

FROM Mining Recorder at Mayo

TO Supervising Mining Recorder at Whitehorse, Y.T.

OR ACTION ARE:

☐ NEW APPL'N for PLACER LEASE to PROSPECT: Name:

☐ RENEWAL APPL'N PLACER LEASE to PROSPECT: Name:

Lease No.

☐ AFFIDAVIT of EXPENDITURE on PLACER LEASE. Name:

Lease No.

☐ ASSIGNMENT of PLACER LEASE No.

From:

To:

☐ GROUPING APPL'N UNDER SEC. 52(2) PLACER MINING ACT.

Owner:

☒ DIAMOND DRILL LOGS

Claims:

JASON & AEE

Claim sheet no.

105-0-1

☐ QUARTZ ASSESSMENT REPORT

Claims:

Claim sheet no.

Type of report:

Submitted by:

PAN OCEAN OIL LTD.

Cls. work performed on:

JASON 2'; 55; 57; 58; 155

\$ Req. for ren. application

27 HOLES
11169.69 METRES

Signature [Signature]

REPLY ACTION

Date Ret.

CC
GEOLOGY SECTION

fo

090986

Signature _____

INVOICE SUMMARY SHEET

Dec. 2, 1981

INVOICE NO.PERIOD COVEREDAMOUNT

Heath & Sherwood Ltd.

8965	March - April	\$ 28,019.40
9025	May 16-31	\$ 68,471.25
9001	May 13-15	\$ 61,230.20
9046	June 1-15	\$166,087.91
9052	June 16-30	\$176,067.79
9091	July 1-15	\$125,642.68
9159	July 16-31	\$127,141.15
9269	Aug 1-15	\$108,270.67
9320	Aug 16-31	\$164,296.10
9338	Sept 1-15	\$204,458.05
9374	Sept 16-30	\$195,584.84
9379	Oct 1-15	\$160,498.66
9426	Oct 16-31	\$147,925.73
?	Nov 1-	\$117,000.00

E. Caron Diamond Drilling Ltd.

1071	Sept 3-15	\$ 60,509.01
1082	Sept 16-Oct 8	\$ 81,739.89
TOTAL		\$1,992,943.33

TOTAL METREAGE DRILLED 11,169.69

DIRECT COST PER METREAGE \$178.42 (excluding Fuel, Mud, Assay, and overhead)



[Redacted]

020286

SUMMARY OF APPLICATION FOR WORK - JASON PROPERTY 1981

<u>Mineral Claim</u>	<u>Diamond Drill Hole</u>	<u>Metreage</u>	<u>Total Metreage</u>	<u>Direct Drilling Cost</u>	<u>Group No.</u>	<u>Work Period</u>	<u>Dollars Applied</u>
Jason 21	69	1043.33	1043.33	\$ 186,155.34	1	May 20-	\$6,400.00
					2	Aug 14	6,000.00
					3		5,600.00
Jason 55	71	108.20					
	72	203.00					
	73	24.99					
	74	274.93					
	75	553.82	2154.01	\$ 384,327.57	4	June 8-	\$6,400.00
	77	298.09			5	Oct 5	6,000.00
	80	249.02			6		6,000.00
	81	109.73					
	83	332.23					
Jason 58	84	621.49	621.49	\$ 110,888.88	7	Oct 3-	\$6,400.00
					8	Nov 16	6,000.00
					9		6,000.00
Jason 57	68	971.39					
	68A	516.94					
	68B	129.23					
	68C	511.76					
	68D	690.37					
	68E	720.55					
	70	847.65	6426.71	\$1,146,680.79	10	May 17-	\$6,400.00
	70A	472.75			11	Nov 23	5,600.00
	76	168.25			12		4,800.00
	78	428.55					
	78A	52.73					
	78B	205.74					
	85	324.31					
	85A	386.49					
Jason 155	79	403.86	924.15	\$ 164,890.75	13	Sept 4-Oct 4	\$5,600.00
	82	520.29					
TOTAL:			11,169.69	\$1,992,943.33			\$77,200.00
(Cost per metre = 178.424)				Excess work not applied			\$1,915,743.33



suite 908, 40 University Avenue,

Toronto, Ontario,
M5J 1T1

November 23rd, 1981

Cordilleran Engineering,
to 1418-355 Burrard Street,
Vancouver, B.C.

Invoice No. 9426
D.O. 378
Project No. 80-184

RECEIVED

NOV 27

in account with

heath & sherwood drilling

division of challenger international services Ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

HQ,NQ,BQ diamond drilling northeast of Ross River, Yukon
Territory - October 16th-31st, 1981

Drill #1

81-68E	90° NQ coring				
	566.93	600.00	33.07	113.75	3,761.71
	600.00	673.92	73.92	119.60	8,840.83
	673.92	677.88	3.96	S/O Wedge	
	677.88	750.00	72.12	119.60	8,625.55
	750.00	900.00	150.00	126.45	18,967.50
	900.00	908.92	8.92	134.35	1,198.40

41,393.99

Special Operations - Borehole Surveys

Rig Hrs. Man Hrs.

Oct. 16	3	6
17	1	2
18	2	4
19	1	2
20	2	4
21	2	4
22	2	4
23	1	2
24	1	2
25	1	2
26	1	2
27	3	6
28	1	2
29	2	4
30	1	2
31	1	2
	25	50

- Wedging

Oct. 20	15	30
21	3	6
	18	36

- Conditioning Hole

Oct. 24	3	6
25	1	2
e. & o. 26	1	2

CORDILLERAN ENGINEERING	
Client	Pano
Project	Jason
	147,925.73
Extensions	
Voucher No.	
Approved	
Date Paid	B

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

November 23rd, 1981

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Invoice No. 9426

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
Oct. 27	1	2				
28	1	2				
29	1	2				
30	2	4				
31	4	8				
	14	28				
			- Change Core barrel			
Oct. 19	3	6				
	60	120				
	Rig Hours	60 only	49.00	2,940.00		
	Man Hours	120 only	19.25	2,310.00	5,250.00	
	<u>Materials</u>					
Oct. 20	N. Clappison wedge assy. - used				185.00	
	<u>Drill #2</u>					
81-85	90° NQ coring					
	137.47	140.51	3.04	99.95		
	140.51	145.39	4.88	S/O Wedge		
	145.39	150.00	4.61	99.95		
	150.00	156.36	6.36	104.05		
	156.36	159.72	3.36	S/O Wedge		
	159.72	174.65	14.93	104.05		
	174.65	179.22	4.57	S/O Wedge		
	179.22	192.94	13.72	104.05		
	192.94	197.51	4.57	S/O Wedge		
	197.51	211.23	13.72	104.05		
	211.23	212.45	1.22	S/O Wedge		
	206.05	207.88	1.83	S/O Wedge		
	207.88	235.61	27.73	104.05		
	235.61	238.66	3.05	S/O Wedge		
	238.66	253.90	15.24	104.05		
	253.90	255.43	1.53	S/O Wedge		
	255.43	300.00	44.57	104.05		
	300.00	324.31	24.31	108.55		
	282.55	288.34	5.79	S/O Wedge		

suite 908, 40 university avenue,

toronto, ontario, November 23rd, 1981
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Invoice No. 9426

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division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	288.34	300.00	11.66	104.05	
	300.00	301.15	1.15	108.55	
	301.15	305.72	4.57 S/O Wedge		
	305.72	320.04	14.32	108.55	
	320.04	324.62	4.58 S/O Wedge		
	324.62	351.44	26.82	108.55	
	351.44	352.96	1.52 S/O Wedge		
			<u>263.65</u>		
			7.65	99.95	764.62
			147.93	104.05	15,392.12
			66.60	108.55	7,229.43
			41.47 S/O Wedge		
			<u>263.65</u>		
	Special Operations - Borehole Surveys				
	Rig Hrs.	Man Hrs.			
Oct. 16	1	2			
17	1	2			
18	1	2			
19	2	4			
20	3	6			
21	1	2			
22	1	2			
23	2	4			
24	1	2			
25	4	8			
26	2	4			
27	1	2			
29	1	2			
31	2	4			
	<u>23</u>	<u>46</u>			
			- Wedging		
Oct. 16	13	26			
17	17	34			
18	18	36			
19	15	30			
20	4	8			
21	20	40			
e. & o. e.					

23,386.17

suite 908, 40 university avenue,

toronto, ontario, November 23rd, 1981
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Invoice No. 9426

in account with

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terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed		rate	
Oct. 22	16	32				
23	8	16				
24	18	36				
27	21	42				
28	26	32				
29	16	32				
30	5	10				
31	12	24				
	<u>199</u>	<u>398</u>				
	<u>222</u>	<u>444</u>				
	Rig Hours		222 only	49.00	10,878.00	
	Man Hours		444 only	19.25	<u>8,547.00</u>	19,425.00
	<u>Materials</u>					
	N Clappison wedge assy - used					
	Oct. 16,17,18,19,21 am, 23,24,					
	28 am, 29 pm, 31					
			10 only	185.00		1,850.00
	N Directional deflecting wedge assy					
	Oct. 21 pm, 28					
	Plus 14%					
			2 only	605.00	1,210.00	
					<u>169.40</u>	1,379.40
	<u>Drill #3</u>					
81-84	85° NQ coring					
	236.53	284.38	47.85	104.05	4,978.79	
81-84	85° BQ Coring					
	284.38	287.43	3.05	93.80	286.09	
	287.43	292.00	4.57	S/O Wedge		
	292.00	300.00	8.00	93.80	750.40	
	300.00	311.51	11.51	97.90	1,126.83	
	311.51	314.56	3.05	S/O Wedge		
	314.56	330.71	16.15	97.90	1,581.09	
	330.71	332.24	1.53	S/O Wedge		
	332.24	367.29	35.05	97.90	3,431.40	
	367.29	368.81	1.52	S/O Wedge		
	368.81	450.00	81.19	97.90	7,948.50	
	450.00	471.23	21.23	102.65	<u>2,179.26</u>	22,282.36

suite 908, 40 university avenue,

toronto, ontario, November 23rd, 1981
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Invoice No. 9426

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
<u>Special Operations - Borehole Surveys</u>					
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
Oct. 16	1	2			
17	2	4			
18	1	2			
19	3	6			
20	1	2			
21	4	8			
22	1	2			
24	2	4			
26	1	2			
27	2	4			
28	1	2			
29	1	2			
31	4	8			
	<u>24</u>	<u>48</u>			
<u>Special Operations - Wedging</u>					
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
Oct. 16	2	4			
19	4	8			
20	11	22			
21	4	8			
22	11	22			
23	17	34			
25	19	38			
	<u>68</u>	<u>136</u>			
			- Conditioning Hole		
Oct. 31	4	8			
			- Reduce to BQ		
Oct. 19	10	20			
	<u>106</u>	<u>212</u>			
	Rig Hours		106 only	49.00	5,194.00
	Man Hours		212 only	19.25	<u>4,081.00</u>
					9,275.00
<u>Special Operations - Standby</u>					
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
Oct. 16	1	2			

suite 908, 40 university avenue,

toronto, ontario, November 23rd, 1981
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Invoice No. 9426

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terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
Oct. 18	5	10			
20	1	2			
21	<u>1</u>	<u>2</u>			
	8	16			
	Rig Hours	8 only	42.35	338.80	
	Man Hours	16 only	19.25	<u>308.00</u>	646.80
	<u>Materials</u>				
	B Clappinson wedge assy - used assy.				
	Oct. 20, 21, 23	3 only	375.00	1,125.00	
		- new assy.			
	Oct. 25	1 only		<u>1,190.00</u>	2,315.00
	<u>Tractor Rental</u>				
	Oct. 16-31	1/2 month	7000.00		3,500.00
	<u>Tractor Driver</u>				
	Oct. 17-31	1/2 month	5890.00/M		2,945.00
	<u>Skidder Rental</u>				
	Oct. 16-31	1/2 month	3320.00/M		1,660.00
	<u>Skidder Driver</u>				
	Oct. 16-31	186 hrs.	19.25/hr.		<u>3,580.50</u>
	<u>Cost Plus Diamond Tools</u>				
		31.00 cts.	26.00 cts.	20.00 cts.	Settings
1F-8928	NXC Shell			36.06	141.00
1F-8926	NXC Ball bit	55.43			159.70
1F-1478X	HW casing shoe				219.00
1F-3853	NX Shell			15.73	129.00
1G-2149	NXC Core bit		38.93		145.25
1G-1338	HWC Shell			27.76	210.00
1G-4951	BXC Concave bit	21.29	21.29		117.68
1G-3564	NQ bit	15.99			104.70
1G-3565	NQ bit	15.99			104.70
1G-4952	BXC Canve bit		21.29		117.68
1A-4181	NXC Shell			30.93	141.00
1F-8942	NXC Core bit			31.25	141.00
1G-3649	NXC core bit			29.97	141.00
		87.41	81.51	171.70	1,871.71

suite 708, 40 university avenue,

toronto, ontario, November 23rd, 1981
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Invoice No. 9426

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>
Diamonds		87.41 cts. 31.00	2,709.71
		81.51 cts. 26.00	2,119.26
		171.70 cts. 20.00	3,434.00
Settings			1,871.71
			10,134.68
Plus 14%			1,418.86

11,553.54

Cost Plus Diamond Tool Credit

1F-8928	NXC Shell - lost down the hole		
1F-8926	NXC Ball bit - lost down the hole		
1F-1478X	HW casing shoe - lost down the hole		
1G-3587	NQ core bit	11.05 cts.	
1G-4048	BXC Concave bit	18.05	
1C-6880	NQ core bit	8.90*	
1G-4045	BXC Concave bit	12.65	
1G-3288	BQ core bit	6.30	
1F-1533	NQ Core bit	3.60	
1G-2149	NXC Core bit	28.90	
		<u>89.45</u>	
		80.55 cts. 26.00	2,094.30
		8.90* cts. 31.00	275.90
			2,370.20
Plus 14%			331.83

(2,702.03)

\$147,925.73

toronto, ontario, October 26th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.

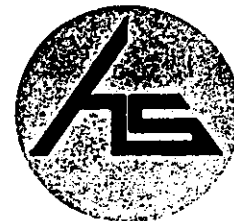
D.O. 378

Project No. 80-184

NOV - 3

heath & sherwood drilling

division of challenger international services ltd.

**terms: net cash 15 days after date of invoice**

hole no.	<u>to cover diamond drilling for the period</u>				
	<u>from</u>	<u>to</u>	<u>footage completed</u>		<u>rate</u>
HQ,NQ,BQ diamond drilling northeast of Ross River, Yukon Territory - October 1st-15th,1981					
<u>Drill #1</u>					
81-68D	<u>90° NQ coring</u>				
	704.71	748.90	44.19	119.60	5,285.12
81-68E	<u>90° NQ coring</u>				
	262.74	265.79	3.05 S/O Wedge		
	265.79	300.00	34.21	104.05	3,559.55
	300.00	450.00	150.00	108.55	16,282.50
	450.00	470.01	20.01	113.75	2,276.14
	470.01	474.58	4.57 S/O Wedge		
	474.58	502.01	27.43	113.75	3,120.16
	502.01	506.58	4.57 S/O Wedge		
	506.58	566.93	60.35	113.75	<u>6,864.81</u>
37,388.28					
<u>Special Operations - Borehole Surveys</u>					
Oct. 1	1 rig hrs.	2 man hrs.			
2	10	20			
6	1	2			
7	4	8			
8	3	6			
9	2	4			
10	3	6			
11	2	4			
12	1	2			
13	1	2			
14	1	2			
15	2	4			
	<u>31</u>	<u>62</u>			
		- Wedging			
Oct. 4	18	36			
5	24	48			
11	8	16			
12	14	28			
13	<u>18</u>	<u>36</u>			
	<u>82</u>	<u>164</u>			

213

Approved
OSH
Tel. Trans 1/8

Extensions
Per No.
Approved

Pono
Lason
160.498.666

B

c. & o. e.

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981
MSJ ITI

to

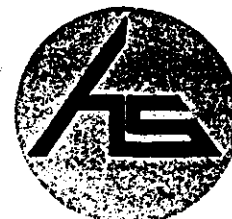
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Invoice No. 9379

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed		rate	
Oct. 3			- Cementing			
4	6	12				
	<u>4</u>	<u>8</u>				
	10	20				
			- Change from W/L to Standard core barrel			
	<u>3</u>	<u>6</u>				
	126	252				
	Rig Hours		126 only	49.00	6,174.00	
	Man Hours		252 only	19.25	<u>4,851.00</u>	11,025.00
	<u>Special Operations</u> - Waiting for cement to set					
Oct. 3	12 rig hrs.	24 man hrs.				
4	<u>2</u>	<u>4</u>				
	14	28				
	Rig Hours		14 only	42.35	592.90	
	Man Hours		28 only	19.25	<u>539.00</u>	1,131.90
	<u>Materials</u>					
Oct. 5	N direction deflecting wedge assy				605.00	
	Chibougamau plug				<u>38.50</u>	
					643.50	
	Plus 14%				<u>90.09</u>	733.59
12	N Clappison wedge assy - new				985.00	
	- used				<u>185.00</u>	1,170.00
	<u>Drill #2</u>					
81-78B	83° NQ coring					
	335.59	376.74	41.15	108.55	4,466.83	
81-85	HQ coring					
	0	16.00	16.00 O/B	119.65	1,914.40	
	16.00	21.95	5.95 O/B	139.65	830.92	
	21.95	52.12	30.17	114.65	3,458.99	
	49.38	52.43	3.05 S/O	Wedge		
	52.43	71.63	19.20	114.65	2,201.28	
	68.28	71.32	3.04 S/O	Wedge		
	71.32	87.78	16.46	114.65	1,887.14	
	84.43	85.95	1.52 S/O	Wedge		
	85.95	121.31	35.36	114.65	4,054.02	

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981
M5J 1T1

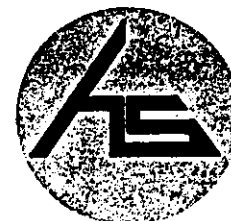
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Invoice No. 9379

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	117.04	120.09	3.05 S/O Wedge		
	120.09	137.47	17.38 114.65	<u>1,992.62</u>	20,806.20
	<u>Footage Premium re Triple tube coring</u>				
81-78B	366.68	376.74	10.06 20.20		203.21
	<u>Special Operations - Borehole Surveys</u>				
Oct. 1	2 rig hrs.	4 man hrs.			
9	1	2			
10	3	6			
11	2	4			
12	1	2			
13	1	2			
15	3	6			
	<u>13</u>	<u>26</u>			
	- Wedging				
10	12	24			
11	4	8			
12	13	26			
13	12	24			
14	22	44			
15	3	6			
	<u>66</u>	<u>132</u>			
	79	158			
	Rig Hours	79 only	49.00	3,871.00	
	Man Hours	158 only	19.25	<u>3,041.50</u>	6,912.50
	<u>Special Operations - Standby Rate</u>				
Oct. 4	Move between holes	12 rig.hrs.	48 man hrs.		
5	"	12	36		
6	"	8	16		
11	Wait for surbeys	<u>5</u>	<u>10</u>		
		37	110		
	Rig Hours	37 only	42.35	1,566.95	
	Man Hours	110 only	19.25	<u>2,117.50</u>	3,684.45

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981

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to

Invoice No. 9379

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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period						
	from	to	footage completed		rate		
	<u>Materials</u>						
Oct. 10	H Directional deflecting wedge assy				1,639.40		
11	"				1,639.40		
13	"				1,639.40		
14	"				1,639.40		
					<u>6,557.60</u>		
	Plus 14%				<u>918.06</u>		7,475.66
	<u>Drill #3</u>						
81-84	<u>HQ Coring</u>						
	0	16.00	16.00 O/B	119.65	1,914.40		
	16.00	28.35	12.35 O/B	139.65	1,724.68		
	28.35	82.60	54.25	114.65	6,219.76		
81-84	<u>NQ Coring</u>						
	82.60	119.48	36.88	99.95	3,686.16		
	119.48	124.06	4.58 S/O Wedge				
	124.06	150.00	25.94	99.95	2,592.70		
	150.00	231.65	81.65	104.05	8,495.68		
	231.65	236.53	4.88 S/O Wedge				24,633.38
	<u>Special Operations - Borehole Surveys</u>						
Oct. 6	1 rig hrs.	2 man hrs.					
8	1	2					
9	1	2					
10	1	2					
12	3	6					
13	2	4					
14	1	2					
	<u>10</u>	<u>20</u>					
			- Wedging				
11	11	22					
15	<u>21</u>	<u>42</u>					
	<u>32</u>	<u>64</u>					
	<u>42</u>	<u>84</u>					
	Rig Hours	42 only	49.00		2,058.00		
	Man Hours	84 only	19.25		1,617.00		3,675.00

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981
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Invoice No. 9379

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
<u>Special Operations - Moving between holes</u>						
Oct. 1	12 rig hrs.	24 man hrs.				
2	12	48				
3	12	36				
	36	108				
	Rig Hours		36 only	42.35	1,524.60	
	Man Hours		108 only	19.25	<u>2,079.00</u>	3,603.60
<u>Materials</u>						
Oct. 11	N Clappison wedge - used assy.				185.00	
15	" - used assy.				<u>185.00</u>	370.00
<u>Drill #4</u>						
81-83	HQ coring					
	236.83	300.00	63.17	119.15	7,526.71	
	300.00	332.24	32.24	124.20	<u>4,004.21</u>	11,530.92
<u>Special Operations - Borehole Surveys</u>						
Oct. 1	1 rig hr.	2 Man hrs.				
2	1	2				
3	1	2				
5	8	16				
	11	22				
	Rig Hours		11 only	49.00	539.00	
	Man Hours		22 only	19.25	<u>423.50</u>	962.50
<u>Demobilization - Drill #4</u>						
- from drill site to staging area						
Oct. 6	12 rig hrs.	36 man hrs.				
7	12	12				
8	12	12				
	36	60				
	Rig Hours		36 only	42.35	1,524.60	
	Man Hours		60 only	19.25	<u>1,155.00</u>	2,679.60

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981
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to

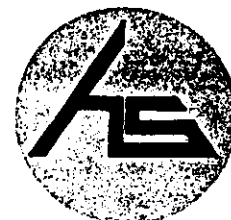
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Invoice No. 9379

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from	to	footage completed	rate
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Tractor Rental

Oct. 1 - 15	12/ month	7000.00/M	3,500.00
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Tractor Driver

Oct. 1 - 13	13 days	5890.00/M	2,470.00
-------------	---------	-----------	----------

Skidder Rental

Oct. 1 - 15	1/2 month	3320.00/M	1,660.00
-------------	-----------	-----------	----------

Skidder Driver

Oct. 1- 15	169 hrs.	19.25	3,253.25
------------	----------	-------	----------

Cost Plus Diamond Tools

	31.00 cts.	26.00 cts.	20.00 cts.	Setting
--	------------	------------	------------	---------

1G-3590	NQ core bit	13.00		98.25
1G-3614	"	18.31		105.61
1C-6880	"	13.19		100.00
1G-7585	NXC ball bit	41.46		158.60
1G-4045	BXC concave bit	21.21		123.28
1G-4052	"	21.21		123.28
1D-8036	AXC wedge bit	15.29		58.30
Z-2397	BXC ball bit	18.83		102.00
1G-3288	BQ core bit	9.55		70.00
1G-3594	NQ core bit	13.00		098.25
1G-3587	"	13.00		098.25
1G-1242	HWC cone bit	96.01		400.00
1G-4950	BXC concave bit	21.29		117.68
1G-3651	NXC reaming bit		29.97	141.00
1G-2148	NXC cone bit	38.93		145.25
1G-3553	NQ core bit	15.99		104.70
1G-4953	BXC concave bit	21.29		117.68
1G-3556	NQ core bit	15.99		104.70
1G-3554	"	15.99		104.70
1F-1533	BQ core bit	8.06		70.00

102.62	328.98	29.97	2,441.53
--------	--------	-------	----------

Diamonds

102.62 cts.	31.00	3,181.22
328.98 cts.	26.00	8,553.48
29.97	20.00	599.40

Settings

2,441.53

Y-03863	NX Wedge bit	24.85 cts.	35.00	869.75
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Setting

145.00

e. & c. e.

Plus 14%

15,790.38
2,210.65

18,001.03

suite 908, 40 university avenue,

toronto, ontario, October 26th, 1981

MSJ 171

to

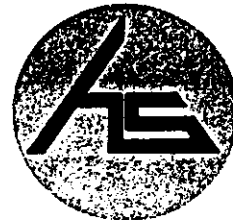
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Invoice No. 9379

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>
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Cost Plus Diamond Tool Credit

1G-4046	BXC concave bit	16.82 cts.	
1G-4049	"	16.83	
1G-3648	NXC wedge bit	23.63	
1G-3652	"	23.63	
1F-7046	"	23.64	
1F-8927	NXC ball bit	45.20	
1D-6285	NQ core bit	10.65	
1D-6322	"	10.20	
4J-907	NQ concave bit	10.75	
1G-3590	NQ core bit	10.20	
1G-4614	"	14.43	
1G-3594	"	8.98	

214.96 cts. 26.00 5,588.96

Plus 14%

782.45

(6,371.41)

\$160,498.66

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

October 14th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.

Invoice No. 9374
D.O. 378
Project No. 80-184

in account with

heath & sherwood drilling

division of challenger international services ltd.



OCT 21

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

HQ-NQ, BQ diamond drilling, northeast of Ross River, Yukon
Territory - September 16th-30th, 1981

Drill #1

90° NQ Coring

81-68-D	212.75	230.43	17.68	104.05	1,839.60
	230.43	231.96	1.53	S/O Wedge	
	231.96	249.63	17.67	104.05	1,838.56
	249.63	251.16	1.53	S/O Wedge	
	251.16	276.46	25.30	104.05	2,632.47
	276.46	277.98	1.52	S/O Wedge	
	277.98	300.00	22.02	104.05	2,291.18
	300.00	376.43	76.43	108.55	8,296.48
	376.43	377.96	1.53	S/O Wedge	
	377.96	450.00	72.04	108.55	7,819.94
	450.00	600.00	150.00	113.75	17,062.50
	600.00	704.71	104.71	119.60	12,523.32

54,304.05

Special Operations - Borehole Surveys

Rig Hrs. Man Hrs.

Sept 16	1	2
17	1	2
18	2	4
19	2	4
20	4	8
21	1	2
22	2	4
23	2	4
24	2	4
25	2-1/2	5
26	1	2
27	1-1/2	3
28	1	2
29	2	4
	<u>25</u>	<u>50</u>

CORDILLERAN
ENGINEERING

Client

Project

(213)

Extensions

Voucher No.

Approved

Date Paid

suite 908, 40 university avenue,

toronto, ontario, October 14th, 1981
M5J 1T1

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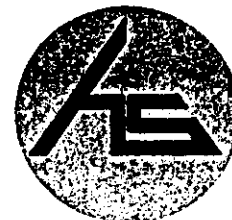
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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.

**terms: net cash 15 days after date of invoice**

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	- Wedging					
Sept 16	1	2				
17	19	38				
18	15-1/2	31				
19	3	6				
21	14	28				
	52-1/2	105				
	77-1/2	155				
	Rig Hrs.		77-1/2 only	49.00	3,797.50	
	Man Hrs.		155 only	19.25	<u>2,983.75</u>	6,781.25
	<u>Materials</u>					
	N Clappison wedges - used assembly					
	Sept 17 am, pm, Sept 18 & 21 4 only				185.00	740.00
	<u>Drill #2</u>					
81-78	83° NQ coring					
	382.22	428.55	46.33	108.55	5,029.12	
81-78A	83° HQ coring					
	131.68	137.77	6.09	114.65	698.22	
81-78A	83° NQ coring					
	137.77	181.97	44.20	104.05	4,599.01	
	170-99	173.43	2.44	S/O Wedge		
	173.43	202.08	28.65	104.05	2,981.03	
	202.08	206.66	4.58	S/O Wedge		
	206.66	233.78	27.12	104.05	2,821.84	
	233.78	235.31	1.53	S/O Wedge		
	235.31	300.00	64.69	104.05	6,730.99	
	300.00	335.59	35.59	108.55	<u>3,863.29</u>	26,723.50
	<u>Special Operations - Borehole Surveys</u>					
	<u>Rig Hrs.</u>		<u>Man Hrs.</u>			
Sept 16	1	2				
17	10	20				
20	2	4				
21	2	4				
23	1	2				
24	1-1/2	3				
e. & o. e.						

suite 908, 40 university avenue,

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October 14th, 1981

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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
Sept 25	1	2				
- 27	1	2				
28	1	2				
29	2	4				
30	2	4				
	<u>24-1/2</u>	<u>49</u>				
		- Wedging				
Sept 19	12	24				
22	24	48				
23	11	22				
24	14-1/2	29				
25	1	2				
26	20	40				
	<u>82-1/2</u>	<u>165</u>				
		- Cement				
Sept 18	12	24				
		- Conditioning hole				
27	4	8				
	<u>123</u>	<u>246</u>				
	Rig Hours	123 only	49.00	6,027.00		
	Man Hours	246 only	19.25	<u>4,735.50</u>	10,762.50	
	Special Operations - Wait for cement to set					
Sept 18		12 rig hrs.	42.35	508.20		
		24 man hrs.	19.25	<u>462.00</u>	970.20	
	<u>Materials</u>					
Sept 17	N directional deflecting wedge assy			605.00		
	Chibougamau plug			<u>38.50</u>		
				<u>643.50</u>		
	Plus 14%			<u>90.09</u>	733.59	
22	N Clappison wedge assy - new			<u>985.00</u>		
23	" - used			185.00		
24	" - new			985.00		
26	" - used			<u>185.00</u>	2,340.00	

suite 908, 40 university avenue,

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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed		rate	
	Drill #3					
81-70	80° NQ coring					
	712.02	733.66	21.64	119.60	2,588.14	
	733.66	738.23	4.57	S/O Wedge		
	738.23	750.00	11.77	119.60	1,407.69	
	750.00	754.08	4.08	126.45	515.92	
81-70	80° BQ coring					
	754.08	763.53	9.45	114.20	1,079.19	
	763.53	768.11	4.58	S/O Wedge		
	768.11	793.71	25.60	114.20	2,923.52	
	793.71	798.28	4.57	S/O Wedge		
	798.28	900.00	101.72	114.20	11,616.42	
	900.00	910.45	10.45	121.35	<u>1,268.11</u>	21,398.99
	Special Operations - Borehole Surveys					
	<u>Rig Hrs.</u>		<u>Man Hrs.</u>			
Sept 19	2		4			
20	3		6			
30	<u>13</u>		<u>26</u>			
	18		36			
	- Wedging					
Sept 16	9		18			
17	24		48			
18	8		16			
20	9		18			
21	19		38			
22	9		18			
23	<u>18</u>		<u>36</u>			
	96		192			
	- Reduce from NQ to BQ					
19	<u>12</u>		<u>24</u>			
	126		252			
	Rig Hours		126 only	49.00	6,174.00	
	Man Hours		252 only	19.25	4,851.00	11,025.00

suite 908, 40 university avenue,

toronto, ontario, October 14th, 1981
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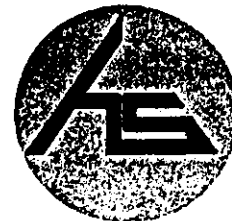
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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period						
	from	to	footage completed	rate			
	<u>Materials</u>						
Sept 16	N Clappison Wedges						
	1 Used assy					185.00	
	B. Clappison Wedges						
Sept 20,23	2 used assy					375.00	935.00
	<u>Drill #4</u>						
81-81	<u>HQ coring</u>						
	0	7.32	7.32 O/B	119.65	875.84		
	7.32	109.73	102.41	114.65	11,741.31		
81-83	<u>HQ coring</u>						
	0	9.75	9.75 O/B	119.65	1,166.59		
	9.75	150.00	140.25	114.65	16,079.66		
	150.00	236.83	86.83	119.15	<u>10,345.79</u>	40,209.19	
	<u>Footage premium re triple tube drilling</u>						
81-81	93.57	109.73	16.16	28.35		458.14	
	<u>Special Operations - Borehole Surveys</u>						
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>					
Sept 19	2	4					
20	1	2					
22	4	8					
25	2	4					
26	3	6					
27	1-1/2	3					
28	2	4					
29	2	4					
30	2	4					
	<u>19-1/2</u>	<u>39</u>					
	- Reaming Casing						
Sept 16	2	4					
18	7	14					
19	8	16					
	<u>17</u>	<u>34</u>					
	- Wedging						
Sept 22	12	24					
e. & o.e. 23	<u>11</u>	<u>22</u>					
	<u>23</u>	<u>46</u>					

suite 908, 40 university avenue,

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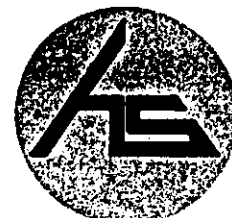
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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
	- Pulling Casing					
Sept 23		<u>4</u> 63-1/2	<u>8</u> 127			
	Rig Hours		63-1/2 only	49.00	3,111.50	
	Man Hours		127 only	19.25	<u>2,444.75</u>	5,556.25
	<u>Special Operations - Standby Rate</u>					
		<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
Sept 16	Moving between					
	holes	5	10			
23	"	6	12			
24	"	12	24			
25	"	1	2			
22	Wait for					
	Geologist	<u>2</u> 26	<u>4</u> 52			
	Rig Hrs.		26 only	42.35	1,101.10	
	Man Hrs.		52 only	19.25	<u>1,001.00</u>	2,102.10
	<u>Materials</u>					
Sept 22	10 ft. HWL rods		8 only	127.00	1,016.00	
23	2 ft. HW casing		54 only	51.85	2,799.90	
	HW casing shoe 1F1476X		1 only		<u>219.00</u>	
					4,034.90	
	Less 20% useage for rod & casing (return shoe)				<u>763.18</u>	
					3,271.72	
	Plus 14%				<u>458.04</u>	3,729.76
	<u>Tractor Rental</u>					
	Sept 16-30		1/2 month	7000.00		3,500.00
	<u>Tractor Driver</u>					
	Sept 16-30		1/2 month	5890.00		2,945.00
	<u>Skidder Rental</u>					
	Sept 16-30		1/2 month	3320.00		1,660.00
	<u>Skidder Driver</u>					
	Sept 16-30		174 hrs.	19.25		3,349.50
	<u>Extra Crew</u>					
	K. Kelly Sept 16-27		144 hrs.	19.25		2,772.00

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toronto, ontario, October 14th, 1981
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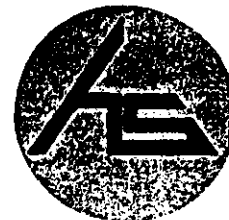
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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

Cost plus diamond tools

		Cts.	Settings		
1G-4048	BXC concave bit	21.21	123.28		
1A-4125	NQ-3 core bit	12.00	115.93		
1A-4132	NQ-3 core bit	12.00	115.93		
1A-4133	NQ-3 core bit	12.00	115.93		
1A-4134	NQ-3 core bit	12.00	115.93		
1A-4135	NQ-3 core bit	12.00	115.93		
1G-5052	NQ-3 core bit	19.31	111.68		
1G-4043	BXC concave bit	21.21	123.28		
		121.73	937.89		

Diamonds	121.73 cts.	26.00	3,164.98	
Settings			937.89	
			4,102.87	
			574.40	

Plus 14%

Cost plus diamond tools Credit

Usable Recovery

4,677.27

1 only	NX BW 1E-8641	7.90 cts.		
5 only	BXC concave bits			
	1E-4524, 1G-4044, 1G-4047			
	1G-4050, 1G-4051	71.90		
1 only	NXC ball bit 1F-8925	40.35		
1 only	NQ core bit 1G-3592	8.75		
1 only	NQ core bit 1D-6283	9.20		
3 only	NX BW bit 1E-8639, 1E-8642			
	1E-8644	28.95		
1 only	NQ core bit 1D-6287	4.40		
1 only	NQ core bit 1G-3593	7.00		
* 1 only	NXC ball bit 1A-8373	39.00		
5 only	NQ-3 core bits 1A-4125,			
	1A-4132, 1A-4133, 1A-4134			
	1A-4135	44.90		
1 only	NQ-3 core bit 1G-5052	14.95		
1 only	BXC concave bit 1G-4043	15.85		
		293.15 cts.	26.00	7,621.90
1 only	NXC reaming big 1E-9409	22.00		
2 only	NXC wedge bit 1G3647,			
	1G-3650	35.95		

suite 908, 40 university avenue,

toronto, ontario, October 14th, 1981
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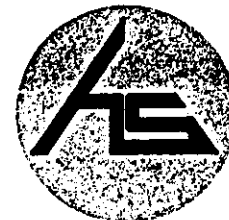
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Invoice No. 9374

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
2 only	NXC reaming shells		48.20			
	1A-4169, 1A-4170					
1 only	NXC reaming bit 1F-8941		25.40			
1 only	NXC Shell 1A-4165		<u>17.55</u>			
			<u>149.10</u> cts.	20.00	<u>2,982.00</u>	
					<u>10,603.90</u>	
	Plus 14%				<u>1,484.55</u>	
					CREDIT	(12,088.45)
						<u>\$195,584.84</u>
					<p><i>Less P 6</i> <i>Extra crew</i></p>	
						<u>2772.00</u>
					<p><i>192,812.84</i></p>	

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
M5J 1T1

Cordilleran Engineering,
to 1418-355 Burrard Street,
Vancouver, B.C.

Invoice No. 9338
D.O. 378
Project No. 80-184

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	HQ. NQ, BQ diamond drilling, northeast of Ross River, Yukon..					
	Territory - September 1st-15th, 1981					
	Drill #1					
81-68C	90° NQ coring					
	467.57	469.09	1.52 S/O wedge			
	469.09	600.00	130.91	113.75	14,891.01	
	600.00	726.35	126.35	119.60	15,111.46	
81-68D	90° NQ coring					
	60.66	63.70	3.04 S/O wedge			
	63.70	150.00	86.30	99.95	8,625.69	
	150.00	181.66	31.66	104.05	3,294.22	
	181.66	183.19	1.53 S/O wedge			
	183.19	200.26	17.07	104.05	1,776.13	
	200.26	204.83	4.57 S/O wedge			
	204.83	212.75	7.92	104.05	824.08	
						44,522.59
Special Operations - Borehole Surveys						
	Rig Hrs. Man Hrs.					
Sept. 2	3	6				
3	2	4				
4	1	2				
5	1	2				
6	2	4				
10	11	22				
12	1	2				
13	4	8				
14	2	4				
15	1	2				
	28	56				
			- Wedging			
Sept. 1	18	36				
12	12	24				
14	11	22				
15	11	22				
	52	104				
			- Cementing			
Sept. 11	4	8				
	84	168				

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suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
M5J 1T1

to

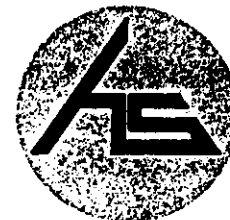
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Invoice No. 9338

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
Sept 11	Rig Hours		84 only	49.00	4,116.00	
	Man Hours		168 only	19.25	3,234.00	7,350.00
	<u>Standby - Waiting for cement to set</u>					
			16 rig hrs.	42.35	677.60	
			32 man hrs.	19.25	616.00	1,293.60
	<u>Materials</u>					
	N Clappison wedges					
	Sept. 1 new assembly					
	Sept.14 used assembly					
	Sept.15 used assembly					
81-78	N directional deflecting wedge assembly					
	Sept. 12					
	Plus 14%					
	Chibougamou plug					
	Plus 14%					
	<u>Drill #2</u>					
	83° HQ coring					
	92.36	150.00	57.64	114.65	6,608.43	
	150.00	300.00	150.00	119.15	17,872.50	
	300.00	338.94	38.94	124.20	4,836.35	
81-78	338.94	382.22	43.28	108.55	4,698.04	34,015.32
<u>Special Operations - Borehole Surveys</u>						
Sept. 2	1-1/2 rig hrs. 3 man hrs.					
5	1 2					
7	1 2					
8	1 2					
9	1 2					
11	1 2					
12	1-1/2 3					
14	1 2					
	9		18			
- Reduce to N hole size						
13	10		20			
e. & o. o.	19		38			

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
MSJ 1T1

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Invoice No. 9338

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	Rig Hours		19 only	49.00	931.00
	Man Hours		38 only	19.25	<u>731.50</u>
					1,662.50
	Special Operations - Other				
	Sept 1 Tripod		11 rig hrs.	42.35	465.85
			22 man hrs.	19.25	<u>423.50</u>
					889.35
	Drill #3				
81-70	80° NQ coring				
	552.61	564.80	12.19	113.75	1,386.61
	564.80	566.02	1.22	S/O wedging	
	566.02	600.00	33.98	113.75	3,865.23
	600.00	604.73	4.73	119.60	565.71
	604.73	606.25	1.52	S/O wedging	
	606.25	646.18	39.93	119.60	4,775.63
	646.18	648.32	2.14	S/O wedging	
	648.32	673.31	24.99	119.60	2,988.80
	673.31	674.84	1.53	S/O wedging	
	674.84	712.02	37.18	119.60	<u>4,446.73</u>
					18,028.71
	Special Operations - Borehole Surveys				
	Rig Hrs. Man Hrs.				
Sept. 1	3	6			
4	1	2			
5	1	2			
7	1	2			
8	3	6			
9	3	6			
15	2	4			
	<u>14</u>	<u>28</u>			
			- Wedging		
Sept. 1	6	12			
2	16	32			
3	8	16			
6	14	28			
7	5	10			
9	19	38			
10	5	10			
11	11	22			
e. & o. 12	24	48			
13	<u>10</u>	<u>20</u>			
	<u>118</u>	<u>236</u>			

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
MSJ 171

Invoice No. 9338

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
		132	264			
	Rig Hours		132 only	49.00	6,468.00	
	Man Hours		264 only	19.25	5,082.00	11,550.00
	Materials	<i>water line Rights 4 @ 42.05</i>			169.40	
	N. Clappison wedges	<i>man hrs 8 @ 19.25</i>			154.00	323.40
	Sept 3 1 new assembly				985.00	
	Sept. 6, 9, 12 3 used assemblies			185.00	555.00	1,540.00
	Drill #4					
81-77	83° NQ coring					
	182.27	185.32	3.05 S/O Wedge			
	185.32	202.08	16.76	104.05	1,743.88	
	202.08	203.61	1.53 S/O wedge			
	203.61	220.07	16.46	104.05	1,712.66	
	220.07	221.59	1.52 S/O wedge			
	221.59	298.10	76.51	104.05	7,960.87	
81-80	83° HQ coring					
	0	7.32	7.32 O/B	119.65	875.84	
	7.32	150.00	142.68	114.65	16,358.26	
	150.00	249.02	99.02	119.15	11,798.23	40,449.74
	Footage Premium re Triple Tube drilling					
81-77	281.94	289.26	7.32 NQ	20.20	147.86	
81-80	217.93	249.02	31.09 HQ	28.35	881.40	1,029.26
	Special Operations - Borehole Surveys					
	Rig Hrs.	Man Hrs.				
Sept. 1	3	6				
2	1	2				
4	3	6				
6	6	12				
8	1	2				
9	1	2				
10	2	4				
11	3	6				
12	2	4				
e. & o] 13	2	4				
15	8	16				

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
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Invoice No. 9338

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
			- Wedging			
Sept. 1	9	18				
2	8	16				
3	20	40				
	37	74				
			- Reaming casing			
Sept. 8	9	18				
10	1	2				
	10	20				
	79	158				
	Rig Hours	79 only	49.00	3,871.00		
	Man Hours	158 only	19.25	3,041.50	6,912.50	
	Special Operations - Standby Rate					
			- Wait for decision			
Sept. 2	1	2				
			- Moving between holes			
Sept. 7	10	20				
Sept. 15	4	8				
	14	28				
	15	30				
	Rig Hours	15 only	42.35	635.25		
	Man Hours	30 only	19.25	577.50	1,212.75	
	Materials					
	N. Clappison wedges					
	Sept 1 am 1 new assembly				985.00	
	Sept 1 pm, 3, 2 used assemblies				185.00	
					370.00	
					1,355.00	
	Less 1 used assembly charged Aug. 31st				185.00	1,170.00
	2 ft. HW casing				51.85	518.50
	Less 20% useage					103.70
						414.80
	HW casing shoe 1F1483X					219.00
						633.80
	Plus 14%					88.73
						722.53

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
M5J 1T1

to

Invoice No. 9338

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period			
	from	to	footage completed	rate
	<u>Tractor Rental</u>			
	Sept. 1 - 15		1/2 month	7,000.00
	<u>Tractor Driver</u>			
	Sept. 1 - 15		1/2 month	5,890.00
	<u>Skidder Rental</u>			
	Sept. 1 - 15		1/2 month	3,320.00
	<u>Skidder Operator</u>			
	Sept 1 - 15		56 hrs.	19.25
	<u>Extra Crew</u>			
	K. Kelly Sept 1 - 15		182 hrs.	19.25
	<u>Cost Plus Diamond Tools</u>			
	Description	26.00 cts.	20.00 cts.	Setting
4J907	NQ concave	21.05		108.00
1E8639	NX bevelwall	13.79		59.00
1E8642	NX Bevelwall	13.79		59.00
1E8644	NX Bevelwall	13.79		59.00
1D6287	NQ step	13.77		107.20
1G3593	NQ core	13.00		98.25
1G3647	NXC wedge		29.97	141.00
1G3650	NXC wedge		29.97	141.00
1A4169	NXC reaming shell		30.93	141.00
1A4170	NXC reaming shell		30.93	141.00
1E8641	NX Bevelwall	13.79		59.00
1E4524	BXC concave	29.69		114.00
1F8925	NXC ball bit	49.88		145.25
1D6283	NQ core	13.77		107.20
1F8941	NXC reaming bit		31.25	141.00
1A4165	NXC reaming shell		30.93	141.00
1G3648	NXC wedge		29.97	141.00
1F7046	NXC wedge		29.21	141.00
1G4049	BXC concave	21.21		123.28
1F8927	NXC ball	55.43		145.25
1D6285	NX core	13.77		107.20
1D6322	NX core	14.05		102.25
		300.78	243.16	2,521.88

1463.00

suite 908, 40 university avenue,

toronto, ontario, September 29th, 1981
M5J 1T1

Invoice No. 9338

to

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
Diamonds		300.78 cts.	26.00	7,820.28
		243.16 cts.	20.00	4,863.20
Settings				<u>2,521.88</u>
				15,205.36
Plus 14%				<u>2,128.75</u>

17,334.11

~~\$204,458.05~~

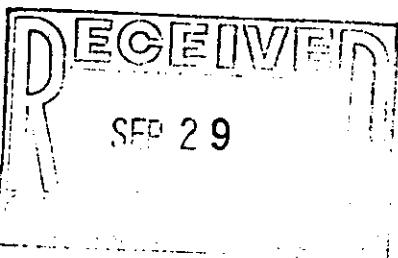
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suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981
M5J 1T1

Cordilleran Engineering,
to 1418 - 355 Burrard Street,
Vancouver, B.C.

Invoice No. 9320
D.O. 378
Project No. 80-184

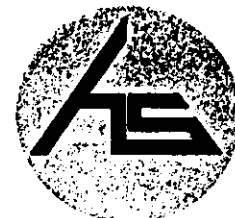


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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed		rate
	HQ, NQ, BQ diamond drilling northeast of Ross River, Yukon Territory August 16th-31st, 1981 Drill #1				
81-68B	90° NQ coring				
	736.71	750.00	13.29	119.60	1,589.48
	750.00	806.82	56.82	126.45	7,184.89
81-68C	90° NQ coring				
	217.33	235.31			
	235.31	236.83	1.52	S/O wedge	
	236.83	255.12			
	255.12	256.64	1.52	S/O wedge	
	256.64	270.36			
	270.36	271.58	1.22	S/O wedge	
	271.58	288.65			
	288.65	289.87	1.22	S/O wedge	
	289.87	300.00			
	300.00	305.72			
	305.72	306.94	1.22	S/O wedge	
	306.94	328.88			
	328.88	330.10	1.22	S/O wedge	
	330.10	351.13			
	351.13	352.35	1.22	S/O wedge	
	352.35	413.92			
	413.92	415.45	1.53	S/O wedge	
	415.45	438.00			
	438.00	439.53	1.53	S/O wedge	
	439.53	450.00			
	450.00	467.57	17.57	113.75	1,998.59
	217.33	300.00	82.67		
	Less Wedging footage		5.48		
			77.19	104.05	8,031.62
	300.00	450.00	150.00		
	Less Wedging footage		6.72		
			143.28	108.55	15,553.04
					34,357.62

213

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swam
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159,907.10
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suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981
MSJ 171

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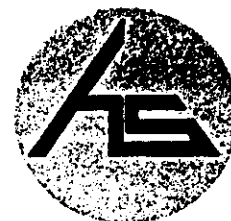
Page -2-

Invoice No. 9320

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
<u>Special Operations - Borehole Surveys</u>						
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>				
Aug 18	10	20				
Aug 19	4	8				
Aug 20	1-1/2	3				
Aug 21	1	2				
Aug 23	1	2				
Aug 24	1	2				
Aug 25	3	6				
Aug 26	1	2				
Aug 28	2	4				
Aug 29	1	2				
Aug 30	1	2				
Aug 31	2	4				
	<u>28-1/2</u>	<u>57</u>				
	- Wedging					
Aug 20	14-1/2	29				
Aug 21	19	38				
Aug 22	21	42				
Aug 23	9	18				
Aug 24	19	38				
Aug 25	12	24				
Aug 26	12	24				
Aug 27	5	10				
Aug 29	18	36				
Aug 30	10	20				
Aug 31	6	12				
	<u>145-1/2</u>	<u>291</u>				
	- Cementing					
Aug 19	7	14				
Aug 20	2	4				
	<u>9</u>	<u>18</u>				
	<u>183</u>	<u>366</u>				
Rig Hours		183 only	49.00	8,967.00		
Man Hours		366 only	19.25	<u>7,045.50</u>	16,012.50	

suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981

M5J 1T1

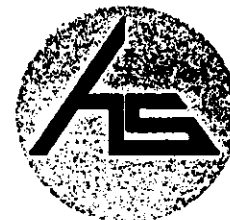
Invoice No. 9320

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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
Aug 19	<u>Standby - Waiting for cement to set</u>					
	Rig Hours.	5 only	42.35	211.75		
	Man Hours	10 only	19.25	192.50		404.25
	<u>Materials</u>					
	N Directional deflecting wedge ass.	Aug 20		605.00		
	Plus 14%			84.70		689.70
	N Clappison wedges	Aug 21 am , pm, 22 pm, Aug 23 pm, 24 pm, 25 pm, Aug 26 pm, 29pm, 30 pm 9 only	185.00			1,665.00
	<u>Cost Plus Diamond Tools</u>					
	BXC concave bit 1G-4050	21.21 cts.	26.00	551.46		
	Setting	1 only		123.28		
	NXC reaming bell bit 1G-3652	29.97 cts.	20.00	599.40		
	Setting	1 only		141.00		
	NQ bit 1G-3592	13.00 cts.	26.00	338.00		
	Setting	1 only		98.25		
	BXC concave bit 1G-4046	21.21 cts.	26.00	551.46		
	Setting	1 only		123.28		
	NQ bit 1G-3587	13.00 cts.	26.00	338.00		
	Setting	1 only		98.25		
				2,962.38		
	Plus 14%			414.73		3,377.11
	<u>Drill #2</u>					
81-76	60° HQ coring					
	19.20	150.00	130.80	123.15	16,108.02	
	150.00	168.25	18.25	128.15	2,338.74	
81-78	83° HQ coring					
	0	5.79	5.79 O/B	119.65	692.77	
	5.79	92.36	86.57	114.65	9,925.25	29,064.78
	<u>Footage Premium re Triple tube drilling</u>					
81-76	131.68	168.25	36.57	28.35		1,036.76
e. & o. e.						

suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981

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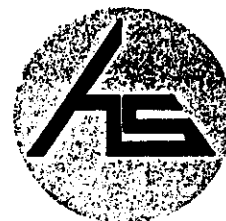
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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
<u>Special Operations - Borehole Surveys</u>						
		<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
81-76	Aug 18	1	2			
	Aug 20	1	2			
	Aug 25	8	16			
81-78	Aug 28	1	2			
	Aug 29	1	2			
	Aug 31	1	2			
		<u>13</u>	<u>26</u>			
- Hole conditioning						
81-76	Aug 18	1	2			
		<u>14</u>	<u>28</u>			
	Rig Hours		14 only	49.00	686.00	
	Man Hours		28 only	19.25	<u>539.00</u>	1,225.00
<u>Special Operations - Moving between holes</u>						
		<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
Aug 26		2	4			
- Tripod						
Aug 30		6	12			
		<u>8</u>	<u>16</u>			
	Rig Hours		8 only	42.35	338.80	
	Man Hours		16 only	19.25	<u>308.00</u>	646.80
<u>Drill #3</u>						
81-70A	440.44	450.00	9.56	108.55	1,037.74	
	450.00	463.61	13.61	113.75	1,548.14	
	463.61	465.13	1.52 S/O Wedge			
	465.13	483.42	18.29	113.75	2,080.49	
	483.42	484.94	1.52 S/O Wedge			
	484.94	552.61	67.67	113.75	<u>7,697.46</u>	12,363.83
<u>Footage Premium re Mini-Deve</u>						
	444.09	463.61	19.52			
	469.09	483.42	14.33			
	485.86	512.38	<u>26.52</u>			
			60.37 M	21.95		1,325.12

suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981
MSJ 1T1

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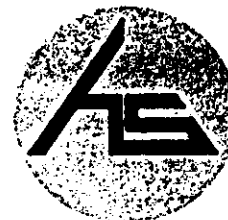
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Invoice No. 9320

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
81-70A	<u>Special Operations - Borehole Surveys</u>					
		<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
	Aug 18	4	8			
	Aug 23	3	6			
	Aug 24	1	2			
	Aug 29	1	2			
	Aug 31	2	4			
		11	22			
			- Wedging			
	Aug 16	18	36			
	Aug 17	12	24			
	Aug 19	24	48			
	Aug 20	7	14			
	Aug 21	8	16			
	Aug 22	12	24			
		81	162			
			- Drilling Cement			
	Aug 16	6	12			
		98	196			
	Rig Hours		98 only	49.00	4,802.00	
	Man Hours		196 only	19.25	3,773.00	8,575.00
	<u>Materials</u>					
	N Clappison Wedges					
	Aug 19th and 22nd		2 only	185.00		370.00
	<u>Cost Plus Diamond Tools</u>					
	NXC belt bit 1A-8373	47.91 cts.		26.00	1,245.66	
	Setting	1 only			141.00	
	BXC concave bit 1G-4047	21.21 cts.		26.00	551.46	
	Setting				123.28	
					2,061.40	
	Plus 14%				288.60	2,350.00
	<u>Drill #4</u>					
	80° NQ coring					
81-75	499.57	553.83	54.26	113.75	6,172.08	
e. & o. e.						

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

September 16th, 1981

to

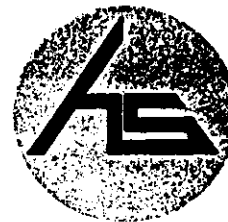
Page -6-

Invoice NO. 9320

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period						
	from	to	footage completed		rate		
81-77	83° HQ coring						
	0	3.96	3.96	O/B	119.65	473.81	
	3.96	121.01	117.05		114.65	13,419.78	
81-77	83° NQ coring						
	121.01	150.00	28.99		99.95	2,897.55	
	150.00	180.75	30.75		104.05	3,199.54	
	180-75	182.27	1.52	S/O. Wedge			26,162.76
	Footage Premium re Triple tube drilling						
81-75	515.73	553.83	38.10		20.20		769.62
	Special Operations - Borehole Surveys						
	Rig Hrs.		Man Hrs.				
81-75	Aug 19	9	18				
81-77	Aug 22	1	2				
	Aug 23	2	4				
	Aug 24	1	2				
	Aug 25	1	2				
	Aug 26	2	4				
	Aug 27	2-1/2	5				
	Aug 29	2	4				
	Aug 30	3	6				
		23-1/2	47				
				- Wedging			
81-77	Aug 30	6-1/2	13				
	Aug 31	24	48				
		30-1/2	61				
				- Pulling casing			
81-75	Aug 20	24	48				
	Aug 21	1	2				
		25	50				
				- Reduce to N hole size			
81-77	Aug 27	6	12				
		85	170				
	Rig Hours		85 only	49.00		4,165.00	
	Man Hours		170 only	19.25		3,272.50	7,437.50
e. & o. e.							

suite 908, 40 university avenue,

toronto, ontario, September 16th, 1981
MSJ 1T1

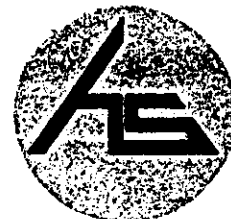
to Page -7-

Invoice No. 9320

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
<u>Standby Rate</u>					
Moving between holes					
		<u>Rig Hrs.</u>	<u>Man Hrs.</u>		
Aug 21		1	2		
Wait for Geologist decision					
Aug 27		1	2		
Aug 29		<u>1</u>	<u>2</u>		
		3	6		
Rig Hours			3 only	42.35	127.05
Man Hours			6 only	19.25	<u>115.50</u>
					242.55
<u>Materials</u>					
N Clappison wedge Aug 31			1 only		185.00
<u>Cost Plus Diamond Tools</u>					
BXC concabe bit 1G-4051			21.21 cts.	26.00	551.46
Setting			1 only		<u>123.28</u>
					674.74
Plus 14 1/2%					<u>94.46</u>
					769.20
<u>Tractor Rental</u>					
Aug 16-31			1/2 month	7,000.00/M	3,500.00
<u>Tractor Driver</u>					
Aug 16-31			1/2 month	5,890.00/M	2,945.00
<u>Skidder Rental</u>					
Aug 16-31			1/2 month	3,320.00/M	1,660.00
<u>Skidder Operator</u>					
Aug 16-31			144 hrs.	19.25	2,772.00
<u>Extra Crew</u>					
D. MacMillan					
Aug 18-20 incl.	3 days x 12 hrs.		36 man hrs.		
K. Kelly					
Aug 21-31 incl.	11 days x 12 hrs.		132		
Lalonde					
Aug 26-30 incl	5 days x 12 hrs.		<u>60</u>		
			228 hrs.	19.25	
					4,389.00

please provide backup

\$164,296.10



E. CARON DIAMOND DRILLING LTD.

7 Roundel Road Whitehorse Yukon Y1A 3H3

Phone (403) 668-2424 Telex 036-8-337

September 15, 1981

Invoice #-1071

88-28

IN ACCOUNT WITH:

Cordilleran Engineering,
1418 - 355 Burrard Street,
Vancouver, B. C.
V6C 2G8

CSH - Copy Sept 25/81

Drilling Charges September 3 to 15, 1981:

(MacPass)

Hole: 81-79/55Moving

84 man hrs. @ \$23.00 per hr. = \$ 1,932.00

Drilling & Reducing

10 man hrs. @ \$23.00 per hr. = \$ 230.00

5 machine hrs. @ \$13.50 per hr. = \$ 67.50 \$ 297.50

Casing

20 man hrs. @ \$23.00 per hr. = \$ 460.00

10 machine hrs. @ \$13.50 per hr. = \$ 135.00 \$ 595.00

Reaming Cave

10 man hrs. @ \$23.00 per hr. = \$ 230.00

5 machine hrs. @ \$13.50 per hr. = \$ 67.50 \$ 297.50

Waterline

8 man hrs. @ \$23.00 per hr. = \$ 184.00

Mud Time & Recovering Return

36 man hrs. @ \$23.00 per hr. = \$ 828.00

18 machine hrs. @ \$13.50 per hr. = \$ 243.00 \$ 1,071.00

Testing

2 man hrs. @ \$23.00 per hr. = \$ 46.00

1 machine hrs. @ \$13.50 per hr. = \$ 13.50 \$ 59.50

Casing

0 - 3.28m @ \$137.80 per m. = \$ 451.98

Coring

3.28 - 138.07 = 134.79 m @ \$132.05 per m. = \$17,799.02

138.07 - 150 = 11.93 m @ \$124.67 per m. = \$ 1,487.31

150 - 300 = 150 m. @ \$127.95 per m. = \$19,192.50

300 - 401.42 = 101.42 m @ \$135.00 per m. = \$13,691.70 \$52,170.53 \$57,059.01

Mobilization Charge

= \$ 3,450.00

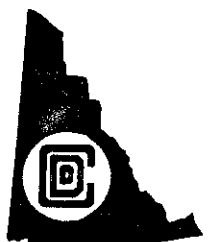
Total Invoice

\$60,509.01

213

Pan O
Jason
60,509.01

B





E. CARON DIAMOND DRILLING LTD.

7 Roundel Road, Whitehorse, Yukon Y1A 3H3

Phone (403) 668-2424 Telex 036-8-337

Pandacan
*Person**213*
81.739.89

Sept. 30, 1981

Invoice #- 1082

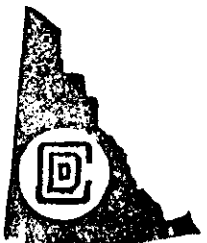
IN ACCOUNT WITH:Cordilleran Engineering,
1418 - 355 Burrard St.,
Vancouver, B.C.
V6C 2G1

Drilling Charges Sept. 16 to Oct. 8, 1981:

(MacPass)

Hole 81-79/55/NQTesting22 man hrs. ✓ @ \$ 23.00 per hr. = \$ 506.00
11 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 148.50 \$ 654.50¹Coring401.42 - 403.96 = 2.54 m @ \$135.00 per m = \$ 342.90⁸ \$ 997.40⁸Hole 81-82/75/HQ/NQMoving197 214 man hrs. @ \$ 23.00 per hr. = \$ 4,922.00^{4531.00}
8½ mach. hrs. @ \$ 13.50 per hr. = \$ 114.75^{4645.75}Drilling8 man hrs. ✓ @ \$ 23.00 per hr. = \$ 184.00[✓]
4 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 54.00[✓] \$ 238.00[✓]Casing20 man hrs. ✓ @ \$ 23.00 per hr. = \$ 460.00[✓]
10 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 135.00[✓] \$ 595.00[✓]Reaming Cave2 man hrs. ✓ @ \$ 23.00 per hr. = \$ 46.00[✓]
1 mach. hr. ✓ @ \$ 13.50 per hr. = \$ 13.50[✓] \$ 59.50[✓]Mud Time6 man hrs. ✓ @ \$ 23.00 per hr. = \$ 138.00[✓]
3 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 40.50[✓] \$ 178.50[✓]Testing52 man hrs. ✓ @ \$ 23.00 per hr. = \$ 1,196.00[✓]
26 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 351.00[✓] \$ 1,547.00[✓]

* Oct 5 D 18 hrs not 35





E. CARON DIAMOND DRILLING LTD.

7 Roundel Road Whitehorse, Yukon Y1A 3H3

Phone (403) 668-2424 Telex 036-8-337

Truck Loading

8 truck hrs. ✓ @ \$ 45.00 per hr. = \$ 360.00 ✓

Standby

6 man hrs. ✓ @ \$ 23.00 per hr. = \$ 138.00

3 mach. hrs. ✓ @ \$ 13.50 per hr. = \$ 40.50 \$ 178.50 ✓

Casing

0 - 4.87 = 4.87 m @ \$137.80 per m ✓ = \$ 671.08 ✓

Coring

4.87 - 147.25 =

142.38 metres @ \$132.05 per m = \$18,801.27 ✓

147.25 - 150 = 2.75 m @ \$124.67 per m = \$ 342.84 ✓

150 - 300 = 150 m @ \$127.95 per m = \$19,192.50

300 - 450 = 150 m @ \$135.00 per m = \$20,250.00

450 - 520.29 = 70.29 m @ \$145.00 per m = \$10,210.90 68,778.66 77,251.99

192.05

\$68,797.51\$77,661.84Demobilization

demob @ \$ 1,150.00 = \$ 1,150.00

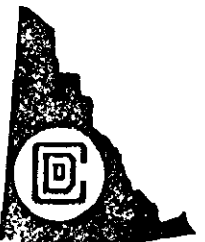
Items Consumed & ChargeableHole 81-79/55/HQ/NQ

17 HQ Rods @ \$ 150.55 X.80% = \$ 2,047.48

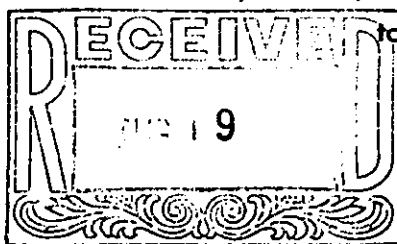
+ 15% = \$ 307.12

\$ 2,354.60 ✓Total Invoice: \$82,163.84

81,739.89



suite 908, 40 university avenue,



Toronto, Ontario,
M5J 1T1

August 13th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8

Invoice No. 9159
D.O. 378
Project No. 80-184

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	HQ, NQ, BQ diamond drilling northeast of Ross River, Yukon Territory July 16th-31st, 1981					
81-68A	90° NQ coring - Drill #1					
	459.33	600.00	140.67M	113.75	16,001.21	
	600.00	694.65	94.65	119.60	11,320.14	27,321.35
	Special Operations - Borehole Surveys					
	Rig Hrs.	Man Hrs.				
July 16	1	2				
July 17	1	2				
July 18	1	2				
July 19	2	4				
July 20	1	2				
July 21	2	4				
July 22	1	2				
		- Wedging				
July 17	8	16				
July 18	7	14				
	24	48				
	Rig Hours		24 only	49.00	1,176.00	
	Man Hours		48 only	19.25	924.00	2,100.00
	Footage Premium re Triple Tube System					
	615.09	694.65	79.56 M	20.20		1,607.11
81-69	80° BQ Coring - Drill #2					
	776-32	900.00	123.68M	114.20	14,124.26	
	900.00	913.50	13.50	121.35	1,638.23	15,762.49
	Special Operations - Borehole Surveys					
	Rig Hrs.	Man Hrs.				
July 16	1	2				
July 19	1	2				
July 25	2	4				
July 26	1	2				
July 29	2	4				

Handwritten signatures and dates:
 213 / 27, 41.15
 b

suite 908, 40 university avenue,

toronto, ontario, August 13th, 1981
MSJ 171

to

Page -2-

Invoice No. 9159

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
	- Hole Conditioning					
July 16	2	4				
July 19	2	4				
July 20	4	8				
July 21	4	8				
July 22	2	4				
July 23	1	2				
July 28	1	2				
	23	46				
	Rig Hours		23 only	49.00	1,127.00	
	Man Hours		46 only	19.25	885.50	2,012.50
	Footage Premium re Triple Tube Systems					
	805.29	810.47	5.18			
	843.39	913.50	70.11			
			75.29M	17.70		1,332.63
81-70	80° NQ Coring - Drill #3					
	574.24	600.00	25.76	113.75	2,930.20	
	600.00	654.41	54.41	119.60	6,507.44	
	654.41	656.24	1.83	S/O Wedge		
	656.24	749.51	93.27	119.60	11,155.09	20,592.73
	Special Operations - Borehole Surveys					
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>				
July 20	1	2				
July 21	1	2				
July 22	1	2				
July 23	1	2				
July 26	1	2				
July 27	1	2				
July 29	1	2				
July 31	3	6				
	10	20				
	- Wedging					
July 24	18	36				
July 25	23	46				
	51	102				

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

August 13th, 1981

to

Page -3-

Invoice No. 9159

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	Rig Hours		51 only	49.00	2,499.00
	Man Hours		102 only	19.25	<u>1,963.50</u>
					4,462.50
	<u>Special Operations - Work on Tripod</u>				
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
July 17	10	20			
July 18	12	24			
July 19	<u>12</u>	<u>24</u>			
	34	68			
	Rig Hours		34 only	42.35	1,439.90
	Man Hours		68 only	19.25	<u>1,309.00</u>
					2,748.90
	<u>Footage Premium - 50 ft. Bit Control</u>				
	644.35	655.02	10.67 M	2.10	22.41
		<u>- NQ Mini-Deve</u>			
	644.35	655.02	10.67	19.50	<u>208.07</u>
					230.48
	<u>Material Used</u>				
	N Clappison Wedge		1 only		185.00
81-75	<u>80° HQ Coring - Drill #4</u>				
	127.10	150.00	22.90	114.65	2,625.49
	150.00	300.00	150.00	119.15	17,872.50
	300.00	406.61	106.61	124.20	<u>13,240.96</u>
					33,738.95
	<u>Special Operations - Borehole Surveys</u>				
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
July 16	2	4			
July 17	3	6			
July 18	2	4			
July 19	1	2			
July 20	2-1/2	5			
July 21	1	2			
July 25	1	2			
July 26	1	2			
July 30	<u>1-1/2</u>	<u>3</u>			
	15	30			

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

August 13th, 1981

Invoice No. 9159

to

Page -4-

in account with

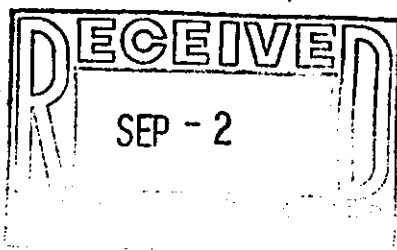
heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
81-74	Rig Hours		15 only	49.00	735.00	
	Man Hours		30 only	19.25	577.50	1,312.50
	<u>Footage Premium - Triple Tube System</u>					
	179.53	274.92	95.39	28.35		2,704.31
	<u>Cost Plus Diamonds</u>					
	BXC Concave bit 1G-4044		1 only			
			21.21 cts.	26.00	551.46	
	Setting				123.28	
					674.74	
	Plus 14%				94.46	769.20
	<u>Tractor Rental</u>					
	July 16-31		1/2 month	7000.00/M		3,500.00
	<u>Tractor Operator</u>					
	July 16-31		1/2 month	5890.00/M		2,945.00
	<u>Skidder Rental</u>					
July 16-31		1/2 month	3320.00/M		1,660.00	
July 1-15		1/2 month	3320.00/M	1,660.00		
Less amount charged on invoice 9091				1,160.00	500.00	
<u>Skidder Operator</u> CORDILLERAN						
July 16-31		ENGINEERING	86 hours	19.25	1,655.50	
	Client	lan O				
	Project	JASON				
		127,141.15				
	Extensions					
	Voucher No.					
	Approved	B				

suite 908, 40 university avenue,


toronto, ontario, August 27th, 1981
M5J 1T1

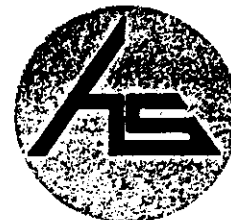
to Cordilleran Engineer,ing
1418-355 Burrard Street,
Vancouver, B.C.
66C 2G8

Invoice No. 9269
D.O. 378
D.O. 80-184

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	HQ, NQ, BQ diamond drilling northeast of Ross River Yukon Territory August 1st-15th, 1981					
	<u>Drill #1</u>					
81-68A	<u>90° NQ coring</u>					
	694.65	750.00	55.36M	119.60	6,619.86	
	750.00	862.90	112.90	126.45	14,276.21	
81-68B	<u>90° NQ coring</u>					
	680.02	736.71	56.69	119.60	6,780.12	27,676.19
	<u>Special Operations - Borehole Surveys</u>					
	<u>Rig Hrs.</u>	<u>Man Hrs.</u>				
Aug 1	2	4				
3	3-1/2	7				
9	<u>11</u>	<u>22</u>				
	16-12	33				
			- Cementing			
10	12	24				
12	<u>20</u>	<u>36</u>				
	32	60				
			- Wedging			
13	24	48				
14	<u>10</u>	<u>20</u>				
	<u>34</u>	<u>68</u>				
	82-1/2	161				
	Rig Hours		82-1/2	49.00	4,042.50	
	Man Hours		161	19.25	3,099.25	7,141.75
	<u>Standby - Wait for cement to set</u>					
Aug 10	12	24				
11	24	48				
12	<u>4</u>	<u>8</u>				
	<u>40</u>	<u>80</u>				
	Rig Hours		40 only	42.35	1,694.00	
	Man Hours		80 only	19.25	1,540.00	3,234.00

suite 908, 40 university avenue,

toronto, ontario, August 27th, 1981
M5J 1T1

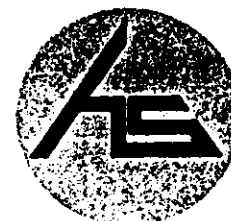
Invoice No. 9269

to Page -2-

in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period						
	from	to	footage completed		rate		
	<u>Special Operations - Other</u>						
July 24	Sand in water tank		10 rig hrs.	42.35	423.50		
			20 man hrs.	19.25	385.00		
					808.50		
	Less Contractor's share				404.25	404	25
	<u>Materials</u>						
Aug 13	N. Directional deflecting wedge assy		1 only		605.00		
	N. Grout plug		1 only		38.50		
					643.50		
	Plus 14%				90.09	733	59
	<u>Footage Premium re Triple Tube System</u>						
81-68A	694.65	716.29	21.64M	20.20		437	13
	<u>Drill #2</u>						
81-69	<u>80° BQ coring</u>						
	913.50	1043.34	129.84M	121.35	15,756.08		
81-76	<u>60° HQ coring</u>						
	0	3.05	3.05 O/B M	133.15	406.11		
	3.05	19.20	16.15	123.15	1,988.87	18,151	06
	<u>Footage Premium re Mini-Deve</u>						
81-69	1003.11	1043.34	40.23M	19.50		784	49
	<u>Special Operations - Borehole Surveys</u>						
	<u>Rig Hrs.</u>		<u>Man Hrs.</u>				
81-69	Aug 1	1	2				
	3	1	2				
	5	1	2				
	10	4	8				
	12	1	2				
	13	2	4				
		10	20				
	- Hole Conditioning						
81-69	Aug 2	1	2				
	11	4	8				
e. & o. e.	5	1	2				
		6	12				

suite 908, 40 university avenue,

toronto, ontario, August 27th, 1981
M5J 1T1

Invoice No. 9269

to

Page -3-

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed		rate	
81-69	Aug 7	<u>8</u> 24	- Reaming Mini-Deve <u>16</u> 48			
	Rig Hours		24 only	49.00	1,176.00	
	Man Hours		48 only	19.25	<u>924.00</u>	2,100.00
Aug 14	Moving between holes - 81-69 to 81-76					
			12 rig hrs.	42.35	508.20	
			24 man hrs.	19.25	<u>462.00</u>	970.20
81-69 July 24	Special Operations - Other					
	Cleaning mud tanks		2 rig hrs.	42.35	84.70	
			4 man hrs.	19.25	<u>77.00</u>	161.70
81-70	Drill #3					
	80° NQ coring					
	749.51	750.00	0.46	119.60	58.60	
	750.00	847.66	97.66	126.45	<u>12,349.11</u>	12,407.71
Aug. 3	Special Operations - Borehole Surveys					
12	Rig Hrs.	Man Hrs.				
	3	6				
	<u>17</u>	<u>26</u>				
	<u>20</u>	<u>32</u>				
11	7	14	- Hole conditioning			
			- Cementing			
13	14	28				
14	3	6				
15	<u>18</u>	<u>36</u>				
	<u>35</u>	<u>70</u>				
	<u>62</u>	<u>116</u>				
	Rig Hours		62 only	49.00	3,038.00	
	Man Hours		116 only	19.25	<u>2,233.00</u>	5,271.00

suite 908, 40 university avenue,

toronto, ontario, August 27th, 1981

MSJ 171

Invoice No. 9296

to

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	- Waiting on Cement to set					
Aug 13	10	20				
14	21	42				
15	6	12				
	37	74				
	Rig Hours		37 only	42.35	1,566.95	
	Man Hours		74 only	19.25	1,424.50	2,991.45
	<u>Materials</u>					
	N Directional deflecting wedge					
	assembly		1 only		605.00	
	Chigougamau plus (Grout)		2 only	38.50	77.00	
					682.00	
	Plus 14%				95.48	777.48
	<u>Drill #4</u>					
81-75	<u>80° HQ coring</u>					
	406.61	450.00	43.39M	124.20	5,389.04	
	450.00	486.77	36.77	129.95	4,778.26	
	<u>80° NQ coring</u>					
	486.77	499.57	12.80	113.75	1,456.00	11,623.30
	<u>Special Operations - Borehole Surveys</u>					
	Rig Hrs.	Man Hrs.				
Aug. 2	1	2				
5	1-1/2	3				
	2-1/2	5				
	- Reduce to N hole size					
11	12	36				
12	12	36				
13	12	36				
	36	108				
	38-1/2	113				
	Rig Hours		38-1/2	49.00	1,886.50	
	Man Hours		113	19.25	2,175.25	4,061.75
	- Clean mud tanks resand					
July 21	3	6				
e. & o. e.						

suite 908, 40 university avenue,

toronto, ontario, August 27th, 1981

M5J 1T1

Invoice No. 9296

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in account with

heath & sherwood drilling

division of challenger international services ltd.

COPILLERAN
ENGINEERING

terms: net cash 15 days after date of invoice

Client

Project

hole no.

to cover diamond drilling for the period

from to footage completed

Extensions

rate

Voucher No.

Approved

Date Paid

July 24
25
26
27
31

8 16
3 6
3 6
3 6
3 6
23 0 46 0

Rig Hours

23 only

42.35 847⁰⁰ 974.05

Man Hours

46 only

19.25 770 885.50

1617 1,859.55

Less Contractor's share (5%)

80850 929.78

80850
929.77

- Modify drill shack

Aug 8

4 rig hrs.

42.35 169.40

8 man hrs.

19.25 154.00

Mechanic - J. Marchand

10 man hrs.

19.25 192.50

515.90

Cost Plus diamonds cutout credits

1 only

NXC reaming bit 1F-7047

Useable recovery

17.80 cts.

20.00 356.00

2 only

BXC concave bits

1F-2743, 1F-2742

Useable recovery

40.95 cts.

26.00 1,064.70

2 only

NX BW core bits

1E-8634, 1E-8638

Useable recovery

10.60 cts.

26.00 275.60

1,696.30

Plus 14%

237.48

(1,933.78)

Tractor Rental

Aug 1-15

1/2 month

7000.00/M

3,500.00

Tractor Driver

Aug 1-15

1/2 month

5890.00/M

2,945.00

Skidder Rental

Aug 1-15

1/2 month

3320.00/M

1,660.00

Skidder Operator

Aug 1-15

96 hrs.

19.25

1,848.00

\$108,391.94

\$108,270.67

c. & o. e.

suite 908, 40 university avenue,

toronto, ontario, July 23, 1981

MSJ 1T1

to Cordilleran Engineering,
1418-355 Burrad Street,
Vancouver, B.C.
V6C 2G8

Invoice No. 9091
D.O. 378
Project No. 80-184

Attn: O.S. Hairsine

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

HQ, NQ, BQ diamond drilling northeast of Ross River, Yukon
Territory - July 1st - 15th, 1981

81-68(A)

90° NQ coring - Drill #1

348.69	364.84	16.15M	NQ	108.55	1,753.08
364.84	366.36	1.52	S/O Wedge		
366.36	385.57	19.21		108.55	2,085.25
385.57	387.09	1.52	S/O Wedge		
387.09	407.51	20.42		108.55	2,216.59
407.51	408.73	1.22	S/O Wedge		
408.73	450.00	41.27		108.55	4,479.86
450.00	459.33	9.33		113.75	1,061.29

11,596 07

Special Operations

Date	Rig Hrs.	Man Hrs.
July 1	8	16
2	4	8
3	3	6
	15	30

- Wedging

July 6	16	32
7	15	30
8	16	32
9	14	28
10	20	40
14	22	44
15	7	14
	110	220

213 / 25,642.68

Extensions	
per No.	
owed	

suite 908, 40 university avenue,

toronto, ontario,

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
<u>- Hole Conditioning</u>				
July 1	3	6		
<u>- Washing Cement</u>				
July 1	5	10		
2	2	4		
3	7	14		
	14	28		
<u>- Borehole Surveys</u>				
July 6	1	2		
7	2	4		
8	2	4		
9	1	2		
11	2	4		
12	1	2		
13	1	2		
14	2	4		
15	1	2		
	13	26		
	155	310		
Rig Hours		155 only	49.00	7,595.00
Man Hours		310 only	19.25	5,967.50
<u>- Waiting on Cement</u>				
July 1	3	6		
2	18	36		
3	14	28		
4	24	48		
5	24	48		
6	5	10		
	88	176		
Rig Hours		88 only	42.35	3,726.80
Man hours		176 only	19.25	3,388.00
				13,562.50
				7,114.80

e. & o. e.

suite 908, 40 university avenue,

toronto, ontario,

MSJ 111

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
	<u>Materials Supplied</u>					
2 only	5/8 X 95ft hoisting cables		148.65	297.30		
	Plus 14%			41.62		
1 only	BQ W/L Bit #1F-1937			320.00		
	Plus 14%			44.80		
				703.72		
	Less amount charged on Invoice No. 9052			620.00	83.	72
	<u>N. Clappison Wedges - July 6,7,8,9,14</u>					
2 only	"N" Grout plugs	5 only	185.00		925.	00
	Plus 14%		38.50	77.00		
				10.78	87.	78
	<u>Drill #2</u>					
31-69	<u>80° BQ coring</u>					
	623.31	750.00	126.69M	108.00	13,682.52	
	750.00	776.32	26.32	114.20	3,005.74	16,688. 26
	<u>Special Operations</u>					
	<u>- Borehole Surveys</u>					
	<u>Date</u>	<u>Rig Hrs.</u>	<u>Man Hrs.</u>			
	July 1	1	2			
	7	1	2			
	10	1 1/2	3			
	12	1	2			
	15	1	2			
		5 1/2	11			
	<u>- Hole Conditioning</u>					
	July 1	7	14			
	2	7	14			
	4	2	4			
	5	4	8			

suite 908, 40 university avenue,

toronto, ontario,

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>
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July 7	4	8	
8	2	4	
13	1	2	
14	3	6	
15	2	4	
	<u>32</u>	<u>64</u>	

- Reaming Hole

July 3	<u>1</u>	<u>2</u>	
	38 1/2	77	

Rig hours	38 1/2 only	49.00	1,886.50
Man hours	77 only	19.25	<u>1,482.25</u>

3,368. 75

- Work on set up (tower)

July 15	2 rig hrs	42.35	84.70
	4 man hrs	19.25	<u>77.00</u>

161. 70

Drill #3

80° NQ Coring

403.56	421.84	18.28	108.55	1,984.29
421.84	423.06	1.22	S/O Wedge	
423.06	442.26	19.20	108.55	2,084.16
442.26	444.09	1.83	S/O Wedge	
444.09	450.00	5.91	108.55	641.53
450.00	461.16	11.16	113.75	1,269.45
461.16	462.39	1.23	S/O Wedge	
462.39	483.41	21.02	113.75	2,391.03
483.41	484.63	1.22	S/O Wedge	
484.63	574.24	89.61	113.75	<u>10,193.14</u>

18,563. 60

suite 908, 40 university avenue,

toronto, ontario,

M5J 1T1

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

Special Operations

- Borehole Surveys

<u>Date</u>	<u>Rig Hrs</u>	<u>Man Hrs</u>
July 1	1	2
2	1	2
3	1	2
4	3	6
6	1	2
7	1	2
8	1	2
10	2	4
11	1	2
12	4	8
13	1	2
14	1	2
15	2	4
	<u>20</u>	<u>40</u>

- Wedging

July 2	19	38
3	12	24
4	8	16
5	23	46
6	11	22
7	21	42
9	23	46
	<u>117</u>	<u>234</u>

- Reaming Hole

July 3	<u>3</u>	<u>6</u>
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suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>
-------------	-----------	--------------------------	-------------

- Hole Conditioning

July 8	<u>1</u> 141	<u>2</u> 282	
Rig Hours		141 only	49.00
Man Hours		282 only	19.25
			6,909.00
			5,428.50

12,337. 50

Footage Premium - 50'Bit Control

403.56	421.84	18.28	
423.06	442.26	19.20	
444.09	461.16	17.07	
462.39	483.41	21.02	
		75.57	6.89

520. 68

Materials Used"N" Clappison Wedges

July 2,5,6,9,14	5 only	185.00	
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925. 00

Drill #480° HQ Coring

124.05	150.00	25.95	114.65	2,975.17
150.00	274.92	124.92	119.15	14,884.22

81-74

80° HQ Coring

0	4.26	4.26 O/B	119.65	509.71
4.26	127.10	122.84	114.65	14,083.61

32,452. 71

81-75

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
	<u>Special Operations</u>					
	- <u>Borehole Surveys</u>					
	<u>Date</u>	<u>Rig Hrs</u>	<u>Man Hrs.</u>			
	July 2	1	2			
	11	6	12			
	12	2	4			
	13	2	4			
	14	1 1/2	3			
	15	4	8			
		16 1/2	33			
	- <u>Install Grout Plug</u>					
	July 11	2	4			
		18 1/2	37			
	Rig Hours		18 1/2 only	49.00	906.50	
	Man Hours		37 only	19.25	712.25	1,618.75
	- <u>Waiting on Instructions</u>					
	July 11	3 rig hrs		42.35	127.05	
		6 man hrs		19.25	115.50	242.55
	<u>Materials Supplied</u>					
81-74	1 only H Grout plug			60.55		
	Plus 14%			8.48		69.03
81-74	6 only 2ft HW casing	51.85		311.10		
	1 only HW Casing shoe #1F-1471X			219.00		
	Plus 14%			530.10		
				74.21		604.31

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period					
	from	to	footage completed	rate		
	<u>Cost Plus Diamonds</u>					
1 only	BXC concave Bit #1F-2743					
			24.86cts	26.00	646.36	
	Settings				<u>122.36</u>	
					768.72	
	Plus 14%				107.62	876.34
2 only	NX BW Bits #IE-8634, IE-8638					
	2 bits @ 13.79 cts.		27.58cts	26.00	717.08	
	Settings		2 only	59.00	<u>118.00</u>	
					835.08	
	Plus 14%				<u>116.91</u>	951.99
1 only	NXC Reaming Bit #1F-7047					
	Setting		29.21cts	20.00	584.20	
					<u>141.00</u>	
					725.20	
	Plus 14%				<u>101.52</u>	826.72
	<u>Diamond Cutout Credits</u>					
6 only	NX BW Bits					
	IE-8632, IE-8633					
	IE-8635 to IE-8637 incl					
	IE-8640					
	Useable recovery		57.90cts	26.00	1,505.40	
2 only	NXC Ball bits					
	1D-9716, 1F-8924					
	Useable recovery		95.05cts	26.00	2,471.30	
3 only	BXC Concave bits					
	IE-4519, IE-4520, IF-2744					
	Useable recovery		68.25cts	26.00	1,774.50	

suite 908, 40 university avenue,

toronto, ontario,

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
3 only	NXC Reaming shells				
	IE-4175, IE-4180, IE-1161				
	Useable recovery		86.85cts	20.00	1,737.00
1 only	NXC Reaming bit				
	IE-9410				
	Useable recovery		18.60cts	20.00	372.00
					7,860.20
	Plus 14%				1,100.43
	Tractor Rental				(8,960.63)
	July 1-15	1/2 month	7000.00/M		3,500.00
	Tractor Operator				
	July 1-15	1/2 month	5890.00/M		2,945.00
	Skidder Rental				
	July 1-15	1/2 month	2320.00/m		1,160.00
	Skidder Operator				
	July 1-15	156 hrs	19.25/Hr		3,003.00
	Labour charge re Mechanic - Grant Construction				
	July 3	4 hrs	39.75		159.00
	Parts supplied - Dozer Corner bits				
	2 only @	113.40	226.80		
	Plus 14%		31.75		258.55
					126,142.68

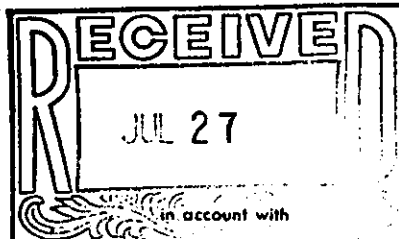
add to 125,642.68

suite 908, 40 university avenue,

toronto, ontario,

July 8th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8.



