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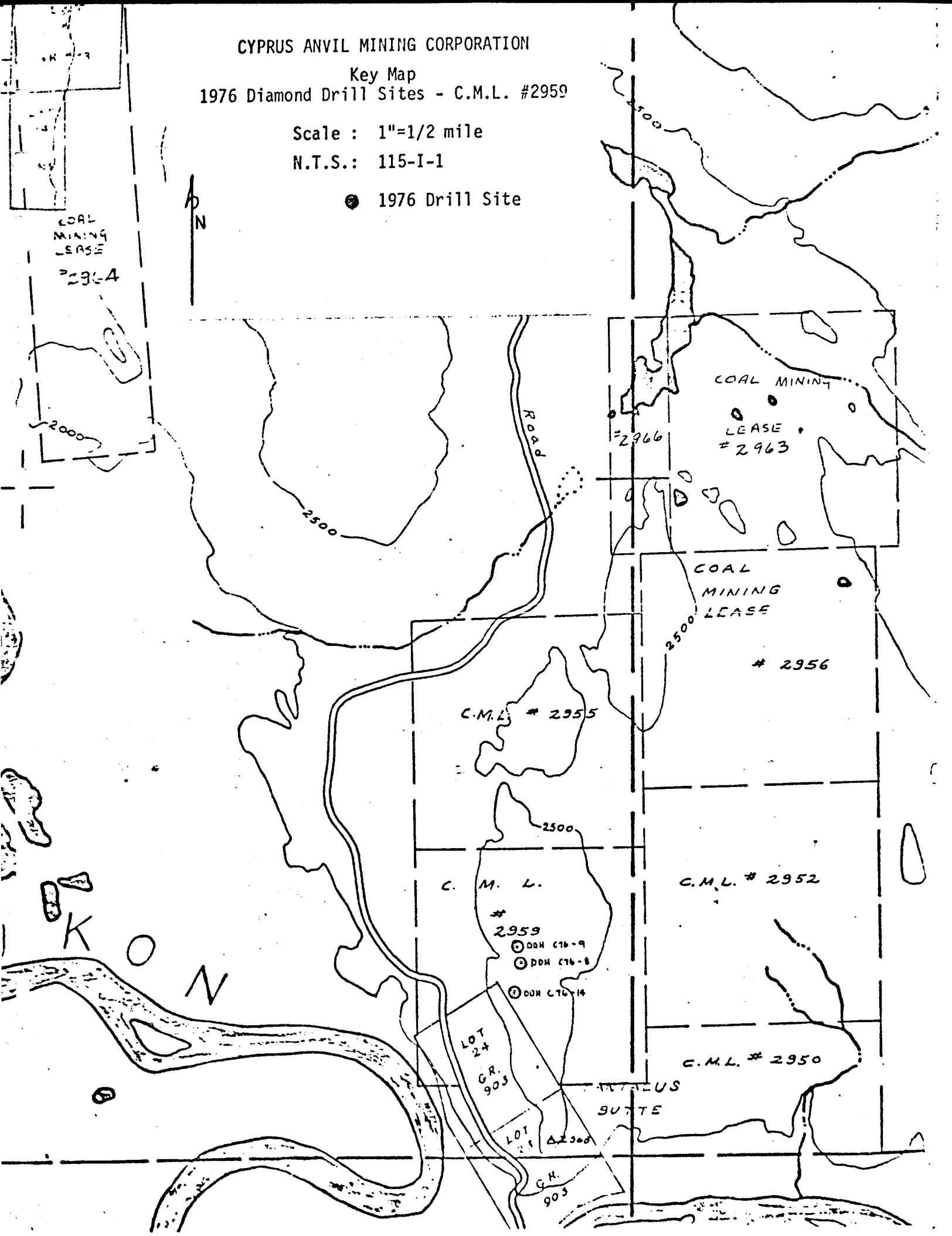
CYPRUS ANVIL MINING CORPORATION

Key Map
1976 Diamond Drill Sites - C.M.L. #2959

Scale : 1"=1/2 mile

N.T.S.: 115-I-1

● 1976 Drill Site



COAL MINING LEASE #2964

COAL MINING LEASE #2963

#2966

COAL MINING LEASE #2956

C.M.L. # 2955

C.M.L. # 2952

C. M. L. # 2959

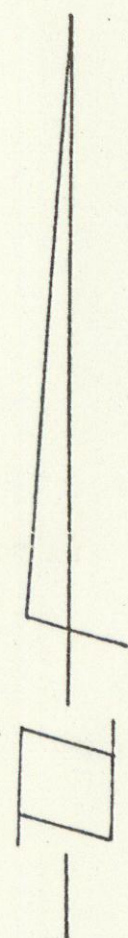
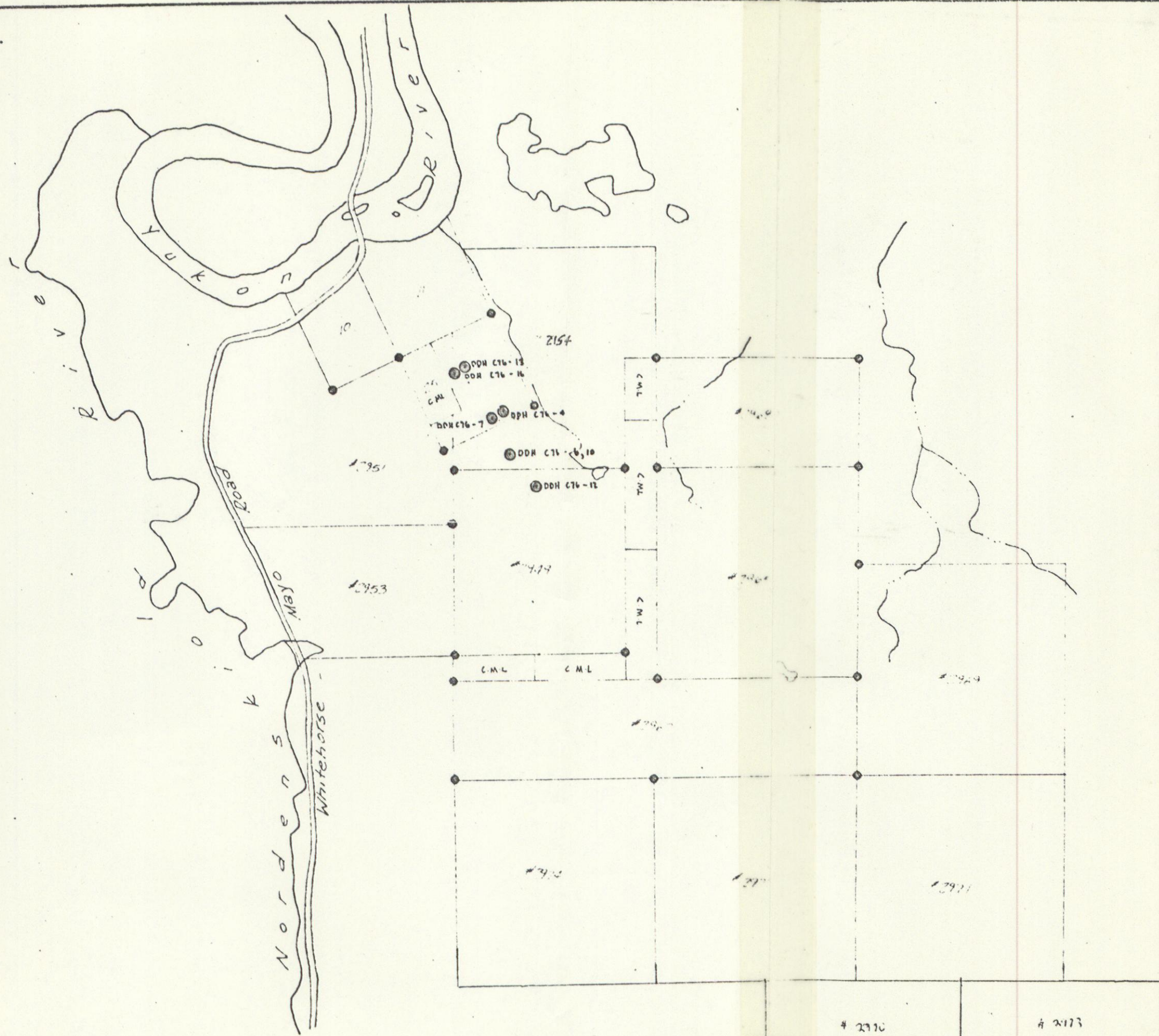
- DDH C16-9
- DDH C16-8
- DDH C16-14

C.M.L. # 2950

LOT 24 GR. 905

LOT 25 GR. 905

TRACUS SUITE



CYPRUS ANVIL MINING CORPORATION
 Key Map
 1976 Diamond Drill Sites - C.M.L. #2949, 2954

Scale : 1"=1/2 mile
 N.T.S.: 115-I-1

- 1976 Drill Sites
- Targets Placed for Aerial Photographs

2910

2913

CYPRUS ANVIL MINING CORPORATION

CARMACKS COAL PROJECT

1. IMMEDIATE AND POTENTIAL DEMAND FOR COAL

A. Supply of Coal for Anvil Mine

The annual consumption of coal at Faro for plant heating and concentrate drying is approximately 25,000 tons.* Stock in hand and measured, developed reserves within the present underground operation at Tantalus Butte are sufficient to supply this demand for a maximum of three years. If plant heating and concentrate drying operations are to remain coal-fired, and assuming Anvil has a life-of-mine of ten years from now, an additional 25,000 tons per year (175,000 tons over seven years commencing 1980) must be found.

B. Supply of Coal for Other Customers

Kerr-Addison Mines and Asarco-Silver Standard have approached Cyprus Anvil concerning the possibility of supplying coal for similar purposes for the Grum deposit and Minto deposit respectively. Assuming that these operations will require similar tonnages to Anvil, potential markets exist for an annual production of an additional 50,000 tons (i.e. 500,000 tons over ten years, commencing in approximately 1979). If coal can be mined at Carmacks with an operating profit of between \$10 and \$20 per ton, annual sales of 50,000 tons could result in an annual profit to the company of between \$0.5 and \$1 million. Anvil, Grum and Minto deposits would require an aggregate annual output of about 75,000 tons (total of 675,000 over ten years commencing 1979).

C. Power Generation

It has been calculated that a thermal power station installed at Faro with sufficient capacity to supply the Faro townsite, the Anvil Mine and the Grum deposit would require approximately 120,000 tons of coal per year (1,200,000 tons over ten years commencing in 1979). It is possible that such an installation would result in substantial savings in energy costs to the company over the proposed ten-year period.

