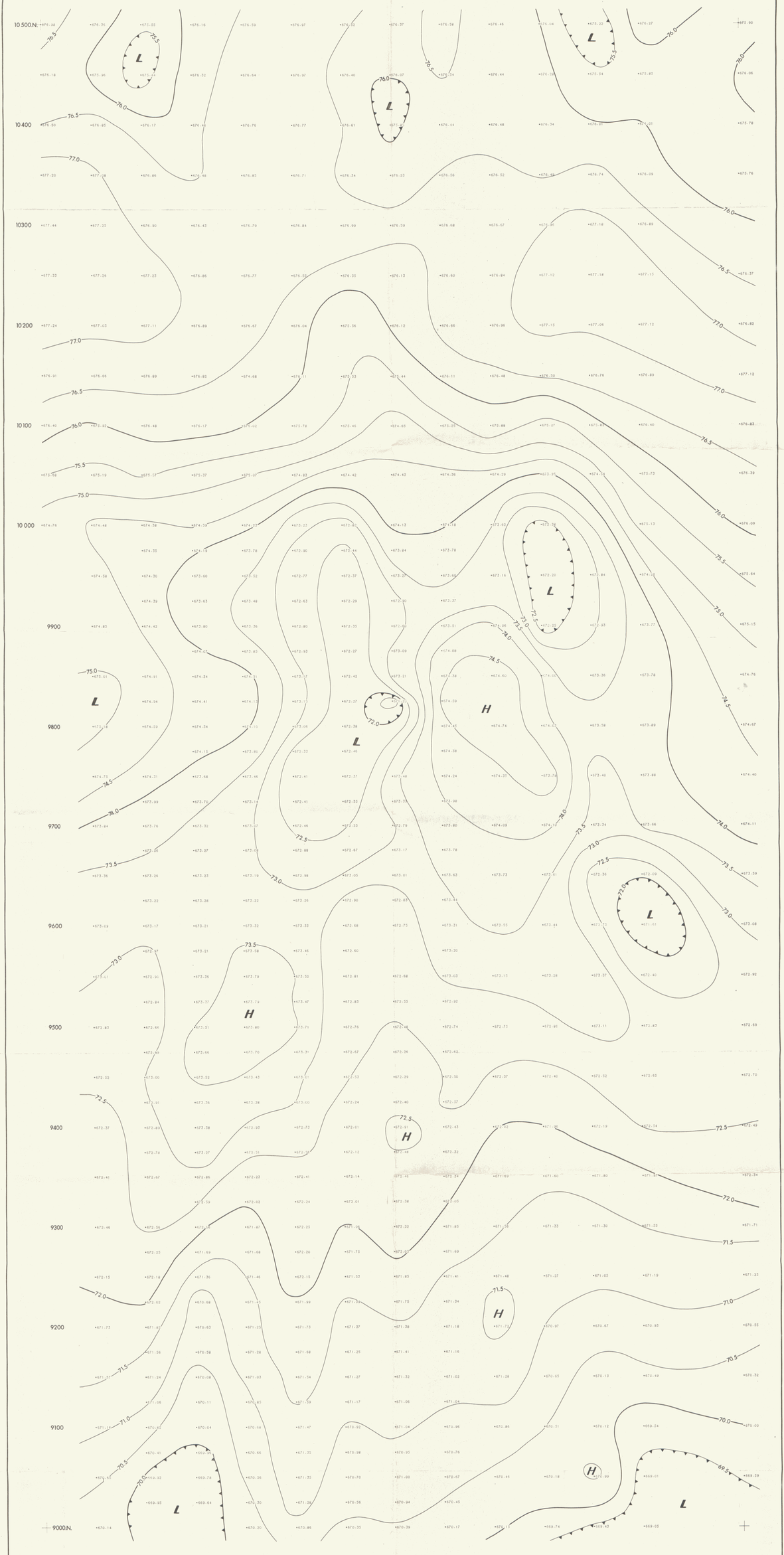
FIGURE No : 5B

DATE : Nov 78 DRAWN BY : G.C.