Invoice No. 9052
D.O. 378
Project No. 80-184

attn: Mr. O.S. Hairsine

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

213 176,067.79

hole no.	to cover diamond drilling for the period					extensions
	from	to	footage completed	rate		
	HQ. NQ, BQ diamond drilling northeast of Ross River, Yukon Territory June 16-30th, 1981					
	90° NQ coring - Drill #1					
81-68	597.71	600.00	2.29 M.	113.75	260.49	
	600.00	750.00	150.00	119.60	17,940.00	
	750.00	900.00	150.00	126.45	18,967.50	
	900.00	971.39	71.39	134.35	9,591.25	46,759.24
	Special Operations - Borehole Surveys					
	Date	Rig Hrs.	Man Hrs.			
81-68	June 17	1	2			
	19	2	4			
	24	1	2			
	29	1	2			
	30	8	16			
		13	26			
	- Hole Conditioning					
	June 18	3	6			
	19	18	36			
	20	5	10			
		26	52			
	Rig Hours		39 only	49.00	1,911.00	
	Man Hours		78 only	19.25	1,501.50	3,412.50
81-69	80° NQ/BQ coring - Drill #2					
	552.30	600.00	47.70 NQ	113.75	5,425.88	
	600.00	604.11	4.11 NQ	119.60	491.56	
	604.11	623.31	19.20 BQ	108.00	2,073.60	7,991.04
	Special Operations - Borehole Surveys					
	Date	Rig Hrs.	Man Hrs.			
	June 16	1	2			
	18	1	2			
		2	4			
	- Reaming Hole					
	June 18	2	4			
	19	2	4			
		4	8			

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981

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in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
		- <u>Cementing</u>		
June 20	1	2		
28	1	2		
29	3	6		
	5	10		
		- <u>Hole Conditioning</u>		
June 18	2	4		
19	22	44		
26	6	12		
27	4	8		
28	7	14		
	41	82		
		- <u>Drilling Cement</u>		
June 21	24	48		
22	12	24		
23	12	24		
24	12	24		
25	12	24		
26	6	12		
30	12	24		
	90	180		
		- <u>Washing Cement</u>		
June 20	13	26		
		- <u>Stuck Rods</u>		
June 20	10	20		
28	4	8		
	14	28		
Rig Hours	169 only	49.00	8,281.00	
Man Hours	338 only	19.25	6,506.50	14,787.50
<u>Special Operations - Waiting on Cement</u>				
June 29	9 rig hrs.	42.35	381.15	
	18 man hrs.	19.25	346.50	727.65
<u>Materials supplied</u>				
5/8" x 95 ft. hoisting cable	2 only		300.00	
NQ impregnated core bit	1 only		320.00	620.00

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981

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division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

81-70

80° NQ coring - Drill #3

from	to	footage completed	rate
128.63	150.00	21.37	99.95
150.00	211.53	61.53	104.05
211.53	213.05	1.52	S/O Wedge
213.05	231.03	17.98	104.05
231.03	232.56	1.53	S/O Wedge
232.56	261.51	28.95	104.05
261.51	262.73	1.22	S/O Wedge
262.73	299.92	37.19	104.05
299.92	301.42	1.50	S/O Wedge
301.42	403.56	102.14	108.55

28,378.12

Footage Premium - Mini-Deve

143.87	211.53	67.66	
213.05	231.03	17.98	
232.56	261.51	28.95	
262.73	299.92	37.19	
301.42	314.55	13.13	
		164.91 M	21.95

3,619.77

- 50 ft. Bit Control

143.87	211.53	67.66	
213.05	231.03	17.98	
232.56	261.51	28.95	
262.73	299.92	37.19	
301.42	403.56	102.14	
		253.92 M	6.89

1,749.51

5,369.28

Special Operations - Borehole Surveys

Date	Rig Hrs.	Man Hrs.
June 16	4	8
17	4	8
18	1	2
19	2	4
20	2	4
21	1-1/2	3
22	1	2
24	1-1/2	3
25	1	2

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981
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Invoice No. 9052

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>	
June 26	1-1/2	3		
27	1-1/2	3		
28	2-1/2	5		
29	1-1/2	3		
30	<u>1</u>	<u>2</u>		
	26	52		
		- Wedging		
June 16	1	2		
19	17	34		
20	11	22		
21	22-1/2	45		
22	2	4		
23	22	44		
24	6-1/2	13		
25	18	36		
26	<u>6-1/2</u>	<u>13</u>		
	106-1/2	213		
Rig Hours		132-1/2	49.00	6,492.50
Man Hours		265	19.25	<u>5,101.25</u>
				11,593.75

Materials Used

June 19	N Clappison Wedge assy -Used	1 only	185.00	
20	"	1 only	185.00	
23	"	1 only	185.00	
25	"	1 only	<u>185.00</u>	740.00

Cost Plus Diamonds

1 only	BXC Concave bit 1F2742	24.86 cts.	26.00	646.36
	Setting			<u>122.36</u>
				768.72
	Plus 14%			<u>107.62</u>
				876.34

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981
M5J 1T1

to

Page -5-

Invoice No. 9052

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period						
	from	to	footage completed		rate		
81-72	80° HQ Coring - Drill #4						
	0	8.84	8.84 M O/B	119.65	1,057.71		
	8.84	150.00	141.16	114.65	16,183.99		
	150.00	202.99	52.99	119.15	6,313.76		
81-73	80° HQ Coring						
	0	3.66	3.66M O/B	119.65	437.92		
	3.66	24.99	21.33	114.65	2,445.48		
81-74	80° HQ Coring						
	0	3.66	3.66 O/B	119.65	437.92		
	3.66	124.05	120.39	114.65	13,802.71	40,679.49	
Moving between holes							
	Rig Hrs.		Man Hrs.				
From 81-71 to 81-72							
	June 16	1	2				
From 81-72 to 81-73							
	June 24 am	3	6				
	pm	4	8				
From 81-73 to 81-74							
	June 26 am	2	4				
		10	20				
	Rig Hours		10 only	42.35	423.50		
	Man Hours		20 only	19.25	385.00	808.50	
Special Operations - Borehole Surveys							
	Date	Rig Hrs.	Man Hrs.				
81-72	June 20 am	2-1/2	5				
	24 am	9	18				
81-73	June 25	1	2				
81-74	June 27 am	1	2				
	pm	1	2				
	28 am	1	2				
		15-1/2	31				
- Pulling Casing							
81-73	June 26 am	2	4				
	Rig Hours		17-1/2	49.00	857.50		
	Man Hours		35	19.25	673.75	1,531.25	
e. & o. e.							

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981
MSJ 171

to

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Invoice No. 9052

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	<u>Company Delays</u>				
	June 23 pm		3 rig hrs.	42.35	127.05
			6 man hrs.	19.25	<u>115.50</u>
					242.55
	<u>Extra crew charges re Spare diller/Timberjack operator</u>				
	May 18th	10 man hrs.			
	19th	8			
	20th	5			
	21st	12			
	22nd	12			
	23rd	12			
	25th	12			
	26th	12			
	27th	12			
	28th	12			
	29th	12			
	31st	12			
		131 man hrs.			
	<u>Less - Tractor Driver Hours</u>				
	May 24th	12			
	25th	12			
		<u>24</u>			
		107 man hours	19.25		2,059.75
	<u>Materials Supplied</u>				
	Valaclay sausages	32 only	9.85	315.20	
	Displacement plugs	24 only	10.70	<u>256.80</u>	
				572.00	
	Plus 14%			<u>80.08</u>	652.08
	<u>Labour charges re Mechanic - Cordilleran</u>				
	May 13th	6			
	19th	1			
	25th	3			
		10 man hours	19.25		192.50

suite 908, 40 university avenue,

toronto, ontario, July 8th, 1981

M5J 1T1

Invoice No. 9052

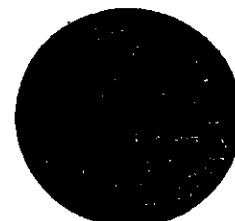
to

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in account with

heath & sherwood drilling

division of challenger international services ltd.



terms: net cash 15 days after date of invoice

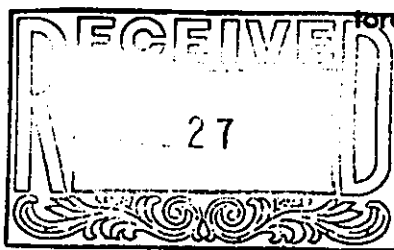
hole no.	to cover diamond drilling for the period					
	<u>from</u>	<u>to</u>	<u>footage completed</u>	<u>rate</u>		
	<u>Labour charges re Mechanic - Grant Construction</u>					
	May 21st	5				
	June 17th	3				
	23rd	1				
	27th	2				
		11 man hours		39.75		437.25
	<u>Tractor Rental</u>					
	June 16-30		1/2 month	7000.00/M		3,500.00
	<u>Tractor Operator</u>					
	June 16-30		12/30 month	5890.00/M		2,356.00
	<u>Skidder Rental</u>					
	June 16-30		1/2 month	3320.00/M		1,660.00
	<u>Skidder Operator</u>					
	June 16-30		36 hrs.	19.25		693.00
						<u>\$176,067.79</u>

suite 908, 40 university avenue,

Toronto, Ontario,
M5J 1T1

June 30th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8



Invoice No. 9046
D.O. 378
Project No. 80-184

attn: O.S. Hairsine

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				ENGINEER
	from	to	footage completed	rate	Project
	HQ, NQ, BQ diamond drilling northeast of Ross River, Yukon Territory - June 1st-15th, 1981				(213) 166.087.91
	<u>Mobilization</u> - from drill staging area to first drill sites				Extensions
	Drills #3 and #4				Voucher
					Approve
	Date	Rig Hrs.	Man Hrs.		
	June 4	8	8		
	5		32		
	6	24	48		
	7	22	20		
		54	108		
	Rig Hours	54 only	42.35	2,286.90	
	Man Hours	108 only	19.25	2,079.00	4,365.90
81-68	<u>90° NQ coring - Drill #1</u>				
	213.06	298.09	85.03M	104.05	8,847.37
	298.09	299.62	1.53 S/O Wedge		
	299.62	300.00	.38	104.05	39.54
	300.00	325.22	25.22	108.55	2,737.63
	325.22	326.44	1.22 S/O Wedge		
	326.44	359.05	32.61	108.55	3,539.82
	359.05	360.27	1.22 S/O Wedge		
	360.27	412.69	52.42	108.55	5,690.19
	412.69	414.22	1.53 S/O Wedge		
	414.22	432.21	17.99	108.55	1,952.81
	432.21	433.43	1.22 S/O Wedge		
	433.43	447.45	14.02	108.55	1,521.87
	447.45	448.97	1.52 S/O Wedge		
	448.97	450.00	1.03	108.55	111.81
	450.00	597.71	147.71	113.75	16,802.01
	<u>Footage Premium - Mini-Deve</u>				
	213.06	241.70	28.64		
	303.89	308.76	4.87		
	374.29	379.48	5.19		
			38.70	21.95	849.47
e. & o. e	- Bit Restriction (50 ft.)				
	213.06	576.68	363.62	6.89	2,505.34
					3,354.81

suite 908, 40 university avenue,

toronto, ontario, June 30th, 1981
M5J 1T1

to

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Invoice No. 9046

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

Special Operations - Wedging

Date Rig Hrs. Man Hrs.

June 3	14-1/2	29
4	7	14
5	9	18
6	15	30
7	3	6
8	18	36
9	18	36
10	17-1/2	35
	<u>102</u>	<u>204</u>

- Borehole Surveys

June 1	2	4
2	2	4
3	3	6
4	1	2
5	3	6
6	1	2
7	1/2	1
8	2	4
9	1	2
10	1	2
11	2	4
12	2	4
13	2	4
14	2	4
15	<u>1</u>	<u>2</u>
	25-1/2	51

Rig Hours	127-1/2 only	49.00	6,247.50	✓	
Man Hours	255 only	19.25	4,908.75	✓	11,156.25

Wedging materials used

1 only Clappison deflecting wedge

Date

June 3	New assembly	985.00	
4	Used assembly	185.00	
6	"	185.00	
8	"	185.00	
9	"	185.00	
10	"	185.00	✓ 1,910.00

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

June 30th, 1981

Page -5-

INVOICE No. 9046

to

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from	to	footage completed	rate
------	----	-------------------	------

Company Delays

June 9	2 rig hrs.	42.35	84.70
	4 man hrs.	19.25	77.00

161.70

Wedging Materials Used

June 10 Used assembly			185.00
14 "			185.00
15 "			185.00

555.00

50° HQ/NQ Coring - Drill #4

0	12.80	12.80M O.B	133.15	1,704.32
12.80	108.20	95.40 HQ	123.15	11,748.51

13,452.83

Special Operations - Borehole Surveys

Date	Rig Hrs.	Man Hrs.
------	----------	----------

June 12	1-1/2	3
15	3	6
	4-1/2	9

Rig Hours	4-1/2 only	49.00	220.50
Man Hours	9 only	19.25	173.25

393.75

Tractor Rentals

June 1-15	1/2 month	7000.00/M
-----------	-----------	-----------

3,500.00

Tractor Operator

June 1-15	1/2 month	5890.00/M
-----------	-----------	-----------

2,945.00

Skidder Rental

June 1-15	1/2 month	3320.00/M
-----------	-----------	-----------

1,660.00

Skidder Operator

June 5-15	96 hrs.	19.25/hr
-----------	---------	----------

1,848.00

Truck Rental

Billed 2 trucks	1/2 month	850.00/M	850.00
Plus 14%			119.00
			969.00

Should have billed

2/31 month 2 trucks	850.00/M	54.84
Plus 14%		7.68
		62.52

Net Credit

(906.48) ✓

suite 908, 40 university avenue,

**toronto, ontario,
M5J 1T1**

June 30th, 1981

to

Invoice No. 9046

Page -6-

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

[illegible]

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

June 12th, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8

Invoice No. 9025
D.O. 378
Project No. 80-184

Attn: Mr. O.S. Hairsine

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
	HQ, NQ, BQ diamond drilling northeast of Ross River, Yukon Territory May 16th - 31st, 1981				
	Mobilization - from drill staging area to first drill sites				
Date	Rig Hrs.	Man Hrs.			
May 16	24	108			
17	24	60			
18	2	8			
19		12			
20		7			
24		60			
25		24			
26		4			
28		4			
29		4			
	50	291			
	Rig Hours		50 only	42.35	2,117.50
	Man Hours		291 only	19.25	5,601.75
	90° HQ Coring Drill #1				
81-68	0	7.92 M	7.92 O/B	119.65	947.63
	7.92	150.0 HQ	142.08	114.65	16,289.47
	150.0	213.06 HQ	63.06	119.15	7,513.60
	Special Operations - Overburden Reaming Casing				
	Rig Hrs.	Man Hrs.			
May 18	7	14			
	Rig Hours		7 only	49.00	343.00
	Man Hours		14 only	19.25	269.50
	Bore Hole Surveys				
	Rig Hrs.	Man Hrs.			
May 19	1	2			
20	2	4			
21	5	10			
29	4-1/2	9			
30	3	6			
31	2	4			
e. & o. e.	17-1/2	35			

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Jasan
213
68.47/25
OKA

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

June 12th, 1981

to Page -2-

Invoice No. 9025

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
81-68	Rig Hours		17-1/2	49.00	857.50
	Man Hours		35	19.25	673.75
	<u>Wedging</u>				
	Rig Hrs.	Man Hrs.			
May 28	19-1/2	39			
	Rig Hours		19-1/2	49.00	955.50
	Man Hours		39	19.25	750.75
	<u>Company Delays</u>				
	Rig Hrs.	Man Hrs.			
May 21	2	4			
	Rig Hours		2	49.00	98.00
	Man Hours		4	19.25	77.00
	<u>Bit Restrictions</u>				
May 29	20 ft. control HQ 107.28 M to 113.38				
			= 610	44.62	272.18
May 29 to					
31	50 ft. bit control HQ 113.38 to 213.05				
			= 99.67	11.81	1,177.10
	<u>80° HQ Drilling - Drill #2</u>				
81-69	0	12.19	12.19 O/B	119.65	1,458.53
	12.19	150.0 HQ	137.81	114.65	15,799.92
	150.0	171.90 HQ	21.90	119.15	2,609.88
	<u>Special Operations - Overburden Ream casing</u>				
	Rig Hrs.	Man Hrs.			
May 21	11	22			
29	3	6			
31	11-1/2	23			
	25-1/2	51			
	Rig Hours		25-1/2	49.00	1,249.50
	Man Hours		51	19.25	981.75
e. & o. e.					

suite 908, 40 university avenue,

toronto, ontario, June 12th, 1981
MSJ 171

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Invoice No. 9025

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.	to cover diamond drilling for the period				
	from	to	footage completed	rate	
<u>Bore Hole Surveys</u>					
	Rig Hrs.	Man Hrs.			
May 23	1-1/2	3			
25	1	2			
26	1	2			
27	1	2			
28	1	2			
29	1	2			
	6-1/2	13			
	Rig Hours		6-1/2	49.00	318.50
	Man Hours		13	19.25	250.25
<u>Tractor Rental</u>					
	May 16th-31st		1/2 month	7000.00/M	3,500.00
<u>Tractor Operator</u>					
	May 16th-31st		1/2 month	5890.00	2,945.00
<u>Skidder Rental</u>					
	May 30th and 31st		2/31/M	3320.00	214.19
<u>Skidder Operator</u>					
	May 30th		12 hours	19.25	231.00
<u>Truck Rental —</u>					
	May 16-31st (2 trucks)		1/2 month	850.00/M	
	Plus 14%			119.00	969.00
					<u>\$68,471.25</u>
<i>OK will come for Truck Rent next invoice</i>					

CORDILLON
ENGINEERING

Client

Project

Extensions

Voucher No.

Approved

Date Paid

e. & o. e.

suite 908, 40 university avenue,

toronto, ontario,
M5J 1T1

June 3rd, 1981

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8

Invoice No. 9001
D.O. 378
Project No. 80-184

Attn: Mr. O.S. Hairsine

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.		to cover diamond drilling for the period			
		from	to	footage completed	rate
		HQ, NQ, BQ diamond drilling north east of Roos River, Yukon Territory			
		Mobilization - to drill staging area - Lump Sum			
		75% of \$62,540.00			
		- From drill staging area to first drill sites			
		2 drills			
					46,905.00
Date		Rig Hrs.	Man Hrs.		
May 13		24	108		
14		24	108		
15		24	108		
		72	324		
		Rig Hours	72 hrs.	42.35	3,049.20
		Man Hours	324 hrs.	19.25	6,237.00
		<u>Tractor Rental</u>			
		May 1st-15th	1/2 month	7000.00/M	3,500.00
		Tractor Operator	3/31 month	5890.00/M	570.00
		<u>Truck Rental</u>			
		May 1st-15th	2 Trucks 1/2 month @ \$850.00/M		
		Plus 14%		119.00	969.00
					\$61,230.20

CORDILLERAN
ENGINEERING

Client _____

Project _____

2/13 Extensions _____

Voucher No. _____

Approved _____

suite 908, 40 university avenue,

toronto, ontario, May 5th, 1981
M5J 1T1

to Cordilleran Engineering,
1418-355 Burrard Street,
Vancouver, B.C.
V6C 2G8

Invoice No. 8965
D.O. 378
Project No. 80-184

in account with

heath & sherwood drilling

division of challenger international services ltd.

terms: net cash 15 days after date of invoice

hole no.

to cover diamond drilling for the period

from to footage completed rate

HQ, NQ, BQ diamond drilling Jason property northeast of Ross River, Yukon Territory.

Extra costs re early mobilization

Air fare - 4 men x 1820.00

7,280.00 ✓

Labour

March 25th 20 man hrs.

26th 32

27th 32

28th 32

29th 32

30th 32

31st 32

April 1st 32

2nd 32

3rd 32

4th 48

5th 32

6th 32

7th 32

8th 32

484 man hrs.

Handwritten: 213 28019.40

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Tractor Rental

March 23rd-Apr 30, 1981 1-9/31 months 7000.00/M

9,032.25 ✓

Advance Truck Rentals (2)

March 25th-31st 2 x 198.31 396.62

April 1st-30th 2 x 850.00 1,700.00

2,096.62

Plus 14%

293.53

2,390.15 ✓

\$28,261.40

Handwritten: #2109 11/29/81

Handwritten: Pd

28.019.40

G E O L O G F I L D L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-7N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 75-DH001
TOTAL DEPTH/LENGTH : 31.09
CORE/HOLE DIAMETER : 60WCOLLAR ELEVATION: 1295.86
NORTHING(- IF S): 7002620.00
EASTING (- IF W): 436462.69AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

F - I N T E R V A L -		CORE	T- %	TYPI- HAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																			
K L (UNITIS = . DEC. PLACE DECIM-		W M ROCK	RYING	MIN	THRES	CHARACS		H	H	H	H	ANY	H	H	ANY	ALT	ORE														
F A (MI=METRIC FT=FOOTRIC)		ERY	G I	TM	TM	MAI	TX	TX	F	C	%	M	ARG	/RJ	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-
Y G F R Q M - T O - T H T (.)		D X	TYPE	1	2	QMI	1	2	F	F	C	A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
K F		ROCK	FM	RT	TR	QMI	TX	TX	S	C	O	O	CHT	1	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E L		QUAL	AGE	FR	W	LC	3		3	4	0		/	2	A7M	RT	H	H	H	H	H	H	H	H	H	H	1		1		
Y G		DESIG	MIN	COL					R		C				STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	2		2		

R SVY 0.00 0.00 NO DRILL HOLE SURVEYS.

R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAC OCEAN OIL LTD.

JASCO PH-ZE-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRVERSE :75-DH004
TOTAL DEPTH/LENGTH : 67.67
CORE/HOLE DIAMETER : BQ41COLLAR ELEVATION : 1305.03
NORTHING (= IF S): 7002697.00
EASTING (= IF E): 436466.50AZIMUTH(DEG) : 180.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810618
PROJECT NUMBER : J-MAIN

R HED

ORIGINALLY LOGGED BY DR. K.I.LU.

F = 10 T E R M A L =		CORE T = %	TYPT= DAL	TEX= GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY															
K	L (UNITS = DEC.PLACE)	RECV=	W A ROCK	FLYING	BIT	TUBES	CHARACS																			
E	A (METRIC FT=FOOTRIC)	FRY	D I	TX	TX	TX	F C % M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	MIN	-	-	-	
Y	G F R O D = 10 = 10 T (.)	D X	TYPE	1	2	OP1	1	2	F F (A		1	AZM	RT	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A
K	F	ROCK	FM	RT	FM	Q42	TX	TX	S C O U	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA		
E	L	QUAL	AGE	EN=	Q	LC=	3	3	4	0	/	2	AZM	RT	H	H	H	H	H	H	H	H	H	1	1	
Y	G	DESIG	VIR	COL			R	C																2	2	

/ QVB 0.01 36.27 36.27

OVER

P

K 041 36.27 36.27 0.00

/ L SX 36.27 51.21 14.94

SULF

BA

LM

P

L5

L)

L)

48

L

L=

/ L 43.28 47.85 4.57

X SULF

BA

GRX LM

R

L5

L)

L)

48

L

L=

/ 47.85 50.29 2.44

X LOST

R

/ 50.29 51.21 0.92

X SULF

BA

LM

R

L)

L5

L)

L)

48

L

L=

K LM1 51.21 51.21 0.00

/ 51.21 53.95 2.74

ARGI

DE

S12

0 2 2 2

P

V)

V)

L)

L

/ 53.95 67.67 13.72

BRBT

*SI

RS DE

NO2

P

#1

L

5A

G; CH 2

1

MN6

R 53.95 67.67

RADIA SEQUENCES ARE :ABC,ABA

A UTM	SAMPLE		% PB	% ZR	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH	
A LAB	SERIAL		B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		
A TYP	NUMBER		H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH			BA	BA	BA	WA	WA	WA	WA	WA		
R ASY	0.00	0.00	B.CLG = HOLDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00	BA = GET ANALYSIS.									
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01									
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	36.27	37.19	092	1.18	3.54	49.10	-0.01	-0.1	-0.1	-0.1	0.01	53.52
A 001	37.19	38.40	121	0.50	3.78	44.13	0.03	-0.10	-0.1	-0.1	0.02	48.26
A 001	38.40	40.23	183	1.03	4.14	39.34	-0.01	-0.10	-0.1	-0.1	0.02	44.22
A 001	40.23	43.28	305	0.20	6.54	-0.1	0.12	-0.1	-0.1	-0.1	-0.1	6.36
A 001	43.28	47.85	457	4.88	13.15	2.92	1.00	-0.10	-0.1	-0.1	0.09	21.74
R ASY	40.28	47.85	SLUDGE SAMPLE ONLY.									
A 001	50.29	51.21	092	5.17	13.73	0.93	1.94	-0.10	-0.1	-0.1	0.08	22.55
A MAX	36.27	51.21		5.17	13.73	49.10	1.94	-0.10	-0.1	-0.1	0.09	70.73

A MIN				0.20	3.54	-0.1	-0.01	-0.10	-0.1	-0.1	0.01	3.34
A CMP	56.27	43.28	701	0.61	5.04	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	5.05
A CMP	43.28	47.35	457	4.48	13.15	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	17.43
R ASY	47.85	50.29	NO CORE.									
A CMP	50.29	51.21	092	6.17	13.73	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	19.30
R ASY	0.00	0.00	OLD LOGS SHOW ONLY COMBINED PB+ZR% FOR A CMP LOGS DO NOT SHOW									
R ASY	0.00	0.00	SEPARATED VALUES FOR PB AND ZR IN % COMBINED, SAMPLE NUMBERS									
R ASY	0.00	0.00	AND CORE RECOVERY.									

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAC OCEAN OIL LTD.
JASOR PD-75-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE :75-00005
TOTAL DEPTH/LENGTH : 149.82
CORE/HOLE DIAMETER : 304LCOLLAR ELEVATION: 1315.00
NORTHING (= IF S): 7002748.00
EASTING (= IF E): 436468.56AZIMUTH(DEG) : 180.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810619
PROJECT NUMBER : J-MAIN

R HED ORIGINALLY LOGGED BY DR. K.I.LO, 1975.

F - I N T E R V A L -		CORE	T- %	TYPI- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																				
K L (UNITS = DEC.PLACE) RECDV=		R K	ROCK	FLYING	MIN	TURES	CHARACS	H	H	H	H	ANY	H	H	ANY	ALT	ORE															
E	A	(M=METRIC FT=FOOTRIC)	ERY	D I	TM	TM	MAI	TX	TX	F	C	%	M	ARG	/RT	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-
Y	G	F R D 4 - T D - I N T (.)	D Y	TYPE	1	2	QRI	1	2	F	F	C	A		1		AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2

K	F		ROCK	FR	RT	TM	MAI	TX	TX	S	C	U	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA			
E	L		QUAL	AGE	FR	D	LC	3		3	4	O	/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1	
Y	G		DESG	MIR	COL					R	C						STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2	

Z DVB 1.00 5.05 5.05 OVER P
R 1.00 5.05 CORE IS BADLY BROKEN. RECOVERY IS VERY POOR.

Z 5.05 18.40 15.35 ARSB SI2 LM RD 2 2 5 2 P 3 RD 055 L)
L S (L RD

Z FLT 18.40 19.40 1.00 ARSB SI2 LM RD 2 2 5 2 P 3 RD 055 L)
L S (L RD

Z FLT 19.40 26.00 6.20 FAUL *S7 P
L *R2 1 9

Z 26.00 88.39 60.39 ARBL CR SF SM1 LM CH 1 1 1 P RD 40 V* L)
L 4 SI1 // CC

Z 42.50 49.00 6.50 X ARSJ SI2 LM 1 4 2 4 P RD 20 K) V.
L 5 //

Z 66.39 94.18 5.79 BRBT BS DB OP5 P
L 6 R; 2 2 2 C NO1
R 66.39 94.18 BS ARE ARC AND AD. FOUND FROM 88.39 TO 103.33

Z 94.18 95.40 1.22 SAND 4 4 4 P 2 D=
L 6

Z 95.40 99.97 4.57 ARBL CR LM 1 1 1 P RD 30 L) L=
L 4 SF SI1 CC

Z 99.97 101.00 1.03 BRBT L02 P
L 6 DB 7 6 0 LM2

[illegible]

A UNM	SAMPLE		% PR	% 7H	% BA	OZ AG	% CU	% FE	OZ AU	% CO	HASH	
A LAP	SERIAL		B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		
A TYP			H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH			WA	WA	WA	WA	WA	WA	WA	WA		
R ASY	0.00	0.00	B.CLG = BODAR CLERG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00	WA = WET ANALYSIS.									
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -0.1. E.G. -0.01									
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	94.18	95.40	122	0.01	0.04	0.87	0.01	-0.10	-0.1	-0.1	0.01	0.64
A 001	103.33	105.46	213	1.05	5.22	39.08	-0.01	-0.10	-0.1	-0.1	0.01	45.05
A 001	105.46	106.98	152	0.75	5.66	41.71	-0.01	-0.10	-0.1	-0.1	0.01	47.82
A 001	106.98	108.51	153	0.75	4.26	46.60	-0.01	-0.10	-0.1	-0.1	0.01	51.31
A 001	108.51	110.93	152	0.90	4.08	46.84	-0.01	-0.10	-0.1	-0.1	0.01	51.52
A 001	110.93	111.56	153	1.18	3.96	46.14	-0.01	-0.10	-0.1	-0.1	0.01	50.98
A 001	111.56	113.04	148	1.08	3.18	47.82	-0.01	-0.10	-0.1	-0.1	0.01	51.78
A 001	113.04	114.60	152	1.03	4.20	44.85	0.03	-0.10	-0.1	-0.1	0.01	49.82
A 001	114.60	116.13	153	1.03	3.30	43.76	-0.01	-0.10	-0.1	-0.1	0.01	47.79
A 001	116.13	117.65	152	0.65	5.66	39.02	-0.01	-0.10	-0.1	-0.1	0.02	45.04
A 001	117.65	119.18	153	0.35	3.90	44.62	0.03	-0.10	-0.1	-0.1	0.02	49.12
A 001	119.18	120.70	152	3.45	4.74	42.80	0.03	-0.10	-0.1	-0.1	0.02	50.74
A 001	120.70	122.22	152	0.85	3.42	38.42	-0.01	-0.10	-0.1	-0.1	0.01	42.39
A 001	122.22	123.75	153	1.00	2.52	41.81	0.03	-0.10	-0.1	-0.1	0.01	45.37
A 001	123.75	125.27	152	1.13	3.42	41.28	-0.01	-0.10	-0.1	-0.1	0.02	45.54
A 001	125.27	126.80	153	6.39	5.77	8.10	0.15	-0.10	-0.1	-0.1	0.02	20.13
A MAX	94.18	126.80		6.39	5.77	47.82	0.15	-0.10	-0.1	-0.1	0.02	59.85

A MIN				0.01	0.04	0.87	-0.01	-0.10	-0.1	-0.1	-0.01	0.80
A CMP	104.53	119.18	1585	0.93	4.37	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.70
A CMP	119.18	126.80	762	2.57	4.03	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	6.00

G E O L O G I C A L L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PACIFIC OIL LTD.

JASIN 28-20-AR-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 75-DH066

COLLAR ELEVATION: 1262.21

AZIMUTH(DEG) : 45.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 117.65

NORTHING(- IF S): 7092617.00

VERTICAL ANGLE : -50.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 80MM

EASTING (- IF W): 436109.06

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-RECC

F - I N T E R V A L -		CORE	T- 2	TYPI- NAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L	(UNITS = . DEC.PLACE)RECOV-	F	R	ROCK	FRYING	MINS	TUNES	CHARACS			
E	A	(FT=METRIC FT=FOOTRIC) ERY	G	J	1	2	3	4	5	6	7	8
Y	G	F R O I - T D - I N T (.)	D	X	TYPE	1	2	3	4	5	6	7
K	F	ROCK	FR	RT	1	2	3	4	5	6	7	8
E	L	DUAL	AGE	EN	1	2	3	4	5	6	7	8
Y	G	DESIG	VER	COL	1	2	3	4	5	6	7	8

R SVY 0.00 0.00 NO DOWN HOLE SURVEY DATA.

R ASY 0.00 0.00 NO SIGNIFICANT ASSAY DATA (I.E. NO SULFIDE INTERSECTIONS).

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASCO PA-26-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 75-04007

COLLAR ELEVATION: 1271.44

AZIMUTH(DEG) : 225.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 163.98

DEPTH(= IF S): 7092638.00

VERTICAL ANGLE : -50.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 80MM

EASTING (= IF S): 436162.00

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

F - I N F E R V A L -		CORE	1 - 2	TYPI- GAL	TEX- GRAID	PGT	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																					
K	L (UNITS = . DEC.PLACE)RECOV-	W	A	ROCK	RYING	DIV	TUNES	CHARACS	H	H	H	H	ANY	H	H	ANY	ALT	ORE															
E	A (MT=METRIC FT=FOOTRIC)	ERY	H	T	TR	TR	TR	TR	TX	TX	F	C	Z	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	MIN	-	-	-	-
Y	G	F	R	D	H	-	I	D	-	I	D	I	D	I	D	I	D	I	D	I	D	I	D	I	D	I	D	I	D	I	D	I	D
K	F																																
E	L																																
Y	G																																

R SVY 0.00 0.00 NO DOWN HOLE SURVEY DATA.

R ASY 0.00 0.00 NO SIGNIFICANT ASSAY DATA (I.E. NO SULFIDE INTERSECTIONS).

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

FORMAT VERSION : 6B02

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-RECC

SER. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	121.92	0.00	-48.00
2	152.00	0.00	-42.50
3	182.88	0.00	-35.00
4	213.56	0.00	-31.00
5	245.84	0.00	-28.00
6	274.52	0.00	-24.50
7	306.80	0.00	-28.00
8	335.28	0.00	-25.50

F - I - E - R - V - A - L - CORE T - % TYPE - GAL TEX - GRAIN PGI STRUCTUR-1 ALTERATION MINS ORE - TYPE MINS SUMMARY																		
K	L	(CHITS = DEC. PLACE)	RECOV -	M - H	ROCK	RYING	MIN	TURES	CHAPACS	PGI	STRUCTUR-1	ALTERATION	MINS	ORE - TYPE	MINS	SUMMARY		
F	A	(LI=METRIC FI=FOOTRIC)	ERY	D	T	IN	TX	TX	F C % M	ARG	/RI	T	ID	STK	DIP	A A A A A MIN A A A MIN	- - - -	
Y	G	F R O H - T H - T R T (.)	D	X	TYPE	1	2	041	1	2	F F C A		1	AZM	RT	OZ FL CY CA BA XX PY CP GL YY	A 1 A 2	
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
K	F		ROCK	FM	RT	IN	042	TX	TX	S C O O	CHT		1	ID	STK	DIP	MG MU CL SD QS HA PR MT SL HA	
F	L		QUAL	AGE	FR	O	LC	3	3	4	O	/	2	AZM	RT	H H H H H H H H H H	1 1	
Y	G		DESIG		VIR	COL				R	C			STRUCTUR-2		A A A A A A A A A A	2 2	

R SVY	0.00	0.00	DTP TESTS ONLY.
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R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAC OCEAN OIL LTD.

JASIN PP-7R-AG-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE :76-DH010	COLLAR ELEVATION: 1246.54	AZIMUTH(DEG) : 90.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 133.20	NORTHING(- IF S): 7002368.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : 80MM	EASTING (- IF E): 436381.94	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

F - I T E R V A L - CORE T- % TYPE- QAL TEX- GRAIN										PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY									
K L (UNITS = . DEC.PLACE)RECOV- M B ROCK FRYING MIN TURES CHARACS										H H H H H ANY H H H ANY ALT ORE									
E A (M1=METRIC FT=FOOTRIC) ERY B T 1M TM QAT TX TX F C % M ARG /RI T ID STK DIP A A A A A MIN A A A MIN - - - -																			
Y G F R Q A - T O - I N T (.) D X TYPE 1 2 QM1 1 2 F F C A										1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2									
K F ROCK FR RT TM QM2 TX TX S C O O CHT										T ID STK DIP MG MU CL SD QS HA PR MT SL HA									
E L QDAL AGE FM- H LC- 3 3 4 O /										2 AZM RT H H H H H H H H H H 1 1									
Y G FESIG VIR COL R C										STRUCTUR-2 A A A A A A A A A A 2 2									

R SVY 0.00 0.00 NO DATA HOLE SURVEY DATA.

R ASY 0.00 0.00 NO ASSAY DATA THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAC OCEAN OIL LTD.
JASON PR-7R-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 76-DH011	COLLAR ELEVATION: 1274.16	AZIMUTH(DEG) : 0.00	GEOLOGGED BY : BHO + JMM
TOTAL DEPTH/LENGTH : 141.75	DEPTHING(= IF S): 7002524.00	VERTICAL ANGLE : -55.00	DATE (YY/MM/DD): 811023
CORE/HOLE DIAMETER : 804L	EASTING (= IF S): 436652.00	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	0.00	-53.00
2	60.95	0.00	-45.00
3	91.44	0.00	-35.00
4	121.92	0.00	-30.00

R HED ORIGINALLY LOGGED BY DR. K. I. LU, AUG. 1976.

R HED (1)TARGET: THE PURPOSE OF 76-DH011 WAS TO DETERMINE THE POSSIBLE

R HED EASTERN EXTENSION OF THE MAIN ZONE BEYOND OF

R HED 75-DH005.

R HED (2)RESULTS: THE ORE ZONE WAS INTERSECTED AT BENCH LEVEL, 1195

R HED METERS AND 168 METERS EAST OF 75-DH005. THE ORE ZONE

R HED EXTENDS FROM 122.83 M. TO 138.38 M., WITH AN

R HED APPARENT THICKNESS OF 15.55 METERS. THE TRUE

R HED THICKNESS IS 7.78 METERS. MINOR AMOUNTS OF PB, ZN

R HED AND AG OCCURS IN THE UNDERLYING BRECCIA. THE AVERAGE

R HED GRADE OF PR-7R IN THE INTERVAL BETWEEN 122.83 TO

R HED 139.90 IS 1.65% PB AND 6.17% ZN. THE PERCENT CORE

R HED RECOVERY FROM 122.83 TO 138.38 IS 19.14%. DUE TO

R HED THIS LOW RECOVERY, OBSERVATIONS IN ORE ZONE ARE

TENTATIVE.

(3) MINERALIZATION: AVAILABLE CORE INDICATES THAT THE ZONE WAS

PREDOMINANTLY LOSS WITH LOCAL INTERVALS OF

FIG. 8. SLUDGE SAMPLES WERE TAKEN OVER THE

INTERVAL BETWEEN 127.10 AND 130.76 METERS

AND SAMPLE IS IN THE CORE BOX.

44.57 45.37 QUARTZ VEINS, BOTH APPROX. 8 CFS.

AutoTid BY **BBF**

G E U L G G

JASON PR-26-AG-PA STF DEPOSIT, Y.T.
DRILLHOLE/IKOVERSE --- 76-DH011 --- (CONTINUED)

PAGE - 3

[illegible]

R	45.37	50.07	THE UNIT IS INTERMIXED WITH TWO BRECCIA EVENTS OF BRHT
R	45.37	50.07	COMPOSITION. THE INTERVAL GETS FINER TOWARDS THE TOP. IT
R	45.37	50.07	CONTAINS MAINLY THE A HORIZON IN THE FOUMA SEQUENCE.

/ 45.37 95.95 9.56 x CORR *US F* R* L03 R () D)

1				RA	*S1	3 0 1	KN5		D*
R	45.37	45.95	FAIRIX IS SAND RICH.						

Z	46.60	47.24	0.64	X CGCR	*05 F* R*	L03	R	>=	R)
L				8A	*9=	3	L06	D=	
R	45.66	47.24	MATRIX IS SAND RICH.						

7	47.43	47.67	0.24	7 MEIN SF	5.22 54X	R	>7	D-
1				5.9				D)

/	50.07	51.43	1.81	REPT	SI= SS FI	MF8	P	
1				4A	*I= F* R* 3	KN=		(R)

R	50.07	51.88	THERE IS APPROX. 2% TO 3% SANDSTONE CLASTS IN THE INTERVAL.
R	50.07	51.88	THERE APPEARS TO BE A GRADUAL FINEING UPWARDS WITHIN THIS FLOW.

1	51.88	56.98	5.10	BRIT	*C1 F* R*	LR5	P	U	D)
				6A	*S= FU	2	=	J04	D-

R	51.88	56.98	THERE IS 5% SANDSTONE FRAGMENTS RANGING UP TO 2 CMS. THERE IS
R	51.88	56.98	A GRADUAL FINING UPWARDS OF THE FRAGMENTS. NEAR THE TOP OF
R	51.88	56.98	THE UNIT, THERE IS A THINLY LAMINATED UNIT OF BRSN.

51.88	52.50	0.62	X	RRPM	502	BD	FU	1	2	1	N	KN6	R	2	BD	U35	R*
				4A	SI	F*	R*	5			0	JM1					

R	51.88	52.50	THERE IS GRADUAL FINING UPWARDS. NEAR THE TOP, IT IS WELL BEDDED
R	51.88	52.50	AND THIS BEDDING SHOWS A FINING UPWARDS. IT REPRESENTS
R	51.88	52.50	A PERIOD OF QUIESCENCES AND SLOW DEPOSITION.

56.98	57.81	0.83	SAND	SN7 BD BS 1 5 3 M	P 2 BD	U40	R)
			RA	SI= FU R* 5			D+

R	56.98	57.81	THE INTERVAL IS VERY COARSE NEAR THE BASE WITH SUBROUNDED TO
R	56.98	57.81	SUBANGULAR CLASTS. IT BECOMES FINER AND HEDDED TOWARDS THE TOP.
R	56.98	57.81	POSSIBLE REPRESENTS A AR SEQUENCE IN A TURBIDITE. SIDERITE IS A
R	56.98	57.81	BROWNISH-YELLOW AND OCCURS INTERSTITIALLY.

7	57.81	63.48	5.57	RIGHT	SP = P * F *	MR7	P	<=	R)
1				5A	*C1	4	KIN1	<)	

1	53.35	66.91	2.62	RRHT	*C* F* H*	LQ4	P	V1	D)
				HA	*VE	KN4		V.	

/ FRG	66.00	71.87	5.87		AES1		BD SS	P	2 BD	30 <*
J					34		= SC			

R	65.00	71.87	LOCALLY REJECTED DUE TO HUMIDITY.
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7	68.30	71.00	2.70	X 4831	510 80 58	R 2 80	65 <*
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K F F R O M - T O - 1 N T RECDV		BL % ROCK TX		TX TX F C % M ARG		RI 1 ID AZM DIP QZ FL CY CA BA XX PY CP GL YY A 1 A 2	
E -L-	---	---	---	---	---	---	---
Y G	R O D	AGE	EV RD	LC	TX TX	S C O O	CHT
							2 ID AZM DIP MG MU CI SD QS HA PR MT SL HA

/	71.00	71.87	0.87	X ARSI	SI1 BD SS	R 2 BD	40 <*
L							

/	71.87	73.15	1.28	BRHT	SI= F* F*	LQ4 P	D*
L				7A	*C2 R*	3 + J04	

/	73.15	76.80	3.65	PRHT	SI1 SS SC	MR8 P	R+
L				4A	SI=	4 LK+	
R	73.15	76.80	THIS UNIT IS MAINLY AN ARSI WHICH HAS BEEN HIGHLY BRECCIATED				
R	73.15	76.80	DUE TO SLUMPING.				

/	76.80	79.22	2.42	BRHT	SA= SS R*	LR6 P	R+
L				5A	*C= F*	4 K01	V*

/	79.22	85.80	6.58	SIL1	SN= BD	0 1 6 G	P 1 BD 25 <)
L				2A CR S17	7		<)

R	79.22	85.80	THE UNIT IS MODERATELY FRACTURED AND BROKEN UP. SLIPPAGE PLANES				
R	79.22	85.80	ARE PARALLEL WITH BEDDING. IT IS LOCALLY CARBONACEOUS.				

/ SHR	79.22	82.40	3.18	X SIL1 GR	SN= BD	0 1 6 G	R 1 BD 25 <)
L							R)
R	79.22	82.40	THE CORE IS HIGHLY FRAGMENTED DUE TO SHEARING.				

/	85.80	86.71	0.91	ARSI	SI= BD SS	P 2 BD	U25 <=
L				6A	SI= SC FU		R+

/	86.71	88.20	1.49	ARSI	SI= LM	P 1 L1	40 <=
L				3A	SI=		R)

R	86.71	88.20	THERE ARE A FEW BANDS OF GRIT AND GRIT RICH LAYERS WITHIN				
R	86.71	88.20	THIS INTERVAL. THEY REPRESENT MINOR PULSES OF COARSER SEDIMENT				
R	86.71	88.20	INFILTR DURING A MAINLY WET PERIOD.				

/	88.20	88.99	0.79	CGPS	SI= R* F* 0 5 2 N	P	U <*
L				7A	*C3 TM G; 6 + 0		<.

R	88.20	88.99	THIS INTERVAL CONTAINS 20-30% MATRIX, WHICH IS MAINLY MUD AND				
R	88.20	88.99	GRIT. THE PEBBLES ARE SUB-ANGULAR TO SUBANGULAR. THERE ARE				
R	88.20	88.99	SEVERAL MINOR SHEAR ZONES. SANDSTONE FRAGMENTS RANGE UP TO 2.5%.				

/	88.99	91.45	2.46	BRHT	*C2 R* F*	MR5 P	<)
L				6A PY	*C=	3 = L03	<)

/	91.45	93.88	2.43	SAND	SI= R* F* 0 4 3 M	P	U <=
L				8A	SI= FU SS 7		D=
R	91.45	93.88	THIS UNIT CONTAINS SEVERAL CYCLES OF A BOUMA SEQUENCE.				
R	91.45	93.88	SOME SHEARING HAS TAKEN PLACE ALONG BEDDING PLANES.				

/	93.88	98.06	0.18	CGPS	*C3 R* F*	LR4 P	<)
L				9A	*C3 G; 7/ 4 +	K05	<)
R	93.88	98.06	GRADES TO SMALL PEBBLES. SEE RANGE -2 TAD CYCLES -END OF 1ST				
R	93.88	98.06	CYCLE AT 95.3 %. SHARP PL. CONTACT AT BASE OF CYCLE.				

7	LSX	124.05	125.43	1.78	LSX SE SX 1 3 LM	P 1	V1	D*	L= L)
1					BA			D)	L) L+

JAS. DR-20-AR-BA STF DEPOSIT, Y.T.
DRILLHOLE/TRAVERSE --- 76-DR011 --- (CONTINUED)

[illegible]

R 124.05 125.83 RECOVERY IS EXTREMELY POOR.

124.05	125.83	1.78	4 ANGLES	LM
			3A	

7	LSX	125.83	130.76	4.93	LSX SF SX CR2 LM	P	V2	D =	L =	L +
					7A			D)		L) L =

L	127.10	130.76	SLUDGE SAMPLES HAVE BEEN COLLECTED OVER THIS INTERVAL AND ARE AVAILABLE IN CORE BOX.
R			
R	127.10	130.76	

LSX	130.76	139.90	9.14	LSX	SX	SF	CH = LM	P	<	D)	L3	L)
				AY						D)	L2	L=

130.76 139.90 THE DWF IS LOCALLY FRAGMENTED. CANNOT PICK CONTACTS DUE TO
130.76 139.90 POOR RECOVERY.

K LM1	139.90	139.90	0.00
-------	--------	--------	------

1	139.90	141.74	1.83	brkt SF	SF1 B* B*	L03	P	<	C.	R+	D
1				7A	*C3	4	+	K14			D+

L 139.90 141.73 THE CORE IS HIGHLY FRAGMENTED WITH POOR RECOVERY. IT IS VERY
R
R 139.90 141.73 MUGGY DUE TO LEACHING.

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G E D L D B

A DMM	SAMPLE	% PB	% ZN	% BA	0Z AG	% CU	% FE	07 AU	% CD	HASH
A LAB	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 R.CLG = BONDAR CLEGG, VANDER VER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WET ANALYSIS.

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	122.83	124.55	7951	1.34	6.25	-0.1	0.07	-0.1	-0.1	-0.1	-0.1	7.16
A 001	124.55	125.88	7952	1.64	5.64	-0.1	0.04	-0.1	-0.1	-0.1	-0.1	4.82
A 001	125.88	128.02	7953	5.66	11.05	-0.1	0.06	-0.1	-0.1	-0.1	-0.1	15.90
A 001	128.02	130.76	7954	1.70	6.51	-0.1	0.02	-0.1	-0.1	-0.1	-0.1	7.53
A 001	130.76	132.28	7955	1.34	3.55	-0.1	0.05	-0.1	-0.1	-0.1	-0.1	4.45
A 001	132.28	133.81	7956	1.30	3.55	-0.1	0.05	-0.1	-0.1	-0.1	-0.1	4.70
A 001	133.81	135.33	7957	0.41	6.61	-0.1	0.06	-0.1	-0.1	-0.1	-0.1	6.58
A 001	135.33	136.86	7958	0.58	7.30	-0.1	0.06	-0.1	-0.1	-0.1	-0.1	7.44
A 001	136.86	138.38	7959	0.76	8.40	-0.1	0.07	-0.1	-0.1	-0.1	-0.1	8.73
A 001	138.38	139.90	7960	0.10	3.13	-0.1	0.05	-0.1	-0.1	-0.1	-0.1	2.78
A CMP	122.83	139.90		1.65	6.17	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	7.22

G E O L O G

A MIN		0.10	3.13	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.63
A MAX	122.63 139.90	5.66	10.68	-0.1	0.07	-0.1	-0.1	-0.1	-0.1	15.91

A HRM
A TYP
A MTHRSD
CM
B-BSP.GR.
SG
WEIGH

A LAB

FLD

FLD

R ASY 0.00 0.00

RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00

ROD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00

ROD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00

AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00

BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00

CC INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00

JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00

OF EACH FIELD.

R ASY 0.00 0.00

B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00

AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00

ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00

BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00

RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00

THE AMTH HEADER.

R ASY 0.00 0.00

THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00

SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 0.00 1.83 00 00

OVERBURDEN

R ASY 0.00 1.83

OVERBURDEN

A 100 1.83 3.35 55 00

OVERBURDEN

A 100 3.35 3.96 30 00

OVERBURDEN

A 100 3.96 5.49 15 00

OVERBURDEN

A 100 5.49 6.09 55 00

OVERBURDEN

A 100 6.09 7.01 46 00

OVERBURDEN

A 100 7.01 7.92 91 09

OVERBURDEN

A 100 7.92 8.23 15 00

OVERBURDEN

A 100 8.23 8.84 61 00

OVERBURDEN

A 100 8.84 9.75 91 18

OVERBURDEN

A 100 9.75 10.67 61 09

OVERBURDEN

A 100 10.67 12.19 152 19

OVERBURDEN

A 100 12.19 13.12 91 22

OVERBURDEN

A 100 13.12 14.32 104 10

OVERBURDEN

A 100 14.32 15.24 70 25

OVERBURDEN

A 100 15.24 15.85 24 00

OVERBURDEN

A 100 15.85 17.07 21 00

OVERBURDEN

A 100 17.07 17.98 67 00

OVERBURDEN

A 100 17.98 19.81 73 00

OVERBURDEN

A 100 19.81 20.43 49 00

OVERBURDEN

A 100 20.43 21.54 85 11

OVERBURDEN

A 100 21.54 21.95 49 10

OVERBURDEN

A 100 21.95 22.56 55 00

OVERBURDEN

A 100 22.56 22.86 30 00

OVERBURDEN

A 100 22.86 23.47 61 00

OVERBURDEN

A 100 23.47 24.38 55 10

OVERBURDEN

A 100 24.38 24.69 31 00

OVERBURDEN

A 100 24.69 24.99 30 00

OVERBURDEN

A 100 24.99 25.60 37 00

OVERBURDEN

A 100 25.60 25.91 31 00

OVERBURDEN

A 100 25.91 26.21 30 12

OVERBURDEN

A 100 26.21 26.52 15 00

OVERBURDEN

A 100 26.52 27.74 40 18

OVERBURDEN

A 100 27.74 29.87 21 41

OVERBURDEN

G E O L O G

A UMS
A TYP
A MTH
A LABRHO
CG
B-R
FLDSP. GR.
SG
WEIGH
FLD

A 100	29.87	31.09	37	09
A 100	31.04	33.53	24	91
A 100	33.53	35.05	152	70
A 100	35.05	37.19	116	09
A 100	37.19	39.01	73	58
A 100	39.01	39.93	82	20
A 100	39.93	41.15	97	00
A 100	41.15	42.67	146	15
A 100	42.67	44.19	149	21
A 100	44.19	47.24	315	67
A 100	47.24	50.59	326	114
A 100	50.59	51.51	88	00
A 100	51.51	52.43	76	17
A 100	52.43	53.64	110	10
A 100	53.64	55.17	153	34
A 100	55.17	56.08	88	09
A 100	56.08	57.51	152	29
A 100	57.51	58.52	79	00
A 100	58.52	64.62	582	141
A 100	64.62	67.67	305	170
A 100	67.67	71.93	347	91
A 100	71.93	73.46	152	33
A 100	73.46	76.20	247	38
A 100	76.20	77.72	152	54
A 100	77.72	84.43	591	45
A 100	84.43	85.95	149	23
A 100	85.95	87.48	152	36
A 100	87.48	90.53	305	234
A 100	90.53	92.05	146	60
A 100	92.05	93.88	137	00
A 100	93.88	95.71	94	00
A 100	95.71	96.93	98	38
A 100	96.93	97.54	52	25
A 100	97.54	99.06	64	36
A 100	99.06	99.97	84	00
A 100	99.97	102.41	85	20
A 100	102.41	103.33	70	00
A 100	103.33	104.24	64	00
A 100	104.24	104.55	12	00
A 100	104.55	105.77	88	25
A 100	105.77	107.29	134	21
A 100	107.29	108.20	67	00
A 100	108.20	109.42	61	00
A 100	109.42	111.56	122	00
A 100	111.56	112.17	46	00
A 100	112.17	113.69	113	16
A 100	113.69	116.43	177	11
A 100	116.43	117.96	104	00
A 100	117.96	119.48	98	00
A 100	119.48	120.79	122	09
A 100	120.79	122.22	152	56

A	TIME				POD	SP. GR.
A	TYP				CM	SG
A	WTH				R-L	WTH
A	LAB				FLD	FLD
A	100	122.22	123.14	35	00	
A	100	123.44	124.05	61	00	
A	100	124.95	125.19	61	00	
A	100	126.19	128.02	06	00	
A	100	128.02	129.54	00	00	
A	100	129.54	130.76	00	00	
A	100	130.76	131.67	21	00	
A	100	131.67	132.57	79	00	
A	100	132.57	133.19	15	00	
A	100	133.19	134.42	21	00	
A	100	134.42	135.94	30	00	
A	100	135.94	136.86	06	00	
A	100	136.86	138.28	91	00	
A	100	138.28	138.99	52	00	
A	100	138.99	139.90	91	00	

G E O L O G F O I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PACIFIC OCEAN OIL LTD.

JASON RE-7N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 76-04012
TOTAL DEPTH/LENGTH : 149.96
CORE/HOLE DIAMETER : 60COLLAR ELEVATION: 1315.91
NORTHING (- IF S): 7002815.00
EASTING (- IF W): 436328.37AZIMUTH(DEG) : 180.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810622
PROJECT NUMBER : J-MAINSER. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	30.48	180.00	-54.00
2	60.96	180.00	-47.00
3	91.44	180.00	-43.00
4	121.92	180.00	-38.00

R HED

ORIGINALLY LOGGED BY DR. K.I.LU: AUG, 1976.

F - I N T E R V A L -		CORE	1- %	TYPT- DAL	TEX-	GRAID	PGT	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC. PLACE)	RECOV-	M H ROCK	RYING MIN	TURES	CHARACS			H H H H H	ANY H	H H H	ANY	ALT ORE
E	A (MT=METRIC FT=FOOTRIC)	ERY	O I	TA TM CAT	TX TX F C % M	ARG	/RI	T ID STK DIP	A A A A A	MIN A	A A A	MIN	- - -
Y	G F R D - I O - I N T (.)	O X TYPE	1 2 3 4 1	1 2 F F C A			1	AZM RT QZ FL CY CA BA XX PY CP GL YY					A 1 A 2
K F		ROCK	FM	RT	TH	Q2 TX TX S C O O CHT		T ID STK DIP	MG MU CL SD QS HA PR MT SL HA				
E L		DUAL	AGE	EN- 0	LC- 3	3 4 0 /		2 AZM RT H H H H H H H H H					1 1
Y G		DESIG	VIR	COL		R C		STRUCTUR-2	A A A A A A A A A A				2 2

/ DVR 0.00 3.65 3.65

OVER

P

/ 3.65 16.76 13.11

ARGL 5 S4+ (L BM

P 2 80 D48

/ 16.76 23.32 6.56

BRPM 6 SF DB 2 2 5 0 MP1

P V) B.

/ 23.32 49.58 26.26

BRHT 5 DB NR3 2 5 C NO1

P V* V. B.

/ 49.58 59.14 9.56

SAND 7 BD FU 4 4 4

P 4 80 D42 V1 V- V-

/ 52.90 54.60 1.70

Y SAND 7 BD FU 4 4 4

R 4 80 D42 V8 V- V-

/ 54.60 59.14 4.54

3 ARSI 6 LF (L (F

R

/ 59.14 61.21 2.07

BRPM 4 S43 6S G; NO3 FU 2 0 MN2

P V(V(

R 59.14 61.21 RAUMA SEQUENCES FROM 16.76 TO 63.39 ARE ABC, ABCE AND AB.

/ 61.21 63.39 2.18

SAND 6 MX 4 4 4

P V6 V(

L

FD

V(

[illegible]

Z	65.59	107.89	44.50	APGL	SF	SN2	LR	LM	1	1	1	P	BD	30	V(D)
L				4		SI1	(L	BN								V=	
Z	70.94	71.31	0.37	2	FAUL			GG5				R					
L								SF									
Z	87.70	89.00	1.30	8	FAUL							R					
Z	107.89	125.88	17.99		RRHT			BS			DR3	P		V(V(
L				5					2		C MN2						
R	111.21	112.81		DADA-A SEED LICES ARE ALSO, AB, A.													
Z	0.00	0.00	0.00	X	SAND			62	4	4		R					
L				6													
Z	112.81	114.87	2.26	X	APGL	CR		LM	1	1	1	R	BD	22	V)	L)	L(
L				4				SI1									
Z	121.40	121.60	0.26	X	SAND				4	4	4	R	BD	37			
L				6													
K DM1	125.88	125.88	0.00														
Z LSA	125.38	145.59	19.81		SOLF	BA		LM	2	2	2	P	0 BD	D66	L1	L5	L= L) 48
L				7		SF	SI1						1				L=
Z	141.52	144.26	2.74	X	BRPD	BA		DR			OP1	R		V)		D.	
L				5			SI1		2		0 NO6						
K LM1	145.69	145.69	0.00														
Z	145.69	149.95	4.27		RRHT			SN2			OP3	P					
L				5		SF			2	5	C MN2						

RYAN

A URM	SAMPLE				Z PR	Z 7N	Z BA	OZ AG	% CU	% FE	OZ AU	% CO	HASH
A LAB	SERIAL				B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP					H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					GA	GA	GA	GA	GA	GA	GA	GA	
R ASY	0.00	0.00	B.CLG = BODDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	GA = NET ANALYSIS.										
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01										
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1										
A 001	124.55	125.85	153	4554	0.01	0.04	4.20	0.04	-0.1	-0.1	-0.1	-0.1	3.89
A 001	125.88	126.49	061	4555	0.76	6.28	38.10	0.08	-0.1	-0.1	-0.1	-0.1	44.82
A 001	126.09	128.02	153	4556	0.33	7.16	38.81	0.02	-0.1	-0.1	-0.1	-0.1	45.92
A 001	128.02	129.54	152	4557	0.22	5.66	46.84	-0.01	-0.1	-0.1	-0.1	-0.1	52.31
A 001	129.54	131.06	152	4558	0.68	3.20	48.30	-0.01	-0.1	-0.1	-0.1	-0.1	51.77
A 001	131.06	132.59	153	4559	1.10	3.22	44.22	-0.01	-0.1	-0.1	-0.1	-0.1	48.13
A 001	132.59	134.11	152	4560	0.81	0.36	44.70	-0.01	-0.1	-0.1	-0.1	-0.1	49.46
A 001	134.11	135.64	153	4561	0.77	2.80	45.80	-0.01	-0.1	-0.1	-0.1	-0.1	48.96
A 001	135.64	137.16	152	4562	0.83	3.12	46.16	-0.01	-0.1	-0.1	-0.1	-0.1	49.70
A 001	137.16	138.68	152	4563	0.76	3.06	38.60	-0.01	-0.1	-0.1	-0.1	-0.1	42.01
A 001	138.68	140.21	153	4564	1.12	3.80	40.00	0.01	-0.1	-0.1	-0.1	-0.1	44.53
A 001	140.21	141.73	152	4565	0.29	5.90	42.50	0.02	-0.1	-0.1	-0.1	-0.1	46.31
A 001	141.73	143.26	153	4566	0.07	0.12	0.56	0.02	-0.1	-0.1	-0.1	-0.1	0.37
A 001	143.26	144.78	152	4567	1.56	4.76	18.89	0.05	-0.1	-0.1	-0.1	-0.1	24.86
A 001	144.78	145.84	091	4568	3.50	7.08	11.40	0.12	-0.1	-0.1	-0.1	-0.1	21.70
A 001	145.84	147.22	153	4569	0.25	1.02	0.58	0.02	-0.1	-0.1	-0.1	-0.1	1.47
A 001	147.22	148.74	152	4570	0.22	1.72	2.59	0.03	-0.1	-0.1	-0.1	-0.1	4.16
A MAX	124.55	148.74			3.50	7.16	48.50	0.01	-0.1	-0.1	-0.1	-0.1	58.57

A MIN				0.01	0.04	0.56	-0.01	-0.1	-0.1	-0.1	-0.1	-0.1	0.20
A CMP	125.68	128.02	214	0.45	6.91	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	6.76
A CMP	128.02	143.26	1520	0.07	3.92	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.39
A CMP	143.26	145.69	243	2.29	5.63	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	7.32
A CMP	145.69	148.74	305	0.24	1.37	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.01

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6B02

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

F - I D T E R V A L -										CORR		T - %		TYPT= DUAL		TEX=		GRAIN		PGI		STRUCTUR-1		ALTERATION		MINS		ORE-TYPE		MINS		SUMMARY		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK		
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T		
Y	G	F	R	O	R	-	T	O	-	I	N	T	(.)	O	X	T	Y	P	1	2	3	4	5	6	7	8	9	0	1	2		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK		
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T		
Y	G	F	R	O	R	-	T	O	-	I	N	T	(.)	O	X	T	Y	P	1	2	3	4	5	6	7	8	9	0	1	2		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	
Y	G	F	R	O	R	-	T	O	-	I	N	T	(.)	O	X	T	Y	P	1	2	3	4	5	6	7	8	9	0	1	2		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	
Y	G	F	R	O	R	-	T	O	-	I	N	T	(.)	O	X	T	Y	P	1	2	3	4	5	6	7	8	9	0	1	2		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	
Y	G	F	R	O	R	-	T	O	-	I	N	T	(.)	O	X	T	Y	P	1	2	3	4	5	6	7	8	9	0	1	2		
K	F	L	(UNITS =	DEC. PLACE)	RECHV-	C	R	R	R	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK	CK
E	A	(MT=METRIC	FT=FOOTRIC)	ERY	O	I	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	T	
Y	G	F	R	O	R	-																												

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R SVY      0.00      0.00      NO DOME HOLE SURVEY DATA.

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R ASY 0.00 0.00 NO ASSAY DATA THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PACIFIC OIL LTD.

JASUR PR-79-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 76-08014

COLLAR ELEVATION: 1194.05

AZIMUTH(DEG) : 0.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 102.11

NORTHING(= IF S): 7902474.00

VERTICAL ANGLE : -53.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 80

EASTING (= IF N): 436914.56

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-MAIN

SEC. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	30.08	0.00	-47.00
2	60.96	0.00	-42.50
3	91.44	0.00	-39.50

F - L I N E I N T E R V A L -		CORE	T- %	TYP- GAL	TEX- GRAIN	PGI	STRUCTUR-1 ALTERATION MINS										ORE-TYPE MINS				SUMMARY											
K	L (UNITS = DEC. PLACE)	RECHV-	M B	ROCK	FLYING MIN	TURES	CHARACS																									
F A	(GT=METRIC FT=FOOTRIC)	ERY	U I		IN IN	SAT	TX TX	F C	%	N	ARG	/RI	T ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-			
Y G	F R O I - T O - J N T (.)	P X	TYPE	1	2	QMI	1	2	F F	C A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
K F		ROCK	FM	RT	16	QMI	TX TX	S C	0	0	CHT	T ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA								
E L		UAL	AGE	EN- 0	LC- 3		3	4	0	/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1						
Y G		DESIG	MIR	CUL			R	C				STRUCTUR-2										A	A	A	A	A	A	A	A	A	2	2

R SVY 0.00 0.00 DIP TESTS ONLY.

/ 0.00 71.63 71.63 MISS P

K UMI 71.63 71.63 0.00

/ 71.63 81.99 10.36 MISS P

K LMI 81.99 81.99 0.00

/ 81.99 102.11 20.12 MISS P

A DMB			SAMPLE	% PB	% ZV	% HA	OZ AG	% CU	% FE	OZ AU	% CD	HASH	
A LAB			SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		
A TYP			NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH				WA	WA	WA	WA	WA	WA	WA	WA		
R ASY	0.00	0.00	B.CLG = BORDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	PA = PET ANALYSIS.										
R ASY	0.00	0.10	LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01, -0.05										
R ASY	0.00	0.00	AD ASSAY INFORMATION ENTERED AS -0.1										
A 001	71.63	73.13	05	4571S	2.22	9.52	0.34	0.10	-0.1	-0.1	-0.1	0.02	11.90
R ASY	71.63	73.13	4571S IS A SLUDGE SAMPLE ASSAY.										
A 001	73.13	74.63	24	4572	0.67	4.24	0.18	0.08	-0.1	-0.1	-0.1	0.01	4.88
A 001	74.63	76.20	12	4575	0.26	1.83	0.11	0.10	-0.1	-0.1	-0.1	-0.01	1.99
A 001	76.20	77.72	116	10534	3.36	8.64	0.09	0.09	-0.1	-0.1	-0.1	0.01	11.89
A 001	77.72	78.94	85	10535	2.46	8.16	0.14	0.13	-0.1	-0.1	-0.1	0.01	10.60
A 001	78.94	80.44	107	10536	0.35	3.34	0.18	0.06	-0.1	-0.1	-0.1	-0.01	3.62
A 001	80.44	81.94	122	10537	0.17	6.16	0.28	0.06	-0.1	-0.1	-0.1	0.01	6.38
A 001	81.99	83.51	61	19325	0.05	0.37	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.18
A 001	83.51	85.03	43	19326	-0.05	-0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.70
A CMP	71.63	81.99			1.32	7.03	-0.1	0.10	-0.1	-0.1	-0.1	-0.1	7.95
R ASY	71.63	81.99	COMPOSITE USES WEIGHTED CORE + SLUDGE VALUES.										

A MIN		-0.05	-0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.70
A MAX	71.55 85.05	3.56	8.64	0.28	0.13	-0.1	-0.1	-0.1	0.01	12.21

100% BY BPF

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASPER PP-79-AG-6A STE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 76-09015
TOTAL DEPTH/LENGTH : 157.28
CORE/HOLE DIAMETER : 60

COLLAR ELEVATION: 1158.09
NORTHING (- IF S): 7002393.00
EASTING (- IF E): 437109.00

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AZIMUTH( DEG ) :      0.00
VERTICAL ANGLE  :     -50.00
CO-ORD SYSTEM   :      UTM

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GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEC. 40 OF
SURVEY DATA

LENGTH FROM COLLAR
TO SURVEY POINT

AZIMUTH
(DEG)

VERT. ANGLE
(DEG)

1	30.48	0.00	-51.00
2	60.96	0.00	-41.00
3	91.44	0.00	-33.50
4	121.92	0.00	-31.50
5	152.40	0.00	-27.00

INTERVAL - CORP										T- %		TYPT- DIAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION		MINS		ORE-TYPE		MINS		SUMMARY	
L (UNITS = DEC.PLACE) RECOV- R M ROCK										FLYING MIN		TUBES		CHARACS						H H H H H		ANY H H H ANY		ALT ORE					
F A (MT=METRIC FT=FOOTRIC) FRY- D I										IN TM		MAT TX TX		F C % M ARG		/RI		T ID STK DIP		A A A A A		MIN A A A MIN		- - - -					
Y G F R D M - I - I M T (.) D X TYPE										1 2		DRI 1 2		F F C A		1		AZM RT QZ FL CY CA BA XX PY CP GL YY		A 1 A 2									
-----										---		---		---		---		---		---		---		---		---			
K F ROCK FG RI										IN RY2		TX TX		S C O O CHT		T ID STK DIP		MG MU CL SD OS		HA PR MT SL		HA							
F L GUAL AGE ES- N LC- 3										3 4		D		/		2		AZM RT H H H H H		H H H H H		1 1							
Y G BESTG VIR CBI										P		C		STRUCTUR-2		A A A A A		A A A A A		2 2									

R SVY 0.00 0.00 ACID DIP TESTS ONLY.

/	0.00	130.61	150.61	MISS
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K 1041	130.61	130.61	0.00
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1	130.61	131.98	1.37	MISS
---	--------	--------	------	------

K 121	131.98	131.98	0.00
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/	131.98	157.28	25.30	MISS
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A UMM	SAMPLE	Z PB	Z ZN	Z BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	
A TYP	CORPER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 R.CLG = BORDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WET ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.05

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001 128.02 130.81 144 10544 0.05 -0.05 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.60

A 001 130.61 130.91 15 10545 -0.05 2.45 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -1.80

A 001 130.91 131.52 31 10546 0.06 0.35 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.19

A 001 131.52 131.93 23 10547 0.05 5.70 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 5.15

A 001 131.93 133.50 36 10548 0.05 0.65 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 0.10

A 001 133.50 135.03 61 10549 0.05 0.65 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 0.10

A 001 135.03 136.55 0 10550 0.23 1.50 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 1.13

R ASY 135.03 136.55 SLUDGE ASSAY ONLY.

A 001 136.55 137.40 78 19301 0.29 1.23 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 0.92

A 001 137.46 139.90 125 19302 0.16 1.78 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 1.34

A 001 139.90 142.65 168 19303 0.10 1.90 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 0.50

A MIN		-0.05	-0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.70
A MAX	128.62 142.65	0.29	5.70	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	5.39

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

FORMAT VERSION : 6B02

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

VERT. ANGLE
(DEG)

F - I N T E R V A L - CORE 1 - % TYPE- QUAL TEXT- GRAIN PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY											
K	L (UNITS = . DEC. PLACE)	RECOV- M D ROCK	FRYING MIN	TURES	CHARACS					H H H H H ANY H H H ANY ALT ORE	
E	A (MI=MEIR(C FT=FOOTRIC)	FRY	0 1	TX TX	TX TX	F C % M ARG	/RI	T ID	STK DIP	A A A A A MIN A A A MIN	- - - -
Y	G F R D - T D - 1 K 1 (.)	D X TYPE	1 2	QMI	1 2	F F C A		1	AZM RT	QZ FL CY CA BA XX PY CP GL YY	A 1 A 2
-	-----	-----	-----	-----	-----	-----	---	-	---	---	- - - -
K	F	ROCK FM RT	FM QMP	TX TX	S C O O	CHT		T ID	STK DIP	MG MU CL SD QS HA PR MT SL HA	
E	L	QUAL AGE EN- N LC- 3		3 4	H	/		2	AZM RT	H H H H H H H H H	1 1
Y	G	DESIG VIR COL			R	C			STRUCTUR-2	A A A A A A A A A A	2 2

p

P

4

1	54.56	122.22	67.66	6158
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A UMM	SAMPLE	% PR	% 7N	% BA	OZ AG	% CU	% FE	OZ AU	% CO	HASH
A LAB	SERIAL	B.CLG	H.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A BTH		AA	NA	NA	NA	NA	NA	NA	NA	

R ASY 0.00 0.00 B.CLG = ROODAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 AA = WFT ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.05

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	45.11	48.45	185	19304	0.05	1.73	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.18
A 001	48.46	49.99	167	19305	0.05	0.85	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.30
A 001	49.99	51.51	82	19306	0.06	3.10	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.56
A 001	51.51	53.34	113	19307	0.05	1.60	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.05
A 001	53.34	54.56	101	19308	0.05	1.45	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.90
A 001	54.56	57.51	235	19309	0.04	0.70	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.14
A 001	57.61	60.66	231	19310	0.05	0.54	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.01
A 001	60.66	62.79	167	19311	-0.05	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.60
A CMP	49.99	54.56	296		0.05	2.06	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.51

A MIN			-0.05	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.61
A MAX	45.11	62.79	0.06	3.10	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.56

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PACIFIC OCEAN OIL LTD.

FORMAT VERSION : 6802

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-RECC

SEQ. NO. OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.50	0.00	-89.00
2	62.50	0.00	-89.00
3	91.40	0.00	-81.00
4	121.90	0.00	-77.00
5	152.40	0.00	-67.00
6	182.90	0.00	-60.00
7	213.40	0.00	-56.50
8	228.60	0.00	-55.50
9	243.80	0.00	-53.50
10	259.10	0.00	-51.00
11	274.30	0.00	-51.00
12	289.60	0.00	-49.00
13	306.30	0.00	-46.00
14	320.00	0.00	-42.50
15	335.60	0.00	-39.50
16	352.30	0.00	-41.50
17	367.90	0.00	-41.00
18	483.10	0.00	-37.50
19	398.40	0.00	-35.50
20	412.70	0.00	-33.50
21	428.20	0.00	-32.50
22	443.20	0.00	-29.00
23	458.70	0.00	-29.00
24	477.00	0.00	-27.00
25	482.80	0.00	-27.00

INTERVAL - CORE										GRAIN										STRUCTUR-1										STRUCTUR-2																			
F L (UNITS = . DEC.PLACE) RECOV- T- %										PGI										ALTERNATION MINS										ORE-TYPE MINS										SUMMARY									
E A (MT=METRIC FT=FOOTRIC) ERY B 1										/RI T ID STK DIP										H H H H H ANY H H H ANY										ALT ORE																			
Y G F R O B - T O - I O T (.) D X TYPE 1 2 QM1 1 2 F F C A										1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2																																							
K F ROCK FB RT TM QM2 TX TX S C O U CHT										T ID STK DIP MG MU CL SD OS HA PR MT SL HA																																							
F L DUAL AGE FN- D IC- 3 3 4 O /										2 AZM RT H H H H H H H H H H										1 1																													
Y G DESIG VIR CUL R C										STRUCTUR-2 A A A A A A A A A A										2 2																													

R SVY 0.00 0.00 DIP TESTS ONLY.

R ASY 0.00 0.00 NO ASSAYS FROM THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASON PB-76-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 76-DH01A	COLLAR ELEVATION: 1389.28	AZIMUTH(DEG) : 180.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 56.69	CORRECTING (- IF S): 7003448.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : NO	EASTING (- IF A): 436403.25	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

F	-	I	N	T	E	R	V	A	L	=		CORR	I-	%		TYPE=	DAL	TEX=	GRAIN		PGI		STRUCTUR-1		ALTERATION MINS		ORE-TYPE MINS	SUMMARY
K	L	(UNITS = . DEC.PLACE)	MEDUV=	M G	PUCK	FXING	MIS	TURES	CHARACS		H H H H H ANY H H H ANY ALT ORE																	
F	A	(MT=METRIC FT=FOOTRIC)	ERY	O I		IM TH	BAT	TX TX F C % M ARG	/PI T JD STK DIP A A A A A MIN A A A MIN - - - -																			
Y	G	F K D N - L G - J A I (.)	O X TYPE	1 2 QD) 1 2 F F C A		1					1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2																	

[illegible]

R SVY 0.00 0.50 NO DRILL HOLE DIP TESTS TAKEN.

R ASY 0.00 0.10 NO CORE ASSAYS TAKEN; SLUDGE ASSAY ALL <0.05 PB AND ZN.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASCO PB-70-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 76-08019	COLLAR ELEVATION: 1388.38	AZIMUTH(DEG) : 0.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 130.45	NORTHING(- IF S): 7003327.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : 60	EASTING (- IF W): 430368.25	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	60.96	0.00	-39.50
2	91.44	0.00	-32.50
3	130.45	0.00	-27.00

F - INTERVAL -		CORE	T- %	TYPT- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																						
X	L (UNITS = . DEC.PLACE)	RECHV-	R	R	ROCK	RYING	MIN	TURES	CHARACS	H	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE													
E	A	(METRIC F=FOOTRIC)	ERY	0	I	TR	TR	AT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F R D H - I D - I N T (.)	0	X	TYPE	1	2	QV1	1	2	F	F	C	A			1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	

K	F		ROCK	FM	RT	TR	QV2	TX	TX	S	C	0	0	CHT			1	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L		QUAL	AGE	FN=	0	LC=	3		3	4	0	/				2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G		DESIG	VIR	COL								C					STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 DIP TESTS ONLY.

R ASY 0.00 0.10 NO SIGNIFICANT ASSAYS IN THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 76-08020

COLLAR ELEVATION: 1253.13

AZIMUTH(DEG) : 0.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 121.92

NORTHING(= IF S): 7002399.00

VERTICAL ANGLE : -49.50

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 86

EASTING (= IF W): 436452.00

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-MAIN

SEQ. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	31.70	0.00	-46.00
2	64.00	0.00	-45.00
3	91.40	0.00	-42.50
4	121.92	0.00	-40.00

F - I N T E R V A L -		CORE	T- %	TYPI=	QAL	TEX=	GRAIN	PGI	STRUCTUR-1 ALTERATION MINS										ORE-TYPE MINS SUMMARY																											
K	L (UNITS = . DEC.PLACE) RECOV=	A	M	ROCK	RYING	MIS	TURES	CHARACS		H	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE																									
E	A (MT=METRIC FT=FOOTRIC) ERY	G	J		TH	IN	NAT	TX	TX	F	C	%	M	ARG	/RT	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-													
Y	G	F	R	O	M	-	I	D	-	I	N	T	(.)	D	X	TYPE	1	2	QM1	1	2	F	F	C	A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
K	F																																													
E	L																																													
Y	G																																													
K	F																																													
E	L																																													
Y	G																																													
R	SVY	0.00	0.00																																											

DIP TESTS ONLY.

A UNM	SAMPLE	% Pb	% Zn	% BR	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAP	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 B.CLG = BUNDAR CLEGG, VACUUMER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WFT ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.05

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	29.00	30.00	96	19347	0.06	0.12	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.42
A 001	30.00	31.00	96	19348	0.07	0.09	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.44
A 001	31.00	32.00	96	19349	0.11	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.44
A 001	32.00	33.00	96	19350	0.10	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.45
A 001	33.00	34.00	96	19351	4.50	-0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.85
A 001	34.00	35.00	96	19352	0.35	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.20

A MIN			0.06	-0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.59
A MAX	29.00	35.00	4.50	0.12	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.02

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASDD PH-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 76ADH009

COLLAR ELEVATION : 1248.92

AZIMUTH(DEG) : 270.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 85.34

NORTHING(= IF S): 7002373.00

VERTICAL ANGLE : -50.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 89MM

EASTING (= IF W): 436509.75

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-RECC

F - I X F E R V A L - CORE T- % TYPE- QAL TFX- GRAIN										PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY									
K L (UNITS = DEC.PLACE)RECUV- W N ROCK FYING MIN TURFS CHARACS										H H H H H ANY H H H ANY ALT ORE									
E A (SI=METRIC FT=FOOTERIC) ERY D T TR IN MAI TX TX F C % M ARG										/RI T ID STK DIP A A A A A MIN A A A MIN - - -									
Y G F R D R - I D - L K T (.) D X TYPE 1 2 QM1 1 2 F F C A										1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2									
K F ROCK FM RT TM QM2 TX TX S C O D CHT										T ID STK DIP MG MU CL SD QS HA PR MT SL HA									
E L QUAL AGE EN- 0 LC- 3 3 0 0 /										2 AZM RT H H H H H H H H H 1 1									
Y G DESIG VIR COL R C										STRUCTUR-2 A A A A A A A A A 2 2									

R SVY 0.00 0.00 NO DOWN HOLE SURVEY DATA.

R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASOR PH-7N-AG-PA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILL HOLE/TRAVERSE : 75AD0013
TOTAL DEPTH/LENGTH : 90.53
CORE/HOLE DIAMETER : 88MMCOLLAR ELEVATION: 1201.10
NORTHING (- IF S): 7002518.00
EASTING (- IF W): 436913.50AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.48	0.00	-51.00
2	60.96	0.00	-50.00

F - J E I E P V A L -		CORE	T- %	TYPI- GAL	TEX- GRAIN	PGT	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K L (UNITS =	DEC. PLACE)	RECLV-	F T	ROCK	FLYING MIN	TURES	CHARACS	H H H H H	ANY	H H H	ANY	ALT ORE
E A (METRIC FT=FOOTRIC)	ERY	D 1		TM TM NAT	TX TX F C % M ARG	/RT T	ID STK DIP	A A A A A	MIN A A A	MIN	- - -	- - -
Y G F W D R - T O - I N T (.)			U X TYPE	1 2 QM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY				A 1 A 2

K F		ROCK	FM	RT	TM QM2	TX TX S C U O CHT	1	ID STK DIP MG MU CL SD QS HA PR MT SL HA				
F L		QUAL	AGE	EN- D	LC- 3	3 4 0 /	2	AZM RT H H H H H H H H H				1 1
Y G		DESIG	VIR	COL		R C		STRUCTUR-2 A A A A A A A A A				2 2

R SVY 0.00 0.00 CO-ORDS ENTERED ON LOGGING SHEET ARE WRONG. SURVEY TABLE USED.

/ 0.00 17.68 17.68 MISS P

K DM1 17.68 17.68 0.00

/ 17.68 22.25 4.57 MISS P

K LM1 22.25 22.25 0.00

/ 22.25 90.53 68.28 MISS P

A URM	SAMPLE	% PC	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 B.CLG = BODAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WFT ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -0.1. E.G. -0.05

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	17.66	20.42	21	19327	0.22	6.45	0.71	0.02	-0.1	-0.1	-0.1	0.01	7.11
A 001	20.42	21.64	31	19328	0.58	8.05	1.75	0.04	-0.1	-0.1	-0.1	0.01	10.13
A 001	21.64	22.25	03	19329	0.14	5.50	0.36	0.04	-0.1	-0.1	-0.1	0.01	5.75
A 001	22.25	23.77	03	19330	-0.05	0.18	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.47
R ASY	0.00	0.00		SLUDGE ASSAYS NOT ENTERED.									
A CMP	17.66	22.25	55		0.31	6.75	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	6.46

A MIN			-0.05	0.18	-0.1	-0.1	-0.1	-0.1	-0.1	-0.47
A MAX	17.08	25.77	0.58	8.05	1.75	0.04	-0.1	-0.1	-0.1	10.13

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASOP PA-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 77-DH021	COLLAR ELEVATION: 1193.10	AZIMUTH(DEG) : 1.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 171.91	NORTHING(= IF S): 7062455.00	VERTICAL ANGLE : -71.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : 80	EASTING (= IF W): 436916.44	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	15.24	10.25	-70.50
2	30.48	10.25	-69.50
3	60.96	16.25	-68.00
4	76.20	19.25	-67.50
5	91.44	19.25	-67.00
6	106.88	22.00	-65.50
7	121.92	24.75	-64.50
8	137.16	25.25	-64.50
9	152.40	26.75	-64.50
10	167.64	27.25	-64.00

F	=	I	=	I	F	R	V	A	L	=	CORE	1	=	Z	TYPE	=	QUAL	TEX	=	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY											
K	I	(DITS =	.	DEC.PLACE)	RECDV	=	R	M	ROCK	RYING	MIN	TURES	CHARACS									H	H	H	H	H	ANY	H	H	ANY	ALT	ORE						
E	A	(MT=METRIC	FT=FOOTRIC)	ERY																	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-
Y	G	F	R	O	M	=	T	O	=	I	G	I	(.)	D	X	TYPE	1	2	QMI	1	2	F	F	C	A											
K	F																																					
E	L																																					
Y	G																																					

R SVY 0.00 0.00 ALL SPEERY SUD SURVEY DATA.

/ 0.00 125.36 125.36 MISS P

K DM1 125.36 125.36 0.00

/ 125.36 147.83 22.07 MISS P

K LM1 147.83 147.83 0.00

/ 147.83 171.91 20.00 MISS P

G E O L O G

A U4M	SAMPLE	% PR	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 B.CLG = BODDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WFT ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -0.1. E.G. -0.01

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	122.32	125.36	207	6002	0.02	0.07	1.12	0.03	-0.1	-0.1	-0.1	-0.01	0.93
A 001	125.36	125.91	33	6003	1.18	4.13	0.03	0.09	-0.1	-0.1	-0.1	0.01	5.14
A 001	125.91	126.34	16	6004	1.75	7.15	0.02	0.09	-0.1	-0.1	-0.1	0.02	8.73
A 001	126.34	127.53	46	6005	0.30	3.90	0.10	0.03	-0.1	-0.1	-0.1	0.01	3.64
A 001	127.53	128.47	71	6006	1.50	6.65	0.02	0.06	-0.1	-0.1	-0.1	0.02	8.15
A 001	128.47	128.93	24	6007	0.02	0.88	0.02	0.04	-0.1	-0.1	-0.1	-0.01	0.65
A 001	128.93	129.42	26	6008	1.98	6.45	0.02	0.10	-0.1	-0.1	-0.1	0.02	8.27
A 001	129.42	129.84	17	6009	1.23	7.45	-0.01	0.08	-0.1	-0.1	-0.1	0.02	8.47
A 001	129.84	130.15	9	6010	0.46	4.55	-0.01	0.05	-0.1	-0.1	-0.1	0.01	4.76
A 001	130.15	130.97	25	6011	2.80	9.10	-0.01	0.07	-0.1	-0.1	-0.1	0.02	11.68
A 001	130.97	131.92	54	6012	4.80	16.80	-0.01	0.14	-0.1	-0.1	-0.1	0.04	21.47
A 001	131.92	132.28	26	6013	2.90	10.10	-0.01	0.08	-0.1	-0.1	-0.1	0.02	12.79
A 001	132.28	133.81	124	6014	2.47	11.80	0.01	0.02	-0.1	-0.1	-0.1	0.02	14.02
A 001	133.81	135.58	155	6015	2.26	12.70	0.02	0.04	-0.1	-0.1	-0.1	0.02	14.74
A 001	135.58	136.40	72	6016	3.23	18.10	0.01	0.06	-0.1	-0.1	-0.1	0.03	21.13
A 001	136.40	137.59	105	6017	2.25	11.00	0.03	0.03	-0.1	-0.1	-0.1	0.02	13.03
A 001	137.59	138.38	71	6018	1.92	7.21	-0.01	0.04	-0.1	-0.1	-0.1	0.01	8.87
A 001	138.38	139.39	95	6019	1.75	7.65	-0.01	0.04	-0.1	-0.1	-0.1	0.01	9.14
A 001	139.39	139.75	36	6020	2.15	6.10	0.02	0.04	-0.1	-0.1	-0.1	0.01	8.02
A 001	139.75	140.51	76	6021	0.93	5.34	-0.01	0.02	-0.1	-0.1	-0.1	0.01	5.99
A 001	140.51	140.90	39	6022	0.47	4.38	0.01	0.04	-0.1	-0.1	-0.1	0.01	4.61
A 001	140.90	142.04	114	6023	3.33	13.90	0.03	0.06	-0.1	-0.1	-0.1	0.01	17.08
A 001	142.04	142.52	48	6024	2.40	13.70	0.01	0.09	-0.1	-0.1	-0.1	0.01	15.91
A 001	142.52	143.16	60	6025	2.05	8.80	8.36	0.03	-0.1	-0.1	-0.1	0.01	18.95
A 001	143.16	143.96	80	6026	1.53	5.20	42.80	0.03	-0.1	-0.1	-0.1	0.01	49.27
A 001	143.96	145.48	136	6027	2.10	13.40	0.86	0.07	-0.1	-0.1	-0.1	0.01	16.14
A 001	145.48	146.04	32	6028	0.61	6.40	4.08	0.08	-0.1	-0.1	-0.1	-0.01	10.86
A 001	146.04	147.22	56	6029	0.54	9.30	0.03	0.08	-0.1	-0.1	-0.1	0.01	9.66
A 001	147.22	147.83	34	6030	0.11	3.09	2.87	0.06	-0.1	-0.1	-0.1	-0.01	5.82
R ASY	125.36	147.83			MAIN ORE ZONE INTERVAL.								
A 001	147.83	150.88	277	6031	0.05	1.28	2.42	0.06	-0.1	-0.1	-0.1	-0.01	3.50
A 001	150.88	153.47	225	6032	0.08	2.65	0.32	0.05	-0.1	-0.1	-0.1	-0.01	2.79
A 001	153.47	154.08	56	6033	0.27	8.00	0.43	0.10	-0.1	-0.1	-0.1	-0.01	8.49
A 001	154.08	154.53	41	6034	0.04	0.62	0.43	0.06	-0.1	-0.1	-0.1	-0.01	0.84
A 001	154.53	154.84	30	6035	0.31	5.10	0.60	0.15	-0.1	-0.1	-0.1	0.01	5.87
A 001	154.84	157.87	290	6036	0.04	0.85	1.00	0.11	-0.1	-0.1	-0.1	-0.01	1.69

G E O L O G

PAN OCEAN OIL LTD.

