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**ASSESSMENT REPORT**

describing

**HELICOPTER-BORNE MAGNETIC AND RADIOMETRIC SURVEYS**

Surveys completed July 5, 2015

at the

**IDAHO PROPERTY**

Idaho 1-22	YC41111-YC41132
Idaho 23-52	YC46510-YC46539
Idaho 53-58	YE12153-YE12158

NTS 115J/10

Latitude 62°43'N; Longitude 138°32'W

in the

Whitehorse Mining District  
Yukon Territory

prepared by

Archer, Cathro & Associates (1981) Limited

for

**ATAC RESOURCES LTD.**

by

J. Lane, B.Sc., P.Geo.

January 2016

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Idaho 1-58 Mineral Claims  
January 7, 2016

Labour

H. Burrell (geologist) 3 hours March to January at \$106/hr	333.90
J. Mariacher (office) 6 hours March to January at \$90/hr	567.00
L. Smith (office) 1 hour March to January at \$69/hr	<u>72.45</u>
	973.35

Contract Geophysical Survey (including management)

Precision GeoSurveys Inc.	<u>16,747.62</u>
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\$17,720.97

**APPENDIX I**

**PHYSICAL COPY OF GEOPHYSICAL SURVEY REPORT**

# AIRBORNE GEOPHYSICAL SURVEY REPORT



## Idaho Creek Survey Block Prepared for ATAC Resources Ltd.

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July 2015

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## 1.0 Introduction

This report outlines the geophysical survey operations and data processing procedures taken during the high resolution airborne magnetic and radiometric survey flown at the Idaho Creek survey block for ATAC Resources Ltd. The Idaho Creek survey block area is centered 102.1 km west of Pelly Crossing, Yukon and covers a total of 13.9 km<sup>2</sup>, including a 100 m buffer zone around the perimeter of the claim block (Figure 1). The geophysical survey was started on and completed on July 5, 2015.



Figure 1: Idaho Creek survey block location map.

## 1.1 Survey Area

The Idaho Creek survey block is approximately 102.1 km west of Pelly Crossing, Yukon and 86.0 km west of the Minto airstrip (Figure 2). The block covers a rectangular area of 5.7 km by 3.0 km and its survey plan includes 30 survey lines and 6 tie lines.



Figure 2: Idaho Creek survey block; boundary outline of the 100 m buffer zone in red and the survey block boundary in white; west of Pelly Crossing, Yukon.

The Idaho Creek survey block was flown at 100 meter spacing at a  $066^{\circ}/246^{\circ}$  heading; the tie lines were flown at 1000 meter spacing at a heading of  $156^{\circ}/336^{\circ}$  (Figures 3 and 4). The survey proceeded as planned, and as a result, the total line km flown for the entire survey block remains approximately as estimated, a total of 157 line km.

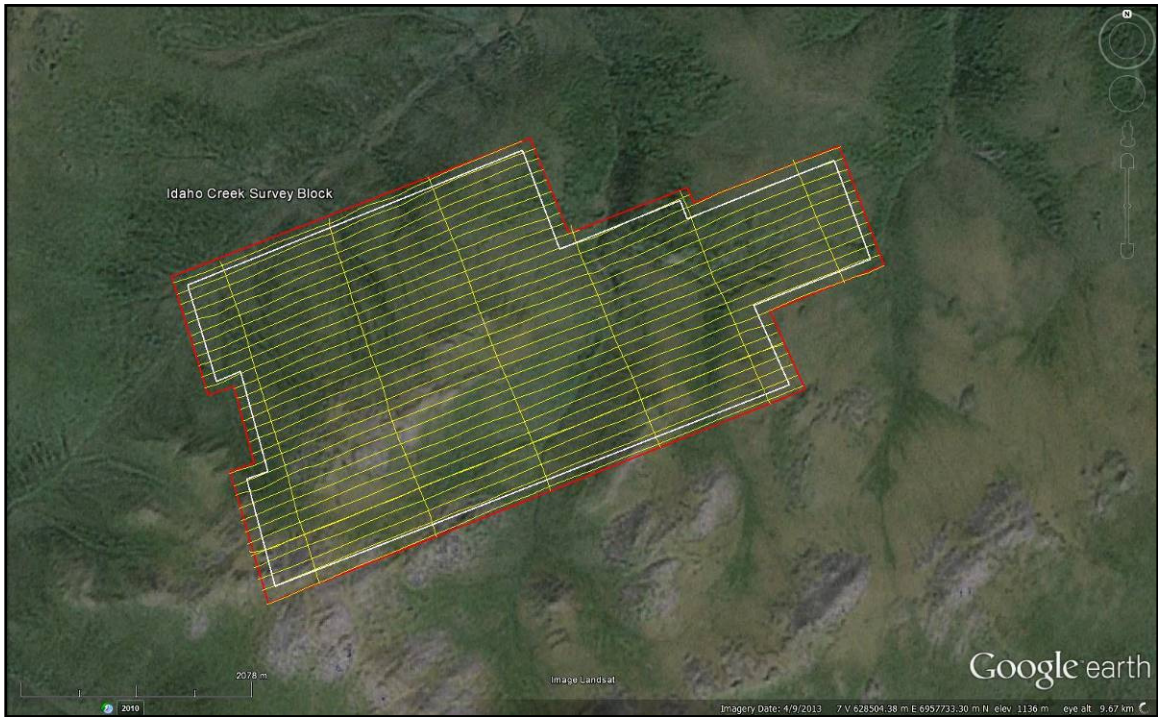


Figure 3: Plan View –Idaho Creek survey block boundary in red with actual flight lines displayed in yellow, the 100 m buffer zone outlined in red, and the block boundary in white.

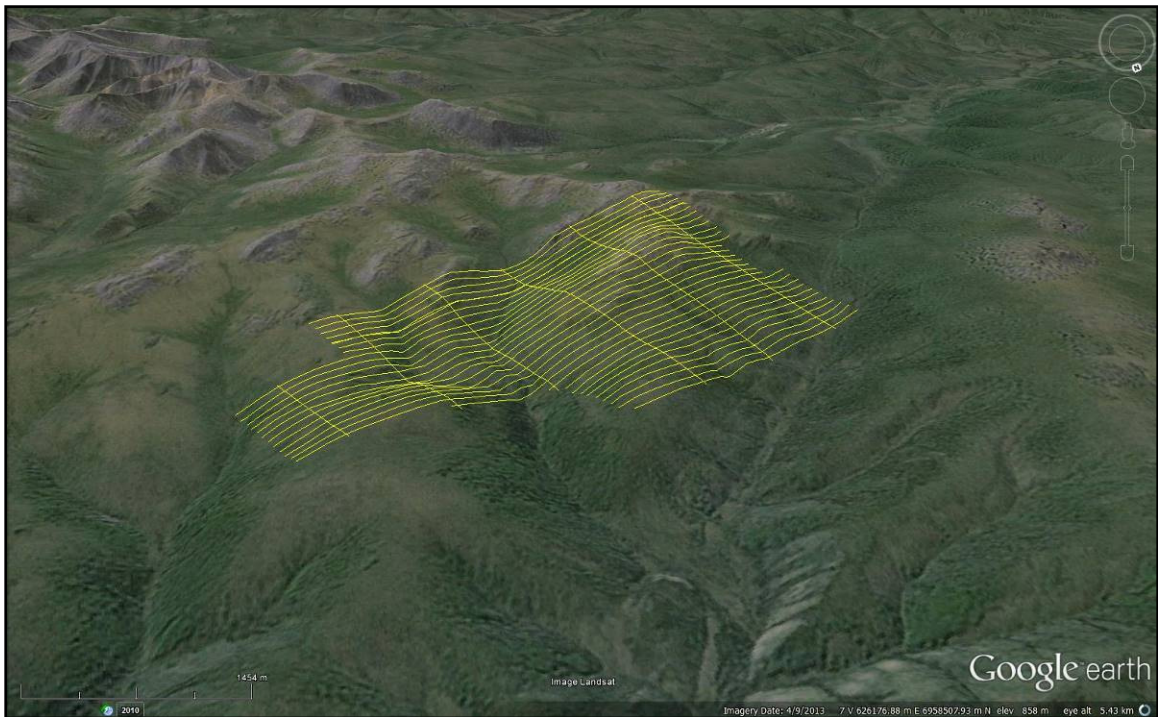


Figure 4: Terrain View – Idaho Creek survey block with actual flight lines displayed in yellow.

## 1.2 Survey Specifications

The geodetic system used for this survey is WGS 84 and the area is contained in zone 7N. A total of 157 line km was flown (Figure 5). The survey data acquisition specifications and coordinates for the survey are specified as follows (Tables 1 and 2).

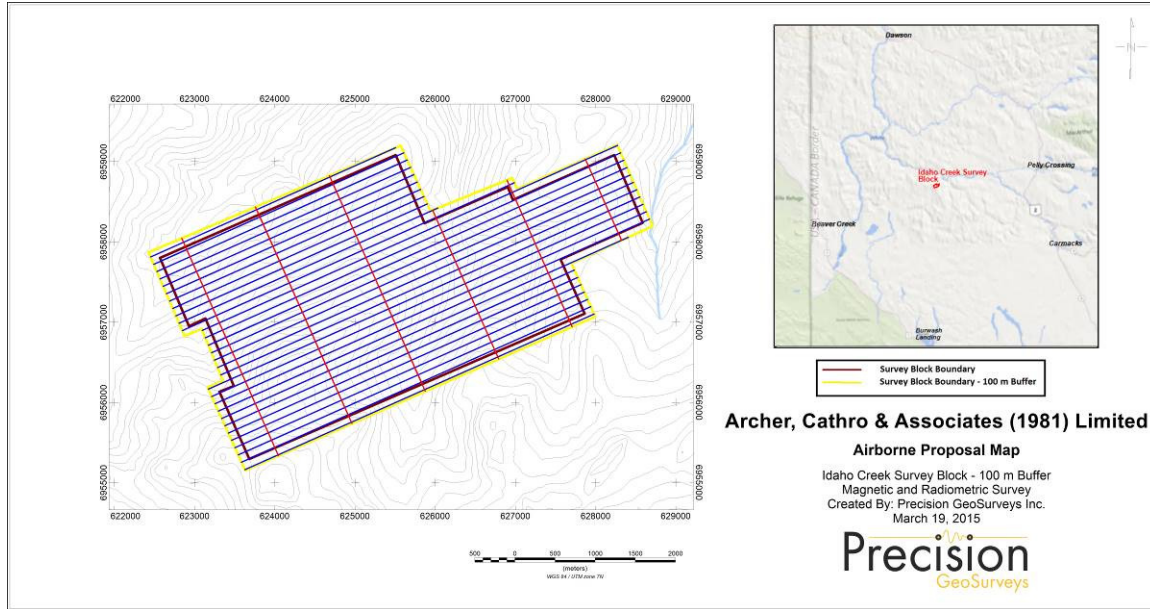


Figure 5: Survey map of Idaho Creek survey block area showing proposed survey and tie lines. Survey block boundary in brown, 100 m buffer outline in yellow, survey lines in blue, and tie lines in red.

Block Name	Area (km <sup>2</sup> )	Line Type	Planned No. of Lines	Planned Line Spacing (m)	Line Orientation	Nominal Survey Height (m)	Actual Survey Height (m)	Total Planned Line km	Total Actual km Flown
Idaho Creek	13.9	Survey	30	100	066°/246°	35	35.4	142	142
		Tie	6	1000	156°/336°	35	35.1	15	15
		<b>Total:</b>							<b>157</b>

Table 1: Idaho Creek survey area flight line specifications.

Longitude	Latitude	Easting	Northing	N/S	E/W
138.60464798	62.73077763	622426	6957869	N	W
138.54224663	62.74165210	625568	6959200	N	W
138.53556279	62.73422490	625941	6958386	N	W
138.51533522	62.73755942	626960	6958797	N	W
138.51424611	62.73630981	627021	6958660	N	W
138.48943355	62.74078976	628269	6959208	N	W
138.48158546	62.73156081	628710	6958196	N	W
138.50171598	62.72775346	627698	6957732	N	W
138.49641483	62.72171386	627995	6957070	N	W
138.58308830	62.70600874	623631	6955152	N	W
138.59151129	62.71544813	623161	6956187	N	W
138.58764273	62.71610909	623356	6956268	N	W
138.59240664	62.72199213	623088	6956914	N	W
138.59663049	62.72130119	622875	6956829	N	W

Table 2: Idaho Creek survey block with 100 buffer zone polygon coordinates using WGS 84 in zone 7N.

## 2.0 Geophysical Data

Geophysical data are collected in a variety of ways and are used to aid in determination of geology, mineral deposits, oil and gas deposits, geotechnical investigations, contaminated land sites and UXO detection.

For the purposes of this survey, airborne magnetic and radiometric data were collected to serve in the exploration for gold-copper deposits.

### 2.1 Magnetic Data

Magnetic surveying is probably the most common airborne survey type to be conducted for both mineral and hydrocarbon exploration. Aeromagnetic surveys measure and record the total intensity of the magnetic field at the magnetometer sensor, which is a combination of the desired magnetic field generated in the Earth as well as tiny variations due to the temporal effects of the constantly varying solar wind and the magnetic field of the survey aircraft. By subtracting the solar, regional, and aircraft effects, the resulting aeromagnetic map shows the spatial distribution and relative abundance of magnetic minerals (most commonly the iron oxide mineral magnetite) in the upper levels of the Earth's crust. The type of survey specifications, instrumentation, and interpretation procedures depend on the objectives of the survey. Typically magnetic surveys are performed for:

1. Geological Mapping - to aid in mapping lithology, structure and alteration.

2. Depth to Basement Mapping - for exploration in sedimentary basins or mineralization associated with the basement surface.

## 2.2 Radiometric Data

Radiometric surveys detect and map natural radioactive emanations, called gamma rays, from rocks and soils. All detectable gamma radiation from earth materials come from the natural decay products of three primary radioelements: uranium (U), thorium (Th), and potassium (K). The purpose of radiometric surveys is to determine either the absolute or relative amounts of U, Th, and K in surface rocks and soils which are then useful in mapping lithology, alteration, and structure.

## 3.0 Survey Operations

Precision GeoSurveys flew the survey out of the Minto airstrip, Yukon. The experience of the pilot helped to ensure that the data quality objectives were met and that the safety of the flight crew was never compromised given the potential risks involved in airborne geophysical surveying. Field processing and quality control checks were done daily.