D. Summary

Immediate and potential demand for coal for Anvil, Grum and Minto deposits and power generation at Faro would require about 1,875,000 tons over ten years, commencing approximately 1979. Such an output could result in a direct annual profit of between \$0.5 and \$1 million, plus substantial savings in energy costs at Faro.

2. 1976 EXPLORATION PROGRAM

A. Summary of Results

(i) Carmacks North

Diamond drilling has indicated that the "main seam" probably extends down dip to river level beneath the present underground

* All tonnage figures are short tons.

workings at Tantalus Butte for much of their length. Assuming a strike length of 3,500 feet, down dip extent of 500 feet (dipping at 45°), average seam thickness of 8 feet, coal density of 1.1 tons/cubic yard and 50% recovery, this information indicates underground reserves of approximately 285,000 tons. (Note: - with the present limit of drilling information, these reserves cannot be regarded as proven.) Extraction of these reserves would require a new portal at river level.

In the same area, two or three coal seams were penetrated above the main seam in some holes. One of these seams may be the "hangingwall seam". Each of these seams appears to be discontinuous, relatively thin (5 feet or less) and of poor quality. No reserves have been calculated for these seams owing to insufficient data.

In the area immediately to the north of the present northern extent of the underground workings, diamond drilling has indicated that the geological structure becomes very complicated, including tight folds and faulting. It is interpreted that in the vicinity of the "north cross-cut" (approximately at grid line 14,600N) the underground workings hit a fault zone, and the main entry passed from the "main seam" into another seam some distance stratigraphically below it (possibly the "foot-wall seam"). This lower seam may have been penetrated at the bottom of hole C-76-5, with the main seam above it. Alternatively, the main seam may be repeated by folding and/or faulting. Present information is inconclusive on these points. General indications are that a northward extension of the present workings would not be feasible without considerable additional surface drilling and underground development.

Detailed field mapping, trenching and limited diamond drilling in the open pit area have shown that the pit itself occupies a narrow, tight syncline complicated by high-angle strike faulting. Indications are that this syncline extends for several hundred feet to the south, and thus surface-mineable reserves may be present in this area. Any such mining operation would require the removal of substantial overburden, and hence mining would be more expensive than last year's operation. Reserves in this area have been very roughly calculated at 40,000 tons at a stripping ratio of about 5:1 over a strike length of 300 feet. This would cost about \$20/ton.

In the area to the north of the open pit, the main seam appears to resume a regular westerly dip, and has been traced over a strike length of about 1,400 feet. This will have to be verified by drilling. Assuming a distance down dip between surface and river level of 1,100 feet, an average seam thickness of 8 feet, coal density of 1.1 tons/cubic yard and 50% recovery, this area could hypothetically yield, by underground mining, approximately 251,000 tons. Such an operation would require either a vertical or steeply-inclined shaft or a tunnel driven in from the west, both of which would be extremely expensive. An open pit extending 100 feet down dip with 80% recovery could hypothetically yield about 36,000 tons of coal, at a stripping ratio of about 10:1.

All analyses of coal from Carmacks North indicate a thermal coal of good quality without coking characteristics (approximately 12,000 B.T.U./lb.; average of 13% ash).

(ii) Carmacks South

Trenching and diamond drilling along the ridge extending south-eastwards from the site of the old Tantalus Mine has proved the presence of a coal seam varying in thickness from ten to fifty feet over a strike length of 6,600 feet. This seam is present on the western limb of a deep syncline, which is apparently overturned towards the east. At the highest elevations, the seam dips about 50° east, but at depth it apparently steepens beyond verticality and dips up to 70° west. Indications are that the seam is lenticular, and thins rapidly with depth. Reserves in this area have been roughly calculated at 500,000 tons at a stripping ratio of about 10:1. Such a situation would be very unfavourable towards a small-scale open pit designed merely to supply Anvil, but may lend itself to a large-scale operation.

Stratigraphic information indicates that this coal horizon is not the same horizon as that mined at Tantalus Butte, and may not be the same horizon which was formerly mined at the old Tantalus Mine. It is more probably a lower horizon, within the uppermost part of the Laberge Formation, and hence is probably the same seam which was formerly mined at Five Fingers Mine. Many analyses of coal from this area indicate good coking characteristics (F.S.I. between 4½ and 7) and calorific values of about 11,000 B.T.U./lb., but ash contents up to 50%. Washing samples to 8% ash raised F.S.I. to about 8 and calorific values to 14,000 B.T.U./lb., but with low yields (30 to 50%). Some samples have comparable analyses but lack coking characteristics.

The eastern limb of the syncline has not been found, and may be present beyond the eastern limit of the property. Additional leases should be staked here immediately. Adjacent to the syncline on the west is an anticline; the western limb of the anticline has been located, but so far coal has not been found here.

B. Additional Inferences

- (i) The most important single result of the 1976 program has been the discovery that two coal horizons may be present. The upper horizon, on the northern property, consists entirely of thermal coal while the lower horizon, on the southern property, consists predominantly of coking coal. There therefore exists the potential for locating the lower horizon on the northern property and the upper horizon on the southern property, thereby increasing reserves of both types of coal.

If the lower horizon is present on the northern property, it should outcrop just below the Laberge/Tantalus contact in the valley to the east of Tantalus Butte. If the upper horizon is present on the southern property, it should outcrop on both limbs of the syncline, east of the known seam outcrop.

- (ii) At the northern end of the northern property, information from a couple of outcrops could be interpreted to indicate that the Tantalus Formation rocks are folded by an anticline-syncline pair, with the syncline on the east. Over most of this eastern area there are no exposures, and such a hypothesis could only be tested by geophysical methods or by drilling. If such a syncline is present, there is the potential for substantial reserves in this area.
- (iii) On the southern property, the total strike length of the known coal seam is not known. If this seam trends around the southern closure of the syncline and northwards along its eastern limb, there exists the potential for an additional strike length of 40,000 feet. If the seam is present along the western limb of the anticline, there exists the potential for an additional strike length of 8,000 feet. This additional strike length gives the potential for an additional 3,600,000 tons of open pit coal at a stripping ratio of about 10:1.
- (iv) With the present extent of information, the total reserves of coal within the property may be summarized as follows:-

Measured reserves	- 30,000 tons (within present underground mine).
Inferred reserves	- 285,000 tons (beneath present workings). - 40,000 tons (open pit area). - 500,000 tons (known open pit coal on southern property).
Hypothetical reserves	- 3,600,000 tons (additional strike length on southern property). - 251,000 tons (additional strike length on northern property, including 36,000 tons open pit).
Speculative reserves	- Unknown (includes potential for syncline east of Tantalus Butte Mine, and presence of lower horizon in north and upper horizon in south).

Total potential reserves - Minimum of 4,706,000 tons.

3. CONCLUSIONS

- A. To assure supplies of coal for the Anvil Mine over the next ten years, an additional 175,000 tons must be raised from the inferred category to the measured category. At the present level of information, the most promising areas are beneath the present underground workings, in the open pit area, and the known coal seam on the southern property. Each of these areas will require substantial additional drilling to provide sufficient information to allow mining to proceed (roughly estimated at \$100,000 per year over the next five years or so).

- B. To assure supplies of coal for the Grum and Minto deposits, an additional 500,000 tons must be raised from the inferred category to the measured category. The most promising areas are those outlined above. Substantial additional exploration will be required, roughly estimated at \$200,000 per year over the next five years or so.
- C. To assure supplies of coal for the proposed power station in Faro, an additional 1,200,000 tons of coal must be raised from the hypothetical category to the measured category. Substantial additional exploration will be required, roughly estimated at \$200,000 per year over the next five years or so.
- D. Present information is sufficient to indicate a high probability that these demands can be met, given sufficient additional exploration. Such exploration must, out of necessity, be carried out over the next two years before we are in a position to know whether or not we can supply enough coal to meet the demands of the Anvil Mine, the Grum and Minto deposits, and the proposed power station in Faro.
- E. With available information, a few promising areas have been outlined. However, we do not know if these are the best areas, i.e. other more attractive mining situations may be present. In addition, the total potential of the property as a whole is largely unknown, but could be considerable (e.g. it would be unwise to use a potential metallurgical coal as thermal coal until the potentiality of mining metallurgical coal as such has been fully explored).
- F. Any further exploratory and development work on the Carmacks coal leases must take the form of three parallel courses of action:-
 - (a) assuring the supply of coal for the Anvil Mine,
 - (b) estimating the capability of supplying coal for the Grum and Minto deposits and the proposed power station in Faro,
 - (c) outlining the potential of the property as a whole for future marketing considerations.

4. RECOMMENDATIONS

An extensive exploration programme for 1977 is proposed, consisting of the following work:

A. Photogrammetry

Some additional photogrammetry is required to upgrade the standard of topographic mapping in the areas of active exploration (estimated expenditure approximately \$25,000).

B. Geophysics

Lack of exposure over most of the property would result in a very considerable expense in diamond drilling to provide the necessary information, hence every effort must be made to employ geophysical

methods to locate coal seam suboutcrops and help outline structures. Of the methods which have been tried to date, C.E.M. appears to offer the most potential, and V.L.F.-E.M. and scintillometer surveys may give promising results. Methods which have not yet been tried are seismic and gravity surveys. An extensive programme of geophysical experimentation and surveying is proposed (estimated expenditure approximately \$50,000).

C. Drilling

Total contract cost for diamond drilling in 1976 was slightly under \$30 per foot, and this is considered to be very high for the amount of information obtained. Thus an attempt will be made to substitute rotary-percussion drilling for diamond drilling, at least for a large part of the work. Such a move should result in a lowering of drilling costs by at least 50%. Geophysical logs would be run on rotary holes, resulting in a comparatively small loss of information brought about by the loss of core, and the coal seams themselves could still be cored for analytical work.

A programme of exploratory drilling is proposed, primarily concerned with outlining measured reserves for the short-term supply of coal for Anvil, and secondarily concerned with increasing structural and stratigraphic control over larger areas of the property. Sites of some of the proposed holes are shown on the accompanying maps.