JASUR PU-7N-AG-BA STF DEPOSIT, Y.T.
DRILLHOLE/TRAVERSE --- 77-DH021 --- (CONTINUED)

PAGE - 3

A MIN		0.02	0.07	-0.01	0.02	-0.1	-0.1	-0.1	-0.01	-0.21
A MAX	122.52 157.87	4.89	18.10	42.80	0.15	-0.1	-0.1	-0.1	0.04	65.59

REVISION BY DATE

G E O L O G I C A L L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRaverse : 77-04022

COLLAR ELEVATION: 1275.69

AZIMUTH(DEG) : 0.00

GEOLOGGED BY : HDG +

TOTAL DEPTH/LENGTH : 263.96

NORTHING (- IF S): 7002545.00

VERTICAL ANGLE : -72.00

DATE (YY/MM/DD): 810726

CORE/HOLE DIAMETER : 80

EASTING (- IF W): 436651.62

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-MAIN

SEP. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	15.24	358.75	-75.00
2	30.48	359.25	-75.00
3	45.72	359.25	-72.00
4	76.20	5.25	-71.00
5	106.68	12.25	-69.75
6	137.16	17.25	-68.25
7	167.64	18.25	-67.00
8	198.12	21.75	-66.00

F	-	I	N	T	E	R	V	A	L	-	CORE	T	-	%	TYPI	-	NAL	TEX	-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY	
K	L	(UNITS	=	.	DEC.	PLACE)	RECUV-			R	M	ROCK	FRYING	MIN	TURES	CHARACS											
F	A	(MT=METRIC	FI=FOOTRIC)	FRY																							
Y	G	F	R	O	E	-	T	O	-	I	N	T	(.)	O	X	TYPE	1	2	Q	1	2	F	F	C	A	
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
K	F							ROCK	FR		RI		IN	Q	2	TX	TX	S	C	O	O	CHT						
F	L							DUAL	AGE	EN	-	O	LC	-	3		3	4	O		/							
Y	G							DESIG		VIR		COL																

R SVY 0.00 0.00 ALL SURVEYS WERE DONE WITH SPERRY-SUN EQUIPMENT.

/ DVB 0.00 4.33 4.53 OVER P

/ CON 4.33 20.60 16.27 ARST SC LM 1 3 = 3 P I LM 57 L*

L 3 2

R 4.53 20.60 SAND BANDS ARE PYRITIC, INCREASING TO 10% NEAR THE BASE OF THE

R 4.53 20.60 UNIT.

/ CON 20.60 25.90 5.30 ARHT L07 P

L 3 3 KN1 **

R 20.60 25.90 PYRITE IS PRIMARILY FOUND AS A REPLACEMENT MINERAL IN CHERT

R 20.60 25.90 FRAGMENTS.

/ CON 25.90 29.18 3.28 ARHT LP4 P

L 3 3 LM2 D*

R 29.18 34.45 5.27 CGRR SN2 G: M02 P V) D*

R 29.18 34.45 SMALL SAND SIZED ANGULAR CHERT FRAGMENTS, OCCUR INTERSTITIALLY

R 29.18 34.45 TO LARGER CHERT AND ARGILLITE FRAGMENTS.

/ 29.18 30.78 1.60 7 SAND G: RD 1 3 7 5 R 2 RD U52 >= D*

L 7 8 C

/	123.45	120.15	2.80	BRBT	MP4	P	★)
L				4	3	LN2	

090986

K	M/D	179.83	179.85	0.00																
Z		179.83	180.10	0.27	K SAND	SP6 RD	1 3 6 3	R 2 BD	55											L+
L					5	SI3	7													
R		179.83	180.10		SMALL DISSEMINATED PYRITIC EHDHEDRAL CRYSTALS CONCENTRATE IN															
R		179.83	180.10		SANDSTONE BEDS.															
Z	CON	181.30	184.74	3.44	SILT CR	RD //	1 2 7 5	P 2 BD	57											L+
L					3		8													
Z		181.30	182.29	0.99	R SAND	RD G:		R 2 BD	060											D+
L						LC														
Z	CON	184.74	190.20	5.46	BRHT CR			LN6 P												B+
L					3		5	KN1												
R		184.74	190.20		THE ARGILLIC CLASSIFICATION FOR BRECCIA SIZE AND PERCENT IS															
R		184.74	190.20		USED TO DESCRIBE THE SILTSTONE CLASTS.															
Z	CON	190.20	194.10	3.90	SILT CR	MX	1 2 8 4	P	053 <)											D+
L					2		6													<)
Z	CON	194.10	201.76	7.66	BRHT CR	SK		KM1 P	FO	53 <)										
L					6			KM2												<)
R		194.10	201.76		THIS UNIT IS POORLY CONSOLIDATED INDICATING THE POSSIBILITY OF															
R		194.10	201.76		A FAULT. QUARTZ AND SPHALERITE STOCKWORK VEINING IS PREVALENT.															
Z	CON	201.76	202.39	0.63	BRHT	BR		JM2 P												D=
L					CY 7		3	KL1												B=
R		201.76	202.39		THIS IS A TRANSITIONAL ZONE BEFORE THE ORE ZONE WHICH CONTAINS															
R		201.76	202.39		SILICIFIED FRAGMENTS IN A CLAY MATRIX.															
K	UMI	201.78	201.78	0.00																
Z	FSX	202.39	203.91	1.52	FGSX SF	CH4		P	M4											#+
L					8															#=
Z	LSX	203.91	204.52	0.61	LMSX SF		LC LM	P 1 LM	54											L=
L					9															L2
Z	LSX	204.52	206.04	1.52	LMSX SF		LC LM	P 1 LM	54 L6											L1
L					7		BR													L3
R		204.52	206.04		THIS INTERVAL CONTAINS BRECCIATED, SILICIFIED ARGILLIC FRAGMENTS															
Z	LSX	206.04	207.36	1.32	LMSX SF		LC LM	P 1	L4											L1
L					6 CR															L3 L3
R		206.04	207.36		A HIGHLY DISTORTED INTERVAL WHICH CONTAINS SILICIFIED,															
R		206.04	207.36		BRECCIATED, ARGILLIC FRAGMENTS.															
Z	LSX	207.36	209.70	2.34	LMSX SF															

[illegible]

/	208.79	209.70	0.91	X LMSX SF	LC LM	P 1 LM	65 L6	LC	B2	L=		
L				8	9D					L2		
/	CON	209.70	215.04	5.34	SILT	S15 LM	1 2 5 2	P 3 LM	60 L2	L1	L+	
L				4	LC						L2	
R		209.70	215.04	SILTSTONE BEDS RANGE FROM 0.2 CM TO 10 CM IN THICKNESS.								
/		210.52	213.36	2.84	X SILT	S15 LM	1 2 5 2	R 3 LM	64 L2	L1	L+	
L												
/		213.36	215.04	1.68	X SILT	S15 LM	1 2 5 2	R 3 LM	59 L2	L1	L+	
L												
/	LSX	215.04	216.10	1.06	LMSX SF	LC LM		P 1 LM	60 L5	L1	L)	
L					2	BR					L3	
R		215.04	216.10	TWO LAYERS OF ARGILLITE OF 3 CM THICK ARE PRESENT. MILD								
R		215.04	216.10	BRECCIATION OF THESE LAYERS IS STILL OBSERVED.								
/	LSX	216.10	218.02	1.92	LMSX SF	LC LM		P 1 LM	68 L5	LC	B1	L1
L					8							L4
/		216.65	217.02	0.37	X LMSX SF	LC LM		R 1 LM	68 L5	LC	B1	L1
L					8							Q2 L2
R		216.65	217.02	BEDS ARE HIGHLY CONTORTED WITH PATCHES OF MARCASITE AND								
R		216.65	217.02	SILTSTONE INTERMIXED.								
/		217.02	218.02	1.00	X LMSX SF	X8 LM		R 1 LM	68 L5	LC	L1	L1
L												L4
R		217.02	218.02	END OF ORE ZONE.								
X	LM1	218.02	218.02	0.00								
/	CON	218.02	220.80	2.78	ARGL CR	9X	0 1 1 1	P 2 FO	66		B+	
L					3		9					
/	CON	220.80	233.90	13.10	CGGR		MP2	P		V+		D+
L					5		4	C L04				
R		220.80	233.90	THIS INTERVAL CONTAINS A PYRITIC BOULDER WITH QUARTZ VEINING.								
/		228.71	229.10	0.39	X CGGR PY		MP2	R		V=		#=
L												
R		228.71	229.10	A HIGHLY PYRITIZED MATRIX IS PROBABLY ASSOCIATED WITH AN								
R		228.71	229.10	INCREASE IN QUARTZ VEINING.								
/	CON	233.10	233.90	0.80	9 SAND PY	S67	1 3 7 5	R			B+	
L					4		6					
R		233.10	233.90	RIP-UP CLASTS ARE EMBEDDED WITHIN THE SANDSTONE BEDS.								
/	CON	233.90	263.96	30.06	ARGL CR	SN+ RD //	0 3 + 3	P 1	63		L=	
L					2							

R	260.03	260.13	PYRITIC RINGS OCCUR WITHIN THE ARGILLITE.
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A URM				SAMPLE	% PB	% Zn	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BUNDAK CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		BA = WFT ANALYSIS.									
R ASY	0.00	0.00		501 ASSAY INFORMATION ENTERED AS -0.1									
A 001	168.55	170.34	107	6128	0.02	0.06	0.68	-0.1	-0.1	-0.1	-0.1	-0.1	0.26
A 001	170.08	170.99	73	6129	0.01	0.04	0.46	-0.1	-0.1	-0.1	-0.1	-0.1	0.01
A 001	170.99	172.52	140	6130	0.02	0.03	0.95	-0.1	-0.1	-0.1	-0.1	-0.1	0.50
A 001	186.98	190.50	152	6037	0.04	0.80	0.02	-0.1	-0.1	-0.1	-0.1	-0.1	0.36
A 001	190.50	192.02	119	6038	0.06	0.90	0.06	-0.1	-0.1	-0.1	-0.1	-0.1	0.52
A 001	192.02	193.55	142	6039	0.06	0.28	0.07	-0.1	-0.1	-0.1	-0.1	-0.1	-0.09
A 001	193.55	195.07	152	6040	0.48	3.15	0.01	-0.1	-0.1	-0.1	-0.1	-0.1	3.14
A 001	195.07	196.60	153	6041	0.40	2.23	0.03	-0.1	-0.1	-0.1	-0.1	-0.1	2.16
A 001	196.60	198.12	152	6042	0.11	0.74	0.01	-0.1	-0.1	-0.1	-0.1	-0.1	0.36
A 001	198.12	199.64	152	6043	0.23	1.55	0.01	-0.1	-0.1	-0.1	-0.1	-0.1	1.29
A 001	199.64	201.17	153	6044	0.28	2.40	0.01	-0.1	-0.1	-0.1	-0.1	-0.1	2.19
A 001	201.17	201.78	61	6045	0.16	1.25	0.03	-0.1	-0.1	-0.1	-0.1	-0.1	0.94
A 001	201.78	202.39	61	6046	0.84	3.10	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	3.49
A 001	202.39	203.91	152	6047	1.05	2.30	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	2.90
A 001	203.91	204.52	61	6048	3.00	17.50	0.05	0.11	-0.1	-0.1	-0.1	-0.1	20.26
A 001	204.52	206.04	152	6049	5.10	19.30	0.03	0.99	-0.1	-0.1	-0.1	-0.1	25.02
A 001	206.04	207.36	103	6050	4.10	14.40	0.04	0.29	-0.1	-0.1	0.01	-0.1	18.54
A 001	207.36	208.79	130	6051	2.10	8.50	0.02	0.04	-0.1	-0.1	-0.1	-0.1	10.26
A 001	208.79	209.70	91	6152	0.98	13.40	0.10	-0.1	-0.1	-0.1	-0.1	-0.1	13.98
A 001	209.70	211.53	183	6053	0.76	10.00	0.09	-0.1	-0.1	-0.1	-0.1	-0.1	10.35
A 001	211.53	213.36	183	6054	0.42	5.00	0.07	-0.1	-0.1	-0.1	-0.1	-0.1	4.99
A 001	213.36	215.04	145	6055	0.25	8.00	0.08	-0.1	-0.1	-0.1	-0.1	-0.1	7.83
A 001	215.04	216.10	106	6056	0.62	15.15	0.07	-0.1	-0.1	-0.1	-0.1	-0.1	15.34
A 001	216.10	216.65	55	6057	0.82	20.40	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	20.76
A 001	216.65	217.02	37	6058	0.82	10.30	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	10.66
A 001	217.02	218.02	98	6059	0.67	18.80	0.03	-0.1	-0.1	-0.1	-0.1	-0.1	19.00
A 001	218.02	219.46	138	6060	0.06	0.51	0.03	-0.1	-0.1	-0.1	-0.1	-0.1	0.10
A 001	224.94	225.86	88	6061	0.02	0.10	0.15	-0.1	-0.1	-0.1	-0.1	-0.1	-0.23
A 001	225.86	226.77	84	6062	0.02	0.04	0.25	-0.1	-0.1	-0.1	-0.1	-0.1	-0.19
A 001	226.77	227.69	90	6063	0.02	0.08	0.26	-0.1	-0.1	-0.1	-0.1	-0.1	-0.14
A 001	235.61	237.28	107	6131	0.02	0.03	0.78	-0.1	-0.1	-0.1	-0.1	-0.1	0.33
A 001	237.28	238.05	49	6132	0.02	0.03	0.62	-0.1	-0.1	-0.1	-0.1	-0.1	0.17
A 001	238.05	238.20	15	6133	1.08	5.95	0.22	-0.1	-0.1	-0.1	-0.1	-0.1	6.75
A 001	238.20	239.73	138	6134	0.02	0.05	0.75	-0.1	-0.1	-0.1	-0.1	-0.1	0.32
A CMP	203.91	218.02	1350		1.67	12.35	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	13.42

A MIN		0.01	0.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.56
A MAX	168.55 239.73	5.10	20.40	0.78	0.99	-0.1	-0.1	-0.1	-0.1	26.87

DRILL BY BGF

K	F	F	K	D	K	-	I	D	-	I	N	T	RECDV	ND	%	ROCK	IN	IM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
F	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G																																																

/		82.47	87.73	4.81																																													
L																																																	

K	LM1	84.12	84.12	0.00																																													
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K	DM1	119.73	119.73	0.00																																												
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/		119.73	122.53	2.80																																													
L																																																	

/	LSX	122.53	122.83	0.30																																													
L																																																	

/		122.83	128.02	5.19																																													
L																																																	

R		122.83	128.02																																														
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SEQUENCE ABA

G E O L O G

A UNM	SAMPLE		% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CO	HASH
A LAB	SERIAL		R.CLG	R.CLG	R.CLG	R.CLG	B.CLG	R.CLG	R.CLG	B.CLG	
A TYP			H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH			WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00	R.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.								
R ASY	0.00	0.00	LA = MET ANALYSIS.								
R ASY	0.00	0.00	ALL ASSAY INFORMATION ENTERED AS -0.1								
A 001	82.30	82.91	061	6064	0.04	0.20	3.15	-0.1	-0.1	-0.1	2.89
A 001	82.91	84.12	121	6065	0.08	0.18	7.53	-0.1	-0.1	-0.1	7.29
A 001	84.12	85.34	122	6066	0.24	7.15	14.74	-0.1	-0.1	-0.1	21.63
A 001	85.34	86.25	090	6067	0.28	10.00	21.48	-0.1	-0.1	-0.1	31.26
A 001	86.25	87.78	152	6068	0.19	7.80	18.10	-0.1	-0.1	-0.1	25.59
A 001	87.78	88.39	061	6069	0.30	7.30	39.57	-0.1	-0.1	-0.1	46.67
A 001	88.39	89.92	153	6070	0.37	3.93	46.62	-0.1	-0.1	-0.1	50.42
A 001	89.92	91.44	124	6071	0.25	3.95	47.17	-0.1	-0.1	-0.1	50.87
A 001	91.44	92.95	107	6072	0.73	2.75	47.08	-0.1	-0.1	-0.1	50.06
A 001	92.95	94.49	151	6073	1.00	3.65	46.92	-0.1	-0.1	-0.1	51.07
A 001	94.49	96.01	149	6074	1.25	2.50	48.77	-0.1	-0.1	-0.1	52.02
A 001	96.01	97.54	148	6075	0.92	3.30	45.99	-0.1	-0.1	-0.1	49.71
A 001	97.54	99.06	152	6076	0.82	3.67	47.02	-0.1	-0.1	-0.1	51.01
A 001	99.06	100.58	150	6077	0.54	2.83	48.27	-0.1	-0.1	-0.1	51.14
A 001	100.58	102.11	145	6078	0.40	6.40	44.00	-0.1	-0.1	-0.1	50.30
A 001	102.11	103.63	144	6079	0.50	3.80	47.72	-0.1	-0.1	-0.1	51.52
A 001	103.63	105.40	154	6080	0.66	2.60	44.80	-0.1	-0.1	-0.1	47.56
A 001	105.40	106.68	108	6081	0.98	4.27	38.92	-0.1	-0.1	-0.1	43.67
A 001	106.68	108.20	141	6082	0.46	2.85	45.06	-0.1	-0.1	-0.1	47.87
A 001	108.20	109.58	128	6083	1.04	2.65	44.63	-0.1	-0.1	-0.1	47.22
A 001	109.58	111.25	152	6084	1.10	2.10	45.64	-0.1	-0.1	-0.1	47.74
A 001	111.25	112.78	125	6085	0.26	0.21	27.07	-0.1	-0.1	-0.1	27.04
A 001	112.78	114.30	140	6086	1.22	3.23	45.67	-0.1	-0.1	-0.1	49.62
A 001	114.30	116.13	150	6087	0.39	3.25	40.03	-0.1	-0.1	-0.1	43.17
A 001	116.13	117.35	100	6088	0.55	3.25	26.85	-0.1	-0.1	-0.1	30.15
A 001	117.35	118.87	134	6089	0.43	4.51	35.29	-0.1	-0.1	-0.1	39.73
A 001	118.87	119.73	086	6090	0.74	5.10	42.28	-0.1	-0.1	-0.1	47.62
A 001	119.73	121.01	123	6091	0.36	1.20	2.73	-0.1	-0.1	-0.1	3.79
A 001	121.01	121.61	058	6092	0.17	0.24	3.06	-0.1	-0.1	-0.1	2.97
A 001	121.61	122.53	068	6093	0.82	2.75	5.94	-0.1	-0.1	-0.1	9.01
A 001	122.53	122.83	029	6094	1.45	4.85	2.40	-0.1	-0.1	-0.1	8.20
A 001	122.83	123.44	058	6095	0.15	0.42	2.54	-0.1	-0.1	-0.1	2.61
A 001	123.44	124.97	153	6096	0.22	2.40	5.59	-0.1	-0.1	-0.1	7.71
A MAX	82.30	124.97			1.45	10.00	48.27	-0.1	-0.1	-0.1	59.22

A MIN				0.04	0.18	2.40	-0.1	-0.1	-0.1	-0.1	-0.1	2.12
A CMP	84.12	88.39	927	0.24	8.00	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	7.64
A CMP	88.39	119.73	2889	0.69	3.29	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.38
A CMP	119.73	124.97	512	0.41	1.84	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.65
A CMP	84.12	119.73	3316	0.63	3.90	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.93

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BASITE DEPOSIT YUKON

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 77-DP020
TOTAL DEPTH/LENGTH : 294.13
CORE/HOLE DIAMETER : 80COLLAR ELEVATION: 1293.40
SOUTHING (= IF S): 7002576.00
EASTING (= IF E): 436462.37AZIMUTH(DEG) : 358.00
VERTICAL ANGLE : -70.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : BHO +
DATE (YY/MM/DD): 811101
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	15.24	356.25	-72.50
2	30.48	1.25	-72.50
3	45.72	4.75	-72.00
4	60.96	6.25	-71.00
5	91.44	11.25	-69.00
6	121.92	15.25	-68.00
7	152.40	17.25	-67.50
8	182.88	25.25	-67.25
9	213.36	29.25	-67.50
10	243.84	31.25	-67.00
11	274.32	37.25	-67.00
12	294.13	37.25	-66.50

R HED ORIGINALLY LOGGED BY K.I.LU IN OCT. 77, THEN RELOGGED BY HJV IN

R HED JOIN OF R1, FROM PHOTOS.

F	T	R	E	R	V	A	L	-	CORE	T	%	TYPE	QUAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY				
K	L	(UNITS =	.	DEC.	PLACE)	REC'D	-	M	N	ROCK	FLYING	MIN	TURES	CHARACS												
E	A	(METRIC	FI=FOOTRIC)	ERY																						
Y	G	F	R	O	M	-	T	O	-	I	N	T	(.)	D	X	TYPE	1	2	QM1	1	2	F	C	A
K	F					ROCK																				
E	L					QUAL																				
Y	G					DESIG																				

/	OVR	6.00	6.01	6.01	OVER	P
---	-----	------	------	------	------	---

/	L	6.01	9.91	3.90	ARST	SN1	LM	RD	P	1	BD	U65
---	---	------	------	------	------	-----	----	----	---	---	----	-----

/	SHR	6.01	9.91	3.90	ARST	GR	SN1	LM	RD	R	1	BD	U65
---	-----	------	------	------	------	----	-----	----	----	---	---	----	-----

R	6.01	9.91	THE INTERVAL IS HIGHLY TO MODERATELY SHEARED. THE CORE IS VERY									
R	6.01	9.91	ROBBLY IN PLACES. IT IS LOCALLY BRECCIATED DUE TO SLUMPING.									
R	6.01	9.91	TOPS WERE PICKED UP THE HOLE IN THE OLD LOGS FROM LINING UPWARDS									
R	6.01	9.91	IN THE SAND BEDS.									

/	L	9.91	23.62	13.71	BRHT	*C= F* R*	NS6	P	HE L (
					SA	*S=	2	=	C.

X	F	R	D	E	T	I	REC'D	MB	%	RUCK	IN	TM	Q1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	DZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G						R	D	D	AGE	EV	RO	LC	TM	Q2	TX	TX	S	C	D	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA			

R 9.91 23.62 THIS UNIT IS ALSO FRIABLE AND RUBBLY DUE SHEARING AND FAULTING.

/ FLT 19.80 23.62 3.62 X BRRT GR GG1 F* B* NS6 R HE L(

L 19.80 23.62 THE INTERVAL IS MODERATELY OXIDIZED.

/ 23.62 25.01 1.39 CGPS SM3 F* B* 0 6 5 0 P D-

L 23.62 25.01 7A *C1 5 0
R 23.62 25.01 THE UNIT CONTAINS 10% ROUNDED ARGL FRAGMENTS AND CLOSE TO 50%
R 23.62 25.01 CHERT.

/ 25.01 42.56 17.55 BRRT SM= SS NT6 P D*

L 25.01 42.56 4A SI= 1 + KO=
R 25.01 42.56 THE INTERVAL CONTAINS SEVERAL LARGE ARSI FRAGMENTS AND SEVERAL
R 25.01 42.56 LARGE BRRT FRAGMENTS. THERE IS ALSO ONE SAND STONE FRAGMENT.
R 25.01 42.56 STARTING AT 29.13 TO 29.39M. MOST OF THE SHEARING HAS TAKEN
R 25.01 42.56 PLACE ALONG BEDDING PLACES IN THE ARSI FRAGMENTS.

/ 33.43 34.43 1.05 X BRRT SM= SS IM LO3 R D-

L 33.43 34.43 4A SI= 5 0 JL=

/ 42.56 46.20 3.64 BRRT SM+ SS SC NR7 P SC 60 R*

L 42.56 46.20 4A *C1 10 R* 3 JM+

R 42.56 46.20 THE INTERVAL SHOWS CRUDE BEDDING. THE FRAGMENTS ARE LENTICULAR
R 42.56 46.20 AND ELONGATED IN A 60 DEGREE ORIENTATION. PYRITE IS A
R 42.56 46.20 REPLACEMENT FEATURE IN THE CHERT AND ALSO OCCURS IN THE POROUS
R 42.56 46.20 SAND BANDS AND FRAGMENTS.

/ 46.20 60.96 14.76 BRRT *C F* B* MR6 P <(C. L)

L 46.20 60.96 5A SM= 3 *) KP2 <-

/ FLT 58.10 59.74 1.64 X BRRT GR GG1 R <* D)

L 58.10 59.74 5A CR <-

R 58.10 59.74 CORE IS LIGHTLY FRIABLE AND RUBBLY.

/ 60.96 65.52 4.56 BRRT *C1 SS RU MQ3 P V* D-

L 60.96 65.52 6A *S= 2 = LO3 V.

R 60.96 65.52 THE INTERVAL BETWEEN 60.94 TO 63.40M. IS CORRELATED WITH DH-75-2
R 60.96 65.52 FROM 74.27 TO 76.10M. THIS PORTION CONTAINS LARGE RIP UP CLAST
R 60.96 65.52 OF ARGL. FROM 63.40 TO 65.52, THERE ARE TWO SMALL UNITS OF
R 60.96 65.52 DIFFERENT COMPOSITIONS BUT TOO SMALL TO PGI. THIS INTERVAL IS

R 60.96 65.52 ALSO CUT BY A FAULT.