### 3.1 Operations Base and Crew

The base of operation for this survey was located at the Minto airstrip, 86.0 km east of the Idaho Creek survey block (Figure 6).



Figure 6: Map showing base of operation at Minto airstrip east of the Idaho Creek survey block.

The Precision geophysical crew consisted of four members:

Harmen Keyser – Helicopter Pilot  
 Erik Keyser – Geophysical technician  
 Brenton Keyser – Fixed wing pilot; air and ground support  
 Jenny Poon (off-site) – Geophysicist and data processor

The survey was started and completed on July 5, 2015. The survey did not encounter any delays.

### 3.2 Base Station Specifications

Base station magnetometers were set up before the survey to record diurnal magnetic variations during the survey flights. In this case, two GEM GSM 19T base stations were located at the east end of the Minto airstrip (Table 3; Figures 7 and 8).

Station name	Easting/ Northing	Longitude/ Latitude	Datum/ Projection
GEM 2 (Serial # 2105650 )	0404560E, 6941500N	136° 51' 30.64" W 62° 35' 30.98" N	WGS 84, Zone 8N
GEM 3 (Serial # 5081669)	0404556E, 6941497N	136° 51' 30.89" W 62° 35' 30.88" N	WGS 84, Zone 8N

Table 3: Base station specifications.

Base station readings were reviewed at regular intervals to ensure that no data were collected during periods of high diurnal magnetic activity (greater than 5 nT per minute). The magnetic base stations were installed at a magnetically noise-free area, away from metallic items such as ferromagnetic objects, vehicles, or power lines that could affect the base station or survey data.



Figure 7: GEM 2 (left) and GEM 3 (right) magnetic base stations at Minto airstrip.



Figure 8: GEM 2 and GEM 3 magnetic base stations located near the east end of the Minto airstrip, Yukon on Google Earth.



The diurnal magnetic variations recorded by the stationary base stations were removed from the magnetic data recorded in flight to ensure that the anomalies seen were real and not due to solar activity. On this survey, the magnetic data recorded by GEM 3 were used for diurnal corrections and GEM 2 was used as a backup.

### 3.3 Field Processing and Quality Control

On a flight-by-flight basis, the survey data were transferred from the helicopter's data acquisition system onto a USB flash drive and copied onto a field data processing laptop. The raw data files were in PEI binary data format and were converted into Geosoft GDB database format. Using Geosoft Oasis Montaj 8.3.3, the quality of the data was inspected to see if it met the contract specifications (Table 4). Navigational accuracy (left/right or up/down) for all survey and tie lines were within contract specifications (Figure 9), and no re-flights were required due to navigational error. All suspect anomalies, especially those found on a single flight line, were re-flown for confirmation. Re-flight lines were a minimum of 2000 m long, so that survey line re-flights crossed at least two tie lines, and tie line re-flights crossed at least 10 survey lines.

Specification	Parameter	Details
Line Spacing	Position	Flight line deviation from flight path by more than 10 m left/ right for 1 km or more.
Height		Nominal flight height of 35 m above ground. Flight height deviation by more than 10 m up/down for 1 km or more, provided line deviation from height is not due to tall trees, topography, cultural features, mitigation of livestock harassment, or other obstacles beyond the pilot's control.
GPS		Any flight lines where 3 or less GPS satellites received for distances of greater than 1 km, provided signal loss is not due to topography.
Diurnal Variations	Magnetics	Non-linear magnetic diurnal variations exceed 10nT from a linear chord of length one (1) minute.
Normalized 4 <sup>th</sup> Difference		Magnetic data exceeding 0.30 nT peak to peak for distances greater than 1 km or more (provided noise is not due to geological or cultural features).

Table 4: Contract re-flight specifications.

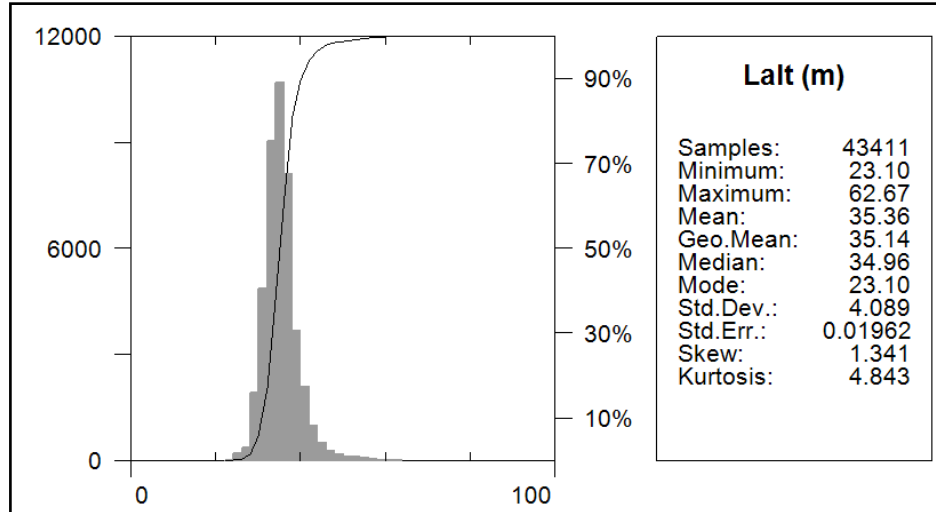


Figure 9: Histogram showing survey elevation vertically above ground.

## 4.0 Aircraft and Equipment

All geophysical and subsidiary equipment are carefully installed on Precision GeoSurveys aircraft. For this survey, a magnetometer, a spectrometer, a data acquisition system, laser altimeter, magnetic compensation system, a pilot guidance unit (PGU), a GPS navigation system, and magnetic base stations were required to carry out the survey and collect quality, high resolution data. The survey magnetometer was carried in an approved “stinger” configuration to enhance flight safety and improve data quality.

### 4.1 Aircraft

Precision GeoSurveys flew the Idaho Creek survey block using a Eurocopter AS350 helicopter (Figure 10), registration C-GOHK. The survey lines were flown at a nominal line spacing of one hundred (100) meters spacing and the tie lines were flown at one thousand (1000) meters spacing for both the magnetometer and spectrometer.



Figure 10: Eurocopter AS350 helicopter equipped with mag stinger for magnetic data acquisition, and internal spectrometer crystals for radiometric data acquisition.

## 4.2 Equipment

### 4.2.1 AGIS

The Airborne Geophysical Information System, AGIS, (Figure 11), is the main computer used in data recording, data synchronizing, displaying real-time quality control data for the geophysical operator, and the generation of navigation information for the pilot and operator display system. Information such as magnetic field, total gamma count, counts of various radioelements (K, U, Th, etc.), temperature, cosmic radiation, barometric pressure, atmospheric humidity and survey altitude can all be monitored on the AGIS on-board display for immediate quality control.



Figure 11: AGIS operator display installed in the Eurocopter AS350, with screen displaying real time flight line recording and navigation parameters.

The AGIS was manufactured by Pico Envirotec and uses standardized Pico software. External sensors are connected to the system via RS-232 serial communication cables. The AGIS data format is converted into Geosoft or ASCII file formats by a conversion program called PEIView. Additional Pico software allows for post or real time magnetic compensation and survey quality control procedures.

#### 4.2.2 Magnetometer

The airborne magnetic sensor used by Precision GeoSurveys is a Scintrex cesium vapor CS-3 magnetometer. The system was housed in a front mounted “stinger” (Figure 12). The CS-3 is a high sensitivity/low noise magnetometer with automatic hemisphere switching and a wide voltage range, the static noise rating for the unit is +/- 0.01 nT. On the AGIS monitor the operator can view the raw magnetic response, the magnetic fourth difference, compensated and uncompensated data, aircraft position, and the survey altitude for immediate QC (quality control) of the magnetic data. The magnetic data are recorded at 10 Hz. A fluxgate magnetic compensator is also used to remove noise created by the movement of the helicopter as it pitches, rolls and yaws within the Earth’s geomagnetic field.



Figure 12: View of the mag stinger.

### 4.2.3 Spectrometer

The IRIS, or Integrated Radiometric Information System, is a fully integrated, gamma radiation detection system containing 16.8 litres of NaI (Tl) synthetic downward looking crystals and 4.2 litres of NaI (Tl) synthetic upward looking crystals (Figure 13) with 256 channel output at 1 Hz sampling rate. The downward-looking crystals are designed to measure gamma rays from below the aircraft and are equipped with upward-shielding high density RayShield® gamma-attenuating blankets to minimize cosmic and solar gamma noise. The upward looking crystal measures solar gamma radiation from above the survey helicopter and a 6 mm thick lead plate is used for downward-shielding. Real time data acquisition, navigation and communication tasks are integrated into a single unit that is installed in the rear cabin of the aircraft.



Figure 13: GRS-10 Thallium-activated Sodium Iodide spectrometer crystal pack. The open unit on the right shows two individual 4.2 liter detectors.

#### 4.2.4 Base Stations

For monitoring and recording of the Earth's diurnal magnetic field variation, Precision GeoSurveys operates two GEM GSM-19T magnetometer base stations continuously throughout the airborne data acquisition operation. The base stations were positioned on the east end of the Minto airstrip, in a region with low magnetic gradient, to give accurate magnetic field readings. The base stations were located in an area away from electric transmission power lines and moving ferrous objects, such as motor vehicles that could affect the survey data integrity.

The GEM GSM-19T magnetometer with integrated GPS (Figure 14) time synchronization uses proton precession technology with a 0.5 Hz sampling rate. The GSM-19T has an accuracy of +/- 0.2 nT at 1 Hz. Base station data are recorded on the internal solid-state memory, and downloaded onto a field laptop computer using a serial cable and GEMLink 5.0 software. Profile plots of the base station readings are generated and updated at the end of each survey day.



Figure 14: GEM GSM-19T proton precession magnetometer.

#### 4.2.5 Laser Altimeter

The pilot is provided with terrain guidance and clearance information from an Opti-Logic RS800 laser altimeter (Figure 15). This is attached at the aft end of the magnetometer boom. The RS800 sensor is a time-of-flight sensor that measures distance by a rapidly-modulated and collimated laser beam that creates a dot on the target surface. The maximum range of the laser altimeter is 700 m off of natural surfaces with an accuracy of +/- 1 meter on 1 x 1 m<sup>2</sup> diffuse target with 50% (+/- 20%) reflectivity. Within the sensor unit, reflected signal light is collected by the lens and focused onto a photodiode. Through serial communications and digital outputs, the ground clearance data are transmitted to an RS-232 compatible port and recorded and displayed by the AGIS and PGU at 10 Hz in meters.

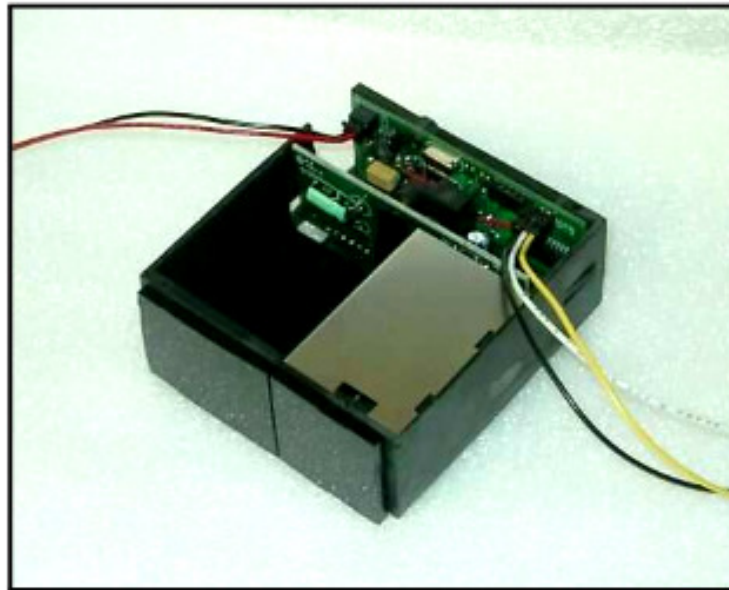


Figure 15: Opti-Logic RS800 laser altimeter.

#### 4.2.6 Pilot Guidance Unit

The PGU (Pilot Guidance Unit) is a graphical display type unit that provides continuous steering and elevation information to the pilot (Figure 16). It is mounted remotely from the data system on top of the helicopter's instrument panel. The PGU assists the pilot in keeping the helicopter on the flight path and at the desired ground clearance.



Figure 16: Pilot Guidance Unit.

The LCD monitor measures 7 inches, with a full VGA 800 x 600 pixel display. The CPU for the PGU is housed in the PC-104 console and uses Windows XP Embedded operating system control, with input from the GPS antenna, laser altimeter, and AGIS.

#### 4.2.7 GPS Navigation System

A Hemisphere R220 GPS receiver (Figure 17) navigation system integrated with the pilot display (PGU) and AGIS provided navigational information and control. The R220 GPS receiver features RTK (Real Time Kinematic) for fast, reliable, and long range centimeter level performance. It employs COAST technology that allows continuous operation for at least 40 minutes during temporary signal outages.





Figure 17: Hemisphere R220 GPS Receiver.

It can track GPS, SBAS (Satellite-Based Augmentation System), and L-Band (OmniSTAR HP and XP) differential corrections to provide high precision positioning.

## 5.0 Data Acquisition Equipment Checks and Calibration

Airborne equipment tests were conducted at the start of the survey. There are three tests conducted for the airborne magnetometer: compensation flight, lag test, and heading error test. Gamma ray spectrometer checks and calibrations are also conducted prior to the start of the survey. The three spectrometer tests were the calibration pad test, cosmic flight test, and the Breckenridge test range.

### 5.1 Magnetometer Checks

#### 5.1.1 Compensation Flight Test

During aeromagnetic surveying a small but significant amount of noise is introduced to the magnetic data by the aircraft itself, as the magnetometer is within the helicopter's magnetic field. Movement of the aircraft (roll, pitch and yaw) and the permanent magnetization of certain aircraft parts (engine and other ferrous magnetic objects) contribute to this noise. To remove noise generated by the aircraft a process called magnetic compensation is implemented. The magnetic compensation process starts with a test flight at the beginning of the survey where the aircraft flies in the four orthogonal headings required for the survey (066°/246° and 156°/336° in the case of this survey) at a sufficient altitude (typically > 1,500 m AGL) where the Earth's magnetic field becomes nearly uniform at the scale of the compensation flight (Table 5). In each heading direction, three specified roll, pitch, and yaw maneuvers are performed by the pilot at

constant elevation so that any magnetic variation recorded by the airborne magnetometer can be attributed to the aircraft movement. The variations recorded by these maneuvers provide the data that are required to calculate the necessary parameters for compensating the magnetic data and removing the aircraft noise.