SCALE : 1 : 1250

20,200	N		2.0	2.2	2.4	1.6	2.7	3.8	3.0	1.7	1.2	2.7	1.9	2.5	2.8	2.0	2.0
			2.3	2.2	2.2	1.6	1.6	3.8	1.1	1.2	1.4	0.8	0.8	1.0	2.0	2.6	2.0
20,150	N		0.8	1.8	2.1	1.2	1.8	3.4	1.7	2.2	1.3	1.7	1.1	1.7	1.3	2.2	2.6
			1.6	1.9	1.9	0.8	1.5	3.0	2.0	2.3	2.4	1.6	3.1	1.2	1.4	1.6	2.0
20,100	N		1.8	1.5	1.6	0.9	2.8	2.8	2.4	2.9	2.8	2.0	1.6	1.4	1.6	1.9	2.0
			1.6	1.1	1.4	0.9	1.1	3.6	2.0	2.5	2.6	4.8	1.1	1.6	1.5	1.2	3.7
20,050	N		1.1	1.2	1.6	1.1	1.2	4.5	2.0	4.4	2.9	1.2	1.5	5.4	2.3	1.3	2.0
			0.6	1.6	1.2	1.2	1.3	2.8	2.0	2.9	2.2	0.8	2.3	3.4	3.0	3.8	2.4
20,000	N	B.L.	1.2	2.0	1.6	1.2	1.3	3.1	2.8	1.2	2.4	0.5	1.2	1.1	2.1	1.9	3.0
			1.0	1.6	1.7	1.3	1.4	3.2	2.4	2.6	2.4	0.6	1.7	3.2	1.1	2.1	2.7
19,950	N		1.3	1.8	2.0	1.4	1.8	2.2	3.6	2.6	2.2	0.5	0.7	1.1	2.3	3.5	3.1
			1.1	1.6	1.9	1.3	1.8	2.6	3.0	4.8	2.4	1.9	1.3	2.3	0.9	1.8	4.0
19,900	N		0.9	1.5	1.9	1.3	2.4	2.5	3.6	11.4	26.0	0.8	3.0	3.1	2.2	1.7	3.0
			0.8	1.4	1.7	1.2	2.3	2.6	2.8	3.6	9.0	1.5	2.2	2.5	2.4	3.0	4.1
19,850	N		0.8	1.6	1.2	1.2	2.7	2.4	3.3	3.5	2.9	2.0	3.0	2.4	2.2	1.8	2.5
			1.1	1.2	1.3	1.4	2.5	2.8	2.6	2.6	3.8	2.2	3.7	2.6	2.2	1.6	3.0
19,800	N		1.3	1.7	1.6	2.0	2.1	2.7	3.7	3.3	2.2	3.4	2.8	2.2	3.3	1.1	1.4
			1.5	1.5	2.6	1.6	2.8	4.0	3.8	4.7	2.7	1.5	3.9	1.7	1.9	3.1	2.6
19,750	N		1.2	2.0	1.7	1.9	2.6	4.4	4.0	4.4	5.8	1.9	2.6	2.9	2.6	3.0	
			0.8	1.8	3.6	2.3	3.2	5.2	5.3	4.2	4.2	2.0	3.2	2.3	1.8	2.2	
19,700	N		2.4	2.8	3.3	2.4	3.4	4.0	3.5	4.4	1.7	1.6	2.3	2.7	1.3		
			20,000 E	20,025 E	20,050 E	20,075 E	20,100 E	20,125 E	20,150 E	20,175 E	20,200 E	20,225 E	20,250 E	20,275 E	20,300 E	20,325 E	20,350 E