/ FLT 64.90 64.92 0.02 X BRRT GG1 SS RU MQ3 R V* D-

L 64.90 64.92 5A

K M/D 65.52 65.52 0.00

/ 65.52 66.22 0.70 SAND SM5 G: BD 1 5 1 P 2 RD U65 <* D-

L 65.52 66.22 6A S11 LC RS 5 0 <-

R 65.52 66.22 THE UNIT IS MAINLY A SAND BUT LOCALLY IS A BRECCIA, CONTAINING

```
K F P R O B - T D - I N T RECDV MD % RJCK IN TN RM1 TX TX F C % M ARG RT 1 ID AZM DIP QZ FL CY CA BA XX PY CP GL YY A 1 A 2  
E -L- ----.- --.--.- ---.- --.- -- -- -- -- -- -- -- -- -- -- -- -- -- -- -- -- --  
Y G          R O D AGE EV RD LC TM RM2 TX TX S C U O CHT      2 ID AZM DIP MG MU CL SD QS HA PR MT SL HA
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R	65.52	66.22	PEBBLE SIZE ANGULAR FRAGMENTS.									
Z	66.22	67.82	1.60	BRHT	*C=	MQ5	P				D=	
L				5A	SI=	3	LN3					
Z	67.82	99.06	31.24	BRHT	SN= SS SC	MO7	P				L*	
L				4A	*C* F*	KO+						
Z	67.82	99.06	31.24	1 BRHT	SN= F* B*	MO5	R				R(
L				6A	*C= R*	KO2						
R	67.82	99.06	THE INTERVAL CONTAINS SEVERAL LARGE ARSI FRAGMENTS RANGING UP TO									
R	67.82	99.06	2.5 METERS. BEDDING IN THESE FRAGMENT VARIES FROM 30 TO 90%.									
R	67.82	99.06	THE UNIT ALSO CONTAINS SEVERAL FRAGMENTS OF BRHT.									
Z	99.06	101.31	2.25	BRHT	SN= R* F*	LP4	P				R)	
L				5A	*C1 H* SS 3	KO2						
Z	SHR	99.06	99.80	0.74	X BRHT GR CR	SN= R* F*	LP4	R			R)	
L					4A	*C1 H* SS 3	KO2					
R		99.06	101.31	THERE IS APPROX 2.5% SAND FRAGMENTS								
Z		101.31	104.85	3.54	SAND	SN5 BS BD 0 4 2 0	P	2 BD	U45 <(C*	D*	
L					6A	SI1 SS FU 5				D=		
R		101.31	104.85	THE INTERVAL IS LOCALLY A BRHT.								
Z	FAL	104.45	104.35	0.10	X SAND GR CR GGS		R				C)	
L					3A							
K	M/C	104.85	104.85	0.00								
Z		104.85	106.53	1.68	SAND	SN7 BS BD 0 4 1 N	P	2 BD	U70 V)	L=	D)	
L					6A	SI1 SS FU 5				D)		
R		104.85	106.53	THIS MARKER BED WAS PICKED BY K.L.LU. AT 106.37 METERS. WE FIND								
R		104.85	106.53	PYRO-BITUMEN IN BRECCIA FILLING. THERE IS HEMATITE COATINGS ON								
R		104.85	106.53	FRACTURE/SHEAR SURFACES.								
Z		106.53	110.00	3.47	ARSI CR	SN+ BD CU	P	3 BD	55 <*	C=	R(
L					4A	SI=						
Z	SHR	106.53	107.95	1.42	X ARSI GR SF SN+ BD CU		R	3 BD	55 <*	C=	R(
L					3A CR SI=							
R		106.53	110.00	THE ARSI CONTAINS SEVERAL BANDS OF COARSE SAND RANGING UP TO 8								
R		106.53	110.00	CMS. THESE BANDS SHOW COARSING UPWARD WHICH POSSIBLE INDICATES								
R		106.53	110.00	A LARGE FRAGMENT. THE UNIT IS SOMEWHAT SILICIFIED TOWARDS THE								
R		106.53	110.00	TOP AND CARBONEOUS TOWARDS THE BASE.								
Z		110.00	110.85	0.85	SAND SD	SN8 BS BD 0 4 1 L	P	2 BD	45 <=		D)	
L					7A	SI1 FU	6			D+		
R		110.00	110.85	POSSIBLE FRAGMENT.								
Z		110.60	110.85	0.25	X ARSI	SI= BD	R	2 BD	45			
L					3A	SN+						

[illegible]

R 110.60 110.65 POSSIBLE FRAGMENT.

Z	110.85	127.50	15.65	RIGHT	SA= F* R*	MU5	P	V*	C. HE R)
L				SA	*C= G; H* 2) +	LD3			C. D) C.

Z	SHR	120.10	121.20	1.10	x	ARSI	GR	SII	RD	SS	R	2	RD	85	<=		D*
L							4A	SI	=	SC						D)	

R	120.10	121.20	LARGE FRAGMENT.
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Z	M/B	127.50	132.85	5.35		SABD SD	SR6 //	RU 0	5	A U		P	2 BD	U65		C. HE D)
L						7A	SR1 FU	(L 5								D) C.

R	127.50	132.85	THIS UNIT REPRESENTS SEVERAL AB AND ABD CYCLES OF A ROOMA
R	127.50	132.85	SEQUENCE. IT IS VERY COARSE AT THE BASE AND FINES UPWARDS.
R	127.50	132.85	CORRELATION OF THIS MARKER BED STARTS AT 131.22M. THIS
R	127.50	132.85	REPRESENTS THE BASE OF THE RIP UP UNIT, WHICH IS CORRELATED WITH
R	127.50	132.85	OTHER HOLES. BELOW 131.22 THE UNIT HERE IS NOT SEEN IN OTHER
R	127.50	132.85	SECTIONS. THE INTERVAL HAS TWO LARGE ARG1 FRAGMENTS WHICH MEANS
R	127.50	132.85	THAT WE ARE CLOSE TO A FAULT SCARP. LOAD CASTING CAN BE SEEN AT
R	127.50	132.85	131.96m.

Z FRG	132.56	132.85	0.29	X ARSI CP	SI= SS	R
				54	59)	

7	132.85	133.93	1.08	SA 40	SM 3	BS	FU	U	1	3	M	P	D*
1				7A	SL			S					01

R 132.85 133.93 REPRESENT MAINLY THE ACYCLE OF A ROOMA SEQUENCE. SAND CONTENT
R 132.85 133.93 INCREASES TOWARDS THE TOP.

/	133.93	138.00	4.07	BRAT	S11 SS F*	MR6	P	C. HE D)
L				SA	*C= F* 3)	KD1		<- C.

2 153.95 158.00 SMALL VEIN OF PYRO-BITUMEN AT 158.23M.

/	158.00	146.52	8.52	BRHM	S1= SS SC	MR7	P	L)	C-	R)
L				DA	SA+ E* F* 3	JO+			<-	

/ SHR	141.80	144.03	2.23	x	RRHM	GR	S1=	SS	SC	MR7	R	L)	C=	R)
L						4A	S0+	R*	F* 3	JO+			<=	

/	146.52	160.90	14.38	DRRT	Su1 F* R*	LS6	P	C. HE R)
L				5A	*C=	J02		D- C.

R	146.52	160.90	THE INTERVAL IS LOCALLY A PRS ⁰ . THE UNIT IS CUT BY TWO. SHEAR
R	146.52	160.90	ZONES.

/ SHR 149.00 149.66 0.66 X BRHT GR SN1 F* R* LS6 R C. HE R)

/	152.12	153.40	1.10	x	BRSSN	SN2	F*	R*	0	2	3	0	M03	R	R*
L					SA	SI1			4			0	DN2		D*

/ SHR 154.20 156.67 1.87 X BHT GR SNI F* R* LS6 R C. HE R)

R 249.42 249.98 THE UNIT ALSO CONTAIN APPROX 40% LAMINATED ARGL WHICH IS VERY
R 249.42 249.98 SILICEOUS.

	7	SHR	284.84	286.97	2.13	ARGL BA CR	LF	P	1 LM	55	80	L)
L						34						
R			284.84	286.97		BARITE OCCURS AS NODULES IN DISTINCT BEDS UP TO 1CM (SPOTTED BA)						
R			284.84	286.97		THE UNIT IS MODERATELY BROKEN UP.						

[illegible]

/	256.97	238.65	1.68	4.86	*C = F*	2*	MD3	P	4	C =	R)
L				5.8	SI = F*	4	LM4				

/	288.65	289.10	0.45	SA-00	9Y	SA07	BD	BS	0	4	4	K	P	1	BD	U40	C.	D+
---	--------	--------	------	-------	----	------	----	----	---	---	---	---	---	---	----	-----	----	----

L	9A	SI1 FU // 6	0
---	----	-------------	---

R 288.05 289.10 THE INTERVAL SHOWS A 90 CYCLE OF THE BOUMA SEQUENCE.

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/      289.10  294.13   5.03      ARSI Ck      SI= AX BD      P 1 BD      60      <-  L)

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L 30

R 289.10 294.13 BARITE ALSO OCCURS INTERSTITIALLY WITH THE PYRITE BANDS. THE

R	289.10	294.13	PYRITE BANDS RANGE UP TO 1CM. THERE IS A 15CM BAND OF CHERT
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R 299.10 294.13 NODULES AT 293.07M. PYRITE REPLACING THE OUTER EDGE AND ALSO

R	289.10	294.13	DESSIMATED.
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A URM	SAMPLE				% Pb	% Zn	% Ba	OZ AG	% Cu	% Fe	OZ AU	% Cd	HASH
A LAB	SERIAL				B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	H-CORE				H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH	WA				WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00	B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	WA = WET ANALYSIS.										
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1										
A 001	246.69	248.41	152	6097	0.16	0.95	3.38	-0.1	-0.1	-0.1	-0.1	-0.1	3.99
A 001	248.41	249.42	101	6098	0.26	1.30	2.37	-0.1	-0.1	-0.1	-0.1	-0.1	3.43
A 001	249.42	250.55	109	6099	1.50	3.75	1.74	-0.1	-0.1	-0.1	-0.1	-0.1	6.49
A 001	250.55	251.46	089	6100	1.50	3.67	49.05	-0.1	-0.1	-0.1	-0.1	-0.1	53.72
A 001	251.46	252.68	109	6101	0.55	3.71	45.23	-0.1	-0.1	-0.1	-0.1	-0.1	48.99
A 001	252.68	254.51	149	6102	0.92	4.40	47.47	-0.1	-0.1	-0.1	-0.1	-0.1	52.29
A 001	254.51	255.73	121	6103	1.32	3.08	53.00	-0.1	-0.1	-0.1	-0.1	-0.1	56.90
A 001	255.73	257.56	181	6104	0.95	3.40	51.93	-0.1	-0.1	-0.1	-0.1	-0.1	55.78
A 001	257.56	259.08	150	6105	0.74	2.40	51.11	-0.1	-0.1	-0.1	-0.1	-0.1	53.75
A 001	259.08	260.60	149	6106	0.50	2.00	48.40	-0.1	-0.1	-0.1	-0.1	-0.1	50.40
A 001	260.60	262.13	151	6107	0.51	2.40	41.30	-0.1	-0.1	-0.1	-0.1	-0.1	43.71
A 001	262.13	263.65	152	6108	0.44	3.85	46.53	-0.1	-0.1	-0.1	-0.1	-0.1	50.32
A 001	263.65	265.18	138	6109	0.55	2.33	50.48	-0.1	-0.1	-0.1	-0.1	-0.1	52.86
A 001	265.18	266.70	119	6110	0.64	2.60	49.74	-0.1	-0.1	-0.1	-0.1	-0.1	52.48
A 001	266.70	268.22	140	6111	0.40	2.90	45.27	-0.1	-0.1	-0.1	-0.1	-0.1	48.07
A 001	268.22	269.75	135	6112	0.54	2.75	52.38	-0.1	-0.1	-0.1	-0.1	-0.1	55.17
A 001	269.75	271.27	131	6113	0.57	2.83	50.15	-0.1	-0.1	-0.1	-0.1	-0.1	53.05
A 001	271.27	272.80	129	6114	0.60	3.05	50.72	-0.1	-0.1	-0.1	-0.1	-0.1	53.87
A 001	272.80	274.32	140	6115	0.98	2.72	48.74	-0.1	-0.1	-0.1	-0.1	-0.1	51.94
A 001	274.32	275.91	159	6116	0.43	4.03	45.00	-0.1	-0.1	-0.1	-0.1	-0.1	48.96
A 001	275.91	277.28	137	6117	0.43	7.86	3.91	-0.1	-0.1	-0.1	-0.1	-0.1	11.64
A 001	277.28	278.28	106	6118	0.22	8.80	3.34	-0.1	-0.1	-0.1	-0.1	-0.1	11.86
A 001	278.28	279.59	131	6119	0.10	4.76	5.93	-0.1	-0.1	-0.1	-0.1	-0.1	10.23
A 001	279.59	280.87	124	6120	0.08	2.95	5.32	-0.1	-0.1	-0.1	-0.1	-0.1	6.95
A 001	280.87	282.18	131	6121	0.19	3.83	3.68	-0.1	-0.1	-0.1	-0.1	-0.1	7.20
A 001	282.18	283.16	098	6122	0.80	12.60	8.17	-0.1	-0.1	-0.1	-0.1	-0.1	21.07
A 001	283.16	284.84	137	6123	0.57	9.80	2.61	-0.1	-0.1	-0.1	-0.1	-0.1	12.48
A 001	284.84	286.97	195	6124	0.04	0.20	1.19	-0.1	-0.1	-0.1	-0.1	-0.1	0.93
A 001	286.97	288.04	107	6125	0.03	0.16	1.08	-0.1	-0.1	-0.1	-0.1	-0.1	0.77
A 001	288.04	289.09	079	6126	0.02	0.05	0.62	-0.1	-0.1	-0.1	-0.1	-0.1	0.19
A MAX	246.69	289.09			1.50	12.60	53.00	-0.1	-0.1	-0.1	-0.1	-0.1	66.60

A MIN				0.02	0.05	0.62	-0.1	-0.1	-0.1	-0.1	-0.1	0.19
A CMP	249.42	275.91	2447	0.73	3.09	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.22
A CMP	275.91	284.84	375	0.34	6.94	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	6.68
A CMP	282.18	233.16	098	0.80	12.60	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	12.80
A CMP	249.42	284.87	3325	0.63	4.07	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.10

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASDE PB-ZH-AG-BA STE DEPOSIT, V.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 77-DH025
TOTAL DEPTH/LENGTH : 263.65
CORE/HOLE STAGE/HR : 10

COLLAR ELEVATION:	1316.49
ROUTING (- IF S):	7002827.00
FASTING (- IF B):	436326.87

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AZIMUTH( DEG ) : 174.25
VERTICAL ANGLE : -71.00
CO-ORD SYSTEM : UTM

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GEOLOGGED BY : HDG +
DATE (YY/MM/DD): 810815
PROJECT NUMBER : J-MAIN

SEQ. NO. OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	15.24	182.25	-66.50
2	30.48	181.25	-65.00
3	45.72	179.25	-63.00
4	60.96	179.25	-62.00
5	91.44	177.25	-59.75
6	121.92	174.25	-56.00
7	152.40	172.25	-56.00
8	182.88	171.25	-51.00
9	209.70	171.25	-47.00
10	243.84	171.25	-45.00
11	263.65	171.25	-43.75

R HED		ORIGINALLY LOGGED BY P. WELLS ON OCT. 7, 1977.																														
F - I N T E R V A L -		CORP		T - %		TYPT - DAL		TEX -		GRAIN		PGI		STRUCTUR-1		ALTERATION		MINS		ORE-TYPE		MINS		SUMMARY								
K	L (UNITS = . DEC. PLACE)	REC'D	RY	ROCK	TY	DA	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	ALT	ORE		
E	A (MT=METRIC FT=FOOTRIC)	ERY	O	I	TM	TM	MAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	ALT	ORE	
Y	G F R D M - I D - I N T (.)	D	X	TYPE	1	2	RM1	1	2	F	F	C	A		1		AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
K	F	ROCK	FM	RT	TM	Q42	TX	TX	S	C	O	O	CHT																			
E	L	DUAL	AGE	EN- 3	LC- 3		3	4	O				/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1	
Y	G	DESIG		VIR	COL				R				C				STRUCTUR-2			A	A	A	A	A	A	A	A	A	A	2	2	

/ DVS	0.60	5.66	5.66	OVER	P
/	5.66	50.10	46.00	ARSI	SN2 BD SS 0 3 2 3 P 2 BD 55 L+
L				3A LC 7	<+
R	5.66	50.10		THE PYRITE APPEARS AS VERY FINE GRAINS IN THE ARGILLITE, AND AS	
R	5.66	50.10		FINE GRAINED LAMINATIONS IN THE SANDSTONE LAYERS.	
R SPC	5.66	50.10		SAMPLE D.G. 255 TAKEN AT 30.2 METERS.	
/	18.02	22.56	4.54	X ARSI	SN2 BD SS 0 3 2 3 R 4 BD 50 V+ L+
L					D(<
R	18.02	22.56		LARGE DISSEMINATED PATCHES OF PYRITE OCCUR IN CONFORMABLE	
R	18.02	22.56		5 CM. BEDS. FREQUENTLY MINOR AMOUNTS OF PYRRHOTITE ARE DETECTED	
R	18.02	22.56		WITHIN THESE BEDS. SPHALERITE IS FOUND IN VEINS AMOUNTING TO	
R	18.02	22.56		LESS THAN 1% BY VOLUME.	
/	27.49	27.78	0.29	X ARSI	SN2 BD SS 0 3 2 3 R 2 BD 45 D+
L					V1
/	26.25	31.50	5.25	X ARSI	SN2 BD SS 0 3 2 3 R 3 BD 50 L+
L					D(

	Top of Interval (m)	Bottom of Interval (m)	Interval Thickness (m)	Interval Description	Interval Type	Interval Grade	Interval Color	Interval Texture	Interval Structure	Interval Notes	Interval Remarks
R	28.25	31.50		Same remark as in repeat interval 18.02 to 22.56 meters.							
/	35.30	36.41	1.11	X ARSI	SN2 BD SS 0 3 2 3	R	2 BD	50			
L											
R	35.30	36.41		THIS INTERVAL IS A MILDLY BRECCIATED, QUARTZ-SIDERITE STOCKWORK							
R	35.30	36.41		VEINED, SILTY ARGILLITE.							
/	37.49	38.01	0.52	7 BRHM	SS	KN9	R				
L											
/	38.05	40.18	2.13	X ARSI	SN2 BD SS 0 3 2 3	R	1 BD	59 <+			
L											
/	42.37	50.10	7.73	Y ARSI	SN2 BD SS 0 3 2 3	R	2 BD	55			
L											
R	42.37	50.10		LARGE SUB-EHEDRAL PYRITE CRYSTALS OCCUR WITHIN SANDSTONE							
R	42.37	50.10		LAMINATIONS.							
R	42.37	50.10		SAMPLE D.G. 256 TAKEN AT 47.25 M.							
R	42.37	50.10									
/	50.10	64.02	13.92	BRHM	*C= F* KN1 P						
L											
R	50.10	64.02		THE PEBBLY MUDSTONE CONTAINS A SANDSTONE MATRIX. NORMAL GRADING							
R	50.10	64.02		INDICATES THAT STRATIGRAPHIC TOPS ARE DOWNHOLE.							
/	55.40	56.20	0.80	7 BRHM CR	K05 R						
L											
R	55.40	56.20		THIS PEBBLY MUDSTONE CONTAINS A MUDSTONE MATRIX.							
/	56.20	57.10	0.90	9 BRHM CR	SS LP9 R						
L											
R	56.20	57.10		THE BOTTOM OF THE REPEAT INTERVAL IS VERY PYRITIC, AND CONTAINS							
R	56.20	57.10		QUARTZ-SIDERITE STOCKWORK VEINING.							
/	57.60	58.33	0.73	8 SAND	MX F I 7 J R						
L											
/	60.10	61.30	1.20	8 BRHM CR	*C= F* J01 R						
L											
R	60.10	61.30		THE MATRIX IS A COMBINATION OF SAND AND CARBONACEOUS ARGILLITE.							
/	64.02	70.41	6.39	SAND	MX A I 7 6 P						
L											
R	64.02	70.41		THIS MASSIVE SANDSTONE CONTAINS A NUMBER OF THIN, CONVOLUTED							
R	64.02	70.41		ARGILLIC BEDS. GALENA IS PRESENT IN SMALL QUARTZ-FILLED							
R	64.02	70.41		FRACTURES AND VEINS.							
/	70.41	76.20	5.79	CGRR	*C= F* L02 P						
L											
R	70.41	76.20		GALENA OCCURS IN SMALL BLEB AND FRACTURES WITHIN THE							
R	70.41	76.20		CHERT PEBBLE MATRIX.							
R	70.41	76.20		SAMPLE D.G. 257 TAKEN AT 74.98 M.							

/	SHR	165.66	166.42	0.76	x	ARGL CR	GGG BD //	0 1 + 5	R	2 BD	50	
L						2A	84*	B				V+

/	232.14	232.52	9.18	FGSX	BR	P	V1	V+	M3	B1
---	--------	--------	------	------	----	---	----	----	----	----

K	F	F	R	D	T	D	T	RECDV	ED	%	ROCK	TM	TM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Y	G								R	G	D	AGE	EV	RR	LC	TM	DM2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	NG	MU	CL	SD	QS	HA	PR	MT	SL	HA		

K UM1 232.32 242.32 0.00

/ 232.32 253.00 20.68
L

ARGL SN+ LM 1 3 + 3 P 0 LM 40 L+
3A LC RR 8 L+

/ 232.32 232.55 0.23
L

X ARGL SN+ BP 1 3 + 3 R 0 LM 40 L+
3A LC RR 8 L+ L+

/ 253.00 263.65 10.65
L

ARST CR SN1 LM LC 1 3 1 3 P LM 38 L+
3A CC 8

R SPC 253.00 263.65 SAMPLE D.G. 268 TAKEN AT 255.13 m.

A UMM	SAMPLE				% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL				B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP					H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00	B.CLG = HONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	WA = NET ANALYSIS.										
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1										
A 001	216.40	218.59	190	6135	0.01	0.05	4.43	-0.1	-0.1	-0.1	-0.1	-0.1	3.99
A 001	218.59	218.69	030	6136	0.03	0.53	8.71	-0.1	-0.1	-0.1	-0.1	-0.1	8.77
A 001	218.69	219.61	092	6137	1.80	10.20	0.42	-0.1	-0.1	-0.1	-0.1	-0.1	11.92
A 001	219.61	220.51	070	6138	0.53	7.15	29.45	-0.1	-0.1	-0.1	-0.1	-0.1	36.93
A 001	220.51	220.98	067	6139	0.59	9.10	8.92	-0.1	-0.1	-0.1	-0.1	-0.1	18.11
A 001	220.98	222.50	106	6140	0.48	7.45	42.43	-0.1	-0.1	-0.1	-0.1	-0.1	49.86
A 001	222.50	223.42	092	6141	0.20	6.65	42.49	-0.1	-0.1	-0.1	-0.1	-0.1	48.84
A 001	223.42	224.70	128	6142	0.41	4.62	46.59	-0.1	-0.1	-0.1	-0.1	-0.1	51.12
A 001	224.70	225.80	106	6143	0.69	4.45	48.33	-0.1	-0.1	-0.1	-0.1	-0.1	52.97
A 001	225.80	226.77	087	6144	0.54	3.65	49.72	-0.1	-0.1	-0.1	-0.1	-0.1	53.41
A 001	226.77	227.50	066	6145	0.51	2.75	40.87	-0.1	-0.1	-0.1	-0.1	-0.1	43.63
A 001	227.50	228.11	056	6146	0.85	3.08	45.43	-0.1	-0.1	-0.1	-0.1	-0.1	48.86
A 001	228.11	229.51	129	6147	0.48	2.85	46.28	-0.1	-0.1	-0.1	-0.1	-0.1	49.11
A 001	229.51	230.12	061	6148	1.00	2.80	43.00	-0.1	-0.1	-0.1	-0.1	-0.1	46.30
A 001	230.12	231.65	153	6149	1.15	6.00	38.90	-0.1	-0.1	-0.1	-0.1	-0.1	45.55
A 001	231.65	232.14	049	6150	4.00	11.10	1.18	1.39	-0.1	-0.1	-0.1	-0.1	17.27
A 001	232.14	232.32	018	6151	3.60	11.50	2.04	1.34	-0.1	-0.1	-0.1	-0.1	18.08
A 001	232.32	232.56	024	6152	0.52	0.15	2.03	-0.1	-0.1	-0.1	-0.1	-0.1	2.20
A 001	232.56	234.07	151	6153	0.03	0.52	4.72	-0.1	-0.1	-0.1	-0.1	-0.1	4.77
A MAX	216.40	234.07			4.00	11.50	49.72	1.39	-0.1	-0.1	-0.1	-0.1	66.21

A MTU				0.01	0.05	0.42	1.34	-0.1	-0.1	-0.1	-0.1	1.42
A CMP	218.69	223.42	471	0.75	8.02	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	8.17
A CMP	223.42	230.12	637	0.58	3.54	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.52
A CMP	230.12	232.32	220	1.99	7.59	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	8.98

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

JASON PH-ZN-AG-BA S1F DEPOSII, Y.I.

FORMAT VERSION : 6802

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	18.29	333.25	-72.00
2	30.78	333.25	-72.00
3	45.72	336.25	-72.00
4	61.26	341.25	-71.00
5	97.84	350.25	-70.00
6	122.22	355.25	-69.00
7	152.70	3.25	-67.50
8	182.88	6.25	-65.50
9	213.36	13.25	-62.00
10	241.09	17.25	-57.00
11	280.42	19.25	-55.00

[illegible]

R SVY 0.00 0.00 SPERRY SURV TESTS.

1	0.00	247.95	247.95	MISS
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K	UM1	247.95	247.95	0.00
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1	247.95	257.25	9.30	MISS
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X	LM1	257.25	257.25	0.00
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1	257.25	283.16	25.91	MISS
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A UMM	SAMPLE	% PR	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	B.CLG	H.CLG	H.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		NA	NA	NA	NA	NA	NA	NA	NA	

R ASY 0.00 0.00 B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 NA = NET ANALYSIS.

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	235.51	236.83	53	6159	0.05	0.10	1.22	-0.1	-0.1	-0.1	-0.1	-0.1	0.87
A 001	236.83	237.13	50	6160	0.09	2.27	0.65	-0.1	-0.1	-0.1	-0.1	-0.1	2.51
A 001	237.13	238.96	141	6161	1.34	7.00	0.22	-0.1	-0.1	-0.1	-0.1	-0.1	8.06
A 001	238.96	240.79	110	6162	1.46	6.70	0.09	-0.1	-0.1	-0.1	-0.1	-0.1	7.75
A 001	240.79	241.55	53	6163	0.64	5.12	2.65	-0.1	-0.1	-0.1	-0.1	-0.1	7.91
A 001	241.55	243.08	153	6164	0.05	0.43	11.02	-0.1	-0.1	-0.1	-0.1	-0.1	11.00
A 001	243.08	247.00	84	6165	0.06	0.23	7.83	-0.1	-0.1	-0.1	-0.1	-0.1	7.62
A 001	247.00	247.95	46	6166	1.95	7.70	1.24	-0.1	-0.1	-0.1	-0.1	-0.1	10.39
A 001	247.95	248.41	98	6167	1.02	7.05	1.02	-0.1	-0.1	-0.1	-0.1	-0.1	8.59
A 001	248.41	249.60	156	6168	1.85	9.70	0.07	-0.1	-0.1	-0.1	-0.1	-0.1	11.12
A 001	249.60	251.25	110	6169	1.70	9.70	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	10.94
A 001	251.25	252.68	41	6170	2.30	19.80	0.09	0.05	-0.1	-0.1	-0.1	-0.1	21.84
A 001	252.68	253.47	96	6171	1.95	14.40	0.09	0.06	-0.1	-0.1	-0.1	-0.1	16.10
R ASY	253.47	254.51											
A 001	254.51	255.30	82	6173	1.28	9.05	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	9.87
A 001	255.30	257.25	128	6174	0.38	2.93	1.46	-0.1	-0.1	-0.1	-0.1	-0.1	4.27
A 001	257.25	259.08	122	6175	0.15	1.55	1.94	-0.1	-0.1	-0.1	-0.1	-0.1	3.14
A 001	259.08	260.60	138	6176	0.10	1.02	4.53	-0.1	-0.1	-0.1	-0.1	-0.1	5.15
A 001	260.60	262.13	93	6177	0.08	1.25	5.32	-0.1	-0.1	-0.1	-0.1	-0.1	6.15
A 001	262.13	263.19	92	6178	0.19	2.05	3.08	-0.1	-0.1	-0.1	-0.1	-0.1	4.82
A 001	263.19	264.41	44	6179	1.90	5.10	0.52	-0.1	-0.1	-0.1	-0.1	-0.1	7.02
A 001	264.41	265.02	151	6180	0.09	0.58	6.27	-0.1	-0.1	-0.1	-0.1	-0.1	6.44
A CMP	265.02	266.55	308		1.27	6.55	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	7.22
A CMP	266.55	267.25	674		1.68	10.72	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	11.80

INTERVAL MISSING.

A MIN	0.05	0.10	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.45
A MAX 255.51 266.55	2.30	19.80	11.02	-0.1	-0.1	-0.1	-0.1	-0.1	32.62

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-PB STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 7A-DH027
TOTAL DEPTH/LENGTH : 221.28
CORE/HOLE DIAMETER : 89COLLAR ELEVATION: 1213.26
NORTHING(- IF S): 7002476.00
EASTING (- IF W): 435828.69AZIMUTH(DEG) : 360.00
VERTICAL ANGLE : -70.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	9.15	356.00	-70.00
2	21.94	355.00	-69.50
3	50.44	359.00	-69.00
4	91.46	15.00	-68.00
5	121.95	22.00	-64.00
6	152.44	24.00	-62.00
7	182.93	23.00	-59.50
8	213.41	27.00	-59.50

F	- I N T E R V A L -	CORE	T- %	TYPE	QUAL	TEX-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECOV-	R E	ROCK	TYING	MIN	TURES	CHARACS						
E	A (METRIC FT=FOOTRIC)	ERY	U I		TM	TM	MAT	TX	TX	F	C	%	M	ARG
Y	G	F	R	O	M	-	I	O	-	I	N	T	(.)
K	F													
E	L													
Y	G													

R SVY 0.00 0.00 SPERRY SURF TESTS.

/ 0.00 195.24 195.24 MISS P

K UM1 195.24 195.24 0.00

/ 195.24 209.95 14.71 MISS P

K LM1 209.95 209.95 0.00

/ 209.95 221.28 11.33 MISS P

A URM				SAMPLE	% PR	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		00 ASSAY INFORMATION ENTERED AS -0.1									
A 001	193.24	195.24	200	12276	0.05	0.88	3.92	-0.1	-0.1	-0.1	-0.1	-0.1	4.35
A 001	195.24	197.20	156	12277	1.40	6.40	37.80	-0.1	-0.1	-0.1	-0.1	-0.1	45.10
A 001	197.00	198.40	135	12278	0.74	4.00	47.10	-0.1	-0.1	-0.1	-0.1	-0.1	51.34
A 001	198.40	199.80	140	12279	0.73	3.03	47.80	-0.1	-0.1	-0.1	-0.1	-0.1	51.06
A 001	199.80	201.00	105	12280	0.67	6.13	38.50	-0.1	-0.1	-0.1	-0.1	-0.1	44.80
R ASY	199.80	201.00		SPECIFIC GRAVITY OF ORE IS 3.60.									
A 001	201.00	202.20	110	12281	0.71	4.25	47.00	-0.1	-0.1	-0.1	-0.1	-0.1	51.46
A 001	202.20	203.80	140	12282	0.86	3.95	52.20	-0.1	-0.1	-0.1	-0.1	-0.1	55.61
A 001	203.80	205.20	124	12283	0.80	2.30	51.60	-0.1	-0.1	-0.1	-0.1	-0.1	54.20
A 001	205.20	206.70	146	12284	1.02	2.70	51.60	-0.1	-0.1	-0.1	-0.1	-0.1	54.82
A 001	206.70	208.60	180	12285	0.48	2.32	48.80	-0.1	-0.1	-0.1	-0.1	-0.1	51.10
R ASY	206.70	208.60		SPECIFIC GRAVITY OF ORE IS 3.95									
A 001	208.60	209.45	80	12286	2.92	11.60	2.07	0.28	-0.1	-0.1	-0.1	-0.1	16.47
A 001	209.45	209.95	46	12287	2.80	13.40	1.35	0.18	-0.1	-0.1	-0.1	-0.1	17.33
A 001	209.95	211.60	120	12288	0.65	3.52	2.35	-0.1	-0.1	-0.1	-0.1	-0.1	6.02
A 001	211.60	214.00	204	12293	0.06	1.72	8.83	-0.1	-0.1	-0.1	-0.1	-0.1	10.11
A 001	214.00	215.00	83	12289	0.11	3.25	6.47	-0.1	-0.1	-0.1	-0.1	-0.1	9.33
A 001	215.00	216.15	75	12290	0.18	6.75	0.63	-0.1	-0.1	-0.1	-0.1	-0.1	7.06
A 001	216.15	217.07	85	12291	0.10	4.10	0.76	-0.1	-0.1	-0.1	-0.1	-0.1	4.46
A 001	217.07	218.00	93	12292	0.03	0.11	1.05	-0.1	-0.1	-0.1	-0.1	-0.1	0.69
A CMP	195.24	217.07	1992		0.76	4.18	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.34

A MIN		0.05	0.11	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.44
A MAX	193.24 216.00	2.92	13.40	52.20	-0.1	-0.1	-0.1	-0.1	-0.1	68.02

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASCO PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 78-DH028

COLLAR ELEVATION: 1155.67

AZIMUTH(DEG) : 350.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 367.26

NORTHING(= 1F S): 7002337.00

VERTICAL ANGLE : -72.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : HQ

EASTING (= 1F W): 437109.81

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	15.24	359.00	-69.50
2	30.48	2.00	-70.50
3	45.72	360.00	-70.50
4	60.96	359.00	-70.00
5	91.44	10.00	-68.00
6	121.92	16.00	-66.50
7	152.40	26.00	-65.00
8	182.88	33.50	-62.00
9	213.36	35.50	-59.00
10	243.84	40.00	-57.00
11	274.32	42.00	-53.00
12	306.80	40.00	-49.00
13	365.76	45.00	-39.50

F	- I N T E R V A L -	CORE	T- %	TYPE	QUAL	TEX-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC. PLACE) RECOV-	N M ROCK	RYING	MIN	TURES	CHARACS								
E	A (MT=METRIC FT=FOOTRIC) ERY	O I	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100											
Y	G F R U M - T O - I N T (.)	D X TYPE	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100											
K	F	ROCK	FR	RT	TX	TX	S	C	O	O	CHT			
E	L	QUAL	AGE	FR	LC	3	3	4	0	/				
Y	G	DESIG	VIR	COL			K	C						

R SVY 0.00 0.00 SPERRY SUR TESTS.

/ 0.00 307.00 307.00 MISS P

K DM1 307.00 307.00 0.00

/ 307.00 312.30 5.30 MISS P

K LM1 312.30 312.30 0.00

/ 312.30 367.26 54.96 MISS P

A UMM	SAMPLE	% PB	% ZN	% PA	OZ AG	% CU	% FE	OZ AU	% CD	HASH		
A LAB	SERIAL	B.CLG	F.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG			
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE			
A MTH		BA	VA	VA	WA	WA	WA	WA	WA			
R ASY	0.00	0.00	B.CLG = RONDAK CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00	WA = WET ANALYSIS.									
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	306.60	307.00	34	12294	0.07	1.23	-0.1	-0.1	-0.1	-0.1	-0.1	0.70
A 001	307.00	309.10	210	12295	0.25	5.95	-0.1	-0.1	-0.1	-0.1	-0.1	5.63
A 001	309.10	310.00	80	12296	0.11	1.00	-0.1	-0.1	-0.1	-0.1	-0.1	0.51
A 001	310.00	312.30	230	12297	0.29	4.45	-0.1	-0.1	-0.1	-0.1	-0.1	4.14
A 001	312.30	313.30	60	12342	0.06	1.50	-0.1	-0.1	-0.1	-0.1	-0.1	0.96
R ASY	312.30	313.30	GEOCHEM ANALYSIS.									
A GHP	306.60	313.30	522		0.22	3.82	-0.1	-0.1	-0.1	-0.1	-0.1	3.44

A MIN		0.06	1.23	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.69
A MAX	506.60 313.30	0.28	5.95	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	5.63

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASON PB-ZN-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 73-DH029	COLLAR ELEVATION : 1286.88	AZIMUTH(DEG) : 180.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 91.14	NORTHING(- IF S) : 7002528.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD) : 0
CORE/HOLE DIAMETER : HQ	EASTING (- IF W) : 436463.19	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S

SPN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	91.14	174.00	-42.00
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[illegible]

R SVY	0.00	0.00	SPERRY-SUB TESTS.
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R ASY 0.00 0.00 NO ASSAY RESULTS FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-7N-AG-BA STE DEPOSIT YUKON

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 78-DH030	COLLAR ELEVATION: 1261.76	AZIMUTH(DEG) : 177.00	GEOLOGGED BY : PCH +
TOTAL DEPTH/LENGTH : 257.56	NORTHING(= IF S): 7002417.00	VERTICAL ANGLE : -51.00	DATE (YY/MM/DD): 811031
CORE/HOLE DIAMETER : 40	EASTING (= IF N): 436480.56	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S1

SED. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	15.24	166.00	-50.00
2	30.48	166.00	-49.50
3	60.96	169.00	-48.50
4	91.44	168.00	-48.00
5	121.92	166.50	-47.00
6	152.40	170.00	-44.17
7	192.88	172.00	-42.75
8	213.36	169.00	-41.17
9	257.56	170.00	-40.00

R HED ORIGINALLY LOGGED BY DR K.L.LU - J.D ROWE IN JUNE 1978

R HED 78-DH030 SOUTH ZONE DISCOVERY HOLE!

R HED

R HED TARGET: THE TARGET WAS SELECTED ON THE BASIS OF GEOLOGICAL AND

R HED GEOCHEMICAL INTERPRETATION. EVIDENCE OF MULTIPLE

R HED SULPHIDE DEPOSITIONAL EVENTS WAS OBSERVED IN 77-DH020

R HED GALENA FRG'S WERE NOTED IN SLUMP BRECCIAS. ANOMALOUS BA/

R HED RE GEOCHEM VALUES FROM BECKER OVERBURDEN PROFILES ALSO

R HED INDICATED A SECOND SOURCE OTHER THAN THE MAIN ZONE

R HED HORIZON. THESE RESULTS INFLUENCED THE PLANNING OF THE

R HED 1978 EXPLORATORY DRILLING PROGRAM, SUCCESSFULLY PROVING

R HED THE EXISTENCE OF A NEW ZONE (COMMUNICATIONS WITH DR.K.LU)

R HED RESULTS: THE MINERALIZED ZONE WAS ENCOUNTERED FROM 183.93 M TO

R HED 186.05M

R HED TRUE THICKNESS: 1.8M

R HED WEIGHTED AVERAGES: 3.75% PB

R HED 21.26% ZN

R HED 1.70 OZ/T AG

R HED AVERAGE CORE RECOVERY= 94.6%

R HED

R HED MINERALIZATION:

R HED

R HED THE ORE ZONE CONSISTS OF MASSIVE SPHALERITE, PYRITE + GALENA

R HED WITH RICHEST CONCENTRATIONS IN THE UPPER PART OF THE ZONE. THE

R HED LOWER PART OF THE ZONE IS MORE LAMINATED WITH A HIGHER CHERT,

R HED ARGILLITE CONTENT. THE ENTIRE ZONE IS CHARACTERIZED BY SOFT

R HED SEDIMENT DEFORMATION FEATURES

R HED

R HED GEOLOGICAL CORRELATIONS:

R HED

R HED A DERRIS FLOW MEGASEQUENCE (DF) HAS BEEN IDENTIFIED FROM 57.25

R HED TO 132.36M THESE MASS FAILURE DEPOSITS APPEAR TO BE THE RESULT

R HED OF EPISODIC SEISMIC SHOCKS REACTIVATING THE SCARP MARGIN, IN

R HED CONTRAST TO THE QUIESCENT SULFIDE POOLING ENVIRONMENT IN PLACE

R HED BEFORE DISTURBANCE

R HED

R HED THE FOLLOWING CORRELATIONS IN FOOTNALL ALTERATION STRATIGRAPHY

R HED BETWEEN DDH 30 & 41 ARE OBSERVED

DDH 41

123.30-126.40M

118.87-123.30N

82.30-118.87A

LI D+

1 2 3 4

[illegible]

	Top of Bed (ft)	Base of Bed (ft)	Thickness (ft)	Bedrock Unit	Stratigraphic Unit	Grain Size	Bedding Type	Bedding Orientation	Bedding Color	Bedding Description	Bedding Notes
/	56.40	56.40	0.00	X ARSI	SSI LN			R	1 BD	40	LI D+
X UDF	57.25	57.25	0.00								
/	57.25	62.75	5.50	BRHT	*S+			OP8	P		
L							+	LN2			
/	62.75	67.75	5.00	BRHM				NS9	P		
L								0			
/ SHR	64.70	66.00	1.30	X BRHT	GG3			MO8	R		
L				3A				LN2			
/	67.50	67.75	0.25	X VETN	GG2				R		V8
L											
/	67.75	70.00	2.25	CGSN PY	SN3 FU BS H L 6 0			P			C+
L					OR 77 6			C	8		
R	67.75	70.00		COMPLETE BOUMA SEQUENCE TAE FU CYCLE SHOWING DISORGANIZED							
R	67.75	70.00		REDDING TO COARSE PEBBLES AT BASE TO PLANAR LAM SANDS NEAR TOP							
/	70.00	73.65	3.65	CGSN	SN2 MX	H L 8 N		P			
L						5		C	9		
R	70.00	73.65		BOUMA SEQUENCE TAE CYCLE							
/	73.65	76.60	2.95	CGPS	SN6 RU G; H L 3 0			P			
L					M: 5			C			
R HLT	73.65	76.60		CHARACTERIZED BY WELL ROUNDED ARG CLASTS + WISPY IRREGULAR RIPUP							
R	73.65	76.60		CLASTS COARSENING UPWARD NEAR UPPER PART OF CYCLE							
/	76.60	86.20	9.60	BRHT	*S1			OS7	P		<+
L						1 1		MO3			
/ FRG	79.35	80.10	0.75	X CGXX	SN3	H L 6 M		R			
L						6		0			
/	86.20	98.20	12.00	BRHM				PT9	P		
L				510		2		C MM)			
/ FRG	90.70	92.20	1.50	X ARSI					R		
L											
/ FRG	94.40	95.50	1.10	X ARSI					R		
L											
/	98.20	106.10	7.90	BRHM				OP9	P		L*
L						2		LN=			
/	106.10	110.20	4.10	BRPM				OP6	P		
L				710		3		0 LN3			

G F O L D G		K F F R O M - T O - I N T R E C O V		R D % R O C K T X T M N M 1 T X T X F C % M A R G		R I 1 I D A Z M D I P Q Z F L C Y C A B A X X P Y C P G L Y Y A 1 A 2	
F - L -		R D D A G E E V R R L C T X Q Q 2 T X T X S C O D C H T		2 I D A Z M D I P M G M U C L S D Q S H A P R M T S L H A			
Y G							

R	216.00	224.90		MODERATELY FRACTURED-LOCAL CONCENTRATIONS OF DISS PY(10%)+CP(2-3			
R	216.00	224.90		%) FROM 221.50-223.00			
/	217.60	217.60	0.00	X ARGL SF	ST GR	R 2 BD	59 <)
/	221.00	221.00	0.00	X ARGL SF	ST GR	R 2 BD	68 <)
/	224.90	228.40	3.50	MISS P			
R EDT	224.90	228.40		DISCONTINUOUS PGI -- ENTERED AS MISSING (22490-22840)			
/	228.40	237.10	8.70	SILT CR SF	2 2 - 2	P	D)
L				4A PY			
R	228.40	237.10		DISTURBED BEDDING			
/	231.65	234.40	2.75	X BRHM	*S+	NP9 R	C*
L				MN=			
R	231.65	234.40		FINE NETWORK OF QZ + 50 FT WHITE MINERAL (CLAY-SERICITE?)			
/	237.10	240.90	3.80	BRHT SF	S*1	DS7 P	
L				2 MO1			
R	237.10	240.90		CHAOTIC ASSORTMENT OF CARB SLST X SIF ARGL CLASTS			
/	240.90	252.65	11.75	SILT SD SF	2 2 - 2	P BD	45 <)
L				BR			
/	246.60	246.70	0.10	X FAUL	GG3	R	<=
L				*S2			
/	252.65	255.10	2.45	BRHT CR SF	*S2	DS7 P	<)
L				MO1			
R	252.65	255.10		LARGEST CLASTS CONSIST OF CARB ARGL (STRONGLY SIF)			
/	255.10	257.56	2.46	SAND // SF GG=	4 4 - 4	P SH	<)
L				4 BD U30			
R	255.10	257.56		A FEW BANDS OF MOO-SIF ARGL CLASTS, UP TO 10CM TH WITH INTERLAM			
R	255.10	257.56		PY 3 TO 5% RU CLASTS IN SS			

A DMM				SAMPLE	% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	HASH
A TYP					H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					NA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = PONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = NET ANALYSIS.									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	181.50	183.93	111	12332	0.30	0.31	-0.1	0.14	-0.1	-0.1	-0.1	-0.1	0.25
A 001	185.93	185.32	125	12333	5.80	26.05	-0.1	1.88	-0.1	-0.1	-0.1	-0.1	31.23
A 001	185.32	185.81	049	12334	4.50	15.20	-0.1	1.69	-0.1	-0.1	-0.1	-0.1	21.19
A 001	185.81	186.05	024	12335	1.29	5.93	-0.1	0.72	-0.1	-0.1	-0.1	-0.1	7.44
A 001	186.05	187.91	165	12336	0.06	0.06	-0.1	0.07	-0.1	-0.1	-0.1	-0.1	-0.31
A MAX	181.50	187.91	474		4.80	26.05	-0.1	1.88	-0.1	-0.1	-0.1	-0.1	32.13

A MIN				0.06	0.06	-0.1	0.07	-0.1	-0.1	-0.1	-0.1	-0.21
A CMP	183.93	186.05	198	3.75	21.26	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	24.41

S E D L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-2N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 78-08031
TOTAL DEPTH/LENGTH : 619.35
CORE/HOLE DIAMETER : 4330COLLAR ELEVATION: 1186.89
NORTHING(- IF S): 7002298.00
EASTING (- IF N): 436849.19AZIMUTH(DEG) : 4.00
VERTICAL ANGLE : -70.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	15.24	4.00	-72.00
2	30.48	4.00	-70.00
3	45.72	360.00	-70.00
4	60.96	8.00	-70.00
5	76.20	13.00	-69.75
6	91.44	14.00	-69.50
7	106.68	10.00	-70.00
8	121.92	14.00	-69.75
9	137.15	21.00	-71.00
10	152.40	27.00	-71.25
11	167.64	30.00	-71.00
12	182.88	34.00	-72.00
13	213.36	38.00	-70.00
14	243.84	47.00	-68.00
15	274.32	46.00	-66.00
16	304.80	49.00	-66.00
17	335.28	53.00	-65.00
18	365.75	54.00	-62.00
19	396.24	55.00	-56.00
20	426.72	52.00	-53.00
21	457.20	54.00	-52.00
22	487.68	55.00	-50.00
23	518.16	54.50	-49.00
24	548.64	53.00	-44.00
25	579.12	54.00	-45.00
26	619.35	52.00	-43.00

R HED HQ CORE FROM 0-537.6M; NN CORE FROM 537.6-619.35M.

F	- I N T E R V A L -	CORE	T- 2	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K L	(UNITS = . DEC.PLACE)RECDV-	M M	ROCK	FYING MIN	TURES CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E A	(MT=METRIC FT=FOOTRIC) ERY	Q I	TM TM	MAT TX TX	F C % M ARG	/RI T	ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y G	F R O M - T O - I N T (.)	D X	TYPE	1 2 QM1	1 2 F F C A	1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K F		ROCK	FM	RT	TM QM2 TX TX	S C O O	CHT	T ID STK DIP MG MU CL SD QS HA PR MT SL HA		
E L		QAL	AGE	ER- Q LC- 3	3 4 D	/	2	AZM RT H H H H H H H H H H	1 1	
Y G		DESIG	VIR	COL	R	C	STRUCTUR-2	A A A A A A A A A A	2 2	

R SVY 0.00 0.00 ALL TESTS DONE WITH SPERRY SUP.

R ASY 0.00 0.00 NO ASSAYED "ORE" HORIZON IN THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-2N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILL HOLE/TRVERSE : 78-04032	COLLAR ELEVATION: 1240.15	AZIMUTH(DEG) : 180.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 121.92	NORTHING(- IF S): 7602334.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : HQ	EASTING (- IF W): 436489.19	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	177.00	-52.00
2	60.96	173.00	-49.00
3	91.44	170.00	-44.00
4	121.92	170.00	-44.00

F - I N T E R V A L -		CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY	
K L (UNITS = . DEC.PLACE)RECDV=	M M	ROCK	RYING	MIN	TURES	CHARACS		H H H H H	ANY	H H H	ANY	ALT ORE	
E A (MT=METRIC FT=FOOTRIC)	ERY	D I	TX TX	4AT	TX TX	F C % M ARG	/RI T	ID	STK	DIP	A A A A A	MIN A A A MIN - - -	
Y G F R D 4 - T D - I N 1 (.)	D X	TYPE	1 2	Q1	1 2	F F C A	1	AZM	RT	QZ	FL	CY CA BA XX PY CP GL YY A 1 A 2	

K F	ROCK	FM	RT	14	Q2	TX TX	S C D D	CHT	T	ID	STK	DIP	MG MU CL SD QS HA PR MT SL HA
E L	QUAL	AGE	EN- D	LC- 3	3	4 D	/	2	AZM	RT	H H H H H	H H H H H	1 1
Y G	DESIG	VIR	COL						STRUCTUR-2	A A A A A	A A A A A	2 2	

R SVY 0.00 0.00 ALL TESTS DONE WITH SPERRY SUN.

R ASY 0.00 0.00 NO ASSAYS OF "ORE" ZONE IN THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASOP PB-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRVERSE : 78-04033

COLLAR ELEVATION: 1246.31

AZIMUTH(DEG) : 180.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 154.53

NORTHING(= IF S): 7002368.00

VERTICAL ANGLE : -62.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 80

EASTING (= IF W): 436380.75

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

SER. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	30.48	172.00	-64.00
2	60.96	176.00	-63.00
3	91.44	179.00	-62.00
4	121.92	179.00	-62.00
5	152.40	179.00	-61.00

F - I N T E R V A L -		CORE	T- %	TYPE	QUAL	TEX	GRAIN	PGI	STRUCTUR-1		ALTERATION MINS				ORE-TYPE MINS				SUMMARY														
K	L (UNITS = . DEC. PLACE)	RECOV-	M	M	ROCK	FR	IN	AT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-
E	A (MT=METRIC FT=FOOTRIC)	ERY	O	I																													
Y	G F R D M - T O - I N T (.)	D	X	TYPE	1	2	Q	M	1	2	F	F	C	A																			
K	F	ROCK	FR	RT	TE	Q	M	2	TX	TX	S	C	O	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA			
E	L	QUAL	AGE	EN	Q	LC	3		3	4	H				/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1	
Y	G	DESIG	VTR	COL							R				C			STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 SPERRY SON TESTS.

R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE.

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

FORMAT VERSION : 6B02

GEOLOGGED BY : BHO +
DATE (YY/MM/DD): 811014
PROJECT NUMBER : J-MAIN

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.48	6.00	-56.00
2	60.96	9.00	-56.00
3	91.44	12.00	-54.00
4	121.92	13.00	-53.00
5	152.40	16.00	-52.00

[illegible]

K	F	- I N T E R V A L -	CORE	T- Z	TYPE-	QUAL	TEX-	GRAIN		PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
E	A	(UNITS = . DEC.PLACE) RECUV-	M M ROCK	FYING MIN	TURES	CHARACS					H H H H H ANY H H H ANY	ALT ORE				
Y	G	(MT=METRIC FT=FOOTRIC) ERY	D I	TM TM MAT TX TX F C % M ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -								
		F R U N - I D - I N T (.)	D X TYPE	1 2 QM1	1 2 F F C A						1 AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2				
K	F		ROCK	FM	RT	TM	QM2	TX TX S C D D CHT			T ID STK DIP MG MU CL SD QS HA PR MT SL HA					
E	L		QUAL	AGE EN- D	LC- 3		3 4 D /				2 AZM RT H H H H H H H H H H	1 1				
Y	G		DESIG	VIR	COL		R C				STRUCTUR-2 A A A A A A A A A A	2 2				

R SVY 0.00 0.00 SPERRY SUN TEST RESULTS.

OVER	0.00	24.33	24.33	OVER	P
------	------	-------	-------	------	---

/	24.38	69.76	45.38	ARGL	SI+ LN	0 1 + 1	P 1 LM	65 <-	C.	L+ <.	<.
L				3A CR			CV	30	<*		<

R	24.38	69.76	SIDERITE, QUARTZ-SIDERITE VEINS RANGE UP TO 1CM. THEY CONTAIN
R	24.38	69.76	TRACES OF THE ABOVE MINERALS. THESE VEINS OCCUR BETWEEN 27.00
R	24.33	69.76	TO 32.00 METERS, 39.00 TO 41.00 METERS AND 68.00 TO 69.00
R	24.38	69.76	PYRITE LAMINATIONS AVERAGE A WIDTH OF 1 TO 2MM. CARBONEOUS
R	24.38	69.76	LOCALLY.

/ SHR	33.53	69.75	36.23		X	ARGL	GR	CR	SI+	LM	0	1	+	1		R	1	LM	65	<-		C.	L+	<.	<.
-------	-------	-------	-------	--	---	------	----	----	-----	----	---	---	---	---	--	---	---	----	----	----	--	----	----	----	----

R	33.53	69.76	THE WHOLE INTERVAL APPEARS TO BE SHEARED AND FRACTURED. THE
R	33.53	69.76	ZONE BETWEEN 40.15 AND 59.59 METERS IS BROKEN UP THE MOST. IN
R	33.53	69.76	PLACES THE CORE IS BROKEN UP TO A RUBBLE, PEBBLE SIZE FRAGMENTS.
R	33.53	69.76	AXIAL PLANE CLEAVAGE IS WILL DEFINED THROUGHOUT THE INTERVAL.

Z	69.76	78.14	8.38	ARSI	SI= LM	0 2 = J	P 2 BD	60 <.	C.	L)	<.
L				3A	SN)	SS			<*		<.

R	69.76	78.14	THE SOFT SEDIMENT DEFORMATION FEATURE OCCURS NEAR THE BASE OF
R	69.76	78.14	THE INTERVAL. THE BEDDING ANGLE VARIES FROM 50' TO 70'.
R	69.76	78.14	POSSIBLE DUE TO MINOR SLUMPING.

[illegible]

/ FLT	72.70	72.95	0.25	X ARSI CR GR GG9				R				D)		
L														
/ FSX	78.14	78.78	0.64	BRHM	*S2 SS		ND6	P	<	L-		L*		
L						4 2				L-		L*		
R	78.14	78.78		THIS INTERVAL IS AN ARSI WHICH AS BEEN BRECCIATED DUE TO SOFT										
R	78.14	78.78		DETERMINATION SULPHIDES ARE CONCENTRATED NEAR THE BASE. IT IS										
R	78.14	78.78		LAMINATED AND SOMEWHAT CONFORMABLE WITH THE ORIGINAL BEDDING.										
R	78.14	78.78		THESE SULPHIDES OCCUR IN LENTICULAR FRAGMENTS DUE TO										
R	78.14	78.78		SYN-TECTONIC DEFORMATION.										
/	78.78	80.30	1.52	SAND	SN7 MS	0 3 4 L	P		V+	C-	D)	B+		
L				8A	SI1	BS				V+		L)		
R	78.78	80.30		THE UNIT APPEARS TO GET COARSE GRAINED TOWARDS THE TOP GALENA IS										
R	78.78	80.30		COARSE GRAINED IN VUGS.										
K LM1	79.20	79.20	0.00											
/	80.30	81.90	1.60	BRHM	S02 SS LM		NS7	P 1 LM	75		C.	D)	L)	
L				4A CR	*S=	LC 4	= 0			L-		L+		
R	80.30	81.90		THE BEDDING IS DEFINED AT THE TOP BUT IT BECOMES PROGRESSIVELY										
R	80.30	81.90		MORE DISTURBED TOWARDS THE BASE. THE UNIT IS A ARSI THAT HAS										
R	80.30	81.90		BEEN BRECCIATED DUE TO SLUMPING. BARITE APPEARS TO COAT THE										
R	80.30	81.90		SPHALERITE.										
/	81.90	84.53	2.63	SAND SF	S07 SS MX	0 3 5 0	P		>1	C.	D)	D+		
L				8A	SI1					<)		D*		
R	81.90	84.53		TIS SANDSTONE IS LOCAALLY BRECCIATED. QUARTZS VEINS RANGE UP TO										
R	81.90	84.53		10CMS. SANDSTONE CONTAINS DISSEMINATED GRAINS OF GALENA, PYRITE										
R	81.90	84.53		AND MINOR SPHALERITE. GALENA RANGES FROM A FINE DISSEMINATION										
R	81.90	84.53		TO COARSE GRAINED CRYSTALS. THERE IS ALSO A MINOR SHEAR IN THIS										
R	81.90	84.53		UNIT.										
/ FLT	84.43	84.53	0.10	X SAND GR CR GG6				R	<-		D)	D.		
L												D.		
K LM1	84.53	84.53	0.00											
/	84.53	87.17	2.64	BRHM SF	SN3 SS SC		MR5	P BD	75		C.		D.	
L				5A CR	*S=	LC 4	= 0 LM+					D.		
R	84.53	87.17		THIS UNIT IS MAINLY A ARSN BUT IS LOCALLY BRECCIATED DUE TO SOFT										
R	84.53	87.17		SEDIMENT DEFORMATION. TH BOTTOM 2 METERS IS LESS DISTURBED THAN										
R	84.53	87.17		THE UPPER PART. THERE IS ONE CPG FRAGMENT AT 85.45 METERS.										
/	87.17	89.60	2.43	ARSI	SI1 SS SC	0 1 1 E	P 1 LM	70		D.	D*	D.		
L				4A	LM					L-				
/ SHR	88.85	89.60	0.75	X ARSI GR				SI1 SS SC	0 1 1 E	R 1 LM	70	D.	D*	D.
L				4A CR	LM									
R	88.85	89.60		THIS INTERVAL IS MODERATELY SHEARED AND THE CORE IS RUBBY.										

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/ FRG 116.33 116.96 0.63 X ARSJ SI= SS SC R 1 LM 80 0)
L 3A GR SP+

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R	116.33	116.96		THIS LARGE ARSI FRAGMENT IS LIGHTLY SHEARED AND FRAGMENTED.											
/	116.96	120.54	3.58	SAND	SF	SN7	H*	0	4	5	I	P	<*	D+	
L				QA		SIP		7						D-	
/	117.65	118.05	0.40	X BRHT		SM1	F*	H*				L03	R	D)	
L				KA		*C1		3				K05			
/	120.54	142.70	22.16	BRHT		SM1	F*	H*				K04	P	D)	
L				KA		*S= SS		4				K04		D-	
R	120.54	142.70		THIS PGI IS LIGHTLY SHEARED AND FAULTED WITH NUMEROUS QUARTZES											
R	120.54	142.70		VEINS. IT CONTAINS POSSIBLE FRAGMENTS OF SAND AND ARSN. DUE TO											
R	120.54	142.70		THE HIGHLY DISRUPTED NATURE OF THE UNIT, IT IS VERY DIFFICULT TO											
R	120.54	142.70		TELL IF THEY ARE DEPOSITIONAL OR NOT.											
/	122.60	126.30	3.70	7 VEIN SF		*C1	F*	H*				L01	R	D)	
L				AM								K01		B+ D*	
R	122.60	126.30		THIS LARGE QUARTZ VEIN HAS APPROX. 30% BRHT INCORPORATED INTO											
R	122.60	126.30		IT. SERICITE OCCURS AS BLENDS OR PATCHES WITHIN THE VEIN.											
/	133.25	136.55	3.30	X BRHT		GGS	F*	H*				K04	R	D)	
L															
/	136.55	139.20	2.65	X ARSN		SM3	SS	SC				033	R	B)	
L				SA		SI=								D)	
R	136.55	139.20		SIDERITE OCCURS INTERSTITIALLY WITHIN THE SAND RICH LAYERS.											
R	136.55	139.20		BEDDING ANGLE CHANGES DRAMATICALLY.											
/	142.70	146.70	4.00	ARSI		SI1	SS	SC				P	2 BD	D)	
L				KA		SN=								D*	
R	142.70	146.70		THE BEDDING IS LOCALLY DISRUPTED DUE TO SLUMPING. THE BEDDING											
R	142.70	146.70		ANGLE VARIES FROM 40' TO 50'. THERE IS A 30CM THICK SAND UNIT											
R	142.70	146.70		STARTING AT 145.70M. IT SHOWS NORMAL GRADING AND IS POSSIBLY A											
R	142.70	146.70		FRAGMENT.											
/	146.70	152.30	5.60	BRHT		SM1	SS	F*				LR4	P	D)	
L				SA		*C1	H*	3				K03		D*	
/	152.30	154.22	1.92	ARSI		SI1	SS					P	2 LM	D)	
L				KA									CV	<	
R	152.30	154.22		THE FIRST METER IS FOLDED AND HAS A STRONG AXIAL PLANE CLEAVAGE.											
R	152.30	154.22		THE UNIT IS MODERATELY BROKEN UP AS A RESULT. THERE ARE SEVERAL											
R	152.30	154.22		MINOR SHEAR ZONES.											

A UMM	SAMPLE	% PB	% ZN	% RA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP	NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 RA = WET ANALYSIS.

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	77.20	78.20	92	12379	0.22	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.34
A 001	78.20	79.20	100	12380	0.34	0.56	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.30
A 001	79.20	80.20	97	12381	2.50	1.65	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.55
A 001	80.20	81.20	72	12382	0.26	0.15	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.19
A 001	81.20	82.20	100	12383	0.16	4.28	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.84
A 001	82.20	83.20	86	12384	2.25	0.53	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.18
A 001	83.20	84.20	96	12385	2.20	0.15	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.75
A CMP	79.20	84.20	447		1.47	1.35	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.22

A MIN		0.16	0.04	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.40
A MAX	17.20 84.20	2.50	4.28	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	6.18

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6802

GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

1	30.48	288.00	-52.00
2	60.96	290.00	-50.00
3	91.44	288.00	-48.00
4	121.92	285.50	-47.00

R SVY	0.00	0.00	SPERRY SUN SURVEY TESTS.
R ASY	0.00	0.00	ON ASSAYS THIS HOLE.

19 01 00

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BASIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :78-DH036
TOTAL DEPTH/LENGTH : 230.13
CORE/HOLE DIAMETER : HQCOLLAR ELEVATION: 1157.45
NORTHING(- IF S): 7002644.00
EASTING (- IF A): 437263.06AZIMUTH(DEG) : 269.00
VERTICAL ANGLE : -51.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	284.00	-46.50
2	60.96	286.00	-42.00
3	91.44	284.00	-39.00
4	121.92	287.00	-36.50
5	152.40	286.00	-35.00
6	182.88	285.50	-32.50
7	213.36	282.00	-32.00
8	230.13	281.00	-31.50

F - I N T E R V A L -		CORE	T- %	TYPI- GAL		TEX- GRAIN	PGI	STRUCTUR-1		ALTERATION MINS					ORE-TYPE MINS					SUMMARY						
K	L (UNITS = . DEC.PLACE)	RECOV-	N M ROCK	RYING MIN	TURES	CHARACS				H	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE					
E	A (MT=METRIC FT=FOOTRIC)	ERY	0 1	TA TM MAT	TX TX	F C % M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	- - -			
Y	G F R O M - T O - I N T (.)	U X TYPE	1 2 DM1	1 2	F F C A			1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
K	F	ROCK	FM	RT	TM	DM2	TX TX	S C O	0	CHT			T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA
E	L	DUAL	AGE	ED- 0	LC- 3		3 4 0	/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1
Y	G	DESIG	VTR	COL			R	C			STRUCTUR-2		A	A	A	A	A	A	A	A	A	A	A	A	2	2

R SVY 0.00 0.00 SPERRY SUN TEST RESULTS

R ASY 0.00 0.00 NO ASSAY RESULTS FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-2N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 74-DH037	COLLAR ELEVATION: 1158.98	AZIMUTH(DEG) : 90.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 54.86	NORTHING(- IF S): 7002644.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : 80	EASTING (- IF W): 437249.31	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	89.00	-48.00
2	54.86	84.00	-46.00

F	- I N T E R V A L -	CORE	T - %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)RECOV-	M M	ROCK	RYING MIN	TURES CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E	A (MT=METRIC FT=FOOTRIC) ERY	G I		TO IN MAT	TX IX F C % M ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y	G F R O M - T O - I N T (.)	D X	TYPE	1 2 QM1	1 2 F F C A	1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
-	- - - - -	-	-	-	-	-	-	-	-	-
K	F	ROCK	FR	RT	TX TX S C O O CHT	T	ID STK DIP	MG MU CL SD QS HA PR MT SL HA		
E	L	DUAL	AGE	FR- 0 LC- 3	3 4 0 /	2	AZM RT H H H H H H H H H	1 1		
Y	G	DESIG	VIR	CUL	H C		STRUCTUR-2	A A A A A A A A A	2 2	

R SVY 0.00 0.00 SPERRY SUR TEST RESULTS.

R ASY 0.00 0.00 NO ASSAY RESULTS FROM THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASON PB-ZB-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 78-DH036
TOTAL DEPTH/LENGTH : 30.40
CORE/HOLE DIAMETER : HQ

COLLAR ELEVATION:	1155.26
NORTHING (= IF S):	7002540.00
EASTING (= IF X):	437185.37

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AZIMUTH( DEG ) : 344.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTM

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GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

K	F	- I N T E R V A L - C O R F	T = %		TYPT=	DAL	TEX=	GRAIN	
E	L	(UNITS = . DEC.PLACE) RECV-	R M ROCK		FYING	MIN	TURES	CHARACS	
Y	G	(AT=METRIC FT=FOOTRIC)	BRY	O I	TM TM	MAT	TX TX	F C % M	ARG
		F R D M - T D - I N T (.)	O X TYPE		1 2 DM1		1 2	F F C A	
<hr/>									
K	F		ROCK	FM	RT	TD	DM2	TX TX	S C O O CHT
E	L		QUAL	AGE	ED- Q	LC- 3		3 4 O	/
Y	G		DESIG		VIR	COL		R	C

PGI	STRUCTUR-1				ALTERATION				MINS				ORE-TYPE				MINS				SUMMARY	
/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	A	MIN	-	-	-	-	ALT	ORE	
1			AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				

2			AZM	RT	H	H	H	H	H	H	H	H	H	H	1			1				
			STRUCTUR-2				A	A	A	A	A	A	A	A			2		2			

R SVY	0.00	0.00	DO DOWN HOLE SURVEY.
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R ASY 0.00 0.00 NO ASSAY RESULTS FOR THIS HOLE.

01163 BT M.B.F.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASCO PR-70-4G-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 75-04-039	COLLAR ELEVATION : 1156.61	AZIMUTH(DEG) : 164.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 58.58	NORTHING (- IF S) : 7002563.00	VERTICAL ANGLE : -45.00	DATE (YY/MM/DD) : 0
COREHOLE DIAMETER : 00	EASTING (- IF E) : 437179.81	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	159.00	-42.00
2	45.72	156.00	-42.00
3	68.58	156.00	-41.00

F - INTERVAL - CORE		I - %		TYPICAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION MINS		ORE-TYPE MINS		SUMMARY														
K	L (UNITS = . DEC.PLACE)	RECOV-	N X ROCK	FT/IN	MAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-
E	A (MT=METRIC FT=FOOTRIC)	ERY	D I	1	2	0	1	1	2	F	F	C	A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
Y	G FROM - TO - INT (.)	D X	TYPE	1	2	0	1	1	2	F	F	C	A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
K	F	ROCK	FM	RT	1	2	0	1	1	2	F	C	A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	L	QUAL	AGE	EN- G	IC- 3			3	4	0	/			2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1
Y	G	DESIG	VIR	COL				R	C					2	STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	A	2	2

R SVY 0.00 0.00 SPERRY SUR TEST RESULTS.

A UMM				SAMPLE	% PR	% ZK	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BORDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	29.50	30.50	53	12483	0.02	0.23	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.35
A 001	30.50	31.85	117	12484	0.02	0.10	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.48
A 001	31.85	32.93	92	12485	0.04	0.51	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.05
A 001	32.93	33.95	69	12486	0.03	4.30	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.73
A 001	33.95	34.59	49	12487	0.14	4.15	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.68
A 001	34.59	35.66	94	12488	0.05	5.70	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	5.15
A 001	35.66	36.74	89	12489	0.04	4.70	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.14
A 001	36.74	37.45	54	12490	0.12	8.28	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	7.80
A 001	37.45	39.05	80	12491	0.11	4.20	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.71
A 001	39.05	40.00	52	12492	0.38	4.51	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.29
A 001	40.00	41.22	84	12493	0.36	4.95	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	4.71
A 001	41.22	42.73	141	12494	0.12	0.50	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.02
A 001	42.73	44.10	102	12495	0.45	3.68	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.53
A 001	44.10	44.50	14	12496	0.15	1.54	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.09
A 001	44.50	45.52	97	12497	0.17	3.17	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	2.74
A 001	45.52	46.33	59	12498	0.06	0.83	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	0.29
A 001	46.33	47.75	121	12499	0.14	1.52	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.06
A CMP	32.93	45.52	934		0.18	4.05	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	3.63

A MIN			0.02	0.10	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.48
A MAX	29.50	47.75	0.45	8.28	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	8.13

100% BY N/A

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAW OCEAN OIL LTD.

JASON PB-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :78-0H000
TOTAL DEPTH/LENGTH : 97.50
CORE/HOLE DIAMETER : 40COLLAR ELEVATION: 1155.87
NORTHING(- IF S): 7002489.00
EASTING (- IF W): 437168.31AZIMUTH(DEG) : 56.00
VERTICAL ANGLE : -55.00
COORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	55.00	-54.00
2	60.96	54.00	-51.00
3	96.01	51.00	-48.00

F	- I N T E R V A L -	CORE	1- %	TYPE	QUAL	TEX-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																			
K	L (UNITS @ . DEC.PLACE)	RECOV-	M M	ROCK	FYING	MIN	TURES	CHARACS		H	H	H	H	ANY	H	H	H	ANY	ALT	ORE													
E	A (MT=METRIC FT=FOOTRIC)	ERY	0	I	TX	TX	MAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G F R O N - I D - I N T (.)		0	X	TYPE	1	2	QV1	1	2	F	F	C	A		1		AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
K	F	ROCK	FR	RT	TX	TX	OM2	TX	TX	S	C	D	D	CH1		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1
F	L	QUAL	AGE	ER	D	LC	3		3	4	D	/																					
Y	G	DESIG	VTR	COL														STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2	

R SVY 0.00 0.00 SPERRY SUN TESTS.

A UMM				SAMPLE	% PR	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BORDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		RE ASSAY INFORMATION ENTERED AS -0.1									
A 001	81.20	82.65	79	12520	0.94	1.18	0.56	-0.1	-0.1	-0.1	-0.1	-0.1	1.28
A 001	82.65	83.00	21	12521	0.23	1.28	0.67	-0.1	-0.1	-0.1	-0.1	-0.1	1.68
A 001	83.00	84.84	136	12522	0.12	-0.1	0.47	-0.1	-0.1	-0.1	-0.1	-0.1	-0.01
A 001	84.84	84.98	11	12523	0.07	0.40	0.47	-0.1	-0.1	-0.1	-0.1	-0.1	0.44
A 001	84.98	86.10	78	12524	0.12	1.19	0.61	-0.1	-0.1	-0.1	-0.1	-0.1	1.42
A 001	86.10	87.17	73	12525	0.16	1.80	0.64	-0.1	-0.1	-0.1	-0.1	-0.1	2.10
A 001	87.17	89.61	51	12526	0.05	1.52	0.74	-0.1	-0.1	-0.1	-0.1	-0.1	1.81
A 001	89.61	90.53	6	12527	0.07	1.56	0.49	0.09	-0.1	-0.1	-0.1	-0.1	1.81
A 001	90.53	90.70	10	12529	0.03	3.52	0.03	0.44	-0.1	-0.1	-0.1	-0.1	3.62
R ASY	89.61	90.53		ASSAYS 12527 AND 12528 AVERAGED.									
A 001	90.70	91.70	78	12530	0.03	0.55	0.53	-0.1	-0.1	-0.1	-0.1	-0.1	0.61
A 001	91.70	93.00	105	12531	0.01	0.48	1.05	-0.1	-0.1	-0.1	-0.1	-0.1	1.04
A 001	93.00	94.00	83	12532	0.02	0.61	1.01	-0.1	-0.1	-0.1	-0.1	-0.1	1.34
A 001	94.00	95.00	81	12533	0.02	0.23	1.01	-0.1	-0.1	-0.1	-0.1	-0.1	0.76

A MIN		0.01	-0.1	0.63	-0.1	-0.1	-0.1	-0.1	-0.1	-0.56
A MAX	81.20 95.00	0.23	3.52	1.05	0.44	-0.1	-0.1	-0.1	-0.1	4.84

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-BA STE DEPOSIT YUKON

FORMAT VERSION : 6B02

DRILLHOLE/TRVERSE :78-DH001
TOTAL DEPTH/LENGTH : 144.78
CORE/HOLE DIAMETER : 60COLLAR ELEVATION: 1209.67
NORTHING (- IF S): 7002206.00
EASTING (- IF E): 436465.25AZIMUTH(DEG) : 45.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810702
PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	36.58	49.00	-56.00
2	60.96	47.00	-57.00
3	91.44	46.00	-55.50
4	143.26	46.00	-53.00

R HED ORIGINALLY LOGGED BY J.D. ROWE, SEPT. 1978.

R HED TARGET: SOUTH ZONE. BENCH LEVEL 1100M TO 1080M AT 436520E

R HED 7002260M. TO DETERMINE THE EASTERN EXTENSION OF DDH 78-30

R HED MINERALIZED INTERSECTION.

R HED RESULTS: ORE GRADE MINERALIZATION WAS INTERSECTED FROM

R HED 7002259.75M 436523E BENCH LEVEL 1100M TO 7002261.5M 436524.75E

R HED BENCH LEVEL 1096M. MINERALIZATION WAS INTERSECTED FROM 133.70M

R HED TO 136.60M WITH A TRUE WIDTH OF 1.9M. WEIGHTED AVERAGES: 11.72%

R HED PB, 28.96% ZN, 3.77 OZ/TON AG. CORE RECOVERY WAS GOOD (90.37%)

R HED MINERALIZATION: MINERALIZATION APPEARS BANDED AND CONSISTS OF

R HED ZONES RICH IN SPHALERITE AND ZONES RICH IN GALENA. EXTENSIVE

R HED HANDLING OF THE CORE HAS RESULTED IN SHUFFLING OF THE PIECES,

R HED NOT ALLOWING DETERMINATION OF THE LOCATION OF THE ZONES WITH

R HED RESPECT TO ANOTHER. J.D. ROWE LOGGED A LAMINATED GALENA RICH

G E O L O G

R HED ZONE FROM 133.70M TO 135.10M FOLLOWED BY A SPHALERITE RICH ZONE

R HED FROM 135.10M TO 135.60M. THE SULPHIDES ARE INTERBEDDED WITH

R HED SILICIFIED ARGILLITE AND AN OXIDIZED POWDERY MATERIAL THAT

R HED RESPONDS LIGHTLY TO ZINC ZAP. A BRECCIATED SULFIDE ZONE OCCURS

R HED FROM 135.60M TO 136.60M CONTAINING BLEACHED CHERT FRAGS. THE

R HED HIGHEST ASSAYS: 23.35% PB, 37.09% ZN OCCURRED IN THE GALENA

R HED RICH ZONE FROM 134.40M TO 135.10M. PY OCCURS THROUGHOUT AS

R HED LAMS IN THE LAMINATED ZONE AND AS DISSEMINATIONS AND BLEBS

R HED ELSEWHERE. QIZ OCCURS AS MICROVEINS AND BLEBS. THE CORE IS

R HED POROUS DUE TO LEACHING. THE ORE ZONE IS TRUNCATED BY AN

R HED EROSIONAL EVENT WHICH DEPOSITED THE HETEROLITHIC BRECCIA (BRHT)

R HED STRATIGRAPHICALLY ABOVE IT. THIS EVENT WAS PROBABLY

R HED RESPONSIBLE FOR THE BRECCIATION IN THE UPPER PART OF THE ZONE

R HED AND POSSIBLY FOR THE TOTAL EROSION OF THE 2 OTHER SULFIDE UNITS

R HED USUALLY FOUND IN THE SOUTH ZONE. THE CORE IS FRIABLE MAINLY

R HED DUE TO THE HIGH POROSITY CAUSED BY LEACHING.

R HED CANOL FORMATION: THE BEDS DIP VERTICALLY (70 TO 90 DEGREES)

R HED WITH TOPS DOWNHOLE IE TO THE NORTHEAST. 22.86M OF OVERBURDEN

R HED PRECEDES A SANDSTONE WITH INTERBEDDED SILTY ARGILLITES THAT

R HED CONTINUES TO 28.00M. THIS IS FOLLOWED BY AN ARGILLITE AND AN

R HED ARSI DOWN TO 56.39M. A FEW MINOR FAULTS AND SHEARS CUT THROUGH

R HED THE ABOVE UNITS. A STRONGLY CARBONACEOUS SILT SHEARED LOCALLY

R HED BETWEEN 69.60M TO 75.80M OCCURS FROM 56.39M TO 83.00M. THIS

R HED SHEAR CAN BE CORRELATED TO A SURFACE FAULT STRIKING 130 DEGREES

R HED AND DIPPING VERTICALLY. WHEN SHEARED, THIS UNIT TURNS TO A

R HED FINE GRAINED MATERIAL SIMILAR TO UNLITHIFIED SILT. MAJOR

G E O L O G

R HED PRIMARY TEXTURES ARE OFTEN PRESERVED EVEN THOUGH SHEARING HAS
R HED REDUCED THE ROCK TO POWDER. STRATIGRAPHICALLY UPSECTION, A

R HED SILICIFIED ARGILLITE WITH UNSILICIFIED CARBONACEOUS STYLOLITES
R HED CONTINUES DOWN TO 118.87M. IT IS NOTEWORTHY THAT SIDERITE AS
R HED MICROVEINS AND DISSEMINATIONS INCREASES DRAMATICALLY IN

R HED COINCIDENCE WITH SILICIFICATION. AN INTERESTING ALTERATION
R HED ZONE OCCURS FROM 118.87M TO 123.30M. IT CONSISTS OF
R HED LAMINATED CHERT (SIF ARGILL?) INTERBEDDED WITH HEAVILY

R HED SIDERITIZED LIGHTLY CARBONACEOUS ARGILLITE OVERLAIN BY THE SAME
R HED ARGILLITE CONTAINING BRECCIATED FRAGMENTS OF SILICIFIED
R HED ARGILLITE. THE MAJORITY OF THESE CLASTS ARE CONCENTRATED FROM

R HED 121.25M TO 122.05M AND HAVE BEEN REBRECCIATED BY SIDERITE,
R HED PYRITE AND GALENA (2 %). THE CARBONACEOUS ARGILLITE MATRIX
R HED MATERIAL APPEARS TO BE RESISTANT TO SILICIFICATION. THIS MAY

R HED COMPRISE A FEEDER PIPE. DOWNHOLE, FROM 123.30M TO 133.70M.
R HED THERE IS A SILICIFIED LAMINATED ARGILLITE AND A BRHM FOLLOWED
R HED BY THE ORE ZONE DESCRIBED ABOVE. THE ORE ZONE APPEARS TO HAVE

R HED BEEN FORMED BY A GRAVITY FLOW THAT DEPOSITED THE BRHT
R HED UPSECTION.

R HED CONCLUSION: THE HOLE WAS SUCCESSFUL BECAUSE IT EXTENDED THE

R HED ORE BODY TO DEPTH BY 25M AND TO THE SOUTHEAST BY 65M AND

R HED CONFIRMED THE FINDINGS OF DDH 78-30.

F - I N T E R V A L -		CORE	T - %	TYPE - GAL	TEX - GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY															
K	L (UNITS = . DEC. PLACE)	RECOV -	M M	ROCK	FYING MIN	TURES	CHARACS																				
E	A (MT=METRIC FT=FOOTRIC)	ERY	0 1		TX TX	TX TX	F C % M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G F R D N - 1 0 - 1 0 1 (.)	U X	TYPE	1	2	QM1	1	2	F F C A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2

K	F	ROCK	FR	RT	TX	TX	S C O O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L	QUAL	AGE	ED	LC	3	3	4	0	/	2	AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G	DESIG	VTR	CHL			R	C																2	2		

R SVY 0.00 0.00 ALL SPERRY-SUN SURVEY DATA.

/ 0.00 22.86 22.86 OVER P

/ 22.86 28.00 5.14

SAND

6A

SI/ AX IR A H 5 J

R

P 4 80

70 <*

D)

B*

R	22.86	28.00		SILICEOUS MATRIX. INTERBEDDED WITH FAINTLY CARBONACEOUS ARGL						
R	22.86	28.00		UNITS REPEATED BELOW. ARST CORE BROKEN UP.						
/	25.20	24.98	0.88	X ARST CR	ST)	A D + H	R	1 LM	70	
L				2A	SN+					
R	23.20	24.68		CORE BROKEN UP						
/	25.40	25.41	0.01	X OVER			R			
L										
/	26.20	26.35	0.15	X ARST CR	SN= MX LM A G = G		R	1		
L				2A						
R	26.20	26.35		CONVOLUTED BARCASITE VEINLETS 1MM THICK.						
/	26.60	26.80	0.20	X ARGL	MX	A A A	R			
L				2A						
/	27.13	27.43	0.30	Y ARST	ST) LM	A G = G	R	2 LM	65	
L				2A	SN=					
/	28.00	45.00	17.00	ARST CR	ST) BD	A G = H	P	3 BD	65	
L				2A	SN=					
R	28.00	45.00		SAND BEDS CONTAIN FINELY DISS PY. SOME BEDS CONTAIN CROSS LAM.						
R	28.00	45.00		MAJOR BEDS DESCRIBED BELOW. FROM 28.00M TO 56.39M CORRELATES						
R	28.00	45.00		WITH DDH 78-33, 152.53M TO 142.55M X MT < DECREASES DOWNHOLE.						
/	33.20	33.24	0.04	X SHER			R			
L										
/	33.20	33.60	0.40	X SAND	MX	A F 5 H	R			
L				6A						
R	35.20	35.60		SILICEOUS MATRIX.						
/	37.20	37.37	0.07	X FAUL	GB9		R			
L										
/	41.34	41.52	0.18	X SAND	LM FH A F 3 T		R	0 LM	58	
L				5A						
R	41.34	41.52		SILICEOUS MATRIX. ARGL LAMS.						
/	45.00	56.39	11.39	ARGL	ST) MX LM A D + E		P			
L				2A	SN)					
R	45.00	56.39		LESS ST SN THAN ABOVE PGT. FROM 45.00M TO 56.39M CORRELATABLE						
R	45.00	56.39		WITH DDH 78-33, 143.55M TO 123.75M.						
/	48.30	48.55	0.25	X ARGL	MT2	A D 2 D	R			
L				4A						
/	48.30	48.55	0.25	X SHER			R			
L										
R	48.30	48.55		CORE BROKEN UP. EXACT HABIT OF MT NOT DETERMINED. BLEBS OR						

K	F	F	R	D	I	I	I	RECOV	MD	%	ROCK	TM	TM	RM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	NZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
F	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																						2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

R 48.30 48.55 DISS OR VEIN.

/ 52.10 52.30 0.20 X ARGL MT2 A D 2 L R

L 52.10 52.30 MT AS GLOBULES AND VETHELETS.

R 56.39 57.60 PROBABLY A FAULT.

/ 56.39 83.00 26.61 SILT CR1 LH A D 5 G P 0 LM 40 D)

L 56.39 83.00 26.61 SILT CR1 LH A D 5 G P 0 LM 40 D)

/ FAL 56.39 57.60 1.21 X LOST R

L 56.39 83.00 57.60M TO 82.30M CORRELATES TO DDH 78.30, 228.4M TO 237.10M AND

R 56.39 83.00 240.40M TO 252.65M. OCCASIONAL FAINT LAMS. STRONGLY

R 56.39 83.00 CARBONACEOUS.

/ SHR 56.40 61.90 5.50 X SILT CR1 A D 5 G R

L 56.40 61.90 HAS A CONSISTENCY SLIGHTLY COARSER THAN GOUGE. APPEARS

R 56.40 61.90 DELITHIFIED BUT NOT DISRUPTED.

/ FLT 69.60 69.90 0.30 X FAUL GG4 R

L 69.60 69.90 0.30 X FAUL GG4 R

/ SHR 75.10 74.00 0.90 X SHER GG1 R <=

L 75.10 74.00 0.90 X SHER GG1 R <=

/ SHR 74.67 75.99 0.42 X SHER GG3 R <1

L 74.67 75.99 0.42 X SHER GG3 R <1

/ SHR 75.66 75.80 0.14 X SHER GG6 R

L 75.66 75.80 0.14 X SHER GG6 R

/ 75.30 76.54 0.74 X SILT CR1 LM A D 5 G R 0 LM 65 <1 D)

L 75.30 76.54 0.74 X SILT CR1 LM A D 5 G R 0 LM 65 <1 D)

/ SHR 78.84 78.99 0.15 X SHER R

L 78.84 78.99 0.15 X SHER R

/ 82.30 83.00 0.70 X LOST R

L 82.30 83.00 0.70 X LOST R

/ 83.00 118.87 35.87 ARG L GR+ LM ST A A A P 0 LM 37 <= D* D.

L 83.00 118.87 35.87 ARG L GR+ LM ST A A A P 0 LM 37 <= D* D.

R 83.00 118.87 GRAPHITE OCCURS AS STYLOLITES PREDOMINANTLY PARALLEL TO BEDDING.

R 83.00 118.87 STRONGLY SILICIFIED THROUGHOUT. UNIT CORRELATES WITH DDH 78.30

R 83.00 118.87 224.90M TO 203.55M.

/ 86.96 87.12 0.16 X ARG L GR+ MX ST A I 7 K R 0 LM 37 <= D)

L 86.96 87.12 0.16 X ARG L GR+ MX ST A I 7 K R 0 LM 37 <= D)

R 86.96 87.12 VERY HIGH SIDERITE %.

R 86.96 87.12 VERY HIGH SIDERITE %.

/	118.87	119.78	0.91		CHAR SF	SIF RD EP A A	A	P	4 BD	30	D2	D+
L					GA	CHZ VG						

	Interval	Depth (m)	Grain Size (mm)	Lithology	Notes	Other	Remarks	Grade (%)	Comments
Z L	118.87 - 119.20	0.33	X ARG L	GR+ MX BR A A A R		D+	D=		
R	118.87 - 119.78		INTERBEDDED CHERT AND LIGHTLY CARBONACEOUS SILICIFIED ARG L						
R	118.87 - 119.78		BRECCIATED BY SIDERITE PYRITE. CHERT IS OCCASIONALLY POROUS						
R	118.87 - 119.78		DUE TO LEACHING OF SIDERITE.						
Z L	119.78 - 123.30	3.52	ARG L	GR+ MX BR A N P D	P	<=	D1	D+ D- D-	
R	119.78 - 123.30		LIGHTLY GRAPHITIC ARG L CONTAINING BRECCIATED SILICIFIED ARG L -						
R	119.78 - 123.30		ZONE REPEATED PELON. ARG L AND BRECCIA MATRIX ARE SIDERITIZED						
R	119.78 - 123.30		TOUGH NOTABLY UNSILICIFIED UNLIKE THE FRAGMENTS.						
Z L	121.25 - 122.05	0.80	X BRXX	S01 BR A N 5 O	R		D1	#1 #* B+	
R	121.25 - 122.05		SS TEXTURES IN FRAGS INDICATE SLUMPING PRECEDED SI PY BREC.						
Z L	123.30 - 126.40	3.10	ARG L	SI/ LM ST A A A	P 0 LM	58 <=	<)	<+	
R HLT	123.30 - 126.40		UNIT CORRELATES WITH DDH 78-30, 199.35M TO 195.75M. MINOR SD						
R	123.30 - 126.40		BREC.						
Z L	126.40 - 129.90	3.50	BRHM	SD= BR NO4	P			3+	
R	126.40 - 129.90		ARG L FRAGS IN A SLIGHTLY DARKER, LIGHTLY GRAPHITIC ARG L MATRIX.				<=		
R	126.40 - 129.90		N EITHER ARE SIF. SO OCCURS PREDOMINANTLY IN UPHOLE HALF OF UNIT						
R	126.40 - 129.90		AS < REBRECCIATING EVERYTHING. PY OCCURS MAINLY DISS IN FRAGS.						
R	126.40 - 129.90		FRAG % DECREASES CONSIDERABLY IN DOWNHOLE 1/3 OF UNIT.						
Z L	129.90 - 132.95	3.05	BRHM	*S) BR SS MO9	P CL	50		B=	
R	132.32 - 132.43	0.11	X BRHM	*S) BR SS MO9	R CL	50	<=	D3 <+	B=
Z L	132.95 - 133.70	0.75	BRHM	GR) BR SS MO8	P LM+		<=	D+ <=	B* B(
R	132.95 - 133.70		UNIT ARTIFICIALLY TRUNCATED DUE TO ASSAY SAMPLE INTERVAL. UNIT						
R	132.95 - 133.70		ACTUALLY CONTINUES DOWN TO 133.97. MATRIX LIGHTLY GRAPHITIC.						
R	132.95 - 133.70		LOCALLY LIGHTLY SILICIFIED - BOTH MATRIX AND FRAGS.						
K US1	133.70 - 133.70	0.00							
Z L	133.70 - 135.60	1.90	LMSX GL SL	LM PR C F X I	P 1 LM	45 <*	M1	L1 L1	
R	133.70 - 135.60		BEDDING ANGLE TEEPEMS DOWNHOLE. MINOR LOCAL BRECCIATION ESP						
R	133.70 - 135.60		NEAR LOWER CONTACT. HIGH POROSITY ABOUT 15%.						
Z L	135.60 - 136.60	1.00	SXFG	SIF BR LM MN2	P LM	70	D1	O= L+	
R	135.60 - 136.60		CORE MISSING 20%. LIGHTLY SILICIFIED. ORE BRECCIATED AND						

G F O L C G

K	F	F	R	O	M	-	T	O	-	T	R	I	RECOV	DD	%	ROCK	TM	TM	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	DD	AGE	EV	RR	LC	TM	QMP	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA						

R 135.60 136.60 PROBABLY ERODED BY GRAVITY FLOW. GALENA RICH FROM 133.70 TO
R 135.60 136.60 135.10M AND SPHALERITE RICH FROM 135.10 TO 135.60M.

K ISI 136.60 136.60 0.00

/ 136.60 139.40 2.80 BRHT *S) BR NQ8 P <= B+ B(
L 3A +) LM=

R 136.60 139.40 MATRIX SIMILAR DOWN TO T.O. PROBABLY ONE SLUMP EVENT.

/ FRG 139.40 139.90 0.50 CGSN SIF BR F* G M 6 L P <= D*
L 3A H* 7

/ 139.90 141.15 1.25 BRPM SIF PR NO1 P B-
L 3A KN2
R 139.90 141.15 SAND GRIT MATRIX.

/ 141.15 143.74 2.59 BRPM BR SS OR9 P D.
L 2A - IL+

R 141.15 143.74 LIGHTLY CARBONACEOUS MATRIX.

/ FRG 142.70 143.30 0.60 X ARGL SS A A A R CL 30

L 2A
R 142.70 143.30 CLEAVAGE MAY BE A SLUMP CLEAVAGE.

/ 143.74 144.58 0.84 BRPM BR ST LN1 P D(
L 3A H* KN2 D)
R 143.74 144.58 SIMILAR TO 139.90 TO 141.15M.

/ 144.58 144.78 0.20 BRPM BR SS PRX P D(
L 2A <(
R 144.58 144.78 PROBABLY ANOTHER SLUMPED ARSI FRAGMENT SIMILAR TO 142.70 TO
R 144.58 144.78 143.30M.

A IMM				SAMPLE	% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP					H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WFT ANALYSIS.									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	153.70	134.40	064		17.80	29.25	-0.1	6.08	-0.1	-0.1	-0.1	-0.1	52.63
A 001	134.40	135.10	060		23.35	37.09	-0.1	5.68	-0.1	-0.1	-0.1	-0.1	65.62
A 001	135.10	136.00	081		4.10	34.26	-0.1	2.26	-0.1	-0.1	-0.1	-0.1	40.12
A 001	136.00	136.60	057		2.48	11.20	-0.1	1.12	-0.1	-0.1	-0.1	-0.1	14.30
A 001	136.60	137.35	072		0.05	1.65	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.10
A 001	137.35	138.35	097		0.04	1.90	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.34
A MAX	133.70	138.35	431		23.35	37.09	-0.1	6.08	-0.1	-0.1	-0.1	-0.1	66.02

A MIN				0.04	1.65	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	1.09
A CMP	133.70	136.50	262	11.72	28.96	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	40.08

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASON PH-ZN-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 78-DH042	COLLAR ELEVATION: 1204.17	AZIMUTH(DEG) : 45.00	GEOLOGGED BY : GEC + DWB
TOTAL DEPTH/LENGTH : 143.26	NORTHING(- IF S): 7002168.00	VERTICAL ANGLE : -55.00	DATE (YY/MM/DD): 811012
CORE/HOLE DIAMETER : HQ	EASTING (- IF W): 436511.00	CO-ORD SYSTEM : UTM	PROJECT NUMBER : JASON

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	45.72	45.00	-60.00
2	76.20	44.00	-59.00
3	100.58	47.00	-56.00
4	140.21	44.00	-55.00

R HED CORE ORIGINALLY LOGGED BY J.D. ROWE - SEPTEMBER, 1978.

INTERVAL - CORE										T- %		TYPI- DAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION				MINS		ORE-TYPE				MINS		SUMMARY	
L (UNITS = . DEC.PLACE) RECOV- M % ROCK										FYING MIN		TURES		CHARACS								H H H H H ANY H H H ANY						ALT ORE					
E L (MT=METRIC FT=FOOTRIC) ERY O I										TM TM		MAT TX TX		F C % M		ARG		/RI		T ID STK DIP		A A A A A MIN A A A MIN											
Y G F R O M - T O - I N T (.) D X TYPE										1 2 QM1		1 2		F F C A				1		AZM RT QZ		FL CY CA BA XX PY CP GL YY		A 1 A 2									
K F										ROCK		FM RT		TM QM2		TX TX		S C O O		CHT		T ID STK DIP		MG MU CL SD QS HA PR MT SL HA									
E L										QUAL		AGE EN- Q		LC- 3		3 4 O		/		2		AZM RT H H H H H H H H H		1 1									
Y G										DESIG		VIR		CUL		R C				STRUCTUR-2		A A A A A A A A A		2 2									

R SVY 0.00 0.00 ALL SURVEY BY SPERRY-SUN.

1	0.00	24.38	24.38	OVER	P
L					
R	0.00	24.38	FROM 22.86 TO 24.38 METERS-LOOSELY CONSOLIDATED GRAVELS AND MUD		

/	24.38	43.59	19.21	ARGL PY	LM 60 0 3 2 3	P 2	40	<
1				46				

/	43.59	53.34	9.75	LOST	p
---	-------	-------	------	------	---

1	53.54	59.54	6.20	ARGL CR	ED	0 1) 1	P 2	45
				2A				

R	53.34	59.54	INTERVAL IS EXTREMELY FRIABLE AND IT IS UNCLEAR WHETHER IT IS
R	53.34	59.54	BOUGY OR NOT.

/	59.54	52.00	2.46	BRHT PY	SI2		QS7	P	R)
L				3A		3	LO1		

/	62.00	73.15	11.15	ANGL PY	MX	0 3 2 3	P	< (D =
1				3A					

R	62.00	73.15	INTERVAL IS QUIBBLY + EXHIBITS MINOR LOCAL SHEAWS (GRAPHITIC)