Pre-Compensation					Post-Compensation				
Heading	Roll	Pitch	Yaw	Total	Heading	Roll	Pitch	Yaw	Total
062°	8.7980	2.7880	2.4176	14.0036	062°	0.1498	0.1672	0.1256	0.4426
151°	8.4538	3.9726	2.0502	14.4766	151°	0.1938	0.1533	0.2084	0.5555
242°	5.8716	3.3845	1.7683	11.0244	242°	0.1568	0.1561	0.2220	0.5349
328°	6.1246	2.3431	1.5909	10.0586	328°	0.1195	0.1860	0.1210	0.4265
<b>Total</b>	29.2480	12.4882	7.8270		<b>Total</b>	0.6199	0.6626	0.6770	
<b>FOM =49.5632 nT</b>					<b>FOM = 1.9595 nT</b>				

Table 5: Figure of Merit maneuver test results for compensation flight flown on July 5, 2015 at an area southwest of Mayo, Yukon.

### 5.1.2 Lag Test

A lag test was performed to determine the relationship between the time the digital reading was recorded by the instrument magnetic sensor and the time for the position fix that the fiducial of the reading was obtained by the GPS system. The test was flown in the four orthogonal headings over an identifiable magnetic anomaly (ie. Truck, Trailer, etc.) at survey speed and height. A lag of 7 fiducials (0.7 seconds) was determined from the lag test.

### 5.1.3 Heading Error Test

To determine the magnetic heading effect a cloverleaf pattern flight test was conducted. The cloverleaf test was flown in the same orthogonal headings as the survey and tie lines (066°/246° and 156°/336° at >1000 m AGL in an area with low magnetic gradient. For all four directions the survey helicopter must pass over the same mid-point all four times at the same elevation (Table 6 and Figure 18).

Line Number	Fiducials	Heading	Mag (nT)	Average (nT)
L066	779.8	NW – 066°	57113.2454	
L156	563.9	SE – 156°	57111.3228	
L246	907.1	SW - 246°	57084.7276	
L336	690.4	NE - 336°	57085.9402	
				57098.809

Table 6: Heading error test data format flown on July 5, 2015 southwest of Mayo, Yukon.

```

/Geosoft Heading Correction Table
/
/=Direction:real:i
/=Correction:real
/
/Direction Correction|
066      -14.4364
156      -12.5138
246      +14.0814
336      +12.8688

```

Figure 18: Heading data results in .tbl format in Geosoft table.

## 5.2 Gamma-ray Spectrometer Checks and Calibrations

Pre-survey calibrations and testing of the GRS-10 airborne gamma-ray spectrometry system were carried out prior to the start of the survey. The calibration of the spectrometer system involved three tests which enabled the conversion of airborne data to ground concentration of natural radioactive elements. These tests were the calibration pad test, cosmic flight test, and the Breckenridge test range. The measurements were made in accordance with IAEA technical report series No. 323, “Airborne Gamma Ray Spectrometer Surveying”, and AGSO Record 1995/60, “A Guide to the Technical Specification for Airborne Gamma-Ray Surveys”.

### 5.2.1 Calibration Pad Test

The calibration pad test was conducted by Pico Envirotec at the GSC (Geological Survey of Canada) testing facility in Ottawa, Ontario over the approved GSC calibration pad. It is a slab of concrete containing known concentrations of the radioelements (K, Th, and U) and is ideally used to simulate a geological source of radiation. The measurements collected from the calibration pad test are used to determine the Compton scattering and Grasty Backscatter (spectral overlap between element windows) coefficients.

### 5.2.2 Cosmic Flight Test

While the background source of gamma radiation from the aircraft itself is essentially constant, the amount of signal detected from ground sources varies with ground clearance. As the height of the aircraft increases, the distance between the ground and the spectrometer crystals increase, and the proportion of cosmic radiation in each spectral window increases exponentially due to radiation of cosmic origin. The cosmic flight test is conducted to determine the aircraft’s background attenuation coefficients for the detector crystal packs and the cosmic coefficients. The pilot is required to fly over the same location repeatedly in opposite directions starting from 1,500 m to 3,000 m at 500 m intervals for approximately 2

minutes each to collect gamma data used to determine the amount of non-terrestrial gamma signal.

### 5.2.3 Breckenridge Test Range

The Breckenridge test range is very similar to the cosmic flight test but is conducted at lower elevations (from ground level). The pilot is required to fly over the same location at the following elevations in meters above ground; 30, 50, 100, 150, 200, 250, and 300. As the distance of the aircraft increases away from the radioactive ground source, the source signature exponentially degrades. As a result, this test is used to determine the altitude attenuation coefficients and the radio-element sensitivity of the airborne spectrometer system.

## 6.0 Data Processing

After all the data were collected from a survey flight several procedures were undertaken to ensure that the data met a high standard of quality. All data were processed using Pico Envirotec software and Geosoft Oasis Montaj 8.3.3 geophysical processing software along with proprietary processing algorithms.

### 6.1 Magnetic Processing

The data obtained from the compensation flight test were applied to the raw magnetic data before any further processing and editing. A computer program called PEIComp was used to create a model from the compensation flight test for each survey to remove the noise induced by aircraft movement; this model was applied to each survey flight so the data could be further processed.

Over glassy water or fog, the laser altimeter is unable to record a valid reading and a zero is recorded; therefore all data points recorded at zero were replaced with a nominal height of 35 m. Filtering was then applied to the laser altimeter data to remove vegetation clutter and to show the actual ground clearance. To remove vegetation clutter a Rolling Statistic filter was applied to the laser altimeter data and a low pass filter was used to smooth out the laser altimeter profile to eliminate isolated noise. As a result, filtering the data will yield a more uniform surface in close conformance with the actual terrain. A digital terrain model channel was calculated by subtracting the filtered laser altimeter data from the filtered GPS altimeter data defined by the WGS 84 ellipsoidal height.

The processing of the magnetic data first involved the correction for diurnal variations. The base station data that were used for the correction came from GEM 3. The diurnal data were edited, plotted and merged into a Geosoft (.gdb) database on a daily basis. The airborne magnetic data were corrected for diurnal variations by subtracting the observed magnetic base station deviations. Following the diurnal correction, a lag correction was applied. A lag correction of 0.7 seconds was applied to the total magnetic field data to compensate for the combination of lag in the recording system and the magnetometer

sensor flying 15.2 m ahead of the GPS antenna. Lastly, a heading correction was applied to the data.

The initial Total Magnetic Intensity (TMI) data from the survey and tie lines were used to level the entire survey dataset. Two forms of leveling were applied to the corrected data: conventional leveling and micro-leveling. There were two components to conventional leveling; the first involved statistical leveling of magnetic data to correct miss ties (intersection errors) followed by specific patterns or trends. For the second component, tie lines were brought to a common regional base value using the mean value of the cross-level error. To obtain the best possible leveled data, individual corrections were edited at selected intersections. Lastly, micro-leveling was applied to the corrected conventional leveled data. This will remove any residual noise related to flight line direction, and any low amplitude component of flight line noise, that still remained in the data after tie line leveling.

### 6.1.1 IGRF Removal and Calculation of the First Vertical Derivative

The International Geomagnetic Reference Field (IGRF) model is the empirical representation of the Earth's magnetic field (main core field without external sources) collected and disseminated from satellites and from observatories around the world. The IGRF is generally revised and updated every five years by a group of modelers associated with the International Association of Geomagnetism and Aeronomy (IAGA). In this case, the IGRF values were calculated from the recently updated model (IGRF – 12) year 2015 and the actual survey dates were obtained from the “Date” channel.

With the removal of the IGRF from the observed Total Magnetic Intensity (TMI) a Residual Magnetic Intensity (RMI) was generated. This created a more valid model of individual near surface anomalies and the data will not be referenced to a time which can be easily incorporated into databases of magnetic data acquired in the past or in the future.

The first vertical derivative was computed from the Total Magnetic Intensity (TMI) data. Long wavelengths and vertical rate of change were suppressed in the magnetic field. Therefore, the edges of magnetic anomalies were highlighted and spatial resolution was increased.

## 6.2 Radiometric Processing

Radiometric surveys map the concentration of radioelements at or near the earth's surface; typically up to 1.5 meters below surface. Thus, the first step which is vital before processing of the airborne radiometric data was to calibrate the spectrometer system. Once calibration of the system was complete, the radiometric data were processed by windowing the full spectrum to create channels for U, K, Th and total count. A 5-point Hanning filter was applied to the Cosmic window before going any further with processing the radiometric data.

Aircraft background and cosmic stripping corrections were applied to all three elements, and total count using the following formula:

$$C_{ac} = C_{lt} - (a_c + b_c * \text{Cos}_f)$$

where:  $C_{ac}$  is the background and cosmic corrected channel  
 $C_{lt}$  is the live time corrected channel  
 $a_c$  is the aircraft background for this channel  
 $b_c$  is the cosmic stripping coefficient for this channel  
 $\text{Cos}_f$  is the filtered cosmic channel

The radon backgrounds were first removed and followed by Compton stripping. Spectral overlap corrections were applied on to potassium, uranium, and thorium as part of the Compton stripping process. This was done by using the stripping ratios that have been calculated for the spectrometer by prior calibration; this breaks the corrected elemental values down into the apparent radioelement concentrations. Lastly, attenuation corrections were applied to the data which involves nominal survey altitude corrections, in this case 35.4 metres is applied to total count, potassium, uranium, and thorium data.

With all corrections applied to the radiometric data, the final step was to convert the corrected potassium, uranium, and thorium to apparent radioelement concentrations using the following formula:

$$eE = C_{cor} / s$$

where:  $eE$  is the element concentration K(%) and equivalent element concentration of U(ppm) & Th(ppm)  
 $s$  is the experimentally determined sensitivity  
 $C_{cor}$  is the fully corrected channel

Finally, the natural air exposure rate was determined by using the following formula:

$$E = [(13.08 * K + 5.43 * eU + 2.69 * eTh) / 8.69]$$

where:  $E$  is the absorption dose rate in  $\mu\text{R}/\text{h}$   
 $K$  is the concentration of potassium (%)  
 $eU$  is the equivalent concentration of uranium (ppm)  
 $eTh$  is the equivalent concentration of thorium (ppm)

To calculate for radiometric ratios the guidelines of the IAEA were followed. Due to statistical uncertainties in the individual radioelement measurements, some care was taken in the calculation of the ratio in order to obtain statistically significant values. Following IAEA guidelines, the method of determining ratios of the eU/eTh, eU/K and eTh/K was as follows:

1. Any data points where the potassium concentration was less than 0.25% were neglected.
2. The element with the lowest corrected count rate was determined.
3. The element concentrations of adjacent points on either side of each data point were summed until they exceeded a pre-determined threshold value. This threshold was set to be equivalent to 100 counts of the element with the lowest count rate. Additional minimum thresholds of 1.6% for potassium, 20 ppm for thorium, and 30 ppm for uranium were set up to ensure meaningful ratios.
4. The ratios were calculated using the accumulated sums.

With this method, the errors associated with the calculated ratios were minimized and comparable for all data points.

## 7.0 Deliverables

All digital data are presented on a compact disc (CD) and USB memory stick with the logistic report. The survey data are presented as digital databases, maps, and a report.

### 7.1 Digital Data

The file format will be provided in two (2) formats, the first will be a .GDB file for use in Geosoft Oasis Montaj, the second format will be a .XYZ file, this is text file. A complete file provided in each format will contain magnetic and radiometric data separately. Full description of the digital data and contents are included in the report (Appendix B).

The digital data are represented into grids. The following grids are prepared for the Idaho Creek survey block listed below:

- Digital terrain model (DTM)
- Total magnetic intensity (TMI)
- Residual magnetic intensity (RMI) – removal of IGRF from TMI
- Calculated vertical gradient (CVG) - first vertical derivative of TMI
- Potassium – Equivalent Concentration (%K)
- Thorium – Equivalent Concentration (eTh)
- Uranium – Equivalent Concentration (eU)
- Total Count – Equivalent Dose Rate (TCcor)
- Total Count – Exposure Rate (TCexp)
- Potassium over Thorium Ratio (%K/eTh)

- Potassium over Uranium Ratio (%K/eU)
- Uranium over Thorium Ratio (eU/eTh)
- Thorium over Potassium Ratio (eTh/%K)
- Uranium over Potassium Ratio (eU/%K)
- Ternary Map (TM)

## 7.2 KMZ Grids

The digital data represented into grids were exported into kmz files which can be displayed using Google Earth. The grids can be draped onto topography and rendered to give a 3D view.

## 7.3 Maps

Digital maps were created for the Idaho Creek survey block. The following map products were prepared:

Survey Overview Maps (colour images with elevation contour lines):

- Actual flight lines
- Digital terrain model

Magnetic Maps (colour images with elevation contour lines):

- Total magnetic intensity
- Total magnetic intensity with plotted flight lines
- Residual magnetic intensity
- Calculated vertical gradient of the total magnetic intensity

Radiometric Maps (colour images with elevation contour lines):

- Potassium – Equivalent Concentration in Percentage
- Thorium – Equivalent Concentration
- Uranium – Equivalent Concentration
- Total Count – Equivalent Dose Rate
- Total Count – Exposure Rate
- Potassium over Thorium Ratio
- Potassium over Uranium Ratio
- Uranium over Thorium Ratio
- Thorium over Potassium Ratio
- Uranium over Potassium Ratio
- Ternary Map

All maps were prepared in WGS 84 and UTM zone 7N.



## 7.4 Report

The logistics report provides information on the acquisition procedures, magnetic and radiometric processing, and presentation of the Idaho Creek survey block data. A pdf copy of the report is included along with the digital data and maps that are provided on the CD and USB stick.