1. Six holes in the open pit area (total 1,200 feet) to test the width, depth and southerly extent of the syncline and to assess the feasibility of extending the pit. These holes must be drilled this year in order to determine whether or not this area can produce coal when the present supply is exhausted (see Figure 1).
2. One additional hole on the section immediately north of the present underground workings (700 feet), to resolve present uncertainty about the geological structure and assess the feasibility of a northward advance of the existing underground workings. Since stratigraphic information is critical at this location, diamond drilling is proposed for this hole (see Figure 2).
3. Two additional holes to test the down dip extent of the main seam beneath the underground workings (1,400 feet). These holes would be particularly necessary if the drilling outlined in 1 and 2 above should fail to locate readily accessible coal. If it should be decided before the summer that a second, lower portal is not feasible, then this footage could very usefully be employed in the open pit area since it is possible that the syncline is accompanied by an anticline on the west which may yield additional surface reserves.
4. On the southern property, drilling information is confined to a strike length of 3,600 feet over a narrow width. The most satisfactory method of exploring this property further is to

step away from this area, and probe a larger prospective area with holes at spacings of approximately 1 mile. Siting of such holes would be contingent upon satisfactory geophysical results. It is considered that a minimum of 4,000 feet of diamond drilling (8 holes of 500 feet) would be required. Should a rotary rig become available, it is probable that we could at least double the footage for the same cost.

A total expenditure for drilling of approximately \$190,000 is anticipated.

Total expenditure for the proposed programme would be approximately \$300,000.

Respectfully submitted,



Roderic P. Hill

January, 1977

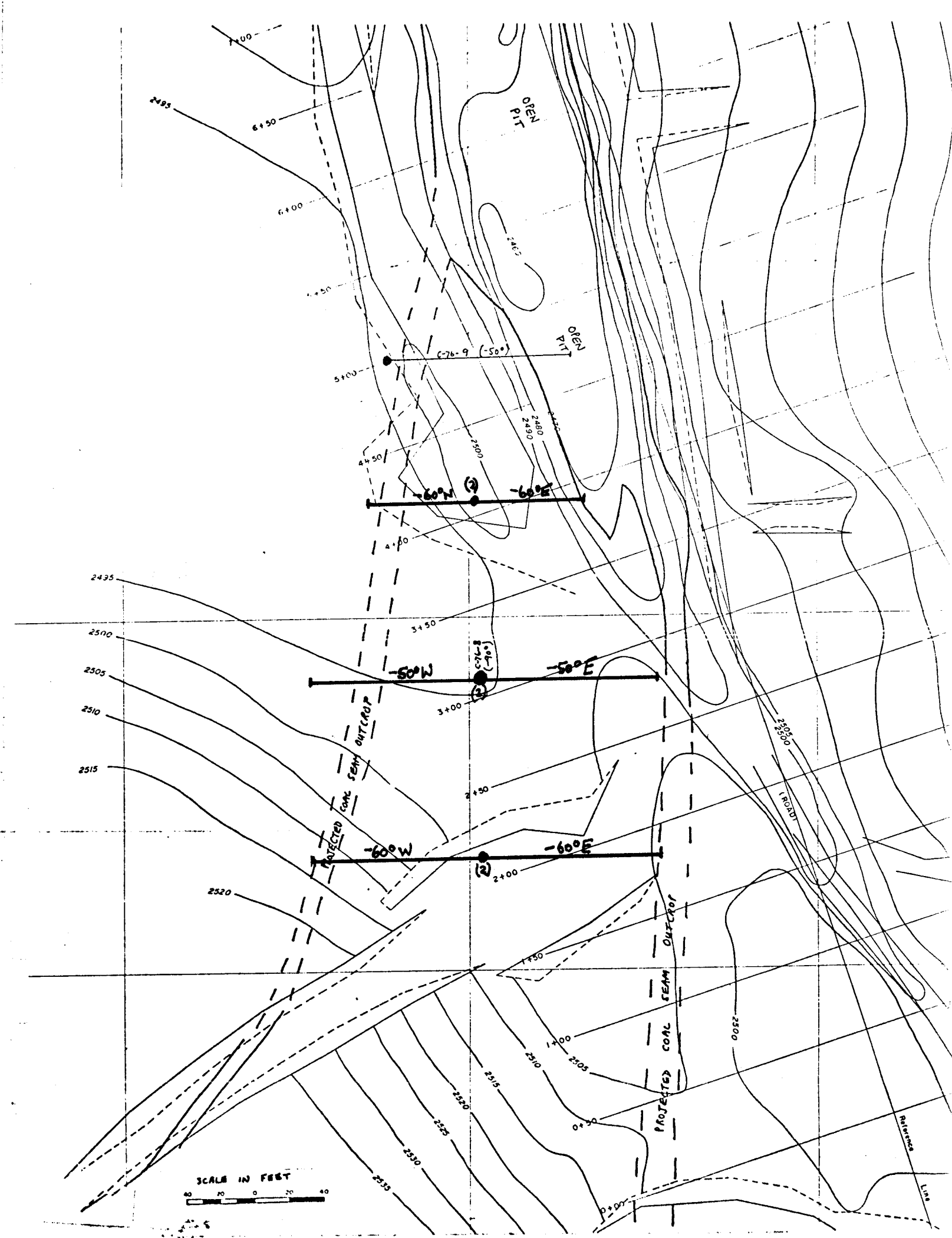
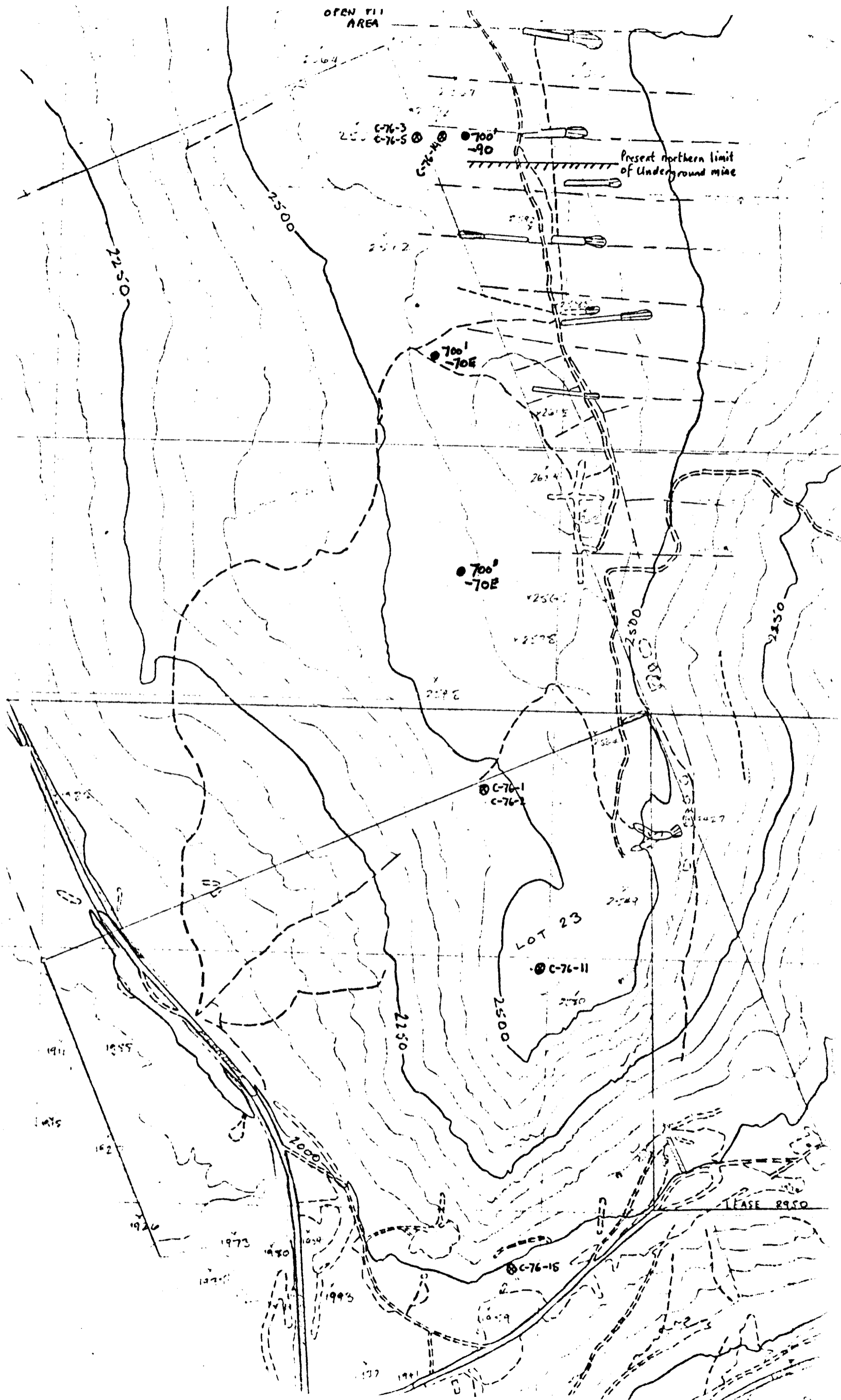


FIGURE 1.
 CARMACKS NORTH
 OPEN PIT AREA

—60°E— PROPOSED HOLES, 1977



APPENDIX I - DRILL LOGS

COLLAR:		HOLE SURVEY		
NORTH _____	FOOTAGE	AZIMUTH	DIP	
EAST _____				
ELEVATION _____				
LOGGED BY _____				
DATE LOGGED _____				
MAP REFERENCE NO. _____	METHOD:			

Diamond Drill Record

COMPANY NAME _____
 PROPERTY NAME _____
 DRILLING CONTRACTOR _____
 ASSAYER _____
 PURPOSE OF HOLE _____

PAGE 4 OF 7

HOLE NO.	C-76-7
CLAIM NAME	_____
COMMENCED	_____
FINISHED	_____
PROJECT NO.	_____

FROM	TO	RECOVERY	DESCRIPTION	SAMPLE				ASSAYS					
				FROM	TO	WIDTH	NO.						
242	257	~80%	Pebbly sandstone; as 240-242; 20% pebbles up to 1" diameter; core angle at 240'~30°; conglomerate layers present.										
257	278	~90%	Conglomerate - as above; ~80% pebbles up to 1" diameter; core angle at 265'~60°.										
278	282	~40%	Sand - poor recovery; brown to light grey; soft.										
282	295	~80%	Conglomerate - as above; 80-90% pebbles up to 2" diameter; core angle at 287'~20°.										
295	295.5	~90%	Sandstone - fine-grained; soft; brownish-grey; no distinct bedding.										
295.5	328	~90%	Conglomerate - as above; 70-90% pebbles up to 2" diameter; core angle at 307'~65°; at 327'~60°.										
328	337	~90%	Pebbly sandstone - light grey; coarse-grained; 0-40% pebbles up to 2" diameter; small conglomerate layer present.										
337	345	~90%	Conglomerate - as above; ~90% pebbles up to 2" diameter.										
345	346	~90%	Pebbly sandstone - light grey; medium grained; 5% pebbles up to 1" diameter; core angle at 345'~40°.										
346	353	~90%	Conglomerate - as above; ~70% pebbles up to 1/2" diameter.										
353	358	~90%	Pebbly sandstone and conglomerate interbedded; both lithologies as above; 0-90% pebbles up to 1/2" diameter.										
358	367	~80%	Pebbly sandstone - medium-grained to coarse-grained; light grey; indistinct bedding; carbonaceous at 365' only; 0-10% pebbles up to 2" diameter.										