R	62.00	73.15	LOCAL BRECCIATION + INFILLING WITH QTZ VNS. SILICIFICATION IS
R	62.00	73.15	ASSOCIATED WITH QTZ VNG (EG. 68.20 - 68.30M).

7	75.15	81.00	7.85	ARSI	PY *S- LB	D 3 3 3	P 1	40	<
1				3A					

[illegible]

Z	81.00	82.00	1.00	ARGL SD SL	MX	0 3 1 3	P		<	<
L				3A				<=		
R	81.00	82.00		INTERVAL IS MASSIVE ARGL WITH OCCASIONAL CARB (SID?) VNS.						
R	81.00	82.00		CONTAINING MINOR GL AND PYR.						
Z	82.00	83.50	1.50	FGSX PY SD			P		#+	#+
L				3A				#=		
R	82.00	83.50		SULPHIDES ARE PRESENT AS FILLINGS ALONG FRACTURE SURFACES IN						
R	82.00	83.50		ARGL						
Z	83.50	84.50	1.00	ARGL PY	MX	1 3 1 3	P		#+	<
L				3A				<(
R	83.50	84.50		INTERVAL IS ONLY SLIGHTLY MINERALIZED						
Z	84.50	109.30	24.80	ARGL PY DZ	MX	1 3 1 3	P		<+	<(
L				3A				<+		
R	84.50	109.30		VEINING INCREASES DOWN HOLE-ARG. IS LOCALLY DISTURBED NEAR						
R	84.50	109.30		BOTTOM OF HOLE BUT NOT SUFFICIENTLY TO BE A BRHM.						
Z	109.30	110.30	1.00	ARGL PY SD			P		<+	<=
L				3A				<*		
R	109.30	110.30		FROM 109.30 TO 122.00 HAS BEEN ASSAYED AS IT CONTAINS MINOR						
R	109.30	110.30		AMOUNTS OF GL, SL + PY TO MTZ-SID VEINS AND BRECCIA FILLINGS.						
Z	110.30	111.45	1.15	ARGL PY SD			P		#+	#)
L				3A				#+ #*		
R	110.30	111.45		HOST IS ARGL.						
Z	111.45	112.45	1.00	ARGL PY SD			P		#)	#*
L				3				#+ #*		
R	111.45	112.45		HOST IS ARGL.						
Z	112.45	113.45	1.00	ARGL PY SD			P		<+ <*	D)
L										#*
R	112.45	113.45		HOST IS ARGL.						
Z	113.45	114.45	1.00	ARGL PY QS			P		D+ <= <*	
L				3A				<=		
R	113.45	114.45		HOST ROCK IS ARGL.						
Z	114.45	115.45	1.00	ARGL PY QS			P		<)	<)
L				3A					<=	
R	114.45	115.45		MINERALIZATION IS DISSEMINATED THROUGH QS - PY VEINS IN ARGL.						
Z	115.45	116.45	1.00	ARGL PY QS			P		<)	<+
L				3A					<=	
R	115.45	116.45		MINERALIZATION IS DISSEMINATED THROUGH QS-PY VEINS IN ARGL.						
Z	116.45	117.45	1.00	ARGL PY QS			P		<+	<)
L				3A					<=	<=

R	116.45	117.45	MINERALIZATION IS DISSEMINATED THROUGH QS-PY VEINS IN ARGL									
/	117.45	118.55	1.10	ARGL PY			P	<)	<.	D*	<.	<.
L				3A								
R	117.45	118.55	MINERALIZATION IS IN NARROW QTZ VEINS - PY IS DISSIMINATED IN									
R	117.45	118.55	HOST ARGL.									
/	118.55	119.70	1.15	ARGL PY QS			P		<+	D)	<*	
L				3A								
R	118.55	119.70	MIN IS ASSOC. WITH EXTENSIVE QS VEINING IN ARGL - LOWER PART OF									
R	118.55	119.70	INTERVAL IS RUBBLY.									
/	119.70	121.00	1.30	ARGL QS PY			P		V+	<+	V=	
L				3A								
R	119.70	121.00	MINERALIZATION IS DISS IN QS VEINS ALSO DISSEM. IN HOST ARGL									
R	119.70	121.00	ASSOCIATED WITH PYRITE-INTERVAL IS RUBBLY.									
/	121.00	122.00	1.00	BRPM PY		*S-	PQ8	P			D*	
L				4A			4	-	MN2			
R	121.00	122.00	INTERVAL IS RUBBLY.									
/	122.00	126.49	4.49	BRHT		*S2 F*	NQ3	P				
L				4A		*C-	3	2	MO4			
R	122.00	126.49	INTERVAL IS LOCALLY RUBBLY.									
/	126.49	131.94	5.45	BRHT		*S= *F	PR8	P			R+	
L				4A		*C-	3	=	LN+			
/	131.94	137.86	5.92	BRHM		SD=	DS9	P			D*	
L				4A			3		MO)			
/	137.86	143.26	5.40	BRHT		*S+ F*	DS7	P			R+	
L				4A		*C(3	+	MP2			
R	137.86	143.26	INTERVAL IS LOCALLY RUBBLY.									

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :78-0H043
TOTAL DEPTH/LENGTH : 192.02
CORE/HOLE DIAMETER : HOCOLLAR ELEVATION: 1196.74
NORTHING(- IF S): 7002103.00
EASTING (- IF W): 436581.00AZIMUTH(DEG) : 45.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : WJJ + DWB
DATE (YY/MM/DD): 811012
PROJECT NUMBER : JASON

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	39.62	47.00	-53.00
2	97.54	50.00	-50.00
3	143.62	49.00	-48.00
4	188.98	46.00	-46.00

F	- I N T E R V A L -	CORE	T- %	TYPI- GAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)RECDV-	N M ROCK	FYING MIN	TURES	CHARACS					
F	A (MT=METRIC FT=FOOTRIC)	ERY	0 I	TR TM MAT	TX TX F C % M ARG	/RI	T ID STK DIP	A A A A A	MIN A A A MIN	- - - -
Y	G F R D - I D - I N T (.)	D X TYPE	1 2 DM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K	F	ROCK	FM	RT	TR DM2 TX TX S C O O CHT	1	ID STK DIP MG MU CL SD QS HA PR MT SL HA			
F	L	QUAL	AGE	EM- Q LC- 3	3 4 O /	2	AZM RT H H H H H H H H	1 1		
Y	G	DESIG	VIR	COL	R C		STRUCTUR-2	A A A A A A A A	2 2	

R SVY 0.00 0.00 SPERRY SUN SURVEY DATA.

/ 0.00 24.38 24.38 OVER P

/ 24.38 25.20 0.82 SAND LM A F 7 I P 0 LM 75 <★ D(

L 24.38 25.20 5A
R POROUS SANDSTONE WITH ARG LAMS CONTAINING DISS PY.

/ 25.20 31.30 6.10 ARG L SI(LM MX A H 1 G P 0 LM 70 <(D(

L 25.20 31.30 2A SN= D.

R CORE HIGHLY BROKEN UP.

/ 31.30 32.90 1.60 SAND LM A F 6 H P 0 LM 70 <★ D=

L 31.30 32.90 5A SS
R ARG LAMS. MINOR DISRUPTION DUE TO SS AT BOTTOM OF UNIT.

/ 32.90 54.31 21.41 ARSI SI(BD LM A D 2 F P 4 LM 60 D(D.

L 32.90 54.31 3A SN= < D.

R SAND BEDS CONTAIN ARG LAMS. SAND BEDS DESCRIBED BELOW.

R 35.18 35.50 SAND BED.

R 36.45 36.58 SAND BED.

R 39.01 39.15 SAND BED.

R 41.50 41.80 SAND BED. UPPER HALF OF BED CONSISTS OF QZ GRIT CONTAINING ARG L

R 41.50 41.80 FRAGS 2% UP TO 3CM, AVG SIZE 1MM. SHARP CONTACT BETWEEN SN-GRIT

R 44.47 44.60 SAND BED.

R 46.40 46.74 SAND BED.

R 48.95 49.15 SAND BED.


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/ FLT 176.84 176.90 0.06 x FAIL GGX R

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G E O L O G

A UMM
A TYP
A MTHRQD
CM
B-BSP.GR.
SG
WEIGH

A LAB

FLD

FLD

R ASY	0.00	0.00	RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)	
R ASY	0.00	0.00	RQD=ROCK QUALITY DESIGNATOR(C27-32)MEASURED IN CM BLOCK TO BLOCK	
R ASY	0.00	0.00	RQD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE	
R ASY	0.00	0.00	AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED	
R ASY	0.00	0.00	BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM)TIMES 100	
R ASY	0.00	0.00	CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT	
R ASY	0.00	0.00	JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN	
R ASY	0.00	0.00	OF EACH FIELD.	
R ASY	0.00	0.00	B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK	
R ASY	0.00	0.00	AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.	
R ASY	0.00	0.00	ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN	
R ASY	0.00	0.00	BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR	
R ASY	0.00	0.00	RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN	
R ASY	0.00	0.00	THE AMTH HEADER.	
R ASY	0.00	0.00	THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,	
R ASY	0.00	0.00	SHOULD BE ENTERED FIRST -- SEE BELOW.	
A 100	0.00	24.38	00	00
R ASY	0.00	24.38	OVERBURDEN	
A 100	24.38	25.30	39	00
A 100	25.30	27.44	100	00
A 100	27.44	28.96	93	00
A 100	28.96	29.87	47	00
A 100	29.87	31.09	75	17
A 100	31.09	32.00	38	23
A 100	32.00	32.92	71	17
A 100	32.92	34.14	75	00
A 100	34.14	35.66	120	00
A 100	35.66	36.68	76	00
A 100	36.68	39.01	37	00
A 100	39.01	39.92	60	00
A 100	39.92	42.37	120	00
A 100	42.37	43.28	48	00
A 100	43.28	44.29	81	00
A 100	44.29	45.70	108	00

A UMM				RND	SP.GR.
A TYP				CM	SG
A MTH				H-R	WEIGH
A LAB				FLD	FLD
A 100	45.79	46.92	120	45	
A 100	46.92	47.85	93	22	
A 100	47.85	48.77	92	00	
A 100	48.77	49.68	61	00	
A 100	49.68	51.21	152	19	
A 100	51.21	53.34	98	00	
A 100	53.34	54.86	18	00	
A 100	54.86	56.39	118	00	
A 100	56.39	57.91	147	43	
A 100	57.91	58.83	92	00	
A 100	58.83	60.05	101	74	
A 100	60.05	60.96	85	18	
A 100	60.96	62.48	120	17	
A 100	62.48	64.01	108	00	
A 100	64.01	65.53	120	00	
A 100	65.53	66.10	61	00	
A 100	66.14	67.06	92	00	
A 100	67.06	68.20	72	00	
A 100	68.29	69.79	150	00	
A 100	69.79	71.32	136	21	
A 100	71.32	72.85	100	18	
A 100	72.85	74.07	104	00	
A 100	74.07	74.98	55	00	
A 100	74.98	76.20	68	00	
A 100	76.20	77.11	97	00	
A 100	77.11	78.03	23	00	
A 100	78.03	79.25	100	00	
A 100	79.25	79.55	10	00	
A 100	79.55	81.08	114	00	
A 100	81.08	82.29	79	46	
A 100	82.29	83.32	50	00	
A 100	83.34	85.34	43	00	
A 100	85.34	86.87	78	21	
A 100	86.87	88.39	10	00	
A 100	88.39	89.92	87	00	
A 100	89.92	91.44	147	00	
A 100	91.44	92.92	147	00	
A 100	92.92	94.49	50	00	
A 100	94.49	96.01	62	00	
A 100	96.01	97.54	104	00	
A 100	97.54	99.06	76	00	
A 100	99.06	100.58	91	00	
A 100	100.58	102.11	128	00	
A 100	102.11	103.63	73	00	
A 100	103.63	104.55	88	00	
A 100	104.55	105.77	60	00	
A 100	105.77	106.68	76	00	
A 100	106.68	107.59	40	00	
A 100	107.59	108.20	36	00	
A 100	108.20	109.73	102	00	
A 100	109.73	110.95	62	00	

A JMH

A TYP

A MTH

A LAB

RHD

CM

R-H

FLD

SP.GR.

SG

WEIGH

FLD

A 100	110.95	111.86	63	00
A 100	111.86	112.78	49	00
A 100	112.78	113.69	79	00
A 100	113.69	114.30	61	00
A 100	114.30	115.82	152	00
A 100	115.82	118.26	92	00
A 100	118.26	119.18	74	00
A 100	119.18	120.40	122	00
A 100	120.40	122.22	138	89
A 100	122.22	123.44	95	20
A 100	123.44	124.97	58	00
A 100	124.97	126.49	55	00
A 100	126.49	128.02	55	00
A 100	128.02	129.24	66	00
A 100	129.24	130.15	91	00
A 100	130.15	131.06	91	00
A 100	131.06	131.98	72	00
A 100	131.98	133.20	76	00
A 100	133.20	134.11	76	00
A 100	134.11	135.32	64	00
A 100	135.32	136.24	33	00
A 100	136.24	137.50	40	00
A 100	137.50	138.41	29	00
A 100	138.41	139.59	65	00
A 100	139.59	140.20	46	00
A 100	140.20	141.92	26	00
A 100	141.92	143.26	134	00
A 100	143.26	144.78	138	00
A 100	144.78	146.30	146	20
A 100	146.30	147.83	153	19
A 100	147.83	149.35	130	00
A 100	149.35	150.88	105	00
A 100	150.88	151.79	91	00
A 100	151.79	153.51	141	24
A 100	153.51	153.92	39	00
A 100	153.92	155.45	91	21
A 100	155.45	156.97	144	00
A 100	156.97	158.50	118	00
A 100	158.50	160.02	191	19
A 100	160.02	161.54	151	23
A 100	161.54	163.07	125	00
A 100	163.07	164.59	130	37
A 100	164.59	165.81	81	00
A 100	165.81	167.03	115	00
A 100	167.03	167.55	28	00
A 100	167.55	168.86	127	00
A 100	168.86	170.08	114	22
A 100	170.08	171.60	147	25
A 100	171.60	173.13	117	40
A 100	173.13	174.65	137	00
A 100	174.65	175.87	100	00

A UMM		RQD	SP.GR.
A TYP		CM	SG
A MTH		B-B	WEIGH
A LAB		FLD	FLD

A 100	175.87	176.78	91
A 100	176.78	177.39	36
A 100	177.39	178.31	30
A 100	178.31	179.83	97
A 100	179.83	181.05	105
A 100	181.05	182.27	106
A 100	182.27	182.88	54
A 100	182.88	184.10	76
A 100	184.10	185.32	21
A 100	185.32	185.93	49
A 100	185.93	187.45	136
A 100	187.45	188.98	112
A 100	188.98	190.50	134
A 100	190.50	192.02	130

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G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 79-DH044
TOTAL DEPTH/LENGTH : 60.35
CORE/HOLE DIAMETER : 40COLLAR ELEVATION: 1234.20
NORTHING(- IF S): 7002307.00
EASTING (- IF W): 436400.25AZIMUTH(DEG) : 45.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-SSEQ. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)1
236.58
60.3545.00
45.00-49.00
-49.00

F - INTERVAL -		CORE	T- %	TYPI- VAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECDV-	M N ROCK	EXING MIN	TURES	CHARACS		H H H H H	ANY H	H H H	ANY	ALT ORE
E	A (MT=METRIC FT=FOOTIRIC)	ERY	D I	TM TM MAT	TX TX	F C % M ARG	/RT T	ID STK DIP	A A A A A	MIN A	A A A	MIN - - -
Y	G F R D H - T D - I N T (.)	D X TYPE	1 2 RM1	1 2 F F C A			1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2			
K	F	ROCK	FM	RT	TM RM2	TX TX S C O O CHT	T	ID STK DIP	MG MU CL SD QS HA PR MT SL HA			
E	L	QUAL	AGE	EN- 2	LC- 3	5 4 U /	2	AZM RT H H H H H H H H				1 1
Y	G	DESIG	VIR	CUL		R C		STRUCTUR-2	A A A A A A A A A A			2 2

R SVY 0.00 0.00 SPERRY SUN TEST.

R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE.

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

FORMAT VERSION : 6B02

SEC. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	45.00	-47.00
2	45.72	42.00	-47.50
3	76.20	44.17	-45.00
4	144.78	43.25	-41.50

F	- I N T E R V A L -	CORE	T- %	TYPE	DAL	TEX-	GRAIN		PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY	
K	L (UNITS = DEC.PLACE)	RECOV-	N M	ROCK	EYING	MIN	THRES	CHARACS			H H H H H ANY H H H ANY				ALT ORE	
E	A (MT=METRIC FT=FOOTRIC)	ERY	O I		TM TM	PAT	TX TX	F C % M	ARG /RI	T ID STK DIP	A A A A A MIN A A A MIN				- - - -	
Y	G F R O M - T O - I N T (.)	D X	TYPE	1 2	DM1	1 2	F F C A			1 AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2					
-	-----	----	--	----	--	--	--	--	----	---	---	---	---	---	---	---
K	F	ROCK	FM	RT	TD	DM2	TX TX	S C D O	CHT	T ID STK DIP MG MU CL SD QS HA PR MT SL HA						
E	L	QUAL	AGE	EB= 0	LC= 3		3 4 0	/		2 AZM RT H H H H H H H H H					1 1	
Y	G	DESIG	VIR	COL			R	C		STRUCTUR-2	A A A A A A A A A A				2 2	

R SVY 0.00 0.00 SPERRY SUN TEST DOWN THE HOLE.

R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE.

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 79-04946	COLLAR ELEVATION: 1203.16	AZIMUTH(DEG) : 270.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 277.06	NORTHING(= IF S): 7000399.00	VERTICAL ANGLE : -60.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER :	EASTING (= IF W): 437509.44	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

SEC. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	76.20	270.00	-59.00
2	106.68	280.00	-48.00
3	137.16	276.00	-36.00
4	167.64	273.00	-30.00
5	198.12	271.00	-26.00
6	227.08	265.00	-18.00
7	277.06	260.00	-22.00

F	- T N I E R V A L -	CORE	T- %	TYPT=	QAL	TEX-	CHAIN		PGT	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECOV=	N M ROCK	TYTG	MIN	TURES	CHARACS			H H H H H ANY H H H ANY	ALT ORE				
E	A (M=METRIC FT=FOOTIC)	ERY	D I	T1 T1 MAT	TX TX	F C % M ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -					
Y	G F R D A - I D - I W T (.)	D X TYPE	1 2 QMI	1 2	F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2						
<hr/>															
K	F	ROCK	FR	RT	IN OM2	TX TX	S C O O CHT	T ID STK DIP MG MU CL SD QS HA PR MT SL HA							
E	L	DUAL	AGE ED=	O LC=	3	3 4 O /	2	AZM RT H H H H H H H H H	1 1						
Y	G	DESIG	VIR	COL	R	C		STRUCTUR-2	A A A A A A A A A A	2 2					

R SVY 0.00 0.00 AZM AT 227.08 AND 277.06 ARBITRARILY DEFINED BY APPARENT TREND.

R SVY	0.00	0.00	SPERRY SUN TESTS.
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R ASY 0.00 0.00 NO ASSAYS DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASOP PR-79-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 79-DH047
TOTAL DEPTH/LENGTH : 166.12
CORE/HOLE DIAMETER : 80COLLAR ELEVATION: 1259.40
NORTHING (- IF S): 7002540.00
EASTING (- IF W): 436166.31AZIMUTH(DEG) : 223.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-S

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	73.15	224.00	-51.00
2	103.63	224.00	-52.00
3	164.59	224.00	-51.50

F - I R I E R V A L -		CORE	T- 2	TYPI- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY	
K	L (UNITS = . DEC. PLACE)	RECDV-	R M ROCK	RYING MIN	TYPES	CHARACS							
E	A (MT=METRIC FT=FOOTRIC)	FRY	0 T	TM 1X	MAI TX TX	F C % M	ARG	/RI	T	ID	STK	DIP	A A A A A MIN A A A MIN
Y	G F R U M - T O - I N T (.)	0 X	TYPE	1 2	QMI	1 2 F F C A			1	AZM	RT	QZ FL CY CA BA XX PY CP GL YY	A 1 A 2
K	F	ROCK	FM	RT	TM QM2	TX TX S C O O	CHT		1	ID	STK	DIP	MG MU CL SD QS HA PR MT SL HA
E	L	QUAL	AGE	EN- R	LC- 3	3 4 0	/		2	AZM	RT	H H H H H H H H	1 1
Y	G	DESIG	VIR	COL		R C				STRUCTUR-2	A A A A A A A A	2 2	

R SVY 0.00 0.00 SPERRY SON TESTS.

R ASY 0.00 0.00 NO ASSAYS OF CORE FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-24-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :79-DH048
TOTAL DEPTH/LENGTH : 87.48
CORE/HOLE DIAMETER : NOCOLLAR ELEVATION: 1310.00
NORTHING(- IF S): 7003183.00
EASTING (- IF W): 434828.00AZIMUTH(DEG) : 225.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-RECC

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	45.72	232.00	-55.00
2	87.48	217.00	-54.00

F - I N T E R V A L -		CORE	T- %	TYPI- NAL	TEX- GRAIN	PGT	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
X L (UNITS = . DEC.PLACE)	RECOV-	M M ROCK	RYING MIN	TURES	CHARACS							
E A (MT=METRIC FT=FOOTRIC)	ERY	D T	TM TM MAT	TX TX	F C % M ARG	/RI T	ID STK DIP	A A A A	A MIN	A A A MIN	- - - -	
Y G F R D W - 1 0 - T V T (.)	D X TYPE	1 2 DM1	1 2 F F C A			1	AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2					

K F	ROCK	FM	RT	TM DM2	TX TX S C D D CHT	T ID	STK DIP	MG MU CL SD QS HA PR MT SL HA				
E L	QUAL	AGE EN- 0	LC- 3	3 4 0	/	2	AZM RT H H H H H H H H H H					
Y G	DESG	VIR	COL		R C		STRUCTUR-2	A A A A A A A A A A				2 2

R SVY 0.00 0.00 SPERRY SUN TEST DATA.

R ASY 0.00 0.00 NO ASSAYS VALUES FOR THIS HOLE.

G E O L O G F O I I L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZV-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 79-08049

COLLAR ELEVATION: 1283.50

AZIMUTH(DEG) : 200.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 281.90

NORTHING(- IF S): 7002830.00

VERTICAL ANGLE : -57.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : HQ

EASTING (- IF W): 436113.00

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-MAIN

SER. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	57.91	197.00	-58.00
2	76.20	196.00	-59.00
3	106.68	197.00	-56.00
4	137.16	192.00	-52.00
5	198.12	187.00	-42.50
6	274.32	189.00	-49.00

F - INTERVAL - CORE T- %		TYPI- QAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION MINS		ORE-TYPE MINS		SUMMARY																		
K L (UNITS = . DEC.PLACE)RECV-	M M ROCK	RYING	MIM	TURES	CHARACS			H	H	H	H	H	ANY	H	H	ANY	ALT	ORE														
E A (MT=METRIC FT=FOOTRIC) ERY	D I	TH	TH	HAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-		
Y G F R O - T D - I N T (.)	D X	TYPE	1	2	QRI	1	2	F	F	C	A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	-	-	-	-
K F	ROCK	FM	RT	TH	QRI	TX	TX	S	C	O	O	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA						
E L	DUAL	AGE	EN	4	LC	3	3	4	O	/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1				
Y G	DESIG	VIR	CDL						R	C			STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	A	2	2				

R SVY 0.00 0.00 SPERRY SUN TESTS.

R ASY 0.00 0.00 NO ASSAYS VALUES FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-24-AG-KA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :79-DH050	COLLAR ELEVATION: 1336.90	AZIMUTH(DEG) : 45.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 397.76	NORTHING(= IF S): 7003019.00	VERTICAL ANGLE : -55.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : NO	EASTING (= IF N): 434733.50	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

SEP. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	60.96	42.00	-50.50
2	152.40	42.00	-46.50
3	213.36	42.00	-42.50
4	304.80	29.50	-29.50
5	397.76	28.50	-23.00

F	-	I	-	T	E	R	V	A	L	-	CORE	T	-	%	TYPI	-	QAL	TEX	-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY											
K	L	(UNITS =	.	DEC.	PLACE)	RECOV	-	M	M	ROCK	FYING	MIN	TURES	CHARACS																								
E	A	(MT=METRIC	FI=FOOTRIC)	ERY		D	I			TM	TM	MAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F	R	D	N	-	T	D	-	I	N	I	(.)	D	X	TYPE	1	2	QMI	1	2	F	F	C	A											

K	F					ROCK	FM		RT		TM	QMI	TX	TX	S	C	D	D	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L					QUAL	AGE	FD	-	D	LC	-	3		3	4	D		/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G					DESIG	VIR		COL						R		C						STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 SPERRY SUR TESTS.

G E O L O G

A UMS				SAMPLE	% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAR				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	PA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	39.55	40.55	91	18776	0.12	5.40	-0.1	-0.1	0.03	-0.1	-0.1	-0.1	5.05
A 001	40.55	41.45	84	18777	0.38	3.62	-0.1	-0.1	0.01	-0.1	-0.1	-0.1	3.51
A CMP	39.55	41.45	175		0.24	4.53	-0.1	-0.1	0.02	-0.1	-0.1	-0.1	4.29

A MIN			0.12	3.62	-0.1	-0.1	0.01	-0.1	-0.1	-0.1	3.25
A MAX	39.55	41.45	0.38	5.40	-0.1	-0.1	0.03	-0.1	-0.1	-0.1	5.31

100% BY A.P.F.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-BASITE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRaverse : 79-0H051

COLLAR ELEVATION: 1198.10

AZIMUTH(DEG) : 32.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 3.96

NORTHING(= IF S): 7002146.00

VERTICAL ANGLE : -60.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : HO

EASTING (= IF W): 436572.00

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

R HED

THIS HOLE WAS ABANDONED.

F - I N T E R V A L -		CORE	T- %	TYPICAL		TEX-	GRAIN	PGI	STRUCTUR-1		ALTERATION MINS					ORE-TYPE MINS					SUMMARY											
K	L (UNITS = . DEC. PLACE)	RECOV-	M M	ROCK	FLYING	MINS	TURES	CHARACS		T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-						
Y	G	F R O P - T O - T A L (.)	D	X	TYPE	1	2	OR1	1	2	F	F	C	A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	A	(PT=METRIC FT=FOOTRIC)	ERY	0	J																											
K	F		ROCK	FM	RI																											
E	L		QUAL	AGE	ER-	Q	LC-	3																								
Y	G		DESIG	VIR	COL																											

R SVY 0.00 0.00 EASTING IS APPARENTLY DIFFERENT FROM EASTING FOR 79ADH051.

R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-EA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILL HOLE/TRAVERSE : 79-DH052
TOTAL DEPTH/LENGTH : 209.39
CORE/HOLE DIAMETER : 50COLLAR ELEVATION: 1374.00
NORTHING(- IF S): 7003590.00
EASTING (- IF W): 435322.00AZIMUTH(DEG) : 45.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-RECCSED. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	121.92	45.00	-45.75
2	206.65	42.00	-37.00

F - INTERVAL -		CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE) RECHV-	M M ROCK	FYING MTH	TURES	CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E	A (MT=METRIC FT=FOOTRIC) ERY	U 1	TM TM MAT	TX TX	F C % M ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y	G F R O N - T O - I N T (.)	D X TYPE	1 2 QM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K	F	ROCK FM RT	TM QM2	TX TX	S C D D CHT	T	ID STK DIP MG MU CL SD QS HA PR MT SL HA			
E	L	DUAL AGE EP- N LC- 3	3 4 U	/		2	AZM RT H H H H H H H H H H	1 1		
Y	G	DESG VER COL		R C			STRUCTUR-2 A A A A A A A A A A	2 2		

R SVY 0.00 0.00 SPERRY SON TESTS.

R ASY 0.00 0.00 NO ASSAYS FROM THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-7N-AG-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 79ADH051
TOTAL DEPTH/LENGTH : 305.41
CORE/HOLE DIAMETER : 4000COLLAR ELEVATION : 1198.10
NORTHING (= IF S) : 7002146.00
EASTING (= IF W) : 436430.00AZIMUTH(DEG) : 32.00
VERTICAL ANGLE : -60.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD) : 810615
PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	143.26	36.00	-58.00
2	251.46	29.00	-48.50
3	305.41	26.00	-44.00

R HED

ORIGINALLY LOGGED BY DR. GOOD AND DR. K.I.LU ON OCT 8, 1979.

F - I N T E R V A L -		CORE	1- %	TYPT- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY											
K	L (UNITS = . DEC.PLACE)	RECOV- M N	ROCK	TYPT- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY											
E	A (MT=METRIC FI=FOOTRIC)	ERY	C I	1M 1M	TX TX	F C % M	ARG	/RI	T ID	STK	DIP	A A A A A MIN A A A MIN											
Y	G F R O M - T O - I N T (.)	D X	TYPE	1 2	PM1 1 2	F F C A		1	AZM	RT	QZ	FL CY CA BA XX PY CP GL YY A 1 A 2											
K	F	ROCK	FM	RI	TX	PM2	TX TX	S C D O	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA
E	L	QUAL	AGE	FM- 9	LC- 3	3	4	0	/	2	AZM	RT	H H H H H H H H H	1	1								
Y	G	DESIG	VIR	CUL					C		STRUCTUR-2	A A A A A A A A A	2	2									

/ OVR 0.00 36.57 36.57

OVER

P

/ 36.57 84.60 48.03

ARGL CR GR SII LM // 1 1 1
4 SF CU RD

P

BD

D64 V(L.

L*

COMPOSITIONAL LAMINATIONS INCREASE DOWNWARDS, BECOMING LESS SILI-
CIFIED DOWN HOLE. WHITE MINERAL (ZEOLITE??) COATING FRACTURES.

/ CON 84.60 151.30 66.70

SAND *R1 MX BS 4 4 4
7 LC RD

P

CN

70 V(

L*

PS ARE ARE, RCDE AND RCD ALTERNATING. PYRITIZED ARGL FRAGMENTS
IN THOSE BRXX INTERBEDS.

/ SHR 121.66 124.70 3.02

X SAND *R1 MX BS 4 4 4

R

CN

70 V(

L*

/ 128.24 130.06 1.82

X SAND *R1 MX BS 4 4 4

R

BD

V79 V(

L*

GUES BACK THROUGH SAME GENERAL SUCCESSION, WHICH SEEMS TO BE
REPEATED AS PREVIOUSLY INTERVAL. FOLDING IS ALSO DEDUCTED.

/ 151.30 173.50 22.20

ARGL CR GR LM // 1 1 1
5 SF SM1 G; RN

P

BD

66 V(

V(V.

/ 173.50 180.00 6.50

SAND MX LM 5 5 5

P

/ 180.00 218.40 38.40

BRHT CR GR 003
4 SF DB 2 3 3 C NO1

P

CV

V+ 54

V(

[illegible]

A UMM	SAMPLE		% PB	% ZN	% RA	OZ AG	% CU	% FE	OZ AU	% CO	HASH		
A LAR	SERIAL		R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG			
A TYP			H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE			
A MTH			WA	WA	WA	WA	WA	WA	WA	WA			
R ASY	0.00	0.00	R.CLG = BONDAR CLGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	WA = NET ANALYSIS.										
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01										
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1										
A 001	268.75	269.92	099	18788	0.01	-0.01	10.71	0.04	-0.01	-0.1	-0.1	-0.1	10.44
A 001	269.92	272.00	190	18789	0.04	0.01	9.52	0.04	0.01	-0.1	-0.1	-0.1	9.32
A 001	272.00	272.86	062	18790	3.70	2.65	4.20	0.61	0.01	-0.1	-0.1	-0.1	10.87
A 001	272.86	273.80	076	18791	2.12	7.55	2.70	0.34	-0.01	-0.1	-0.1	-0.1	12.40
A 001	273.80	274.60	063	18792	0.30	0.84	8.72	0.10	-0.01	-0.1	-0.1	-0.1	9.65
A 001	274.60	275.84	122	18793	2.20	5.42	2.39	0.33	-0.01	-0.1	-0.1	-0.1	10.03
A 001	275.84	276.90	087	18794	3.60	14.50	0.81	0.46	0.01	-0.1	-0.1	-0.1	19.08
A 001	276.90	277.55	065	18795	5.18	11.20	0.86	0.68	0.02	-0.1	-0.1	-0.1	17.64
A 001	277.55	278.16	058	18796	2.88	4.60	1.57	0.35	0.01	-0.1	-0.1	-0.1	9.11
A 001	278.16	278.35	069	18797	0.95	0.96	0.51	0.11	0.04	-0.1	-0.1	-0.1	2.28
A MAX	268.75	278.85			5.18	14.50	10.71	0.68	0.04	-0.1	-0.1	-0.1	30.81

A MIN				0.01	-0.01	0.51	0.04	-0.01	-0.1	-0.1	-0.1	0.24
A CMP	272.00	278.16	533	2.83	6.85	3.0	0.4	-0.1	-0.1	-0.1	-0.1	12.68
A CMP	275.84	277.55	152	4.39	13.25	-0.1	0.54	-0.1	-0.1	-0.1	-0.1	17.68

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 89-04053
TOTAL DEPTH/LENGTH : 309.37
CORE/HOLE DIAMETER : 50COLLAR ELEVATION: 1221.90
NORTHING (= IF S): 7002262.00
EASTING (= IF E): 436340.75AZIMUTH(DEG) : 30.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810713
PROJECT NUMBER : J-S

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	45.72	32.00	-54.00
2	76.20	34.00	-53.00
3	137.16	29.00	-48.00
4	182.88	30.00	-44.00
5	238.66	26.00	-36.00
6	274.32	26.00	-34.50
7	309.37	26.00	-32.50

R HED

ORIGINALLY LOGGED BY ANGIE SIARTA IN JUNE 1980.

F	I	R	V	A	L	CORE	T	%	TYPE	VAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY														
K	L	(UNITS =	DEC. PLACE)	RECOV	%	ROCK	TYING	MIN	TURES	CHARACS																							
E	A	(MT=METRIC FT=FOOTRIC)	ERY	0	1	IN	IN	IN	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	MIN	-	-	-	
Y	G	F	R	O	M	-	I	O	-	I	N	T	(.)	D	X	TYPE	1	2	001	1	2	F	F	C	A						
K	F					ROCK	FR	RT	TX	TX	S	C	O	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA			
F	L					DUAL	AGE	EN	LC	3	3	4	O	/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G					DESIG	VIR	COL			R	C						STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 IN S001 V-ANG -58 WAS UNCERTAIN; -54 DEGREE IS CHOSEN IN CROSS
 R SVY 0.00 0.00 SECTION. IN S006 AND S007 AZIMUTH RESULTS FROM SPERRY SUN TEST
 R SVY 0.00 0.00 WERE CONSIDERED INVALID. A VALUE OF 26.00 IS CHOSEN IN CROSS
 R SVY 0.00 0.00 SECTION.

/ QVR 0.00 33.83 33.83 OVER P
 / 33.83 98.60 64.77 ARGU SE SI1 // LC 1 2 1 2 P 1 BD D73 V* L) LI
 L 5 CR SJ= SS LR 2 BD 55 V(L? C-
 R 33.83 98.60 BD VARIES THUS: D73 FROM 33.83 TO 50.40; 90 DEGREES FROM 50.40
 R 33.83 98.60 TO 78.10; AND 55 FROM 78.10 TO 98.60.

/ 88.45 89.98 1.53 X BRHM DB JO2 R D-
 L 5 2 0 LN3
 / 95.75 96.40 0.65 X ARSI SI1 LR RD 1 4 3 4 R 1 BD 59 L+
 L 5 S03 LC LM 5 B?

/ 98.60 109.32 10.72 BRHM DB NS2 P CN 55 V) LI
 L 5 5/ 2 2 0 NP3 C-
 R 98.60 109.32 INTERVAL 109.20-113.30 CORRELATES TO 111.00-116.13 OF HOLE 78-33
 / 100.67 105.64 4.97 X ARGU CR LC LR 1 1 1 R BD 55 V- L-
 L 5 SF SS (L V-

G E O L O G

K	F	F	R	O	M	-	T	O	-	I	N	T	RECDV	MD	%	ROCK	TO	FM	Q1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	Q	D	AGE	EV	RQ	LC	IN	Q12	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R 100.67 105.64 VERY POOR RECOVERY BETWEEN 102.10 AND 103.60; POSSIBLE FAULT
R 100.67 105.64 ZONE .

/ 109.32 113.70 4.38 SAND CR 4 4 4 P L*
L 5 *R+ RM

/ 112.50 113.70 1.20 X SAND CR GG6 4 4 4 R F1 L*
L 6 *R+ RM

/ 113.70 153.37 39.67 ANGL SF CR SI1 LM LC 1 1 1 P 1 BD D55 V* MS D) B. B- LI 75
L 5 SD SM= RM (L 4 BD 37 L* V) V* B. C-

R 113.70 153.37 INTERVAL 129.34-109.70 CORRELATES TO 70.00-99.20(?) OF HOLE
R 113.70 153.37 78-33. INTERVAL 113.70-129.34 CORRELATES TO 98.20-105.90 OF HOLE
R 113.70 153.37 78-33.

/ 122.85 123.40 0.55 X ANGL SF CR SI1 LM LC 1 1 1 R 1 BD D55 V* MS V* B. B- LI 75
L V1 V1

/ 126.80 127.30 0.50 X ANGL SF CR SI1 LM LC 1 1 1 R 1 BD D55 V) K2 MS D) B. B(LI 75
L 6

/ 128.64 129.14 0.30 X ANGL SF CR SI1 LM LC 1 1 1 R 1 BD D55 V* MS D) B. B. LI 75
L RM

/ 129.50 129.65 0.15 X ANGL SF CR SI1 LM LC 1 1 1 R 1 BD D55 V* MS D) B. V. LI 75
L V.

/ 134.36 137.30 2.94 X ANGL SF CR GG5 LM LC 1 1 1 R 1 F/ D55 V* MS D) B. B- LI 75
L

/ 147.60 149.10 1.50 X ANGL SF CR SI1 SS LC 1 1 1 R 1 BD D55 V* MS D) B. B- LI 75
L K2

/ 153.37 158.60 5.23 BRHM DB KP1 P V* L)
L 6 2 0 J04 V=

/ 154.70 154.95 0.25 X BRHM DB KP1 R V* M9 L)
L 8 2 0 J04 V=

/ 155.20 157.90 2.70 B ANGL LM 1 1 1 R V- V*
L 5 (L V1

/ 158.60 176.83 18.23 BRPM SM1 G; OU4 P V- L)
L 5 *R- DB 2 + 0 NO2 V. V.

/ 176.83 190.94 14.11 BRHT *R= DB PT5 P V. D-
L 6 *S= RS 2 1 C NO1

R 176.83 190.94 BS IS ABC

/ 183.06 183.36 0.30 X SAND 4 4 4 R BD U50
L 6 BD (L

[illegible][illegible]

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASPER PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 89-DH054
TOTAL DEPTH/LENGTH : 386.79
CORE/HOLE DIAMETER : NO

COLLAR ELEVATION: 1217.80
NORTHING (- IF S): 7002359.00
EASTING (- IF E): 436672.25

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AZIMUTH( DEG ) : 206.00
VERTICAL ANGLE : -65.00
CO-ORD SYSTEM : UTM

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GEOLOGGED BY : HJV +
DATE (YY/MM/DD): 810715
PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	38.40	206.00	-68.00
2	45.72	191.00	-66.00
3	91.44	187.00	-65.50
4	121.92	190.00	-64.00
5	152.40	171.00	-57.00
6	213.36	168.00	-53.00
7	274.32	161.00	-47.00
8	335.28	161.00	-39.50
9	384.35	163.00	-37.00

R HED

ORIGINALLY LOGGED BY A.R. HILDEBRAND IN JULY 1980.

INTERVAL - CORP T- % TYPE- QUAL TFX- GRAIN										PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY									
L (UNITS = . DEC.PLACE) RECD- M M ROCK FLYING MIN TURES CHARACS										H H H H H ANY H H H ANY ALT ORE									
E A (M=METRIC FT=FOOTRIC) ERY D I TM TM MAT TX TX F C % M ARG /RI T ID STK DIP A A A A A MIN A A A MIN - - - -																			
Y G F R D M - T D - I M T (.) D X TYPE 1 2 QP1 1 2 F F C A										1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2									
K F ROCK FM RT TM QM2 TX TX S C O O CHT										1 ID STK DIP MG MU CL SD QS HA PR MT SL HA									
E L QUAL AGE EN- O LC- S 3 4 O /										2 AZM RT H H H H H H H H H 1 1									
Y G DESIG VIR COL R C										STRUCTUR-2 A A A A A A A A A A 2 2									

R SVY	0.00	0.00	THE CROSS SECTION FOR THIS HOLE WAS PLOTTED AS AN IDEAL SMOOTH CURVE, AND VALUES FOR INCLINATION IN S004, S007, S008, S009; AND FOR AZIMUTH IN S001, S004, S007, S008 ARE READINGS FROM THIS CURVE. VALUES FOR AZIMUTH IN S002, S003, S009 ARE FIELD READINGS CONSIDERED TO BE AFFECTED BY LOCAL MAGNETIC DISTURBANCE.
R SVY	0.00	0.00	
R SVY	0.00	0.00	
R SVY	0.00	0.00	
R SVY	0.00	0.00	
R SVY	0.00	0.00	

/	DVB	0.00	21.34	21.34	OVER		P		
/		21.34	218.50	197.16	BRAT	G;	QT5	P	SH 55 V)

L	R	21.34	218.50	CRYSTALS OF PY OCCUR MAINLY IN CHT FRAGMENTS AND BLEBS IN ARG	FRAGMENTS SLICKERSIDED AND SHEAR PLANES ARE COMMON ALL THROUGH	OUT THE PGI. FAULT ZONES AT 59.0;70.0;AND 106.80.	COLOR CHANGES GRADUALLY TO GA BETWEEN 79.0-85.80 AND 176.0-189.0
R	21.34	218.50					
R	21.34	218.50					
R	21.34	218.50					

7	88.70	91.80	3.10	X RPPH	SN= RS G;	NP2	R
L				5	SI1 DR	2	2 0 JO=
R	88.70	91.80	COATINGS OF NATIVE COPPER OCCUR AT 89.41 ON FRACTURES SURFACE.				

99.70 101.30 1.60 Y R4P4 BS G: NS6 R CN 047 V1 B-

/	366.50	386.79	20.29	RRM	SM2	DR	QSB	P	V(0*
L				5	SF	RS	2	0 JM+		*(
R	366.50	386.79	US ARE AB, ABC.							

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 89-DH055	COLLAR ELEVATION: 1278.90	AZIMUTH(DEG) : 225.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 242.93	NORTHING(= IF S): 7002628.00	VERTICAL ANGLE : -65.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : HQ	EASTING (= IF W): 436261.81	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	231.00	-67.00
2	76.20	211.00	-61.00
3	121.92	208.00	-57.00
4	182.88	208.00	-52.00
5	237.88	208.00	-46.00

F - I N T E R V A L - CORE										T- %		TYPI- GAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION MINS					ORE-TYPE MINS					SUMMARY		
L (UNITS = DEC.PLACE) RECOV-										M M ROCK		FYING MIN		TURES		CHARACS		/RI		T ID STK DIP		H H H H H ANY H H H ANY					ALT ORE					
E A (PI=METRIC FT=FOOTRIC) ERY										O I		TM TM MAT		TX TX		F C % M ARG						A A A A A MIN A A A MIN					- - - -					
Y G F R O M - T O - I N T (.)										O X TYPE		1 2 DM1		1 2		F F C A				1		AZM RT		QZ FL CY CA BA XX PY CP GL YY					A 1 A 2			
- - - - -										- - - - -		- - - - -		- - - - -		- - - - -		- - - - -		- - - - -		- - - - -					- - - - -					
K F										ROCK		FM		RT		TM QM2		TX TX		S C O O		CHT		T ID STK DIP		MG MU CL SD QS HA PR MT SL HA						
F L										QUAL		AGE		EM- O		LC- 3		3 4 O		/		2		AZM RT		H H H H H H H H H H					1 1	
Y G										DESIG		VIR		COL		R		C		STRUCTUR-2		A A A A A A A A A A					2 2					

R SVY 0.00 0.00 S004 READING IS ACTUALLY 212 DEG BUT IS UNCERTAIN, THEREFORE
R SVY 0.00 0.00 208 IS CHOSEN FOR MAPS.

G E O L O G

A UMI	A LAB	A TYP	A MTH	SAMPLE SERIAL NUMBER	% PH B.CLG H-CORE	% ZN B.CLG H-CORE	% BA B.CLG H-CORE	OZ AG B.CLG H-CORE	% CU B.CLG H-CORE	% FE B.CLG H-CORE	OZ AU B.CLG H-CORE	% CD B.CLG H-CORE	HASH
					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BUNBAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WFT ANALYSIS.									
R ASY	0.00	0.00		LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	231.40	232.50	80	RS9814	0.02	-0.01	0.02	0.09	0.02	3.95	-0.1	-0.1	3.89
A 001	232.50	234.90	144	RS9815	0.04	0.01	0.07	0.06	0.02	6.00	-0.1	-0.1	6.00
A 001	234.00	235.20	96	RS9816	0.19	-0.01	0.05	0.08	0.02	10.85	-0.1	-0.1	10.98

A MIN		0.02	-0.01	0.02	0.06	0.02	3.95	-0.1	-0.1	3.86
A MAX	231.40 235.20	0.19	0.01	0.07	0.09	0.02	10.85	-0.1	-0.1	11.03

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BASIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE :80-DH056

COLLAR ELEVATION: 1230.00

AZIMUTH(DEG) : 228.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 23.62

NORTHING(- IF S): 7002464.00

VERTICAL ANGLE : -70.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : HQ

EASTING (- IF W): 436749.62

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

R HED

HOLE LOST AND TERMINATED.

F	-	I	N	T	E	R	V	A	L	-	CORE	T	-	%	TYPT	-	HAL	TFX	-	GRAIN	PGI	STRUCTUR	-	1	ALTERATION	MINS	ORE	-	TYPE	MINS	SUMMARY															
K	L	(UNITS =									REC'D	-	M	M	ROCK	FLYING	MIN	TUPES	CHARACS																											
F	A	(MT=METRIC FT=FOOTRIC)									ERY		D	I		1	4	TM	HAT	TX	TX	F	C	Z	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-	
Y	G	F	R	O	M	-	T	O	-	J	N	I	(.)	D	X	TYPE	1	2	OM1	1	2	F	F	C	A		1	AZM	RT	DZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
K	F										ROCK		FM		RT		1	4	TM	HAT	TX	TX	F	C	Z	M	ARG	/RI	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L										QUAL		AGE	EN	-	0	LC	-	3			3	4	0		/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1			
Y	G										DESIG		VIR		COL														STRUCTUR	-	2	A	A	A	A	A	A	A	A	A	A	2	2			

R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASIN PR-ZR-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 80-DH057	COLLAR ELEVATION: 1159.40	AZIMUTH(DEG) : 75.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 17.98	NORTHING(= IF S): 7601814.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : NN	EASTING (= IF E): 436572.31	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-RECC

R HED

HOLE LOST AND TERMINATED.

F - INTERVAL -		CORE	T- %	TYPI- DAL	TEX-	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECOV-	R M ROCK	TYING MIN	TURES	CHARACS			H H H H H	ANY H	H H H	ANY	ALT ORE
F A	(METRIC FT=FOOTRIC)	ERY	0 T	12 TM MAT	TX TX	F C % M ARG	/RI T	ID STK DIP	A A A A A	MIN A	A A A	MIN	- - - -
Y G	F R O N - T O - I N T (.)	D X TYPE	1 2 QM1	1 2 F F C A			1	AZM RT QZ FL CY CA BA XX PY CP GL YY					A 1 A 2

K F		ROCK	FM RT	TH QM2	TX TX	S C O O CHT	T	ID STK DIP	MG MU CL SD QS	HA PR	MT SL	HA	
E L		QUAL	AGE FM- Q LC- 3	3 4 0	/		2	AZM RT H H H H H	H H H H H				1 1
Y G		DESIG	VIR COL		R C			STRUCTUR-2	A A A A A	A A A A A			2 2

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASOP PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 80-DH058

COLLAR ELEVATION: 1451.20

AZIMUTH(DEG) : 225.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 170.99

NORTHING(- IF S): 7003984.00

VERTICAL ANGLE : -70.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 80

EASTING (- IF W): 435041.62

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-RECC

SEQ. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	32.31	224.00	-70.00
2	93.27	224.00	-60.00
3	163.37	224.00	-54.00

F - J N T E R V A L -		CORE	T- %	TYPT- GAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC. PLACE)	RECOV-	N H ROCK	FYING MIN	TURES	CHARACS		H H H H H ANY	H H H ANY	ALT ORE
E	A (MT=METRIC FT=FOOTRIC)	ERY	I	TX TX	TX TX	F C % M ARG	/RI	T ID STK DIP	A A A A A MIN	A A A MIN - - -
Y	G F R U M - T D - I N T (.)	D X TYPE	1 2	UM1	1 2	F F C A	1	AZM RT QZ FL CY CA BA	XX PY CP GL YY	A 1 A 2

K	F	ROCK	FR	RT	TX TX	S C O O CHT		T ID STK DIP	MG MU CL SD QS HA PR MT SL HA	
E	L	DUAL	AGE EN- N LC- 3		3 4 0	/	2	AZM RT H H H H H H H H		1 1
Y	G	DESIG	VIR	COL		R C		STRUCTUR-2	A A A A A A A A A A	2 2

R SVY 0.00 0.00 S002 AZIMUTH WAS RECORDED AS 221 BUT IS UNCERTAIN.

R SVY 0.00 0.00 SPERRY SUN TESTS.

R ASY 0.00 0.00 NO ASSAY VALUES FOR THIS HOLE.

G E O L O G F O I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-2N-AG-PA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 89-DH059

COLLAR ELEVATION: 1407.20

AZIMUTH(DEG) : 205.00

GEOLOGGED BY : HDG +

TOTAL DEPTH/LENGTH : 153.31

NORTHING(= IF S): 7604797.00

VERTICAL ANGLE : -50.00

DATE (YY/MM/DD): 810826

CORE/HOLE DIAMETER : NO

EASTING (= IF S): 433273.44

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-END

SFD. NO OF
SURVEY DATALENGTH FROM COLLAR
TO SURVEY POINTAZIMUTH
(DEG)VERT. ANGLE
(DEG)

1	91.40	195.00	-51.00
2	121.90	187.00	-52.00
3	152.40	186.00	-49.50

R HED

ORIGINALLY LOGGED BY ANGIE STARIA IN JULY 1980.

F - I N T E R V A L -		CORE T- %		TYPI- QAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION MINS		ORE-TYPE MINS		SUMMARY															
K	L (UNITS = . DEC.PLACE)RECOV- R = ROCK	E	A (MT=METRIC FT=FOOTRIC) ERY	O	I	1	2	UN1	1	2	F	F	C	A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
K	F	ROCK	FM	RT	IM	Q2	TX	TX	S	C	O	O	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L	QUAL	AGE	EN- R	LC- 3		3	4	O	/				2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G	DESIG	VTR	COL					R	C					STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

/ OVR 0.00 15.24 15.24

OVER

P

/ 15.24 118.72 103.48

ARGL CR

LM 0 2) 3

P 0 LM 45

B+

L 15.24 118.72

3A

MX 9

<+

R 15.24 118.72

TO GENERAL, THIS CARBONACEOUS ARGILLITE IS FAINTLY LAMINATED

R 15.24 118.72

WITH SILT TO SAND SIZE PARTICLES. EUHEDRAL PYRITE CUBES OCCUR

R 15.24 118.72

AT INTERVALS AVERAGING .4CM IN DIAMETER. QUARTZ-SIDERITE VEINS

R 15.24 118.72

ARE PREVALENT AND ARE PROBABLY RESPONSIBLE FOR MINOR DEFORMATION

R 15.24 118.72

WITHIN THE ARGILLITE INTERVAL. OVERALL, THE ROCK RECOVERY AND

R 15.24 118.72

ROCK QUALITY IS POOR.

/ 19.81 20.02 0.21

X ARGL SF

LM 0 2) 3

R 0 LM 45

D*

L 19.81 20.02

V3

/ 26.17 26.40 0.23

1 BRHM

SS

LM9

R

FO

40

B1

L 26.17 26.40

4T

5

<+

R 26.17 26.40

PYRITE OCCURS AS EUHEDRAL CUBES THAT AVERAGE .5CM IN DIAMETER.

/ 26.28 28.42 0.14

8 SILT

0 2 6 2

R

B=

L 26.28 28.42

ST

LC LM 8

<)

/ 30.57 32.41 1.84

7 BRHM CR

SS

LM9

R

B+

L 30.57 32.41

3A

4

<+

R 30.57 32.41

SOFT SEDIMENT SLUMP WITHIN THE ARGILLITE HAS RESULTED IN MINOR

R 30.57 32.41

BRECCIATION. PYRITE OCCURS MAINLY AS EUHEDRAL CRYSTALS, HOWEVER

R		30.57	32.41	IT ALSO OCCURS IN VEINS WITH A QUARTZ ENVELOPE.											
/	L	33.25	37.75	4.50	X ARGL CR		BR 0 3 2 3		R 0 LM	45	#+	B+			
R		33.25	37.75	THE QUARTZ-SIDERITE VEINS SURROUND THE ANGULAR, ARGILLIC BRECCIA FRAGMENTS.											
/	L	39.62	41.12	1.50	X ARGL SF		LM 0 2) 3		R 0 LM	45	V=	<)	B=		
R		39.62	41.12	THIS INTERVAL IS BADLY BROKEN. THE EUBEDRAL CUBES OF PYRITE											
R		39.62	41.12	AVERAGE .7CM IN DIAMETER.											
/	L	45.58	46.20	0.62	X ARGL CR		LM 0 2) 3		R 0 LM	45 E+		B+	S)		
R SPC		45.58	46.20	SAMPLE D.G. 205 TAKEN AT 45.58 METRES.											
/	L	47.24	48.12	0.88	X ARGL CR		LM 0 2) 3		R 0 LM	45		B+	B=		
/ FLT		52.43	52.88	0.45	X ARGL CR	GG6	LM 0 2) 3		R 0 LM	45 V=		B+	D+		
R		52.43	52.88	THIS ZONE IS HEAVILY GOUGED AND BROKEN. THE FINE WHITE POWER WITHIN THE ARGILLITE IS PROBABLY WEATHERED QUARTZ.											
/	L	54.35	62.80	8.45	X ARGL CR		LM 0 2) 3		R 0 LM	50 <)		B+	D+		
/	L	66.14	103.43	37.29	X ARGL CR		LM 0 2) 3 LC		R 0 LM	45		B+	D=		
R SPC		66.14	103.43	SAMPLE D.G. 206 TAKEN AT 75.90 METRES. THIS SAMPLE HAS QUARTZ- SIDERITE VEINS SURROUNDING BRECCIATED ARGILLITE CLASTS. SAMPLE P.G 207 TAKEN AT 92.63 METRES. THIS SAMPLE CONTAINS CONVOLUTED VEINS OF QUARTZ-SIDERITE.											
R		66.14	103.43												
R		66.14	103.43												
R		66.14	103.43												
/ FAL		103.43	114.30	10.87	X ARGL GP	GG2	LM 0 2) 3		R 0 LM	45		B+	D=		
R SPC		103.43	114.30	SAMPLE DG 208 TAKEN AT 103.51 METRES. QUARTZ-SIDERITE VEINS ENVELOPE GRAPHITIC ARGILLITE FRAGMENTS. SAMPLE D.G. 172 TAKEN AT 115.52 METRES. THE MATRIX CONSISTS OF SAND SIZED GRAINS.											
R		103.43	114.30												
R		103.43	114.30												
R		118.72	119.27												
/	L	118.72	122.68	3.96	CGBR SF	*C1	F*	KM1	P	V=			D+		
					SA	B*	3	KN4							
/	L	118.72	119.27	0.55	X BRPM SF	*C=	F*	KL1	R	V1			D+		
					SA	B*	3	O KL2							
R SPC		118.72	122.68	SAMPLE DG 171 TAKEN AT 120.52 METRES.											
/	L	121.95	122.68	0.73	X CGBR SF	*C1	F*	KM1	R	V=			D+		
R		121.95	122.68	AROUND THE CHERT BRECCIA CLASTS ARE SWIRLS OF CARBONACEOUS											

R		121.95	122.68													
X \$SX		122.68	122.68	0.00												
/		122.68	123.50	0.82	CHER	CH6		JK*	P	FO	50		L1	D1		
L					BA	RR BN		LN6				<=	L)	L1		
R		122.68	123.50		BANDS OF SULPHIDES PINCH OUT INTO SMALL VEINLETS, THAT AVERAGE LESS THAN .1MM. SPHALERITE BANDS ARE MAUVE TO LIGHT BROWN IN COLOUR AND AVERAGE 3MM. IN WIDTH. GALENA IS ASSOCIATED WITH THE SPHALERITE AS MEDIUM GRAINED CUBES. IT ALSO OCCURS AS DISSEMINATED, FINE GRAINED CRYSTAL IN THE MILDLY BRECCIATED											
R		122.68	123.50		CHERT AND LARGE Euhedral crystals in quartz-siderite lined vugs.											
R		122.68	123.50		PYRITE AND PYRROTHITE PREDOMINANTLY OCCUR IN VEINLETS ENVELOPES OF QUARTZ-SIDERITE ARE COMMON AROUND DISCONTINUOUS BANDS OF SPHALERITE.											
R SPC		122.68	123.50		SAMPLE D.G. 170 TAKEN AT 123.0 METRES (T.S.).											
/		123.50	124.00	0.50	CHER	CH6		JK*	P	FO	50		L1	D1		
L																
/		124.00	125.00	1.00	CHER	CH4		JK*	P	FO	50		M2	D2		
L															M=	D1
R		124.00	125.00		FE-SULPHIDES OCCUR AS MASSIVE, FINE GRAINED, ANHEDRAL CRYSTALS WITH SMALL CROSSCUTTING VEINLETS OF QUARTZ-SIDERITE. Euhedral,											
R		124.00	125.00		MEDIUM GRAINED GALENA APPEARS IN VUGS AND INTERSTITIAL SPACES.											
R SPC		124.00	125.00		SAMPLE D.G. 169 TAKEN AT 124.3 METRES (P.T.).											
/		125.00	126.00	1.00	\$SSX SF	CH2	MX		P		V=		V3	D2		
L					3T		VG					<)	B1	D1		
R		125.00	126.00		GALENA OCCURS IN 1MM VEINLETS AND AS DISSEMINATED CRYSTALS, WITH SPHALERITE, IN A SILICIOUS MATRIX.											
R SPC		125.00	126.00		SAMPLE D.G. 168 TAKEN AT 125.4m (P.T).											
R		125.00	126.00		CHERT RICH INTERVALS ARE FROM 10-30CMS WIDE, AND OCCUR BETWEEN MASSIVE SULPHIDE INTERVALS OF 15-40CMS IN WIDTH.											
R		125.00	126.00													
/		126.00	127.00	1.00	\$SSX SF	CH2	MX		P		V=		V3	D2		
L																
/		127.00	128.00	1.00	\$SSX SF	CH2	MX		P		V=		V3	D2		
L																
/		128.00	129.00	1.00	\$SSX PY		MX BN		P		<+		M3 B(<2			
L															M3 M)	M1 <1
R		128.00	129.00		GALENA, SPHALERITE AND QUARTZ OCCASIONALLY OCCUR IN BANDS, PYRITE AND SIDERITE OCCUR AS MASSIVE PATCHES. VEINLETS OF											
R		128.00	129.00		GALENA, SPHALERITE AND CHALCOPYRITE RUN BETWEEN THESE MASSIVE AREAS IN A BOXWORK STRUCTURE. PYRROTHITE IS CLOSELY ASSOCIATED											
R		128.00	129.00		WITH THE PYRITE. LARGE LENSES OF WHITE Euhedral, MEDIUM GRAIN QUARTZ IS COMMON OPEN SPACE FILLING TEXTURES ARE PREVALENT.											
R SPC		128.00	129.00		SAMPLE D.G. 167 TAKEN AT 128.3 METRES (P.T.).											
/		129.00	130.00	1.00	\$SSX PY		MX BN		P		<+		M3 B(<2			
L																

[illegible]

1	152.70	153.31	0.61	ARSI	LC	P	V=
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U.S. OFFICE, BY APPOINTMENT

A UMH	SAMPLE				% PB	% ZN	% BR	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL				B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP					H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00	B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	WA = WET ANALYSIS.										
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -0.1. E.G. -0.01										
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1										
A 001	120.40	122.53	166	8460	0.04	0.03	-0.01	0.05	0.03	8.27	-0.01	-0.1	8.30
A 001	122.63	123.50	056	8461	5.55	5.50	0.01	1.54	0.02	12.70	-0.01	-0.1	25.21
A 001	123.50	124.00	050	8462	7.97	5.45	-0.01	1.60	-0.01	6.50	-0.01	-0.1	21.39
A 001	124.00	125.00	100	8463	8.55	5.10	0.02	2.07	0.02	19.18	-0.01	-0.1	34.83
A 001	125.00	126.00	100	8464	9.35	4.00	-0.01	2.50	0.03	34.32	-0.01	-0.1	50.08
A 001	126.00	127.00	100	8465	8.13	4.65	-0.01	2.53	0.02	25.91	-0.01	-0.1	41.12
A 001	127.00	128.00	100	8466	7.05	5.30	-0.01	2.16	0.02	28.22	-0.01	-0.1	42.63
A 001	128.00	129.00	100	8467	13.50	3.00	-0.01	3.18	0.03	33.01	-0.01	-0.1	52.60
A 001	129.00	130.00	100	8468	16.65	4.65	-0.01	3.95	-0.01	27.17	-0.01	-0.1	52.29
A 001	130.00	131.00	100	8469	8.40	1.58	-0.01	2.10	0.03	33.67	-0.01	-0.1	45.66
A 001	131.00	132.00	100	8470	11.76	3.00	-0.01	2.82	0.03	32.10	-0.01	-0.1	49.59
A 001	132.00	133.00	100	8471	11.31	3.73	-0.01	2.64	0.01	34.27	-0.01	-0.1	51.84
A 001	133.00	134.00	100	8472	12.99	9.35	-0.01	2.97	0.01	24.80	-0.01	-0.1	50.00
A 001	134.00	135.00	100	8473	12.79	3.50	-0.01	2.78	0.02	29.84	-0.01	-0.1	48.81
A 001	135.00	136.00	100	8474	9.18	2.62	-0.01	1.87	0.01	31.40	-0.01	-0.1	44.96
A 001	136.00	137.00	099	8475	26.51	1.27	-0.01	5.21	0.01	26.04	-0.01	-0.1	59.02
A 001	137.00	138.00	099	8476	6.50	1.67	-0.01	1.54	0.01	33.16	-0.01	-0.1	42.76
A 001	138.00	139.00	097	8477	2.97	1.61	-0.01	0.93	0.01	35.63	-0.01	-0.1	41.03
A 001	139.00	140.00	093	8478	4.40	4.10	-0.01	1.23	0.02	26.07	-0.01	-0.1	35.70
A 001	140.00	140.60	056	8479	13.97	3.15	0.01	3.15	0.03	20.49	-0.01	-0.1	40.69
A 001	140.60	142.10	141	8480	6.91	1.26	-0.01	1.78	0.01	11.09	-0.01	-0.1	20.93
A 001	142.10	143.00	087	8481	0.28	0.10	-0.01	0.07	-0.01	5.24	-0.01	-0.1	5.56
A 001	145.48	148.96	037	8482	3.12	0.13	-0.01	0.76	0.03	10.24	-0.01	-0.1	14.16
A MAX	120.40	148.96			26.61	9.35	0.02	5.21	0.03	35.63	-0.01	-0.1	76.74

A MIN				0.04	0.03	-0.01	0.05	-0.01	5.24	-0.01	-0.1	5.23
A CMP	122.68	137.00	1413	11.51	4.12	-0.1	2.71	-0.1	27.40	-0.1	-0.1	45.34
A CMP	122.68	142.10	1900	10.16	3.61	-0.01	2.43	0.02	26.64	-0.1	-0.1	42.65

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASIN PR-74-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

COLLAR ELEVATION: 1407.20
NORTHING (- IF S): 7004797.00
EASTING (- IF W): 433273.44

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AZIMUTH( DEG ) : 205.00
VERTICAL ANGLE : -70.00
CO-ORD SYSTEM : UTM

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GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-END

VERT. ANGLE
(DEG)

1	30.48	209.70	-69.00
2	57.91	215.00	-68.00
3	88.39	214.00	-67.00
4	118.87	208.00	-64.50
5	149.35	206.00	-62.00
6	182.88	195.00	-61.00
7	213.36	191.00	-61.00
8	240.79	189.00	-60.00

F - I N T E R V A L - CORF T- %										PGI										STRUCTUR-1										ALTERATION MINS										ORE-TYPE MINS										SUMMARY									
L (UNITS = . DEC.PLACE)RECDV- R M ROCK										FYJIG MIN TURES CHARACS										/RI T ID STK DIP										H H H H H ANY H H H ANY										ALT ORE																			
F A (MT=METRIC FT=FOOTRIC) FRY D I										TM IN MAT TX TX F C % M ARG										1 AZM RT QZ FL CY CA BA XX PY CP GL YY										A 1 A 2																													
Y G F R D N - T D - I N T (.) D X TYPE										1 2 NM1 1 2 F F C A										1																																							
K F										TM RM2 TX TX S C U O CHT										T ID STK DIP MG MU CL SD QS HA PR MT SL HA																																							
E L										QUAL AGE EN- D LC- 3 3 4 D /										2 AZM RT H H H H H H H H H H										1 1																													
Y G										DESIG VIR COL R C										STRUCTUR-2 A A A A A A A A A A										2 2																													

R SVY	0.00	0.00	SPEERY SUN TESTS.
R SVY	0.00	25.60	HOLE TRICONED TO BYPASS BROKEN GROUND.
R SVY	0.00	145.66	NO CORE; 145.66-242.32(END) NO CORE.
R SVY	30.48	57.91	AZIMUTH HAS BEEN EXTRAPOLATED.

A UMM				SAMPLE	% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BONDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		LESS THAN DETECTION LIMIT ENTERED AS -0.L, E.G. -0.01									
R ASY	0.00	0.00		NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	128.76	129.76	100	KL9327	-0.01	1.28	0.08	-0.05	-0.01	5.45	-0.002	-0.1	6.638
A 001	129.76	130.31	52	KL9328	0.01	0.12	0.09	0.04	0.01	4.50	-0.002	-0.1	4.668
A 001	130.31	131.03	61	KL9329	0.01	8.20	0.01	0.06	0.01	5.55	-0.002	-0.1	13.738
A 001	184.32	185.32	91	8548	0.05	-0.01	0.12	0.06	-0.01	4.13	-0.002	-0.1	4.238
A 001	185.32	186.32	100	8531	0.48	0.12	0.01	0.09	0.03	33.18	-0.002	-0.1	33.808
A 001	186.32	188.64	224	8532	7.91	0.08	-0.01	2.09	0.02	34.50	0.002	-0.1	44.492
A 001	188.64	189.77	103	8533	11.50	0.10	0.01	2.12	0.03	18.55	0.002	-0.1	32.212
A 001	189.77	191.57	172	8534	13.20	0.34	0.06	1.90	0.01	10.15	-0.002	-0.1	25.558
A 001	191.57	192.57	98	8549	0.13	0.11	0.09	0.04	0.01	8.55	0.002	-0.1	8.832
A CMP	186.32	191.57	525		10.50	0.17	0.03	2.03	0.02	22.72	0.002	-0.1	35.372

A MIN		-0.01	-0.01	-0.01	-0.05	-0.01	4.50	-0.002	-0.1	4.308
A MAX	128.76 191.67	13.20	8.20	0.12	2.12	0.03	34.50	0.002	-0.1	58.072

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G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILL HOLE/TRAVERSE : 89-DH061	COLLAR ELEVATION: 1277.00	AZIMUTH(DEG) : 216.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 203.30	NORTHING(= IF S): 7002478.00	VERTICAL ANGLE : -78.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : HQ	EASTING (= IF N): 436545.87	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	15.24	214.00	-78.00
2	30.48	211.50	-78.50
3	45.72	209.00	-77.00
4	60.96	207.50	-72.50
5	76.20	206.00	-69.00
6	91.44	204.00	-67.00
7	106.64	202.00	-67.00
8	121.92	195.00	-67.00
9	137.16	195.00	-65.00
10	152.40	194.00	-63.50
11	167.64	194.00	-62.00
12	182.88	194.00	-59.50
13	198.12	194.00	-59.00

F	- I N T E R V A L -	CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECOV-	M M ROCK	FYING	MINS	TURES	CHARACS					
F	A (METRIC FT=FOOTRIC)	ERY	D I	TM	IN	TX	TX	F C % M	ARG	/RI	T ID	STK DIP
Y	G F R D M - T D - I N T (.)	D X	TYPE	1	2	NM1	1	2	F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2
K	F	ROCK	FM	RT	TX	TX	S C O O	CHT				
E	L	QUAL	AGE	FM- D I C- 3		3	4	0	/		2	AZM RT H H H H H H H H H H 1 1
Y	G	DESIG	MTR	COL			R	C				STRUCTUR-2 A A A A A A A A A A 2 2

R SVY 0.00 0.00 SPERRY SUN TESTS. AZIMUTH WITH INCONSISTENT TRENDS HAVE BEEN

R SVY 0.00 0.00 DELETED.

R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE.

R ASY 30.48 45.72 AZIMUTH HAS BEEN EXTRAPOLATED.

R ASY 60.96 76.20 AZIMUTH HAS BEEN EXTRAPOLATED.

R ASY 91.44 106.64 AZIMUTH HAS BEEN EXTRAPOLATED.

R ASY 167.64 182.88 AZIMUTH HAS BEEN EXTRAPOLATED.

R ASY 182.88 198.12 AZIMUTH HAS BEEN EXTRAPOLATED.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-7A-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :80-04062
TOTAL DEPTH/LENGTH : 135.64
CORE/HOLE DIAMETER : 40COLLAR ELEVATION: 1373.80
NORTHING(- IF S): 7004611.00
EASTING (- IF W): 434316.19AZIMUTH(DEG) : 27.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-END

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.48	30.00	-50.00
2	60.96	31.00	-49.00
3	91.44	33.00	-48.00
4	135.64	31.00	-48.00

F - I N T E R V A L -		CORE	T- %	TYPI- NAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = DEC.PLACE)RECUV-	M M ROCK	RYING MIN	TURES	CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E	A (MT=METRIC FT=FOOTRIC) ERY	G T	TM TM MAT	TX TX F C % M	ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y	G F R O M - I D - I N T (.)	D X TYPE	1 2 NM1	1 2 F F C A			1 AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K	F	ROCK	FM	RT	TM NM2	TX TX S C G O	CHT	1 ID STK DIP MG MU CL SD QS HA PR MT SL HA		
E	L	QUAL	AGE EN- D	LC- 3	3 4 D	/	2	AZM RT H H H H H H H H H H	1 1	
Y	G	DESIG	VIR	CUL	R	C		STRUCTUR-2 A A A A A A A A A A	2 2	

R SVY 0.00 0.00 SPERRY SURV TESTS.

A UMM				SAMPLE	% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB				SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP				NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH					WA	WA	WA	WA	WA	WA	WA	WA	
R ASY	0.00	0.00		B.CLG = BOGDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00		WA = WET ANALYSIS.									
R ASY	0.00	0.00		LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01									
R ASY	0.00	0.00		ED ASSAY INFORMATION ENTERED AS -0.1									
A 001	83.85	84.85	46	AH8565	0.02	0.02	0.12	0.07	0.01	5.90	-0.1	-0.1	5.94
A 001	84.85	85.85	40	AH8566	2.90	0.14	0.07	0.67	0.02	7.00	-0.1	-0.1	10.60
A 001	85.85	86.07	22	AH8567	4.85	6.90	0.12	1.84	0.02	27.10	-0.1	-0.1	40.63
A 001	86.07	87.07	59	AH8568	4.50	1.16	0.05	0.95	0.01	4.58	-0.1	-0.1	11.05
A 001	87.07	88.07	40	AH8569	4.20	2.35	0.09	0.83	0.01	3.80	-0.1	-0.1	11.08
A 001	88.07	89.07	44	AH8570	4.13	2.16	0.07	0.65	0.02	12.15	-0.1	-0.1	18.98
A 001	89.07	90.07	46	AH8571	1.16	0.92	0.04	0.36	0.02	10.30	-0.1	-0.1	12.60
A 001	90.07	90.42	16	AH8572	0.84	1.02	0.05	0.15	0.01	4.73	-0.1	-0.1	6.60
A 001	90.42	91.28	40	AH8573	1.59	0.54	0.03	0.25	0.01	6.10	-0.1	-0.1	8.32
A 001	91.28	91.44	16	AH8574	8.00	5.25	0.09	1.95	0.02	18.20	-0.1	-0.1	33.31
A 001	91.44	92.22	37	AH8575	2.70	1.05	0.03	0.53	0.01	16.60	-0.1	-0.1	20.72
A 001	92.22	93.22	40	AH8576	0.20	0.07	0.09	0.14	0.01	6.63	-0.1	-0.1	6.94
A 001	93.22	96.01	84	AH8577	0.04	0.04	0.11	0.07	0.01	10.25	-0.1	-0.1	10.32
A 001	96.01	97.54	00		-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.80
A 001	97.54	100.58	49	AH8578	0.02	0.02	0.04	0.02	-0.01	7.90	-0.1	-0.1	7.79
A CMP	85.85	89.07			4.32	2.23	0.70	0.88	0.01	8.23	-0.1	-0.1	16.17
R ASY	85.85	89.07		ACMP OVER 3.22M HAS A TRUE THICKNESS OF 2.54M.									

A MIN		-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.1	-0.80
A MAX	83.85 100.58	8.00	6.90	0.12	1.95	0.02	27.10	-0.1	-0.1	43.89

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASIR PR-ZN-AG-BA-SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :80-DH063
TOTAL DEPTH/LENGTH : 591.62
CORE/HOLE DIAMETER : HUNDCOLLAR ELEVATION: 1295.40
PORTING(- IF S): 7002611.00
EASTING (- IF W): 435463.25AZIMUTH(DEG) : 183.00
VERTICAL ANGLE : -72.67
CO-ORD SYSTEM : UTMGEOLOGGED BY : JDK + JER
DATE (YY/MM/DD): 810611
PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	3.05	183.27	-71.77
2	30.48	183.22	-70.88
3	60.96	181.45	-70.64
4	91.44	179.11	-68.60
5	121.92	175.12	-62.59
6	152.40	173.57	-61.94
7	182.88	173.58	-60.62
8	213.36	174.52	-58.49
9	220.98	174.55	-57.63
10	228.60	174.14	-56.58
11	236.22	174.03	-55.70
12	243.84	175.06	-54.85
13	274.32	175.45	-52.77
14	304.80	175.43	-50.72
15	335.28	176.28	-49.42
16	365.76	178.39	-47.43
17	396.24	179.18	-45.57
18	426.72	177.51	-41.87
19	457.20	176.02	-37.50
20	487.68	175.36	-34.77

F	- I N T E R V A L -	CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)RECUV-	M H ROCK	FYING MIN	TURES	CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E	A (M=METRIC FT=FOOTRIC) ERY	U I	TM TM MAT	TX TX F C % M ARG	/RI T ID STK DIP	A A A A A MIN A A A MIN				
Y	G F R O M - T O - T N T (.)	D X TYPE	1 2 DM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K	F	ROCK	FR	RT	TM QM2 TX TX S C O O CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA			
E	L	QUAL	AGE	EN- N LC- 3	3 4 0 /	2	AZM RT H H H H H H H H H	1 1		
Y	G	DESIG	VIR	COL	R C		STRUCTUR-2 A A A A A A A A A	2 2		

R SVY	0.00	0.00	DATA REPRESENTS MERGER OF GYROSCOPIC SURVEY DATA OBTAINED FR	
R SVY	0.00	0.00	THE UPPER PART OF THE DETAILED SURVEY OF DDH 80-638 WITH THE	
R SVY	0.00	0.00	LESS DETAILED (LOWER PART OF HOLE) GYROSCOPIC SURVEY OF	
R SVY	0.00	0.00	DDH 80-63. (IE: 0.0 - 243.84M FROM DDH 80-638).	
R SVY	251.77	251.77	HALL AND ROBE STEEL WEDGE. FULL STEEPENING.	
R SVY	359.97	359.97	HALL AND ROBE STEEL WEDGE. FULL STEEPENING.	
R SVY	398.07	398.07	HALL AND ROBE STEEL WEDGE. FULL STEEPENING.	

/ OVR	0.00	4.75	4.75	OVER	P
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/	4.75	18.90	14.15	TRIC	P
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/ RET	18.90	34.05	15.16	0.5	BR44	*S=	MQ9	P	D*
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L						1A	C		
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[illegible][illegible]

[illegible]

[illegible]

R	507.60	512.00	NODULE-LIKE PY MAY BE REPLACED SAND CLASTS. MATRIX BRPM.									
/	508.70	508.90	0.20	X BRBT	*C= R* H*	NR8	R	<+			85	
L												
/	510.70	510.80	0.10	X BRBT	*C= R* H*	NR8	R	>3		>=	61	
L										>)		
/	512.00	513.40	1.40	BRPM	*C3 R* H*	MQ2	P	<1			R1	
L				2A		LO3				C.		
/	513.40	518.20	4.80	BRBT SF	*C= R* H*	NR8	P	<+			71	
L				1A	*S=	C KO=				C.		
/	518.20	524.46	6.26	ARSI SF	RR SS		P	2 BD	50	<1	61	
L				1A	//			CV	30		C.	
/	518.20	518.75	0.55	X ARSI SF CR	// SS		R	2 BD	50	<1	61	
L				1A	SS			CV	30		C.	
R	518.20	524.46	ARGL BEDS WITH SILT LM.									
/	520.40	524.46	3.97	X ARSI SF	// NO		R	2 BD	50	<)	63 R L.	
L					BD LM						L.	
R	520.40	524.46	PY AS LM REPLACEMENT, BLERS, RARE NODULES, SELVAGES IN QZ-VEINS.									
R	520.40	524.46	NOTE: HALF CORE SAMPLES TAKEN, BUT NO ASSAY RESULTS, ONLY									
R	520.40	524.46	GEOCHEM.									
/	523.43	523.70	0.27	X VEIN			R	>9		>*		
L										C. >)		
K US2	524.46	524.46	0.00									
/	524.46	527.30	2.84	LMSX SF SL CH3 SS LC		P	2 BD	70	V1	L1	7+ 6=	
L				4A GL // IR			1 LM	70			L=	
R	524.46	527.30	CHERT (2-5CM) INTERBEDDED WITH SULPHIDE/ATE LM. LOCAL SULPHIDE									
R	524.46	527.30	(GL, PY) MICROVEINS.									
/	525.15	525.30	0.15	X VEIN			R	>9		>*	B.	
L										C. >)	B.	
/	526.70	527.30	0.60	X ARSI SF	//		R	2 BD	45	>1	83 R+ B.	
L				1A				CV	45		C. B*	
/	527.30	528.30	1.00	LMSX SF SL CH=	// IR		P	1 LM	050	V1	L1 7+ 6=	
L				6A	XP LC			CV	50			
/	527.30	528.30	1.00	5 ARGL SF	SIS IR // 0 1 5 2		R	2 BD	50			
L				1A	SC XB 6			CV	50			
R	527.30	528.30	PARALLEL LM MILDLY LC. QZ-VEINS CUT BY SC. ARGL TRUNCATED BY									
R	527.30	528.30	LSX.									
R	527.30	528.30	VERY SILTY ARGILLITE INTERBEDDED WITH LMSX.									

K	F	F	R	D	I	I	N	T	RECDV	MD	%	ROCK	TR	TM	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L
Y	G	G	G	G	G	G	G	G	R	Q	D	AGE	EV	RG	LC	TM	QM2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

K LS2 528.30 528.30 0.00

/ 528.30 529.30 1.50
LARGL SF
1A S12 // SS012 P 2 BD 50 V1
7 CV 50

83 L+ B(

/ 529.80 538.34 8.54
LARGL SF
1A S12 // SS012 P 2 BD 35 <=
7 CV 35

C. <1 8= B.

R 529.80 538.34 INTERMITTANTLY SILICIFIED.

/ 534.60 534.80 0.20
L

X ARGL SF S12 BR SS

012 R 2 BD 50 >7

>7 82 B(

/ 536.00 536.20 0.20
L

X ARGL SF S12 // SS

012 R 2 BD 50 V1

83 B6 B(

/ 536.20 536.35 0.15
LX ARSN S14 FU // 0 3 4 3
3A 4

R 1 LM 045 >1

R2 B/

R 536.20 536.35 MAY BE REVERSE GRADING.

/ 536.35 538.34 1.99
L

X ARGL SF S12 BR SS

012 R 2 BD 50 <2

83 L+ B(

/ 538.34 540.80 2.46
LARSI SF S12 // SS 0 1 2 2
1A CH 6P 2 BD 40 <=
CV 40

C. L= L= L/

/ LSX 538.34 540.80 2.46
L4 LMSX // LC
6A CH1

R 1 LM 40

C. L4 L+

R 538.34 540.80 EARLY-CHERT LM BECOMING MORE FREQUENT.

R 538.34 540.80 SULPHIDE/ATE LM CONCENTRATED 539.3 TO 539.7 M.

/ 540.80 543.90 3.10
LARSI CR SF SI= // LC
1AP 2 BD 65 <=
CV 65

7+

/ 540.80 543.90 3.10
LX ARSI SF SF SI= // SS
1AR 2 BD 48 <=
CV 48

7+

R 540.80 543.90 SF LESS INTENSE IN LATTER PART OF UNIT.
R 540.80 543.90 SOFT SED. DEFORM. INCREASES/ 543.90 546.51 2.61
LBRPM SN3 F* B*
3A *C2LN1 P
L03

<+ <) R+

/ 543.90 544.20 0.30
LX BRPM SN2 F* B*
1A *C2 R* RRL06 R
MM2

<+ <) R+

R 543.90 546.51 ROUNDED ARGL, AND LARGE CHERT CLASSTS. SMALLER CHERT ANGULAR.
R 543.90 546.51 POORLY SORTED MATRIX OF CLAY TO SAND./ FAL 546.25 546.51 0.26
LX BRPM SN3 F* B*
GG9

LN1 R

<) R+

/ 546.51 548.80 2.29
L

LOST

P

			CR	BR SS
L				
R	587.35	591.62	CORE/BEDDING 40 TO 70 DEGREES. LESS CARBON AND MORE CARBONATE.	
R	587.35	591.62	NOT AS SILICIFIED AS PREVIOUS UNITS. KNIEST POORLY DEVELOPED.	

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASIN PB-ZR-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 90-DR064
TOTAL DEPTH/LENGTH : 204.96
CORE/HOLE DIAMETER : 80COLLAR ELEVATION: 1373.80
NORTHING(- IF S): 7004612.00
EASTING (- IF W): 433317.75AZIMUTH(DEG) : 207.00
VERTICAL ANGLE : -60.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-ENDSEQ. NO OF LENGTH FROM COLLAR AZIMUTH VERT. ANGLE
SURVEY DATA TO SURVEY POINT (DEG) (DEG)

1	46.02	212.00	-61.50
2	91.74	207.00	-61.00
3	143.56	207.00	-61.00
4	204.52	207.00	-60.00

F	UNIT	VAL	CORE	T	%	TYPT	CAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																			
K	L	(UNITS = . DEC.PLACE)	RECOV	R	R	ROCK	FI	IG	MIN	TURES	CHARACS	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE													
E	A	(M=METRIC FT=FOOTRIC)	FRY	D	I		TM	TM	NAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F R D M - T D - I N T (.)	D	X	TYPE	1	2	QM1	1	2	F	F	C	A			1		AZM	RT	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
K	F		ROCK	FR	RT	IN	QM2	TX	TX	S	C	O	O	CHT			2		AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1	
E	L		QUAL	AGE	EN	N	LC	3	3	4	O	/																							
Y	G		DESG	VIR	COL																														
R	SVY	0.00	0.00																																
R	ASY	0.00	0.00																																

SPERRY SUB TESTS

NO ASSAYS FOR THIS HOLE

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASIN PB-7M-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 80-DR065

COLLAR ELEVATION : 1411.00

AZIMUTH(DEG) : 210.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 238.05

NORTHING(- IF S): 7064735.00

VERTICAL ANGLE : -70.90

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 40

EASTING (- IF N): 433385.50

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-END

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	15.24	213.80	-68.20
2	30.48	214.60	-66.80
3	45.72	214.40	-66.80
4	60.96	213.20	-66.70
5	76.20	212.90	-66.80
6	91.44	213.40	-66.90
7	106.68	213.20	-66.50
8	121.92	212.40	-66.40
9	137.16	212.00	-65.60
10	152.40	213.50	-65.00
11	167.64	213.20	-64.80
12	182.88	213.00	-64.00
13	198.12	212.80	-62.30
14	213.36	212.05	-62.00

F - INTERVAL -		CORE	T- %	TYPT- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K L (UNITS = . DEC.PLACE)RECV-	M M ROCK	FR	RT	TX TX	FC % M ARG	/RI T	ID STK DIP	A A A A	A A A A	MIN A A A A	MIN A A A A	ALT ORE
E A (MT=METRIC FT=FOOTRIC) FRY	D I	TM TM	BAI	TX TX	F C % M ARG	/RI T	ID STK DIP	A A A A	A A A A	MIN A A A A	MIN A A A A	ALT ORE
Y G FROM - TO - INT (.)	D X TYPE	1 2 DM1	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A	1 2 F F C A
K F	ROCK	FR	RT	TX TX	S C O O CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA	1 1	1 1	1 1	1 1	1 1
E L	QUAL	AGE	EN- J	LC- 3	3 4 0 /	2 AZM RT	H H H H H H H H	1 1	1 1	1 1	1 1	1 1
Y G	DESIG	VIR	COL	R C		STRUCTUR-2	A A A A A A A A	2 2	2 2	2 2	2 2	2 2

R SVY 0.00 0.00 GYROCOMPASS SURVEY

R SVY 0.00 0.00 SPERRY SUD DATA NOT ENTERED.

R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN INTL LTD.

JASON PB-79-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 80-DH066
TOTAL DEPTH/LENGTH : 384.35
CORE/HOLE DIAMETER : 40MMCOLLAR ELEVATION: 1346.80
NORTHING (= 1F S): 7004394.00
EASTING (= 1F E): 433525.62AZIMUTH(DEG) : 31.00
VERTICAL ANGLE : -55.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-END

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	60.96	34.00	-55.50
2	289.86	34.00	-54.00
3	335.58	34.00	-54.00
4	384.35	30.00	-42.00

F	INTERVAL	CORE	T- %	TYPI- QUAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC. PLACE) RECDV- R M ROCK	FYING	MIN	TUBES	CHARACS							
F	A (METRIC FT=FOOTRIC) ERY	O I	TR TM	NAT TX TX	F C % M ARG	/RI	T ID	STK DIP	A A A A A	MIN A A A	MIN	- - -
Y	G F R O M - T O - I D T (.)	O X TYPE	1 2	QMI 1 2	F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2			
K	F	ROCK	FM	RT	TX TX	S C O O	CHT	T ID	STK DIP	MG MU CL SD QS HA PR MT SL HA		
F	L	QUAL	AGE	EN- N	LC- 3	3 4 0	/	2	AZM RT H H H H H H H H H H	1 1		
Y	G	DESIG	VIR	COL	R	C		STRUCTUR-2	A A A A A A A A A A	2 2		

R SVY 0.00 0.00 SPERRY SON TESTS.
 R SVY 0.00 0.00 REDUCED FROM HQ TO HQ AT 254.20 M.
 R ASY 0.00 0.00 NO ASSAYS FOR THIS HOLE.

G E O L O G F I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PH-ZN-AG-BASIF DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE : 80-08067	COLLAR ELEVATION: 1374.90	AZIMUTH(DEG) : 30.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 99.67	NORTHING(- IF S): 7004717.00	VERTICAL ANGLE : -50.00	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER : IN	EASTING (- IF E): 433152.12	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-END

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	52.43	34.00	-52.00
2	98.15	30.00	-51.50

F - I N T E R V A L -		CORE	I - Z	TYPI- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECOV-	M M ROCK	RYING MIN	TURES CHARACS			H H H H H	ANY H H H ANY	ALT ORE
E	A (M=METRIC F=FOOTRIC)	ERY	D 1	TH IN NAT	TX 1X F C % M ARG	/RI T	ID STK DIP	A A A A A	MIN A A A MIN	- - - -
Y	G F R O P - I O - I N T (.)	D X TYPE	1 2	MM1	1 2 F F C A	1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		

K	F	ROCK	FM	RT	TM MM2 TX TX S C O O CHT	T	ID STK DIP MG MU CL SD QS HA PR MT SL HA			
F	L	DUAL	AGE	ED- D	LC- 3 3 4 D /	2	AZM RT H H H H H H H H H	1 1		
Y	G	DESIG	VIR	COL	R C		STRUCTUR-2	A A A A A A A A A	2 2	

R SVY 0.00 0.00 SPERRY SON TESTS.

A ITEM			SAMPLE	% PB	% ZN	% RA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB			SERIAL	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	R.CLG	
A TYP			NUMBER	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH				WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 R.CLG = RONNAR CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 RA = RET ANALYSIS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A 001	77.72	80.50	150	9318	0.02	0.25	0.26	0.05	0.01	4.65	-0.01	-0.1	5.13
A 001	80.50	80.84	25	9301	1.32	0.02	0.01	0.41	0.06	24.75	-0.01	-0.1	26.46
A 001	80.84	81.24	24	9302	1.20	-0.01	-0.01	0.38	0.06	33.50	-0.01	-0.1	35.01
A 001	81.24	81.50	15	9303	0.22	0.01	0.02	2.44	0.03	24.70	-0.01	-0.1	27.31
A 001	81.50	82.91	33	9319	0.04	0.02	0.13	0.44	0.02	13.80	-0.01	-0.1	14.34

A MIN		0.02	-0.01	-0.01	0.05	0.01	4.65	-0.01	-0.1	4.60
A MAX	77.72 02.41	1.32	0.25	0.26	2.44	0.06	33.50	-0.01	-0.1	37.72

Z	61.19	68.70	7.51	BRHM	BR FL	MP7	P	CL	60	D)
L				3A	SS 3					
Z	61.19	62.80	1.61	X OVER	*S(BR FL	MP7	R	CL	60	D)
L				3A	SS 3	LN+				
R	61.19	68.70		CLEAVAGE MAY BE SLUMP CLEAVAGE.						
Z	64.05	65.15	0.30	X OVER	BR FL	MP7	R	CL	60	D)
L						MN)				
Z	66.70	77.00	8.30	BRHT	*S) BR B*	NR3	P			D(
L				4A	F* SS 2)	JD5				B.
Z	68.70	68.80	0.10	X FAUL	GGX		R			
L										
R	68.70	77.00		PY RESTRICTED MAINLY TO CLASTS.						
Z	73.76	74.33	0.57	X BRHM	BR FL	NR8	R			
L				2A	SS 4					
R	73.76	74.33		COMPRISES ONE LARGE CLAST THAT WAS DISRUPTED DURING TRANSPORT.						
Z	77.00	87.78	10.78	BRHT	*S) BR F*	OR5	P			D*
L				4A	B* 3)	JL3				D*
R	77.00	87.78		ARGL CLASTS BECOME COARSER UPHOLE. PY AND SD DISS MAINLY IN						
R	77.00	87.78		CLAST.						
Z	85.37	86.56	3.19	X BRHT	*S* BR B*	NS7	R			D*
L				2A	R* 1 *	MD2				D*
R	85.37	86.56		LARGE ARGL CLASTS INTERNALLY DEFORMED DURING TRANSPORT.						
Z	87.78	101.50	13.72	BRHT	*S* BR F*	NR6	P			D*
L				3A	B* FU 3 *	MD3				D.
R	87.78	101.50		CHERT CLASTS FINE UP. PV, SD & SL OCCUR MAINLY IN CLASTS.						
Z	89.86	90.10	0.24	X FAUL	GGX		R			
L										
Z	98.41	101.50	5.09	X FAUL	GGX		R			
L										
R	98.41	101.50		MAY BE COMPRISED OF UNIT ABOVE OR BELOW FAULT OR BOTH.						
Z	101.50	104.80	3.30	BRHT	BR B*	MN1	P			D(
L				4A	F* 4	KN6				
R	101.50	104.80		PY DISS MAINLY IN CLASTS.						
Z	102.25	104.80	2.55	X ARGL	BY SS A A A		R			B=
L				2A						
R	102.25	104.80		FAINT SLUMP FEATURES EVIDENT. PROBABLY COMPRISES ONE CLAST.						
Z	104.80	110.64	5.84	BRHT	GGP BR B*	NP3	P			D=
L				3A	CU 3	LN2				

[illegible][illegible]

K	F	F	R	D	M	T	D	I	N	T	RECDV	MD	%	ROCK	TM	TM	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G										R	D	D	AGE	EV	RD	LC	TM	QM2	TX	TX	S	C	D	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				

R 197.10 290.35 20 SLATY CLEAVAGE OR 3) DEWATERING TRACES.

/ SHR 207.30 220.98 15.68 X SHER GG1 R
L

/ SHR 225.35 225.70 0.35 X SHER R
L

/ SHR 227.17 227.40 0.23 X SHER R
L

/ SHR 231.92 239.20 7.28 X SHER GG2 R
L

/ SHR 245.60 246.50 0.70 X SHER R
L

/ SHR 246.67 249.70 0.83 X SHER R
L

/ SHR 252.93 253.74 0.81 X SHER R
L

/ SHR 254.81 255.40 0.59 X SHER R
L

/ SHR 264.75 265.44 0.69 X SHER R
L

/ SHR 271.04 271.73 0.69 X SHER R
L

/ SHR 272.70 273.10 0.40 X SHER R
L

/ VET 280.80 290.53 1.58 1 VET DZ6 RR A K 3 M R VN 90 D*
L

R 283.60 290.38 CONTAINS ARGL FRAGMENTS BROKEN OFF BALL ROCK.

/ SHR 290.38 291.74 1.36 BRHT SD1 RR FD LQ2 P D*
L 4A 2 IN7 <*

/ 290.38 291.08 0.70 X CGSH SD2 RR FD I N 6 P R
L 5A 2 <* D*

R 290.38 291.74 POSSIBLY A TURBIDITE THAT WAS SORE SEDIMENT SLUMPED.

/ 291.74 337.72 45.98 BRHM SS FL KR9 P CL 60 D.
L 2A <*

R 291.74 337.72 SAME AS 197.10 TO 290.38M.

/ SHR 297.16 304.95 7.77 X SHER GG2 R