## **Appendix A**

### Equipment Specifications

- GEM GSM-19T Proton Precession Magnetometer (Base Station)
- Hemisphere R220 GPS Receiver
- Opti-Logic RS800 Laser Altimeter
- HC-S3 Temperature and Relative Humidity Probe
- Barometric Pressure Setra Model 276
- Scintrex CS-3 Survey Magnetometer
- Bartington Mag-03 three-axis fluxgate magnetic field sensor
- Pico Envirotec GRS-10 Gamma Spectrometer
- Pico Envirotec AGIS data recorder system (for Navigation, Gamma spectrometer, VLF-EM and Magnetometer Data Acquisition)

## GEM GSM-19T Proton Precession Magnetometer (Base Station) Specifications

<b>Configuration Options</b>	15
<b>Cycle Time</b>	999 sec to 0.5 sec
<b>Environmental</b>	-40°C to +60°C
<b>Gradient Tolerance</b>	7,000 nT/m
<b>Magnetic Readings</b>	299,593
<b>Operating Range</b>	10, 000 to 120,000 nT
<b>Power</b>	12 V @ 0.62 A
<b>Sensitivity</b>	0.1 nT @ 1 sec
<b>Weight (Console/ Sensor)</b>	3.2 Kg
<b>Integrated GPS</b>	Yes

## Hemisphere R220 GPS Receiver Specifications

<b>GPS Sensor</b>	Receiver Type	L1 and L2 RTK with carrier phase	
	Channels	12 L1CA GPS 12 L1P GPS 12 L2P GPS 3 SBAS or 3 additional L1CA GPS	
	Update Rate	10 Hz standard, 20 Hz available	
	Cold Start Time	<60 s	
	Warm Start Time 1	30 s (valid ephemeris)	
	Warm Start Time 2	30 s ( almanac and RTC)	
	Hot Start Time	10 s typical (valid ephemeris and RTC)	
	Reacquisition	<1 s	
	Differential Options	SBAS, Autonomous, External RTCM, RTK, OmniSTAR (HP/XP)	
<b>Horizontal Accuracy</b>		RMS (67%)	2DRMS (95%)
	RTK <sup>1, 2</sup>	10 mm + 1 ppm	20 mm+2 ppm
	OmniSTAR HP <sup>1, 3</sup>	0.1 m	0.2 m
	SBAS (WAAS) <sup>1</sup>	0.3 m	0.6 m
	Autonomous, no SA <sup>1</sup>	1.2 m	2.5 m
<b>L-Band Sensor</b>	Channel	Single channel	
	Frequency Range	1530 MHz to 1560 MHz	
	Satellite Selection	Manual or Automatic (based on location)	
	Startup and Satellite Reacquisition Time	15 seconds typical	
<b>Communications</b>	Serial Ports	2 full duplex RS232	
	Baud Rates	4800 – 115200	
	USB Ports	1 Communications, 1 Flash Drive data storage	
	Correction I/O Protocol	Hemisphere GPS proprietary, RTCM v2.3 (DGPS), RTCM v3 (RTK), CMR, CMR+NMEA 0183, Hemisphere GPS binary	
	Timing Output	1 PPS (HCMOS, active high, rising edge sync, 10kΩ, 10pF load)	
	Event Marker Input	HCMOS, active low, falling edge sync, 10kΩ	
<b>Environmental</b>	Operating Temperature	-30°C to +65°C	
	Storage Temperature	-40°C to +85°C	
	Humidity	95% non-condensing	
<b>Power GPS Sensor</b>	Input Voltage Range	8 to 36 VDC	
	Consumption, RTK	<4.9W (0.40A @ 12 VDC typical)	
	Consumption, OmniSTAR	<5.5W (0.46A @ 12 VDC typical)	

<sup>1</sup> Depends on multipath environment, number of satellites in view, satellite geometry and ionospheric activity.

<sup>2</sup> Depends also on baseline length.

<sup>3</sup> Requires a subscription from OmniSTAR.

## Opti-Logic RS800 Laser Altimeter Specifications

<b>Accuracy</b>	+/- 1m on 1x1 m <sup>2</sup> diffuse target with 50% reflectivity
<b>Resolution</b>	0.2 m
<b>Communication Protocol</b>	RS232-8,N,1
<b>Baud Rate</b>	19200
<b>Data Raw Counts</b>	~200 Hz
<b>Data Calibrated Range</b>	~10 Hz
<b>Calibrated Range Units</b>	Feet, Meters, Yards
<b>Laser</b>	Class I (eye-safe) 905nm +/- 10nm
<b>Power</b>	7-9VDC conditioned required, current draw at full power (~ 1.8W)
<b>Laser Wavelength</b>	RS100 905 nm +/- 10 nm
<b>Laser Divergence</b>	Vertical axis – 3.5 mrad half- angle divergence; Horizontal axis – 1 mrad half- angle divergence; (Approximate beam footprint at 100 m is 35 cm x 5 cm)
<b>Data Rate</b>	~200 Hz raw counts for un-calibrated operation; ~10 Hz for calibrated operation (averaging algorithm seeks 8 good readings)
<b>Dimensions</b>	32 x 78 x 84 mm (lens face cross section is 32 x 78 mm)
<b>Weight</b>	< 227 g (8oz)
<b>Casing</b>	RS100/RS400/RS800 units are supplied as OEM modules consisting of an open chassis containing optics and circuit boards. Custom housings can be designed and built on request.

## HC-S3 Temperature and Relative Humidity Probe Specifications

<b>Operating Temperature</b>	-40°C to +60°C
<b>Temperature Output Signal Range</b>	0 to 1.0 VDC
<b>Temperature Resolution</b>	0.1°C or better
<b>Relative Humidity(RH) Measurement Range</b>	0 to 100 % non-condensing
<b>RH Output Signal Range</b>	0 to 1.0 VDC
<b>RH Accuracy At 23°C</b>	± 1.5 % RH
<b>RH Response Time</b>	12 to 15 secs
<b>RH Typical Long Term Stability</b>	Better than 1% RH per year
<b>Probe Length</b>	168 mm (6.6 in.)
<b>Probe Body Diameter</b>	15.25 mm (0.6 in.)
<b>Housing Material</b>	Polycarbonate
<b>Power Consumption</b>	< 4 mA
<b>Supply Voltage</b>	3.5 to 50 VDC (typically 5 VDC)
<b>Settling Time after power is switched on</b>	3 secs

**Barometric Pressure Setra Model 276 Specifications**

<b>Pressure Ranges</b>	600 to 1100 hPa/mb 800 to 1100 hPa/mb 0 to 20 psia
<b>Accuracy</b>	±0.25% FS
<b>Output</b>	0.1 to 5.1 VDC 0.5 to 4.5 VDC
<b>Excitation</b>	12 VDC (9.0 to 14.5) 24 VDC (21.6 to 26.0) 5 VDC (4.9 to 7.1)
<b>Size</b>	2" dia. x 1" (5 cm x 2.5 cm)

## Scintrex CS-3 Magnetometer Specifications

<b>Operating Principal</b>	Self-oscillation split-beam Cesium Vapor (non-radioactive Cs-133)
<b>Operating Range</b>	15,000 to 105,000 nT
<b>Gradient Tolerance</b>	40,000 nT/metre
<b>Operating Zones</b>	10° to 85° and 95° to 170°
<b>Hemisphere Switching</b>	<ul style="list-style-type: none"> <li>a) Automatic</li> <li>b) Electronic control actuated by the control voltage levels (TTL/CMOS)</li> <li>c) Manual</li> </ul>
<b>Sensitivity</b>	0.0006 nT $\sqrt{\text{Hz}}$ rms
<b>Noise Envelope</b>	Typically 0.002 nT P-P, 0.1 to 1 Hz bandwidth
<b>Heading Error</b>	+/- 0.25 nT (inside the optical axis to the field direction angle range 15° to 75° and 105° to 165°)
<b>Absolute Accuracy</b>	<2.5 nT throughout range
<b>Output</b>	<ul style="list-style-type: none"> <li>a) Continuous signal at the Larmor frequency which is proportional to the magnetic field ( proportionality constant 3.49857 Hz/nT) sine wave signal amplitude modulated on the power supply voltage</li> <li>b) Square wave signal at the I/O connector, TTL/CMOS compatible</li> </ul>
<b>Information Bandwidth</b>	Only limited by the magnetometer processor used
<b>Sensor Head</b>	Diameter: 63 mm (2.5") Length: 160 mm (6.3") Weight: 1.15 kg (2.6 lb)
<b>Sensor Electronics</b>	Diameter: 63 mm (2.5") Length: 350 mm (13.8") Weight: 1.5 kg (3.3 lb)
<b>Cable, Sensor to Sensor Electronics</b>	3m (9' 8"), lengths up to 5m (16' 4") available
<b>Operating Temperature</b>	-40°C to +50°C
<b>Humidity</b>	Up to 100%, splash proof
<b>Supply Power</b>	24 to 35 Volts DC
<b>Supply Current</b>	Approx. 1.5A at start up, decreasing to 0.5A at 20°C
<b>Power Up Time</b>	Less than 15 minutes at -30°C



## Bartington Mag-03 three-axis fluxgate magnetic field sensor Specifications

<b>Number of Axes</b>	3
<b>Bandwidth</b>	0 to 3kHz at 50 $\mu$ T peak
<b>Internal Noise</b>	Basic version: >10 to 20pTrms/ $\sqrt{\text{Hz}}$ at 1Hz Standard version: 6 to $\leq$ 10pTrms/ $\sqrt{\text{Hz}}$ at 1Hz Low Noise version: <6pTrms/ $\sqrt{\text{Hz}}$ at 1Hz
<b>Scaling error (DC)</b>	< $\pm$ 0.5%
<b>Orthogonality error</b>	<0.1 $^{\circ}$
<b>Alignment error (Z axis to reference face)</b>	<0.1 $^{\circ}$
<b>Linearity error</b>	<0.0015%
<b>Frequency response</b>	0 to 1kHz maximally flat, $\pm$ 5% maximum at 1kHz
<b>Input voltage</b>	$\pm$ 12V to $\pm$ 17V
<b>Supply current</b>	+30mA, -10mA (+1.4mA per 100 $\mu$ T for each axis)
<b>Power supply rejection ratio</b>	5 $\mu$ V/V (-106dB)
<b>Analog output</b>	$\pm$ 10V ( $\pm$ 12V supply) swings to within 0.5V of supply voltage
<b>Output impedance</b>	10 $\Omega$
<b>Operating temperature range</b>	-40 $^{\circ}$ C to +70 $^{\circ}$ C
<b>Environmental protection</b>	IP51
<b>Dimensions (W x H x L)</b>	32 x 32 x 152mm
<b>Weight</b>	160g
<b>Enclosure material</b>	Reinforced epoxy
<b>Connector</b>	ITT Cannon DEM-9P-NMB
<b>Mating connector</b>	ITT Cannon DEM-9S-NMB
<b>Mounting</b>	2 x M5 fixing holes

## Pico Envirotec GRS-10 Gamma Spectrometer Specifications

<b>Crystal volume</b>	16.8 litres of NaI (Tl) synthetic downward looking crystals and 4.2 litres of NaI (Tl) synthetic upward looking crystals
<b>Resolution</b>	256/512 channels
<b>Tuning</b>	Automatic using peak determination algorithm
<b>Detector</b>	Digital Peak
<b>Calibration</b>	Fully automated detector
<b>Real Time</b>	Linearization and gain stabilization
<b>Communication</b>	RS232
<b>Detectors</b>	Expandable to 10 detectors and digital peak
<b>Count Rate</b>	Up to 60,000 cps per detector
<b>Count Capacity per channel</b>	65545
<b>Energy detection range:</b>	36 KeV to 3 MeV
<b>Cosmic channel</b>	Above 3 MeV
<b>Upward Shielding</b>	RayShield® non-radioactive shielding on downward looking crystals
<b>Downward Shielding</b>	6 mm thick lead plate is used for downward-shielding
<b>Spectra</b>	Collected spectra of 256/512 channels, internal spectrum resolution 1024
<b>Software</b>	Calibration: High voltage adjustment, linearity correction coefficients calculation, and communication test support Real Time Data Collection: Automatic Gain real time control on natural isotopes, and PC based test and calibration software suite
<b>Sensor</b>	Each box containing two (2) gamma detection NaI(Tl) crystals – each 4.2 liters. (256 cu in.) (approx. 100 x 100 x 650 mm) Total volume of approx 8.4 litres or 512 cu in with detector electronics
<b>Spectra Stabilization</b>	Real time automatic corrections on radio nuclei: Th, Ur, K. No implanted sources

## Pico Envirotec AGIS data recorder system Specifications

(for Navigation, Gamma spectrometer, VLF-EM and Magnetometer Data Acquisition)

<b>Functions</b>	Airborne Geophysical Information System (AGIS) with integrated Global Positioning System Receiver (GPS) and all necessary navigation guidance software. Inputs for geophysical sensors - portable gamma ray spectrometer GRS-10, MMS4 Magnetometer, Totem 2A EM, A/D converter, temperature probe, humidity probe, barometric pressure probe, and laser altimeter. Output for the multi-parameter PGU (Pilot Guidance Unit)
<b>Display</b>	Touch screen with display of 800 x 600 pixels; customized keypad and operator keyboard. Multi-screen options for real-time viewing of all data inputs, fiducial points, flight line tracking, and GPS channels by operator.
<b>GPS Navigation</b>	Garmin 12-channel, WAAS-enabled
<b>Data Sampling</b>	Sensor dependent
<b>Data Synchronization</b>	Synchronized to GPS position
<b>Data File</b>	PEI Binary data format
<b>Storage</b>	80 GB
<b>Supplied Software</b>	PEIView: Allows fast data Quality Control (QC) Data Format: Geosoft GBN and ASCII output PEIConv: For survey preparation and survey plot after data acquisition
<b>Software</b>	Calibration: High voltage adjustment, linearity correction coefficients calculation, and communication test support Real Time Data Collection: Automatic Gain real time control on natural isotopes and PC based test and calibration software suite
<b>Power Requirements</b>	24 to 32 VDC
<b>Temperature</b>	Operating: -10°C to +55°C; storage: -20°C to +70°C

## **Appendix B**

### Digital File Descriptions

- Magnetic database description
- Radiometric database description
- Grids
- Maps

Magnetic Database:

Abbreviations used in the GDB files listed below:

<b>Channel</b>	<b>Units</b>	<b>Description</b>
<b>X_WGS84</b>	m	UTM Easting – WGS 84 Zone 7 North
<b>Y_WGS84</b>	m	UTM Northing – WGS 84 Zone 7 North
<b>Lon_deg</b>	degree	Longitude
<b>Lat_deg</b>	degree	Latitude
<b>Date</b>	yyyy/mm/dd	Dates of the survey flight(s)
<b>FLT</b>		Flight Line numbers
<b>LineNo</b>		Line numbers
<b>STL</b>		Number of satellite(s)
<b>GPSfix</b>		GPS fix
<b>GPStime</b>	Hours:min:secs	GPS time (UTC)
<b>Geos_m</b>	m	Geoidal separation
<b>GHead_deg</b>	degree	Heading of the helicopter
<b>XTE_m</b>	m	Flight line cross distance
<b>Galt</b>	m	GPS height – WGS 84 Zone 7 North
<b>Lalt</b>	m	Laser Altimeter readings
<b>DTM</b>	m	Digital Terrain Model
<b>basemag</b>	nT	Base station diurnal data
<b>IGRF</b>		International Geomagnetic Reference Field 2015
<b>Declin</b>	Decimal degree	Calculated declination of magnetic field
<b>Inclin</b>	Decimal degree	Calculated inclination of magnetic field
<b>TMI</b>	nT	Total Magnetic Intensity
<b>RMI</b>	nT	Residual Magnetic Intensity

Radiometric Database:

Abbreviations used in the GDB files listed below:

<b>Channel</b>	<b>Units</b>	<b>Description</b>
<b>X_WGS84</b>	m	UTM Easting – WGS 84 Zone 7 North
<b>Y_WGS84</b>	m	UTM Northing – WGS 84 Zone 7 North
<b>Lon_deg</b>	degree	Longitude
<b>Lat_deg</b>	degree	Latitude
<b>Date</b>	yyyy/mm/dd	Dates of the survey flight(s)
<b>FLT</b>		Flight numbers
<b>LineNo</b>		Line numbers
<b>STL</b>		Number of satellite(s)
<b>GPStime</b>	Hours:min:secs	GPS time (UTC)
<b>Geos_m</b>	m	Geoidal separation
<b>GPSFix</b>		GPS fix
<b>GHead_deg</b>	degree	Heading of the helicopter
<b>XTE_m</b>	m	Flight line cross distance
<b>Galt</b>	m	GPS height – WGS 84 Zone 7 North
<b>Lalt</b>	m	Laser Altimeter readings
<b>DTM</b>	m	Digital Terrain Model
<b>BaroSTP_kP</b>	KiloPascal	Barometric Altitude (Press and Temp Corrected)
<b>Temp_degC</b>	Degrees C	Air Temperature
<b>Press_kP</b>	KiloPascal	Atmospheric Pressure
<b>COSFILT</b>	counts/sec	Spectrometer - Filtered Cosmic
<b>URUFILT</b>	counts /sec	Spectrometer - Filtered Upward Uranium
<b>Kcor</b>	%	Equivalent Concentration - Potassium
<b>THcor</b>	ppm	Equivalent Concentration - Thorium
<b>Ucor</b>	ppm	Equivalent Concentration - Uranium
<b>TCcor</b>	μR	Equivalent Dose Rate
<b>TCexp</b>	μR/hour	Exposure Rate - SUM(%k, eU, eTh) * determined factors
<b>THKratio</b>		Spectrometer – eTh/%K ratio
<b>UKratio</b>		Spectrometer – eU/%K ratio
<b>UTHratio</b>		Spectrometer – eU/eTh ratio

Grids: Idaho Creek Survey Block, WGS 84 Datum, Zone 7N

FILE NAME	DESCRIPTION
IdahoCreek_DTM_25m.grd	Idaho Creek survey block digital terrain model gridded at 25 m cell size
IdahoCreek_TMI_25m.grd	Idaho Creek survey block total magnetic intensity gridded at 25 m cell size
IdahoCreek_RMI_25m.grd	Idaho Creek survey block residual magnetic intensity gridded at 25 m cell size
IdahoCreek_CVG_25m.grd	Idaho Creek survey block calculated vertical gradient of TMI gridded at 25 m cell size
IdahoCreek_Kcor_25m.grd	Idaho Creek survey block potassium (%K) - equivalent concentration in percentage gridded at 25 m cell size
IdahoCreek_Thcor_25m.grd	Idaho Creek survey block Thorium (eTh) – equivalent concentration gridded at 25 m cell size
IdahoCreek_Ucor_25m.grd	Idaho Creek survey block Uranium (eU) – equivalent concentration gridded at 25 m cell size
IdahoCreek_TCcor_25m.grd	Idaho Creek survey block Total Count (TCcor) – equivalent dose rate gridded at 25 m cell size
IdahoCreek_TCexp_25m.grd	Idaho Creek survey block Total Count (TCexp) – exposure rate gridded at 25 m cell size
IdahoCreek_KThratio_25m.grd	Idaho Creek survey block potassium over thorium ratio (%K/eTh) gridded at 25 m cell size
IdahoCreek_KUratio_25m.grd	Idaho Creek survey block potassium over uranium ratio (%K/eU) gridded at 25 m cell size
IdahoCreek_UThratio_25m.grd	Idaho Creek survey block uranium over thorium ratio (eU/eTh) gridded at 25 m cell size
IdahoCreek_ThKratio_25m.grd	Idaho Creek survey block thorium over potassium ratio (eTh/%K) gridded at 25 m cell size
IdahoCreek_UKratio_25m.grd	Idaho Creek survey block uranium over potassium ratio (eU/%K) gridded at 25 m cell size

Maps: Idaho Creek survey block, WGS 84 Datum, Zone 7N (jpegs and pdfs)

FILE NAME	DESCRIPTION
IdahoCreek_ActualFlightLines	Idaho Creek survey block survey block plotted actual flown flight lines
IdahoCreek_DTM_25m	Idaho Creek survey block digital terrain model gridded at 25 m cell size
IdahoCreek_TMI_25m	Idaho Creek survey block total magnetic intensity gridded at 25 m cell size
IdahoCreek_TMI_with_FlightLines_25m	Idaho Creek survey block total magnetic intensity with plotted actual flight lines gridded at 25 m cell size
IdahoCreek_RMI_25m	Idaho Creek survey block residual magnetic intensity gridded at 25 m cell size
IdahoCreek_CVG_25m	Idaho Creek survey block calculated vertical gradient of TMI gridded at 25 m cell size
IdahoCreek_Kcor_25m	Idaho Creek survey block potassium (%K) - equivalent concentration in percentage gridded at 25 m cell size
IdahoCreek_Thcor_25m	Idaho Creek survey block Thorium (eTh) – equivalent concentration gridded at 25 m cell size
IdahoCreek_Ucor_25m	Idaho Creek survey block Uranium (eU) – equivalent concentration gridded at 25 m cell size
IdahoCreek_TCcor_25m	Idaho Creek survey block Total Count (TCcor) – equivalent dose rate gridded at 25 m cell size
IdahoCreek_TCexp_25m	Idaho Creek survey block Total Count (TCexp) – exposure rate gridded at 25 m cell size
IdahoCreek_KThratio_25m	Idaho Creek survey block potassium over thorium ratio (%K/eTh) gridded at 25 m cell size
IdahoCreek_KUratio_25m	Idaho Creek survey block potassium over uranium ratio (%K/eU) gridded at 25 m cell size
IdahoCreek_UThratio_25m	Idaho Creek survey block uranium over thorium ratio (eU/eTh) gridded at 25 m cell size
IdahoCreek_ThKratio_25m	Idaho Creek survey block thorium over potassium ratio (eTh/%K) gridded at 25 m cell size
IdahoCreek_TernaryMap_25m	Idaho Creek survey block displaying ratios of all three elements (%K, eTh, eU)



## **Appendix C**

### Idaho Creek Survey Block Maps

Survey Overview Maps (colour image with elevation contour lines):

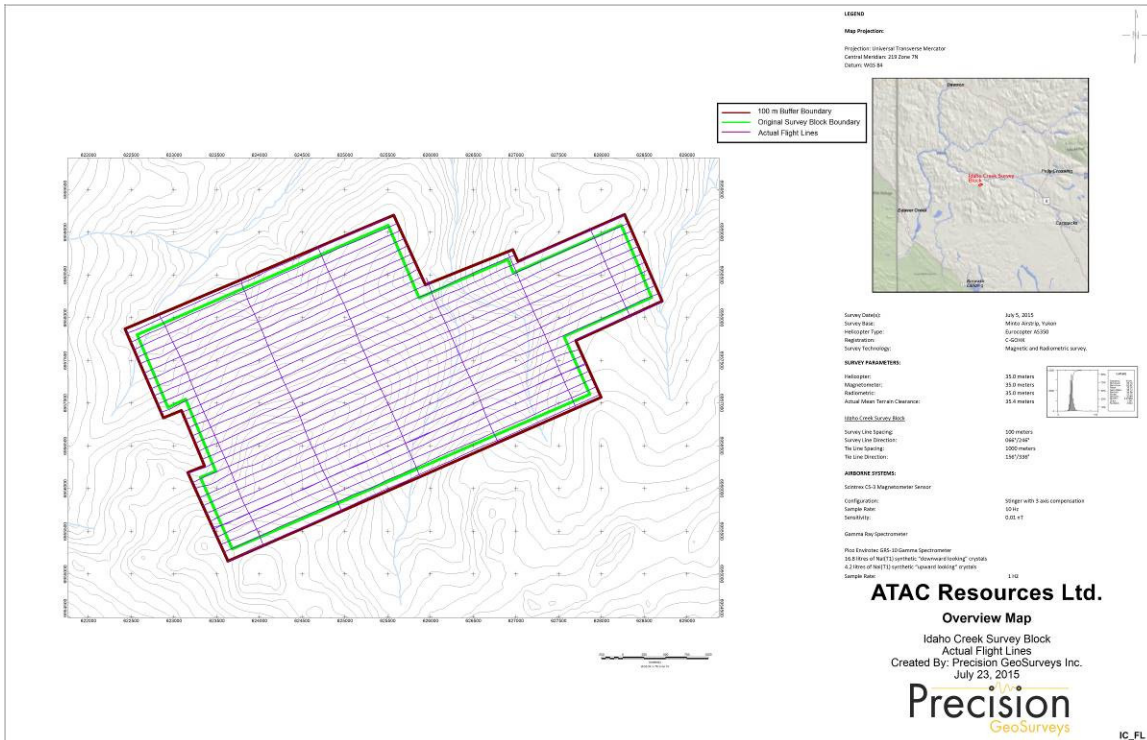
- Flight Lines (FL)
- Digital Terrain Model (DTM)

Magnetic Maps (colour image with elevation contour lines):

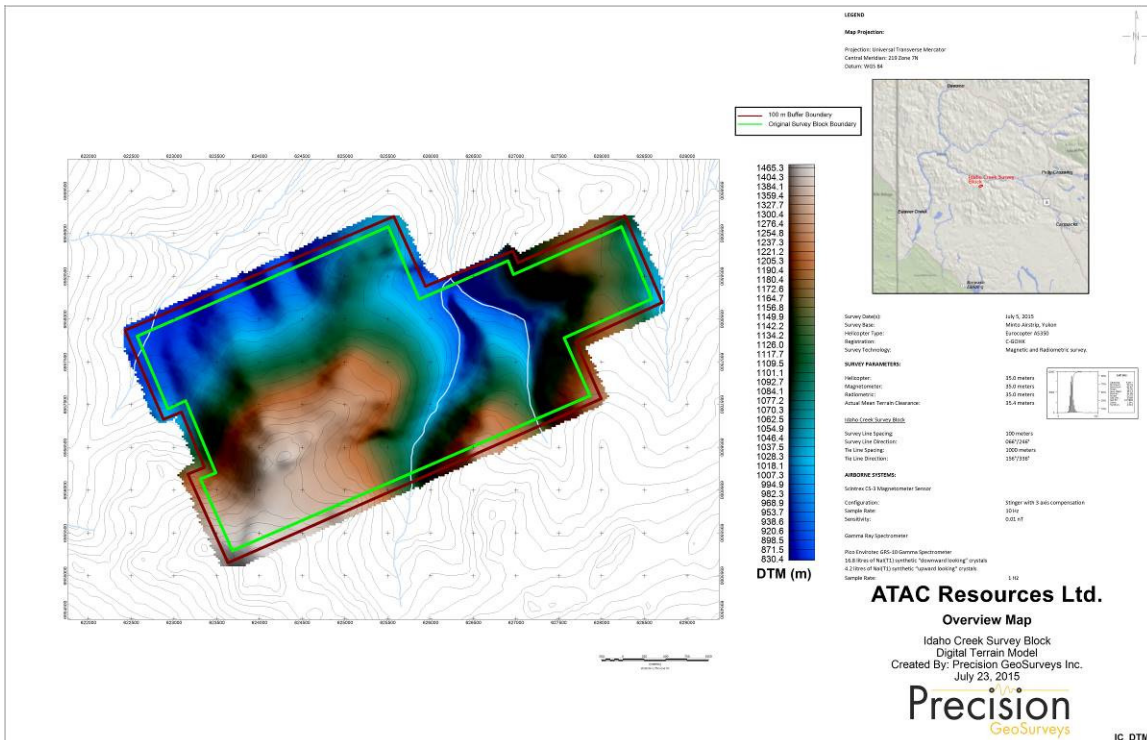
- Total Magnetic Intensity (TMI)
- Total Magnetic Intensity with flight lines (TMI\_wFL)
- Residual Magnetic Intensity (RMI)
- Calculated Vertical Gradient (CVG) of TMI

Radiometric Maps (colour image with elevation contour lines):