3.0 3.0 3.0



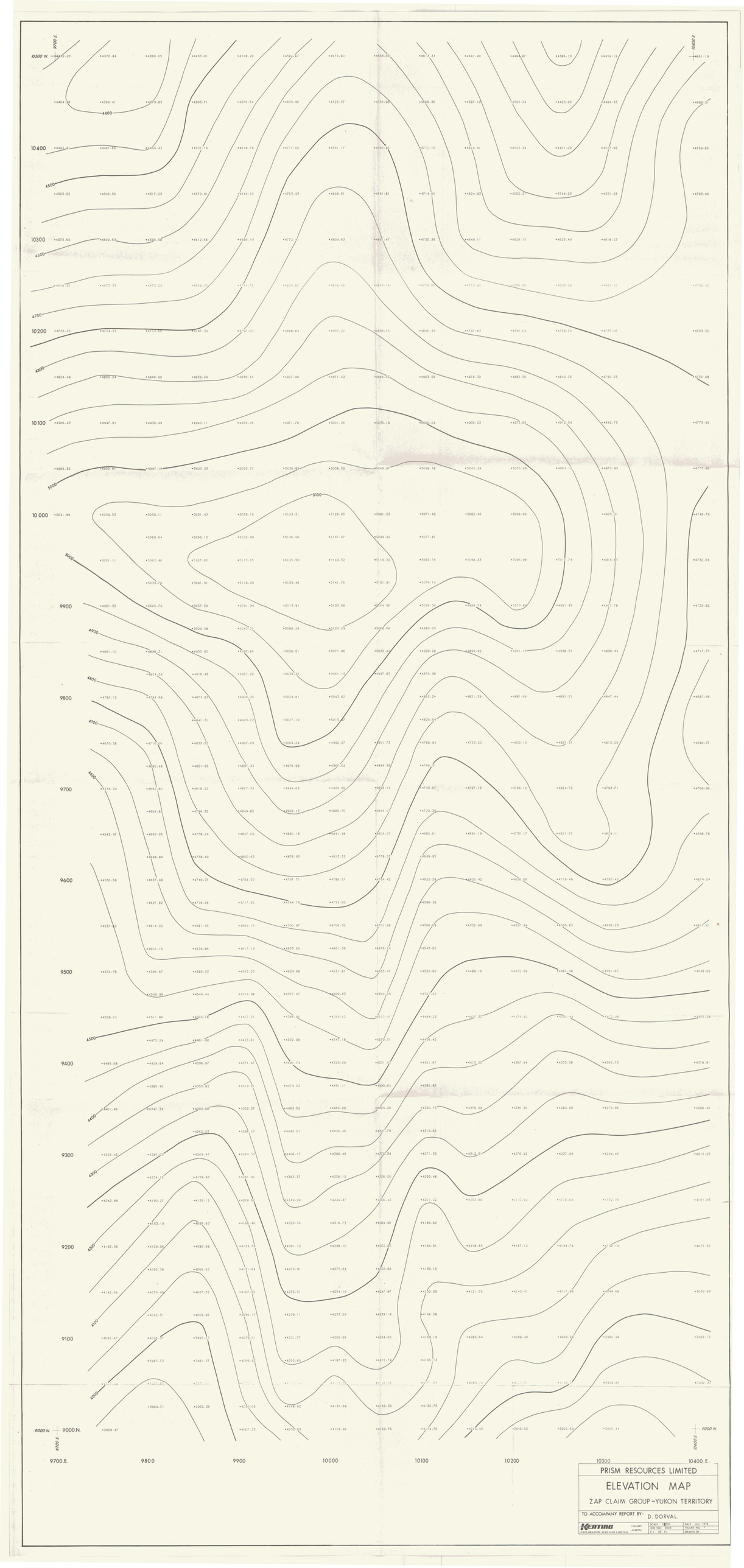
PRISM RESOURCES LIMITED

BOUGUER GRAVITY SURVEY

ZAP CLAIM GROUP – YUKON TERRITORY

TO ACCOMPANY REPORT BY: D. DORVAL.

KENTING EXPLORATION SERVICES LIMITED	CALGARY ALBERTA	SCALE 1:2000	DATE JULY 1975
		JOB NO. 5119	FIGURE NO. 7
		C.I. 0.5 mGals	DRAWN BY



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ELEVATION MAP

ZAP CLAIM GROUP - YUKON TERRITORY

TO ACCOMPANY REPORT BY: D. DORVAL.

Kenting EXPLORATION SERVICES LIMITED	CALGARY ALBERTA	SCALE 1:500	DATE JULY 1978
		JOB NO. 1826	FIGURE NO. 7
		C.I. 20 ft.	DRAWN BY

PRISM RESOURCES LIMITED

RESIDUAL GRAVITY SURVEY

ZAP CLAIM GROUP - YUKON TERRITORY

TO ACCOMPANY REPORT BY: D. DORVAL.

KENTING EARTH SURVEYS LIMITED — CALGARY, ALBERTA

SCALE : 1:5000	DATE JULY 1978
JOB NO. 7836	FIGURE NO. 8
C.I. 0.25 mgals.	DRAWN BY TM