L

[illegible]

K L S2	587.00	587.00	0.00
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Z	L	587.00	600.00	13.00	BRHM 4A	*S+ BR SS 4 +	NQ9 P	<*	B*
Z	L	587.00	589.86	2.86	X BRHM 4A	SIF BR 4	MP9 R	I=	
R		587.00	600.00					<*	
K US3		600.00	600.00	0.00					
Z	L	600.00	612.00	12.00	FGSX PY PR SIF BR RD A M 4 D SD SD 6	P	M4 D. D)		
R		600.00	612.00				D1	D1	
R		600.00	612.00						
R		600.00	612.00						
R		600.00	612.00						
Z	L	609.13	612.00	2.87	X FGSX SD PY SIF BR 6A PR 6	A M 5 D R	I3	D1 D+	
R		609.13	612.00					D=	
K LS3		612.00	612.00	0.00					
Z	L	612.00	630.97	18.97	BRHM 3A	*S= SS CL 3	NT9 P CL 45 <-	D(B.	
R		612.00	630.97				D-		
Z VEN	L	614.49	615.59	1.10	9 VEIN SZ 3	A I 1 D R		B- B.	
R		614.49	615.59						
Z	L	621.04	621.29	0.25	X BRHM 4A	SD= SS R	<1	D* B*	
R		621.04	621.29						
Z FRG	L	630.97	634.49	3.52	CGR 6A	RR SS F*	LO1 P LN6	M+ M2	
R		630.97	634.49						
R		630.97	634.49						
Z	L	634.49	638.80	4.31	BRHM 3A	*S= SS R	NP9 P	B- D. <-	
R		637.03	637.64						
R		637.03	637.64						
Z	L	637.03	638.80	1.77	7 BRHM CR 3A	*S= GR)	NQ9 R CL 35 <+	D- <*	
Z DYK	L	638.00	642.48	5.68	DYFL FX W	HX G I 1 K P	<- D*	MS D. D(D1	
R		638.00	642.48						

G F O L O G

K	F	F	R	H	T	RECDV	MD	%	ROCK	TR	TM	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Y	G						R	D	D	AGE	EV	RD	LC	TX	QM2	TX	TX	S	C	O	O	CHI	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA		

R	642.48	643.50	GRAPHITE DEVELOPMENT ON SLICKENSIDES.																																
/	642.48	647.40	4.92	ANGL		LM		A D 1 0		P		O LM		33																					
L				3A																															
/	642.48	643.50	1.02	X BRHM CR		BR CL		MOB		R		CL		45																					
L				4A																															
R	642.48	643.50	GRAPHITE DEVELOPMENT ON SLICKENSIDES.																																

A MIN		0.02	-0.01	0.02	0.02	-0.01	3.73	-0.1	-0.1	3.570
A MAX	548.00 612.65	24.84	5.80	0.96	10.47	0.11	31.75	0.004	-0.1	73.854

11/10/80 BY HBF

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PH-2N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6H02

DRILLHOLE/TRAVERSE : BOADH057
TOTAL DEPTH/LENGTH : 182.27
CORE/HOLE DIAMETER : 00COLLAR ELEVATION: 1159.40
NORTHING (= IF S): 7001814.00
EASTING (= IF W): 436572.31AZIMUTH(DEG) : 60.00
VERTICAL ANGLE : -50.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-RECC

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	53.34	61.00	-49.00
2	90.83	63.00	-49.50
3	137.16	62.00	-48.00
4	181.36	63.00	-45.00

F - INTERVAL - CORE T-2 TYPI- CAL TEX- GRAIN PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY

X L (UNITS = . DEC.PLACE) RECOV- H M ROCK FLYING MIN TURES CHARACS

E A (M=METRIC FT=FOOTRIC) FRY G I TM TM MAT TX TX F C % M ARG /RI T ID STK DIP A A A A A MIN A A A MIN - - - -

Y G F C D G - T - I M T (.) D X TYPE 1 2 001 1 2 F F C A 1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2

K F ROCK FA RT IM 002 TX TX S C D U CHT T ID STK DIP MG MU CL SD QS HA PR MT SL HA

E L QUAL AGE FU- U LC- 3 3 4 0 / 2 AZM RT H H H H H H H H H H 1 1

Y G DESIG VIR COL R C STRUCTUR-2 A A A A A A A A A A 2 2

R SVY 0.00 0.00 SPERRY SUR TESTS

R ASY 0.00 0.00 NO ASSAY DATA FOR THIS HOLE.

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6B02

GEOLOGGED BY : +
DATE (YY/MM/DD): 810000
PROJECT NUMBER : JSOUTH

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	3.05	183.00	-71.77
2	30.48	183.22	-70.88
3	60.96	181.45	-70.64
4	91.44	179.11	-68.60
5	121.92	175.12	-62.59
6	152.40	173.57	-61.94
7	182.88	175.38	-60.62
8	213.36	174.52	-58.49
9	220.98	174.55	-57.63
10	228.60	174.14	-56.58
11	236.22	174.03	-55.70
12	243.84	172.15	-55.59
13	248.41	171.47	-55.40
14	305.10	163.00	-53.00
15	335.60	160.00	-47.50

F - I N T E R V A L - CORP 1- % TYPE- DUAL TEX- GRAIN PGI															STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY																
K	L	(UNITS = . DEC.PLACE)	RECOV-	M M	ROCK	FYING	MJN	TURES	CHARACS	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-		
F	A	(METRIC FT=FOOTRIC)	ERY	0	T	IN	TM	RAT	TX TX	F C %	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F R O N - T O - I N T (.)	D X	TYPE	1	2	QM1	1	2	F F C	A			1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
K	F		ROCK	FR	RT	TM	QM2	TX	TX	S C O O	CHT			T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
F	L		DUAL	AGE	EN- 0	LC- 3		3	4	O	/			2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G		DESIG		VIR	COL				R	C				STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY	0.00	0.00	DATA FROM COLLAR TO WEDGE OFF POINT (248.41 M) FROM GYROSCOPIC
R SVY	0.00	0.00	SURVEY OF DDH 80-638. REMAINDER FROM SPERRY SUN TESTS.
R SVY	248.41	248.41	BEGINNING OF WEDGED HOLE A.
R SVY	248.41	248.41	HALL AND ROWE STEEL WEDGE. FULL AZIMUTH LEFT.
R SVY	274.00	274.00	HALL AND ROWE STEEL WEDGE. FULL AZIMUTH LEFT.
R SVY	306.30	306.30	HALL AND ROWE STEEL WEDGE. FULL AZIMUTH LEFT.
R SVY	397.78	397.78	HOLE ABANDONED WHEN RODS BROKE AT SECOND WEDGE (274 M).
R SVY	397.78	397.78	UNABLE TO RECOVER DRILL EQUIPMENT BELOW BREAK.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASOP PB-2N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRaverse : 8080H056

COLLAR ELEVATION: 1230.00

AZIMUTH(DEG) : 228.00

GEOLOGGED BY : +

TOTAL DEPTH/LENGTH : 679.71

NORTHING(= IF S): 7002464.00

VERTICAL ANGLE : -70.00

DATE (YY/MM/DD): 0

CORE/HOLE DIAMETER : 00

EASTING (= IF N): 436749.62

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.44	224.00	-68.00
2	91.44	218.50	-66.00
3	152.40	213.00	-64.00
4	213.36	209.50	-64.00
5	274.32	206.00	-61.00
6	362.10	204.00	-57.00
7	365.76	203.00	-56.00
8	373.38	201.00	-56.00
9	381.00	199.50	-55.00
10	387.10	199.40	-54.00
11	411.48	199.00	-54.00
12	443.48	196.00	-53.00
13	472.44	193.00	-53.00
14	504.44	193.50	-51.00
15	533.40	194.00	-50.00
16	563.88	190.90	-50.00
17	571.50	190.20	-50.00
18	601.94	187.00	-49.00
19	632.46	187.80	-45.00
20	640.08	188.00	-46.50
21	679.70	189.00	-45.00

F - I N T E R V A L - CORE T- % TYPI- QUAL TEX- GRAIN PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY																													
K	L	(UNITS = DEC.PLACE)	RECV-	M 4	ROCK	FYING	MIN	TURES	CHARACS							H	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE		
E	A	(MT=METRIC FT=FOOT)	ERY	U I		TM TM	MAT	TX TX	F C % M	ARG	/RI	T ID	STK	DIP		A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F R D 4 - T O - I N T (.)		D X	TYPE	1 2	QM1	1 2	F F C A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
- - - - -																													
K	F		ROCK	FM	RT	FM	QM2	TX TX	S C O O	CHT		T ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					
E	L		QUAL	AGE	FN- U	LC- 3		3	4	U	/	2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G		DESIG		VIR	COL				R	C		STRUCTUR-2			A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 SPERRY SUN TESTS: ERRATIC AZIMUTHS, POSSIBLY DUE TO PYRROTITE,
R SVY 0.00 0.00 ARE DELETED IN THE LISTING.
R SVY 387.10 387.10 BEGINNING OF WEDGED HOLE H.
R SVY 387.10 387.10 HALL AND ROWE STEEL WEDGE - FULL STEEPENING.
R SVY 679.71 679.71 END OF WEDGED HOLE H.

/ 0.00 391.61 391.61 MISS P
/ 391.61 394.70 3.09 BRHM NO9 P <(R)
L 3A 2 JL+
R 391.61 394.70 THE LAST 50MS OF THIS INTERVAL CONTAINS QUARTZ VEINS WITHIN

K	F	F	R	O	M	-	T	O	-	I	E	T	RECOV	MD	%	ROCK	TM	TM	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G												R	D	AGE	EV	RD	LC	TM	QM2	TX	TX	S	C	O	U	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA									

R 391.61 394.70 BRECCIATED FRAGMENTS.

/ FRG 394.70 399.20 4.50 ARST SN2 RD // 0 3 2 3 P 2 BD 43 L*

L 3A H

R 399.20 401.53 THE PEBBLY MUDSTONE CONTAINS ONE 1.25 METRE SILT BANDED

R 399.20 401.53 ARGILLITE FRAGMENT. THE TOP 3CMS IS A MUDSTONE MATRIX, WHICH

R 399.20 401.53 GRADES QUICKLY INTO A SANDSTONE MATRIX, FOR THE REMAINDER OF THE

R 399.20 401.53 BED.

/ 399.20 405.95 6.75 BRHT *C. NU9 P L*

L 3A F* 3 JN1

/ 399.20 401.53 2.33 9 BRPM *C(F* KT1 R R(

L 3A SN7 4 JM2

R 399.20 405.95 LAMINATED PYRITE OCCURS WITHIN THE SANDSTONE LAYER OF SILT

R 399.20 405.95 BANDED ARGILLITES.

/ 405.95 440.07 34.12 BRPM SS LS9 P V(L* L*

L 3A 3

R 405.95 440.07 THE SILT BANDED ARGILLITE FRAGMENTS CONTAIN LAMINATED CARBONITES

R 405.95 440.07 WITHIN THEIR SAND BEDS. THIS INTERVAL IS BROKEN AND SHEARED

R 405.95 440.07 INDICATING SOME FAULTING HAS OCCURRED.

/ 418.26 418.50 0.24 9 SAND MX 0 3 9 3 R V= D*

L 8T 9 <*

R 418.26 418.50 THIS SANDSTONE BED IS POSSIBLY A FRAGMENT.

/ FLT 432.04 432.29 0.25 * BRPM GG8 SS LS9 R V(L*

L

/ 433.35 433.58 0.23 9 BRHT CC KM6 R <=

L 4A 2 JK1

R 433.35 433.58 A 2CM, OVAL PYRITE CONCRETION IS PRESENT WITHIN THIS INTERVAL.

/ 440.07 441.94 1.87 BRPM *C(JP9 P <* L*

L 3A H* 2 JM=

K UDF 441.94 441.94 0.00

/ 441.94 442.36 0.42 BRHT LN3 P D*

L 3A 3 K02 R+

R 441.94 442.36 A TRANSITION OCCURS WITHIN THIS INTERVAL, WHICH GOES FROM MUD TO

R 441.94 442.36 SAND.

/ 442.36 449.88 7.52 CGCP *C+ F* KN2 P V1 C+

L 6A B* G? 5 C K05 <(

/ 442.36 443.72 1.36 9 BRPM KP4 R

L 3A K02

R 442.36 449.88 A NORMAL GRADING OF FRAGMENTS OCCURS INDICATING TOPS ARE UP HOLE

/ 443.72 444.68 0.96 7 BRPM *C(F* KM= R R*

L 3A SN7 H* 4 0 K02

[illegible]

G E O L O G

K	F	F	R	D	A	-	T	D	-	I	N	T	RECDV	RD	Z	BLCK	IN	TR	QRI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Y	G												R	Q	D	AGE	EV	RD	LC	IN	QNP	TX	TX	S	C	O	D	CHI	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

[illegible]

K	F	F	R	O	M	-	T	RECDV	NO	%	ROCK	TM	TM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																						2	ID	AZM	DIP	MG	MU	CL	SO	QS	HA	PR	MT	SL	HA				

R 565.71 566.25 IRREGULAR MIXING. SAMPLE D.G. 179 TAKEN AT 566.25 METRES.
R 565.71 566.25 SAMPLE D.G. 180 TAKEN AT 566.60 METRES.

/ 566.25 568.76 2.51 MSSX MX P 01 M2 M4
L 5A VG Q3 M= M1

R 566.25 568.76 THE RECOVERY OVER THIS INTERVAL IS POOR IN THE MORE SIDERITIC
R 566.25 568.76 VUGGY SECTION AT THE BASE OF THE INTERVAL. NEAR THE TOP OF THE
R 566.25 568.76 INTERVAL, THE ORE IS A MASSIVE GALENA RICH SULPHIDE, WITH
R 566.25 568.76 IRREGULAR PATCHES OF SIDERITE, QUARTZ AND SPHALERITE.

/ 568.76 570.59 1.83 MSSX SO MX P B2 Q)
L 50 VG M6 B)

R 568.76 570.59 THE RECOVERY OVER THIS INTERVAL WAS VERY POOR.

/ 570.59 571.50 0.91 MSSX SO MX P Q= M2 Q=
L 5A VG Q3 B)

R SPC 570.59 571.50 SAMPLE D.G. 181 TAKEN AT 570.20 METRES. THE UPPER HALF OF THE

R 570.59 571.50 MASSIVE SULPHIDE IS RICH IN SIDERITE AND QUARTZ SIDERITE. THE
R 570.59 571.50 LOWER PART IS RICH IN GALENA AND PYRITE.

/ 571.50 574.55 3.05 MSSX SO MX P Q+ M1 M3
L Q2 M2

R 571.50 574.55 ALTERATION OCCURS AROUND MASSIVE REGIONS OF PYRITE, GALENA AND
R 571.50 574.55 SPHALERITION. GALENA AND SPHALERITE FORM AROUND SMALL 3MM
R 571.50 574.55 PATCHES OF QUARTZ, AND IN DENDRITIC TEXTURES IN AND AROUND
R 571.50 574.55 MASSIVE PYRITE.

R SPC 571.50 574.55 SAMPLE D.G. 182 TAKEN AT 571.28 METRES.

R 571.50 574.55 SAMPLE D.G. 183 TAKEN AT 574.50 METRES.

/ 574.55 576.07 1.52 MSSX SO VG P B(M4 M5
L Q1 D1

/ 576.07 576.62 0.55 MSSX SO MX P B(<= Q6
L M3 D=

/ 576.62 577.48 0.86 MSSX SO MX P Q= M2 Q=
L Q2 B1

/ 577.48 578.17 0.69 MSSX SO MX P Q= M2 Q=
L Q2 B)

R SPC 577.48 578.17 SAMPLE D.G. 184 TAKEN AT 577.9 METRES.

/ 578.17 580.95 2.78 MSSX MX VG P LM 25 L= M7
L 3A BM LM B1 X2

R 578.17 580.95 IN PARTS, THE CORE SHOWS FAINT BANDING, AND LAMINATION OF
R 578.17 580.95 SULPHIDES.

/ 580.95 581.86 0.91 MSSX MX VG P LM 25 L= M7
L

R 580.95 581.86 THE UPPER PART IS MASSIVE, WHEREAS THE LOWER PART IS BANDED WITH
R 580.95 581.86 SULPHIDES AND ALTERATION CLAYS (POSSIBLY SERICITE). THE BANDS

G E O L O G

K	F	F	R	O	K	-	I	N	T	RECOV	MD	%	ROCK	TM	TA	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	DZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2			
E	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																																												

R 580.95 581.86 ARE CONVOLUTED, AND FROM 2CM TO 2CM IN WIDTH. TENSION FRACTURES
 R 580.95 581.86 OCCUR IN THE PYRITE PADDS.
 R SPC 580.95 581.86 SAMPLE D.G. 185 TAKEN AT 581.80 METRES.

/ 581.86 582.63 0.77 SULF MX P M6 M2 B2

L 581.86 582.63 9G BR <+ R=
 R 581.86 582.63 THIS HIGHLY ALTERED INTERVAL MAY BE A BLEACH ARGILLITE, RICH IN
 R 581.86 582.63 QUARTZ-SERICITE. SMALL MICROFINS OF CHLORITE CROSSCUT THE
 R 581.86 582.63 MASSIVE ROCK.

/ 582.63 583.43 0.80 MSSX MX P B) B1 M8

L 582.63 583.43 4A VG B1 B=

/ 583.43 584.51 1.08 MSSX SD MX P B= B1 M6

L 583.43 584.51 61 Q2 B* B=

R SPC 583.43 584.51 SAMPLE D.G. 186 WAS TAKEN AT 584.00 METRES.

/ 584.51 586.37 1.86 MSSX MX P <+ M2 B* M4 07

L 584.51 586.37 4A VG B+ B) B+ B=

R 584.51 586.37 THIS INTERVAL IS DOMINATED BY MASSIVE PYRITE AND GALENA.
 R 584.51 586.37 SPHALERITE OCCURS AS SMALL BLES IN MASSIVE GALENA OR AS BANDS
 R 584.51 586.37 ASSOCIATED WITH QUARTZ-SERICITE LENSES.
 R SPC 584.51 586.37 SAMPLE D.G. 187 WAS TAKEN AT 585.60 METRES.

K LSI 586.37 586.37 0.00

/ 586.37 587.04 0.67 BRHT SF *C) R* H* NS4 P <) <= R1 D=

L 586.37 587.04 4A MD SS 3 * KM1 <) <=

R 586.37 587.04 THE MATRIX IS A FAIRLY SANDY PERKY MUDSTONE.

/ 587.04 588.19 1.15 BRHT SF *C) R* H* NS4 P <) <= R= D)

L 587.04 588.19 <) <= R) D)

/ 588.19 591.20 3.01 BRHT SF *C) R* H* NS4 P <) <= R1 D=

L 588.19 591.20

R 588.19 591.20 PYRRHOTITE, PYRITE, SIDERITE, GALENA AND SPHALERITE
 R 588.19 591.20 MINERALIZATION OCCURS IN AN ARGILLITE BOULDER THAT MEASURES 1.21
 R 588.19 591.20 METRES ACROSS.

/ 591.20 592.32 1.12 BRHT SF *C) R* H* NS4 P <) <+ C= B)

L 591.20 592.32 D(D(

R 591.20 592.32 SULPHIDES SURROUND BRECCIA FRAGMENTS AND ALSO OCCUR WITHIN THE
 R 591.20 592.32 FRAGMENTS AND MATRIX AS DISSEMINATED CRYSTALS.

/ 592.32 593.66 1.34 MSSX PY MX P B1 M4 B=

L 592.32 593.66 4H BR M2 M1 L1

R 592.32 593.66 ARGILLIC FRAGMENTS AND BANDS OCCUR THROUGHOUT THE MASSIVE
 R 592.32 593.66 SULPHIDE. THE TOP IS RICH IN SIDERITE, WHEREAS THE BOTTOM IS
 PREDOMINANTLY MASSIVE SULPHIDES.

/ 593.66 594.89 1.23 CGS-I SF LM2 P V+ R= B)

L 593.66 594.89 5A C KM4 E=

[illegible]

[illegible]

K	F	F	R	D	-	T	D	-	T	D	RECDV	NO	%	ROCK	TM	TM	TM	TM	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G																																													

R 641.15 648.00 SIDERITE, IN THE UPPER HALF OF THIS INTERVAL. PYRITE AND
 R 641.15 648.00 PYRRHOTITE OCCUR AS LAMINATED DISSEMINATIONS IN THE SANDY
 R 641.15 648.00 LAMINATIONS WITHIN THE ARGILLITE. MOST OF THE FE-SULPHIDES ARE
 R 641.15 648.00 FOUND WITH SIDERITIZED REGIONS, IN VEINS AND AS THE MATRIX FOR
 R 641.15 648.00 BRECCIATED ARGILLITE FRAGMENTS.

R SPC 641.15 648.00 SAMPLE D.G. 214 TAKEN AT

K US3 643.00 643.00 0.00

/ 643.00 650.00 2.00 ARGL SF SP= BN SS 1 3 = 1 P 1 LM 26 <+ X= B.
 L RE B+

R 643.00 650.00 THIS BRECCIATED SILICIFIED ARGILLITE MAKES UP 70% OF THE TOTAL
 R 643.00 650.00 INTERVAL VOLUME.

/ 650.00 654.00 4.00 BSSX PR BN P LM 20 L2 X3 B.
 L SU LB <1 X1 B.

R 650.00 654.00 THE ARGILLITE, NEAR THE TOP, IS BRECCIATED AND FE-SULPHIDES MAKE
 R 650.00 654.00 UP THE MATRIX. FURTHER DOWN THE SULPHIDES BECOME BANDED IN 1CM
 R 650.00 654.00 LAYERS WITH .5CM LAYERS OF QUARTZ.

/ 650.00 659.47 5.47 ARGL SF SN* LC 0 3 * 3 P 0 BD 25 V1 L=
 L SA SIC LB 8 <+

R SPC 654.00 659.47 SAMPLE D.G. 215 TAKEN AT

K LS3 656.00 656.00 0.00

/ 659.47 660.91 1.44 ARGL CR SN* LM P 0 BD 25 <) L=
 L 4A SIC CC 8 <)

R 659.47 660.91 PYRITE BEDS ARE 1.5 - 2.0 CMS IN THICKNESS. LARGE NODULES OF
 R 659.47 660.91 PYRITE ARE 20CMS IN DIAMETER.

/ 660.91 665.59 4.68 BSSX SS MRB P B=
 L 4A 3 <*

/ MSX 665.59 672.08 6.49 BSSX PY P M4
 L 30 <)

R 665.59 672.08 APPROXIMATELY 80% OF THE MATRIX HAS BEEN REPLACED BY PYRITE.
 R 665.59 672.08 BOTH ARGILLITE AND CHERT FRAGMENTS OCCUR IN THE PYRITIZED MATRIX
 R SPC 665.59 672.08 SAMPLE D.G. 216 TAKEN AT

/ 672.08 672.93 0.85 BRPS LN1 P C1
 L 3A 2 L02

/ 672.93 674.23 1.30 SAND LC LB 0 3 8 3 P L1
 L 4A 8

R 672.93 674.23 A FEW ARGILLITE LAYERS INTERCALATE WITHIN THE SANDSTONE.

/ 674.23 679.71 5.48 ARSI CR SRI BD SK 0 3 1 5 P BD 47 B+
 L 2A 8 V2

A ILM	SAMPLE		% PB	% ZN	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH		
A LAB	SERIAL		B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG			
A TYP	NUMBER		H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE			
A MTH			WA	WA	WA	WA	WA	WA	WA	WA			
R ASY	0.00	0.00	B.CLG = BUNDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.										
R ASY	0.00	0.00	WA = WET ANALYSIS.										
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01										
R ASY	0.00	0.00	ALL ASSAY INFORMATION ENTERED AS -0.1										
A 001	560.47	562.05	123	PH8483	0.27	0.20	0.83	0.12	0.01	8.35	-0.002	-0.1	9.678
A 001	562.05	562.97	62	PH8484	1.41	1.22	1.40	0.84	0.02	8.40	-0.002	-0.1	13.188
A 001	562.97	564.15	96	PH8485	24.99	11.15	0.14	10.65	0.06	7.60	-0.002	-0.1	54.488
A 001	564.15	565.71	127	PH8486	25.52	4.95	0.04	9.15	0.07	25.45	-0.002	-0.1	65.078
A 001	565.71	566.25	31	PH8487	6.00	0.81	-0.01	2.61	0.03	34.50	-0.002	-0.1	43.838
A 001	566.25	568.76	146	PH8488	21.17	6.80	0.04	8.94	0.03	24.80	-0.002	-0.1	61.678
A 001	568.76	570.59	04	PH8489	0.60	0.32	-0.01	0.62	0.01	39.55	-0.002	-0.1	41.028
A 001	570.59	571.50	88	PH8490	3.05	0.34	-0.01	1.82	-0.01	27.70	-0.002	-0.1	32.788
A 001	571.50	574.55	126	PH8491	17.60	7.79	-0.01	8.75	0.01	17.40	-0.002	-0.1	51.438
A 001	574.55	576.07	14	PH8492	26.22	4.75	0.02	11.63	0.02	27.30	-0.002	-0.1	69.838
A 001	576.07	576.62	46	PH8493	30.18	2.60	0.01	14.45	0.03	15.75	-0.002	-0.1	62.918
A 001	576.62	577.48	72	PH8494	35.48	0.24	-0.01	16.53	-0.01	10.50	-0.002	-0.1	62.628
A 001	577.48	578.17	45	PH8495	23.32	0.64	0.01	10.96	-0.01	12.20	0.037	-0.1	47.057
A 001	578.17	580.95	98	PH8496	48.26	16.51	0.06	27.20	0.02	7.70	-0.002	-0.1	99.648
A 001	580.95	581.36	57	PH8497	42.24	17.51	0.10	21.45	0.03	9.75	-0.002	-0.1	90.978
A 001	581.36	582.63	26	PH8498	8.70	2.95	0.10	4.11	0.01	17.60	-0.002	-0.1	33.368
A 001	582.63	583.43	63	PH8499	62.13	2.30	0.02	24.77	0.01	9.50	-0.002	-0.1	98.628
A 001	583.43	584.51	65	PH8500	43.71	0.28	-0.01	16.59	0.04	10.65	-0.002	-0.1	71.158
A 001	584.51	586.37	93	PH8501	23.62	0.81	0.03	9.20	0.11	14.60	-0.002	-0.1	48.268
A 001	586.37	587.04	44	PH8502	2.55	0.11	3.72	0.97	0.01	5.65	-0.002	-0.1	12.908
A 001	587.04	588.19	100	PH8503	0.23	0.01	5.32	0.54	-0.01	2.35	-0.002	-0.1	8.338
A CMP	582.97	586.37	1197		25.78	5.98	-0.03	12.00	-0.03	18.71	-0.002	-0.1	62.308
A 001	591.20	592.32	105	PH8587	0.88	-0.01	1.41	0.37	-0.01	3.55	-0.002	-0.1	6.088
A 001	592.32	593.66	129	PH8588	2.23	-0.66	0.04	1.49	0.04	36.43	-0.002	-0.1	39.468
A 001	593.66	594.80	109	PH8589	0.51	0.03	0.38	0.18	-0.01	4.20	-0.002	-0.1	5.188
A 001	594.80	595.79	94	PH8590	2.89	-0.01	0.36	0.73	-0.01	2.50	-0.002	-0.1	6.358
A 001	595.79	596.85	101	PH8591	9.02	-0.01	0.16	1.87	-0.01	2.70	-0.002	-0.1	13.628
A CMP	592.32	596.85	441		3.53	-0.21	0.22	1.08	-0.01	13.01	-0.002	-0.1	17.518
A 001	609.36	610.00	63	KL8504	8.20	0.03	0.16	2.04	0.18	31.95	-0.002	-0.1	42.458
A 001	610.00	611.00	99	KL8505	2.50	0.03	0.64	0.54	0.09	23.45	-0.002	-0.1	27.148
A 001	611.00	612.00	99	KL8506	0.52	0.02	0.39	0.52	0.07	26.40	-0.002	-0.1	27.818
A 001	612.00	613.00	99	KL8507	10.98	0.05	0.12	1.73	0.06	28.45	-0.002	-0.1	41.288
A 001	613.00	614.00	99	KL8508	1.73	0.02	0.15	0.33	0.10	29.30	0.008	-0.1	31.538
A 001	614.00	615.00	99	KL8509	6.23	0.04	0.05	1.16	0.08	29.35	0.002	-0.1	36.812
A 001	615.00	616.00	100	KL8510	3.60	0.06	0.23	0.64	0.07	26.75	-0.002	-0.1	31.248
A 001	616.00	617.00	100	KL8511	3.85	0.04	0.21	0.72	0.04	28.40	0.002	-0.1	33.162
A 001	617.00	618.00	99	KL8512	5.43	0.01	0.07	1.00	0.09	34.65	-0.002	-0.1	41.048
A 001	618.00	619.00	98	KL8513	3.65	0.02	0.02	0.77	0.18	33.65	-0.002	-0.1	38.188
A 001	619.00	620.00	98	KL8514	0.14	0.01	0.17	0.24	0.14	27.14	-0.002	-0.1	27.738
A 001	620.00	621.00	99	KL8515	8.61	0.06	0.08	1.61	0.06	34.15	-0.002	-0.1	44.468
A 001	621.00	622.00	100	KL8516	1.21	0.02	0.08	0.22	0.07	33.05	-0.002	-0.1	34.548
A 001	622.00	623.00	100	KL8517	5.32	0.02	0.04	0.92	0.06	34.10	-0.002	-0.1	40.358

A UTM	SAMPLE			% Pb	% Zn	% Ba	OZ AG	% Cu	% Fe	OZ AU	% Cd	HASH	
A LAB	SERIAL			B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		
A TYP	NUMBER			H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH				WA	WA	WA	WA	WA	WA	WA	WA		
A 001	623.00	624.00	100	KL8518	4.02	-0.02	0.29	0.73	0.08	31.20	-0.002	-0.1	36.198
A 001	624.00	625.00	99	KL8519	5.15	0.22	0.16	0.84	0.05	28.65	-0.002	-0.1	34.968
A 001	625.00	626.00	99	KL8520	5.60	0.06	0.06	0.75	0.05	32.15	-0.002	-0.1	38.568
A 001	626.00	627.00	99	KL8521	6.75	0.02	0.04	0.95	0.03	31.65	-0.002	-0.1	39.338
A 001	627.00	628.00	99	KL8522	4.38	0.02	0.08	0.69	0.05	27.40	-0.002	-0.1	32.518
A 001	628.00	629.00	99	KL8523	0.96	0.25	0.02	0.27	0.07	36.90	-0.002	-0.1	38.368
A 001	629.00	630.00	99	KL8524	0.15	0.08	0.09	0.16	0.09	20.63	-0.002	-0.1	21.098
A 001	630.00	631.00	99	KL8525	0.12	0.21	0.23	0.14	0.03	7.20	-0.002	-0.1	7.828
A 001	631.00	632.00	99	KL8526	0.04	0.49	0.22	0.07	0.03	9.50	-0.002	-0.1	10.248
A 001	632.00	633.00	99	KL8527	0.12	0.46	0.06	0.15	0.03	26.00	-0.002	-0.1	26.718
A 001	633.00	634.00	99	KL8528	0.13	0.47	0.11	0.22	0.02	25.43	-0.002	-0.1	26.278
A 001	634.00	635.00	97	KL8529	0.04	0.31	0.23	0.12	0.04	21.00	-0.002	-0.1	21.638
A 001	635.00	636.00	97	KL8530	0.03	0.14	0.31	0.15	0.01	8.50	-0.002	-0.1	9.038
A CMP	609.36	630.00	2044		4.16	0.05	0.15	0.78	0.08	29.93	-0.002	-0.1	35.048
A 001	641.15	641.95	79	PH8556	0.01	-0.01	0.28	0.05	0.01	9.10	-0.002	-0.1	9.338
A 001	641.95	643.00	104	PH8551	0.02	-0.01	0.24	0.07	0.03	13.10	-0.002	-0.1	13.348
A 001	643.00	644.04	103	PH8552	0.04	-0.01	0.13	0.18	0.04	21.80	-0.002	-0.1	22.078
A 001	644.04	644.96	87	PH8553	0.01	0.01	0.13	0.08	0.08	27.03	-0.002	-0.1	27.238
A 001	644.96	646.00	94	PH8554	0.01	0.02	0.10	0.27	0.08	28.85	-0.002	-0.1	29.228
A 001	646.00	647.00	91	PH8555	0.02	-0.01	0.20	0.09	0.03	15.00	-0.002	-0.1	15.228
A 001	647.00	648.00	93	PH8556	-0.01	-0.01	0.19	0.04	0.01	11.90	-0.002	-0.1	12.018
A 001	648.00	649.00	99	PH8557	0.01	0.01	0.24	0.07	0.01	9.08	-0.002	-0.1	9.318
A 001	649.00	650.00	99	PH8558	-0.01	0.04	0.25	0.06	0.01	7.55	-0.002	-0.1	7.798
A 001	650.00	651.00	99	PH8559	0.02	0.02	0.08	0.17	0.06	29.30	-0.002	-0.1	29.548
A 001	651.00	652.00	100	PH8560	0.02	0.01	0.10	0.15	0.05	25.90	-0.002	-0.1	26.128
A 001	652.00	653.00	100	PH8561	0.01	-0.01	0.12	0.13	0.02	17.80	-0.002	-0.1	17.968
A 001	653.00	654.00	99	PH8562	0.01	-0.01	0.13	0.14	0.03	20.38	-0.002	-0.1	20.578
A 001	654.00	655.00	98	PH8563	0.02	0.01	0.17	0.16	0.02	14.00	-0.002	-0.1	14.278
A 001	655.00	656.00	98	PH8564	0.02	0.08	0.19	0.21	0.06	7.40	-0.002	-0.1	7.858
A CMP	643.00	656.00	1260		0.02	-0.02	0.16	0.14	0.04	18.14	-0.002	-0.1	18.378
A 001	665.99	667.00	101	PH8616	0.01	-0.01	0.27	0.10	0.05	15.30	-0.002	-0.1	15.618
A 001	667.00	668.00	100	PH8617	0.03	-0.01	0.13	0.11	0.06	24.65	-0.002	-0.1	24.868
A 001	668.00	669.00	100	PH8618	0.03	-0.01	0.14	0.23	0.07	27.60	-0.002	-0.1	27.958
A 001	669.00	670.00	100	PH8619	0.03	-0.01	0.20	0.18	0.04	25.20	-0.002	-0.1	25.542
A 001	670.00	671.00	100	PH8620	0.04	-0.01	0.10	0.12	0.04	29.20	-0.002	-0.1	29.388
A 001	671.00	672.00	108	PH8621	0.02	-0.01	0.10	0.18	0.05	23.45	-0.002	-0.1	23.688

A MIN			-0.01	-0.01	-0.01	0.04	-0.01	2.35	-0.002	-0.1	2.248
A MAX	560.47	672.04	62.13	17.51	5.32	27.20	0.18	39.55	0.037	-0.1	151.82
R ASY	0.00	0.00	MAX HASH TOTAL IS ACTUALLY 151.827; THE 7 HAS BEEN LEFT OFF .								

R ASY 0.00 0.00 NOTE THAT MIN AND MAX WERE CALCULATED FOR EACH WEDGED HOLE.
R ASY 0.00 0.00 SINCE IT MIGHT BE RECOGNIZED AS ONE ASSAY FILE BY THE COMPUTER
R ASY 0.00 0.00 SOME EDITING PROBLEMS MIGHT OCCUR.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASO PA-7N-AG-BA-STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 30340063

COLLAR ELEVATION: 1295.40

AZIMUTH(DEG) : 183.00

GEOLOGGED BY : JER + JDK

TOTAL DEPTH/LENGTH : 561.90

NORTHING(= 1F S): 7002611.00

VERTICAL ANGLE : -72.67

DATE (YY/MM/DD): 810000

CORE/HOLE DIAMETER : NO

EASTING (= 1F S): 436463.25

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S2

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	3.95	183.27	-71.77
2	30.48	183.22	-70.88
3	60.96	181.45	-70.64
4	91.44	179.11	-68.96
5	121.92	175.12	-62.59
6	152.40	173.57	-61.94
7	182.88	173.38	-60.62
8	213.36	174.52	-58.49
9	220.98	174.55	-57.63
10	228.60	174.14	-56.58
11	236.22	174.03	-55.70
12	243.84	172.15	-55.59
13	251.46	171.27	-53.88
14	259.08	170.33	-53.50
15	266.70	170.26	-51.79
16	274.32	170.35	-50.94
17	281.94	170.35	-49.94
18	289.56	170.53	-48.94
19	297.18	171.23	-47.96
20	304.80	171.34	-47.55
21	312.42	171.09	-46.84
22	320.04	171.21	-46.65
23	327.66	171.48	-46.45
24	335.28	171.51	-45.81
25	342.90	171.22	-44.82
26	350.52	171.39	-43.59
27	358.14	171.42	-41.74
28	365.76	172.04	-40.69
29	373.38	172.04	-39.80
30	381.00	172.28	-38.90
31	388.62	172.41	-37.99
32	396.24	172.48	-37.54

33	403.86	174.41	-34.73
34	411.48	176.06	-32.00
35	419.10	165.02	-30.80
36	426.72	164.50	-30.43
37	434.34	165.13	-29.76
38	441.96	165.38	-29.48
39	449.58	165.36	-28.86
40	457.20	165.57	-28.55
41	464.82	166.27	-27.89
42	472.44	165.59	-27.69
43	480.06	166.08	-26.97
44	487.68	165.21	-26.60
45	493.17	166.11	-26.65

F	- I	N	F	R	V	A	L	-	CORE	T	-	%	TYPI	-	UAL	TEX	-	GRAIN	PGI	STRUCTUR	-1	ALTERATION	MINS	ORE	-TYPE	MINS	SUMMARY
K	L	(DEITS =	. DEC.	PLACE)	RECDV	-	M	M	ROCK	FYING	MIN	TURES	CHARACS														
E	A	(METRIC FT=FOOTRIC)	ERY	0	1																						
Y	G	F R G M - I D - I N I (.)	0	X	TYPE	1	2	001	1	2	F	F	C	A													
K	F		ROCK	FR	RT	IN	002	TX	TX	S	C	O	O	CHT													
E	I		QUAL	AGE	EN	0	LC	3	3	4	0	/															
Y	G		DESIG	VIR	COL																						

R SVY 0.00 0.00 ALL DATA FROM DETAILED GYROSCOPIC SURVEY OF DDH 80-638.
R SVY 248.41 248.41 BEGINNING OF WEDGED HOLE A.
R SVY 248.41 248.41 HALL AND ROWE STEEL WEDGE.
R SVY 269.14 269.14 BEGINNING OF WEDGED HOLE B.
R SVY 269.14 269.14 HALL AND ROWE STEEL WEDGE.

/	0.00	269.14	269.14		MISS																									
L																														
/	269.14	321.67	52.53		BRHM			S12	H*	R*				NR9	P	CL	40	<*		<*	<*									
L					1A			F*						LN*																
R	269.14	321.67																												
/	FAL	270.88	271.08	0.20		X	FAUL				GG9																			
L								1A																						
/	SHR	276.75	277.06	0.31		X	FAUL				GG5																			
L								1A																						
/	FLT	280.93	281.34	0.41		X	FAUL				GG5																			
L								1A																						
/	FGT	285.29	291.90	6.61		X	ARST				S12	SS																		
L																														
R	285.29	291.90																												
/		321.67	333.28	11.61		BRHM					S12	H*	R*																	
L																														
/		321.67	333.28	11.61		3	BRHT				*C)	H*	F*																	
L								2A				B*	R*																	
R	321.67	333.28																												
/		333.28	334.89	1.61																										
L																														
R	333.28	334.89																												
R	333.28	334.89																												

R 333.28 334.89 LARGE CLASTS OF CHERT AND ARGL. SAND SIZED PRIMARILY CHERT.
R 333.28 334.89 PYRITE AS DISSEMINATIONS IN SAND, BLSRS IN QUARTZ VEINS.

/ 334.89 334.89 0.00

BRHM

S12 H*

NR9

P

00


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/ LSX  502.69  503.54  9.65          LMSX GL SL CH6 SS          P  1 LM          45 >1          B1 L=          L=          L+
|

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7	LSX	513.75	514.30	0.55	LP SX BA SL CH4 SS	P	1	LM	25	L2	L1	L1
1							0	00	00			1

[illegible]

R	536.75	540.41	THREE ASSAY INTERVALS WERE TAKEN ALONG THIS LENGTH. SULPHIDES
R	536.75	540.41	BEGIN TO SHOW UP AS BLEBS AND AS BRECCIA FILLINGS.
R	536.75	550.16	COMPOSITIONAL CHANGES ARE VERY RAPID WITHIN THIS PGI. IT IS
R	536.75	550.16	DOMINATED BY VARIOUS SIZES OF SAND CLASTS, BUT ARGILLITE BRECCIA
R	536.75	550.16	IS VERY COMMON. THIS BRECCIA IS FREQUENTLY CONTINUOUS WITH
R	536.75	550.16	BRPP, THE LATTER CONTAINING SAND CLASTS UP TO COBBLE SIZE.
R	536.75	550.16	CHERT CLASTS ARE RARE.

/	539.45	539.02	0.57	FROM GL SL SEP	M06	P	>=	>)	61	61
L				1A 9A	C			>1		6)

R	538.45	539.02	THIS INTERVAL IS HIGHLY BRECCIATED, HENCE THE HIGH SULPHIDE
R	538.45	539.02	CONTENT, PRIMARILY AS BRECCIA FILL.

Z	539.02	540.41	1.39	BRECCIA GL SL SP2	M06	P	V+	<	81	0.
L								V+		V*
R	539.02	540.41		BRECCIA ABSENT.						

7	540.41	550.15	9.75	BKHF	5.15	L09	P	<1	<*	8= 8=
L						3 0 KN+			C. <= <1	

/ FGT	540.41	550.15	9.75	2 SAND	CR+ SS	3 4 3 4	2
L					SP9	7	1

/	540.41	550.16	9.75	1	RRP4 CR	SD2 SS P* 0 1	1	R	<1	B=
L							1	KN+	C. <= <1	

R	540.41	550.16	THIS PGY CHARACTERIZED BY NUMEROUS QZ-SO CROSS CUTTING VEINLETS.
R	540.41	550.16	THIS SAND IS CLASTS OR SMALL INTERBEDS WITHIN THE BRHM.

/ FGT	543.57	543.36	0.49	x SAND	3 4 3 4	R	<1	<*	B) B*
L					7			C. <= <1	

Z	FGT	545.67	546.40	0.73	X SAND	3 4 3 4	R	<1	<*	8)
L						7			C. <= <1	

Z	550.16	550.72	0.56	BRPM SY	SN1 SS	0 1	1	P	<)	<=	D= B+
L				E		1			C. <*		

R	550.16	550.72	ASSAYED INTERVAL; CHALCOPYRITE WAS PROBABLY THE IMPETUS.
R	550.16	559.00	ORIGINALLY LOGGED AS STRONGLY KNEIST ZONE WITH POSSIBLE
R	550.16	559.00	CORRELATION WITH DDH-80-63: 555.0 M. - 565.0 M.

1	559.72	559.40	4.28	SE 2	SE	SE 3	NP 8	P	#2	8
1					1A					C #1 #2

7	FGT	550.72	559.00	8.28	3	SAND	Ch)	R	#1	D*
L						2A				C. # = #1

1	550.72	559.00	8.28	2	BRHM SF	R
L					PI	

Q	559.72	559.00	MODERATE TO INTENSE QZ-SD VEINING IN CRACKLE BRECCIA.
R	559.72	559.00	MAINLY IN UPPER PART OF INTERVAL WHERE QZ-SD VEINING REDUCED.
R	559.72	559.00	DOMINATES LOWER INTERVAL, AND HAS INTENSE QZ-SD VEINING.

Z	559.00	561.90	2.90	REFRM CR SF SF= SS SC 0 1	1 K01	P	<)	B*
L					0			
R	559.00	561.90		PYRITE OFTEN REPLACES ARGILLITE CLASTS.			C. <*	<1

G F O I D G

A DMB	SAMPLE		% PR	% ZM	% BA	OZ AG	% CU	% FE	OZ AU	% CD	HASH	
A LAB	SERIAL		B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		
A TYP	NUMBER		H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH			WA	WA	WA	WA	WA	WA	WA	WA		
R ASY	0.00	0.00	B.CLG = BOLDAR CLEGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00	WA = WET ANALYSIS.									
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -D.L. F.G. -0.01									
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1									
A 001	491.49	493.70	215	0.21	0.27	3.84	0.19	-0.01	3.50	-0.002	-0.1	8.498
A 001	493.70	495.10	125	0.82	2.95	2.55	0.18	-0.01	4.48	-0.002	-0.1	10.868
A 001	495.10	498.42	319	0.18	0.22	4.64	0.09	-0.01	1.90	0.010	-0.1	6.930
A 001	498.42	499.30	88	0.66	3.27	0.41	0.12	-0.01	3.60	-0.002	-0.1	7.948
A 001	499.30	499.80	50	0.94	2.68	1.34	0.13	-0.01	1.45	0.002	-0.1	6.432
A 001	499.80	500.72	92	9.10	13.40	1.14	0.70	0.01	1.35	0.003	-0.1	25.603
A 001	500.72	501.36	60	3.18	5.58	1.36	0.25	-0.01	1.95	0.002	-0.1	12.212
A 001	501.36	502.09	73	2.40	4.25	5.41	0.33	-0.01	10.45	-0.002	-0.1	22.728
A 001	502.09	502.89	80	3.00	5.90	2.68	0.52	-0.01	2.67	-0.002	-0.1	14.658
A 001	502.89	503.58	65	1.56	2.13	2.91	0.32	-0.01	1.70	-0.002	-0.1	8.508
A 001	503.58	504.14	60	3.50	7.55	1.26	0.55	-0.01	2.75	-0.002	-0.1	15.498
A 001	504.14	504.74	58	2.70	2.65	9.55	0.47	-0.01	5.45	-0.002	-0.1	20.708
A 001	504.74	505.44	67	0.25	0.27	9.24	0.07	-0.01	3.10	-0.002	-0.1	12.818
A 001	505.44	506.48	100	0.09	0.06	8.04	0.06	-0.01	3.50	-0.002	-0.1	11.638
A 001	506.48	507.30	79	0.15	0.09	5.70	0.08	-0.01	5.10	-0.002	-0.1	11.008
A CMP	499.80	504.74	491	3.91	6.32	-0.10	0.30	-0.01	-0.10	-0.10	-0.1	10.120
A 001	510.24	511.20	95	0.08	0.01	12.53	0.04	-0.01	3.23	-0.002	-0.1	15.778
A 001	511.20	512.21	101	0.10	0.16	13.57	0.10	-0.01	3.45	-0.002	-0.1	17.268
A 001	512.21	513.30	109	2.53	2.70	1.50	0.62	-0.01	5.30	-0.002	-0.1	12.538
A 001	513.30	513.75	45	2.51	3.65	26.04	0.45	-0.01	3.15	-0.002	-0.1	35.888
A 001	513.75	514.30	55	4.50	5.20	0.82	0.75	-0.01	3.50	-0.002	-0.1	14.658
A 001	514.30	514.67	57	4.55	6.65	0.31	0.88	-0.01	3.80	-0.002	-0.1	16.078
A 001	514.67	515.51	64	1.54	5.74	1.66	0.39	-0.01	3.40	-0.002	-0.1	12.618
A 001	515.51	516.56	103	0.22	0.97	13.27	0.10	-0.01	4.25	-0.002	-0.1	18.698
A 001	516.56	517.10	52	1.30	3.15	7.50	0.39	0.01	1.55	-0.002	-0.1	13.798
A 001	517.10	517.64	52	0.21	0.77	14.75	0.10	-0.01	4.50	-0.002	-0.1	20.218
A 001	517.64	518.25	58	1.52	4.05	4.96	0.50	0.01	3.10	-0.002	-0.1	14.038
A 001	518.25	518.93	62	0.08	0.07	2.26	0.10	-0.01	4.50	-0.002	-0.1	7.298
A 001	518.93	519.84	71	0.05	0.04	0.37	0.11	-0.01	5.00	-0.002	-0.1	5.458
A CMP	512.21	515.51	330	3.01	4.55	-0.10	0.62	-0.10	-0.10	-0.10	-0.1	7.680
A 001	536.75	536.45	68	0.81	0.13	0.35	0.03	0.02	5.05	-0.002	-0.1	6.288
A 001	536.45	539.02	45	4.30	0.77	0.08	0.49	0.10	24.18	-0.002	-0.1	29.818
A 001	539.02	540.41	111	0.15	0.07	0.66	0.06	0.04	6.35	-0.002	-0.1	7.228
A 001	550.16	550.72	56	0.02	0.02	0.84	0.33	1.22	4.10	0.002	-0.1	6.432

G E O L O G F O I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PR-7N-AC-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILL HOLE/TRaverse : RT-AD01	COLLAR ELEVATION: 0.00	AZIMUTH(DEG) : 0.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 0.00	NORTHING(- IF S): 0.00	VERTICAL ANGLE :*****	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER :	EASTING (- IF W): 0.00	CO-ORD SYSTEM :	PROJECT NUMBER : JASON

F - I N T E R V A L -		CORE	T- %	TYP1- PAL	TEX-	GRAIN	PGI	STRUCTUR-1 ALTERATION MINS										ORE-TYPE MINS				SUMMARY														
K L (UNITS = . DEC.PLACE) RECUV-		N W ROCK	RYING	MIP	TURES	CHARACS		H	H	H	H	H	ANY	H	H	H	ANY	ALT	ORE																	
E A (MI=METRIC FI=FOOT-IC) ERY		D I	IR	IR	KAT	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-						
Y G F R D N - I D - I N T (.)		D X TYPE	1	2	001	1	2	F	F	C	A		1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2							
-----		ROCK	FR	RT	10	002	TX	TX	S	C	D	D	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA									
K F		QUAL	AGE	EN	0	LC	3		4	4	0	/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1							
F L		DESIG	VIR	CHL												STRUCTUR-2										A	A	A	A	A	A	A	A	A	2	2
Y G																																				

G E O L O G

A URM	SAMPLE	% PB	% Zn	% RA	OZ AG	% CU	% FE	OZ AU	% CD	HASH
A LAB	SERIAL	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	
A TYP		H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	
A MTH		WA	WA	WA	WA	WA	WA	WA	WA	

R ASY 0.00 0.00 ***THIS IS A ASSAY A001 FILE HEADER AND SAMPLE***

R ASY 0.00 0.00

R ASY 0.00 0.00 B.CLG = BENJAMIN CLEGG, VANCOUVER; H-CORE = HALF CORE.

R ASY 0.00 0.00 WA = WFT ANALYSIS.

R ASY 0.00 0.00 HASH TOTALS SHOULD BE FROM ASSAY SHEET SUMS.

R ASY 0.00 0.00 LESS THAN DETECTION LIMIT ENTERED AS -D.L. E.G. -0.01, -0.50

R ASY 0.00 0.00 NO ASSAY INFORMATION ENTERED AS -0.1

A MIN

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAR OCEAN OIL LTD.

JASON PR-ZU-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :81-A005	COLLAR ELEVATION:	0.00	AZIMUTH(DEG) :	0.00	GEOLOGGED BY :	+
TOTAL DEPTH/LENGTH : 0.00	DORTHING(- IF S):	0.00	VERTICAL ANGLE :*****		DATE (YY/MM/DD):	0
CORE/HOLE DIAMETER :	EASTING (- IF S):	0.00	CO-ORD SYSTEM :		PROJECT NUMBER :	JASON

F - I N T E R V A L -		CORE	I- 2	TYPJ- CAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)RECDV-	M-R ROCK	RYING	MIN	TURES	CHARACS		H	H	H	H	ANY
E	A (MT=METRIC FT=FOOTRIC) ERY	D I	IN	TH	NAT	TX TX F C % M ARG	/RI	T	ID	STK	DIP	A A A A A MIN A A A MIN - - - -
Y	G F R O M - I D - I D T (.)	D X TYPE	1	2	QMI	1 2 F F C A	1	AZM	RT	QZ	FL	CY CA BA XX PY CP GL YY A 1 A 2
K	F	ROCK	FM	RT	IN	QMI TX TX S C D O CHT	T	ID	STK	DIP	MG MU CL SD QS HA PR MT SL HA	
F	L	QUAL	AGE	FM- D	IC- 3	3 4 0 /	2	AZM	RT	H	H H H H H H H H H	1 1
Y	G	DESIG	VIR	COL		6 C		STRUCTUR-2	A	A A A A A A A A A		2 2

G E O L O G

JASCO PB-7K-AG-BA STF DEPOSIT, Y.T.
DRILLHOLE/TRAVERSE --- 81-A005 --- (CONTINUED)

A IMM	SAMPLE	L.R.GL	H.R.GL	L.R.SL	H.R.SL	L.R.BA	H.R.BA	L.R.PY	H.R.PY
A LAB	NUMBER	VCR.P.	VCR.P.	VCR.P.	VCR.P.	VCR.P.	VCR.P.	VCR.P.	VCR.P.
A TYP		PS+TS	PS+TS	PS+TS	PS+TS	PS+TS	PS+TS	PS+TS	PS+TS
A MTH		VISUAL	VISUAL	VISUAL	VISUAL	VISUAL	VISUAL	VISUAL	VISUAL

R ASY 0.00 0.00 ***THIS IS A ASSAY A005 FILE HEADER AND SAMPLE***

R ASY 0.00 0.00

R ASY 0.00 0.00 L.R. = LOW RANGE; H.R. = HIGH RANGE; GL = GALENA;

R ASY 0.00 0.00 SL = SPHALERITE; BA = BARITE; PY = PYRITE. SIZE IS IN MM.

R ASY 0.00 0.00 VCR. P. = VANCOUVER PETROGRAPHIES LTD.; PS+TS = POLISHED SEC'NS.

R ASY 0.00 0.00 POLISHED THIN SECTIONS AND THIN SECTIONS OF MINERALIZED SAMPLES.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAC OCEAN OIL LTD.
JASOL PB-70-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 31-A100	COLLAR ELEVATION: 0.00	AZIMUTH(DEG) : 0.00	GEOLOGGED BY : +
TOTAL DEPTH/LENGTH : 0.00	NORTHING(= IF S): 0.00	VERTICAL ANGLE :*****	DATE (YY/MM/DD): 0
CORE/HOLE DIAMETER :	EASTING (= IF N): 0.00	CO-ORD SYSTEM :	PROJECT NUMBER : JASON

F - I N T E R V A L -		CORE	T- %	TYPI- GAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																
K	L (UNITS = . DEC.PLACE)RECDV-	M M ROCK	RYING	MIN	TURES	CHARACS		H H H H H	ANY	H H H	ANY	ALT ORE																
E	A (MI=METRIC FT=FOOTRIC) ERY	Q T	TS TR MAT	TX	TX	F C % M	ARG	/RI	T ID	STK	DIP	A A A A A	MIN A A A	MIN - - -														
Y	G F R D H - T D - I N T (.)	O X TYPE	1	2	QMI	1	2	F F C A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2			
K	F	ROCK	FM	RT	TM	PM2	TX	TX	S	C	O	O	CHT	T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA	
E	L	QUAL	ARE	FO	Q	LC	3	3	4	O	/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1
Y	G	DESIG	VTP	COL				R	C					STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2

G E O L O G

A IMM

ROD

SP.GR.

A TYP

CM

SG

A MTH

R-B

WEIGH

A LAB

FLD

FLD

R ASY 0.00 0.00 ***THIS IS A ASSAY AND FILE HEADER AND SAMPLE***

R ASY 0.00 0.00

R ASY 0.00 0.00 RECOVERY(C17-20) IS MEASURED TO CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 ROD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 ROD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 OR INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 R-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. R-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE A-MTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST.

G E O L O G F I L I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAO OCEAN OIL LTD.
JASOB PR-ZY-AG-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH068	COLLAR ELEVATION: 1275.94	AZIMUTH(DEG) : 0.00	GEOLOGGED BY : DWB + RJT
TOTAL DEPTH/LENGTH : 971.40	NORTHING(- IF S): 7002472.00	VERTICAL ANGLE : -90.00	DATE (YY/MM/DD): 810521
CORE/HOLE DIAMETER : 40MM	EASTING (- IF +): 436496.25	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-S3

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.00	146.90	-89.47
2	61.00	169.10	-87.40
3	91.00	151.30	-85.47
4	122.00	131.50	-86.75
5	152.00	124.20	-86.42
6	183.00	121.80	-86.10
7	213.00	117.80	-86.00
8	244.00	117.20	-85.38
9	274.00	120.10	-84.13
10	305.00	132.80	-84.92
11	335.00	151.50	-84.20
12	368.69	143.00	-85.00
13	350.82	139.00	-84.50
14	369.11	157.00	-83.25
15	419.10	166.00	-80.25
16	425.81	166.00	-80.25
17	436.73	173.00	-80.00
18	445.31	173.00	-79.75
19	459.33	181.00	-78.33
20	475.48	179.00	-77.00
21	491.34	176.00	-76.50
22	505.97	177.00	-75.50
23	518.46	175.00	-75.25
24	535.53	172.00	-74.50
25	555.65	170.00	-73.25
26	571.50	170.50	-72.00
27	588.57	168.00	-70.75
28	605.64	168.00	-68.33
29	617.83	167.00	-67.50
30	620.27	168.00	-68.00
31	630.02	166.00	-66.25
32	642.21	167.00	-66.00

33	654.41	167.00	-66.00
34	666.60	165.00	-65.75
35	673.61	162.00	-65.67
36	678.79	165.00	-65.50
37	690.95	165.00	-65.50
38	703.17	166.00	-65.00
39	715.57	165.50	-65.00
40	727.56	166.00	-65.00
41	739.75	166.00	-65.00
42	751.94	166.00	-64.50
43	764.13	166.00	-63.75
44	776.33	166.50	-63.33
45	788.52	166.00	-63.00
46	800.71	167.00	-62.75
47	803.45	165.00	-62.75
48	812.90	166.50	-62.50
49	825.09	168.00	-62.50
50	837.29	168.00	-62.00
51	849.48	168.00	-61.00
52	867.67	169.00	-60.50
53	873.56	168.50	-59.75
54	886.95	168.00	-59.00
55	898.25	168.00	-58.25
56	910.44	167.00	-57.50
57	922.63	166.00	-56.33
58	933.91	164.00	-56.00
59	934.82	164.00	-54.67
60	947.01	162.50	-52.33
61	962.25	163.00	-52.33
62	968.35	163.00	-52.00

F - INTERVAL - CORE				T- %		TYPE- HAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION		MINS		ORE-TYPE		MINS		SUMMARY	
K L (UNITS = . DEC. PLACE) RECOV-				H M ROCK		FYING MIN		TUPES CHARACS		/RI T		ID STK DIP		A A A A		A A A A		A A A A		A A A A		A A A A	
E A (METRIC FEET) ERY				D T		TX TX TX TX		F C % M		ARG		AZM RT		QZ FL		CY CA		BA XX		PY CP		GL YY	
Y G F R D N - I D - I N T (.)				D X TYPE		1 2 051		1 2 F F C A		1		1		1		1		1		1		1	
K F				ROCK		FR		RT		TX TX TX TX		S C O O		CHT		T ID STK DIP		MG MU		CL SD		QS HA	
E L				QUAL		AGE		FR- D LG- 3		3 4 0		/		2		2		2		2		2	
Y G				DESIG		VTR		COL		R		C		STRUCTUR-2		A A A A		A A A A		A A A A		A A A A	

R SVY	0.00	348.69	DATA FOR UPPER PART OF HOLE OBTAINED FROM GYROCOMPASS SURVEY									
R SVY	0.00	348.69	OF DDH 81-68A. REMAINDER FROM SPERRY SUN MULTI-SHOT.									
R SVY	0.00	348.69	GYROCOMPASS DATA IS CONSIDERED MORE ACCURATE, AND SHOULD BE									
R SVY	0.00	348.69	USED FOR PLOTS.									
R SVY	0.00	348.69	A LISTING OF THE REPLACED SPERRY SUN DATA CAN BE FOUND									
R SVY	0.00	348.69	WITHIN THE "RSUM".									
R SVY	348.69	971.40	SURVEY DATA FROM SPERRY SUN MULTI-SHOT.									
R SVY	99.97	99.97	HALL AND ROSE STEEL WEDGE. DIP IS 1.5 TO STEEPEN									
R SVY	298.09	298.09	CLAP RETREIVABLE WEDGE. DIP.75 TO STEEPEN. HALF AZIMUTH TO									
R SVY	298.09	298.09	RIGHT.									
R SVY	325.22	325.22	CLAP RETREIVABLE WEDGE-FULL AZIMUTH TO THE RIGHT									
R SVY	359.05	359.05	CLAP RETREIVABLE WEDGE-FULL AZIMUTH TO THE RIGHT									
R SVY	412.70	412.70	CLAP RETREIVABLE WEDGE-FULL AZIMUTH TO THE RIGHT									
R SVY	432.21	432.21	CLAP RETREIVABLE WEDGE-FULL AZIMUTH TO THE RIGHT									
R SVY	447.45	447.45	CLAP RETREIVABLE WEDGE-FULL AZIMUTH TO THE RIGHT									

/ 0.00 6.10 6.10

TRIC

P

/ OFT 6.10 35.97 29.87

BRAB

PR9 P

LI B.

L 6.10 35.97 5A *S- 2 - MO+

C. B.

R 6.10 35.97 MINOR PYRITE NODULES WITH HT CORES IN SOME CASES. SIZE FROM

G E O L O G

K F F R D B - T O - I N T R E C O V		M D % R O C K I N T H D M 1 T X T X F C % M A R G		R I 1 I D A Z M D I P Q Z F L C Y C A B A X X P Y C P G L Y Y A 1 A 2	
E - L -		R D D A G E F V G G L C I N D M 2 T X T X S C D D C H T		2 I D A Z M D I P M G M U C L S D Q S H A P R M T S L H A	
Y G					

R 269.89 273.72 PEBBLY CHERT SANDSTONE (GRADING INTO CGCP). THE LARGEST OF THESE
R 269.89 273.72 IS 1.5 CMS.

/ 273.72 281.28 7.56 BRPM LS4 P D-
L 5A *S* 2 + JN+

/ 281.28 297.30 16.02 BRPM ST9 P D.
L 4A *S) 2) LL(

R 281.28 297.30 INTERVAL COMPRISES PREDOMINANTLY LARGE ARSI CLASTS-PROBABLY
R 281.28 297.30 A SLIGHTLY SLOPED ARSI UNIT.

/ 297.30 307.65 10.35 BRPM SL S* MQ8 P D.
L 5A *S* 2 * KO* < D.

/ 298.09 299.62 1.53 X LOST R

/ SHR 303.69 307.65 3.96 X BRPM SL S* MQ8 P D.
L 5A *S* 2 * KO* < D.

R 303.69 307.65 ROCK BETWEEN 303.69 AND 307.65 RUBBLY-PROBABLE SHEAR.
R 307.30 307.65 SL ASSOCIATED WITH SHALE CLAST AT 307.55M. SL OCCURS ALONG
R 307.30 307.65 UPPER AND LOWER MARGINS OF CLAST, PARALLEL TO BEDDING-SUGGESTS
R 307.30 307.65 EITHER PAERENTIAL REPLACEMENT OR ORIGINAL BEDDED SULFIDE
R 307.30 307.65 -PROBABLY A SULFIDE CLAST.

R 307.30 307.65 TRACE SD VETTING DISPLACED BY MINOR FAULTS.

/ 307.65 311.19 3.54 CGXX SF HS I N 3 0 LP1 P D*
L 6A 5 C LN8

/ 307.65 311.19 3.54 3 ARGL GR SII HS 1 1 1 R
L 2A LM

R 307.65 311.19 BOURA SEQ: A-E, A-E; EXCELLENT EXAMPLE! SEVERAL CYCLES
R SIG 307.65 311.19 RANGING FROM CONGLOA TO SANDSTONE. POSSIBLE MARKER BED.

/ 311.19 322.68 11.49 BRPM MT9 P #. #. #.
L 4A *S* 2 * LO+ #.

R 311.19 322.68 PY, PP AND GL OCCUR TOGETHER WITH CALCITE IN A VUG AT 321.92M
R 311.19 322.68 (VUG APPROX 4 CMS DIAMETER).

/ 322.68 353.40 30.72 BRPM MT6 P D.
L 4A *S(2 * (LP+

K UDF 353.40 353.40 0.00
R 353.40 353.40 TOP OF THICK SEQUENCE OF DEBRIS FLONS CHARACTERIZED BY
R 353.40 353.40 CGCP CLASTS.

/ 353.40 366.67 13.27 BRPM MT6 P D.
L 6A 2 LP3

/ 353.40 354.59 1.19 X BRPM / J B R KR4 R D-
L 6A 4 JL4

/ 366.67 380.62 13.95 BRPM MT5 P D.
L 5A 2 3 + MO1

G E O L O G		JASON PR-ZN-AG-BR STF DEPOSIT, Y.T.																				PAGE - 6																															
K F F R O S - I O - T N I		REC'D		MD %		ROCK		TM		TM		QMI		TX		TX		F C %		M ARG		RI 1		ID		AZM		DIP		QZ		FL		CY		CA		BA		XX		PY		CP		GL		YY		A 1		A 2	
E -L- - - - -		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---	
Y G		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---		---	

R 364.67 380.62 INTERVAL CONTAINS SEVERAL LARGE CBGP CLASTS(?), ONE OF WHICH
R 366.67 380.62 IS 1M IN LENGTH.

/ 371.43 372.58 1.15 X CBGP SF SD J M 6 0 LM= R D.
L 8A *S= 5 - 0 M09 0)

/ 380.62 387.77 7.15 BRHT NS9 P D-
L 4A *S* 2) * KN1

/ FLT 380.62 383.97 2.45 X FAUL GR R

/ FLT 384.00 385.50 1.30 X FAUL GR R

/ 386.80 387.77 0.97 X ARG1 SF R D-
L 6A <+

R SIG 386.80 387.77 POSSIBLE FRAGMENT OF BR CHERT-CUT BY NS VNS-FOOTWALL FRAG?

/ 387.77 393.90 6.13 BRHT MS9 P D.
L 4A *S) 2 =) LN+

/ 393.90 409.50 15.60 BRHT CR RT7 P D.
L 4A *S+ 2 + IO=

/ FAL 405.00 407.52 2.52 X FAUL GR G62 R D.

/ 409.50 412.70 3.20 BRHT CR QR7 P D-
L 4A *S* 2 * LN2

R 409.50 412.70 GENERALLY CLOSED; OCCAS OPEN, WITH MOD MTX.

/ 409.50 410.16 0.66 X FAUL GR R D-
R 409.50 410.16 RUBBLY CORE

/ 412.70 418.60 5.90 BRHT CR QR7 P D*
L 4A *S= 2 = M02

R 412.70 418.60 INTERVAL OCCASIONALLY "OPEN" WITH SANDY MTX (I).

/ 418.60 439.17 20.57 BRHT CR RSS P D.
L 4A *S) 2 4) MP=

R 418.60 439.17 INTERVAL CHARACTERIZED BY NUMEROUS LARGE CONG FRAGS RANGING FROM
R 418.60 439.17 20 CMS TO 1 METER. GENERALLY CLOSED; OCCASIONALLY OPEN WITH
R 418.60 439.17 BRHT MTX.

/ 421.80 422.15 0.35 X FAUL GR R
R 421.80 422.15 RUBBLY CORE

/ 432.21 433.73 1.52 X LOST R

/ 437.00 438.42 1.42 X CBGP SF SD 0 L 4 0 K01 R
L 5A *S) 5) 0 KN6 01

R 437.00 438.42 INTERVAL STERILIZED+SILTIFIED, PARTIC. ARG1 FRAGS-ALSO MTX.
R 437.00 438.42 BR HT ASSOCIATED LOCALLY. DERIVED FROM FOOTWALL(?)

K	F	F	R	O	I	-	T	O	-	I	N	T	RECDV	MD	%	ROCK	TM	TM	Q01	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G												R	O	D	AGE	EV	RO	LC	TM	Q02	TX	TX	S	C	D	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA								

R 703.91 704.65 CR BEDS OF SILICEOUS ARGILLITE WITH BEDS OF LAMINATED QC,PY,SL.
 R 703.91 704.65 SILICEOUS; IN DETAIL SULPHIDE LAMINATIONS SHOW PY, SL,
 R 703.91 704.65 INTERSTITIAL TO AUTIGENIC (?) FUEHRAL QZ GRAINS.

/ 704.65 706.65 2.00 ARSI PY LM PY P L=

L 5A
 R 704.65 706.65 WIDESPREAD ALTERATION OF SILICEOUS ARGILLITE BY BANDS OF
 R 704.65 706.65 VEG FUEHRAL TO ANHERAL CARBONATES ?

K US2 706.65 706.65 0.00

/ 706.65 707.35 0.70 MSSX PY CR CH1 MX P X5 X=

L 5L
 R 706.65 707.35 CRUDELY BEDDED-MOTTLED TEXTURE DEFINED BY ARGL & SULFIDE- RICH
 R 706.65 707.35 ZONES. MOD-STRONG SILICIFICATION OF ARGL.

/ 707.35 708.36 1.01 BMSX SF SL CH7 RN P 2 BD T42 <) <) L= L+

L 5A GL L1
 R 707.35 708.36 INTRO CHT, MSSX & POSSIBLY SILICIFIED ARGL. SULFIDE LAYER
 R 707.35 708.36 BUFF-COLOURED-COMPRISED SL, GL, PY & RTZ/MNR CALC.

/ 708.36 707.85 59.49 BMSX RA SL CH5 SS ST P 2 BD T42 <) L4 L+ L+

L 6A GL BN L=
 R 708.36 707.85 ALTERATING BANDS & LAP OF CHT, BARITE & SULFIDES
 R 708.36 707.85 CH1-BUFF, CRXL, CONTAINS SCATTERED CALC PODS.
 R 708.36 707.85 BARITE-VFXL, PGY, SUCROSTIC TEX
 R 708.36 707.85 SULFIDES-GL, SL, PY.
 R 708.36 707.85 -PYR-TENDS TO BE DISSEM THROUGHOUT ROCK IN BOTH CHT & BA
 R 708.36 707.85 BANDS.

R 708.36 707.85 -SL & GL TEND TO OCCUR AS THIN LAM(1-2MM), GENERALLY WITHIN
 R 708.36 707.85 BARITIC BANDS BUT LOCALLY IN CHERTY BANDS. SL & GL ARE
 R 708.36 707.85 INTERGROWN WITH CHT, BARITE & CALCITE.
 R 708.36 707.85 LATE BARREN NTZ VNS TEND TO BE PERPENDICULAR TO BEDDING.

/ 712.80 718.00 5.20 X BMSX BA SL CH5 SS ST R 2 BD T75 <) L4 L+ L+

L

/ 718.00 718.85 0.85 X BMSX BA SL CH5 SS ST R 2 BD T60 <) L4 L+ L+

L

/ 718.85 723.20 4.35 X BMSX BA SL CH5 SS ST R 2 BD T82 <) L4 L+ L+

L

/ 723.20 724.90 1.70 X BMSX BA SL CH5 SS ST R 2 BD T60 <) L4 L+ L+

L

/ 724.90 728.90 4.00 X BMSX BA SL CH5 SS ST R 2 BD T52 <) L4 L+ L+

L

/ 728.90 730.50 1.60 X BMSX BA SL CH5 SS ST R 2 BD T75 <) L4 L+ L+

L

G E O L O G

A UMM			SAMPLE	% P3	% ZN	% BR	OZ AG	% CU	% FE	OZ AU	SG	HASH
A LAB			NUMBER	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		TOTAL
A TYP				H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
A MTH				WA	WA	WA	WA	WA	WA	WA		
R ASY	0.00	0.00	B.CLG = BONDAR CLFGG, VANCOUVER; H-CORE = HALF CORE.									
R ASY	0.00	0.00	WA = DET ANALYSIS									
R ASY	0.00	0.00	HASH TOTALS SHOULD BE ENTERED FROM SUMS ON ASSAY SHEETS.									
R ASY	0.00	0.00	LESS THAN DETECTION LIMIT ENTERED AS -0.1. E.G. -0.01									
R ASY	0.00	0.00	NO ASSAY INFORMATION ENTERED AS -0.1									
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A MAX	652.00	676.74		6.00	18.44	51.06	0.41	0.01	7.73	-0.10	-0.10	83.45

A MIN	0.03	0.40	2.61	0.02	-0.01	0.50	-0.10	2.90	25.32
A MAX	0.42	3.85	41.95	0.66	-0.01	18.47	-0.10	3.90	73.14

G E O L O G

A MIN					0.02	0.20	1.20	0.02	-0.01	1.46	-0.10	-0.10	2.69
A MAX	776.00	797.66			1.70	4.60	13.75	0.10	0.01	6.93	-0.10	2.80	29.79
A 001	652.88	653.88	100	DB9873	0.02	0.07	9.45	0.04	-0.01	2.41	-0.10	-0.10	11.78
R ASY	652.88	676.74		SOUTH ZONE #1: INTERVAL 653.88-671.55M.									
A 001	653.88	654.10	22	DB9874	6.00	18.44	13.77	0.41	0.01	7.73	-0.10	-0.10	46.16
A 001	654.10	655.50	140	DB9875	1.05	2.56	42.09	0.02	-0.01	0.43	-0.10	-0.10	45.94
A 001	655.50	655.93	32	DB9876	1.11	2.18	48.50	0.02	-0.01	1.18	-0.10	-0.10	52.78
A 001	655.93	656.93	100	DB9877	0.88	3.80	51.06	0.02	-0.01	0.57	-0.10	-0.10	56.12
A 001	656.93	657.93	100	DB9878	0.77	3.45	42.77	0.04	-0.01	0.40	-0.10	-0.10	47.22
A 001	657.93	658.98	41	DB9879	1.60	4.60	41.69	-0.02	-0.01	3.64	-0.10	-0.10	51.30
A 001	658.98	660.26	128	DB9880	1.03	3.10	44.16	0.02	-0.01	1.18	-0.10	-0.10	49.28
A 001	660.26	660.81	29	DB9881	2.21	1.98	7.97	0.03	-0.01	2.89	-0.10	-0.10	14.87
A 001	660.81	661.11	30	DB9882	0.48	4.20	8.65	0.04	-0.01	2.51	-0.10	-0.10	15.67
A 001	661.11	662.21	110	DB9883	0.12	0.44	8.06	-0.02	-0.01	2.66	-0.10	-0.10	11.05
A 001	662.21	662.64	12	DB9884	2.08	4.70	28.60	0.04	-0.01	3.77	-0.10	-0.10	38.98
A 001	662.64	663.24	57	DB9885	1.17	3.65	48.40	0.02	-0.01	0.48	-0.10	-0.10	53.51
A 001	663.24	664.16	80	DB9886	1.55	4.05	41.63	-0.02	-0.01	0.70	-0.10	-0.10	47.70
A 001	664.16	664.77	34	DB9887	2.26	4.40	40.89	-0.02	-0.01	0.58	-0.10	-0.10	47.90
A 001	664.77	665.27	31	DB9888	0.78	1.60	16.24	0.02	-0.01	2.28	-0.10	-0.10	20.71
A 001	665.27	666.50	16	DB9889	0.58	3.85	26.69	-0.02	-0.01	2.56	-0.10	-0.10	33.45
A 001	666.50	667.82	63	DB9890	1.78	3.08	39.50	0.02	-0.01	0.98	-0.10	-0.10	45.15
A 001	667.82	669.34	58	DB9891	1.70	4.80	42.75	0.03	-0.01	1.26	-0.10	-0.10	50.33
A 001	669.34	671.17	9	DB9892	1.54	5.05	46.10	0.02	-0.01	0.39	-0.10	-0.10	52.89
A 001	671.17	671.55	11	DB9893	0.14	7.15	24.83	0.02	-0.01	4.42	-0.10	-0.10	36.35
A 001	671.55	672.08	41	DB9894	0.12	1.27	7.10	0.02	-0.01	2.16	-0.10	-0.10	10.46
A 001	672.08	673.08	100	DB9895	0.04	0.26	9.83	0.02	-0.01	7.86	-0.10	-0.10	17.80
A 001	673.08	673.95	87	DB9896	1.88	2.39	9.56	0.10	-0.01	1.86	-0.10	-0.10	15.58
A 001	673.95	674.22	27	DB9897	0.18	0.30	10.15	0.02	-0.01	1.91	-0.10	-0.10	12.35
A 001	674.22	674.83	26	DB9898	1.89	1.26	9.85	0.13	-0.01	2.21	-0.10	-0.10	15.13
A 001	674.83	675.74	42	DB9899	0.07	0.59	6.77	0.02	-0.01	2.46	-0.10	-0.10	9.70
A 001	675.74	676.74	100	DB9900	0.06	0.21	6.24	0.03	-0.01	2.96	-0.10	-0.10	9.29
A 001	703.17	703.91	74	DB9826	0.03	0.40	8.80	0.06	-0.01	6.28	-0.10	3.00	18.46
R ASY	703.17	750.29		SOUTH ZONE #2: INTERVAL 706.65-749.29M.									
A 001	703.91	704.65	74	DB9827	1.24	2.83	9.83	0.31	-0.01	4.52	-0.10	2.90	21.52
A 001	704.65	705.65	100	DB9827	0.43	1.63	11.90	0.13	-0.01	4.32	-0.10	3.00	21.30
A 001	705.65	706.65	100	DB9828	0.48	2.50	11.00	0.16	-0.01	4.32	-0.10	3.00	21.35
A 001	706.65	707.36	71	DB9830	4.42	2.97	2.61	0.66	-0.01	18.47	-0.10	3.40	32.42
A 001	707.36	708.36	100	DB9831	2.65	3.85	9.09	0.43	-0.01	2.26	-0.10	2.90	21.07
A 001	708.36	709.36	100	DB9832	3.32	3.80	22.20	0.53	-0.01	1.26	-0.10	3.20	34.20
A 001	709.36	710.36	100	DB9833	1.92	2.95	39.58	0.24	-0.01	0.60	-0.10	3.60	48.78
A 001	710.36	711.36	100	DB9834	1.22	2.75	33.65	0.19	-0.01	1.00	-0.10	3.40	42.10
A 001	711.36	712.36	100	DB9835	0.93	3.12	34.50	0.14	-0.01	1.41	-0.10	3.50	43.49
A 001	712.36	713.36	100	DB9836	1.18	2.67	36.75	0.29	-0.01	1.20	-0.10	3.60	45.58
A 001	713.36	714.36	100	DB9837	1.18	3.10	32.40	0.25	-0.01	1.33	-0.10	3.40	41.55
A 001	714.36	715.36	100	DB9838	0.84	2.18	39.60	0.18	-0.01	1.76	-0.10	3.60	48.05
A 001	715.36	716.36	100	DB9839	0.52	2.95	36.90	0.18	-0.01	1.76	-0.10	3.50	45.70
A 001	716.36	717.25	89	DB9840	0.60	2.95	34.20	0.18	-0.01	2.79	-0.10	3.50	44.11
A 001	717.25	718.25	100	DB9841	1.25	2.76	26.95	0.19	-0.01	1.66	-0.10	3.30	36.00
A 001	718.25	719.33	108	DB9842	1.16	2.28	29.00	0.15	-0.01	6.33	-0.10	3.60	42.41
A 001	719.33	720.33	100	DB9843	1.90	2.00	32.90	0.30	-0.01	2.54	-0.10	3.50	43.03
A 001	720.33	721.33	100	DB9844	0.98	2.05	22.96	0.23	-0.01	4.94	-0.10	3.20	34.25
A 001	721.33	722.33	100	DB9845	1.45	2.78	37.25	0.20	-0.01	0.83	-0.10	3.60	46.00

G F D L O G

					0.02	0.20	1.20	0.02	-0.01	1.46	-0.10	-0.10	2.69
					B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG	B.CLG		TOTAL
				H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE	H-CORE		
				WA	WA	WA	WA	WA	WA	WA	WA		
					0.02	0.07	0.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A MIN	A LAB	A TYP											
A 001	722.33	723.33	100	DB9846	1.96	2.80	41.55	0.34	-0.01	1.13	-0.10	3.70	51.37
A 001	723.33	724.33	100	DB9847	0.55	2.05	36.35	0.17	-0.01	1.31	-0.10	3.50	43.82
A 001	724.33	725.33	100	DB9848	1.82	1.75	36.30	0.19	-0.01	0.88	-0.10	3.40	44.23
A 001	725.33	726.42	109	DB9849	1.78	2.36	36.29	0.17	-0.01	1.08	-0.10	3.50	45.07
A 001	726.42	727.42	100	DB9850	1.56	2.52	39.70	0.13	-0.01	1.69	-0.10	3.60	49.09
A 001	727.42	728.42	100	DB9851	1.98	1.44	34.35	0.13	-0.01	1.71	-0.10	3.40	42.00
A 001	728.42	729.52	110	DB9852	0.82	1.40	32.13	0.08	-0.01	3.09	-0.10	3.50	40.91
A 001	729.52	730.52	100	DB9853	0.76	1.21	24.60	0.05	-0.01	2.31	-0.10	3.20	32.02
A 001	730.52	731.52	100	DB9854	0.86	1.77	39.50	0.05	-0.01	1.56	-0.10	3.50	47.13
A 001	731.52	732.52	100	DB9855	0.39	0.73	20.05	0.04	-0.01	2.08	-0.10	3.10	26.28
A 001	732.52	733.35	83	DB9856	0.60	1.45	28.53	0.04	-0.01	2.16	-0.10	3.30	35.97
A 001	733.35	734.97	152	DB9857	1.22	1.26	33.60	0.02	-0.01	3.06	-0.10	3.40	42.45
A 001	734.97	735.87	100	DB9858	1.86	1.19	40.30	0.03	-0.01	1.36	-0.10	3.50	48.13
A 001	735.87	736.37	100	DB9859	0.96	1.01	34.90	0.02	-0.01	2.16	-0.10	3.40	42.34
A 001	736.37	737.87	100	DB9860	0.43	1.15	35.15	0.03	-0.01	2.78	-0.10	3.50	42.98
A 001	737.87	738.37	100	DB9861	0.70	1.63	32.60	0.04	-0.01	2.18	-0.10	3.30	40.34
A 001	738.37	739.87	100	DB9862	0.32	1.16	16.75	0.03	-0.01	4.97	-0.10	3.10	26.22
A 001	739.87	740.87	100	DB9863	0.36	2.50	19.00	0.04	-0.01	3.44	-0.10	3.10	28.35
A 001	740.87	741.87	100	DB9864	0.54	2.28	28.20	0.03	-0.01	2.03	-0.10	3.30	36.27
A 001	741.87	742.37	100	DB9865	1.48	2.12	34.25	0.02	-0.01	1.96	-0.10	3.50	43.22
A 001	742.37	743.87	100	DB9866	2.24	2.20	41.60	0.02	-0.01	1.05	-0.10	3.90	50.90
A 001	743.87	744.87	100	DB9867	1.04	2.74	37.50	0.02	-0.01	1.03	-0.10	3.50	45.72
A 001	744.87	745.85	98	DB9868	0.83	2.98	39.50	0.02	-0.01	2.16	-0.10	3.60	49.03
A 001	745.85	746.35	100	DB9869	0.79	2.83	41.95	0.02	-0.01	0.50	-0.10	3.60	49.58
A 001	746.35	747.85	100	DB9870	1.14	3.25	32.25	0.03	-0.01	3.36	-0.10	3.50	43.42
A 001	747.85	749.29	120	DB9871	1.06	3.85	12.33	0.04	-0.01	2.46	-0.10	3.00	22.63
A 001	749.29	750.29	100	DB9872	0.06	0.44	11.91	0.04	-0.01	4.39	-0.10	2.90	19.63
A 001	750.29	751.07	91	66536	0.02	0.24	4.93	0.07	-0.01	4.00	-0.10	2.80	11.95
SOUTH ZONE #3; INTERVAL 778.07-796.66M.													
A 001	778.07	778.07	95	66537	0.02	0.20	8.38	0.04	-0.01	2.35	-0.10	2.80	13.68
A 001	778.07	779.07	100	DB9901	0.03	0.99	7.91	0.02	-0.01	2.85	-0.10	-0.1	11.59
A 001	779.07	780.07	100	DB9902	0.10	3.15	8.52	0.06	-0.01	3.61	-0.10	-0.1	15.23
A 001	780.07	780.92	85	DB9903	0.44	3.44	9.63	0.03	-0.01	2.81	-0.10	-0.1	16.14
A 001	780.92	781.92	100	DB9904	0.62	3.25	10.58	0.02	-0.01	2.11	-0.10	-0.1	16.37
A 001	781.92	782.48	56	DB9905	0.34	1.78	10.26	0.05	-0.01	4.40	-0.10	-0.1	16.62
A 001	782.48	783.48	100	DB9906	0.25	1.70	12.06	0.07	-0.01	3.21	-0.10	-0.1	17.08
A 001	783.48	784.48	100	DB9907	0.23	1.90	13.75	0.03	-0.01	2.96	-0.10	-0.1	18.66
A 001	784.48	785.48	100	DB9908	1.43	4.30	9.63	0.04	-0.01	1.71	-0.10	-0.1	16.90
A 001	785.48	786.48	100	DB9909	1.70	4.00	10.30	0.03	-0.01	1.46	-0.10	-0.1	17.28
A 001	786.48	787.48	100	DB9910	1.32	3.30	11.43	0.06	-0.01	1.81	-0.10	-0.1	17.73
A 001	787.48	788.28	80	DB9911	1.42	2.50	8.27	0.06	-0.01	2.16	-0.10	-0.1	14.20
A 001	788.28	789.28	100	DB9912	0.24	1.05	10.89	0.02	-0.01	3.16	-0.10	-0.1	15.15
A 001	789.28	790.28	100	DB9913	0.62	1.34	8.48	0.05	-0.01	2.26	-0.10	-0.1	12.54
A 001	790.28	791.28	100	DB9914	0.28	1.34	8.50	0.04	-0.01	2.71	-0.10	-0.1	12.66
A 001	791.28	792.28	100	DB9915	0.27	1.80	7.49	0.04	-0.01	2.39	-0.10	-0.1	11.78
A 001	792.28	793.41	113	DB9916	0.24	1.39	8.09	0.04	-0.01	3.82	-0.10	-0.1	13.37
A 001	793.41	794.20	79	DB9917	1.44	4.60	7.26	0.06	-0.01	2.26	-0.10	-0.1	15.43
A 001	794.20	795.20	100	DB9918	1.01	3.75	6.72	0.10	-0.01	2.56	-0.10	-0.1	13.93
A 001	795.20	796.20	100	DB9919	0.26	3.20	2.75	0.02	-0.01	2.56	-0.10	-0.1	8.58
A 001	796.20	796.66	46	DB9920	0.13	3.10	1.20	0.05	-0.01	6.93	-0.10	-0.1	11.27
A 001	796.66	797.66	100	DB9921	0.04	0.33	1.55	0.02	-0.01	3.41	-0.10	-0.1	5.14

A UMM	RND		SP.GR.	
A TYP	CM		SG	
A MTH	B-B		WEIGH	
A LAB	FLD		FLD	
R ASY	0.00	0.00	RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)	
R ASY	0.00	0.00	RND=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK	
R ASY	0.00	0.00	RND IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE	
R ASY	0.00	0.00	AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED	
R ASY	0.00	0.00	BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100	
R ASY	0.00	0.00	CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT	
R ASY	0.00	0.00	JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN	
R ASY	0.00	0.00	OF EACH FIELD.	
R ASY	0.00	0.00	B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK	
R ASY	0.00	0.00	AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.	
R ASY	0.00	0.00	ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN	
R ASY	0.00	0.00	BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR	
R ASY	0.00	0.00	RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN	
R ASY	0.00	0.00	THE AMTH HEADER.	
R ASY	0.00	0.00	THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,	
R ASY	0.00	0.00	SHOULD BE ENTERED FIRST -- SEE BELOW.	
A 100	0.00	6.10	00	00
R ASY	0.00	6.10	OVERBURDEN	
A 100	6.10	7.92	89	19
A 100	7.92	10.67	208	101
A 100	10.67	11.58	75	17
A 100	11.58	14.63	289	149
A 100	14.63	17.68	249	107
				2.71
A 100	17.68	20.73	252	110
A 100	20.73	23.77	200	22
A 100	23.77	25.30	139	63
A 100	25.30	28.35	279	167
A 100	28.35	29.87	132	50
A 100	29.87	31.70	146	23
A 100	31.70	34.75	292	138
A 100	34.75	35.97	82	00
A 100	35.97	38.71	250	92
A 100	38.71	41.76	297	151
A 100	41.76	43.89	203	24
A 100	43.89	46.94	240	39
				2.63
A 100	46.94	49.99	273	145
A 100	49.99	53.04	273	106
A 100	53.04	57.00	321	137
A 100	57.00	59.74	271	19
A 100	59.74	62.79	280	194
A 100	62.79	64.31	126	31
				2.68
A 100	64.31	67.36	305	231
A 100	67.36	69.19	155	25
A 100	69.19	72.24	261	120
A 100	72.24	75.29	270	213
A 100	75.29	78.33	301	211
A 100	78.33	80.16	159	54
				2.69
A 100	80.16	83.21	295	57
A 100	83.21	86.26	301	241
A 100	86.26	89.31	300	269
A 100	89.31	91.74	216	84
				2.69

G E O L O G

A HMM

A TYP

A MTH

A LAB

A MIN

ROD

CM

R-3

FLD

SP.GR.

SG

WEIGH

FLD

0.02 0.07 6.24 -0.02 -0.01 0.39 -0.10 -0.10 9.49

A 100 91.74 93.84 214

A 100 93.88 96.01 141

A 100 96.01 99.36 335

A 100 99.55 102.61 220

R ASY 102.41 105.46 256 199 2.65

R ASY 99.97 102.01 WEDGE GROOVE.

A 100 102.41 103.94 153

A 100 103.94 105.46 152

A 100 105.46 107.29 170

A 100 107.29 110.34 290

A 100 110.34 113.39 293

A 100 113.39 116.13 224

A 100 116.13 119.13 303

A 100 119.13 122.22 208

A 100 122.22 124.36 140

A 100 124.36 126.80 223

A 100 126.80 128.63 173

A 100 128.63 129.84 111

A 100 129.84 132.89 282

A 100 132.89 135.64 226

A 100 135.64 138.68 280

A 100 138.68 139.90 47

A 100 139.90 142.95 290

A 100 142.95 145.69 233

A 100 145.69 148.74 305

A 100 148.74 151.79 240

A 100 151.79 154.84 297

A 100 154.84 157.89 291

A 100 157.89 160.93 291

A 100 160.93 163.98 284

A 100 163.98 167.03 305

A 100 167.03 170.08 306

A 100 170.08 173.13 290

A 100 173.13 176.17 255

A 100 176.17 179.22 251

A 100 179.22 180.14 88

A 100 180.14 182.27 190

A 100 182.27 185.32 287

A 100 185.32 188.37 279

A 100 188.37 191.11 201

A 100 191.11 194.16 123

A 100 194.16 196.29 117

A 100 196.29 198.90 61

A 100 198.90 199.34 181

A 100 199.34 200.25 32

A 100 200.25 203.30 281

A 100 203.30 206.35 272

A 100 206.35 209.70 278

A 100 209.70 210.62 92

A 100 210.62 213.06 177

A 100 213.06 216.10 258

2.70

2.74

2.83

2.75

A UME				RJD	SP. GR.							
A TYP				CM	SG							
A MTH				B-B	WEIGH							
A LAB				FLD	FLD							
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A 100	216.10	219.15	294	245		2.71						
A 100	219.15	222.20	298	253								
A 100	222.20	225.25	288	80								
A 100	225.25	226.77	106	69								
A 100	226.77	228.30	112	84								
A 100	228.30	231.34	294	220		2.73						
A 100	231.34	234.39	305	289								
A 100	234.39	237.44	300	169								
A 100	237.44	239.88	230	150								
A 100	239.88	240.49	40	00								
A 100	240.49	241.10	56	26								
A 100	241.10	241.40	30	14								
A 100	241.40	243.54	130	69								
A 100	243.54	245.97	204	156		2.79						
A 100	245.97	247.50	153	53								
A 100	247.50	249.63	204	92								
A 100	249.63	251.16	116	09								
A 100	251.16	252.68	139	73		2.70						
A 100	252.68	255.73	285	213								
A 100	255.73	258.78	302	277								
A 100	258.78	261.82	295	245								
A 100	261.82	264.26	194	48								
A 100	264.26	266.40	159	118		2.76						
A 100	266.40	268.53	192	118								
A 100	268.53	271.38	319	234		2.73						
A 100	271.38	275.23	326	268								
A 100	275.23	278.59	290	251								
A 100	278.59	281.64	270	166		2.79						
A 100	281.64	283.46	173	168								
A 100	283.46	286.51	305	326		2.73						
A 100	286.51	289.56	300	202								
A 100	289.56	292.61	277	235								
A 100	292.61	295.66	305	269								
A 100	295.66	298.09	243	279								
A 100	298.09	299.62	000	153								
R ASY	298.09	299.62	WEDGE GROOVE									
A 100	299.62	301.14	152	96		2.75						
A 100	301.14	302.57	108	43								
A 100	302.57	303.89	120	00								
A 100	303.89	306.63	203	33								
A 100	306.63	307.85	117	55		2.71						
A 100	307.85	308.76	91	63								
A 100	308.76	310.29	136	98								
A 100	310.29	313.33	282	213								
A 100	313.33	316.38	294	223								
A 100	316.38	319.43	305	219		2.75						
A 100	319.43	322.48	300	251								
A 100	322.48	325.22	274	283								
A 100	325.22	326.75	153	145								
A 100	326.75	329.79	160	118								
A 100	329.79	331.62	166	153								

				RSD	SP.GR.								
				CM	SG								
				B-B	WEIGH								
A LAB				FLD	FLD								
A MTN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49	
A 100	351.62	354.67	297	197									
A 100	354.67	357.72	295	181									
A 100	357.72	360.77	305	301									
A 100	360.77	363.20	234	93									
A 100	363.20	366.25	305	310		2.75							
A 100	366.25	369.61	327	240									
A 100	369.61	372.96	307	304									
A 100	372.96	376.01	287	106									
A 100	376.01	379.23	117	90									
A 100	379.23	382.05	182	127		2.75							
A 100	382.05	385.10	144	93									
A 100	385.10	388.63	61	00									
A 100	388.63	392.67	304	279									
A 100	392.67	396.03	310	234									
A 100	396.03	399.58	335	289									
A 100	399.58	403.99	57	00									
A 100	403.99	407.60	61	47									
A 100	407.60	411.04	237	226									
A 100	411.04	414.98	243	188		2.77							
A 100	414.98	418.30	180	113									
A 100	418.30	421.13	97	00									
A 100	421.13	424.05	92	43		2.71							
A 100	424.05	427.27	120	37									
A 100	427.27	430.32	284	162									
A 100	430.32	433.57	330	179		2.76							
A 100	433.57	436.41	267	155									
A 100	436.41	439.33	87	17									
A 100	439.33	442.07	250	79									
A 100	442.07	445.29	114	25									
A 100	445.29	448.51	116	60									
A 100	448.51	451.95	204	94									
A 100	451.95	455.99	264	94		2.71							
A 100	455.99	460.91	92	15									
A 100	460.91	465.52	45	00									
A 100	465.52	469.95	186	94									
A 100	469.95	474.70	270	226		2.61							
A 100	474.70	479.05	146	92									
A 100	479.05	483.58	153	91		2.75							
A 100	483.58	488.80	108	40									
A 100	488.80	494.01	111	65									
A 100	494.01	499.76	275	190									
A 100	499.76	505.81	268	178									
A 100	505.81	512.72	91	91									
A 100	512.72	519.35	171	96									
A 100	519.35	526.21	290	263									
A 100	526.21	533.73	00	152		2.73							
R ASY	533.73	540.95	WEDGE GROOVE										
A 100	540.95	548.47	122	105									
A 100	548.47	556.00	152	147									
A 100	556.00	564.00	153	132									
A 100	564.00	571.05	300	286		2.84							

A UMM				ROD	SP.GR.							
A TYP				CR	SG							
A MTH				8-8	WEIGH							
A LAB				FLO	FLO							
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A 100	441.05	444.09	292	138		2.70						
A 100	444.09	447.45	317	241		2.74						
A 100	447.45	450.19	144	88								
A 100	450.19	451.71	145	106		2.70						
A 100	451.71	454.76	260	245		2.78						
A 100	454.76	458.11	324	259								
A 100	458.11	461.47	305	257		2.81						
A 100	461.47	464.52	305	264								
A 100	464.52	465.73	88	40								
A 100	465.73	467.55	183	132								
A 100	467.55	468.17	38	00								
A 100	468.17	471.22	305	238								
A 100	471.22	474.27	305	233								
A 100	474.27	477.62	322	289								
A 100	477.62	480.67	261	169								
A 100	480.67	483.72	305	278								
A 100	483.72	486.77	277	231								
A 100	486.77	487.98	121	70		2.81						
A 100	487.98	490.42	195	75								
A 100	490.42	493.47	290	224								
A 100	493.47	495.60	207	152								
A 100	495.60	496.52	92	50								
A 100	496.52	499.26	274	282								
A 100	499.26	502.31	305	267								
A 100	502.31	505.36	301	264								
A 100	505.36	508.10	274	297								
A 100	508.10	508.71	61	00								
A 100	508.71	509.02	24	24								
A 100	509.02	511.15	87	64								
A 100	511.15	513.89	274	163								
A 100	513.89	516.64	206	149								
A 100	516.64	519.07	224	126								
A 100	519.07	519.68	61	00								
A 100	519.68	520.60	86	11								
A 100	520.60	522.43	183	160								
A 100	522.43	525.48	302	294								
A 100	525.48	528.52	300	252								
A 100	528.52	531.57	281	281								
A 100	531.57	534.62	305	285								
A 100	534.62	537.67	305	298								
A 100	537.67	537.97	25	00		2.73						
A 100	537.97	538.28	31	00								
A 100	538.28	539.19	73	26								
A 100	539.19	539.50	29	00								
A 100	539.50	539.80	20	00								
A 100	539.80	541.63	150	72								
A 100	541.63	543.46	183	171								
A 100	543.46	545.29	183	141								
A 100	545.29	546.81	122	114								
A 100	546.81	549.25	205	194								
A 100	549.25	550.47	106	63								

G E O L O G				CORR		SP. GR.					
A TYP				CM		SG					
A MTH				S-B		WEIGH					
A LAB				FLD		FLD					
A MIP				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10 9.49
A 100	550.47	553.52	296	249							
A 100	555.52	556.56	304	268							
A 100	556.56	557.17	49	12							
A 100	557.17	557.78	61	23							
A 100	557.78	558.39	61	23							
A 100	558.39	559.61	120	45							
A 100	559.61	562.66	305	210							
A 100	562.66	564.49	177	145							
A 100	564.49	567.54	305	248							
A 100	567.54	570.59	305	296							
A 100	570.59	573.63	304	289							
A 100	573.63	576.68	260	177							
A 100	576.68	577.29	49	15							
A 100	577.29	580.03	201	127							
A 100	580.03	581.25	122	47							
A 100	581.25	584.61	302	204							
A 100	584.61	585.22	61	37							
A 100	585.22	586.44	122	34		2.76					
A 100	586.44	587.35	61	54							
A 100	587.35	590.40	280	188							
A 100	590.40	591.01	47	00							
A 100	591.01	591.92	84	38							
A 100	591.92	593.14	122	62							
A 100	593.14	595.27	205	117							
A 100	595.27	595.58	31	31							
A 100	595.58	595.88	26	09							
A 100	595.88	597.71	140	101							
A 100	597.71	599.85	207	97							
A 100	599.85	601.37	121	56							
A 100	601.37	602.59	119	36							
A 100	602.59	603.81	122	34							
A 100	603.81	604.42	61	15							
A 100	604.42	605.94	129	15		2.76					
A 100	605.94	607.77	183	48							
A 100	607.77	608.69	67	13							
A 100	608.69	609.60	74	00							
A 100	609.60	610.51	84	00							
A 100	610.51	612.04	153	129							
A 100	612.04	612.95	75	00		2.79					
A 100	612.95	614.17	120	26		2.80					
A 100	614.17	615.09	92	19							
A 100	615.09	616.61	152	61							
A 100	616.61	617.52	91	43							
A 100	617.52	618.74	122	44							
A 100	618.74	620.57	147	18							
A 100	620.57	621.79	122	27							
A 100	621.79	623.01	122	26		2.80					
A 100	623.01	624.54	153	29							
A 100	624.54	625.45	62	19							
A 100	625.45	628.50	291	179							
A 100	628.50	631.55	305	213		2.82					

A DIAM				R00		SP.GR.						
A TYP				CM		SG						
A MTH				S-R		WEIGH						
A LAB				FLD		FLD						
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A 100	631.55	634.59	301	167								
A 100	634.59	637.64	265	156								
A 100	637.64	640.69	305	291		2.81						
A 100	640.69	643.74	305	190								
A 100	643.74	646.18	228	77								
A 100	646.18	647.70	152	93								
A 100	647.70	650.75	305	222		2.86						
A 100	650.75	652.83	190	99								
A 100	652.83	655.93	305	160								
A 100	655.93	658.98	277	116		4.26						
A 100	658.98	660.81	167	95								
A 100	660.81	662.64	169	41		2.81						
A 100	662.64	663.24	80	00		3.90						
A 100	663.24	664.16	92	13								
A 100	664.16	664.77	45	00								
A 100	664.77	666.60	44	00								
A 100	666.60	667.82	72	00		3.67						
A 100	667.82	669.34	69	00								
A 100	669.34	671.17	06	00								
A 100	671.17	671.55	7	00								
A 100	671.55	672.08	41	19								