-Continued

Diamond Drill Record

PAGE 5

COLOR:	HOLE SURVEY		
NORTH _____	FOOTAGE	AZIMUTH	DIP
EAST _____			
ELEVATION _____			
LOGGED BY _____			
DATE LOGGED _____			
MAP REFERENCE NO. _____	METHOD: _____		

COMPANY NAME _____
 PROPERTY NAME _____
 DRILLING CONTRACTOR _____
 ASSAYER _____
 PURPOSE OF HOLE _____

HOLE NO. <u>C-76-7</u>
CLAIM NAME _____
COMMENCED _____
FINISHED _____
PROJECT NO. _____

FROM	TO	RECOVY	DESCRIPTION	SAMPLE				ASSAYS					
				FROM	TO	WIDTH	NO.						
358	367	~80%	core angle at 365'~35°.										
367	377	~90%	Conglomerate - as 358-367'; ~70% pebbles up to 4" diameter.										
377	378	~90%	Pebbly sandstone - as above.										
378	387	~90%	Conglomerate - as above- ~70-80% pebbles up to 1/2" diameter; core angle at 387'~45°.										
387	389	~90%	Sandstone - coarse-grained to very coarse-grained; light grey to white; vuggy in parts; indistinct bedding.										
389	396.5	~90%	Conglomerate - as above; ~90% pebbles up to 2" diameter; carbonaceous at 396' only.										
396.5	397.5	~90%	Sandstone and mudstone interbedded; carbonaceous with COAL partings; medium hard; medium-grey to dark grey; sandstone is medium-grained.										
397.5	415	~80%	Conglomerate - as above; ~80-90% pebbles up to 1" diameter; core angle at 411'~50°.										
415	416	~90%	Mudstone - dark grey; soft; non carbonaceous; indistinct bedding.										
416	458	~90%	Conglomerate - as above; 70-90% pebbles up to 3" in diameter; core angle at 431'~30°; at 451'~30°.										
458	470	~90%	Sandstone - medium grey to white; medium-grained to coarse-grained; indistinct bedding; carbonaceous in parts; calcareous stringers; relatively pebble-free; core angle at 462'~40°.										
470	492	~40%	Conglomerate - as above; 70-90% pebbles up to 1" diameter;										

-Continued

Diamond Drill Record

COLLAR:		HOLE SURVEY		
		FOOTAGE	AZIMUTH	DIP
NORTH _____				
EAST _____				
ELEVATION _____				
LOGGED BY _____				
DATE LOGGED _____				
MAP REFERENCE NO. _____		METHOD: _____		

COMPANY NAME _____

PROPERTY NAME _____

DRILLING CONTRACTOR _____

ASSAYER _____

PURPOSE OF HOLE _____

HOLE NO. <u>C-76-7</u>
CLAIM NAME _____
COMMENCED _____
FINISHED _____
PROJECT NO. _____

FROM	TO	RECOVY	DESCRIPTION	SAMPLE				ASSAYS					
				FROM	TO	WIDTH	NO.						
470	492	~ 40%	Core angle at 482'~55°.										
492	493	~ 90%	Sandstone - light grey; coarse-grained; indistinct bedding; pebble-free.										
493	515	~ 90%	Conglomerate - as above; ~ 80-90% pebbles up to 2" diameter; core angle at 503~55°.										
515	519	~70%	Sandstone - light grey; coarse-grained; pebble-free; indistinct bedding.										
519	522	~90%	Conglomerate - as above; ~70-90% pebbles up to 1" diameter.										
522	523	~ 50%	Sandstone - as above; core angle at 523'~ 30°.										
523	525	~60%	Conglomerate - as above; 90% pebbles up to ½" in diameter.										
525	526	~90%	Pebbly sandstone - coarse-grained; 0-40% pebbles up to ½" in diameter.										
526	530	~90%	Conglomerate - as above; ~90% pebbles up to ½" diameter.										
530	537	~90%	Pebbly sandstone - light grey; medium-grained; 0-20% pebbles up to ½" diameter.										
537	571	~90%	Conglomerate - as above; ~70% pebbles up to 1" diameter; core angle at 538'~50°; at 563'~40°.										
571	585	~70%	Mudstone - dark grey; hard; carbonaceous; bedding indistinct; core angle at 581'~50°.										
585	604	~90%	Mudstone - calcareous; limestone fragments; indistinct bedding; hard; dark grey; carbonaceous in parts; core angle at 601'~60°.										
604	817	~90%	Sandstone - fine-grained to medium-grained; medium grey to light grey; limestone fragments locally non carbonaceous; indistinct bedding;										

-Continued-

Diamond Drill Record

HOLE SURVEY	
NORTH _____	FOOTAGE _____
EAST _____	AZIMUTH _____
ELEVATION _____	DIP _____
LOGGED BY _____	
DATE LOGGED _____	
MAP REFERENCE NO. _____	METHOD: _____

COMPANY NAME _____

PROPERTY NAME _____

DRILLING CONTRACTOR _____

ASSAYER _____

PURPOSE OF HOLE _____

PAGE _____

HOLE NO. C-76-8

CLAIM NAME _____

COMMENCED _____

FINISHED _____

PROJECT NO. _____

FROM	TO	RECOVY	DESCRIPTION	SAMPLE				ASSAYS					
				FROM	TO	WIDTH	NO.						
156	157	80%	Sandstone - light grey; fine-grained; bedding indistinct; non carbonaceous.										
157	158	80%	Mudstone - dark grey; soft; non carbonaceous; calcareous stringers.										
158	164	80%	Sandstone - as above.										
164	166	90%	Mudstone and siltstone - medium grey; indistinct bedding; soft; non carbonaceous.										
166	180	80%	Sandstone - as above; medium hard; distinct bedding in parts; calcareous stringers; core angle at 176' 35°.										
180	181	90%	Mudstone - medium grey to dark grey; soft to hard.										
181	185	90%	Sandstone - as above.										
185	186	90%	Mudstone - as above.										
186	188	80%	Sandstone - as above.										
188	192	80%	Mudstone - medium grey to dark grey; soft; carbonaceous in parts; core angle at 190' 40°.										
192	215	90%	Sandstone - light grey to medium grey; fine-grained; indistinct bedding; calcareous stringers and lenses; core angle at 210' 60°.										
215	226	90%	Interbedded mudstone and siltstone- dark grey to medium grey; soft to hard; carbonaceous in parts; calcareous stringers in parts.										
226	229	90%	Sandstone - as above.										
229	231	90%	Mudstone - dark grey; calcareous stringers; soft to hard; core angle at _____										

-Continued

Diamond Drill Record

COLLAR:	HOLE SURVEY		
NORTH _____	FOOTAGE	AZIMUTH	DIP
EAST _____			
ELEVATION _____			
LOGGED BY _____			
DATE LOGGED _____			
MAP REFERENCE NO. _____	METHOD: _____		

COMPANY NAME _____
 PROPERTY NAME _____
 DRILLING CONTRACTOR _____
 ASSAYER _____
 PURPOSE OF HOLE _____

HOLE NO. <u>C-76-12</u>
CLAIM NAME _____
COMMENCED _____
FINISHED _____
PROJECT NO. _____

FROM	TO	RECOVY	DESCRIPTION	SAMPLE				ASSAYS					
				FROM	TO	WIDTH	NO.						
234	237	~90%	Sandstone - carbonaceous with COAL partings; some mudstone layers; light grey; calcareous; as 232'- 234'.										
237	239	~90%	Mudstone - carbonaceous with COAL partings; soft; indistinct bedding; core angle at 238' ~30°.										
239	250	~90%	COAL - bright; clean; soft; friable.	239.0	245.0	6.0	C-43						
250	251	~90%	Mudstone - carbonaceous with COAL partings; indistinct bedding.	245.0	250.0	5.0	C-44						
251	253	~90%	Sandstone - soft; poor recovery; coarse-grained; no bedding.										
253	257	~90%	Sandstone - fine-grained; medium grey to light grey; carbonaceous in parts; broken up core.										
257	259	~90%	Mudstone - dark grey to black; carbonaceous with COAL partings; calcareous in parts; some sandstone layers interbedded; core angle at 257' ~50°.										
259	261	~90%	Sandstone - coarse-grained; light grey to brown; calcareous; no distinct bedding.										
261	266	~70%	Mudstone - carbonaceous with COAL partings; dark grey to black; soft to hard; non calcareous; few sandstone layers at upper contact.										
266	327	~90%	Sandstone - coarse to very coarse-grained; white to medium grey. Locally calcareous cement, locally with white dolomite (?) fragments up to 1/4" diameter. Indistinct bedding. Core-angle at 278'=35°; at 313'=35°.										
327	334	~90%	Pebbly sandstone - coarse-grained; angular chert pebbles up to 1/2" diameter. Pebbles ~40%; locally contains white dolomite (?) fragments.										

Contd

APPENDIX II - ANALYTICAL REPORTS

CYPRUS ANVIL MINING CORPORATION

Analytical Report

for
Core Testing

PROJECT:

DRILL HOLE #: C-76-4

AREA: Carmacks, T. Y.

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: T5

DATE ANALYZED: December 10, 1976

COMPOSITE NO.: T5
HOLE NO.: C-76-4
SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-12	16.24	0.84	22.56	60.36	12,050	1
Footage: 261-266						
Weight: 6,885 gms.						
Number: C-13	26.35	0.94	23.17	49.54	9,980	1
Footage: 266-271						
Weight: 6,187 gms.						
Number: C-14	11.23	0.99	20.23	67.55	13,000	½
Footage: 271-276						
Weight: 5,868 gms.						
Number: C-15	28.51	0.85	19.11	51.53	9,970	1
Footage: 276-281						
Weight: 5,545 gms.						

Number:
Footage:
Weight:

COMPOSITE NO.: T-5

HOLE NO.: C-76-4

SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-16	21.57	0.80	21.58	56.05	11,110	½
Footage: 281-286						
Weight: 3,612 gms.						

Number: C-17	21.63	0.78	20.07	57.52	11,020	1
Footage: 286-291						
Weight: 5,504 gms.						