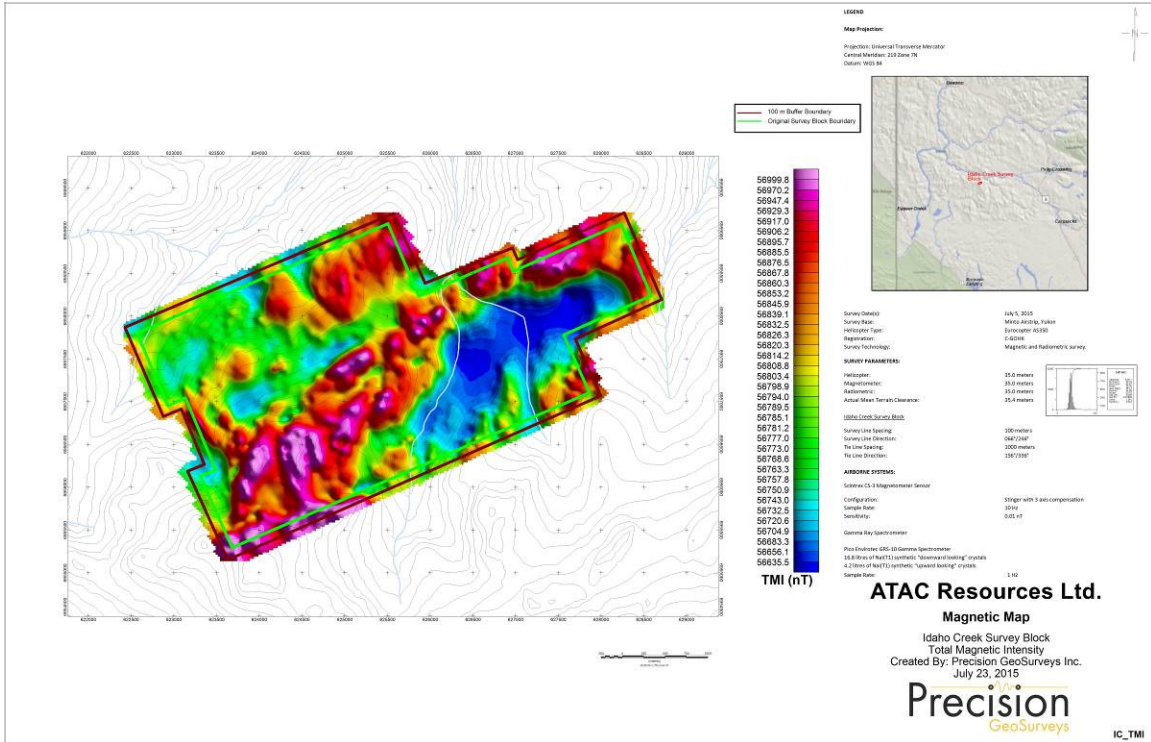
- Potassium – Equivalent Concentration (%K)
- Thorium – Equivalent Concentration (eTh)
- Uranium – Equivalent Concentration (eU)
- Total Count – Equivalent Dose Rate (TCcor)
- Total Count – Exposure Rate (TCexp)
- Potassium over Thorium Ratio (%K/eTh)
- Potassium over Uranium Ratio (%K/eU)
- Uranium over Thorium Ratio (eU/eTh)
- Thorium over Potassium Ratio (eTh/%K)
- Uranium over Potassium Ratio (eU/%K)
- Ternary Map (TM)



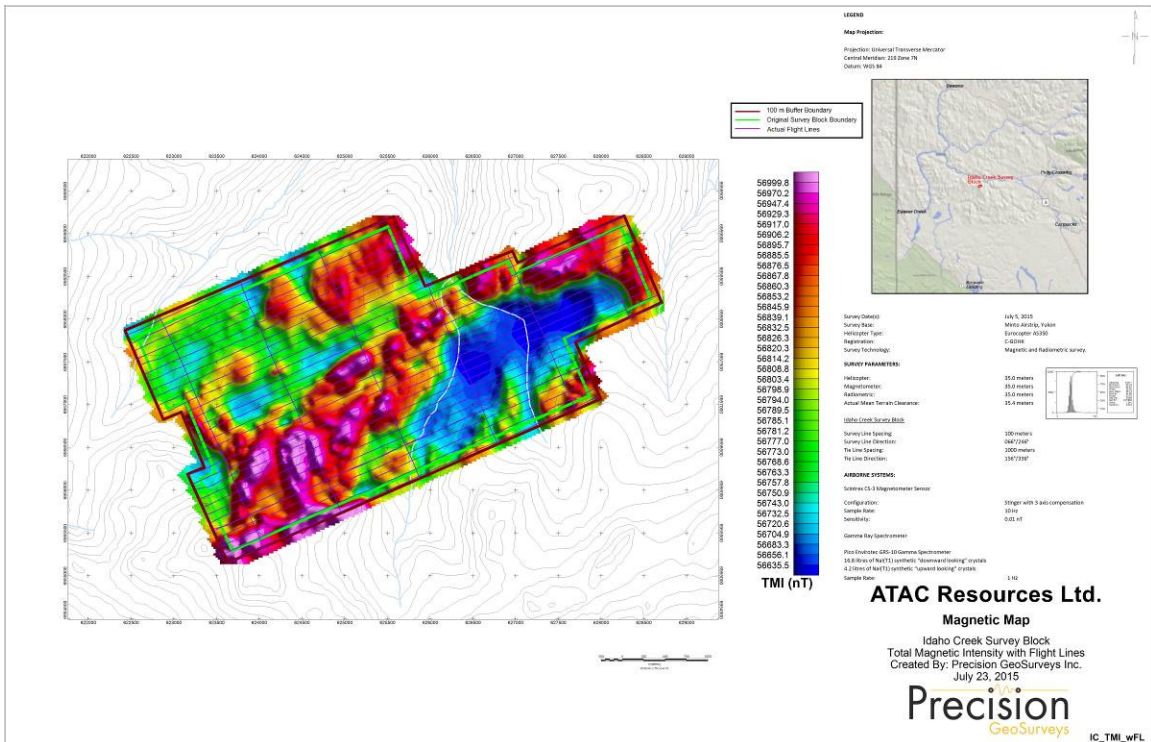
Map 1: Idaho Creek survey block actual flight lines.



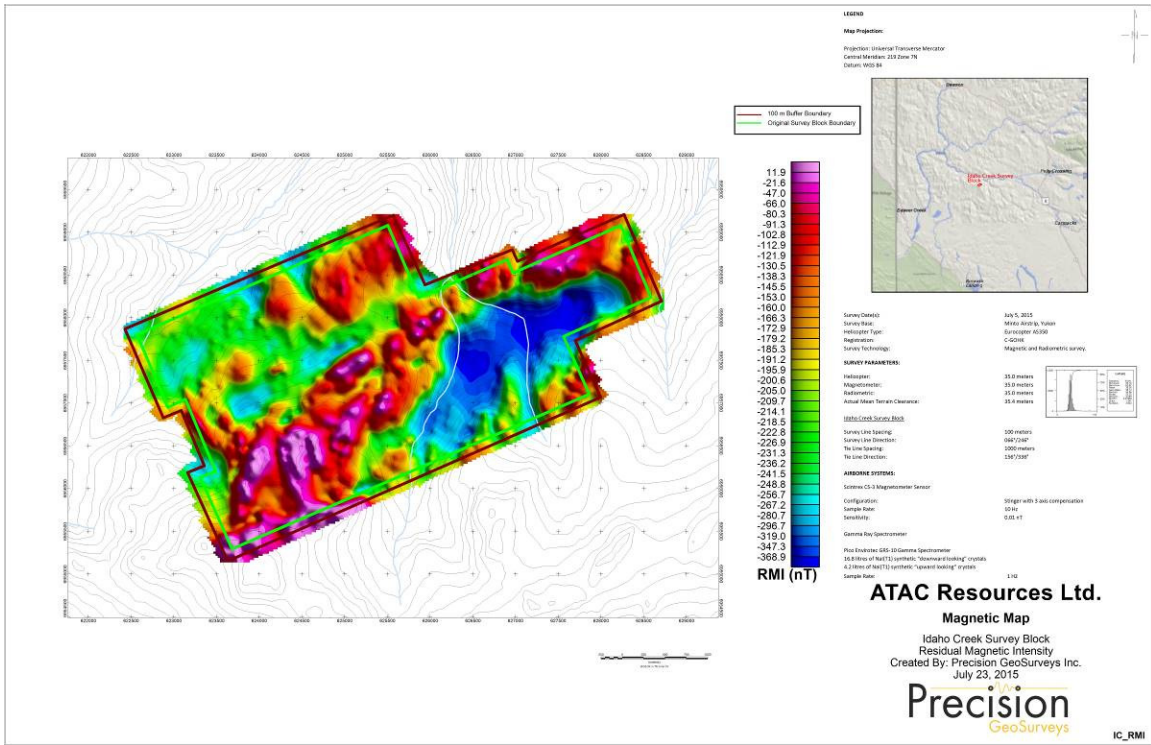
Map 2: Idaho Creek survey block digital terrain model.



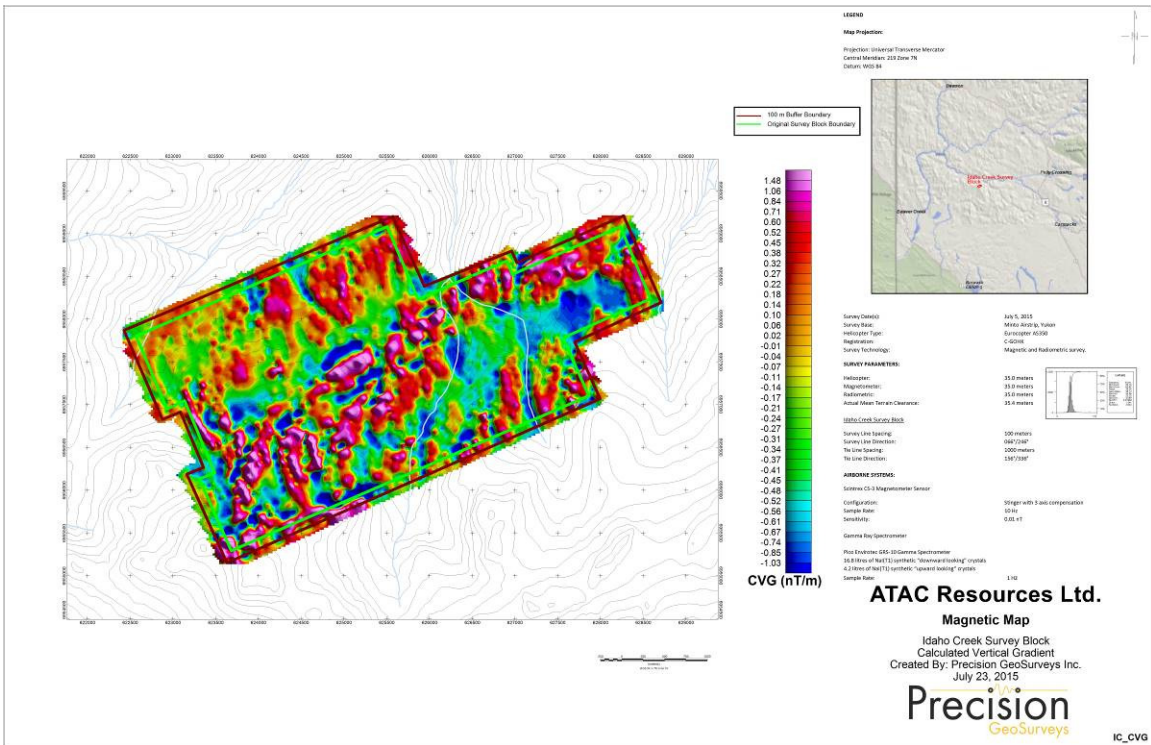
Map 3: Idaho Creek survey block total magnetic intensity.



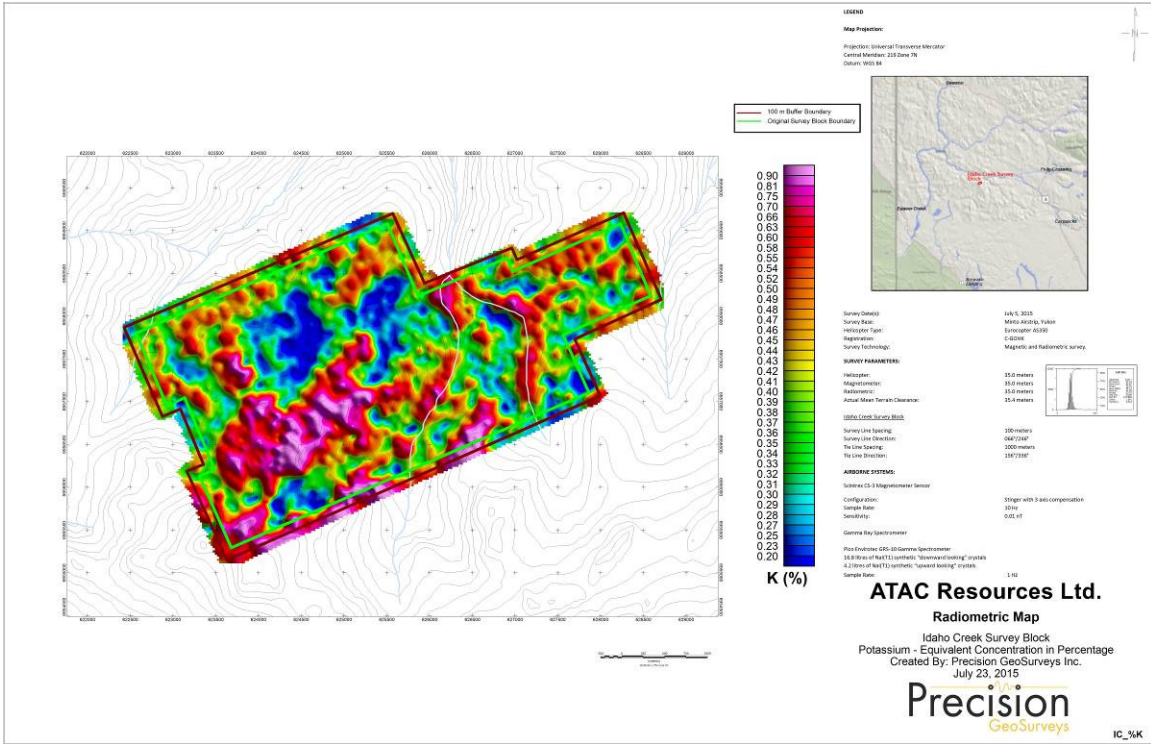
Map 4: Idaho Creek survey block total magnetic intensity with actual flight lines.