A 100	672.08	672.69	61	35								
A 100	672.69	674.22	127	38		2.73						
A 100	674.22	674.83	25	00								
A 100	674.83	675.74	38	00								
A 100	675.74	677.27	103	45								
A 100	677.27	680.31	277	153								
A 100	680.31	683.36	305	235								
A 100	683.36	683.97	42	35		2.70						
A 100	683.97	687.02	299	177								
A 100	687.02	690.07	305	272								
A 100	690.07	690.37	010	000								
A 100	690.37	692.26	158	106								
A 100	692.26	693.12	046	000								
A 100	693.12	694.33	101	040								
A 100	694.33	695.55	117	050		2.69						
A 100	695.55	696.16	61	000								
A 100	696.16	696.77	036	000								
A 100	696.77	697.38	040	000								
A 100	697.38	697.99	031	000								
A 100	697.99	698.60	029	000								
A 100	698.60	698.91	015	000								
A 100	698.91	699.06	012	000								
A 100	699.06	699.82	046	000								
A 100	699.82	701.04	025	000								
A 100	701.04	703.17	201	108								
A 100	703.17	705.31	210	212		2.96						
A 100	705.31	708.36	305	242		2.96						
A 100	708.36	711.40	304	271								
A 100	711.40	714.45	305	250								
A 100	714.45	717.50	305	305								

G E O L O G

A UMa				RQD	SP.GR.						
A TYP				CM	SG						
A MTH				3-B	WEIGH						
A LAB				FLD	FLD						
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10 9.49
A 100	717.50	720.55	305	208							
A 100	720.55	723.60	305	140							
A 100	723.60	726.95	335	264							
A 100	726.95	730.60	305	239	3.45						
A 100	730.60	733.35	335	236							
A 100	733.35	736.70	335	245							
A 100	736.70	739.75	305	300							
A 100	739.75	742.80	305	206							
A 100	742.80	745.85	305	230							
A 100	745.85	748.89	304	246	2.99						
A 100	748.89	751.94	305	171							
A 100	751.94	754.99	305	216							
A 100	754.99	758.04	305	230							
A 100	758.04	761.08	304	241							
A 100	761.08	764.13	305	218							
A 100	764.13	767.18	305	181	2.95						
A 100	767.18	770.23	305	200							
A 100	770.23	773.28	206	279							
A 100	773.28	776.32	290	207							
A 100	776.32	779.07	200	133							
A 100	779.07	782.12	305	225							
A 100	782.12	785.16	304	285							
A 100	785.16	788.51	335	290							
A 100	788.51	788.55	064	000							
A 100	788.55	789.13	058	000	2.92						
A 100	789.13	791.57	244	170							
A 100	791.57	794.61	304	302							
A 100	794.61	797.04	243								
A 100	797.04	797.66	62	94							
A 100	797.66	800.71	305	213							
A 100	800.71	801.32	53	0							
A 100	801.32	803.76	240	135							
A 100	803.76	806.81	285	100							
A 100	806.81	809.85	259	251							
A 100	809.85	811.65	167	111							
A 100	811.65	812.90	119	72							
A 100	812.90	814.43	153	78							
A 100	814.43	816.25	177	86	2.81						
A 100	816.25	819.00	275	130							
A 100	819.00	822.05	298	196							
A 100	822.05	824.79	271	120							
A 100	824.79	827.84	305	223							
A 100	827.84	830.88	284	158							
A 100	830.88	833.93	303	268							
A 100	833.93	836.98	305	199	2.78						
A 100	836.98	837.59	25	20							
A 100	837.59	838.58	91	62							
A 100	838.58	841.55	297	216							
A 100	841.55	844.60	299	246							
A 100	844.60	847.95	302	250							
A 100	847.95	851.31	326	260							

G F O L D G				RED		SP. GR.						
A TYP				CM		SG						
A MTH				R-R		WEIGH						
A LAB				FLD		FLD						
A MIN				0.02	0.07	6.24	-0.02	-0.01	0.39	-0.10	-0.10	9.49
A 100	851.31	854.35	304	310								
A 100	854.35	857.40	305	216								
A 100	857.40	860.45	305	256								
A 100	860.45	863.50	305	204								
A 100	863.50	865.55	138	130								
A 100	865.55	867.77	244	217								
A 100	867.77	870.81	304	209								
A 100	870.81	873.86	305	138								
A 100	873.86	876.91	297	224								
A 100	876.91	879.96	301	265		2.78						
A 100	879.96	883.01	296	222								
A 100	883.01	886.05	295	270								
A 100	886.05	887.88	183	153								
A 100	887.88	891.24	316	265								
A 100	891.24	893.37	213	228								
A 100	893.37	896.72	319	278								
A 100	896.72	899.77	305	260								
A 100	899.77	902.82	305	312								
A 100	902.82	905.87	305	262								
A 100	905.87	909.22	322	189								
A 100	909.22	912.57	312	267		2.78						
A 100	912.57	915.92	325	294								
A 100	915.92	918.97	300	285								
A 100	918.97	922.32	315	246								
A 100	922.32	925.37	305	290								
A 100	925.37	928.73	296	242								
A 100	928.73	931.77	290	233								
A 100	931.77	934.82	287	239								
A 100	934.82	937.87	237	158								
A 100	937.87	940.92	294	270								
A 100	940.92	943.97	296	288		2.84						
A 100	943.97	947.01	277	157								
A 100	947.01	950.06	264	35								
A 100	950.06	952.20	177	0								
A 100	952.20	953.72	69	0								
A 100	953.72	955.85	56	0								
A 100	955.85	957.99	116	0								
A 100	957.99	958.90	72	0								
A 100	958.90	959.51	35	0								
A 100	959.51	961.03	71	0								
A 100	961.03	961.34	12	0								
A 100	961.34	962.86	119	50								
A 100	962.86	963.17	18	0								
A 100	963.17	965.00	124	30								
A 100	965.00	966.22	71	17								
A 100	966.22	968.04	163	126								
A 100	968.04	971.40	279	150								

G E O L O G F O I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAC OCEAN OIL LTD.

JAS 10 RB-ZN-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-00069
TOTAL DEPTH/LENGTH : 1042.72
CORE/HOLE DIAMETER : 8000COLLAR ELEVATION: 1347.38
NORTHING(- IF S): 7002950.00
EASTING (- IF W): 436447.94AZIMUTH(DEG) : 180.00
VERTICAL ANGLE : -80.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : DWH + JER
DATE (YY/MM/DD): 810606
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	25.60	180.00	-79.75
2	40.23	171.00	-78.75
3	76.50	160.00	-77.00
4	110.03	156.00	-76.75
5	137.77	156.00	-76.25
6	152.71	153.00	-75.50
7	167.33	152.00	-75.00
8	175.26	151.00	-74.75
9	181.66	151.00	-74.75
10	188.98	157.00	-73.75
11	204.52	156.00	-73.75
12	237.74	151.00	-73.00
13	268.22	150.00	-72.75
14	299.61	150.00	-71.75
15	308.45	152.00	-71.00
16	326.44	152.00	-69.50
17	343.51	151.00	-68.50
18	356.92	150.00	-68.00
19	371.25	151.00	-66.50
20	399.29	151.00	-62.00
21	435.86	150.50	-59.75
22	466.34	153.00	-58.25
23	500.79	156.00	-56.00
24	517.86	155.00	-55.00
25	539.19	156.00	-54.00
26	568.76	157.00	-53.00
27	598.63	156.00	-52.50
28	626.36	150.00	-51.50
29	661.42	145.00	-51.00
30	694.64	148.00	-51.00
31	726.64	154.00	-51.00
32	755.60	154.00	-50.00

33	789.13	156.00	-48.50
34	815.95	154.00	-47.00
35	851.61	153.00	-42.00
36	886.36	155.00	-37.75
37	918.36	162.00	-34.00
38	949.15	162.00	-31.25
39	980.24	160.00	-30.00
40	1027.48	166.00	-26.00

R HED HQ DRILLED FROM 0.0 M TO 171.90 M, NO DRILLED FROM 171.9 M TO

R HED 604.11 HQ DRILLED FROM 604.11 TO END OF HOLE.

F - INTERVAL -		CORE	T- %	TYPE	JAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY													
K	L	(UNITS = DEC.PLACE)	RECDV-	ROCK	TYING	MIN	TURES	CHARACS		H	H	H	H	ANY	H	H	ANY	ALT	ORE								
E	A	(MT=METRIC FT=FOOTRIC)	ERY	O I	TM	TX	TX	F C % M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-
Y	G	F R O M - T O - I N T (.)	D x	TYPE	1	2	001	1	2	F F C A	1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
K	F	ROCK	FM	RT	TM	002	TX	TX	S C U O	CHT	1	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA			
E	L	QUAL	AGE	FN=	0	LC=	3	3	4	0	2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1	
Y	G	DESIG	VIR	COL				R	C			STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2	

R SVY 184.10 154.10 HOLE WEDGED (RETRIEVABLE) FOR AZIMUTH.

R SVY 303.85 303.85 HOLE WEDGED (RETRIEVABLE) FOR AZIMUTH.

/ 0.00 12.19 12.19 OVER P

/ 12.19 51.82 39.63 ARSI PY SI= LR 0 2 = 2 P 1 V. L+

L 5A

/ FLT 12.19 17.37 5.18 X ARSI GG9 R

L 4A

/ 17.37 17.86 0.49 X ARSI ST1 LM 0 2 1 2 R 1 BD 90

L 5A

/ 17.37 22.85 5.49 X ARSI PY SI= LR 0 2 = 2 R 1 BD 55 V. L+

L 5A

/ 26.82 51.82 25.00 X ARSI PY SI= LR 0 2 = 2 R 1 BD 80 V. L+

L 5A

/ FLT 49.07 49.34 0.27 X ARSI GG9 R

L 6A

/ 51.82 60.42 8.60 BRPM SN2 JL2 P 8.

L 5A JK2

/ 51.82 52.45 0.63 X SAND BD 4 4 4 R 3 BD 70 V* D)

L 6A V.

/ 55.50 57.50 2.00 X SAND R

L 6A

/ FAL 60.42 62.79 2.37 FAUL GG9 P

L 4A

/ 62.79 187.05 124.66 ARSI PY SI= LR 0 2 = 2 P 1 K+ 8*

L 5A

/ 140.82 150.00 9.18 X ARSI GG9 R

L 4A

K	F	F	R	O	N	-	T	O	-	I	N	T	RECOV	MD	%	ROCK	TM	TM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	Q	D	AGE	EV	RD	LC	TM	DM2	TX	TX	S	C	O	U	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R	1015.38	1015.43	CALCAREOUS CEMENT.																											
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Z	1019.50	1025.30	5.80	X	ARST	PY	S12	SS	LR	1	2	3	R	2	BD	40	V-	L*
L																25		

R	1019.50	1025.30	CLEAVAGE AT 45 DEGREES TO BEDDING STRIKE.																											
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Z	SHR	1034.02	1034.17	0.15	X	FAIL							R			>6	>3	D)
L							6A											

A UMM	R00		SP.GR.	
A TYP	CM		SG	
A MTH	B-H		WEIGH	
A LAB	FLD		FLD	
R ASY	0.00	0.00	RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)	
R ASY	0.00	0.00	RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK	
R ASY	0.00	0.00	R00 IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE	
R ASY	0.00	0.00	AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED	
R ASY	0.00	0.00	BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100	
R ASY	0.00	0.00	CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT	
R ASY	0.00	0.00	JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN	
R ASY	0.00	0.00	OF EACH FIELD.	
R ASY	0.00	0.00	B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK	
R ASY	0.00	0.00	AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.	
R ASY	0.00	0.00	ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN	
R ASY	0.00	0.00	BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR	
R ASY	0.00	0.00	RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN	
R ASY	0.00	0.00	THE AMTH HEADER.	
R ASY	0.00	0.00	THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,	
R ASY	0.00	0.00	SHOULD BE ENTERED FIRST -- SEE BELOW.	
A 100	0.00	12.19	00	00
R ASY	0.00	12.19	OVERBURDEN	
A 100	12.19	14.02	151	56
A 100	14.02	15.85	149	22
A 100	15.85	17.37	104	19
A 100	17.37	18.90	115	27
A 100	18.90	20.42	94	00
A 100	20.42	21.64	116	00
A 100	21.64	22.25	61	00
A 100	22.25	22.86	42	00
A 100	22.86	24.38	52	00
A 100	24.38	25.91	70	00
A 100	25.91	26.82	75	00
A 100	26.82	28.04	95	00
A 100	28.04	28.65	57	00
A 100	28.65	30.18	144	00
A 100	30.18	31.70	142	00
A 100	31.70	33.22	136	00

G E O L O G

A UMM

RQD

SP.GR.

A TYP

C₁₀

SG

A MTH

M-H

NEIGH

A LAB

FLO

FLO

A 100 33.22 34.75 130 00

A 100 34.75 35.97 122 33

A 100 35.97 37.19 122 40

A 100 37.19 39.01 100 41

A 100 39.01 40.23 102 30

A 100 40.23 41.15 90 00

A 100 41.15 42.67 110 28

A 100 42.67 44.20 95 00

A 100 44.20 45.11 91 23

A 100 45.11 46.33 122 18

A 100 46.33 47.55 122 20

A 100 47.55 49.07 127 51

A 100 49.07 50.29 118 00

A 100 50.29 51.82 126 00

A 100 51.82 53.34 92 00

A 100 53.34 54.65 94 00

A 100 54.65 56.39 137 00

A 100 56.39 57.30 36 00

A 100 57.30 58.83 102 00

A 100 58.83 60.96 103 00

A 100 60.96 62.79 116 00

A 100 62.79 64.31 95 00

A 100 64.31 66.14 160 00

A 100 66.14 69.19 120 00

A 100 69.19 72.24 92 00

A 100 72.24 74.68 48 00

A 100 74.68 76.20 47 00

A 100 76.20 78.03 104 00

A 100 78.03 79.86 150 18

A 100 79.86 81.69 172 00

A 100 81.69 83.52 183 00

A 100 83.52 85.04 114 00

A 100 85.04 85.65 61 00

A 100 85.65 87.17 110 22

A 100 87.17 88.39 122 00

A 100 88.39 89.61 122 00

A 100 89.61 91.14 125 00

A 100 91.14 92.96 108 19

A 100 92.96 95.71 275 87

A 100 95.71 96.62 84 00

A 100 96.62 98.15 151 00

A 100 98.15 99.67 152 23

A 100 99.67 101.19 134 00

A 100 101.19 102.72 153 00

A 100 102.72 104.85 200 00

A 100 104.85 105.77 68 00

A 100 105.77 107.29 138 00

A 100 107.29 108.20 89 23

A 100 108.20 109.73 48 18

A 100 109.73 111.86 175 29

A 100 111.86 114.69 245 28

A UMM				RJD	SP. GR.
A TYP				CG	SG
A MTH				R-R	WEIGHT
A LAB				FLD	FLD
A 100	114.69	116.74	105	00	
A 100	116.74	119.79	202	00	
A 100	119.79	121.92	178	90	
A 100	121.92	123.75	183	18	
A 100	123.75	124.97	107	21	
A 100	124.97	126.19	99	00	
A 100	126.19	127.71	108	00	
A 100	127.71	128.63	75	00	
A 100	128.63	129.84	100	00	
A 100	129.84	130.76	86	00	
A 100	130.76	131.67	84	00	
A 100	131.67	134.11	50	00	
A 100	134.11	136.25	204	76	
A 100	136.25	139.29	304	99	
A 100	139.29	140.82	120	19	
A 100	140.82	141.73	73	00	
A 100	141.73	142.04	23	00	
A 100	142.04	144.17	213	131	
A 100	144.17	147.22	269	186	
A 100	147.22	150.27	270	164	
A 100	150.27	153.31	304	71	
A 100	153.31	155.45	116	53	
A 100	155.45	157.58	211	49	
A 100	157.58	160.93	329	88	
A 100	160.93	163.98	305	251	
A 100	163.98	165.20	122	97	
A 100	165.20	167.03	172	72	
A 100	167.03	170.08	270	150	
A 100	170.08	171.91	183	47	
A 100	171.91	174.35	230	107	
A 100	174.35	174.96	61	53	
A 100	174.96	175.26	15	00	
A 100	175.26	176.48	71	14	
A 100	176.48	177.70	43	00	
A 100	177.70	178.31	29	00	
A 100	178.31	179.22	91	27	
A 100	179.22	179.83	45	00	
A 100	179.83	180.75	91	26	
A 100	180.75	181.05	30	00	
A 100	181.05	181.66	48	30	
A 100	181.66	182.88	96	63	
A 100	182.88	183.49	44	16	
A 100	183.49	184.10	61	34	
A 100	184.10	185.47	00	137	
K ASY	184.10	185.47	WEDGE GROOVE		
A 100	185.47	185.93	46	26	
A 100	185.93	187.45	46	20	
A 100	187.45	188.06	52	00	
A 100	188.06	188.67	47	00	
A 100	188.67	190.80	79	00	
A 100	190.80	191.11	29	00	

G E O L O G

A UMM

A TYP

A MTH

A LAB

RND

CM

R-B

FLD

SP.GR.

SG

WEIGH

FLD

A 100	191.11	192.63	109	00
A 100	192.63	193.85	111	15
A 100	193.85	194.46	32	00
A 100	194.46	195.68	105	00
A 100	195.68	196.90	36	00
A 100	196.90	199.03	145	45
A 100	199.03	200.25	87	12
A 100	200.25	201.47	89	00
A 100	201.47	202.08	55	00
A 100	202.08	203.00	48	00
A 100	203.00	203.91	69	00
A 100	203.91	206.35	214	00
A 100	206.35	206.96	61	00
A 100	206.96	207.87	19	00
A 100	207.87	208.48	46	00
A 100	208.48	208.79	29	00
A 100	208.79	210.31	000	00
A 100	210.31	210.92	35	00
A 100	210.92	211.53	50	00
A 100	211.53	212.45	30	00
A 100	212.45	212.75	25	00
A 100	212.75	213.66	49	00
A 100	213.66	214.58	71	00
A 100	214.58	215.49	58	00
A 100	215.49	217.02	92	00
A 100	217.02	218.54	130	00
A 100	218.54	220.07	124	18
A 100	220.07	221.89	157	54
A 100	221.89	222.50	57	36
A 100	222.50	223.11	57	00
A 100	223.11	224.33	66	00
A 100	224.33	225.25	80	00
A 100	225.25	226.16	70	00
A 100	226.16	227.03	71	00
A 100	227.03	227.99	00	00
A 100	227.99	228.90	80	00
A 100	228.90	229.21	18	00
A 100	229.21	230.12	00	00
A 100	230.12	230.73	58	00
A 100	230.73	232.26	147	00
A 100	232.26	232.87	56	00
A 100	232.87	234.09	87	00
A 100	234.09	235.00	84	00
A 100	235.00	235.92	66	00
A 100	235.92	236.83	74	00
A 100	236.83	237.74	83	00
A 100	237.74	238.96	72	16
A 100	238.96	240.49	123	00
A 100	240.49	241.40	84	00
A 100	241.40	242.01	61	00
A 100	242.01	243.23	116	00

A DMM				RQD	SP.GR.
A TYP				CR	SG
A MTH				GR-S	WEIGH
A LAB				FLD	FLD
A 100	243.23	244.14	69	00	
A 100	244.14	245.36	116	00	
A 100	245.36	246.58	98	00	
A 100	246.58	247.80	97	00	
A 100	247.80	249.02	96	00	
A 100	249.02	249.94	67	00	
A 100	249.94	250.85	61	00	
A 100	250.85	252.07	98	00	
A 100	252.07	254.20	209	00	
A 100	254.20	255.42	120	00	
A 100	255.42	256.79	124	00	
A 100	256.79	258.17	120	00	
A 100	258.17	258.73	58	00	
A 100	258.73	260.30	126	17	
A 100	260.30	261.21	81	00	
A 100	261.21	263.04	124	00	
A 100	263.04	264.26	71	00	
A 100	264.26	265.18	68	00	
A 100	265.18	265.48	25	00	
A 100	265.48	266.70	20	00	
A 100	266.70	267.61	88	00	
A 100	267.61	268.53	69	00	
A 100	268.53	270.97	220	00	
A 100	270.97	271.58	61	15	
A 100	271.58	271.88	7	00	
A 100	271.88	273.71	122	29	
A 100	273.71	274.62	91	27	
A 100	274.62	276.45	145	14	
A 100	276.45	277.37	91	00	
A 100	277.37	278.59	122	20	
A 100	278.59	280.42	140	06	
A 100	280.42	281.33	91	81	
A 100	281.33	283.46	174	74	
A 100	283.46	286.21	216	71	
A 100	286.21	288.04	152	14	
A 100	288.04	291.08	266	156	
A 100	291.08	294.13	255	249	
A 100	294.13	297.18	271	198	
A 100	297.18	297.48	30	23	
A 100	297.48	300.53	305	270	
A 100	300.53	301.75	107	101	
A 100	301.75	303.89	174	124	
A 100	303.89	305.41	00	00	
A 100	305.41	306.63	80	19	
A 100	306.63	308.15	135	103	
A 100	308.15	309.98	148	128	
A 100	309.98	312.72	217	189	
A 100	312.72	313.33	37	00	
A 100	313.33	314.55	87	19	
A 100	314.55	315.77	110	30	
A 100	315.77	317.91	189	76	

A IMM
A TYP
A MTHRWD
CM
H-RSP.GR.
SG
WEIGH

A LAR

FLD

FLD

A 100	317.91	319.74	183
A 100	319.74	321.56	144
A 100	321.56	322.78	93
A 100	322.78	323.39	61
A 100	323.39	324.31	82
A 100	324.31	325.53	99
A 100	325.53	325.85	21
A 100	325.85	326.57	174
A 100	326.57	329.79	122
A 100	329.79	331.32	100
A 100	331.32	332.23	81
A 100	332.23	333.76	96
A 100	333.76	335.89	211
A 100	335.89	338.94	283
A 100	338.94	341.07	198
A 100	341.07	343.20	191
A 100	343.20	343.81	29
R ASY	343.51	343.81	
A 100	343.81	346.56	275
A 100	346.56	349.00	196
A 100	349.00	350.82	170
A 100	350.82	353.57	275
A 100	353.57	355.70	145
A 100	355.70	359.05	313
A 100	359.05	361.19	214
A 100	361.19	362.71	152
A 100	362.71	364.54	147
A 100	364.54	367.89	302
A 100	367.89	371.25	328
A 100	371.25	373.99	274
A 100	373.99	377.04	293
A 100	377.04	380.09	305
A 100	380.09	381.91	69
A 100	381.91	383.13	108
A 100	383.13	386.18	304
A 100	386.18	387.10	70
A 100	387.10	388.01	86
A 100	388.01	388.62	60
A 100	388.62	389.84	100
A 100	389.84	393.19	304
A 100	393.19	396.54	316
A 100	396.54	396.85	26
A 100	396.85	397.15	00
R ASY	396.85	397.15	
A 100	397.15	398.07	53
A 100	398.07	398.63	00
R ASY	398.07	398.63	
A 100	398.63	400.20	105
A 100	400.20	402.03	183
A 100	402.03	403.25	121
A 100	403.25	404.77	129

GROUND UP BY DRILL.

GROUND1

GROUND2

A UMM				RND	SP. GR.
A TYP				CM	SG
A MTH				R-F	WEIGH
A LAB				FLD	FLD
A 100	404.77	405.69	92	00	
A 100	405.69	407.21	152	99	
A 100	407.21	408.43	109	11	
A 100	408.43	409.04	57	00	
A 100	409.04	409.96	92	00	
A 100	409.96	411.48	135	24	
A 100	411.48	413.92	215	140	
A 100	413.92	416.66	260	180	
A 100	416.66	417.53	54	00	
A 100	417.53	420.01	227	136	
A 100	420.01	422.76	256	209	
A 100	422.76	425.81	268	195	
A 100	425.81	428.55	274	130	
A 100	428.55	430.68	192	109	
A 100	430.68	433.73	305	274	
A 100	433.73	435.56	183	93	
A 100	435.56	438.61	300	221	
A 100	438.61	439.52	91	31	
A 100	439.52	441.35	157	119	
A 100	441.35	443.79	229	112	
A 100	443.79	445.31	152	140	
A 100	445.31	446.53	102	63	
A 100	446.53	448.06	153	106	
A 100	448.06	449.28	95	72	
A 100	449.28	450.19	71	00	
A 100	450.19	450.80	61	12	
A 100	450.80	451.41	58	13	
A 100	451.41	452.32	70	17	
A 100	452.32	454.15	161	122	
A 100	454.15	455.07	92	59	
A 100	455.07	457.81	244	220	
A 100	457.81	460.25	244	196	
A 100	460.25	462.08	147	111	
A 100	462.08	463.30	122	89	
A 100	463.30	466.04	274	222	
A 100	466.04	468.48	198	118	
A 100	468.48	470.00	152	133	
A 100	470.00	472.14	208	146	
A 100	472.14	474.27	206	115	
A 100	474.27	475.13	91	059	
A 100	475.13	476.40	078	013	
A 100	476.40	477.91	61	000	
A 100	477.91	477.93	069	000	
A 100	477.93	479.45	107	036	
A 100	479.45	480.67	090	000	
A 100	480.67	481.23	051	000	
A 100	481.23	481.39	050	000	
A 100	481.39	483.41	124	056	
A 100	483.41	484.33	070	045	
A 100	484.33	486.16	126	071	
A 100	486.16	486.77	060	014	

A UMM A TYP A MTH A LAB				RQD CM R-S FLO	SP.GR. SG WEIGH FLO
A 100	486.77	488.59	166	080	
A 100	488.59	491.93	221	045	
A 100	491.93	492.86	168	121	
A 100	492.86	495.91	278	213	
A 100	495.91	498.35	236	164	
A 100	498.35	500.43	194	064	
A 100	500.43	502.92	244	126	
A 100	502.92	505.05	182	117	
A 100	505.05	508.41	326	274	
A 100	508.41	509.93	149	42	
A 100	509.93	511.45	152	66	
A 100	511.45	513.59	203	137	
A 100	513.59	516.64	305	241	
A 100	516.64	517.55	59	00	
A 100	517.55	518.77	120	24	
A 100	518.77	520.29	119	100	
A 100	520.29	521.82	141	32	
A 100	521.82	524.26	244	91	
A 100	524.26	527.30	296	240	
A 100	527.30	527.91	60	45	
A 100	527.91	530.96	247	120	
A 100	530.96	533.70	248	117	
A 100	533.70	533.86	08	00	
A 100	533.86	534.31	00	00	
R ASY	533.86	534.31	GROUND	11	
A 100	534.31	534.92	44	229	
A 100	534.92	537.67	273	56	
A 100	537.67	539.19	152	00	
A 100	539.19	541.63	187	00	
A 100	541.63	543.76	203	00	
A 100	543.76	546.20	244	105	
A 100	546.20	548.03	161	35	
A 100	548.03	549.55	140	53	
A 100	549.55	551.08	139	18	
A 100	551.08	551.99	76	27	
A 100	551.99	552.30	30	19	
A 100	552.30	552.60	30	31	
A 100	552.60	555.96	316	241	
A 100	555.96	557.48	152	140	
A 100	557.48	560.83	320	301	
A 100	560.83	563.83	305	269	
A 100	563.83	566.62	240	159	
A 100	566.62	569.06	217	71	
A 100	569.06	571.80	260	136	
A 100	571.80	574.85	305	289	
A 100	574.85	577.60	275	178	
A 100	577.60	580.64	304	255	
A 100	580.64	584.00	321	283	
A 100	584.00	587.35	322	264	
A 100	587.35	590.40	305	241	
A 100	590.40	593.75	326	125	

A UMM				RND	SP. GR.
A TYP				CM	SG
A MTH				H-3	WEIGH
A LAB				FLO	FLO
A 100	593.75	594.36	61	67	
A 100	594.36	594.66	23	23	
A 100	594.66	597.71	305	301	
A 100	597.71	601.07	314	223	
A 100	601.07	603.20	172	106	
A 100	603.20	604.11	80	29	
A 100	604.11	605.64	90	87	
A 100	605.64	606.69	291	228	
A 100	606.69	611.73	304	298	
A 100	611.73	614.78	304	304	
A 100	614.78	617.83	298	281	
A 100	617.83	619.96	171	141	
A 100	619.96	622.71	275	240	
A 100	622.71	624.54	154	107	
A 100	624.54	627.89	326	300	
A 100	627.89	629.41	148	98	
A 100	629.41	633.46	314	248	
A 100	633.46	633.68	22	61	
A 100	633.68	634.90	49	00	
A 100	634.90	636.42	140	99	
A 100	636.42	637.03	28	10	
A 100	637.03	640.08	258	191	
A 100	640.08	641.30	94	57	
A 100	641.30	644.35	305	284	
A 100	644.35	645.26	48	34	
A 100	645.26	646.18	62	35	
A 100	646.18	649.22	226	156	
A 100	649.22	650.75	110	86	
A 100	650.75	652.27	97	49	
A 100	652.27	654.41	186	158	
A 100	654.41	657.45	288	239	
A 100	657.45	660.50	238	166	
A 100	660.50	663.55	270	205	
A 100	663.55	666.60	247	158	
A 100	666.60	669.34	208	32	
A 100	669.34	669.95	38	00	
A 100	669.95	671.17	45	11	
A 100	671.17	672.69	45	19	
A 100	672.69	673.00	31	00	
A 100	673.00	673.91	58	00	
A 100	673.91	676.96	214	178	
A 100	676.96	677.27	29	00	
A 100	677.27	679.28	152	91	
A 100	679.28	680.62	87	53	
A 100	680.62	681.84	82	36	
A 100	681.84	682.45	49	00	
A 100	682.45	682.75	15	00	
A 100	682.75	684.58	110	00	
A 100	684.58	685.07	18	00	
A 100	685.07	685.50	16	00	
A 100	685.50	686.29	67	10	

A DMM A TYP A MTH A LAB				RDD CM B-S FLO	SP.GR. SG WEIGH FLO
A 100	685.29	688.85	210	45	
A 100	688.85	690.93	85	10	
A 100	690.93	691.90	40	00	
A 100	691.90	692.20	5	00	
A 100	692.20	693.12	54	14	
A 100	693.12	695.55	195	171	
A 100	695.55	698.60	305	249	
A 100	698.60	699.39	7	00	
A 100	699.39	700.00	57	49	
A 100	700.00	703.05	298	279	
A 100	703.05	706.22	298	246	
A 100	706.22	709.27	294	278	
A 100	709.27	712.32	296	282	
A 100	712.32	715.37	298	291	
A 100	715.37	718.41	304	246	
A 100	718.41	719.02	53	30	
A 100	719.02	721.46	244	213	
A 100	721.46	724.51	291	245	
A 100	724.51	727.56	292	251	
A 100	727.56	730.61	289	156	
A 100	730.61	732.00	139	56	
A 100	732.00	733.65	137	54	
A 100	733.65	736.70	287	212	
A 100	736.70	739.75	298	270	
A 100	739.75	742.80	299	272	
A 100	742.80	744.32	152	128	
A 100	744.32	745.85	151	139	
A 100	745.85	748.89	286	219	
A 100	748.89	751.94	252	107	
A 100	751.94	752.55	61	43	
A 100	752.55	754.99	209	146	
A 100	754.99	756.51	135	38	
A 100	756.51	757.12	59	00	
A 100	757.12	760.17	282	138	
A 100	760.17	763.22	305	202	
A 100	763.22	766.42	312	253	
A 100	766.42	768.55	190	117	
A 100	768.55	770.23	135	48	
A 100	770.23	773.28	296	241	
A 100	773.28	776.33	300	234	
A 100	776.33	779.37	297	192	
A 100	779.37	782.42	292	206	
A 100	782.42	785.47	303	216	
A 100	785.47	788.52	305	267	
A 100	788.52	791.57	297	233	
A 100	791.57	794.61	296	209	
A 100	794.61	797.66	301	253	
A 100	797.66	800.71	296	259	
A 100	800.71	801.01	27	00	
A 100	801.01	803.76	273	239	
A 100	803.76	804.57	61	25	

G E O L O G

JASON PR-7R-AG-8A STF DEPOSIT, V.T.
DRILLHOLE/TRAVERSE --- 81-DH069 --- (CONTINUED)

A UMM	R00			SP.GR.
A TYP	CM			SG
A MTH	H-P			WEIGH
A LAB	FLO			FLO
A 100	804.37	805.24	91	35
A 100	805.28	806.81	130	39
A 100	806.81	808.02	115	55
A 100	808.02	809.09	00	00
A 100	809.09	809.85	76	00
A 100	809.85	810.62	34	00
A 100	810.62	811.68	92	00
A 100	811.68	813.05	130	17
A 100	813.05	814.43	138	22
A 100	814.43	815.80	98	29
A 100	815.80	816.41	61	00
A 100	816.41	817.78	137	36
A 100	817.78	819.00	70	35
A 100	819.00	821.22	219	69
A 100	821.22	821.59	37	25
A 100	821.59	824.79	292	148
A 100	824.79	825.40	55	00
A 100	825.40	826.01	41	00
A 100	826.01	826.47	6	00
A 100	826.47	827.23	9	00
A 100	827.23	828.14	53	11
A 100	828.14	828.45	25	10
A 100	828.45	829.82	73	00
A 100	829.82	830.43	11	00
A 100	830.43	830.58	15	00
A 100	830.58	831.19	08	00
A 100	831.19	831.46	06	00
A 100	831.46	831.49	3	00
A 100	831.49	831.85	05	00
A 100	831.85	832.16	28	17
A 100	832.16	832.23	07	00
A 100	832.23	832.41	05	00
A 100	832.41	832.44	03	00
A 100	832.44	832.59	12	00
A 100	832.59	832.71	8	00
A 100	832.71	832.87	9	00
A 100	832.87	833.20	07	26
A 100	833.20	833.63	43	11
A 100	833.63	834.24	33	18
A 100	834.24	834.54	27	12
A 100	834.54	834.73	14	00
A 100	834.73	834.79	3	00
A 100	834.79	834.88	9	00
A 100	834.88	834.91	3	00
A 100	834.91	835.79	79	13
A 100	835.79	836.68	56	10
A 100	836.68	837.29	33	00
A 100	837.29	837.47	9	00
A 100	837.47	837.74	27	00
A 100	837.74	838.50	74	00
A 100	838.50	839.01	7	00

G E O L O G

A UMM
A TYP
A MTHRND
CM
R-RSP.GR.
SG
WEIGH

A LAB

FLO

FLO

A 100 839.01 839.57 6
A 100 839.57 840.18 8
A 100 840.18 840.79 61
A 100 840.79 841.36 93

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A 100 841.86 842.01 13
A 100 842.01 842.37 10
A 100 842.37 842.52 4
A 100 842.52 842.82 9
A 100 842.82 843.63 23
A 100 843.63 844.30 27

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A 100 844.30 844.45 15
A 100 844.45 844.65 3
A 100 844.65 845.01 7
A 100 845.01 845.16 3
A 100 845.16 845.26 2
A 100 845.26 845.36 3

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A 100 845.36 845.67 4
A 100 845.67 846.12 37
A 100 846.12 846.43 10
A 100 846.43 846.73 17
A 100 846.73 846.81 06
A 100 846.81 846.96 8

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A 100 846.96 847.01 05
A 100 847.01 847.85 72
A 100 847.85 848.03 18
A 100 848.03 849.17 66
A 100 849.17 849.48 31
A 100 849.48 850.39 73

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A 100 850.39 850.85 32
A 100 850.85 851.36 48
A 100 851.36 851.99 28
A 100 851.99 852.27 028
A 100 852.27 852.63 12
A 100 852.63 853.14 51

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A 100 853.14 854.20 104
A 100 854.20 854.96 68
A 100 854.96 856.34 117
A 100 856.34 857.55 104
A 100 857.55 858.16 52
A 100 858.16 859.63 153

18
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45
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13
56

A 100 859.69 861.21 152
A 100 861.21 861.67 33
A 100 861.67 862.89 111
A 100 862.89 864.54 165
A 100 864.54 864.64 10
A 100 864.64 865.94 118

107
22
27
118
00
96

A 100 865.94 867.56 159
A 100 867.56 868.68 94
A 100 868.68 869.14 45
A 100 869.14 870.61 147
A 100 870.61 871.37 76

120
19
09
58
26

A UMM	RQD			SP. GR.
A TYP	CM			SG
A MTH	G-R			WEIGH
A LAB	FLD			FLD
A 100	871.37	872.95	158	86
A 100	872.95	874.57	162	90
A 100	874.57	876.30	165	114
A 100	876.30	877.82	152	88
A 100	877.82	879.50	164	108
A 100	879.50	881.18	164	143
A 100	881.18	882.83	151	78
A 100	882.83	883.92	30	00
A 100	883.92	884.22	30	00
A 100	884.22	884.40	16	00
A 100	884.40	884.65	9	00
A 100	884.65	884.83	20	00
A 100	884.83	886.36	147	39
A 100	886.36	887.43	97	35
A 100	887.43	888.95	151	62
A 100	888.95	890.32	137	92
A 100	890.32	892.00	168	105
A 100	892.00	893.47	136	25
A 100	893.47	894.28	76	58
A 100	894.28	895.69	141	52
A 100	895.69	896.57	75	53
A 100	896.57	897.13	60	00
A 100	897.13	898.70	140	60
A 100	898.70	900.23	149	23
A 100	900.23	901.75	152	67
A 100	901.75	903.43	166	73
A 100	903.43	905.01	158	122
A 100	905.01	906.64	166	125
A 100	906.64	908.38	159	106
A 100	908.38	908.61	23	12
A 100	908.61	910.23	156	85
A 100	910.23	911.81	150	143
A 100	911.81	913.33	151	75
A 100	913.33	915.64	22	00
A 100	915.64	915.16	152	109
A 100	915.16	916.89	168	106
A 100	916.89	917.75	85	35
A 100	917.75	919.51	169	95
A 100	919.51	921.18	164	105
A 100	921.18	923.01	162	139
A 100	923.01	924.00	98	88
A 100	924.00	925.53	144	69
A 100	925.53	927.05	143	74
A 100	927.05	928.60	155	133
A 100	928.60	930.13	144	122
A 100	930.13	931.62	146	77
A 100	931.62	933.25	163	124
A 100	933.25	934.97	167	81
A 100	934.97	936.60	163	88
A 100	936.60	938.12	148	109
A 100	938.12	939.24	100	41

A UMM				RDD	SP.GR.
A TYP				CN	SG
A MTH				R-B	WEIGH
A LAB				FLO	FLO
A 100	939.24	940.77	150	84	
A 100	940.77	942.29	146	70	
A 100	942.29	943.81	149	109	
A 100	943.81	945.34	146	76	
A 100	945.34	946.86	148	55	
A 100	946.86	948.39	153	64	
A 100	948.39	950.11	166	98	
A 100	950.11	951.87	165	61	
A 100	951.87	953.56	149	27	
A 100	953.56	954.53	86	12	
A 100	954.53	955.70	108	00	
A 100	955.70	957.43	167	65	
A 100	957.43	959.05	162	121	
A 100	959.05	960.58	150	103	
A 100	960.58	962.10	152	122	
A 100	962.10	963.65	155	35	
A 100	963.65	965.40	162	129	
A 100	965.40	967.03	163	100	
A 100	967.03	968.73	167	133	
A 100	968.73	969.72	82	66	
A 100	969.72	971.25	150	100	
A 100	971.25	972.77	144	80	
A 100	972.77	974.29	152	104	
A 100	974.29	975.82	149	105	
A 100	975.82	977.01	110	58	
A 100	977.01	977.42	21	00	
A 100	977.42	978.20	78	30	
A 100	978.20	979.93	157	56	
A 100	979.93	981.61	165	48	
A 100	981.61	983.28	167	72	
A 100	983.28	984.96	145	107	
A 100	984.96	986.49	153	134	
A 100	986.49	988.01	149	122	
A 100	988.01	989.53	150	58	
A 100	989.53	991.06	149	117	
A 100	991.06	992.58	152	103	
A 100	992.58	994.26	164	124	
A 100	994.26	995.96	165	115	
A 100	995.96	997.74	166	127	
A 100	997.74	999.36	162	101	
A 100	999.36	1000.20	63	33	
A 100	1000.20	1001.73	144	9	
A 100	1001.73	1001.88	15	00	
A 100	1001.88	1003.25	102	37	
A 100	1003.25	1006.45	290	207	
A 100	1006.45	1009.12	236	183	
A 100	1009.12	1011.86	274	180	
A 100	1011.86	1013.05	119	71	
A 100	1013.05	1013.61	38	9	
A 100	1013.61	1014.07	46	00	
A 100	1014.07	1015.29	63	00	

G E O L O G

JASON PH-7N-AG-BA STF DEPOSIT, Y.T.
DRILLHOLE/TRAVERSE --- 81-DH069 --- (CONTINUED)

A UTM	RDD	SP.GR.
A TYP	CG	SG
A MTH	B-H	WEIGH
A LAB	FLD	FLD

A 100 1015.29 1016.20	91	49
A 100 1016.20 1017.42	114	32
A 100 1017.42 1018.16	54	00
A 100 1018.16 1018.24	4	00
A 100 1018.24 1021.08	251	190
A 100 1021.08 1022.30	122	36
A 100 1022.30 1026.26	359	250
A 100 1026.26 1029.77	351	239
A 100 1029.77 1032.97	302	282
A 100 1032.97 1036.62	321	191
A 100 1036.62 1039.67	305	230
A 100 1039.67 1042.72	305	172

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-RS SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH070
TOTAL DEPTH/LENGTH : 847.65
CORE/HOLE DIAMETER : 43/10COLLAR ELEVATION: 1296.71
NORTHING(- IF S): 7002575.00
EASTING (- IF W): 436528.81AZIMUTH(DEG) : 171.20
VERTICAL ANGLE : -80.10
CO-ORD SYSTEM : UTMGEOLOGGED BY : JWP + BAO
DATE (YY/MM/DD): 810000
PROJECT NUMBER : J-82

SER. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	30.00	165.90	-80.53
2	61.00	168.40	-80.30
3	91.00	172.90	-79.73
4	122.00	168.50	-78.50
5	152.00	166.30	-77.10
6	183.00	165.90	-75.65
7	213.00	160.60	-75.50
8	244.00	158.80	-74.77
9	274.00	156.00	-74.02
10	305.00	152.20	-73.43
11	335.00	150.50	-72.18
12	366.00	149.30	-70.37
13	396.00	149.20	-68.42
14	427.00	150.30	-67.95
15	457.00	154.50	-64.18
16	488.00	160.30	-62.45
17	518.00	160.40	-62.35
18	549.00	159.80	-60.82
19	579.00	159.30	-58.42
20	610.00	163.50	-51.73
21	640.00	170.80	-43.53
22	671.00	170.70	-41.83
23	701.00	171.10	-40.47
24	732.00	171.30	-39.50
25	762.00	171.40	-38.92
26	766.54	170.00	-39.50
27	778.72	170.00	-39.00
28	790.96	170.00	-38.50
29	803.15	170.00	-38.50
30	815.34	170.00	-38.25
31	827.53	170.00	-38.00
32	839.72	170.00	-38.00

F	- I N T E R V A L -	CORE	T- Z	TYPT- GAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE)	RECUV-	M H ROCK	FLYING	HIM	TURES	CHARACS	H H H H H	ANY	H H H	ANY	ALT ORE
F	A (METRIC FT=FOOTRIC)	ERY	D I	TM TM MAT	TX TX F C % M	ARG	/RI T	ID STK DIP	A A A A A	MIN A A A	MIN	- - -
Y	G F R O M - I D - I N T (.)	D X TYPE	1 2 QM1	1 2 F F C A	1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2					
K	F	ROCK	FM RT	16 QM2	1X TX S C O D	CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA				
E	L	QUAL	AGE FM- D LC- 3	3 4 D	/	2	AZM RT H H H H H	H H H H H				1 1
Y	G	DESIG	VIR COL	R	C	STRUCTUR-2	A A A A A	A A A A A				2 2

R	567.14	607.47	ZONES OF CHERT FRAGMENTS SHOWING IRREGULAR CONTACTS WITH ARGL/
R	567.14	607.47	ARSL FRAGMENTS. CHERT ZONES ARE UNSORTED SANDY BRECCIAS WITH

K	F	F	R	D	M	-	T	D	-	I	N	1	RECOV	MD	%	ROCK	TR	TM	Q1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	Q2	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	N	D	AGE	EV	RG	LC	TM	Q2	TX	TX	S	C	D	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

R 773.95 786.62 INTERBEDDED ARG-CHEST CLAST SLUMPS. ARG L WITH LAM FRAMBOIDAL PY
 R 773.95 786.62 BEDS OF CGBR TO 20 CM. SLUMPS WITH >20% CHERT FRAGS HAVE
 R 773.95 786.62 REPLACEMENT BY PY TO 30%.

/ 773.95 776.30 2.35 X ARG L CR BX LM 08)8 R LM 30 V) V. X)

L
 R 773.95 776.30 EUXINIC CONDITIONS IMMEDIATELY PRIOR TO DEBOUCHING OF UPPER
 R 773.95 776.30 SULPHIDE ZONE. Q7-CA VEINS LIKELY TECTONIC TENSION FRACTURES
 R 773.95 776.30 DIFFUSE PY BANDS TO 3 CM.

/ 786.62 792.18 5.56 AKST PY CR 0 3 1 3 P LM 45

L
 R 786.62 792.18 DIFFUSE PY BANDS TO 3 CM, FRAMBOIDAL LAMINAE OF PY. > PY DOWN
 R 786.62 792.18 SECTION.

K US2 792.18 792.18 0.00

/ 792.18 794.24 2.06 BNSX PY GL FR LM P BD 40 V+ L) Q2 Q=
 L L)

R 792.18 794.24 BLENDS AND LAYERS OF COLLIFORM PY, GL REPLACES PY LOCALLY. BOTH
 R 792.18 794.24 CROSSCUT SL-BA LAM. 70% ARGILLITE. HI GL/SL.

/ 794.24 795.25 1.01 BNSX BA SL CH1 LM F9 P LM 60 L4 L) L=
 L GL PY L=

R 794.24 795.25 > GL UPWARDS.

/ 795.25 802.52 7.27 LMSX BA SL CH6 LM P LM 70 L+ L) V)
 L L+

R 795.25 802.52 VERY RHYTHMIC 0.5 TO 2 CM GREY CHERT BEDS INTERBEDDED WITH
 R 795.25 802.52 2-3 CM BANDS OF LAM SL-BA. 2 CH BEDS > DOWNSECTION. 5% Q2
 R 795.25 802.52 TENSION FRACTURES IN CHERT.

/ 802.52 806.70 4.18 BASX GL SL CH3 LM P BD 45 L) Q) Q2
 L L1

R 802.52 806.70 HIGH GRADE ZONE. SL AS CG PATCHES TO 20 CM FG MASSIVE LAM ZONES
 R 802.52 806.70 TO 25 CM, WITH INTERBEDDED RHYTHMIC 1-2 CM GREY CHERT BEDS AND
 R 802.52 806.70 2-5 CM ZONES OF LAM RED SL AND CHERT.

/ 803.13 803.91 0.78 X MSSX GL CH CH2 R Q3 Q3
 L
 R 803.13 803.91 BOTTLED GL-CARBONATE. PROXIMAL VENT TEXTURE.

/ 806.70 807.60 0.90 BNSX BA SL CH1 P BD 40 L2 Q+
 L L1

/ 807.60 808.61 1.01 LMSX SL PY CH6 P BD 50 D) D.
 L L=

R 807.60 808.61 BA-SL LAM 1-4 CM ZONES INTERBEDDED WITH 1-4 CM GREY CHERT BEDS.
 R 807.60 808.61 1% Q2 TENSION FRACTURES IN CHERT WITH FG TOURMALINE WEEDLES &
 R 807.60 808.61 AGGREGATE CLUSTERS.

/ 808.61 809.53 0.92 LMSX BA SL CH5 LM P BD 45 V) L4 L+ D.
 L L+

G E O L O G

A UMM	RQD	SP.GR.
A TYP	CM	SG
A MTH	R-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RQD=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RQD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 R-B=BLOCK-TO-BLOCK (ORILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. R-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE AMTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 0.00 5.49 00 00

R ASY 0.00 5.49 OVERBURDEN

A 100 5.49 6.71 112 69

A 100 6.71 8.23 145 68

A 100 8.23 9.75 152 89

A 100 9.75 11.28 145 20

A 100 11.28 12.80 133 76

A 100 12.80 15.85 217 138

A 100 15.85 18.90 262 152

A 100 18.90 19.81 45 0

A 100 19.81 23.47 250 89

A 100 23.47 26.82 261 158

A 100 26.82 29.87 292 92

A 100 29.87 32.92 291 232

A 100 32.92 35.97 299 169

A 100 35.97 36.58 40 36

A 100 36.58 39.01 243 230

A 100 39.01 42.06 271 169

A UMM				RDD	SP.GR.
A TYP				CM	SG
A MTH				3-R	WEIGH
A LAR				FLO	FLO
A 100	42.06	45.11	258	155	
A 100	45.11	48.16	294	217	
A 100	48.16	51.21	305	170	
A 100	51.21	54.25	296	204	
A 100	54.25	57.30	287	188	
A 100	57.30	60.35	300	240	
A 100	60.35	63.40	279	232	
A 100	63.40	66.14	00	00	
R ASY	63.40	66.14	WEDGE GROOVE		
A 100	66.14	67.97	115	38	
A 100	67.97	70.41	229	114	
A 100	70.41	72.54	200	164	
A 100	72.54	74.57	175	94	
A 100	74.57	76.81	217	138	
A 100	76.81	77.42	61	00	
A 100	77.42	79.25	168	85	
A 100	79.25	81.69	244	170	
A 100	81.69	82.11	42	14	
A 100	82.11	82.60	49	00	
A 100	82.60	84.73	164	131	
A 100	84.73	87.78	258	176	
A 100	87.78	90.83	305	193	
A 100	90.83	93.27	191	129	
A 100	93.27	93.88	61	81	
A 100	93.88	96.62	271	127	
A 100	96.62	99.36	272	178	
A 100	99.36	100.89	117	13	
A 100	100.89	103.02	213	152	
A 100	103.02	105.16	178	97	
A 100	105.16	106.68	152	85	
A 100	106.68	108.51	151	111	
A 100	108.51	109.12	61	59	
A 100	109.12	110.95	169	107	
A 100	110.95	112.17	122	75	
A 100	112.17	115.21	272	94	
A 100	115.21	118.26	305	166	
A 100	118.26	119.79	153	75	
A 100	119.79	121.31	147	106	
A 100	121.31	121.92	61	57	
A 100	121.92	124.36	221	146	
A 100	124.36	125.58	00	00	
R ASY	124.36	125.58	WEDGE GROOVE		
A 100	125.58	127.10	152	114	
A 100	127.10	128.63	143	95	
A 100	128.63	129.84	89	30	
A 100	129.84	130.45	00	00	
R ASY	129.84	130.45	GROUND		
A 100	130.45	132.59	214	232	
A 100	132.59	134.72	177	84	
A 100	134.72	135.94	122	52	
A 100	135.94	137.16	93	00	

A UMM	RQD	SP. GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

A 100	137.15	138.38	122	16
A 100	138.38	139.29	87	39
A 100	139.29	141.12	160	60
A 100	141.12	142.65	138	38
A 100	142.65	143.87	110	45
A 100	143.87	145.69	182	167
A 100	145.69	148.74	305	197
A 100	148.74	151.79	305	246
A 100	151.79	154.84	301	208
A 100	154.84	157.24	223	173
A 100	157.28	158.50	122	38
A 100	158.50	159.11	45	00
A 100	159.11	162.15	284	221
A 100	162.15	163.98	171	132
A 100	163.98	167.03	303	280
A 100	167.03	170.08	305	273
A 100	170.08	173.13	291	211
A 100	173.13	174.96	165	165
A 100	174.96	176.17	120	73
A 100	176.17	179.22	287	186
A 100	179.22	181.66	244	208
A 100	181.66	183.79	203	121
A 100	183.79	185.01	117	65
A 100	185.01	186.84	183	143
A 100	186.84	188.37	137	124
A 100	188.37	189.59	87	39
A 100	189.59	191.41	182	183
A 100	191.41	194.46	305	284
A 100	194.46	197.51	297	278
A 100	197.51	200.56	263	181
A 100	200.56	203.61	305	191
A 100	203.61	205.44	179	179
A 100	205.44	208.48	291	239
A 100	208.48	211.53	305	277
A 100	211.53	213.06	00	153
R ASY	211.53	213.06	WEDGE GROOVE	
A 100	213.06	214.58	152	147
A 100	214.58	216.41	161	118
A 100	216.41	218.85	221	215
A 100	218.85	221.89	304	296
A 100	221.89	224.94	305	289
A 100	224.94	227.99	305	324
A 100	227.99	231.04	305	262
A 100	231.04	234.09	112	305
R ASY	231.04	234.09	WEDGE GROOVE	
A 100	234.09	235.61	137	98
A 100	235.61	237.13	152	139
A 100	237.13	240.18	300	262
A 100	240.18	243.23	305	243
A 100	243.23	246.28	305	195
A 100	246.28	249.63	276	232

G E O L O G

A UMM

A TYP

A MTH

A LAR

RQD

CM

R-B

FLD

SP.GR.

SG

WEIGH

FLD

A 100	249.63	252.68	305	332
A 100	252.68	254.20	151	35
A 100	254.20	256.95	275	114
A 100	256.95	258.17	122	0
A 100	258.17	259.69	152	0
A 100	259.69	261.52	183	65
A 100	261.52	262.74	00	00
R ASY	261.52	262.74	WEDGE GROOVE	
A 100	262.74	264.26	152	153
A 100	264.26	266.09	155	129
A 100	266.09	269.14	296	187
A 100	269.14	269.44	22	22
A 100	269.44	272.49	190	163
A 100	272.49	275.54	305	158
A 100	275.54	278.59	303	251
A 100	278.59	281.64	304	249
A 100	281.64	284.68	294	268
A 100	284.68	287.73	300	294
A 100	287.73	290.78	302	275
A 100	290.78	293.83	305	188
A 100	293.83	296.88	297	282
A 100	296.88	299.92	301	250
R ASY	299.92	301.04	WEDGE REAM	
A 100	301.04	302.67	160	150
A 100	302.67	304.19	140	136
A 100	304.19	306.93	219	188
R ASY	306.93	307.23	GRIND	
A 100	307.23	309.98	242	172
A 100	309.98	311.20	122	00
A 100	311.20	312.12	25	00
A 100	312.12	313.33	121	00
A 100	313.33	313.61	28	00
R ASY	313.61	314.55	GRIND	
A 100	314.55	316.38	176	52
A 100	316.38	319.13	275	39
A 100	319.13	322.17	304	207
A 100	322.17	325.09	91	00
A 100	323.09	325.22	213	146
A 100	325.22	326.75	152	31
A 100	326.75	329.18	226	127
A 100	329.18	330.40	65	21
A 100	330.40	331.01	45	17
A 100	331.01	332.54	78	00
A 100	332.54	333.15	61	18
R ASY	333.15	334.06	GRIND	
A 100	334.06	336.50	122	85
R ASY	336.50	337.41	GRIND	
A 100	337.41	339.55	214	230
A 100	339.55	342.60	288	244
A 100	342.60	345.64	291	200
A 100	345.64	348.69	304	258

A UMM	RED	SP. GR.
A TYP	CM	SG
A MTH	B-F	WEIGH
A LAB	FLD	FLD

A 100	348.69	351.74	280	203
A 100	351.74	352.96	117	35
A 100	352.96	355.70	204	143
A 100	355.70	358.75		
A 100	358.75	361.80	273	229
A 100	361.80	362.10	27	27
A 100	362.10	364.54	220	187
A 100	364.54	367.59	305	268
A 100	367.59	368.20	54	46
A 100	368.20	371.25	267	150
A 100	371.25	372.79	136	83
A 100	372.79	374.60	127	00
A 100	374.60	375.21	36	00
A 100	375.21	376.12	62	31
A 100	376.12	376.73	45	17
A 100	376.73	377.95	107	21
A 100	377.95	379.48	132	51
A 100	379.48	380.70	79	35
A 100	380.70	381.61	57	00
A 100	381.61	382.22	61	00
A 100	382.22	382.83	9	00
A 100	382.83	383.44	46	17
A 100	383.44	383.74	13	00
A 100	383.74	386.79	271	172
A 100	386.79	387.10	30	00
A 100	387.10	390.14	282	224
A 100	390.14	391.36	101	39
A 100	391.36	392.58	97	49
A 100	392.58	395.63	269	194
A 100	395.63	398.07	183	127
A 100	398.07	399.29	89	00
A 100	399.29	400.20	91	41
A 100	400.20	401.12	90	23
A 100	401.12	402.64	108	66
A 100	402.64	403.56	70	24
A 100	403.56	404.16	38	00
A 100	404.16	405.99	140	35
A 100	405.99	406.60	61	75
A 100	406.60	408.13	123	56
A 100	408.13	409.96	140	92
A 100	409.96	412.70	200	193
A 100	412.70	415.75	231	156
A 100	415.75	417.27	84	11
A 100	417.27	418.19	34	00
A 100	418.19	420.01	73	00
A 100	420.01	420.93	75	53
A 100	420.93	421.84	57	00
A 100	421.84	424.59	98	74
A 100	424.59	426.11	81	33
A 100	426.11	427.63	83	00
A 100	427.63	429.16	67	19

A UMM				RDD	SP.GR.
A TYP				CM	SG
A MTH				B-B	WEIGH
A LAB				FLD	FLD
A 100	429.16	430.38	39	00	
A 100	430.38	432.51	134	99	
A 100	432.51	434.34	159	68	
A 100	434.34	436.78	162	134	
A 100	436.78	437.69	42	00	
A 100	437.69	438.91	41	00	
A 100	438.91	440.74	23	00	
A 100	440.74	442.26	94	27	
A 100	442.26	445.31	51	19	
A 100	445.31	447.14	98	94	
A 100	447.14	449.58	193	167	
A 100	449.58	452.63	277	256	
A 100	452.63	455.37	183	146	
A 100	455.37	455.68	13	00	
A 100	455.68	456.59	56	00	
A 100	456.59	457.50	61	42	
A 100	457.50	459.03	101	49	
A 100	459.03	461.16	170	110	
A 100	461.16	463.60	65	12	
A 100	463.60	465.12	95	56	
A 100	465.12	466.34	69	13	
A 100	466.34	467.87	91	00	
A 100	467.87	469.09	82	14	
A 100	469.09	469.70	33	00	
A 100	469.70	470.00	14	00	
A 100	470.00	471.83	135	48	
A 100	471.83	472.44	43	13	
A 100	472.44	474.88	110	00	
A 100	474.88	476.71	88	30	
A 100	476.71	477.01	24	00	
A 100	477.01	477.62	31	00	
A 100	477.62	478.23	20	00	
A 100	478.23	479.15	11	00	
A 100	479.15	480.36	65	00	
A 100	480.36	480.85	7	00	
A 100	480.85	481.28	9	00	
A 100	481.28	483.41	181	88	
A 100	483.41	484.63	00	00	
A 100	484.63	486.00	107	72	
A 100	486.00	487.98	105	00	
A 100	487.98	488.29	29	11	
A 100	488.29	489.51	109	00	
A 100	489.51	490.42	57	13	
A 100	490.42	491.03	58	00	
A 100	491.03	492.56	66	00	
A 100	492.56	493.47	77	00	
A 100	493.47	494.69	104	12	
A 100	494.69	495.91	79	17	
A 100	495.91	496.21	19	00	
A 100	496.21	496.82	13	00	
A 100	496.82	497.74	53	00	

A UMM				RDD	SP.GR.
A TYP				CM	SG
A MTH				R-B	WEIGH
A LAR				FLD	FLD
A 100	497.74	499.26	89	00	
A 100	499.26	499.57	19	00	
A 100	499.57	500.66	35	00	
A 100	500.66	501.77	30	00	
A 100	501.77	502.62	32	00	
A 100	502.62	502.92	26	00	
A 100	502.92	503.22	10	00	
A 100	503.22	504.14	20	00	
A 100	504.14	505.05	46	00	
A 100	505.05	505.66	30	00	
A 100	505.66	507.49	118	18	
A 100	507.49	508.41	35	00	
A 100	508.41	509.02	11	00	
A 100	509.02	510.24	42	00	
A 100	510.24	512.37	118	00	
A 100	512.37	513.89	137	124	
A 100	513.89	515.57	161	00	
A 100	515.57	516.94	102	00	
A 100	516.94	518.46	142	65	
A 100	518.46	519.99	148	62	
A 100	519.99	520.60	38	00	
A 100	520.60	522.12	87	28	
A 100	522.12	523.95	153	00	
A 100	523.95	525.48	142	15	
A 100	525.48	527.00	128	24	
A 100	527.00	528.83	147	00	
A 100	528.83	530.35	132	12	
A 100	530.35	531.57	98	00	
A 100	531.57	533.10	123	13	
A 100	533.10	534.31	78	00	
A 100	534.31	535.53	93	14	
A 100	535.53	537.06	121	24	
A 100	537.06	538.58	130	32	
A 100	538.58	540.11	116	52	
A 100	540.11	541.63	147	32	
A 100	541.63	543.15	137	13	
A 100	543.15	544.68	151	96	
A 100	544.68	546.20	101	00	
A 100	546.20	547.73	143	12	
A 100	547.73	549.55	180	104	
A 100	549.55	550.47	92	00	
A 100	550.47	553.52	292	180	
A 100	553.52	556.56	294	144	
A 100	556.56	559.31	273	109	
A 100	559.31	562.36	285	198	
A 100	562.36	564.49	202	73	
A 100	564.49	567.54	297	217	
A 100	567.54	567.84	27	21	
A 100	567.84	570.89	287	168	
A 100	570.89	573.94	301	159	
A 100	573.94	574.24	30	23	

A UMM				R/D	SP. GR.
A TYP				CM	SG
A MTH				R-R	WEIGH
A LAR				FLD	FLD
A 100	574.24	576.99	270	146	
A 100	576.99	578.82	183	78	
A 100	578.82	581.25	221	127	
A 100	581.25	583.69	223	136	
A 100	583.69	586.74	305	134	
A 100	586.74	588.26	152	00	
A 100	588.26	590.40	208	73	
A 100	590.40	593.45	292	219	
A 100	593.45	596.49	304	191	
A 100	596.49	599.54	267	201	
A 100	599.54	601.98	204	174	
A 100	601.98	602.59	61	62	
A 100	602.59	605.03	194	117	
A 100	605.03	607.47	240	166	
A 100	607.47	610.51	278	160	
A 100	610.51	613.56	272	170	
A 100	613.56	615.09	130	00	
A 100	615.09	618.13	270	96	
A 100	618.13	618.44	24	24	
A 100	618.44	619.66	105	28	
A 100	619.66	623.62	348	126	
A 100	623.62	626.97	282	230	
A 100	626.97	630.02	220	125	
A 100	630.02	633.07	285	152	
A 100	633.07	636.12	301	104	
A 100	636.12	639.17	286	104	
A 100	639.17	639.47	30	00	
A 100	639.47	642.52	268	117	
A 100	642.52	644.35	147	56	
A 100	644.35	645.57	75	56	
A 100	645.57	648.61	271	92	
A 100	648.61	651.66	270	155	
A 100	651.66	655.02	333	207	
A 100	655.02	656.23	00	00	
A 100	656.23	657.76	70	12	
A 100	657.76	659.28	152	52	
A 100	659.28	660.81	143	110	
A 100	660.81	664.16	335	120	
A 100	664.16	667.51	222	124	
A 100	667.51	669.65	191	96	
A 100	669.65	671.78	177	48	
A 100	671.78	675.13	316	187	
A 100	675.13	678.79	343	162	
A 100	678.79	681.23	220	67	
A 100	681.23	682.14	91	16	
A 100	682.14	685.19	303	120	
A 100	685.19	687.93	246	157	
A 100	687.93	691.29	240	179	
A 100	691.29	693.12	178	75	
A 100	693.12	696.77	302	203	
A 100	696.77	699.82	299	113	

A	THM			RQD	SP. GR.
A	TYP			CM	SG
A	MTH			FT	WEIGH
A	LAB			FLD	FLD
A	100	699.82	701.34	149	137
A	100	701.34	704.70	314	155
A	100	704.70	708.05	322	130
A	100	708.05	711.40	318	155
A	100	711.40	715.06	357	246
A	100	715.06	718.11	297	88
A	100	718.11	720.55	224	120
A	100	720.55	722.99	227	36
A	100	722.99	724.81	182	80
A	100	724.81	727.86	299	97
A	100	727.86	728.47	13	00
R	ASY	727.86	728.47	GROUND 60 CM	
A	100	728.47	728.78	23	00
A	100	728.78	732.13	335	109
A	100	732.13	733.35	96	20
A	100	733.35	736.70	323	191
A	100	736.70	740.36	354	227
A	100	740.36	742.49	209	110
A	100	742.49	745.85	319	167
A	100	745.85	749.20	320	203
A	100	749.20	752.55	324	218
A	100	752.55	753.77	118	50
A	100	753.77	757.12	294	113
A	100	757.12	760.78	356	279
A	100	760.78	764.13	325	214
A	100	764.13	767.79	366	258
A	100	767.79	771.14	335	265
A	100	771.14	773.58	232	114
A	100	773.58	776.63	296	181
A	100	776.63	779.68	280	190
A	100	779.68	783.34	351	161
A	100	783.34	785.47	212	177
A	100	785.47	786.99	125	58
A	100	786.99	788.21	100	00
A	100	788.21	788.52	31	00
A	100	788.52	790.35	183	126
A	100	790.35	793.70	307	147
A	100	793.70	797.05	303	183
A	100	797.05	800.40	335	251
A	100	800.40	801.01	61	48
A	100	801.01	804.06	305	241
A	100	804.06	804.67	59	26
A	100	804.67	807.11	241	133
A	100	807.11	810.16	298	230
A	100	810.16	813.21	305	239
A	100	813.21	816.25	288	205
A	100	816.25	819.30	305	259
A	100	819.30	822.35	297	237
A	100	822.35	825.40	293	206
A	100	825.40	828.45	295	198
A	100	828.45	830.28	160	99

A UMM				RDD	SP.GR.
A TYP				CM	SG
A MTH				B-R	WEIGH
A LAR				FLD	FLD

A 100	830.28	832.10	173	110
A 100	832.10	834.54	244	100
A 100	834.54	835.15	55	00
A 100	835.15	836.98	164	29
A 100	836.98	840.33	334	129
A 100	840.33	843.81	136	32
A 100	843.81	846.73	292	242
A 100	846.73	847.65	92	63

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 81-DH071	COLLAR ELEVATION: 1253.00	AZIMUTH(DEG) : 18.00	GEOLOGGED BY : HDG +
TOTAL DEPTH/LENGTH : 108.20	NORTHING(- IF S): 7002550.00	VERTICAL ANGLE : -49.50	DATE (YY/MM/DD): 810613
CORE/HOLE DIAMETER : HU	EASTING (- IF W): 436733.94	CO-ORD SYSTEM :	PROJECT NUMBER : J-MAIN

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	25.60	16.00	-48.25
2	42.67	16.00	-48.00
3	73.15	17.00	-48.25
4	108.20	15.50	-48.00

R HED DRILL HOLE 81-DH071 WAS DIRECTED AT THE MAIN ORE ZONE BETWEEN

R HED 76-DB011 AND 76ADH013, IN ORDER TO OBTAIN ADDITIONAL

R HED INFORMATION ON PB/ZN/BA/AG GRADES. THE ORE INTERSECTION EXTENDED

R HFD FROM 80.36 TO 98.70 METRES, AVERAGING 8.61% ZN, 1.79% PB,

R HED 12.69% FE AND 0.07% BA. THE CENTRE OF THE ORE INTERVAL IS

R HED LOCATED 685 METRES FROM THE ZERO BASELINE AT 1189.3 METRES ABOVE

R HED SEALEVEL. CORE RECOVERY WAS POOR AT 41.5%. BASED ON CORE BEDDING

R HED MEASUREMENTS, THE TRUE THICKNESS OF THE ORE ZONE WAS ESTIMATED

R HED AS 11.5 METRES.

R HED STRATIGRAPHIC CORRELATIONS WERE POSSIBLE USING

R HED THE SANDSTONE MARKER BEDS C, B, A AND D. THE ORE ZONE IS A

R HED SILICATE HOSTED LAMINATED SULPHIDE THAT HAS UNDERGONE MINOR

R HED DEFORMATION AND BRECCIATION DUE TO SOFT SEDIMENT SLUMP.

R SVY 0.00 0.00 ALL SURVEYS DONE WITH THE SPERRY-SUN

/ DVB	0.00	14.16	14.16
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DYER

9

G E O L O G		K F F R O M - T O - I N T R E C O V		M D % R O C K T X T M Q M 1 T X T X F C % M A R G		R I 1 I D A Z M D I P Q Z F L C Y C A B A X X P Y C P G L Y Y A 1 A 2	
E - L -		R O D A G E E V R U L C T M Q M 2 T X T X S C O O C H T		2 I D A Z M D I P M G M U C L S D Q S H A P R M T S L H A			
Y G							

/ CON	14.16	16.02	1.86	BRH4	CR *S*	MD9	P	B*
L				3		KN+		

/ CON	16.02	26.21	10.19	BRH1	CR =C+	F*	MT7	P	FO	35	<(D*
L				5		R*	1	KN2				

/ FLT	26.21	26.59	0.38	FAUL	GG7		P	
L								

K M/C	26.59	26.59	0.00					
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/	26.59	27.24	0.65	SAND CR	SN9 // G: 1 3 9 3	P	2 BD	U25	<(D*
L				8	SI1	8				

/ CON	27.24	29.88	2.64	BRH1 CR		MT8	P	<(R(
L				5		2	KN1		

R 27.24 29.88 PYRITE LAMINATIONS ARE PRESENT WITHIN ARGILLITE CLASTS.

/ CON	29.88	34.82	4.94	ARSI CR	SN1 // LM 1 3 1 3	P	1 LM	81	<(L)
L				2	SI+	8				

R 29.88 34.82 THE LAMINATIONS WITHIN THE ARSI INCREASE IN THICKNESS AND SAND
 R 29.88 34.82 CONTENT AT GREATER DEPTHS. IT IS LIKELY THAT THIS SILT BANDED

R 29.88 34.82 ARGILLITE INTERVAL IS A LARGE CLAST DUE TO THE HIGH BEDDING
 R 29.88 34.82 ANGLE.

K M/B	34.82	34.82	0.00					
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/	34.82	36.47	1.65	SAND	SN9 G: // 0 3) 5 KM)	P	2 BD	U47	<(L*
L				7	SI+	7	JL=			

/ CON	36.47	37.60	1.13	BRH1	SN1 G:	LO4	P	D(
L				7	*C+ F* H*	KM3		

R 36.47 37.60 THERE ARE TWO DISTINCT NORMAL GRADING CYCLES PRESENT IN THIS
 R 36.47 37.60 UNIT.

/	36.70	36.80	0.10	9 SAND	G: BD 0 4 2 5	R	2 BD	U45	D.
L					8				

/	37.32	37.60	0.28	9 ARSE	SN1 G: LM	R	2 LM	U48	D*
L					SI4 //				

/ CON	37.60	38.50	0.90	SAND	SN9 G: 0 5 8 6	P		<.	L(
L				7	SI=	7			

/ CON	38.50	43.70	5.20	CGBR	*S) G:	MR3	P	D*
L				5	*C+ F* H* 2) C LP4			

/ CON	43.70	45.72	2.02	ARSI CR	LM 0 1 0	P	1 LM	40	L)
L				5	2				

/	44.16	44.70	0.54	9 CGBR	*C= F*	LO4	R	R*
L				4	8	LN4		

[illegible]

/ CON	45.72	47.87	2.15	ARGL CX	NX	0	1	1	P	<	B*
L				2		1					

K M/A	47.87	47.87	0.00
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7	47.87	48.98	1.11	SA(0)	G:	3 4 5 6	P	1 BD	40 <)	L(
1				5		2				

CON	48.98	51.21	2.23	CGR	CR	6	MO4	P	D*
					5	3	KM5		

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/ CON      51.21      63.54      12.33      ARSI CR      SI=      0 0 0      P      <      D(
L          2          SN1          1

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/ FLT      S1.21    S4.35    3.14                X ANGL CR      GG4 XX      G O      O      R              D(
|           |         |         |                   |         |         |         |         |         |         |
|           |         |         |                   |         |         |         |         |         |         |

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/	57.75	57.83	0.08	X RIGHT	*C+ G; B*	KL2	R	B*
L				a	R* 5	JK2		

/	58.34	58.63	0.29	X	SAVO	CH	SN7	G	XR	0	3	7	4	R	2	RD	U45	L*
1						5	SI*			2								

R	58.30	58.55	THIS SANDSTONE CONTAINS CARBONACEOUS ARGILLITE WITHIN THE MATRIX
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/	60.66	61.27	0.61	X ARST CR	SN2 G: BD 0 3 3 3	R 2 BD	U40	L*
L				3	ST)	5		

R	60.66	61.27	THE PYRITE OCCURS AS EHDREDAL TO SUBHEDRAL CRYSTALS. USUALLY IT
R	60.65	61.27	IS ASSOCIATED WITH SAND LAYERS.

/	62.70	63.54	0.84	3	RIGHT	FE	LN3	R	B+
L				5		5	JK3		

/	COU	63.54	68.82	5.28		ARGL	STC	FX		P	0	LM	40		D)	
L							STC		LM 2							

/	63.54	64.92	1.38	9	BRHT	SS		MUB	R	<	R*
L					5		3	KM1			

K M/D	65.50	66.50	0.00
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/	56.50	56.45	0.55	x	RRP	SN5	B*	JL=	R	R=
L					5	*C+	R* H* 6	JL2		

R	66.50	66.85	THE PEBBLY MUDSTONE HAS A SANDSTONE MATRIX.
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/	67.25	67.96	0.71	9	RRH1	BR		M07	x	#=
L				5			3	KM1		

R	67.25	67.96	PYRITE IN THE LAST R.R.H.T. APPEARS IN VUGS AS Euhedral, open
R	67.25	67.96	space filling crystals.
R	67.25	67.96	The lower .5 meters of the R.R.H.T. is sheared, indicating a
R	67.25	67.96	possible fault.

CON	93.60	96.04	2.44	SAND	SNB	LP	LC	1383	P	L2	L=
L				7	SI1		4				L3 L1

[illegible]

G E O L O G

A UMM
A TYP
A VTHRQD
CM
B-BSP.GR.
SG
WEIGH

A LAB

FLD

FLD

R ASY	0.00	0.00	RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)		
R ASY	0.00	0.00	RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK		
R ASY	0.00	0.00	RQD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE		
R ASY	0.00	0.00	AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED		
R ASY	0.00	0.00	BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100		
R ASY	0.00	0.00	CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT		
R ASY	0.00	0.00	JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN		
R ASY	0.00	0.00	OF EACH FIELD.		
R ASY	0.00	0.00	B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK		
R ASY	0.00	0.00	AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.		
R ASY	0.00	0.00	ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN		
R ASY	0.00	0.00	BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR		
R ASY	0.00	0.00	RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN		
R ASY	0.00	0.00	THE ANTH HEADER.		
R ASY	0.00	0.00	THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,		
R ASY	0.00	0.00	SHOULD BE ENTERED FIRST -- SEE BELOW.		
A 100	0.00	15.24	00	00	
R ASY	0.00	15.24	OVERBURDEN		
A 100	15.24	16.75	106	00	2.59
A 100	16.75	19.81	209	00	2.52
A 100	19.81	20.42	61	00	
A 100	20.42	22.86	200	00	
A 100	22.86	24.38	135	00	
A 100	24.38	25.91	125	00	
A 100	25.91	27.15	91	00	2.72
A 100	27.15	28.96	127	00	2.30
A 100	28.96	30.18	119	00	2.77
A 100	30.18	30.78	39	00	
A 100	30.78	32.31	153	47	2.79
A 100	32.31	33.22	91	00	
A 100	33.22	34.14	57	00	
A 100	34.14	35.97	163	00	2.62
A 100	35.97	37.80	149	54	2.71
A 100	37.80	40.23	243	69	2.55

G E O L O G				R O D		S P . G R .	
A T Y P				C M		S G	
A M T H				S - R		W E I G H	
A L A B				F L D		F L D	
A 100	40.25	42.37	192	74		2.59	
A 100	42.37	42.67	30	49			
A 100	42.67	43.28	61	23			
A 100	43.28	45.42	214	43		2.51	
A 100	45.42	48.16	191	22		2.51	
A 100	48.16	51.21	86	00			
A 100	51.21	54.25	144	00			
A 100	54.25	56.08	116	00			
A 100	56.08	57.91	144	00			
A 100	57.91	58.83	92	00			
A 100	58.83	60.66	140	00			
A 100	60.66	62.48	137	19			
A 100	62.48	63.40	80	27			
A 100	63.40	64.92	109	00			
A 100	64.92	66.45	148	00			
A 100	66.45	67.97	123	22		2.65	
A 100	67.97	68.28	31	19			
A 100	68.28	70.10	182	69			
A 100	70.10	72.54	244	53		2.68	
A 100	72.54	73.76	114	00			
A 100	73.76	75.59	168	00			
A 100	75.59	77.11	136	00		2.42	
A 100	77.11	78.03	92	00			
A 100	78.03	80.56	114	26			
A 100	80.56	81.12	25	00			
A 100	81.12	82.43	96	00			
A 100	82.43	84.12	33	00			
A 100	84.12	85.44	11	00			
A 100	85.44	91.04	207	00			
A 100	91.04	91.50	25	00			
A 100	91.50	92.05	48	00			
A 100	92.05	93.60	84	00			
A 100	93.60	96.04	62	00			
A 100	96.04	97.10	75	00			
A 100	97.10	98.70	95	00			
A 100	98.70	99.28	54	00			
A 100	99.28	99.55	22	00			
A 100	99.55	100.89	132	00		2.44	
A 100	100.89	102.72	183	25			
A 100	102.72	104.55	179	00			
A 100	104.55	106.07	152	00		2.68	
A 100	106.07	107.29	86	00			
A 100	107.29	108.20	91	00			
R SUM	DRILL HOLE 81-71 WAS DRILLED AT AN AZIMUTH OF 18 DEGREES AND AN						
R SUM	INCLINATION OF -49.5 DEGREES. THERE WAS SUFFICIENT EVIDENCE TO						
R SUM	ESTABLISH THAT STRATIGRAPHIC TOPS ARE TO THE SOUTH, THEREFORE;						
R SUM	DRILLING PROCEEDED THROUGH PROGRESSIVELY OLDER ROCKS. STRATI-						

G E O L O G

JASON Pb-Zn-Ag-Ba STE DEPOSIT, Y.T.
DRILLHOLE/TRVERSE --- 81-DH071 --- (CONTINUED)

R SUM GRAPHIC POSITION, IN RELATION TO THE ORE ZONE, WAS KNOWN THROUGH
R SUM THE CORRELATION OF MARKER BEDS C,B,D, AND O FROM DDH77-21. IT
R SUM WAS THEREFORE POSSIBLE TO ESTABLISH THE DISTANCE TO THE ORE ZONE
R SUM WITH A FAIR DEGREE OF ACCURACY.
R SUM ABOVE THE ORE ZONE, IN THE HANGING WALL THE ROCKS ARE CROSSCUT
R SUM BY QUARTZ AND KALITE MICROVEINS. THE ORE ZONE CONSISTS OF
R SUM SILICEOUS, LAMINATED SULPHIDES. THE LAMINATIONS ARE HIGHLY
R SUM CONVOLUTED AND MILDLY BRECCIATED. A SULPHIDE LAMINATED SILTSTONE
R SUM IS FOUND CONFORMABLY CUTTING THROUGH THE ORE ZONE. THE LACK OF
R SUM FOOTWALL ALTERATION, OR MASSIVE SULPHIDES INDICATES THAT THIS
R SUM ZONE IS DISTALLY LOCATED IN RELATION TO ANY HYDROTHERMAL SOURCE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-7N-AG-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH072	COLLAR ELEVATION: 1253.00	AZIMUTH(DEG) : 18.00	GEOLOGGED BY : HDG +
TOTAL DEPTH/LENGTH : 203.00	NORTHING(- IF S): 7602550.00	VERTICAL ANGLE : -75.00	DATE (YY/MM/DD): 810618
CORE/HOLE DIAMETER : 80	EASTING (- IF N): 436733.94	CO-ORD SYSTEM :	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	33.22	17.00	-74.00
2	48.46	18.00	-74.00
3	63.70	20.00	-73.33
4	78.94	19.00	-73.00
5	94.18	23.00	-72.50
6	109.42	23.00	-72.25
7	124.66	24.00	-72.25
8	139.90	26.00	-72.00
9	155.14	25.00	-72.00
10	170.38	25.00	-72.50
11	185.62	26.00	-73.00
12	200.86	25.00	-73.00

R HED DRILL HOLE 81-DH072 WAS DIRECTED AT THE MAIN ORE ZONE BETWEEN
R HED INTERSECTIONS 77-DH022 AND 78-DH027, IN ORDER TO OBTAIN
R HED SUPPLEMENTARY INFORMATION FOR GRADE AND TONNAGE ESTIMATES.

R HED THE ORE INTERSECTION EXTENDED FROM 162.28 TO 191.81 METRES, WITH
R HED AVERAGE GRADES OF 9.27% ZN, 2.09% PB, 9.85% FE AND 0.05% BA.
R HED CU VALUES WERE BELOW DETECTION LIMITS AND AG WAS LESS THAN

R HED 0.05% OZ. PER TON. THE ORE ZONE INTERSECTION IS 686 METRES FROM
R HED THE ZERO BASELINE AT AN ELEVATION OF 1087 METRES ABOVE SEALEVEL.
R HED BASED ON CORE BEDDING ANGLES, THE TRUE THICKNESS OF THE ORE ZONE
R HED IS ESTIMATED AS BEING 9.0 METRES. CORE RECOVERY IN THE ORE ZONE

R. RED STRATIGRAPHIC CORRELATIONS WERE POSSIBLE USING THE SANDSTONE

MINERAL WAS OBSERVED TO OCCUR WITHIN THE HANGING WALL SEDIMENTS.

K	F	L	(UNITIS = DEC.PLACE)	RECOV-	M M ROCK	TYPI- RAL TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
E	A	(MT=METRIC FT=FOOTRIC)	ERY	O I	TM TM MAT TX TX F C % M ARG	/RI	T ID STK DIP	H H H H H ANY H H H ANY	- - - -	ALT ORE	
Y	G	F R D M - T D - I N T (.)	D Y TYPE	1 2 QM1 1 2 F F C A	1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2				
K	F		ROCK	FM	RT	TM QM2 TX TX S C O O CHT	T ID STK DIP MG MU CL SD QS HA PR MT SL HA				
F	L		DUAL	AGE	EN- Q LC- 3	3 4 U /	2 AZM RT H H H H H H H H	1 1			
Y	G		DESIG	VIR	CUL	R C	STRUCTUR-2 A A A A A A A A	2 2			

R SVY 0.00 0.00 SPERRY-SUP MULTI-SHOT RESULTS.

Z	OV8	0.00	8.84	5.84	OV8P	P
---	-----	------	------	------	------	---

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/ CON      6.84      31.69      22.25      BRHT      *S= G; SC      MQ5      P      FO      75      D)
L          4      *C1 F* F* 2      =      LP3

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/ CON	31.09	36.88	5.79	ANGL GR	FIX	0 1 . 1	P	<.	<*
L				1		9			

/ CON 36.88 40.94 4.06 RRP1 *C= H* KQ3 P
 L 3 H* R* 3 KN1 R)

/ FIT	46.94	25.03	24.09	ANGL CR	GG = 4X	0 3 = 1	P	LM	72	L+
L				J	LM	8				

7	40.94	65.03	24.09	2	3KHT GR	*C)	F*	2	KM1	R	R=
L				1		H*	R*		JM2		

R	40.94	65.03	THIS INTERVAL APPEARS TO BE A CARBONACEOUS ARGILLITE WITH
R	40.94	65.03	INTERCALATED HETEROLITHIC BRECCIA. THE BRECCIA BEDS AVERAGE 20
R	40.94	65.03	CMS IN THICKNESS. THE ALTERNATIVE IS THAT THE WHOLE INTERVAL IS
R	40.94	65.03	A HETEROLITHIC BRECCIA WITH ARGILLITE FRAGMENTS OF 2 METERS IN
R	40.94	65.03	SIZE.

/ CON	65.03	71.30	6.27		RNT	*C=	F*	NIS	P	<.	R)
L					4	R*	5	LOZ			

R	65.03	71.30	THE MAJOR VOLUME OF PYRITE IS FOUND AS LAMINATIONS WITHIN THE
R	65.03	71.30	SILT Banded ARGILLITE FRAGMENTS.

K	M/C	71.30	71.30	0.00
---	-----	-------	-------	------

7	71.40	75.05	3.75	SAND	S88 G; BD	1383	P	2 BD	065	D)
1				5	SH //	8				

72.84	75.05	2.21	3 BRPM	*C= G; H*	KM2	R	D)
			5	R*	KM4		

R	72.84	75.05	THERE ARE FOUR DISTINCT NORMAL GRADED SEQUENCES THAT OCCUR
R	72.84	75.05	WITHIN THE SAND P.G.I. AND GRADE FROM A PEBBLY MUDSTONE WITH
R	72.84	75.05	A SANDSTONE MATRIX.

/	COR	75.95	86.07	11.62		BKPT	CR *C)	Z*		MT7	P	R+
1						3		3		KM1		

[illegible]

/ FAL	151.40	158.30	6.90	BRHT CR	*C= G; F*	MR4	P	<)	<)	R+
L				3	R* R* 2	JN2				
R	151.40	158.30	THE CORE WITHIN THIS INTERVAL IS HIGHLY BROKEN AND SHEARED,							

[illegible]

/	177.21	178.92	1.71	LMSX SF	LM	P	1 LM	78 L5	L1	L1	<	4
L				7							L1	
/	178.92	179.86	0.94	LMSX SF	LM	P	1 LM	78 L5	L1	L1	<	4
L				7							L1	
/	179.86	181.02	1.16	LMSX SF	LM	P	1 LM	78 L5	L1	L1	<	4
L				7							L1	
/	179.86	180.03	0.17	6 MSSX PY	BR MX	R		*3	*=	R5		4
L				4							*)	
/ CON	181.02	183.03	2.01	SILT SF	SI6 BD LC	P	2 BD	72 L1	L1	L1		4
L				3	CH2						L+	
/	183.03	185.03	2.00	SILT SF	SI6 BD LC	P	2 BD	72 L1	L1	L1		4
L				3	CH2						L+	
/	185.03	186.53	1.50	SILT SF	SI6 BD LC	P	2 BD	72 L1	L1	L1		4
L				3	CH2						L+	
/	186.53	188.06	1.53	SILT SF	SI6 BD LC	P	2 BD	72 L1	L1	L1		4
L				3	CH2						L+	
/ CON	188.06	190.20	2.14	SILT SF	SI2 LM LC	P	1 LM	80 L4	L1	L2		4
L				4	CH4						L=	
R	188.06	190.20		SULPHIDES ARE FOUND IN CHERT RICH LAMINATIONS, WHICH INTERBED WITH SILTSTONE LAYERS. THESE CHERTY LAMINATED SULPHIDES ARE FROM								
R	188.06	190.20		5-25 CM IN THICKNESS.								
/ LSX	190.20	191.81	1.61	LMSX	CH8 LC	P	2 LM	30 L8	V+	V=		4
L				7	SI=						L=	
K LM1	191.81	191.81	0.00									
/ CON	191.81	197.96	6.15	SILT CR	MX	P			<	S1		
L				2								
/	193.55	195.99	2.44	X LOST		R						
L												
/	197.96	201.90	3.94	BRHT CR		NR7	P			R1		
L				4		JN1						
/	201.90	202.60	0.70	SAND CR	SN7 MX	P				D=		
L				4								
R	201.90	202.60		CONVULUTED, CARBONACEOUS ARGILLITE INTERFINGERS THE SANDSTONE.								
/	202.60	203.00	0.40	BRPM CR		JK2	P		<*	D=		
L				2		JK1						

R 202.60 203.00 THE PEBBLY MUDSTONE HAS A SANDSTONE MATRIX.

K	F	F	R	D	M	-	T	D	-	T	N	1	RECDV	MD	%	ROCK	TM	TM	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	D	D	AGE	EV	RN	LC	IS	NM2	TX	TX	S	C	D	Q	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R 111.86 112.43 AND BRECCIATION OF THE BRHT UNIT.

/ FLT 112.95 118.86 5.91 ARG L CR SN) SS IM 1 3) 3 P 1 L+
L 5 GG1 9 <)

R 112.95 118.86 SANDSTONE LAMINATIONS WITHIN THE ARG L INCREASE GOING DOWN.

R 112.95 118.86 THE UNIT IS HIGHLY BROKEN UP DUE TO FAULTING.

/ 118.86 127.84 8.98 CGCP SN3 G; LR2 P <) B)
L 6 5 C K04

K M/C 118.86 118.86 0.00

/ 118.86 120.52 1.46 8 SAND SM8 G; BD 2 3 8 5 R 2 BD U52 V+ D)
L 6 GG1 7

/ FLT 121.30 122.50 1.00 X CGCP GG4 G; F* LR2 R <1 B+ D)
L 6 *C+ F* 5 C K04 <+

/ 127.50 127.84 0.34 9 SAND SM9 BD 1 3 9 5 R 2 BD 50 D)
L 6 8

/ 127.84 135.42 7.58 BRHT CR *C+ FD CC L06 P FD 55 B)
L 4 F* 3 K02

R 127.84 135.42 THE ARGILLITE AND CHERT CLASTS ARE SURROUNDED BY A MUDDY MATRIX.

/ 128.55 128.96 0.41 9 SAND SM8 1 3 8 5 R D)
L 6 8

/ 134.41 135.42 1.01 8 CGBR SN2 MP2 R B)
L 6 *C3 F* 6 C KN6

/ 135.42 142.52 7.10 BRHT *S* ND MR7 P *)
L 3 2 * KN1

/ FLT 137.10 137.42 0.32 X BRHT GG7 ND MR7 R D)
L 3 2 * KN1

K M/C 142.52 142.52 0.00

/ 142.52 144.35 1.83 SAND CR GG3 BD 1 3 8 5 P 2 D)
L 8 7

/ 144.35 154.20 9.85 BRHT CR *C+ F* LR8 P L)
L 3 R* 2 K01

R 144.35 154.20 PYRITE OCCURS AS A REPLACEMENT MINERAL IN CHERT CLASTS, AND AS
R 144.35 154.20 LAMINATIONS WITHIN ARSI FRAGMENTS.

/ 151.49 151.67 0.18 9 CGBR SN2 BD G; KL1 R 3 BD U60 R+
L GG+) 7 KN6

R 151.49 151.67 THE CORE IS HIGHLY SHEARED AND CARBONACEOUS INDICATING THE
R 151.49 151.67 POSSIBILITY OF FAULTING.

G F D L O G

A IMM	RDD	SP.GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RCOV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RND=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RDD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE AMTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 3.84 10.36 114 22

A 100 10.36 11.58 112 00

A 100 11.58 12.80 117 60

A 100 12.80 13.72 87 18

A 100 13.72 16.76 290 139 2.62

A 100 16.76 18.90 151 32

A 100 18.90 21.64 267 44

A 100 21.64 24.69 305 78

A 100 24.69 28.04 301 116

A 100 28.04 31.09 305 139

A 100 31.09 31.70 54 00

A 100 31.70 33.53 183 00

A 100 33.53 33.83 30 00 2.54

A 100 33.83 35.66 159 00

A 100 35.66 36.88 116 00 2.73

A 100 36.88 37.49 54 20

A 100 37.49 40.54 305 99

A 100 40.54 43.28 224 21

A UTM				RRD	SP.GR.
A TYP				CM	SG
A MTH				B-B	WEIGH
A LAR				FLO	FLO
A 100	43.28	43.59	27	00	
A 100	43.59	46.63	268	67	
A 100	46.63	47.85	122	00	
A 100	47.85	49.38	110	30	
A 100	49.38	50.29	91	18	2.66
A 100	50.29	50.90	61	00	
A 100	50.90	53.04	184	44	
A 100	53.04	53.95	71	00	
A 100	53.95	54.56	49	00	
A 100	54.56	56.39	151	00	
A 100	56.39	58.22	94	00	
A 100	58.22	59.44	79	00	
A 100	59.44	60.66	97	00	
A 100	60.66	62.18	56	00	
A 100	62.18	63.09	72	00	
A 100	63.09	64.31	96	00	
A 100	64.31	65.53	75	00	
A 100	65.53	67.36	164	43	
A 100	67.36	69.19	181	36	
A 100	69.19	69.80	61	20	2.67
A 100	69.80	72.54	274	21	
A 100	72.54	75.29	258	30	2.63
A 100	75.29	78.03	258	00	
A 100	78.03	79.86	176	45	
A 100	79.86	82.60	268	134	
A 100	82.60	83.21	46	20	
A 100	83.21	85.04	173	00	2.87
A 100	85.04	86.87	183	19	
A 100	86.87	89.92	271	114	2.51
A 100	89.92	92.96	304	138	2.64
A 100	92.96	95.71	275	82	
A 100	95.71	99.06	328	207	
A 100	99.06	102.11	213	91	2.40
A 100	102.11	103.33	122	177	
A 100	103.33	106.38	289	250	
A 100	106.38	109.42	285	115	2.47
A 100	109.42	111.25	176	137	
A 100	111.25	113.69	222	112	2.69
A 100	113.69	115.82	213	88	
A 100	115.82	117.04	95	25	2.57
A 100	117.04	120.40	314	77	
A 100	120.40	122.53	185	28	2.66
A 100	122.53	124.97	240	00	
A 100	124.97	127.41	209	24	
A 100	127.41	128.93	124	00	
A 100	128.93	130.45	152	00	2.15
A 100	130.45	133.50	253	20	
A 100	133.50	134.42	92	44	2.66
A 100	134.42	136.25	171	66	2.75
A 100	136.25	137.46	121	00	
A 100	137.46	138.99	131	00	

A UMM				R00	SP.GR.
A TYP				CM	SG
A MTH				B-B	WEIGH
A LAR				FLD	FLD
A 100	138.99	139.60	49	00	
A 100	139.60	140.82	104	00	
A 100	140.82	141.73	91	00	
A 100	141.73	144.48	257	08	2.69
A 100	144.48	145.69	121	53	
A 100	145.69	148.13	200	20	
A 100	148.13	150.83	275	124	
A 100	150.83	153.92	285	020	
A 100	153.92	155.45	136	000	
A 100	155.45	157.89	190	000	
A 100	157.89	160.91	254	045	
A 100	160.91	162.28	137	000	
A 100	162.28	163.98	101	000	2.39
A 100	163.98	167.03	107	000	2.84
A 100	167.03	168.87	94	000	2.54
A 100	168.87	170.48	42	000	3.20
A 100	170.48	172.76	206	000	2.66
A 100	172.76	175.87	130	000	3.37
A 100	175.87	177.21	132	000	2.80
A 100	177.21	178.92	138	000	1.70
A 100	178.92	181.02	141	000	
A 100	181.02	183.03	180	000	2.68
A 100	183.03	185.03	197	000	
A 100	185.03	186.53	150	000	
A 100	186.53	188.06	140	000	
A 100	188.06	190.20	160	000	2.74
A 100	190.20	191.81	156	000	3.08
A 100	191.81	197.96	272	000	2.84
A 100	197.96	200.25	229	145	
A 100	200.25	202.60	202	72	2.46
A 100	202.60	203.00	40	00	2.32
R SUM	DRILL HOLE 81-72 WAS DRILLED FROM THE SAME SET UP AS DDH81-71.				
R SUM	THE INCLINATION WAS STEEPENED TO -75 DEGREES, AND THE AZIMUTH				
R SUM	MAINTAINED AT 18 DEGREES. THE MARKER UNITS C,B,A,AND D WERE USED				
R SUM	TO LOCATE THE POSITION OF THE DRILL HOLE IN RELATION TO THE ORE				
R SUM	ZONE. OTHER THAN MARKER BEDS, LITHOLOGIC CORRELATIONS BETWEEN				
R SUM	DDH81-71 AND DDH81-72 WERE ONLY FAIR.				
R SUM	AN UNKNOWN BLUE MINERAL WAS FOUND ABOVE THE ORE ZONE IN				
R SUM	DDH81-72 WHICH APPEARS TO CORRESPOND TO A SIMILAR MINERAL FOUND				
R SUM	IN DDH81-75. SAMPLES WERE TAKEN FROM BOTH HOLE FOR IDENTIFICATION				
R SUM	PURPOSES.				

R SUM THE LAMINATED SILTSTONE FOUND WITHIN DDH81-71 ORE ZONE WAS
R SUM ALSO PRESENT IN DDH81-72. THIS BED MAY PROVE TO BE A GOOD MARKER
R SUM HORIZON WITHIN THE MAIN ZONE.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-79-AG-RA STF DEPOSIT, Y.T.

FORMAT VERSION : 6B02

DRILLHOLE/TRAVERSE	: 81-DH073
TOTAL DEPTH/LENGTH	: 24.99
CORE/HOLE DIAMETER	: HQ

COLLAR ELEVATION:	1236.10
NORTHING (- IF S):	7002474.00
EASTING (- IF W):	436718.62

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AZIMUTH( DEG ) :    20.00
VERTICAL ANGLE :   -69.00
CO-ORD SYSTEM :

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GEOLOGGED BY : HDG +
DATE (YY/MM/DD): 810628
PROJECT NUMBER : J-MAIN

SEN. NO OF
SURVEY DATA

LENGTH FROM COLLAR
TO SURVEY POINT

AZIMUTH
(DEG)

VERT. ANGLE
(DEG)

1

17.57

25.00

-65.00

R HED

H1-DH073 WAS DIRECTED AT THE MAIN ZONE, HOWEVER EXTREME

R HED

AZIMUTH DEVIATION FORCED THE ABANDONMENT OF THE HOLE.

[illegible]

Z-DVB	0.00	3.35	3.35
-------	------	------	------

7. CON	3.35	8.50	5.15
--------	------	------	------

/	7.55	7.60	0.05

/	8.50	17.32	8.82
L			

/	17.42	24.99	7.67
L			

Autumn BY R.B.F.

G E O L O G

A ILM	RDD	SP.GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RDD=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RDD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RDD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE ANTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 0.00 2.73 0 0