Number: C-18	28.92	0.76	21.20	49.12	9,650	½
Footage: 291-297						
Weight: 7,266						

Number:

Footage:

Weight:

Number:

Footage:

Weight:

COMPOSITE NO.: T-5
 HOLE NO.: C-76-4
 SEAM:

T A B L E 2. ANALYSIS OF COMPOSITE HEAD SAMPLE

Ash %	23.06
R.M. %	0.81
V.M. %	21.46
F.C. %	54.67
S. %	0.63
B.T.U./LB.	11,040
F.S.I.	$\frac{1}{2}$

T A B L E 3. SIZE CONSIST OF COMPOSITE HEAD SAMPLE

<u>Size</u>	<u>Wt. %</u>
1/4" x 28 M.	68.53
28 M. x 0	31.47
<hr/> Total	100.00

T A B L E 4. ANALYSIS OF SIZE FRACTIONS

	<u>1/4" x 28 M.</u>	<u>28 M. x 0</u>	<u>Total</u>
Ash %	28.16	14.19	23.76
R.M. %	0.86	0.67	0.80
V.M. %	21.24	22.57	21.66
F.C. %	49.74	62.57	53.78
B.T.U./LB.	10,410	12,540	11,080
F.S.I.	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$

COMPOSITE NO.: T-5
HOLE NO.: C-76-4
SEAM:

T A B L E 5. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Fractional Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>
- 1.30	2.47	0.89	2.67	14,970
1.30 - 1.40	39.67	1.10	6.36	14,180
1.40 - 1.60	26.84	0.98	18.97	12,130
1.60 - 1.80	7.69	0.88	40.61	8,180
+ 1.80	23.33	0.66	73.94	2,150
TOTAL	100.00	0.94	28.05	10,380

T A B L E 6. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Cumulative Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>	<u>F.S.I.</u>
- 1.30	2.47	0.89	2.67	14,970	NOT REQUIRED
- 1.40	42.14	1.09	6.14	14,230	
- 1.60	68.98	1.05	11.13	13,410	
- 1.80	76.67	1.03	14.09	12,890	
TOTAL	100.00	0.94	28.05	10,380	

COMPOSITE NO.: T5

HOLE NO.: C-76-4

SEAM:

T A B L E 7. WASHABILITY FOR 1/4" x 28 MESH FRACTION

Sp. Gr.	Fractional		Cumulative			
	Wt. %	Ash %	Floats		Sinks	
			Wt. %	Ash %	Wt. %	Ash %
- 1.30	2.47	2.67	2.47	2.67	100.00	28.05
1.30 - 1.40	39.67	6.36	42.14	6.14	97.53	28.70
1.40 - 1.60	26.84	18.97	68.98	11.13	57.86	44.01
1.60 - 1.80	7.69	40.61	76.67	14.09	31.02	65.68
+ 1.80	23.33	73.94	100.00	28.05	23.33	73.94
Total	100.00	28.05				

COMPOSITE NO.: T-5
HOLE NO.: C-76-4
SEAM:

T A B L E 8. FLOAT-SINK OF 1/4" x 28 MESH FOR 8% ASH IN FLOATS

Specific Gravity: 1.46
Yield of Floats: 54.96%

Analysis of Floats:

Ash % 7.81
R.M. % 0.91
V.M. % 22.11
F.C. % 69.17
S. % 0.75
B.T.U./Lb. 14,000
F.S.I. 1½

Analysis of Sinks:

Ash % 53.60
R.M. % 0.98

FIGURE

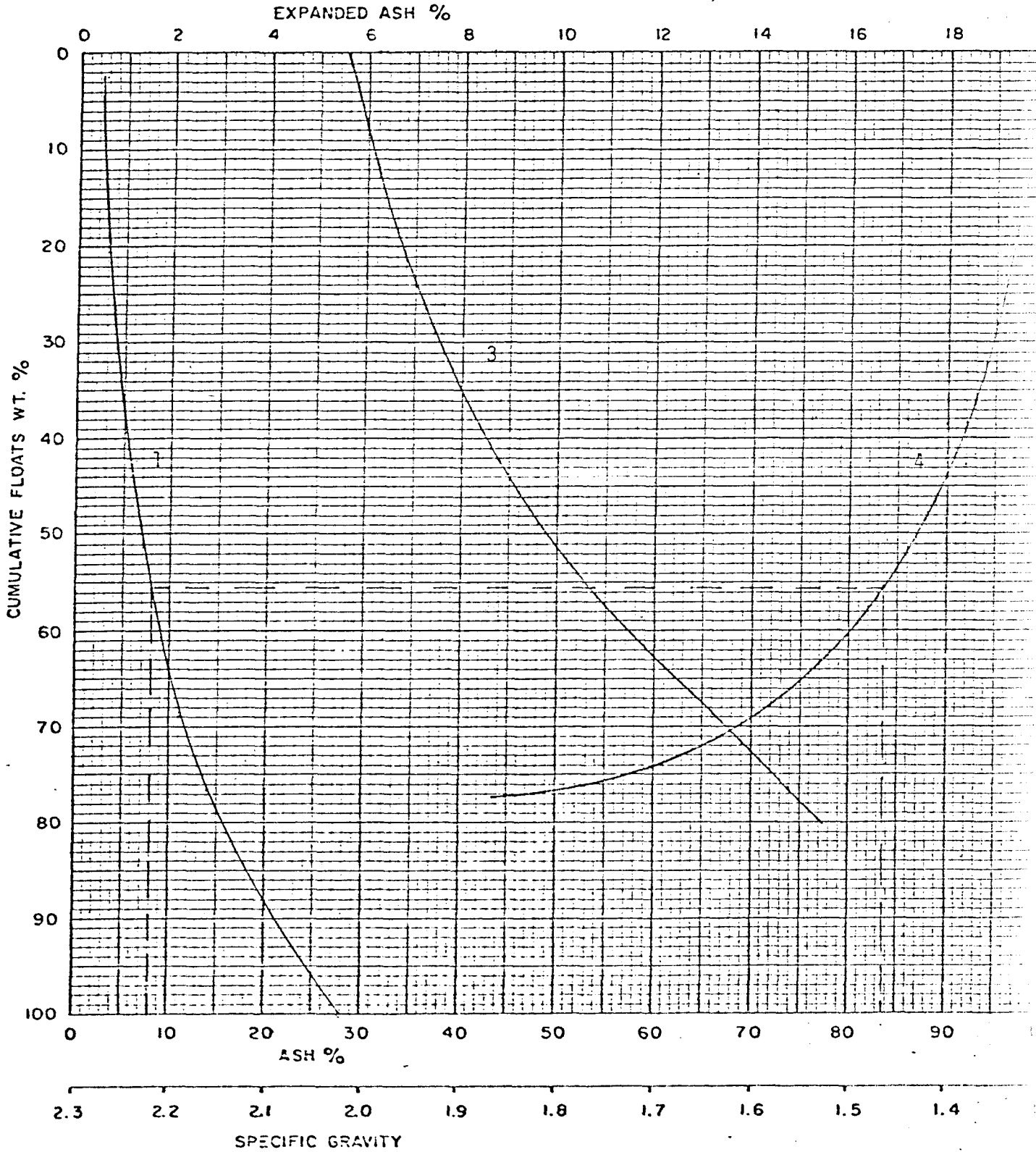
COMPANY CYPRUS ANVIL MINING CORP.

SAMPLE T-5

Size 1/4" x 28 Mesh

WASHABILITY CURVES

- 1 - FLOATS
- 2 - EXPANDED FLOATS
- 3 - SINKS
- 4 - SPECIFIC GRAVITY
- 5 - ELEMENTARY ASH
- 6 - NEAR GRAVITY MATERIAL



DATE

CYCLONE ENGINEERING SALES
EDMONTON ALBERTA CANADA

CYPRUS ANVIL MINING CORPORATION

Analytical Report

for
Core Testing

PROJECT:

DRILL HOLE #: C76-6

AREA: Caramacks, Y.T.

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: T7

DATE ANALYZED: December 13, 1976

COMPOSITE NO.: T7

HOLE NO.: C-76-6

SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-24	19.49	0.83	22.56	57.12	12,180	7
Footage: 294 - 299						
Weight: 4,036						

Number: C-25	23.75	0.94	21.80	53.51	10,840	4½
Footage: 299 - 304.5						
Weight: 6,395						

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

COMPOSITE NO.: T7

HOLE NO.: C-76-6

SEAM:

T A B L E 2. ANALYSIS OF COMPOSITE HEAD SAMPLE

Ash %	21.91
R.M. %	0.93
V.M. %	21.84
F.C. %	55.32
S. %	0.53
B.T.U./LB.	11,420
F.S.I.	6

T A B L E 3. SIZE CONSIST OF COMPOSITE HEAD SAMPLE

<u>Size</u>	<u>Wt. %</u>
1/4" x 28 M.	63.47
28 M. x 0	36.53
<hr/> Total	<hr/> 100.00

T A B L E 4. ANALYSIS OF SIZE FRACTIONS

	<u>1/4" x 28 M.</u>	<u>28 M. x 0</u>	<u>Total</u>
Ash %	23.68	16.54	21.07
R.M. %	0.87	0.87	0.87
V.M. %	21.21	23.50	22.05
F.C. %	54.24	59.09	56.01
B.T.U./LB.	10,620	12,700	11,380
F.S.I.	6	7	6

COMPOSITE NO.: T7
HOLE NO.: C-76-6
SEAM:

T A B L E 5. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Fractional Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>
- 1.30	12.27	0.86	3.07	15,240
1.30 - 1.40	28.71	1.00	7.84	14,150
1.40 - 1.60	25.79	1.01	20.68	11,860
1.60 - 1.80	9.92	0.89	38.12	8,540
+ 1.80	23.31	0.94	71.17	2,880
TOTAL	100.00	0.96	28.33	10,510

T A B L E 6. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Cumulative Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>	<u>F.S.I.</u>
- 1.30	12.27	0.86	3.07	15,240	8½
- 1.40	40.98	0.96	6.41	14,480	6½
- 1.60	66.77	0.98	11.92	13,470	5
- 1.80	76.69	0.97	15.31	12,830	4½
TOTAL	100.00	0.96	28.33	10,510	4

COMPOSITE NO.: T7

HOLE NO.: C-76-6

SEAM:

T A B L E 7. WASHABILITY FOR 1/4" x 28 MESH FRACTION

Sp. Gr.	Fractional		Cumulative			
	Wt. %	Ash %	Floats		Sinks	
			Wt. %	Ash %	Wt. %	Ash %
- 1.30	12.27	3.07	12.27	3.07	100.00	28.33
1.30 - 1.40	28.71	7.84	40.98	6.41	87.73	31.87
1.40 - 1.60	25.79	20.68	66.77	11.92	59.02	43.55
1.60 - 1.80	9.92	38.12	76.69	15.31	33.23	61.30
+ 1.80	23.31	71.17	100.00	28.33	23.31	71.17
Total	100.00	28.33				

COMPOSITE NO.: T7

HOLE NO.: C-76-6

SEAM:

T A B L E 8. FLOAT-SINK OF 1/4" x 28 MESH FOR 8% ASH IN FLOATS

Specific Gravity: 1.46
Yield of Floats: 52.00 %

Analysis of Floats:

Ash % 8.07
R.M. % 0.93
V.M. % 22.26
F.C. % 68.74
S. % 0.67
B.T.U./Lb. 14,080
F.S.I. 6½

Analysis of Sinks:

Ash % 49.53
R.M. % 0.93

FIGURE

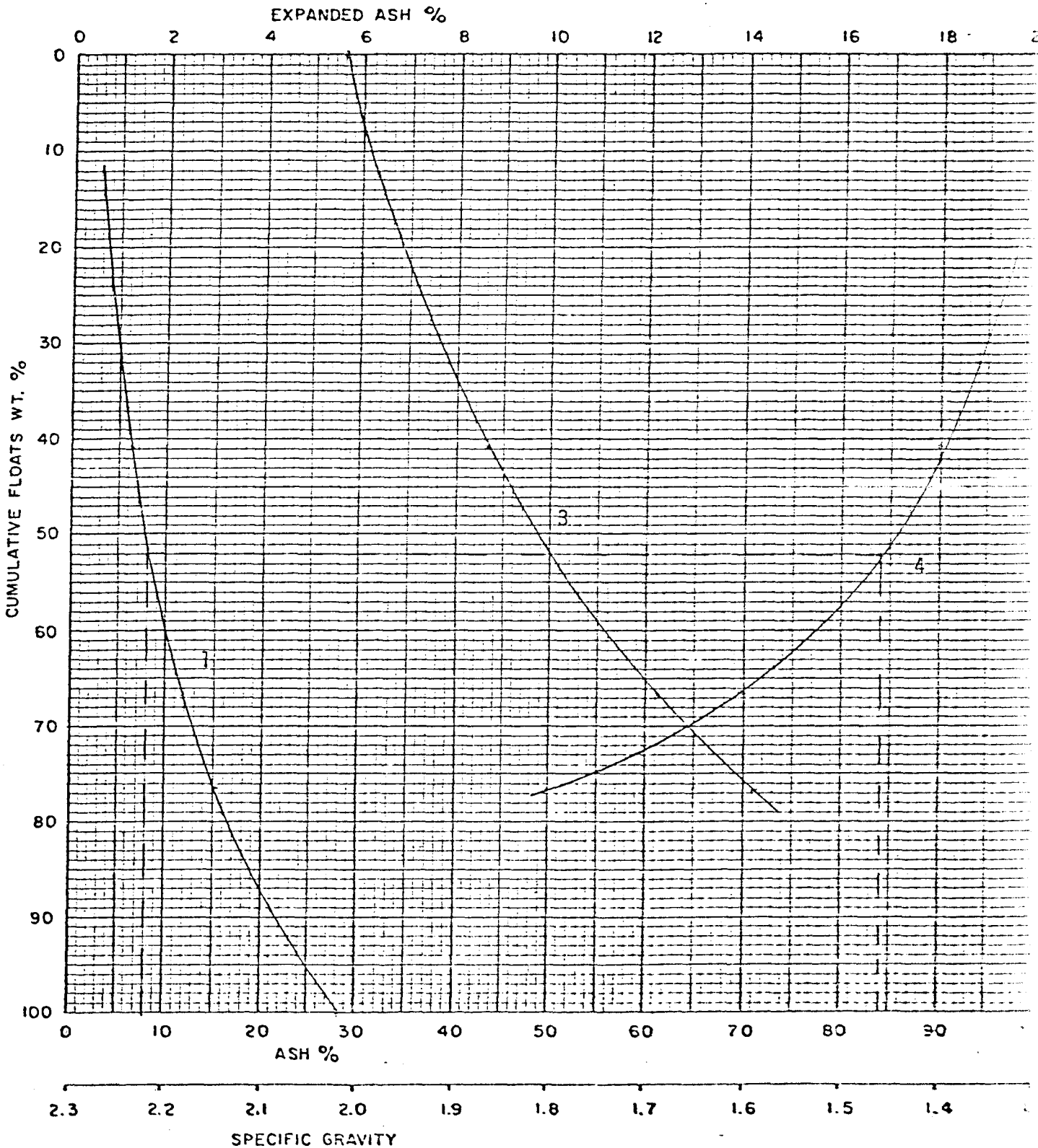
COMPANY CYPRUS ANVIL MINING CORP.

SAMPLE T-7

Size 1/4" x 28 Mesh

WASHABILITY CURVES

- 1 - FLOATS
- 2 - EXPANDED FLOATS
- 3 - SINKS
- 4 - SPECIFIC GRAVITY
- 5 - ELEMENTARY ASH
- 6 - NEAR GRAVITY MATERIAL



DATE

CYCLONE ENGINEERING SALES LTD.
EDMONTON ALBERTA CANADA

CYPRUS ANVIL MINING CORPORATION

Analytical Report
for
Core Testing

PROJECT:

DRILL HOLE #: C-76-6

AREA: Caramacks, Y.T.

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: T-8

DATE ANALYZED: December 16, 1976

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-26	27.71	0.51	21.02	50.76	10,750	7
Footage: 308-313						
Weight: 2,812						
Number: C-27	29.86	0.50	20.97	48.67	10,180	7
Footage: 313-318						
Weight: 5,168						
Number: C-28	27.94	0.54	21.98	49.54	10,600	7½
Footage: 318-323						
Weight: 4,813						
Number: C-29	30.54	0.53	21.03	47.90	10,160	5½
Footage: 323-328						
Weight: 5,836						
Number: C-30	32.68	0.56	19.81	46.95	9,720	5½
Footage: 328-333						
Weight: 4,460						

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-31	28.17	0.56	21.88	49.39	10,500	7
Footage: 333-339						
Weight: 6,554						

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 2. ANALYSIS OF COMPOSITE HEAD SAMPLE

Ash %	29.00
R.M. %	0.54
V.M. %	22.12
F.C. %	48.34
S. %	0.69
B.T.U./LB.	10,270
F.S.I.	6½

T A B L E 3. SIZE CONSIST OF COMPOSITE HEAD SAMPLE

<u>Size</u>	<u>Wt. %</u>
1/4" x 28 M.	70.89
28 M. x 0	29.11
<hr/>	<hr/>
Total	100.00

T A B L E 4. ANALYSIS OF SIZE FRACTIONS

	<u>1/4" x 28 M.</u>	<u>28 M. x 0</u>	<u>Total</u>
Ash %	32.36	21.37	29.16
R.M. %	0.56	0.53	0.55
V.M. %	21.84	22.61	22.06
F.C. %	45.24	55.49	48.23
B.T.U./LB.	9,630	11,760	10,250
F.S.I.	6	7	6

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 5. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Fractional Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>
- 1.30	10.05	0.49	3.30	15,010
1.30 - 1.40	29.22	0.63	9.60	14,340
1.40 - 1.60	19.86	0.53	22.77	11,550
1.60 - 1.80	9.61	0.66	39.48	8,130
+ 1.80	31.26	0.84	70.70	2,610
TOTAL	100.00	0.66	33.55	9,590

T A B L E 6. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Cumulative Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>	<u>F.S.I.</u>
- 1.30	10.05	0.49	3.30	15,010	9
- 1.40	39.27	0.59	7.98	14,510	8½
- 1.60	59.13	0.57	12.95	13,520	7½
- 1.80	68.74	0.58	16.66	12,760	7
TOTAL	100.00	0.66	33.55	9,590	6

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 7. WASHABILITY FOR 1/4" x 28 MESH FRACTION

Sp. Gr.	Fractional		Cumulative			
	Wt. %	Ash %	Floats		Sinks	
			Wt. %	Ash %	Wt. %	Ash %
- 1.30	10.05	3.30	10.05	3.30	100.00	33.55
1.30 - 1.40	29.22	9.60	39.27	7.98	89.95	36.93
1.40 - 1.60	19.86	22.77	59.13	12.95	60.73	50.09
1.60 - 1.80	9.61	39.48	68.74	16.66	40.87	63.36
+ 1.80	31.26	70.70	100.00	33.55	31.26	70.70
Total	100.00	33.55				

COMPOSITE NO.: T-8

HOLE NO.: C-76-6

SEAM:

T A B L E 8. F L O A T - S I N K O F 1 / 4 " x 2 8 M E S H F O R 8 % A S H I N F L O A T S

Specific Gravity: 1.40

Yield of Floats: 39.27 %

Analysis of Floats:

Ash % 7.98

R.M. % 0.57

V.M. % 24.49

F.C. % 66.96

S. % 0.78

B.T.U./Lb. 14,200

F.S.I. 8

Analysis of Sinks:

Ash % 50.09

R.M. % 0.58

FIGURE

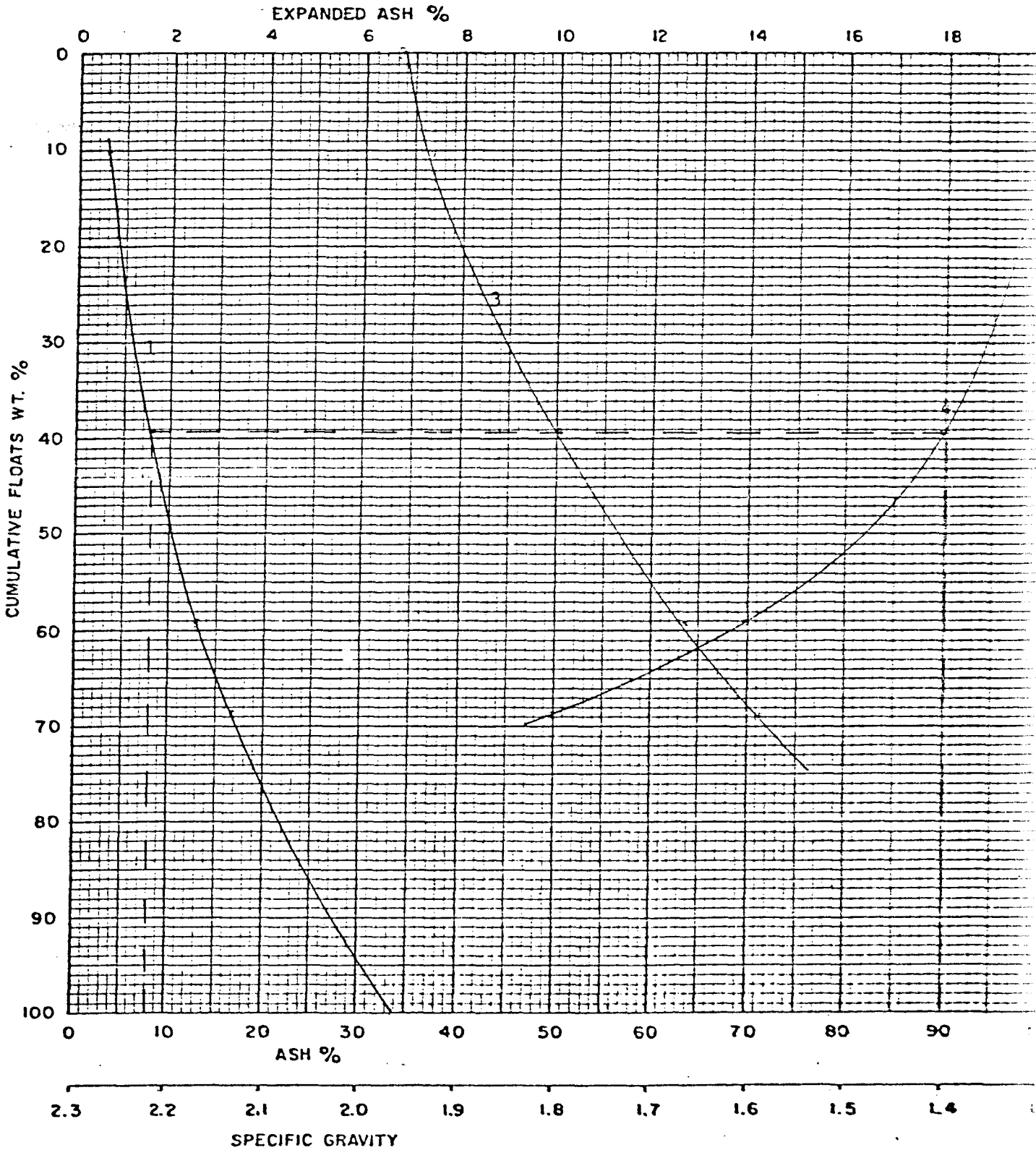
COMPANY CYPRUS ANVIL MINING CORP.

SAMPLE T - 8

Size 1/4" x 28 Mesh

WASHABILITY CURVES

- 1 - FLOATS
- 2 - EXPANDED FLOATS
- 3 - SINKS
- 4 - SPECIFIC GRAVITY
- 5 - ELEMENTARY ASH
- 6 - NEAR GRAVITY MATERIAL



DATE

CYCLONE ENGINEERING SALES LTD
EDMONTON ALBERTA CANADA

CYPRUS ANVIL MINING CORPORATION

Analytical Report

for

Core Testing

PROJECT:

DRILL HOLE #: C76-6

AREA:

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: A3

DATE ANALYZED:

COMPOSITE NO.: A3
HOLE NO.: C-76-6
SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-32	27.02	0.49	21.26	51.23	10,710	6½
Footage: 352 - 357						
Weight: 5,674 gm.						

End of Analysis

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

CYPRUS ANVIL MINING CORPORATION

Analytical Report
for
Core Testing

PROJECT:

DRILL HOLE #: C-76-6

AREA: Caramacks, Y.T.

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: T-9

DATE ANALYZED: December 16, 1976

COMPOSITE NO.: T-9

HOLE NO.: C-76-6

SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-33	52.52	0.52	17.16	29.80	6,390	2½
Footage: 363-368						
Weight: 3,131						
Number: C-34	19.01	0.46	22.82	57.71	12,510	7½
Footage: 368-373						
Weight: 2,212						
Number: C-35	42.07	0.41	17.77	39.75	7,830	2
Footage: 373-378						
Weight: 4,384						
Number:						
Footage:						
Weight:						
Number:						
Footage:						
Weight:						

COMPOSITE NO.: T-9

HOLE NO.: C-76-6

SEAM:

T A B L E 2. ANALYSIS OF COMPOSITE HEAD SAMPLE

Ash %	40.35
R.M. %	0.46
V.M. %	18.04
F.C. %	41.15
S. %	0.74
B.T.U./LB.	8,310
F.S.I.	4

T A B L E 3. SIZE CONSIST OF COMPOSITE HEAD SAMPLE

<u>Size</u>	<u>Wt. %</u>
1/4" x 28 M.	75.05
28 M. x 0	24.95
<hr/> Total	<hr/> 100.00

T A B L E 4. ANALYSIS OF SIZE FRACTIONS

	<u>1/4" x 28 M.</u>	<u>28 M. x 0</u>	<u>Total</u>
Ash %	47.05	22.43	40.91
R.M. %	0.46	0.45	0.46
V.M. %	17.43	21.08	18.34
F.C. %	35.06	56.04	40.29
B.T.U./LB.	7,120	11,350	8,180
F.S.I.	3½	6½	4

COMPOSITE NO.: T-9

HOLE NO.: C76-6

SEAM:

T A B L E 5. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Fractional Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>
- 1.30	12.63	0.41	3.38	15,270
1.30 - 1.40	12.00	0.52	8.67	14,200
1.40 - 1.60	13.85	0.50	22.53	11,570
1.60 - 1.80	8.00	0.49	40.34	8,500
+ 1.80	53.52	0.51	73.99	2,380
TOTAL	100.00	0.50	47.41	7,190

T A B L E 6. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Cumulative Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>	<u>F.S.I.</u>
- 1.30	12.63	0.41	3.38	15,270	9
- 1.40	24.63	0.46	5.96	14,750	9
- 1.60	38.48	0.48	11.92	13,600	7½
- 1.80	46.48	0.48	16.81	12,720	6½
TOTAL	100.00	0.50	47.41	7,190	3½

COMPOSITE NO.: T-9

HOLE NO.: C-76-6

SEAM:

T A B L E 7. WASHABILITY FOR 1/4" x 28 MESH FRACTION

Sp. Gr.	Fractional		Cumulative			
	Wt. %	Ash %	Floats		Sinks	
			Wt. %	Ash %	Wt. %	Ash %
- 1.30	12.63	3.38	12.63	3.38	100.00	47.41
1.30 - 1.40	12.00	8.67	24.63	5.96	87.37	53.78
1.40 - 1.60	13.85	22.53	38.48	11.92	75.37	60.96
1.60 - 1.80	8.00	40.34	46.48	16.81	61.52	69.61
+ 1.80	53.52	73.99	100.00	47.41	53.52	73.99
Total	100.00	47.41				

COMPOSITE NO.: T-9

HOLE NO.: C-76-6

SEAM:

T A B L E 8. FLOAT-SINK OF 1/4" x 28 MESH FOR 8% ASH IN FLOATS

Specific Gravity: 1.46
Yield of Floats: 30.00 %

Analysis of Floats:

Ash % 7.96
R.M. % 0.45
V.M. % 23.77
F.C. % 67.82
S. % 0.80
B.T.U./Lb. 14,310
F.S.I. 8½

Analysis of Sinks:

Ash % 63.55
R.M. % 0.44

FIGURE

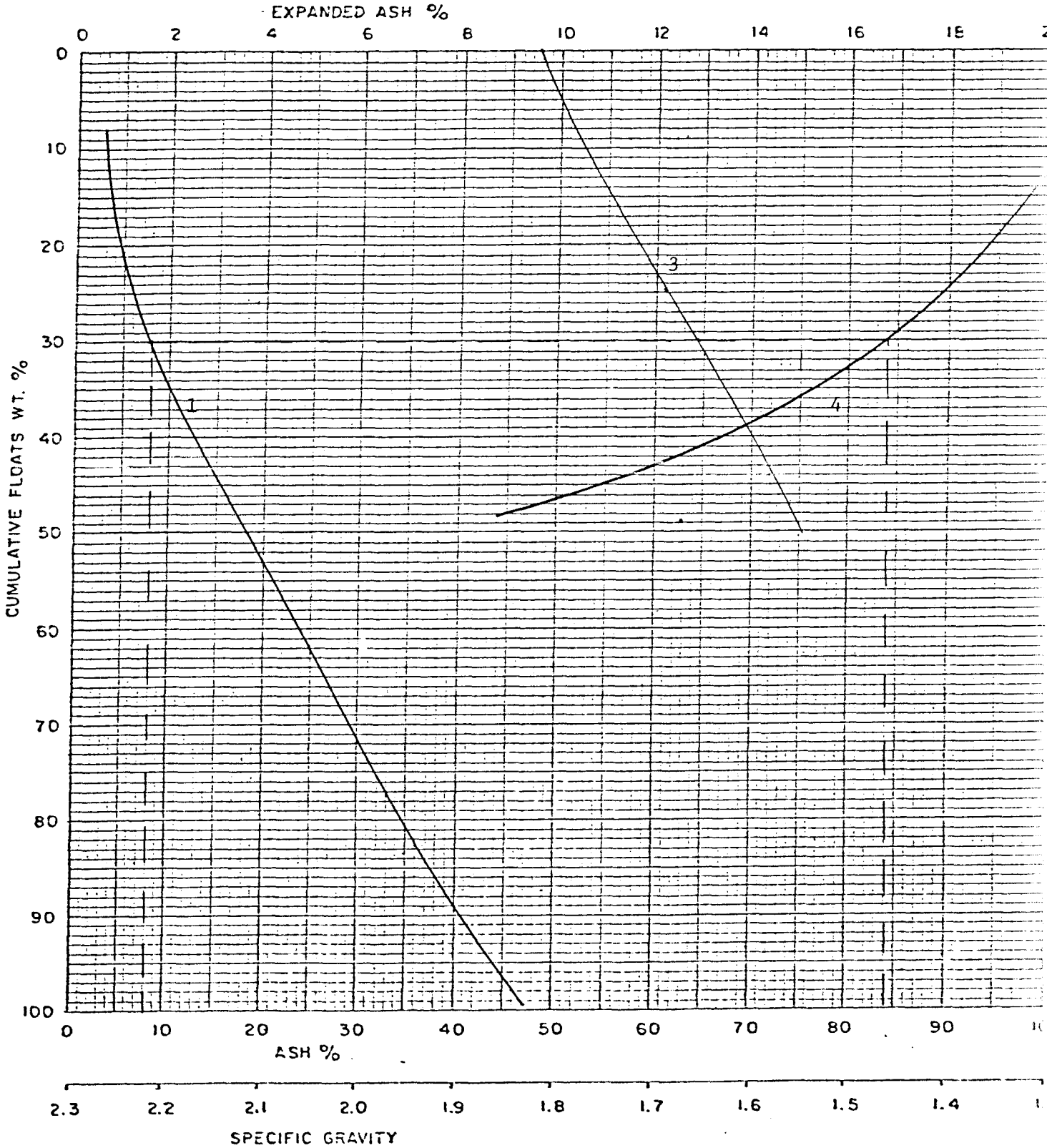
COMPANY CYPRUS ANVIL MINING CORP.