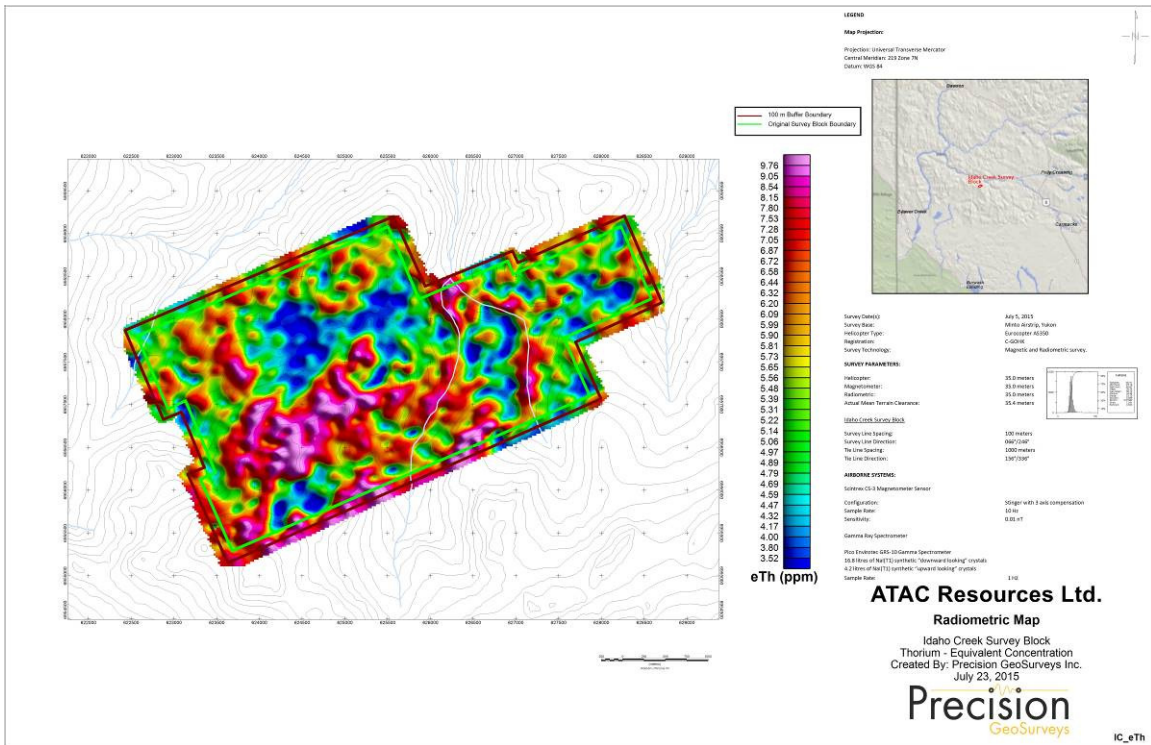
Map 5: Idaho Creek survey block residual magnetic intensity.



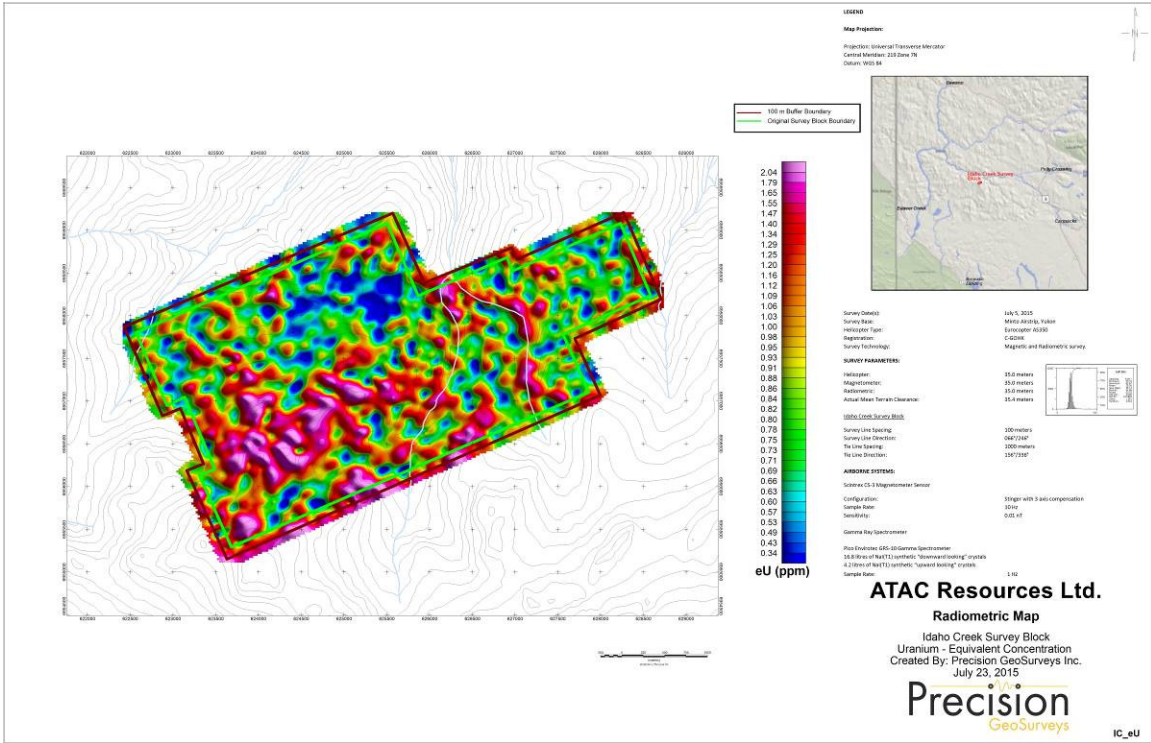
Map 6: Idaho Creek survey block calculated vertical gradient of the total magnetic intensity.



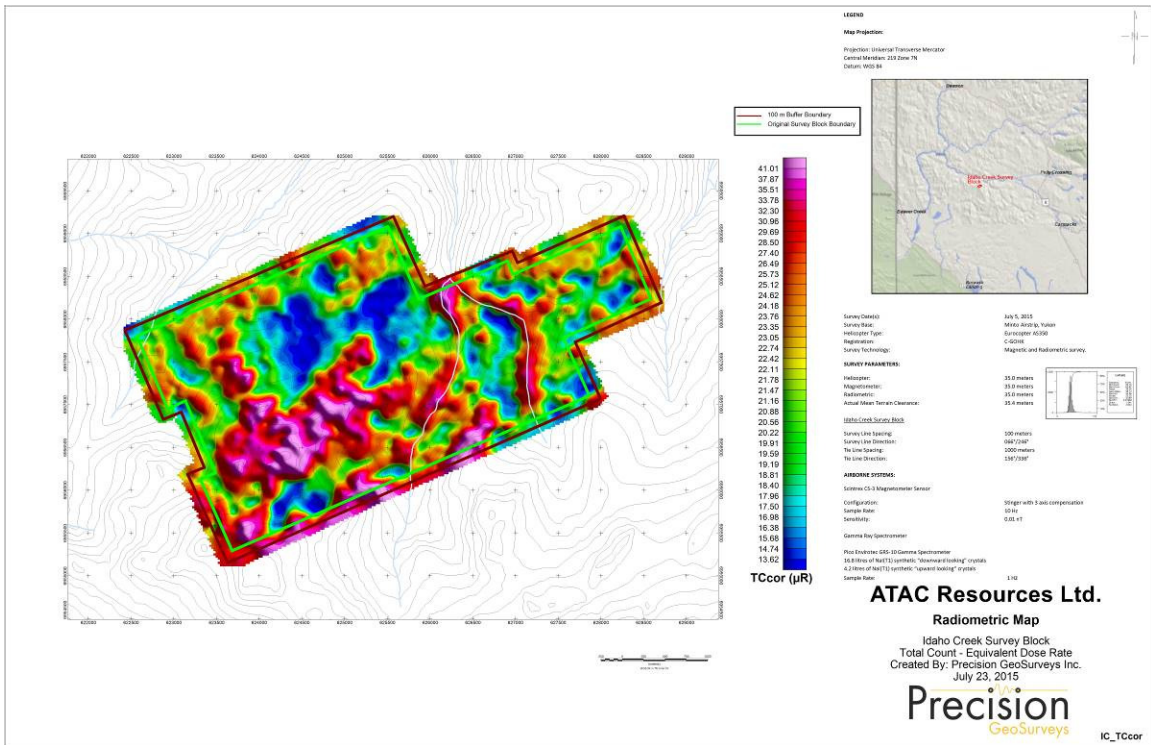
Map 7: Idaho Creek survey block potassium – equivalent concentration in percentage.



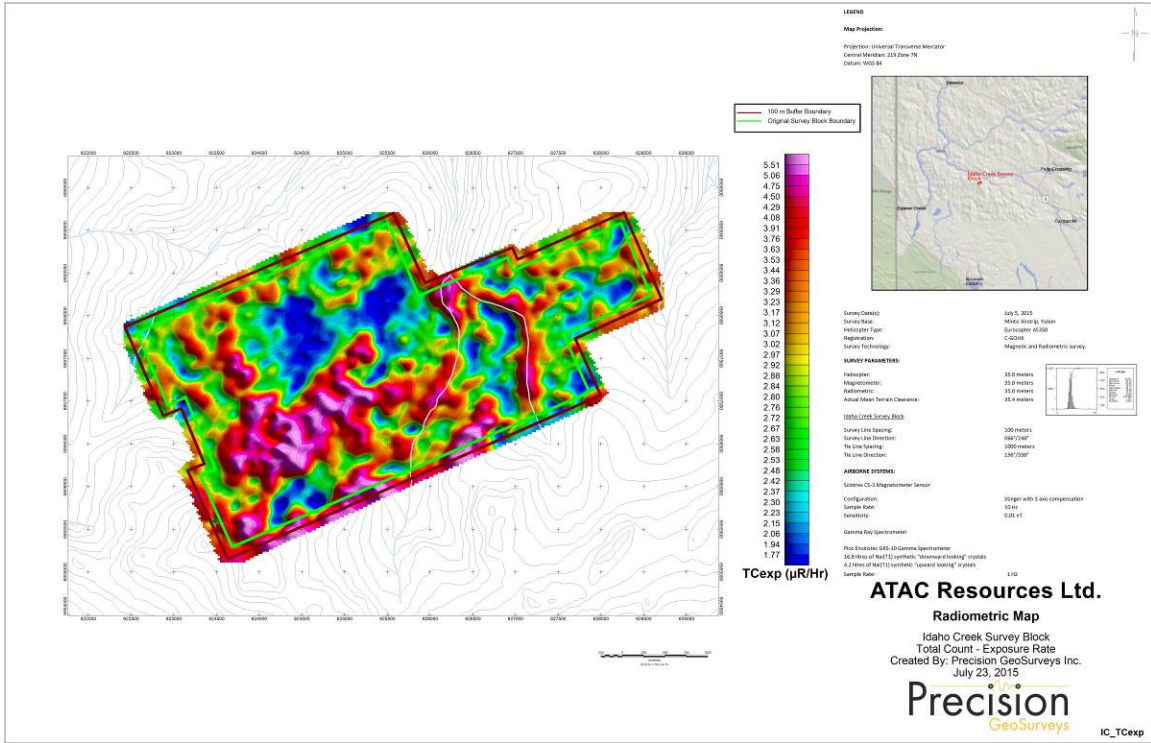
Map 8: Idaho Creek survey block thorium – equivalent concentration



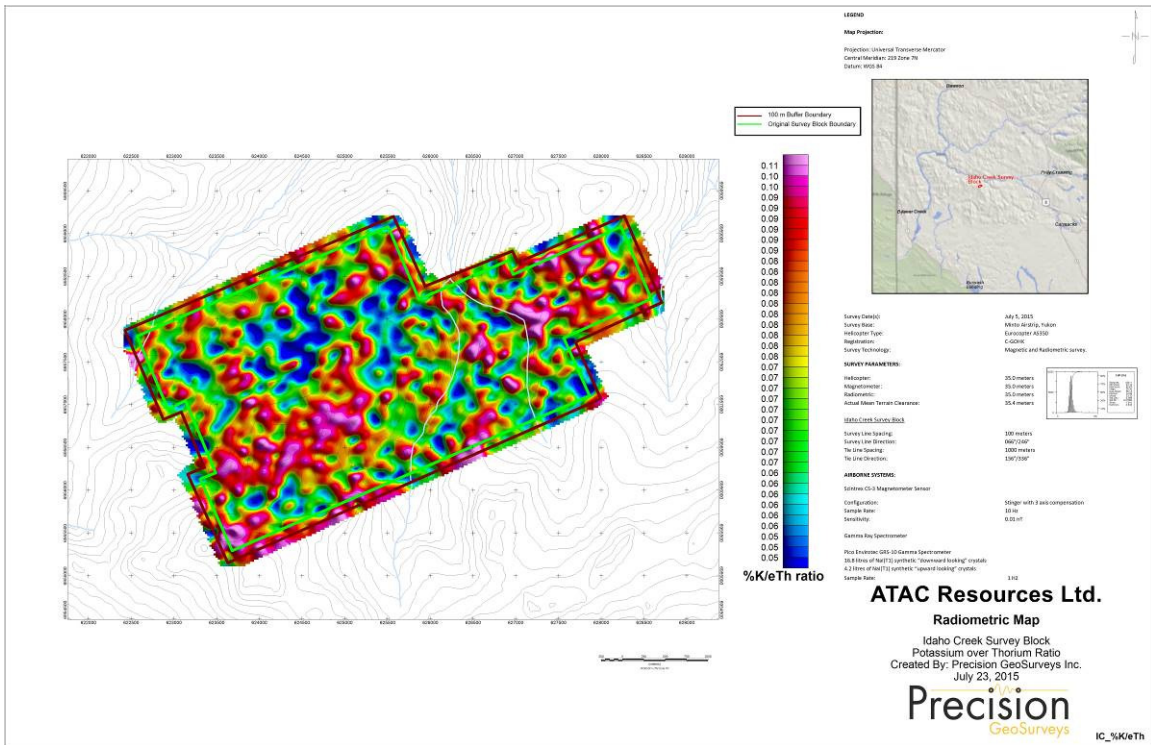
Map 9: Idaho Creek survey block uranium – equivalent concentration.



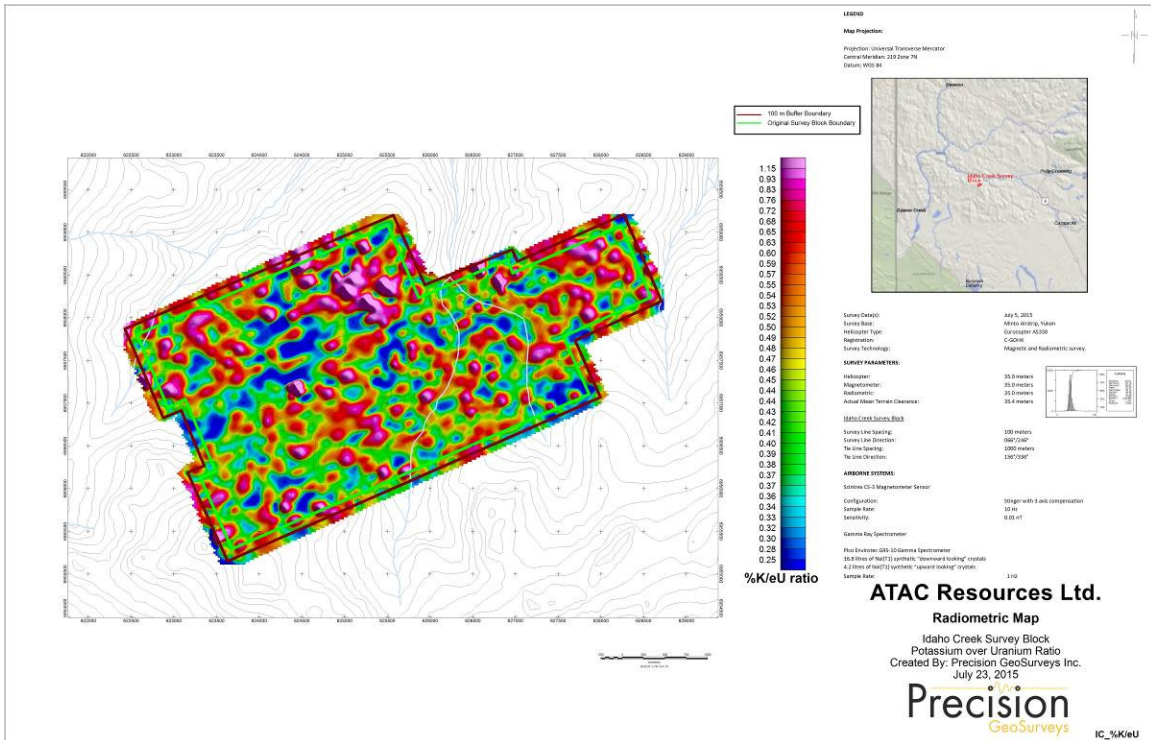
Map 10: Idaho Creek survey block total count – equivalent dose rate.



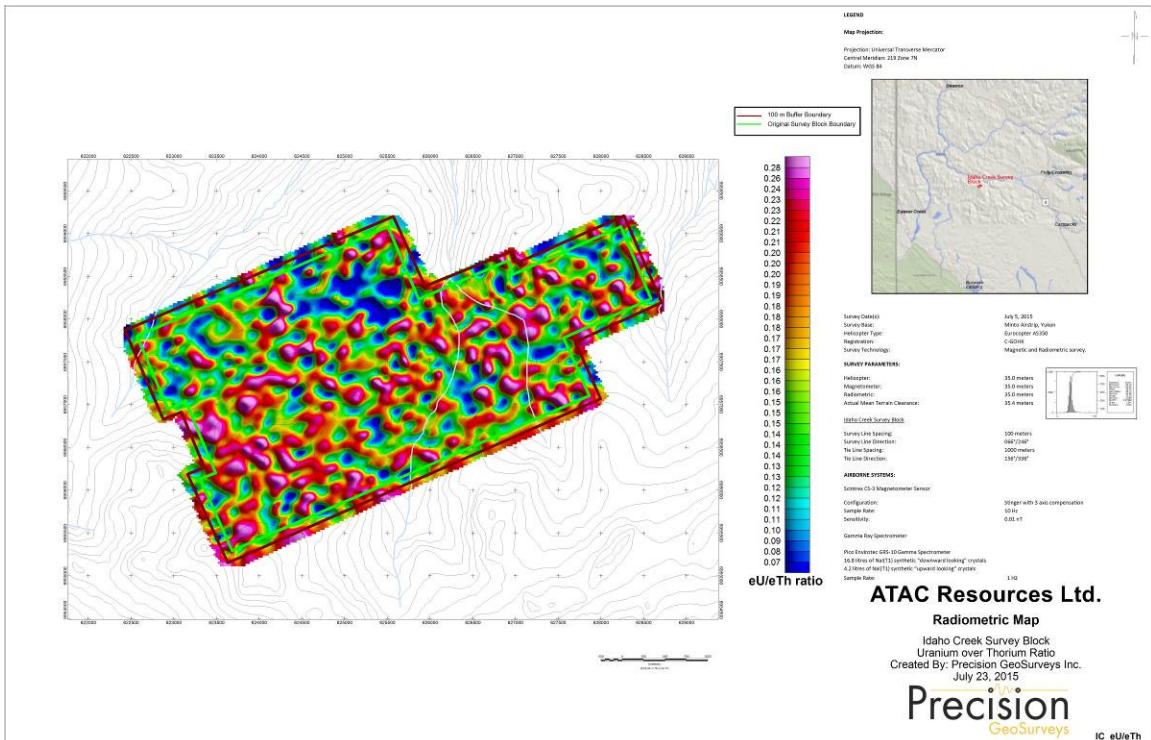
Map 11: Idaho Creek survey block total count – exposure rate.



Map 12: Idaho Creek survey block potassium over thorium ratio.

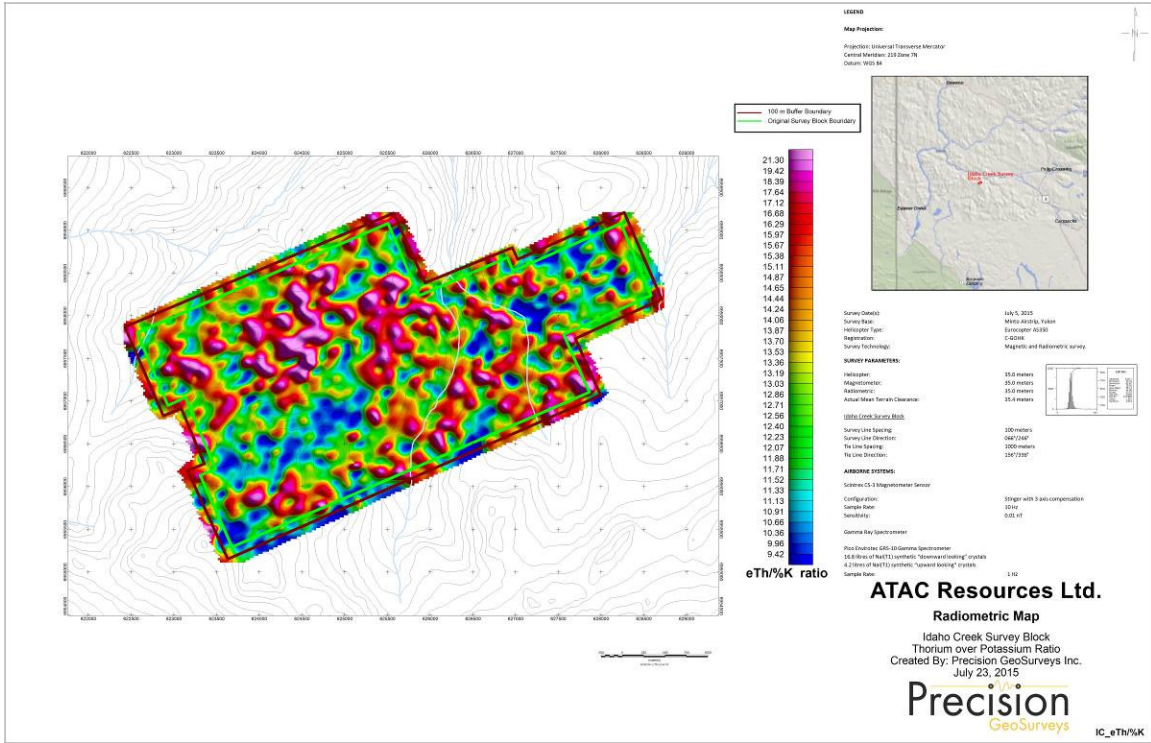


Map 13: Idaho Creek survey block potassium over uranium ratio.

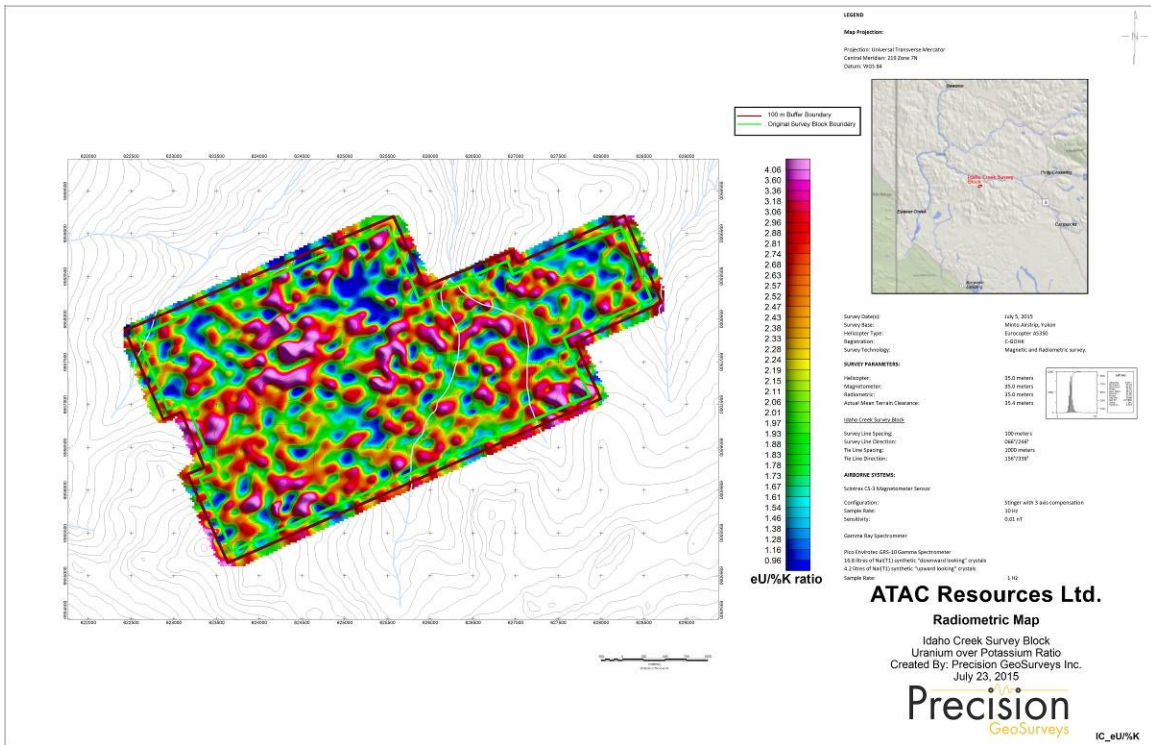


Map 14: Idaho Creek survey block uranium over thorium ratio.

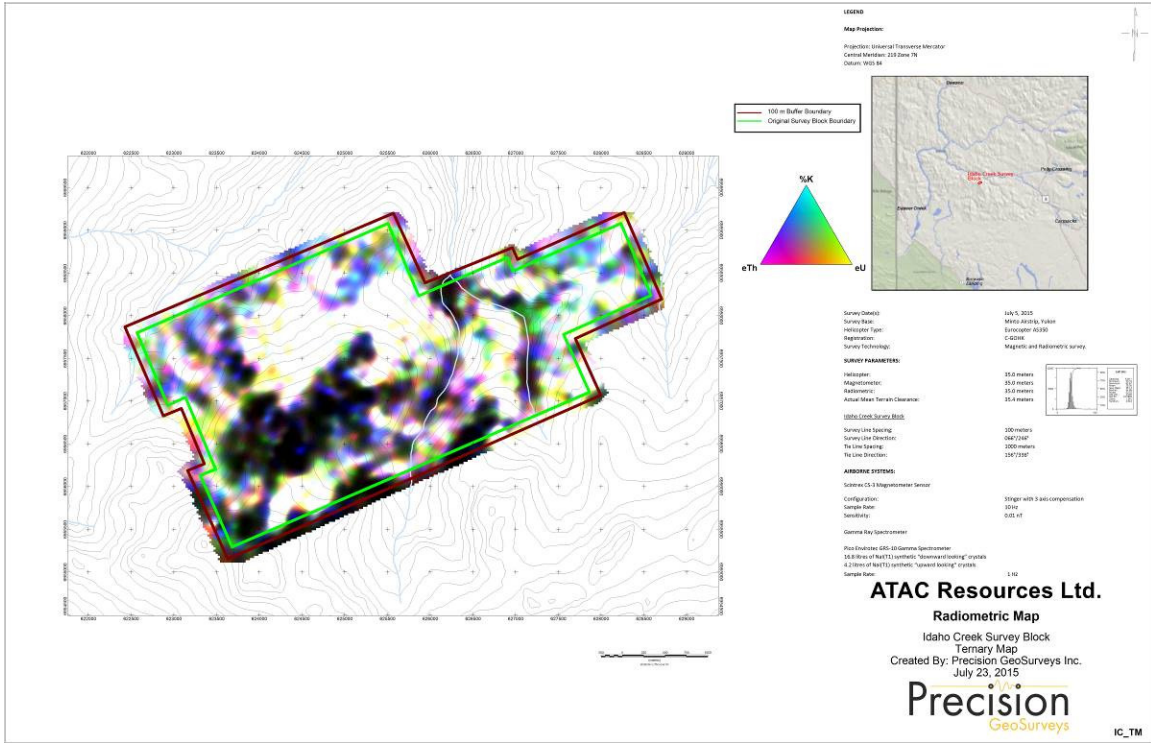




Map 15: Idaho Creek survey block thorium over potassium ratio.



Map 16: Idaho Creek survey block uranium over potassium ratio.



Map 17: Idaho Creek survey block ternary map; ratio of K, Th, and U.

**APPENDIX II**

**DIGITAL COPY OF GEOPHYSICAL SURVEY REPORT**