SAMPLE T-9

Size 1/4" x 28 Mesh

WASHABILITY CURVES

- 1 - FLOATS
- 2 - EXPANDED FLOATS
- 3 - SINKS
- 4 - SPECIFIC GRAVITY
- 5 - ELEMENTARY ASH
- 6 - NEAR GRAVITY MATERIAL



DATE

CYCLONE ENGINEERING SALES LTD
EDMONTON ALBERTA CANADA

CYPRUS ANVIL MINING CORPORATION

Analytical Report

for
Core Testing

PROJECT:

DRILL HOLE #: C76-6

AREA: CARMACKS, Y.T.

SEAM:

DATE SAMPLED:

LAB COMPOSITE #: T10

DATE ANALYZED: December 17, 1976

COMPOSITE NO.: T10
HOLE NO.: C76-6
SEAM:

T A B L E 1. COMPONENTS AND ANALYSIS

	<u>Ash %</u>	<u>R.M %</u>	<u>V.M. %</u>	<u>F.C. %</u>	<u>B.T.U./LB.</u>	<u>F.S.I.</u>
Number: C-36	62.89	0.51	15.60	21.00	4,300	N.A.
Footage: 393-398						
Weight: 3,357						
Number: C-37	43.70	0.67	17.36	38.27	7,450	½
Footage: 398-403						
Weight: 5,394						

Number:

Footage:

Weight:

Number:

Footage:

Weight:

Number:

Footage:

Weight:

COMPOSITE NO.: T10

HOLE NO.: C76-6

SEAM:

T A B L E 2. ANALYSIS OF COMPOSITE HEAD SAMPLE

Ash %	51.13
R.M. %	0.58
V.M. %	16.55
F.C. %	31.74
S. %	0.65
B.T.U./LB.	6,290
F.S.I.	$\frac{1}{2}$

T A B L E 3. SIZE CONSIST OF COMPOSITE HEAD SAMPLE

<u>Size</u>	<u>Wt. %</u>
1/4" x 28 M.	83.82
28 M. x 0	16.18
<hr/> Total	100.00

T A B L E 4. ANALYSIS OF SIZE FRACTIONS

	<u>1/4" x 28 M.</u>	<u>28 M. x 0</u>	<u>Total</u>
Ash %	54.35	34.03	51.06
R.M. %	0.59	0.69	0.61
V.M. %	16.00	18.17	16.35
F.C. %	29.06	47.11	31.98
B.T.U./LB.	5,680	9,080	6,230
F.S.I.	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$

COMPOSITE NO.: T10

HOLE NO.: C76-6

SEAM:

T A B L E 5. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Fractional Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>
- 1.30	0.33	-*	2.47	14,920
1.30 - 1.40	11.64	0.83	6.51	14,240
1.40 - 1.60	15.37	0.70	22.08	11,380
1.60 - 1.80	13.23	0.65	38.77	8,250
+ 1.80	59.43	0.49	74.07	2,080
TOTAL	100.00	0.58	53.31	5,780

T A B L E 6. FLOAT-SINK AND ANALYSIS OF 1/4" x 28 MESH
(Cumulative Basis)

<u>Sp. Gr.</u>	<u>Wt. %</u>	<u>R.M. %</u>	<u>Ash %</u>	<u>B.T.U./Lb.</u>	<u>F.S.I.</u>
- 1.30	0.33	-*	2.47	14,920	
- 1.40	11.97	0.83	6.40	14,260	Not
- 1.60	27.34	0.76	15.21	12,640	Required.
- 1.80	40.57	0.72	22.90	11,210	
TOTAL	100.00	0.58	53.31	5,780	

* Not determined due to small sample.

COMPOSITE NO.: T10

HOLE NO.: C76-6

SEAM:

T A B L E 7. WASHABILITY FOR 1/4" x 28 MESH FRACTION

Sp. Gr.	Fractional		Cumulative			
	Wt. %	Ash %	Floats		Sinks	
			Wt. %	Ash %	Wt. %	Ash %
- 1.30	0.33	2.47	0.33	2.47	100.00	53.31
1.30 - 1.40	11.64	6.51	11.97	6.40	99.67	53.48
1.40 - 1.60	15.37	22.08	27.34	15.21	88.03	59.69
1.60 - 1.80	13.23	38.77	40.57	22.90	72.66	67.64
+ 1.80	59.43	74.07	100.00	53.31	59.43	74.07
Total	100.00	53.31				

COMPOSITE NO.: T10

HOLE NO.: C76-6

SEAM:

T A B L E 8. F L O A T - S I N K O F 1 / 4 " x 2 8 M E S H F O R 8 % A S H I N F L O A T S

Specific Gravity: 1.43
Yield of Floats: 14.00 %

Analysis of Floats:

Ash % 7.96
R.M. % 0.83
V.M. % 23.13
F.C. % 68.08
S. % 0.74
B.T.U./Lb. 14,010
F.S.I. 1½

Analysis of Sinks:

Ash % 59.36
R.M. % 0.51

FIGURE

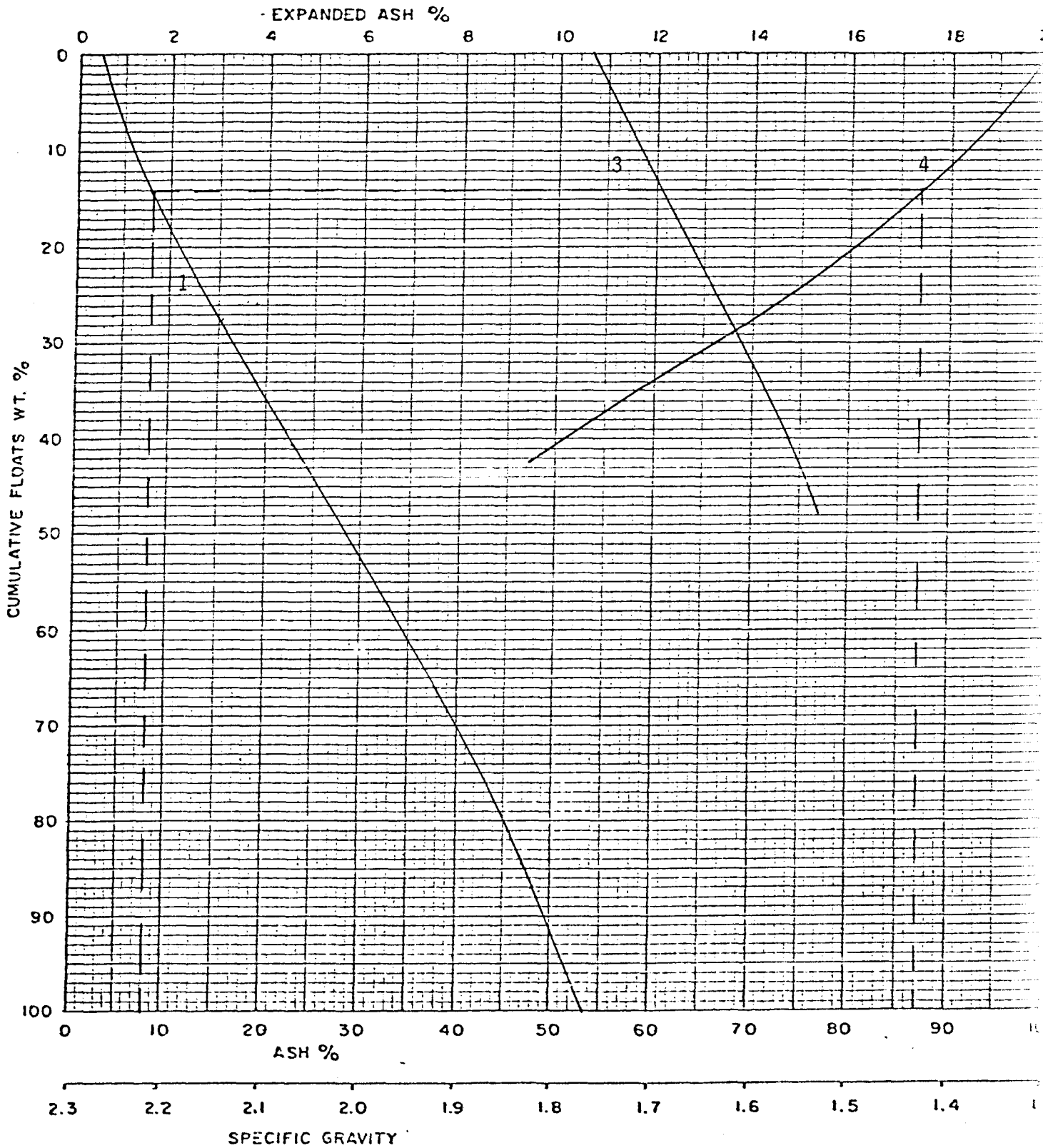
COMPANY CYPRUS ANVIL MINING CORP.

SAMPLE C76-6 Composite T10

Size 1/4" x 20 Mesh

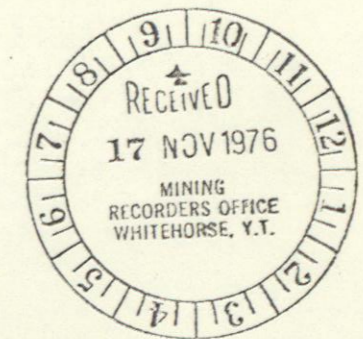
WASHABILITY CURVES

- 1 - FLOATS
- 2 - EXPANDED FLOATS
- 3 - SINKS
- 4 - SPECIFIC GRAVITY
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DATE

CYCLONE ENGINEERING SALES LTD
EDMONTON ALBERTA CANADA



CYPRUS ANVIL MINING CORPORATION
 Key Map
 1976 Diamond Drill Sites - C.M.L. #2949, 2954

Scale : 1"=1/2 mile
 N.T.S.: 115-I-1

- 1976 Drill Sites
- Targets Placed for Aerial Photographs

2970

2973