R ASY 0.00 2.73 OVERBURDEN

A 100 2.73 3.35 61 0

A 100 3.35 3.96 54 0

A 100 3.96 5.49 134 0

A 100 5.49 6.40 59 55

A 100 6.40 8.23 173 94

A 100 8.23 12.50 305 170

A 100 12.50 14.33 183 156

A 100 14.33 17.37 304 222

A 100 17.37 20.42 305 105

A 100 20.42 22.25 173 53

A 100 22.25 24.99 207 144

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAK OCEAN OIL LTD.

JASOR PH-2N-AG-6A STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH074	COLLAR ELEVATION: 1236.10	AZIMUTH(DEG) : 18.00	GEOLOGGED BY : HDG +
TOTAL DEPTH/LENGTH : 274.93	NORTHING(- IF S): 7002473.00	VERTICAL ANGLE : -69.00	DATE (YY/MM/DD): 810628
CORE/HOLE DIAMETER : HQ	EASTING (- IF W): 436718.37	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	29.87	25.00	-63.50
2	44.56	25.00	-61.50
3	59.74	28.00	-60.00
4	74.98	30.00	-59.00
5	90.22	29.00	-59.00
6	105.46	30.00	-58.25
7	120.70	33.50	-58.00
8	135.94	32.00	-57.50
9	151.18	35.00	-56.50
10	166.42	35.00	-56.33
11	181.66	36.00	-56.00
12	196.90	38.00	-56.00
13	212.14	38.00	-54.50
14	227.38	39.50	-51.67
15	242.62	41.00	-51.00
16	257.86	39.50	-51.75
17	273.10	40.00	-51.75

R HED DRILL HOLE 81-DH074 WAS DIRECTED AT THE MAIN ORE ZONE, BENEATH

R HED 81-DH072. THE RESULTS FROM THIS INTERSECTION WOULD BE USED FOR

R HED GRADE AND TONNAGE CALCULATIONS, IN CONNECTION WITH THE MAIN

R HED ZONE.

R HED THE ORE INTERSECTION EXTENDED FROM 243.96 METRES TO 259.38

R HED METRES, WITH AVERAGE GRADES OF 10.45% ZN, 3.18% PB, 8.44% FE AND

R HED 0.05% BA. THE MAJORITY OF CU VALUES WERE BELOW DETECTION LIMITS,

R HED AND AG WAS LESS THAN 0.04% PER TON. THE CENTRE OF THE ORE ZONE

R HED INTERSECTION IS 721 METRES FROM THE ZERO BASELINE AT 1025 METRES

R HED ABOVE SEA LEVEL, BASED ON CORE TO BEDDING ANGLE MEASUREMENTS,

R HED THE TRUE THICKNESS OF THE INTERSECTION WAS ESTIMATED TO BE

R HED 10.0 METRES. CORE RECOVERY WAS CALCULATED AS BEING 69.6%.

R HED STRATIGRAPHIC CORRELATION WAS POSSIBLE WITH MARKER BEDS

R HED D, C, R, A AND O. THE ORE ZONE IS A SILICATE HOSTED, LAMINATED

R HED SULPHIDE WITH MINOR DEFORMATION AND BRECCIATION.

F - INTERVAL - CORE				T- %	TYPI- VAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY																									
K L (UNITS = . DEC.PLACE) RECOV- P M ROCK	RYING MIN	TURES	CHARACS																																	
E A (MT=METRIC FT=FOOTRIC) ERY	O I	IM IM MAT	TX TX F C % M	ARG	/RI	T	ID	STK	DIP	A A A A A	MIN A A A MIN	ALT ORE																								
Y G F R D N - T D - I N T (.)	O X TYPE	1 2 DM1	1 2 F F C A			1	AZM	RT	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A 1 A 2																	
K F	ROCK	FM	RT	TF	DM2	TX	TX	S	C	O	O	CHT	T	ID	STK	DIP	MG	MU	CL	SD	DS	HA	PR	MT	SL	HA										
E L	DUAL	AGE	EN- Q	LC- 3		3	4	0	/				2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	H	H	H	H	H	H	1	1	
Y G	DESIG	VIR	CUL					P	C					STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 SPERRY-SUN MULTI-SHOT RESULTS.

/ OVR 0.00 3.66 3.66 OVER P

/ 3.66 8.23 4.57 BRPM *S* MP6 P D)

/ 6.50 6.80 0.30 X BRPM CR *S* MP6 R D)

/ 7.80 8.10 0.30 X SAND SNX (C 3 3 3 R D.

/ 8.23 20.24 12.01 BRPM CR NR9 P B)

/ 20.24 51.95 31.72 ARSI CR SN1 XB SC 1 3 1 3 P 2 BD 61 L)

/ 51.95 55.47 3.51 BRPM C3 MQ4 P B)

/ 55.47 57.62 2.15 BRHT SN1 G; NQ3 P D)

R 55.47 57.62 THERE IS ONE NORMAL GRADED CYCLE OF CHERT WHICH INDICATES THAT
R 55.47 57.62 STRATIGRAPHIC TOPS ARE UPHOLE. SAND MAKES UP MOST OF THE MATRIX
R 55.47 57.62 BETWEEN CHERT CLASTS.

/ 57.62 59.93 2.31 CGCP *C1 F* NP1 P D)

R 57.62 59.93 THE LARGER CHERT FRAGMENTS ARE WELL ROUNDED WHEREAS THE SMALL
R 57.62 59.93 CHERT CLASTS ARE MORE ANGULAR.

K M/D 57.62 57.62 0.00

/ 57.62 58.29 0.67 9 SAND SN9 G; RD 2 3 9 6 R BD U45 D)

[illegible]

/		59.93	67.29	7.36	BRHT	*S* G;	NS4	P	F0	U55	C)
L					4	*C+ F*	2 *	LP2			
R		59.93	67.29		THE CLASTS ARE SURROUNDED BY A MUDDY MATRIX.						
/		87.29	82.06	14.77	BRPM CR	*S+	MQ4	P			B)
L					3		2 +	JM=			
/		82.06	86.91	4.85	BRPM CR	*S= SS	NP9	P			L+
L					3		3 =				
R		82.06	86.91		THE PYRITE OCCURS WITHIN THE SANDSTONE LAMINATIONS OF THE BRECCIATED ARSI FRAGMENTS.						
/		86.91	88.53	1.62	BRPM	*S= (L	3 6 3 8 LO=	P			D)
L					6		7 + = O LOB				
R		86.91	88.53		CHERT BRECCIA FRAGMENTS ARE SUPPORTED BY A SANDSTONE MATRIX.						
/		88.53	90.61	2.08	BRHT		LQ8	P			D)
L					3		2	LO1			
/		90.61	95.30	4.69	BRHT	*S=	MR4	P	<*		B)
L					4		3 + =	LO2			
/		90.61	91.21	0.60	8 BRPM	SN8	LN1	R			O+
L					6		7	JM3			
R		90.61	91.21		THE MATRIX IS SANDSTONE SUPPORTED.						
/		92.01	92.37	0.36	9 BRPM	SN8	LN=	R			O+
L					6		8	JM2			
R		92.01	92.37		THE MATRIX IS SANDSTONE SUPPORTED.						
/		95.30	101.33	6.03	BRPM	SN6 G;	MP1	P	F0	U50 V)	D+
L					6	*S)	7 *) C LO3				
R		95.30	101.33		THE MATRIX IS SANDSTONE SUPPORTED.						
/		101.33	108.22	6.89	BRHT		MO6	P			R)
L					3		2 *	LO2	V+		
R		101.33	108.22		THE PYRITE OCCURS PREDOMINANTLY IN QUARTZ VEINS AND CHERT CLASTS						
R		101.33	108.22		THE QUARTZ VEINS CUT ACROSS THE ARSI FRAGMENTS AND THE MUDSTONE						
R		101.33	108.22		MATRIX.						
/		108.22	109.87	1.65	BRPM	SN6 G;	KL=	P			D)
L					6	*C+ F* R* 6	0 KN3		<*		
R		108.22	109.87		CHERT BRECCIA FRAGMENTS ARE SUPPORTED BY A SANDSTONE MATRIX.						
/		109.87	112.95	3.08	BRHT		MP7	P			R+
L					4		2	KN1	V+		
/ FLT		111.85	112.43	0.57	X BRHT CR	GG2	MP7	R	<*	R+	C+ B.
L					4		2	KN1	>=		B(
R		111.85	112.43		THE AREA OF FAULTING IS CHARACTERIZED BY SULPHIDE MINERALIZATION						

[illegible]

G F O L O G

K	F	F	R	O	I	T	RECOV	NO	%	ROCK	TM	TM	RM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																					2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				

R 254.51 255.84 THIS HIGHLY CONVOLUTED, MILDLY BRECCIATED LMSX CONTAINS ARGILLITE
 R 254.51 255.84 FRAGMENTS THAT MAY HAVE ORIGINALLY BEEN BEDDED AND LATER
 R 254.51 255.84 DISRUPTED.

/ LSX 255.84 257.76 1.92 LMSX SF BA LM // P 1 LM 40 L5 L2 L1 L+ 8
 L 8 LC SS L2

R 255.84 257.76 ARGILLITE BEDS ARE 5% OF THE TOTAL VOLUME.

/ LSX 257.76 259.33 1.62 LMSX SF PY LM LC P L3 L2 B2 L1 8
 L 4

/ 259.33 260.60 1.22

LOST

P

K LM1 259.96 259.96 0.00

/ 260.60 261.73 1.13

SILT

LM 0 1 8 1

P 1 LM

50 V=

<)

L=

L=

/ 261.73 264.87 3.14

SILT

LM 0 1 8 1

P 1 LM

60 V)

<+

L+

/ 264.87 267.50 2.63

SILT

LC LM 0 1 8 1

P 1 LM

50 L1

<)

L=

R 264.87 267.50 THE SULPHIDE AND QUARTZ LAMINATIONS OCCUR IN DISCRETE 3-5 CM
 R 264.87 267.50 PACKAGES. THE SILTSTONE AND THE LAMINATIONS ARE CONVOLUTED AND
 R 264.87 267.50 MILDLY BRECCIATED.

/ CON 267.50 274.93 7.43

ARGL CR GR ST= LC RW

02=2

P

LM

60 V=

E=

R 267.50 274.93

THIS UNIT IS A CARBONACEOUS ARGL IN WHICH CONVOLUTED INTERVALS
 OF MORE SILICIFIED ARGILLITE ARE BORDERED BY PYRITIC ENVELOPES.
 THESE UNITS ARE LATER CROSSCUT BY SILICIOUS VEINS AND VEINLETS.
 OPEN SPACE FILLING BY QUARTZ AND PYRITE IS ALSO PRESENT. THE
 DISRUPTION OF BEDDING SEEMS TO BE ASSOCIATED WITH THE INTRODUCT-
 ION OF PYRITE AND SILICIFICATION OF THE ARGL.

R 267.50 274.93

R 267.50 274.93

R 267.50 274.93

R 267.50 274.93

R 267.50 274.93

G E O L O G

A UMM	RQD	SP.GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RQDV=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RQD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(10) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE ARTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 0.00 3.66 000 000

R ASY 0.00 3.66 OVERBURDEN

A 100 3.66 5.81 187 46 2.70

A 100 5.81 8.23 242 107

A 100 8.23 11.23 305 172

A 100 11.23 14.33 303 162

A 100 14.33 14.94 61 45

A 100 14.94 17.94 300 291

A 100 17.94 21.34 230 173

A 100 21.34 24.69 335 172 2.70

A 100 24.69 28.04 335 194

A 100 28.04 28.65 61 75

A 100 28.65 30.13 137 69

A 100 30.13 33.22 304 114

A 100 33.22 34.75 152 63

A 100 34.75 35.66 81 20

A 100 35.66 38.17 251 99 2.65

A 100 38.17 41.76 303 51

A UMM				RQD	SP. GR.	
A TYP				CV	SG	
A MTH				B-B	WEIGH	
A LAB				FLO	FLO	
A 100	41.76	44.81	201	122		
A 100	44.81	47.85	304	89	2.73	
A 100	47.85	49.85	124	69		
A 100	49.85	52.43	260	34		
A 100	52.43	55.47	255	77		
A 100	55.47	58.83	295	232	2.76	
A 100	58.83	62.13	313	305		
A 100	62.13	65.52	309	283	2.70	
A 100	65.52	68.53	290	195		
A 100	68.53	71.32	256	225		
A 100	71.32	72.24	92	92		
A 100	72.24	75.29	277	231	2.67	
A 100	75.29	78.33	283	256		
A 100	78.33	81.38	274	208	2.66	
A 100	81.38	84.48	288	236	2.68	
A 100	84.48	86.56	161	70		
A 100	86.56	89.61	255	209	2.66	
A 100	89.61	92.96	282	155	2.70	
A 100	92.96	96.32	217	18		
A 100	96.32	97.54	81	18		
A 100	97.54	99.67	131	87		
A 100	99.67	101.80	126	29		
A 100	101.80	102.72	77	39	2.74	
A 100	102.72	103.94	122	83	2.66	
A 100	103.94	107.29	281	163		
A 100	107.29	110.34	229	115	2.51	
A 100	110.34	111.86	152	16		
A 100	111.86	114.91	191	46	2.72	
A 100	114.91	117.96	138	00	2.73	
A 100	117.96	121.01	158	21		
A 100	121.01	124.05	57	17		
A 100	124.05	126.80	119	88	2.67	
A 100	126.80	128.32	152	66	2.65	
A 100	128.32	130.15	110	33		
A 100	130.15	132.28	152	48		
A 100	132.28	133.20	73	46		
A 100	133.20	136.25	241	137	2.67	
A 100	136.25	139.29	204	93	2.69	
A 100	139.29	142.34	198	76	2.66	
A 100	142.34	145.39	250	71	2.69	
A 100	145.39	146.51	86	17		
A 100	146.51	149.35	193	48		
A 100	149.35	150.57	89	00		
A 100	150.57	151.49	74	00		
A 100	151.49	152.70	88	39		
A 100	152.70	156.06	281	53	2.70	
A 100	156.06	157.58	99	36	2.66	
A 100	157.58	159.41	132	00		
A 100	159.41	160.63	119	00	2.69	
A 100	160.63	162.15	116	00		
A 100	162.15	163.63	83	00		

A UMM	RDD	SP.GR.
A TYP	CM	SG
A MTH	R-H	WEIGH
A LAB	FLD	FLD

A 100	163.68	164.29	41	00	
A 100	164.29	166.73	139	34	
A 100	166.73	168.86	146	23	
A 100	168.86	170.08	62	00	
A 100	170.08	171.30	73	17	2.54
A 100	171.30	172.52	116	31	2.63
A 100	172.52	173.74	89	18	
A 100	173.74	176.78	153	48	
A 100	176.78	177.70	69	00	
A 100	177.70	178.92	21	00	2.71
A 100	178.92	179.53	11	00	
A 100	179.53	180.14	54	17	
A 100	180.14	181.66	112	00	
A 100	181.66	183.18	144	41	
A 100	183.18	184.71	121	76	
A 100	184.71	186.23	114	31	2.41
A 100	186.23	187.76	114	57	
A 100	187.76	189.28	104	47	
A 100	189.28	190.20	59	00	
A 100	190.20	191.41	94	00	
A 100	191.41	192.33	63	18	
A 100	192.33	193.85	108	74	
A 100	193.85	194.77	66	39	
A 100	194.77	195.38	43	21	
A 100	195.38	196.90	98	19	
A 100	196.90	198.42	104	24	
A 100	198.42	199.03	61	00	
A 100	199.03	199.95	39	00	
A 100	199.95	201.17	53	00	
A 100	201.17	202.69	114	00	
A 100	202.69	203.91	70	00	
A 100	203.91	205.44	108	44	2.64
A 100	205.44	206.65	94	51	
A 100	206.65	207.57	44	00	
A 100	207.57	208.48	52	00	
A 100	208.48	209.70	51	00	
A 100	209.70	210.62	38	00	
A 100	210.62	212.14	67	19	
A 100	212.14	213.36	84	43	
A 100	213.36	214.58	88	19	
A 100	214.58	216.10	99	00	
A 100	216.10	217.63	112	36	
A 100	217.63	219.15	121	25	2.64
A 100	219.15	220.68	89	24	
A 100	220.68	222.20	119	21	
A 100	222.20	223.11	84	00	
A 100	223.11	224.33	37	00	
A 100	224.33	225.25	81	13	
A 100	225.25	225.55	30	11	
A 100	225.55	226.77	77	00	
A 100	226.77	227.99	95	28	

A IUM				RDD	SP.GR.
A IYP				CM	SG
A MTH				R-B	WEIGH
A LAB				FLD	FLD
A 100	227.99	229.51	118	21	
A 100	229.51	230.43	50	00	
A 100	230.43	231.34	61	14	
A 100	231.34	232.87	141	51	
A 100	232.87	234.39	86	00	
A 100	234.39	235.92	112	24	
A 100	235.92	237.44	125	00	
A 100	237.44	238.96	120	22	
A 100	238.96	240.32	118	15	2.47
A 100	240.32	241.71	132	00	
A 100	241.71	243.96	225	00	
A 100	243.96	245.63	157	00	
A 100	245.63	247.19	145	00	
A 100	247.19	247.90	70	00	
A 100	247.90	248.66	74	00	
A 100	248.66	250.93	151	00	
A 100	250.93	252.55	152	00	
A 100	252.55	252.98	40	00	
A 100	252.98	254.51	00	00	
A 100	254.51	255.84	69	00	
A 100	255.84	257.76	158	00	
A 100	257.76	259.38	57	00	
A 100	259.38	260.60	00	00	
A 100	260.60	261.73	113	00	
A 100	261.73	264.87	220	00	
A 100	264.87	266.09	89	00	2.90
A 100	266.09	267.00	68	00	
A 100	267.00	268.83	169	00	
A 100	268.83	269.75	59	00	
A 100	269.75	272.19	155	43	
A 100	272.19	273.71	73	00	
A 100	273.71	274.02	20	00	
A 100	274.02	274.50	29	00	
A 100	274.50	274.93	38	00	
R SUM	NORMAL GRADING OF SANDSTONE AND CHERT PARTICLES INDICATES THAT				
R SUM	TOPS ARE IN AN UPHOLE DIRECTION (I.E. SOUTH). MARKER BEDS D,C,B,				
R SUM	A AND G WERE USED TO CORRELATE THE STRATIGRAPHIC POSITION OF				
R SUM	THE DRILL HOLE.				
R SUM	THE SPHALERITE WITHIN THE ORE HORIZON IS COLOURED LIGHT PINK,				
R SUM	CANARY YELLOW AND WHITE, MAKING GRADE ESTIMATES DIFFICULT. THE				
R SUM	MARCASITE AND PYRITE RICH AREAS. SULPHIDE BRECCIATION AND DEFOR-				
R SUM	MATION APPEAR TO RESULT FROM SOFT SEDIMENT SLUMP RELATING TO				
R SUM	MOVEMENT ASSOCIATED WITH HYDROTHERMAL ACTIVITY.				

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-ZH-AG-BA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH075
TOTAL DEPTH/LENGTH : 553.83
CORE/HOLE DIAMETER : 40MMCOLLAR ELEVATION: 1235.54
NORTHING (= IF S): 7002472.00
EASTING (= IF W): 436719.50AZIMUTH(DEG) : 18.00
VERTICAL ANGLE : -82.50
CO-ORD SYSTEM :GEOLOGGED BY : +
DATE (YY/MM/DD): 0
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
---------------------------	---------------------------------------	--------------------	------------------------

1	11.89	18.00	-82.75
2	26.21	20.00	-82.75
3	44.50	29.50	-83.25
4	60.66	34.00	-82.75
5	73.15	41.00	-82.25
6	93.27	56.00	-78.75
7	107.59	60.00	-76.00
8	123.14	61.00	-75.00
9	137.16	62.50	-73.00
10	153.62	63.50	-70.75
11	168.86	64.00	-70.00
12	184.10	64.00	-68.67
13	198.12	65.00	-68.00
14	213.36	62.00	-67.50
15	228.60	64.00	-67.75
16	243.50	63.00	-67.75
17	259.08	62.00	-67.00
18	277.37	63.00	-66.67
19	333.76	64.50	-65.67
20	365.76	63.00	-65.25
21	396.24	66.00	-63.75
22	426.72	64.00	-63.00
23	457.81	64.00	-63.00

F	- I N T E R V A L -	CORE	T- %	TYPI- QUAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC.PLACE) RECDV=	M M ROCK	RYING MIN	TURES	CHARACS		H H H H H	ANY H H H	ANY	ALT	ORE	
E	A (MT=METRIC FT=FOOTRIC) ERY	D J	TR TM MAT	TX TX F C % M	ARG	/RI	T ID STK DIP	A A A A A	MIN A A A	MIN	- - -	- - -
Y	G F R O M - T O - I N T (.)	D X TYPE	1 2 QM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2				
K	F	ROCK	FM	RT	TM QM2	TX TX S C O D CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA				
F	L	QUAL	AGE	EN- D LC- 3	3 4 0	/	2	AZM RT H H H H H H H H	1 1			
Y	G	DESIG	VIR	COL	R	C	STRUCTUR-2	A A A A A A A A A A	2 2			

R SVY 0.00 0.00 SINGLE SHOT RESULTS FROM SPERRY-SUN DIP NOT TURN OUT FOR
R SVY 0.00 0.00 DEPTHS 495.60M., 519.99 M, 544.37 M, AND 550.47 M.

/ DVB 0.00 4.45 4.45 OVER P
L

/ 4.45 19.04 14.59 BRPM *S(CC LR6 P R)
L 4 *C) F* F* 2)) JO=
R 4.45 19.04 PYRITE OCCURS AS A REPLACEMENT MINERAL IN CHERT CLASTS.

R	4.45	19.04	IT ALSO FORMS ALONGATE CONCRETIONS OR NODULES.									
/	19.04	89.61	70.57	BRHM	SS	DD	MR9	P			B9	
L				4								
R	19.04	89.61	PYRITE IS PRESENT IN THE SAND LAYERS OF SILTBANDED ARGILLITE									
R	19.04	89.61	FRAGMENTS.									
/	89.61	91.13	1.52	BRHT	*C)		L07	P			R+	
L				5	F* R* 3		JN1					
R	89.61	91.13	PYRITE OCCURS AS A REPLACEMENT MINERAL WITHIN CHERT FRAGMENTS.									
R	89.61	91.13	CRYSTALS ARE EUBEDRAL TO SUBHEDRAL.									
/	91.13	101.03	9.90	BRHM CR	SS		LR9	P	7		B(
L				3		3						
/	95.93	96.84	0.91	3 BRHM	*C(L07	R	6		R)	
L				3	F* 2		JN1				R(
R	95.93	96.84	SPHALERITE AND PYRITE BOTH APPEAR AS REPLACEMENT MINERAL IN									
R	95.93	96.84	CHERT FRAGMENTS.									
/	97.26	101.03	3.77	9 BRHM CR	*S(SS		K09	R			R)	
L				3		2 (JK)						
R	97.26	101.03	PYRITE ALMOST COMPLETELY REPLACES MOST CHERT FRAGMENTS AND									
R	97.26	101.03	SANDSTONE LAMINATIONS WITHIN ARGILLITE FRAGMENTS.									
/	101.03	108.52	7.49	BRHT CR	*S* G;		L04	P			R)	
L				5	*C+ R* F* 4 *		KP3					
R	101.03	108.52	THE CHERT FRAGMENTS GRADE NORMALLY UPWARDS THE MATRIX CHANGES									
R	101.03	108.52	CHANGES FROM SAND SIZED PARTICLES TO CLAY SIZED.									
K R/D	108.52	108.52	0.00									
/	108.52	113.42	4.90	SAND	*C3 G; RD 1 3 8 5		P	2	U62 V+	**	B)	
L				7	R* F* R						V(
R	108.52	113.42	PYRRHOTITE IS FOUND INFREQUENTLY IN QUARTZ VEINS.									
/	110.53	112.72	2.19	9 CRCP	*C+ G;		LR3	R	V)	**	B)	
L				6	F* R* 5		KN6					
/	113.42	116.95	3.53	CRCP	*C+ F* R*		L01	P	V(F(C)	
L				6		6	KN7					
R	113.42	116.95	PYRITE OCCURS AS BOTH A REPLACEMENT MINERAL IN CHERT FRAGMENTS									
R	113.42	116.95	AND AS A BRECCIA COATING. CALCITE OCCURS AS AN ENVELOPE									
/	116.95	126.80	9.85	BRHT	*C+		MR8	P			R+	
L				3	R* 3		K01			V(B.	
R	116.95	126.80	PYRITE OCCUR AS A REPLACEMENT MINERAL FOR CHERT AND A SELVAGE									
R	116.95	126.80	AROUND ARGILLITE FRAGMENTS.									
/	126.80	137.80	11.00	ARSI	SN1 LC		P	1 LM	22 S.		L)	
L				3	SI+	7						

G E O L O G

K	F	F	R	O	M	-	T	REC'D	MD	%	ROCK	IN	IN	DM	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
E	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																						2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

R 126.80 137.80 THIS UNIT PROBABLY REPRESENTS A LARGE FRAGMENT DUE TO THE SMALL
R 126.80 137.80 BEDDING ANGLE.

/ 137.80 139.29 1.49 BRHT *C) CC MQ6 P R+
L F* R* KP1 R(

R 137.80 139.29 PYRITE PREDOMINATES AS A REPLACEMENT MINERAL IN CHERT FRAGMENTS.
R 137.80 139.29 OCCASIONAL CONCRETIONS OR NODULES OF PYRITE ARE ALSO PRESENT.
R 137.80 139.29 THE MATRIX IS PREDOMINANTLY ARGILLIC.

/ 139.29 150.60 11.31 BRHT *S1 LR8 P **
L MD 1 JK) *

R 139.29 150.60 THE SPHALERITE AND PYRITE BOTH OCCUR AS REPLACEMENT MINERALS IN
R 139.29 150.60 THE CHERT FRAGMENTS. MOST OF THE FRAGMENTS ARE SAND BANDED
R 139.29 150.60 ARGILLITES.

/ 150.60 179.80 29.20 ARST CR SMI BD P 2 BD 65 <) L+
L 3 SI= BR SS 7

R 150.60 179.80 PYRITE OCCURS AS CONCRETIONS, AS WELL AS LAMINATIONS IN THE
R 150.60 179.80 SILT BANDED ARGILLITE. THE CALCITE VEINS ARE ASSOCIATED WITH
R 150.60 179.80 AREAS OF MINOR BRECCIATION.

/ 179.80 183.45 3.65 CGCP *C1 F* LP2 P **
L 6 B* 4 C KP6

R 179.80 183.45 PYRITE OCCURS AS A REPLACEMENT MINERAL IN CHERT FRAGMENTS.

/ 179.80 180.85 1.05 9 BRHT CR *C1 KN5 R **
L 3 B+ F* 2 JM2
R 179.80 180.85 PYRITE OCCURS AS A REPLACEMENT MINERAL IN CHERT.

/ 183.45 190.29 6.84 BRHT CR LS6 P V+ B+
L 4 LN3 V(

/ 186.41 187.09 0.68 9 BRHT *C+ F* LM= R R+
L 6 B* 5 JN2

/ FLT 186.62 190.29 1.67 3 SAND GR G; BD 1 3 8 4 R <= D+
L 5 BR 7

/ 190.29 194.38 4.09 BRHT *C) F* MS6 P V+ **
L 3 P* 3 (KD1 B.

R 190.29 194.38 THE SPHALERITE OCCURS IN QUARTZ VEINS.

/ 194.38 201.25 6.87 BRHT *S+ G; LR2 P **
L 4 *C+ B* F* 4 + C J02 <*

R 194.38 201.25 PYRITE OCCURS AS BOTH A REPLACEMENT MINERAL IN AND AROUND
R 194.38 201.25 CHERT FRAGMENTS. THE MATRIX CONSISTS OF SAND TO SILT SIZED
R 194.38 201.25 PARTICLES.

/ FLT 201.25 203.72 2.47 BRHT GG7 LQ3 P V) B)
L 2 *C+ F* 3 K02

/ 203.72 209.20 5.08 BRHT BR KP8 P B)
L 2 3 JN= V+

[illegible]

[illegible]

Z	CON	300.62	306.65	6.03	ARGL CR	MX	0 0 0	P				D(
L					1		9					
Z		300.62	306.65	6.03	3 BRHT CR	*C+ (L		KM2	P	3		R=
L					3	F* H* B		LN2				
R		300.62	306.65									
R		300.62	306.65									
R	SPC	300.62	306.65									
Z	CON	306.65	312.81	6.16	BRHT	*S+ G;		KR3	P		<)	R+
L					4	*C= F* H* 3	+	L02				
R	SPC	306.65	312.81									
Z	CON	312.81	319.40	6.59	ARSI	SN1 BD //	0 3 1 3		P	1 BD	50	<*
L					4	ST SS 8						>+
R	SPC	312.81	319.40									
Z		313.01	313.12	0.11	9 BRHT			JL1	R			B)
L					3		3	JM2				<+
Z		314.84	315.40	0.56	9 CGCP	GG2 F*		K01	R			**
L					6	*C3	3	C KP6				<)
R	SPC	314.84	315.40									
Z		317.42	317.81	0.39	8 BRHT SF	*C(F*		KL2	R			D+
L					4	H* 3		JK1				>5
R		317.42	317.81									
Z		319.40	325.01	5.61	BRHT			LP3	P			D+
L					5		3	JP2				C)
K	M/B	319.40	319.40	0.00								
Z		319.40	320.87	1.47	8 SAND	SN7 G; BD	0 3 7 6		R	2 BD	U50	D+
L					5	SI1	7					
Z	CON	325.01	332.05	7.04	BRHT CR	*C) BD		LP2	P	2 BD	55	R)
L					1	F* F* 2		JMT				
R		325.01	332.05									
R		325.01	332.05									
R		325.01	332.05									
R		325.01	332.05									
Z	CON	332.05	335.78	3.73	ARGL CR	MX	0 0 0		P			D)
L							9					
Z		335.01	335.78	0.77	4 SAND GR	SN7 FE LC	0 3 7 5		R			D1
L					3		8					
Z	CON	335.78	341.66	5.88	BRHT CR	*C+ R*		L03	P			R=
L					2	R* F*		JN1				

[illegible]

[illegible]

/	488.37	489.75	1.38	2 SILT CL	4X	1	1	1	R	C/	77	<+
L				2A		9						
R	488.37	489.75		SILTSTONE BEDS FROM 1.5 TO 13 CM ARE INTERBEDDED WITHIN THE								

Z	495.50	495.51	0.31	9 SILT CR	S13 LC	1 2 1 3	R 0 LM	69	<)	D*
L				40	Sv1	BR 8				15 1+

K	F	F	R	O	I	I	I	REC	MD	%	ROCK	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2
E	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L
Y	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	

R 495.30 495.61 THIS FINELY LAMINATED SILTSTONE IS EXTREMELY RICH IN FE-SULPHIDES AND PERHAPS SHOULD BE CONSIDERED AS A LAMINATED SULPHIDE. MILD BRECCIATION HAS OCCURRED, RESULTING IN SOME ANGULAR, ARGILLIC CLASTS.

K LM1 497.62 497.62 0.00

/ 497.62 499.00 1.38 SILT CR SI7 LM 1 2 2 2 P 1 LM 70 V= <+ B= <+

R 497.62 499.00 FE-SULPHIDES OCCUR AS SMALL BLEBS, WITHIN SILICATE LENSES, THAT PARALLEL BEDDINGS. QUARTZ VEINS CONTAIN SOME SPHALERITE, AND CROSSBEDDINGS. PYRITE ALSO OCCURS IN 0.4 CM LAMINATIONS WITHIN THE SILTSTONE. LADCASTS WERE OBSERVED BETWEEN THE PYRITE RICH QUARTZ LENSES AND THE SILTSTONE HOST, INDICATING A SYNSEDIMENTARY PERIOD FOR LENSE FORMATION.

/ 499.00 501.00 2.00 SILT CR SI7 LM 1 2 2 2 P 1 LM 75 V= <+

/ 501.00 503.53 2.53 SILT CR SI7 LM 1 2 2 2 P 1 LM 72 V= <+

/ LSX 503.53 504.14 0.61 LSX LC P 1 L2 L1 M3 L3

R 503.53 504.14 HIGHLY CONVOLUTED LAMINATED SULPHIDES ARE INTERCALATED WITH A 7 CM THICK BED OF MASSIVE MARCASITE. THE MASSIVE SULPHIDE IS EXTREMELY VUGGY AND APPEARS TO BE A PRODUCT OF OPEN SPACE FILLING. CARBONACEOUS SILTSTONE BEDS, AVERAGING 1 CM IN THICKNESS, ARE ALSO INTERBEDDED WITHIN THE LAMINATED SULPHIDE AND CONSTITUTE 10% OF THE TOTAL INTERVAL.

/ FLT 504.14 509.45 5.31 SILT CR SI8 LM 1 1 1 P 1 LM 50 <+ <+ D) <)

R 504.14 509.45 THIS INTERVAL IS EXTREMELY BROKEN UP. IT IS LIKELY THAT THE LAMINATED SULPHIDE ABOVE THE SILTSTONE IS PART OF THE MAIN ORE BODY AND HAS BEEN DISPLACED TO ITS PRESENT POSITION BY SUBSEQUENT FAULTING.

/ FLT 509.45 533.40 23.95 ARGILL CR GGI MX 0 0 0 P <+ <+ B)

R 509.45 533.40 THIS UNIT IS HIGHLY BROKEN AND SHEARED. SLICKENSIDE SURFACES ARE OBSERVED WITHIN SHEARED ZONES. PYRITE IS OCCASIONALLY OBSERVED AS THIN .3 CM LAMINATIONS WITHIN THE MASSIVE ARGILLITE.

/ 533.40 553.83 20.43 ARST CR SNI SS XB 0 3 1 3 P 1 BD 070 <+ V)

R 533.40 553.83 THE SANDSTONE LAMINATIONS WITHIN THE ARGILLITE ARE LENSOIDAL AND CROSSBEDDED. OFFSETS ON BEDDING ARE DUE TO SOFT SEDIMENT SLUMP. THIS INTERVAL IS HIGHLY BROKEN, BUT NOT AS BADLY GOUGED AS THE PREVIOUS ARGILLITE (IE 509.45 TO 533.40 M).

A UMM	RDD	SP.GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RECOVER=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RDD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE AMTH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 0.00 4.45 00 00

R ASY 0.00 4.45 OVERBURDEN

A 100 4.45 5.18 73 00

A 100 5.18 7.01 169 80

A 100 7.01 9.45 212 135

A 100 9.45 12.50 276 228

A 100 12.50 12.98 48 28 2.68

A 100 12.98 14.33 123 94

A 100 14.33 17.37 248 185

A 100 17.37 19.51 198 155

A 100 19.51 21.34 169 39

A 100 21.34 24.38 225 139

A 100 24.38 26.21 183 16

A 100 26.21 27.13 81 48

A 100 27.13 28.04 48 30

A 100 28.04 31.09 296 250

A 100 31.09 32.51 149 84

A 100 32.51 34.75 186 165

A UMM				900	SP.GR.
A TYP				CM	SG
A MTH				8-8	WEIGH
A LAB				FLD	FLD
A 100	54.75	58.10	502	226	
A 100	58.10	58.71	61	47	
A 100	58.71	42.06	318	206	
A 100	42.06	42.67	59	00	
A 100	42.67	46.02	332	169	
A 100	46.02	49.38	318	221	
A 100	49.38	51.82	244	131	
A 100	51.82	54.56	272	116	
A 100	54.56	55.17	61	000	
A 100	55.17	58.22	305	160	
A 100	58.22	61.57	304	204	
A 100	61.57	64.01	227	80	
A 100	64.01	67.36	313	212	
A 100	67.36	69.49	209	91	
A 100	69.49	71.63	198	85	
A 100	71.63	72.24	48	20	
A 100	72.24	74.98	264	80	
A 100	74.98	78.21	293	46	
A 100	78.21	83.21	500	134	
A 100	83.21	86.44	312	105	
A 100	86.44	87.17	61	00	
A 100	87.17	87.78	58	21	
A 100	87.78	89.61	145	46	
A 100	89.61	92.96	294	69	2.68
A 100	92.96	96.32	302	130	
A 100	96.32	99.36	304	137	
A 100	99.36	102.41	305	162	2.55
A 100	102.41	105.77	292	216	
A 100	105.77	108.81	255	127	2.67
A 100	108.81	111.86	305	159	2.44
A 100	111.86	114.91	305	200	2.71
A 100	114.91	117.96	298	174	
A 100	117.96	121.01	293	130	2.67
A 100	121.01	124.05	304	150	
A 100	124.05	127.10	197	97	2.71
A 100	127.10	130.15	301	212	
A 100	130.15	133.20	305	100	
A 100	133.20	136.25	303	151	
A 100	136.25	139.29	292	162	2.68
A 100	139.29	142.34	297	201	
A 100	142.34	145.39	305	182	2.67
A 100	145.39	148.44	294	181	
A 100	148.44	151.49	282	89	
A 100	151.49	154.53	297	186	
A 100	154.53	157.58	300	93	2.75
A 100	157.58	160.63	258	125	
A 100	160.63	163.68	302	96	
A 100	163.68	166.73	278	118	
A 100	166.73	169.77	303	167	
A 100	169.77	172.82	292	164	
A 100	172.82	175.87	283	00	

G E O L O G				R O D		S P . G R .	
A T Y P				C M		S G	
A M T H				B - 3		W E I G H	
A L A R				F L D		F L D	
A 100	175.87	178.00	213	00			
A 100	178.00	178.92	92	00			
A 100	178.92	180.75	150	00			
A 100	180.75	183.79	284	95		2.59	
A 100	183.79	185.01	117	24			
A 100	185.01	188.06	288	75			
A 100	188.06	189.89	180	19			
A 100	189.89	193.24	507	00		2.67	
A 100	193.24	195.99	275	00			
A 100	195.99	199.03	296	136		2.68	
A 100	199.03	200.25	110	17			
A 100	200.25	203.30	298	51		2.55	
A 100	203.30	204.52	105	00			
A 100	204.52	205.74	102	00			
A 100	205.74	206.35	55	00		2.65	
A 100	206.35	207.89	107	00			
A 100	207.89	209.40	113	00			
A 100	209.40	211.53	120	00			
A 100	211.53	213.97	235	00			
A 100	213.97	214.88	91	00			
A 100	214.88	215.49	58	00		2.62	
A 100	215.49	216.71	94	00			
A 100	216.71	217.32	34	00		2.73	
A 100	217.32	218.54	71	00			
A 100	218.54	220.07	129	00			
A 100	220.07	220.68	46	00			
A 100	220.68	221.59	69	00			
A 100	221.59	223.72	45	00			
A 100	223.72	225.86	156	00			
A 100	225.86	228.30	241	00			
A 100	228.30	230.73	141	00			
A 100	230.73	231.65	63	00		2.69	
A 100	231.65	235.61	290	00			
A 100	235.61	238.35	166	00			
A 100	238.35	239.88	153	23			
A 100	239.88	242.93	273	103		2.68	
A 100	242.93	244.45	152	23			
A 100	244.45	247.80	300	55			
A 100	247.80	249.02	112	00		2.66	
A 100	249.02	252.07	305	139			
A 100	252.07	253.59	152	47			
A 100	253.59	254.51	10	00			
A 100	254.51	257.56	283	17			
A 100	257.56	259.38	142	81			
A 100	259.38	260.30	53	00			
A 100	260.30	261.82	97	38			
A 100	261.82	263.65	178	125			
A 100	263.65	265.79	155	00			
A 100	265.79	267.61	143	45			
A 100	267.61	267.92	26	00			
A 100	267.92	268.93	32	00			

A UMM				ROD	SP. GR.
A TYP				CM	SG
A MTH				M-3	WEIGH
A LAR				FLD	FLD
A 100	268.83	269.11	21	00	
A 100	269.14	270.35	79	19	
A 100	270.05	270.97	71	23	
A 100	270.97	273.41	80	00	
A 100	273.41	274.02	19	00	
A 100	274.02	274.93	61	00	
A 100	274.93	275.84	71	00	
A 100	275.84	278.23	198	97	
A 100	278.23	278.89	57	23	
A 100	278.89	280.42	93	00	
A 100	280.42	282.85	92	00	2.67
A 100	282.85	283.34	38	00	
A 100	283.34	284.68	89	00	
A 100	284.68	285.29	61	00	
A 100	285.29	286.21	92	19	
A 100	286.21	288.65	105	00	
A 100	288.65	290.17	139	00	
A 100	290.17	292.00	145	00	
A 100	292.00	293.83	173	00	
A 100	293.83	295.96	120	58	
A 100	295.96	297.18	122	00	
A 100	297.18	298.40	103	42	
A 100	298.40	302.06	271	80	
A 100	302.06	305.41	295	61	2.68
A 100	305.41	308.46	288	69	
A 100	308.46	311.81	297	195	2.51
A 100	311.81	315.16	297	108	
A 100	315.16	316.99	115	00	
A 100	316.99	320.04	280	34	2.65
A 100	320.04	322.17	148	17	
A 100	322.17	325.22	202	00	2.67
A 100	325.22	327.96	175	26	2.65
A 100	327.96	331.01	274	70	
A 100	331.01	334.06	296	38	2.68
A 100	334.06	337.72	233	00	
A 100	337.72	340.16	227	54	2.72
A 100	340.16	342.90	201	25	
A 100	342.90	344.42	79	00	
A 100	344.42	346.56	214	00	2.65
A 100	346.56	349.61	268	59	2.61
A 100	349.61	352.65	276	23	
A 100	352.65	352.96	10	00	
A 100	352.96	356.01	276	21	2.61
A 100	356.01	356.31	9	00	
A 100	356.31	357.38	87	00	2.65
A 100	357.38	359.66	195	00	
A 100	359.66	361.80	211	46	
A 100	361.80	363.63	163	33	
A 100	363.63	366.67	192	122	2.70
A 100	366.67	369.72	297	101	
A 100	369.72	373.08	326	37	

G E O L O G				JASON PB-ZD-AG-RA STE DEPOSIT, Y.T.		PAGE - 15	
DRILLHOLE/TRAVERSE --- 81-DH075 --- (CONTINUED)							
A UMM				RHD	SP. GR.		
A TYP				CM	SG		
A MTH				D-B	WEIGH		
A LAR				FLD	FLD		
A 100	373.08	376.43	182	56			
A 100	376.43	377.04	57	00			
A 100	377.04	380.19	267	35			
A 100	380.09	381.61	123	42			
A 100	381.61	384.66	301	92	2.64		
A 100	384.66	386.79	213	29			
A 100	386.79	389.23	244	00			
A 100	389.23	390.75	84	19			
A 100	390.75	392.87	180	00			
A 100	392.87	395.33	236	00			
A 100	395.33	398.37	285	20			
A 100	398.37	401.42	275	19	2.55		
A 100	401.42	404.47	260	111			
A 100	404.47	406.60	174	37			
A 100	406.60	409.60	316	76			
A 100	409.60	410.26	46	00	2.67		
A 100	410.26	412.39	171	28			
A 100	412.39	413.61	122	00			
A 100	413.61	414.83	79	00			
A 100	414.83	416.66	147	28			
A 100	416.66	419.10	219	00			
A 100	419.10	421.54	236	17			
A 100	421.54	423.67	172	23	2.67		
A 100	423.67	424.23	61	36			
A 100	424.23	427.02	260	00	2.66		
A 100	427.02	428.85	142	00	2.64		
A 100	428.85	430.99	161	20			
A 100	430.99	432.51	118	00			
A 100	432.51	434.95	232	00			
A 100	434.95	435.85	83	00			
A 100	435.85	439.22	325	67	2.76		
A 100	439.22	441.05	168	00			
A 100	441.05	441.96	60	00			
A 100	441.96	442.87	62	00	2.73		
A 100	442.87	443.48	54	00			
A 100	443.48	444.70	86	00			
A 100	444.70	445.92	100	00			
A 100	445.92	447.14	122	00			
A 100	447.14	449.28	150	00			
A 100	449.28	450.80	145	38			
A 100	450.80	452.32	133	00			
A 100	452.32	455.63					
A 100	455.63	456.72	253	00	2.67		
A 100	456.72	459.33	61	00			
A 100	459.33	460.25	74	00			
A 100	460.25	462.33	73	17			
R ASY	460.25	461.47			GROUDED		
A 100	462.33	465.43	186	52			
A 100	465.43	468.43	167	13	2.59		
A 100	468.43	471.53	256	96			
A 100	471.53	473.66	160	27			

A UTM			ROD	SP. GR.
A TYP			CD	SG
A MTH			4-B	WEIGH
A LAB			FLD	FLD
R ASY	471.53	471.53		GROUND
A 100	475.66	475.19	61	00
A 100	475.18	475.79	16	00
A 100	475.79	477.01	73	00
A 100	477.01	478.54	110	00
A 100	478.54	480.67	165	00
A 100	480.67	481.89	98	00
A 100	481.89	483.11	122	23
A 100	483.11	486.16	284	52
A 100	486.16	486.77	61	00
A 100	486.77	487.07	00	00
R ASY	486.77	487.07		GROUND
A 100	487.07	487.98	55	00
A 100	487.98	489.75	177	123
A 100	489.75	492.25	190	13
A 100	492.25	492.94	26	00
A 100	492.94	493.62	68	43
A 100	493.62	495.30	76	00
A 100	495.30	497.20	165	34
A 100	497.20	499.00	124	25
A 100	499.00	501.00	122	00
A 100	501.00	503.53	213	00
A 100	503.53	504.14	32	00
A 100	504.14	505.05	50	00
A 100	505.05	506.53	93	00
A 100	506.53	508.10	135	12
A 100	508.10	509.02	85	16
A 100	509.02	509.93	80	12
				2.59
A 100	509.93	510.84	91	32
A 100	510.84	512.06	93	00
A 100	512.06	512.67	47	00
A 100	512.67	513.59	57	00
A 100	513.59	514.50	89	12
A 100	514.50	515.72	87	12
A 100	515.72	516.94	110	00
A 100	516.94	517.25	27	00
A 100	517.25	518.16	52	00
A 100	518.16	519.07	63	00
A 100	519.07	520.29	83	00
A 100	520.29	521.82	146	23
				2.70
A 100	521.82	523.04	93	00
A 100	523.04	524.26	122	00
A 100	524.26	525.17	72	00
A 100	525.17	525.78	61	00
A 100	525.78	527.00	94	29
A 100	527.00	527.61	58	15
A 100	527.61	528.52	56	00
A 100	528.52	529.74	121	12
A 100	529.74	530.66	78	00
A 100	530.66	531.88	106	00
A 100	531.88	533.40	145	19

G E O L O G

JASON PR-ZN-AG-BASIF DEPOSIT, Y.T.
DRILLHOLE TRAVERSE --- 81-DH075 --- (CONTINUED)

A UMM	RDD	SP. GR.
A TYP	CS	SG
A MTH	B-B	WEIGH
A LAB	FLR	FLD

A 100	533.40	534.01	48
A 100	534.01	535.53	132
A 100	535.53	536.75	120
A 100	536.75	538.28	121
A 100	538.28	538.89	61
A 100	538.89	540.11	87
A 100	540.11	541.02	84
A 100	541.02	542.24	122
A 100	542.24	543.76	
A 100	543.76	545.29	153
A 100	545.29	546.20	76
A 100	546.20	547.12	92
A 100	547.12	548.64	152
A 100	548.64	549.55	91
A 100	549.55	550.16	54
A 100	550.16	551.69	113
A 100	551.69	552.60	91
A 100	552.60	553.83	12

2.71

R SUM DRILL HOLES DDH81-75 AND DDH77-22 CORRELATED WELL USING

R SUM MARKER BEDS D,B,A AND C. CORRELATION WITH DDH78-27 WAS ALSO

R SUM FAIRLY ACCURATE IN PREDICTING THE DRILL HOLE LOCATION, WITH

R SUM RESPECT TO THE ORE ZONE, ONCE IT WAS IT WAS REALIZED THAT THE

R SUM MARKER BED C WAS NOT PRESENT. THIS MARKER BED HAS EITHER BEEN

R SUM FAULTED OUT OR GREATLY REDUCED IN SIZE.

R SUM LITHOLOGIC UNIT IN DDH81-75, WERE BROKEN SHEARED AND GOUGED

R SUM THROUGHOUT LARGE PORTION OF THE HOLE. MANY UNITS WERE ALSO

R SUM REPEATED, INDICATING A GREAT DEAL OF FAULTING HAS TAKEN PLACE.

R SUM THE ORE ZONE IS APPARENTLY TRUNCATED AT DEPTH BY A MAJOR FAULT.

R SUM A .5 M ZONE OF MINERALIZATION OCCURS 8 METERS PAST THE MAIN

R SUM ORE ZONE AS A RESULT OF THIS FAULT.

R SUM AN UNKNOWN BLUE MINERAL WAS OBSERVED IN THE HANGING WALL ROCKS

R SUM ABOVE THE ORE ZONE. IT WAS SAMPLED FOR IDENTIFICATION.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASUN PR-ZH-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 81-DH076
TOTAL DEPTH/LENGTH : 169.25
CORE/HOLE DIAMETER : HQCOLLAR ELEVATION : 1296.37
NORTHING (= TE S) : 7002568.00
EASTING (= TE W) : 436555.31AZIMUTH(DEG) : 5.00
VERTICAL ANGLE : -59.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : JER + AMC
DATE (YY/MM/DD) : 810817
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	46.02	7.00	-57.75
2	83.52	10.00	-56.00
3	124.05	13.00	-55.25
4	167.03	16.00	-55.00

F - 1 0 1 E R V A L -		CORE	T- %	TYPI- GAL	THX- GRAIN	PGT	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K L	(UNITS = . DEC.PLACE) RECDV-	M M	ROCK	RYING MIN	TURES CHARACS			H H H H H ANY H H H ANY	ALT ORE	
F A	(METRIC FT=FOOTRIC) ERY	0 T	TM TM	MAT TX TX	F C % M ARG	/RI	T ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y G	F R D N - 1 0 - 1 N T (.)	D X	TYPE	1 2	Q01 1 2 F F C A		1 AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K F	ROCK	FR	RT	TM	Q02 TX TX S C O O	CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA		
E L	QUAL	AGE	ER- 0	LC- 3	3 4 0	/	2 AZM RT H H H H H H H H	1 1		
Y G	DESIG	VTR	COL		R C		STRUCTUR-2	A A A A A A A A A A	2 2	

R SVY 0.00 0.00 ALL SURVEY ARE SPERRY SUN SINGLE SHOT.

/ OVR 0.00 3.77 3.77 OVER P

/ NET 3.77 7.88 4.11 CGCP PY *C1 B* F* MP4 P D*

L 3.77 7.88 OPEN STRUCTURE INVOLVES CHERT AND ARGILLITE SANDSTONE MATRIX.

/ NET 7.48 7.88 0.40 X SAND PY *C+ 4 5 3 7 R LI D*

L 7.48 15.86 7.98 BRBN SI2 NO9 P LI D*

/ 15.86 19.64 3.78 ARSI SI1 SS P 2 BD 62 L*

L 15.86 19.64 PYRITE WITHIN SILT LAMINATIONS. BEDDING PLANE CLEAVAGE.

/ 19.64 47.79 28.06 BRBT *C= K* NS8 P LI D*

L 19.64 47.79 CHLORITE IS BRIGHT GREEN. F* B* LO2 C. C.

/ 30.76 32.16 1.40 X BRBN SF NP9 R D*

L 30.76 32.16 1.40 BRXX LN1 C. B-

/ SHR 30.91 31.00 0.09 X BRXX LN3 R #7 B-

L 30.91 31.00 0.09 6A

[illegible]

/	FAL	71.98	71.96	0.48	X FAUL CR	GG7		R					
L													
/		71.96	87.90	15.94	PRTT CR	*C+ H* R*	NS7	P	<=	<=	D*		
L						F* B*)	M03			<. <=			
/	FLT	75.00	75.19	0.19	X FAUL CR	GG4		R					
L													
/	FAL	75.80	76.28	0.48	X FAUL	GG7		R					
L													
/	SHR	77.90	78.10	0.20	X BRHT CR	*C+ H* R*	NS7	R	<=	<=	D*		
L						GG1 F* R*)	M03			<. <=			
/		82.10	83.70	1.60	X CGCP SF	*C) CU R*	M06	R	>*		D=		
L													
/		83.70	84.16	0.46	X SAND CB	SS	3 4 2 6	R	<=				
I							7						
R		85.70	86.16		CALCITE CEMENT.								
/		87.90	91.00	3.10	SAND	SS	3 4 4	P 2 RD	V+		L=		
L							b			V*			
/		87.90	91.00	3.10	1 ARGL CR	+ LM+		R			D=		
L													
R		87.90	91.00		BITUMENS WITHIN QUARTZ VEINS. PYRITE ALSO IN MASSIVE PATCHES.								
R		87.90	91.00		CHERT CLAST FORM A SMALL PORTION OF THE INTERVAL. SOME APPARENT								
R		87.90	91.00		ANGULAR CLASTS MAY BE BROKEN QUARTZ VEINS. DISTRUCTION OF VEINS								
R		87.90	91.00		DURING SOFT SEDIMENT DEFORMATION INDICATES THAT THE VEINS WERE								
R		87.90	91.00		PRESENT SHORTLY AFTER DEPOSITION. POOR ROCK QUALITY PROHIBITS								
R		87.90	91.00		DISTINGUISHING STRATIGRAPHIC DIRECTION.								
/		91.00	93.22	2.22	BRHT		NQ5	P	V)		C.	D*	
L							O NN4						
/		91.00	93.22	2.22	3 APGL	SS		R	V*		C.	D*	
L													
/		91.00	93.22	2.22	3 BRPM			R	<*		C.	D*	
L													
R		91.00	93.22		THE ROCK IN THIS INTERVAL IS TOO HIGHLY FRACTURED TO ALLOW AN								
R		91.00	93.22		ACCURATE MEASUREMENT OF ARGILLITTE CLAST SIZE.								
R		91.00	93.22		SOFT SEDIMENT DEFORMATION MAKES LITHOLOGICAL IDENTIFICATION								
R		91.00	93.22		DIFFICULT BY SHEARING AND STRETCHING THE ARGILLACEOUS COMPONENTS								
/	SHR	93.22	97.07	4.45	ARSI	SI2 SS	1 2 2 3	P 2 RD	<)		C*	7*	
L							7						
/	FAL	93.22	93.72	0.50	X ARSI	SI2 SS	1 2 2 3	R 2 RD	<)		C*	7*	
L							7						

[illegible]

R 136.38 137.33 THE FIRST HALF OF THIS INTERVAL IS DOMINATED BY A PIECE OF

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/ LSX 146.49 147.50 1.11      L=LSX SX BA CH1 // SS      P 1 80      63      L2      M6      L1

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K	F	F	R	D	T	I	N	T	RECDV	RD	%	ROCK	TM	TM	TM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	GZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2			
E	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L	-L
Y	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G	G

R 146.39 147.50 LAST HALF OF INTERVAL IS ALMOST ENTIRELY MASSIVE, VUGGY PYRITE
 R 146.39 147.50 LAMINATIONS ARE NOT EASILY DISTINGUISHED IN THE PYRITE, BUT ARE
 R 146.39 147.50 NOTICEABLE CONVOLUTE IN THE SULPHIDE-SULPHATE.

/ LSX 147.50 148.44 0.94 LMSX SX BA CH= // SS P 1 BD 65 L6 L1 L1

L 14

/ LSX 148.44 149.42 0.98 LMSX SX BA CH1 // SS P 1 BD 65 L4 L1 L1

L 14

/ LSX 148.44 149.42 0.98 2 ARGL SF R <*

L 2A

R 148.44 149.42 THE CHERTY ARGILLITE SEEMS CONFORMABLE WITH BEDDING IMMEDIATELY
 R 148.44 149.42 ABOVE, BUT BEDDING IS DISTURBED BELOW WITH PLASTIC DEFORMATION
 R 148.44 149.42 OF BARITE. DISTINCT WHITE SPHALERITE POOR CHERTY BARITE PATCHES
 R 148.44 149.42 ABRUPTLY CHANGE TO CHERT POOR, SPHALERITE RICH, YELLOW BARITE.
 R 148.44 149.42 LAMINATIONS ARE CONTINUOUS BETWEEN THE SEPARATE AREAS.

/ LSX 149.42 150.41 0.99 LMSX SX BA CH2 // SS P 1 BD 62 L3 L1 L1

L 1A 2

/ LSX 150.41 151.49 1.08 LMSX SX BA CH2 // SS P 1 BD 62 L3 L1 L1

L 1A 2

/ 150.41 151.49 1.08 1 ARGL SF R <* <3

L 1A

R 150.41 151.49 THE CHERTY ARGILLITE MAY BE A FRAGMENT 30CM LONG. IT IS HIGHLY
 R 150.41 151.49 FRACTURED WITH PYRITE VEINING.

/ LSX 151.49 152.60 1.31 LMSX SX BA CH2 // SS P 1 BD 55 L2 L1 L2

L 2

/ 151.49 152.60 1.31 1 ARSI SF SI1 SS 0 1 1 R 2 BD 55 >1 >3

L 1A

/ LSX 151.62 151.73 0.11 X LMSX SX BA CH1 // SS R 1 BD 65 L1 L8 L=

L 1

R 151.62 151.73 THIS IS THE FINAL INTERVAL OF THE ORE ZONE THE LAMINATIONS ARE
 R 151.62 151.73 VERY REGULAR, AND SHOW LITTLE TECTONIC OR SOFT SEDIMENT
 R 151.62 151.73 DEFORMATION. THE ARGILLITE IS AT THE BOTTOM OF THE INTERVAL.
 R 151.62 151.73 MINOR INTERBEDDING OCCURS WITH 3.5CM OF ARSI SEPARATED FROM THE

R 151.62 151.73 BULK OF THE ARSI BY 8.5CM OF LMSX. THE PYRITE MACROVEINING CUTS
 R 151.62 151.73 BOTH THE SILT AND THE SULPHIDE LAMINATIONS. ASSOCIATED WITH THE
 R 151.62 151.73 PYRITE IS BARITE WHICH FORMS THE CENTRAL PART OF SOME OF THE
 R 151.62 151.73 VEINS.

R 152.80 153.22 A PYRITE MACROVEIN WITH BARITE OCCURS AT THE CONTACT BETWEEN THE
 R 152.80 153.22 BRHT AND ARSI. IT CONTAINS FRAGMENTS OF ARGL BRECCIA, AND

R 152.80 153.22 MICROVEINS EXTEND INTO THE ARSI, BUT NOT INTO THE BRHT.

K LM1 152.80 152.80 0.00

/ CON 152.80 153.23 1.03 BRHT *C) ST R* LP3 P <) B*

L 2A F* R* KM7

G F O L O G

[illegible]

Z	152.80	153.22	0.42	X ARSI		R	2 BD	55	<*	7)
L				1A						
R	152.80	153.83		SEEMS CONFORMABLE WITH ARSI IMMEDIATELY UPHOLE.						
Z	SHR	153.83	154.89	1.06	BRHT	*C1 ST B*	LP3	P	>+	8+
L										
R	153.83	154.89		LARGE QUARTZ VEIN WITH A MULTITUDE OF PYRITE VEINS MAY BE						
R	153.83	154.89		FILLING OF A SHEAR.						
Z	CON	154.75	154.89	0.14	X CGCP	*C1 F* B*	MO1	R	CN	<- 7)
L				3A			MO9			<?
R	154.75	154.89		YELLOW STAINING OF BARITE POSSIBLY SPHALERITE.						
Z		154.89	155.89	1.00	CGCP	*C1 F* B*	MO1	P	<- 7)	<?
L				3A			MO9			
R	154.89	155.89		RECURRENT OF YELLOW STAINED BARITE.						
Z		155.89	156.89	1.00	CGCP	*C1 F* B*	MO2	P	6)	6+
L							8			00
Z		156.89	158.21	1.32	CGCP	*C1 F* B*	MO2	P	6)	6+
L							P8			00
Z		158.21	162.80	4.59	CGCP	*C1 F* B*	MP1	P	<- 7)	
L							P			
Z	CON	162.80	164.15	1.35	SAND	G: DX 3 4 3 6		P	D	<. 7)
L						7				
R	162.80	164.15		CONTACT WITH CGCP IS GRADATIONAL.						
Z		163.50	164.15	0.65	X BRHT	*C1 B* F*	MP4	R	<- 6)	
L						R*	KN6			
R	163.50	164.15		GRADATIONAL CONTACT BETWEEN THE SAND AND BRHT.						
Z		164.15	165.30	1.15	ARSI SF	SF= SS // 0 1 2		P	2 BD	60 <- 8*
L				1A						
R	164.15	165.30		MAY BE A LARGE FRAGMENT, THOUGH CONTACT CONFORMS TO BEDDING.						
Z		164.85	164.80	0.10	X BRHT	*C+ R* F*	MP4	R		D)
L				2A		H*	KN6			
Z		165.25	165.30	0.05	X BRHT	*C. R* F*	MO3	R		B3
L				2A			LN7			
R	165.25	165.30		SEEMS LIKE INJECTION ALONG CONTACT.						
Z	CON	165.30	168.25	2.95	ARGL CR SF	SF= SS // 0 1 2		P	2 BD	59 <*
L					R	ST= FR				B. L)
Z		166.58	167.18	0.60	X ARGL	00 00 600 SS // 0 1 2		R	2 BD	59 <*
L				1A		SI1 00				B. L)

K	F	F	R	O	D	-	T	O	-	I	N	T	RECDV	MD	%	ROCK	TM	TM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	Q	D	AGE	EV	RU	LC	TM	DM2	TX	TX	S	C	D	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

Z	167.46	167.54	0.18										X	ARGL	CH	SF	SF=	SS	//	0	1	2					R	2	BD	59	<1			B.		L+											
L																																															
R	167.46	167.64																																													

STOCKWORK-LIKE QUARTZ VEINING.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZN-AG-RS STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 81-08077
TOTAL DEPTH/LENGTH : 298.09
CORE/HOLE DIAMETER : 80MMCOLLAR ELEVATION: 1235.53
NORTHING(= IF S): 7002472.00
EASTING (= IF N): 436719.94AZIMUTH(DEG) : 18.00
VERTICAL ANGLE : -76.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : HDG +
DATE (YY/MM/DD): 810708
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	19.81	23.00	-72.25
2	36.57	28.00	-69.75
3	57.91	32.00	-67.25
4	72.54	34.00	-65.50
5	88.70	35.00	-65.00
6	106.68	37.00	-62.50
7	118.87	37.00	-62.00
8	128.00	38.00	-61.50
9	146.30	38.00	-61.50
10	160.93	38.00	-60.50
11	174.34	39.00	-60.00
12	198.12	41.00	-57.25
13	220.07	41.00	-55.00
14	235.00	46.00	-52.75
15	249.00	45.00	-52.00
16	264.26	47.00	-50.00
17	279.50	48.00	-49.00
18	294.74	46.00	-48.00

F	I	D	E	R	V	A	L	=	CORE	T	=	%	TYPE	NAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY											
K	L	(UNITS =	DEC. PLACE)	RECOV	M	M	ROCK	FLYING	MTR	TURES	CHARACS	ARG	/RT	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-	ALT	ORE	
E	A	(MT=METRIC FT=FOOTRIC)	ERY	D	I			IN	TH	MAT	IX	TX	F	C	%	M																		
Y	G	F	R	D	M	=	I	D	=	I	D	I	(.)	D	X	TYPE	1	2	001	1	2	F	F	C	A							
K	F																																	
E	L																																	
Y	G																																	

R	SVY	0.00	0.00	SPERRY-SUN SINGLE-SHOT RESULTS.																							
R	SVY	175.87	175.87	CLAPISON WEDGE FULL STEEPENING, WEDGE NO GOOD.																							
R	SVY	180.75	180.75	CLAPISON WEDGE FULL STEEPENING.																							
R	SVY	202.08	202.08	CLAPISON WEDGE FULL STEEPENING.																							
R	SVY	220.07	220.07	CLAPISON WEDGE FULL AZIMUTH RIGHT.																							

Z	OVR	0.00	3.95	3.95	OVER																							
L																												

Z		3.95	11.02	7.07	BRPH *S* MP6 P D)																							
L					2A 2 * KN=																							
R		3.95	11.02	ARGILLITE FILLS THE PEBBLY MUDSTONE MATRIX.																								

Z		11.02	23.30	12.28	BRPH CR SC NR9 P B)																							
L																												

[illegible]

/	62.50	62.80	39.50	ARST CR	SM1 SC RD 1 3 1 5	P 1 RD	54	L)	
L				3A	S1+ YB 8				
/	62.80	67.29	4.49	BRHT	*S*	MP6	P	R)	
L				3A	*C* R* B* 2 1	LN1			
R	62.80	67.29		THE HETEROGENEOUS BRECCIA HAS A REDDLY MUDSTONE MATRIX.					
/	67.29	69.19	1.90	BRHT	*C.	LP6	P	R)	
L				4A	R* 3	LN2			
/	67.29	67.79	0.50	7 CGCP	*C.	LN2	R	R)	
L				5A	R* 4	C LM6			
R	67.29	67.79		FROM THE CHERT PEBBLE CONGLOMERATE TO THE HETEROGENEOUS BRECCIA					
P	67.29	67.79		THERE IS A TRANSITIONAL CHANGE. THIS INVOLVES AN INCREASE IN					
R	67.29	67.79		THE NUMBER OF SILTY ARGILLITES. BOTH INTERVALS HAVE A SANDY					
R	67.29	67.79		MATRIX WITH A CLOSED FRAMEWORK, HOWEVER THE HETEROGENEOUS					
R	67.29	67.79		BRECCIA DOES BECOME MORE OPEN IN THE LAST 20CMS.					
/	69.19	70.90	1.71	SAND	SH7 G; RD 1 3 9 6	P 2 RD	U65 V=	D*	
L				8A	7 0		B*		
/	69.19	70.90	1.71	3 CGCP	*C) G; RD	LO1	R 2 RD	D*	
L				7A		C LO4			
R	69.19	70.90		THE CONGLOMERATE IS INTERBEDDED WITH THE SANDSTONE, AS NORMALLY					
R	69.19	70.90		GRADED INTERVALS WHICH PROGRESS FROM COARSE CHERT FRAGMENTS TO					
R	69.19	70.90		FINE SANDSTONES. THESE CYCLES ARE REPEATED AT LEAST 5 TIMES					
R	69.19	70.90		THROUGH THE TOTAL INTERVAL.					
/	70.90	83.03	12.13	BRHT	*S* F*	NS3	P	R*	
L				3A	*C) R* R* 2	LP2			
R	70.90	83.03		THE BRECCIA IS MAINLY COMPOSED OF SILTY ARGILLIC AND CHERTY					
R	70.90	83.03		FRAGMENT WITHIN A PEBBLY MUDSTONE MATRIX. THE SIZE AND					
R	70.90	83.03		FREQUENCY OF SILTY ARGILLIC FRAGMENTS DECREASES GOING DOWNHOLE					
R	70.90	83.03		UNTIL THE ROCK TYPE CHANGES TO A PEBBLY MUDSTONE.					
/	83.03	90.61	7.58	BRPM	*S* F*	M02	P	R)	
L				3A	*C) R* B* 2 + 0	K02			
/	90.61	92.36	1.75	SAND	SH9 MX	3 3 9 4	P	D*	
L				5A	8				
/	91.01	91.20	0.19	7 BRPM	*C*	K01	R	R+	
L				4A	SH7 F* 3	0 KN2			
R	91.01	91.20		THIS INTERVAL HAS A SANDSTONE MATRIX. IT APPEARS AS A LARGE					
R	91.01	91.20		LENSE WITHIN THE SANDSTONE, RATHER THAN AN INTERBED.					
/	92.36	96.82	4.46	CGCR	*C+ F*	J02	P	R)	
L				5A	B* R* 3	C K03	V+	B*	
R	92.36	96.82		CHERT CLASTS ARE MODERATELY ROUNDED TO INTERMEDIATE. THE MATRIX					
R	92.36	96.82		IS MADE UP OF SAND SIZED PARTICLES, GRADING INTO CLAY NEAR THE					

K	F	F	R	D	T	I	T	REC'D	NO	%	ROCK	TH	IN	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	
F	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																						2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

R 92.36 96.82 BASE. THIN 3CM BEDS OF SANDSTONE, WITH THE OCCASIONAL BRECCIA
 R 92.36 96.82 FRAGMENT, INTERBED WITH THE CONGLOMERATE AND ACCOUNT FOR ABOUT
 R 92.36 96.82 5% OF THE TOTAL INTERVAL VOLUME. SMALL, LIGHT YELLOW, SIDERITE
 R 92.36 96.82 PLEBS ARE FOUND IN THE QUARTZ VEINS.

/ 96.82 99.64 2.82 BRPM *C) LP2 P D*
 L 3A F* R* 1 * 0 K02

/ 99.64 103.50 3.86 BRHT *C) R* LR4 P R*
 L 3A F* 2) 102

R 99.64 103.50 THE ARGILLITE CLASTS BECOME SMALLER NEAR THE BOTTOM OF THIS
 R 99.64 103.50 INTERVAL.

/ 103.50 116.95 13.45 BRPM *C= R* LR2 P D(
 L 3A F* 3 0 LR2

/ 113.00 116.95 3.95 X BRPM R <+

R 113.00 116.95 THE ROCK IS HIGHLY BROKEN DUE TO POSSIBLE FAULTING.

/ 116.95 119.18 2.23 BRHT *S) LR5 P D)
 L 2A 2 KM1 <+

/ 119.18 130.76 11.58 BRPM *S) G: LR2 P <)
 L 3A *C+ R* R* 3) 0 KN2

R 119.18 130.76 THE MATRIX IS SANDSTONE. THIS INTERVAL IS BROKEN AND MILDLY
 R 119.18 130.76 CHEARED WITH QUARTZ-PYRITE VEINS CUTTING THROUGH THE MATRIX AND
 R 119.18 130.76 BRECCIA FRAGMENTS. VEINING IS THEREFORE POST SEDIMENT
 R 119.18 130.76 LITHIFICATION.

/ 119.74 121.41 1.67 7 BRHT *C) R* LP6 R R+
 L 3A 2 KN1 V+

/ 130.76 139.29 8.53 BRHT CR GG1 LR8 P FO 42 <+ <+
 L 2A JL+

/ 139.29 150.12 10.83 CRRR *C) G: LR2 P <)
 L 3A F* C K04 <+

R 139.29 150.12 THE CHERT FRAGMENTS APPEAR MODERATELY ANGULAR TO INTERMEDIATE.

/ 142.34 143.86 1.52 9 SAND SM9 G: 0 3 9 4 R 1 BD U45 <+
 L 3A BD // 8

/ 147.90 148.54 0.74 8 SAND SM6 G: 0 3 9 5 R 2 BD U38 B+
 L 3A BD // 8

/ SHR 150.12 160.02 9.90 BRHT CR MQ8 P D+
 L 2A 2 JK=

R 150.12 160.02 THIS IS A HOMOGENEOUS WITH A PEBBLY MUDSTONE MATRIX.

/ FLT 160.02 169.58 9.56 BRHT CR *S+ SS LR6 P D+
 L 2A CC 2 + KM1 <+

R 281.15 281.53 SILICIFIED ARGILLITES AND LAMINATED SULPHIDES ARE CONVOLUTED TO

R		281.15	281.53		THE POINT OF BRECCIATION. MICRO-QUARTZ VEINS CONTAIN LARGE									
R		281.15	281.53		YELLOW SPHALERITE CRYSTALS.									
/	L	281.53	282.34	0.81	LMSX SF BY	LM LC SS BR	P 0 LM	37 L4			L=			
R		281.53	282.34		A HIGHLY WEATHER BAND OF DIRTY, SOFT SULPHIDE RICH ARGILLITE									
R		281.53	282.34		INTERCALATES AT 281.94 METRES, WITH THE LAMINATED SULPHIDE.									
/	L	282.34	282.97	0.63	LMSX SF	LC BR LM	P 0 LM	37 L4			L=			
R		282.34	282.97		THE TOP AND BOTTOM 10CMS OF THIS LAMINATED SULPHIDE CONSISTS OF									
R		282.34	282.97		BRECCIATED FRAGMENTS OF LAMINATED SULPHIDE AND ARGILLITE IN AN									
R		282.34	282.97		ARGILLIC MATRIX.									
/	L	282.97	283.81	0.84	FSGX 4A	SS BR	P	#5			#1			
R		282.97	283.81											M3 #2
R		282.97	283.81		THE FRAGMENTED, LAMINATED SULPHIDE FRAGMENTS RANGE FROM 3 TO 5									
R		282.97	283.81		CMS IN DIAMETER. DARK BLACK, CARBONACEOUS ARGILLITE FRAGMENTS									
R		282.97	283.81		RANGE FROM .5 - 2CMS IN DIAMETER. THE ANGULARITY AND									
R		282.97	283.81		PRESERVATION OF REMNANT BEDDING INDICATES THAT THE FRAGMENTS									
R		282.97	283.81		HAVE BEEN DISPLAYED VERY LITTLE FROM THEIR ORIGINAL BEDDING.									
R		282.97	283.81		THE MATRIX IS A DARK GREY, SILTY ARGILLITE WHICH IS PROBABLY									
R		282.97	283.81		SULPHIDE RICH. THIS UNIT BECOMES PROGRESSIVELY RICHER IN									
R		282.97	283.81		MASSIVE MARCASITE.									
/	L	283.81	284.61	0.80	LMSX RD	LM LC BR	P 0 LM	57 L4	<*		L=			
R		283.81	284.61											M3 L3
R		283.81	284.61		THE MARCASITE OCCURS AS BOTH FINE LAMINATIONS, AND AS MASSIVE									
R		283.81	284.61		BLOCKS OF SULPHIDE WITH DISSEMINATED GALENA. ARGILLITE BED ARE									
R		283.81	284.61		FROM TC .5 - 5CMS THICK, AND BRECCIATED WHERE LAMINATED									
R		283.81	284.61		SULPHIDES UNDER GO INTENSE DEFORMATION.									
/	L	284.61	284.99	0.36	LMSX	LN LC	P 0 LM	57 L4	<*		L=			
R		284.61	284.99											L1
R		284.61	284.99		ARGILLITC INTERBEDS ARE AS THICK AS 15CMS AND ACCOUNT FOR 30% BY									
R		284.61	284.99		VOLUME, OF THE TOTAL INTERVAL.									
/	L	284.99	286.21	1.22	ARGL CR 1A	LM LC 0 1 BR 9	P	L2	<*		(L)			
R		284.99	286.21											M2 L1
R		284.99	286.21		LAMINATED SULPHIDES INTERBED WITH THE ARGILLITE. SULPHIDE BEDS									
R		284.99	286.21		ARE FROM 1 - 10CMS. IN THICKNESS AND ACCOUNT FOR 40% OF THE									
R		284.99	286.21		TOTAL ROCK INTERVAL.									
K LM1		286.21	286.21	0.00										
/	L	286.21	287.30	1.09	SILT 3A	SIS LM	0 2 6 2 9	P 1 LM	52 <))	<+	D+ B)			
/	L	287.30	289.46	2.16	SILT 3A	SIS LM	0 2 6 2 9	P 1 LM	52 <))	<+	L= B)			
/	L	289.46	292.73	3.27	ARGL CR B	NX LM 9	1 1 1	P LM	50	<+	L=			

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

FORMAT VERSION : 6B02

GEOLOGGED BY : JER +
DATE (YY/MM/DD): 810901
PROJECT NUMBER : J=MAIN

/ OVB L	0.00	5.52	5.52	OVER							P	
/ AET L	5.52	9.05	5.73	ARGL 1A	SI+	SS	SC	0	1	1	P	D.
/ WFT L	5.52	9.05	5.73	3 SAND 2A	SH9	SC	MX	3	4	4	5	R
/ AET L	5.52	9.05	5.73	2 CGCP 5A	*C=	F*	B*				NL3 0 OK7	R
/ WFT L	5.52	9.05	5.73	1 BRHT 1A	SI+						N08 L02	R

[illegible]

Z WET L	9.95	16.79	7.65	CGCP 2A	*C+ F* B* R*	L06 D L04	P				D.
Z WET L	16.79	16.92	2.22	CGCP 2A		LN4 D L06	P				D.
Z WET L	16.79	16.92	2.22	4 BRHT 1A	H* F* B* *	NP8 L02	R				D.
Z WET L	16.92	24.38	5.46	ARGL 1A		CSX C	P				D.
R	16.92	24.38		UNIT GENERALLY HAS CLOSED STRUCTURE, WITH A MATRIX OF BRPM.							
Z WET L	16.92	24.38	5.46	1 BRHT 1A	H*	N09 D LN=	R				D.
Z WET L	16.92	24.38	5.46	1 BRPM 1A		0 1 9 1 LM+	R				D.
R EDT	16.92	24.38		INTERVAL CORRECTED TO MATCH WITH ABOVE.							
Z WET L	24.24	24.38	0.14	X FAUL VA	GG5		R				D*
Z WET L	24.38	30.50	6.12	BRHT 2A	*C= FD F* B* R*	N07 MP3	P				D*
Z WET L	30.50	41.75	11.25	ARGL 1A	S15 SS SC 0 1 2		P	2 80	86		L*
Z WET L	41.75	57.00	15.25	BRHT 2A	*C+ H* F* B*	Q57 C MP3	P				D*
Z WET L	45.79	54.86	9.16	X BRHT 1A	*C* H* R* F* B*	N09 C N0+	R				D=
Z L	57.00	62.79	5.79	ARGL 1A			P				D=
Z L	61.35	61.60	0.25	X BRHT 1A			R				D)
Z FLT L	62.30	62.79	0.49	X FAUL 1A	GG2		R		#)		D)
R	62.79	63.30		YELLOW COLOUR OF BARITE VEIN INDICATES POSSIBLE SPHALERITE.							
Z L	62.79	65.56	2.77	SAND SL 3A	CB= G;	3 4 4 6 5	P	3 80	U75		B*
Z L	62.79	63.30	0.51	X BRHT 3A	SL *C1 F* H* R*	MG3 LM7	R		V1	<*	B.

[illegible]

/	L	62.79	65.55	2.77		1 SAND SL 3A	*C= F* R* R* H*	LN3 MO7	R				B*	
/	L	85.56	80.60	15.04		BRHT	*C1 F* R* R*	NR3 O MP7	P	V*			B)	
R	R	65.56	80.60			SURE ARGL FRAGMENTS SHD*	PRIMARY QUARTZ VEINING.							
R	R	65.56	80.60			MINOR SAND EGT.								
/	L	79.59	80.60	1.01		X BRHT 2A	*C1 F* R* R*	LP7 LO3	R	00			B*	
/	L	80.60	133.22	52.62		BRHM 1A CR	R* F* R*	NS9 O KO1	P	<.	C.	C.	B*	
/	L	SHR L	84.70	85.30	0.60	X FAUL 1A	GG1		R					
/	L	FAL L	94.36	95.40	1.04	X FAUL 1A	GG3		R					
/	L	FLT L	96.84	96.93	0.09	X FAUL 1A	GG2		R					
/	L	FLT L	98.90	99.16	0.16	X FAUL 1A	GG2		R					
/	L		106.63	109.42	2.79	X BRHT 2A	*C2 F* R* CR+ R*	MN4 LP6	R				B*	
R	R		106.63	109.42			GRADATIONAL BOUNDARIES INDICATE INTERVAL CONTINUOUS WITH BRHM. CLASTS IN THIS INTERVAL CARBONACEOUS. CLASTS MAINLY ARSI.							
R	R		120.00	125.00										
/	L	FAL L	120.60	121.01	0.41	X FAUL 1A	GG5		R					
/	L	CON L	133.22	138.38	5.16	SAND CR 3A	SN9 G; FU CRJ SS	3 4 4 5 4	P	1 LM CN	U65 70	P) C.	B*	
/	L		133.22	138.38	5.16	3 BRHT 3A	*C+ R* F* R* MX	LO4 KN6	R	2 BD		C.	B*	
/	L		133.22	138.38	5.16	1 BRHT 3A	*C1 R* F* R*	MP6 LO4	R	4		C.	B*	
/	L	FLT L	138.10	138.38	0.28	X FAUL 1A			R		V1	<+	B)	
R	R		138.10	138.38			FAULT IS HIGH ARGILLITE SAND.					C.		
/	L	FGT L	138.38	140.84	2.46	ARGL 1A	SI= SS 7	0 1 2 7	P	2 BD CL	63 <* 63	C.	D*	
R	R		138.38	140.84			CLEAVAGE COINCIDENT WITH BEDDING PLANE.							

[illegible]

Z	140.64	142.10	1.26	BRHT	*C1 R* F*	LO6	P			8)		
L				5A	B*	C LN4			C.			
Z	142.10	140.90	48.80	BRHT	SL BA SI1	0 1	2 OSX	P	>.	> >.	7*	
L				1A PY					C.	>.	B*	
Z	142.65	151.49	8.84	X ARGL	SI=	0 1	2 MP8	R	2 BD	80 >+	>1 >=	7=
L				1A			LN2				>+ >+	B*
R	142.65	151.49		MICROVEINING CONTAINS CA=BA=QZ=SD=PY AND SL AS BLENDS.								
R	142.55	151.49		THIS INTERVAL IS PROBABLY A FRAGMENT; ITS UPPER AND LOWER								
R	142.65	151.49		BOUNDARIES ARE BOTH BRECCIATED.								
Z	152.50	157.53	5.08	X BRHT	SL BA SI1	0 1	2 OSX	R		#1	#1 #1	7*
L							C				#)	**
Z	159.10	162.50	5.20	X BRHT	*C+ F* B*		MP7	R		V=	V.	B*
L				2A	GG2 R* H*		C LO3			B.	V= V*	
Z	171.90	172.00	1.00	X BRHT	SL BA SI1	0 1	2 OSX	R		#=	#= #)	7*
L											#*	
Z	172.00	173.20	1.20	X BRHT	SL BA SI1	0 1	2 OSX	R		>.	> >.	7*
L					GG2							
Z	173.20	174.90	1.70	X BRHT	*C*		MP9	R				B*
L					GG2		0 KN1					
R	173.20	174.90		MATRIX APPROACHES BRP4 WITH SANDY MUDSTONE.								
Z	180.14	181.05	0.91	X BRHT	GG5			R				
L					*C)							
Z	190.90	204.05	13.15	BRHT	*C) R* F*		MP8	P		<=		D=
L				1A	B*) H*		0 LP2			C.	<.	<=
R	190.90	204.05		INTERVAL IS GRAPHITIC IN SPEARS.								
Z	193.04	193.34	0.30	X BRHT	*C) R* F*		MR8	R		<=		D=
L					GG2							
Z	193.34	194.05	0.71	X BRHT	*C= R* F*		MQ2	R		<=		D*
L					H*		8					B=
Z	194.05	194.55	0.30	X BRHT	=		Q2	R				*
L					GG4 H*		8					
Z	195.50	197.10	1.60	X BRHT	*C= R* F*		MQ2	R		<=		D*
L					H*		8					
Z	197.90	198.40	0.50	X BRHT	CB		NP9	R		<=	D+ <+	B=
L				1A	SG2		KL+				<+ <=	M1
Z	198.40	200.25	1.85	X BRHT	SG= R* F*		MR8	R		<=		D=
L					GG=							

[illegible]

/	204.05	211.65	7.60	CGBR	*CP F* H*	MP2	P		P)	D*
L				3A	GG*	0 L08				
/	204.05	211.65	7.60	2 BRRT	F* H*	MQ6	R	<*		D*
L				2A	*C= SS	0 L04			<.	<*
/	204.05	211.65	7.60	2 BRRT GR CR	*C.	LP8	R	<.		D=
L				1A	GR*	0 K02				
/ FRG	204.05	211.65	7.60	1 SAND CR	CB) MX SS	3 4 2 4	R			B*
L				3A		8				
R	204.05	211.65		MATRIX IS SANDY AND CONTAINS ABOUT 70% ANGULAR CHERT GRAINS.						
R	204.05	211.65		GRAPHITE LINES SHEARS AT IRREGULAR INTERVALS.						
R	204.05	211.65		THE CHERT RICH PORTIONS OF THIS INTERVAL ARE NEARLY IDENTICAL						
R	204.05	211.65		TO THE CGBR PREVIOUSLY DESCRIBED. THE INCREASED ARGILLITE						
R	204.05	211.65		CONTENT IS DUE TO LARGE, DEFORMED FRAGMENTS FOR WHICH THE CGBR						
R	204.05	211.65		FORMS A MATRIX AND TO RELATIVELY SMALL AMOUNTS OF HOMOGENEOUS						
R	204.05	211.65		ARGILLITE SUSPENDING RARE CHERT CLASTS (BRPM).						
R	204.05	211.65		CARBON CONTENT OF INTERVAL VARIES, AND IS GRAPHITIC IN SHEARS.						
/ CON	207.57	207.72	0.15	X SAND	CH1 G; R*	3 4 4 7	R	U		B*
L				3A		3				
R	207.57	207.72		THIS PEBBLY SAND GRADES INTO CARBONACEOUS ARGILLITE BENEATH.						
/ CON	207.72	209.09	1.37	X ARGL CR GR STD	SS 0 1 1		R	CN	60	<.
L				N SF				2 BD	60	<.
R	207.72	209.09		UPHOLE CONTACT IS GRADATIONAL WITH GRADED PEBBLY SAND.						
/ FRG	211.65	224.20	12.55	ARSN CR GR SM4	SS R*	3 4 4	P	2 BD	75	B*
L				2A		ML)				P+
R	211.65	224.20		THE PRESENCE OF RARE CHERT CLASTS IS TENUOUS EVIDENCE FOR						
R	211.65	224.20		PREDECIATION WITHIN THIS INTERVAL. SOFT SEDIMENT DEFORMATION						
R	211.65	224.20		IS STRONG. BEDDING MODULATES BETWEEN 70 AND 80 DEGREES.						
/	222.20	223.90	1.70	X CGCP	F* R*	L03	R	V)		D*
L				2A		0 L07			V.	
/	224.20	224.90	0.70	BRHM CR	*C+ R* H*	MQ7	P	<)		D*
L				1A		K03			<*	
/	224.90	228.90	4.00	SAND GR	SS	3 4 4 7	P	2 BD	>)	65
L				2A		5				
/	224.90	228.90	4.00	1 ARGL CR GF	SS		R			D*
L				N						
R	224.90	228.90		GALFNA OCCURS AS A BLEBS WITHIN QUARTZ VEINS. INTERVAL IS						
R	224.90	228.90		GRAPHITIC IN SHEARS. SMALLER QUARTZ VEINS DEFORMED BY SOFT						
R	224.90	228.90		SEDIMENT DEFORMATION.						
/ CON	225.60	226.30	0.70	X ARS1	S11 SS G; 0 2 8		R	CN	U60 >1	<*
L				1A				2 BD	60	>*

/ FAL	260.09	271.08	5.79	1	RRHT	*C*	H*	H*	MO7	R	<+	<*	D)
L					2A		F*		103			<*	

/	322.50	326.55	4.05	CGCP	*C1 F* B*	KN2	P	7+
I				3A	R* CU	0 L08		
R	322.50	326.55		INTERVAL GENERALLY CHANGES UPWARD, BUT GRADING NOT APPARENT,				
R	322.50	326.55		PYRITE AS BLENDS, AND VEINING.				

/	385.65	385.46	1.81	x SAND	EX SS 3 4 3 4	R	<*	<.	HE
1				20	7				B-

[illegible]

[illegible]

7	LSX	467.49	911.19	3.70	LSX	HA	SL	CL	SS	P	1	LM	65	L9	L+
1						9	GL								B) Ls

7	408.66	410.16	2.10	X L-6X	8A	SL	CO	SS	R	1	LM	70	L9	L+
1					9	6L								8) L=

/	408.55	408.60	0.05	X STLT SF	SIN	1 2 5 3	R 2 RD	65		<-	D-
				1A						<-	

/ FRG	010.16	010.80	0.44	X SULT SF	SIG Ex	1 2 5 3	R		<=	D=
I				1A					<=	

/ LSX	410.89	411.10	0.50		x LSX	6A SL C-1 SS	R	1 LM	60	L9	L+
I						9 GL					B) L=

K LM1	411.19	411.19	0.00
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/	411.19	416.19	5.00	SILT SF SL SIL SS SC	1 2 S 3	P	2 BD	50 >*	83	P)	V*
				LA BA							

/	411.10	416.10	5.00	2 LBSX	CH= SS	R	1 LM	50 >)	88	L+
1				9						L+

R	411.10	416.10	QZ-RA VEINING AS BRECCIA FILL IN LMSX NEAR TOP OF INTERVAL.
R	411.10	416.10	LMSX CONCENTRATED NEAR TOP OF INTERVAL WITH LOCAL REDS.
R	411.10	416.10	BARITE LAMINATIONS THROUGHOUT SILTSTONE. MANY QUARTZ VEINS
R	411.10	416.10	TRUNCATED BY SOFT SEDIMENT DEFORMATION.

7	415.10	416.10	1.00	X	SILY	SF	SL	SL6	SS	SC	1	2	5	3	R	2	BD	60	>*	83	P)
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7	416.10	418.20	2.10	SILY SF SL S11 SS SC 1 2 5 3	P 2 BD	50 K+	83	P)
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/	418.20	428.55	10.35	ARGL CR SL	SC	0	1	1	P	2	BD	73	K=	7)	L*
L				N BA					JK*		CV	70			V)
R	418.20	428.55	CLEAVAGE AT 45 DEGREES TO BEDDING PLANE.												

421.28	428.55	7.27	X	ANGL	CR	SF	SC	0	1	1	R	2	BD	73	<*	<*	L*	0
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/	426.80	427.30	0.50	X B&P SF CR *CO P* H*		R	B+	L1
L					KL3			

[illegible]

/	192.00	192.90	0.90	X	SILT	SD	RD	LC	CC	X	C	R
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G E O L O G

/	271.58	271.59	0.01	X ARSI	LM SS	R	BD	85	
L									
/	274.93	274.94	0.01	X ARSI	LM SS	R	BD	57	
L									
/	279.00	279.01	0.01	X ARSI	LM SS	R	BD	58	
L									
/	283.77	283.78	0.01	X ARSI	LM SS	R	BD	65	
L									
/	287.00	287.01	0.01	X ARSI	LM SS	R	BD	90	
L									
/	294.74	294.75	0.01	X ARSI	LM SS	R	BD	65	
L									
/	299.92	299.93	0.01	X ARSI	LM SS	R	BD	45	
L									
/	306.00	332.20	26.20	ARSI SD	SI3 LC SS	P	3 BD		
L					7 A				V+
/	306.52	306.53	0.01	X ARSI SD	SI3 LC SS	R	3 BD	60	
L					7 A				V+
/	312.42	312.43	0.01	Y ARSI SD	SI3 LC SS	R	3 BD	50	
L					7 A				V+
/	318.82	318.83	0.01	X ARSI SD	SI3 LC SS	R	3 BD	50	
L					7 A				V+
/	325.22	325.23	0.01	Y ARSI SD	SI3 LC SS	P	3 BD	60	
L					7 A				V+
/	331.52	331.53	0.01	X ARSI SD	SI3 LC SS	R	3 BD	65	
L					7 A				V+
/	332.20	403.86	71.66	ARSI SD	SI1 LC SS	P	2 BD		
L					6 A				1 LM
/	334.37	334.38	0.01	X ARSI SD	SI1 LC SS	R	2 BD	60	
L					6 A				1 LM
/	341.50	341.51	0.01	X ARSI SD	SI1 LC SS	R	2 BD	65	
L					6 A				1 LM
/	349.61	349.62	0.01	X ARSI SD	SI1 LC SS	R	2 BD	70	
L					6 A				1 LM

[illegible]

Z	351.74	351.75	0.01	X ARSI SD	SI1 LC SS	R 2 BD	85	1 LM
L					6 A			
Z	358.00	358.01	0.01	X ARSI SD	SI1 LC SS	R 2 BD	90	1 LM
L					6 A			
Z	362.00	362.01	0.01	X ARSI SD	SI1 LC SS	R 2 BD	75	1 LM
L					6 A			
Z	367.28	367.29	0.01	X ARSI SD	SI1 LC SS	R 2 BD	65	1 LM
L					6 A			
Z	373.68	373.69	0.01	X ARSI SD	SI1 LC SS	R 2 BD	65	1 LM
L					6 A			
Z	379.17	379.18	0.01	X ARSI SD	SI1 LC SS	R 2 BD	50	1 LM
L					6 A			
Z	386.16	386.19	0.01	X ARSI SD	SI1 LC SS	R 2 BD	45	1 LM
L					6 A			
Z	392.24	392.29	0.01	X ARSI SD	SI1 LC SS	R 2 BD	45	1 LM
L					6 A			
Z	396.85	396.86	0.01	X ARSI SD	SI1 LC SS	R 2 BD	30	1 LM
L					6 A			
Z FLT	401.42	402.60	1.22	X FAHL	GGP	R		
L								
Z	403.65	403.85	0.01	X ARSI SD	SI1 LC SS	R 2 BD	90	1 LM
L					6 A			

[illegible]

K	F	F	R	D	M	-	T	D	-	1	X	1	REC'D	NO	2	ROCK	TX	IF	QV1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	D	P	AGE	EV	RD	LC	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R 84.02 94.92 THE HETEROLITHIC BRECCIA INTERCALATES WITH THE ARGILLITE IN 30CM
R 84.02 94.92 BEDS. THE CHERT FRAGMENTS ARE SUB-ANGULAR AND INCREASE IN SIZE
R 84.02 94.92 GOING DOWNHOLE. MINOR SHEARING OF THE ARGILLITE OCCURS AT 92.05
R 84.02 94.92 METERS. QUARTZ-PYRITE VEINS OCCUR NEAR THE BOTTOM OF THE P.G.I.

/ 94.92 109.72 14.80 BRHT *C G: LU6 P <*> R+
L SA F* R* 2 LP3 <*>
R 94.92 109.72 SILTY ARGILLITE FRAGMENTS OF GREATER THAN 60CMS ARE RAFTED IN A
R 94.92 109.72 CHERT BRECCIA. COMPACTION OF CHERT BRECCIA RESULTS IN PRESSURE
R 94.92 109.72 SOLUTION BETWEEN GRAIN BOUNDARIES. THE FRAGMENTS ARE ANGULAR.
R 94.92 109.72 BOTH REVERSE AND NORMAL GRADING OF BRECCIA FRAGMENTS OCCUR,
R 94.92 109.72 HOWEVER THE FORMER IS DOMINANT.

/ 94.95 97.04 2.09 X BRHT *C G: LU6 R <)> R+
L V+
R 94.95 97.04 SIDERITE VEINS CUT THROUGH FRACTURED CHERT FRAGMENTS. IN LARGE,
R 94.95 97.04 CHERT CLAST ARE COMPLETELY REPLACED BY FINE GRAINED PYRITE.

/ 109.72 122.40 12.68 SAND CR S08 G; RD 1 3 8 6 P 2 BD U78 <)> L+
L 4A SI1 LC 8
/ FLT 112.72 113.03 0.36 X SAND CR G07 R; RD 1 3 8 6 R 2 BD U78 V1 L+
L 4A SI1 LC 8

/ 117.96 122.40 4.44 5 BRSN CR S06 G; R* KN2 R R)
L 4A *C* R* LC 5 KN2
R 117.96 122.40 AISPY, CONVOLUTED ARGILLITE LAMINATIONS OCCUR THROUGHOUT THE
R 117.96 122.40 SANDY BRECCIA.

/ 122.40 125.65 3.25 BRHT SA CP 3 M08 P R+
L JK+
/ 125.65 127.71 2.06 ARGIL CR 1 1 1 P 0 LM 78 D)
L 0 LC 9

/ 127.71 134.10 6.39 ARSI CR S02 DB LC 1 3 2 6 P 2 BD 74 L+
L 1A SI1 G; 7
/ 127.71 128.21 0.50 7 SAND CR S07 NX 0 3 7 3 R D+
L 3A LC 8
R 127.71 134.10 SAND AND SILT ARE INTERBEDDED WITH A MASSIVE BLACK, CARBONACEOUS
R 127.71 134.10 ARGILLITE. PYRITE LAMINATIONS OCCUR WITHIN SANDY OR SILTY BEDS.

/ 128.42 132.20 3.78 1 BRHT CR KM3 R R+
L 4A G; 3 JL4
R 128.42 132.20 HETEROLITHIC BRECCIAS ARE OFTEN ASSOCIATED WITH SANDY BEDS, AS
R 128.42 132.20 THEY GRADE UP TO COARSER FRAGMENTS. THESE BEDS ARE
R 128.42 132.20 APPROXIMATELY 50CMS WIDE. BETWEEN 129.85 AND 130.15 THE ROCK IS
R 128.42 132.20 VERY PYRITIC (10-20%), AND WEATHERED.

/ 132.20 133.72 1.52 9 SAND CR LM G; 1 3 9 5 R 0 LM U50 <(> D1
L 4A 8

[illegible]

[illegible]

[illegible]

K	F	F	R	D	M	-	T	D	-	I	Q	T	RECOV	ED	%	ROCK	IN	TR	MM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																																																	

R	242.29	243.52	THICK 10CMS. SILICEOUS ARGILLITE BEDS INTERCALATE WITH THE																											
R	242.29	243.52	SULPHATE. THESE INTERBEDS ARE SLIGHTLY BRECCIATED AND																											
R	242.29	243.52	FRAGMENTED, WHICH RESULTS IN LARGE VARIATIONS IN REDDING																											
R	242.29	243.52	THICKNESS. LAMINAE CONVOLUTIONS ARE MORE OBVIOUS IN THE																											
R	242.29	243.52	ARGILLIC REGIONS. THE LAST 42CMS. OF THIS INTERVAL IS MASSIVE																											
R	242.29	243.52	SULPHATE WITH VERY FEW SPHALERITE / GALENA LAMINATIONS. THE																											
R	242.29	243.52	TOTAL VOLUME OF ARGILLITE GOES FROM 40% TO <5% IN THE LAST 42CMS																											

K	LM1	243.52	243.52	0.00																												
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/	243.52	249.02	5.50	ARSI	ST1	LM	LC	0	2	1	2	P	1	LM	71	L=	L=	L+													
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L				3A					8								<*		L+													
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/	243.52	249.02	5.50	1	LM5X		LC	LM				R	0	LM	72		L4	L+	B)													
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L				7A															L=													
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R	SPC	243.52	249.02	SAMPLE D.G. TAKEN AT 243.64 METRES. ONE UNIDENTIFIED MINERAL																											
R		243.52	249.02	WAS FOUND IN SMALL FRACTURES, WITHIN THE ARGILLITE. CHOLORITE																											
R		243.52	249.02	IS ASSOCIATED WITH THE UNIDENTIFIED LIGHT BLUE MINERAL.																											
R		243.52	249.02	INTERCALATED BARITIC BEDS OCCUR THROUGHOUT THE ARGILLITE. THE																											
R		243.52	249.02	BEDS AVERAGE 10 - 15CMS. IN THICKNESS, AND AMOUNT TO 10% OF THE																											
R		243.52	249.02	TOTAL INTERVAL. THE BEDS CONTAIN VERN THIN LAMINATIONS OF																											
R		243.52	249.02	QUARTZ, ARGILLITE, PYRITE AND SPHALERITE.																											

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-RS STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81-DH081	COLLAR ELEVATION: 1219.65	AZIMUTH(DEG) : 25.00	GEOLOGGED BY : HDG +
TOTAL DEPTH/LENGTH : 109.73	NORTHING(- IF S): 7002524.00	VERTICAL ANGLE : -65.00	DATE (YY/MM/DD): 810917
CORE/HOLE DIAMETER : 80	EASTING (- IF N): 436837.19	CO-ORD SYSTEM : UTM	PROJECT NUMBER : J-MAIN

SER. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	34.44	23.00	-64.33
2	44.89	23.00	-64.00
3	46.65	23.00	-64.50
4	52.73	24.00	-64.25
5	58.82	24.25	-64.00
6	64.92	24.50	-63.75
7	71.01	24.00	-63.75
8	75.89	24.00	-63.00
9	77.11	26.00	-63.25
10	83.21	26.00	-63.25
11	89.30	25.00	-63.25
12	95.40	26.00	-63.00
13	101.49	25.00	-63.00
14	107.59	26.00	-62.25

F	- I N T E R V A L -	CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L (UNITS = . DEC. PLACE)	RECOV-	M M	ROCK	FYING MIN	TURES	CHARACS					
E	A (MT=METRIC FT=FOOTRIC)	ERY	D I		TM TM	MAI	TX IX	F C %	M ARG	/RI	T ID	STK DIP
Y	G F R O M - T O - I N T (.)	D X	TYPE	1	2	QAL	1	2	F F C A	1	AZM	RT QZ FL CY CA BA XX PY CP GL YY

K	F	ROCK	FR	RT	TM	QAL	TX	TX	S C O O	CHT	T ID	STK DIP
E	L	QUAL	AGE	FR	LC	3	3	4	0	/	2	AZM
Y	G	DESIG	VIR	CHL			R	C			STRUCTUR-2	A A A A A A A A A A

R SVY 0.00 0.00 THE HOLE WAS DONE BY MULTI-SHOT. WITH 3 SINGLE SHOTS. SO THEY
 R SVY 0.00 0.00 WERE MERGED. SINGLE SHOT TAKEN AT 59.13M WAS DROPPED DUE TO A
 R SVY 0.00 0.00 LARGE DISCREPANCY IN THE AZIMUTH READING.

/ OVR 0.00 15.54 15.54 OVER P

/ WET 15.54 31.09 15.55 ARGILLITE SN= LX 0 3 = 0 3 P <) <+

R 15.54 31.09 THE INTERVAL IS SOFT AND HIGHLY WEATHERED.

/ 31.09 32.31 1.22 LOST P

/ 32.31 42.96 10.65 BRHM NR8 P <) D+

R 32.31 42.96 PYRITE OCCURS WITHIN THE SAND BANDS OF SILTY ARGILLITE FRAGMENTS
 R 32.31 42.96 AND AS A REPLACEMENT MINERAL IN CHERT CLASTS. THE ROCK IS

[illegible]

G E O L O G

[illegible]

R	93.00	93.23		THE LAMINATED SULPHIDE IS HIGHLY DISRUPTED, RELUSTING IN HIGHLY									
R	93.00	93.23		CONVOLUTED LAMINATIONS WHICH BECOME BRECCIATED TOWARDS THE									
R	93.00	93.23		CENTRE OF THE INTERVAL. ARGILLIC CLASTS (2 - 30CMS IN SIZE)									
R	93.00	93.23		AMOUNTING TO 10% BY VOLUME OF THE TOTAL INTERVAL, ARE									
R	93.00	93.23		INTERSPERSED WITH LAMINATED SULPHIDE FRAGMENTS. WHERE THE									
R	93.00	93.23		LAMINATIONS ARE CONVOLUTED BUT NOT BRECCIATED, THE ARGILLITE									
R	93.00	93.23		INTERCALATES WITH THE SILICIOUS SULPHIDES.									
Z L5X	93.42	94.78	1.36	LM5X SF	LC LM	P	LM	61 L3	B1	B=			
L				7Y	BR					L3			
R	93.42	94.78		THE TOP PART OF THIS INTERVAL IS SILICIOUS, WITH FROM 15 - 20%									
R	93.42	94.78		FINE GRAINED SPHALERITE. GOING DOWNHOLE THE AMOUNT OF									
R	93.42	94.78		SPHALERITE INCREASES TO 40%. THE CENTRAL 30CMS HAS BEEN REDUCED									
R	93.42	94.78		TO A SOOPY MUSH, WITH NO DISTINGUISHABLE TEXTURES. IN THE MORE									
R	93.42	94.78		ARGILLIC REGIONS THE SPHALERITE LAMINATIONS ARE LIGHT BROWN IN									
R	93.42	94.78		COLOUR.									
Z FSX	94.78	95.70	0.92	FGSX SF	BR	P		C2	B1	4+			
L				6A	SS					B=	C3		
R	94.78	95.70		FRAGMENT ARGILLITE IS FOUND IN A SILICIOUS SULPHIDE MATRIX.									
R	94.78	95.70		ARGILLITE FRAGMENTS TOTAL 20% BY VOLUME. LAMINATE SULPHIDE									
R	94.78	95.70		FRAGMENTS ARE INTERSPERSED AMONG THE ARGILLIC FRAGMENTS.									
R	94.78	95.70		REMNANT BEDDING SUGGESTS THAT DISRUPTION IS LOCAL, WITH LITTLE									
R	94.78	95.70		OR NO CLASTIC TRANSPORT. PYRITE/MARCASITE BLEBS INCREASE IN SIZE									
R	94.78	95.70		AND AMOUNT IN THE LOWER REGION OF THE INTERVAL. THE SPHALERITE									
R	94.78	95.70		IS PREDOMINANTLY REDDISH BROWN AT THE TOP, VARYING TO LIGHT									
R	94.78	95.70		YELLOW NEAR THE BOTTOM.									
K LM1	95.70	95.70	0.00										
Z	95.70	109.73	14.03	SILT	S18 LM LC 1 2 8 3	P	0 LM	62 <C	<*	D+			
L				3A CR SN+ MX							L=		
Z	95.70	96.00	0.30	X SILT	S18 BR LC 1 2 8 3	R	0 LM	62 <*	<+	D+			
L				3A CR SN+ MX							C=		
R	95.70	109.73		SLTY ARGL INTLAM + INTERO WITH CHT-BARITE LAM CONTAINING PYR + SL									
Z	96.00	104.55	8.55	4 SILT CR	S16 LM LC 1 2 6 2	R	0 LM	64 L=	LC	L=			
L				1A	VG						L+		
R	96.00	104.55		CARBONACEOUS, LAMINATED SILTSTONE INTERCALATES WITH MORE MASSIVE									
R	96.00	104.55		SILTSTONE IN BEDS THAT AVERAGE 10 - 35 CMS. THESE SILTSTONES									
R	96.00	104.55		PART ALONG LAMINATIONS TO GIVE THE CORE A PLATY APPEARANCE.									
R	96.00	104.55		A CYCLIC REPETITION OF QUARTZ, PYRITE AND SILTSTONE LAMINATIONS									
R	96.00	104.55		OCCURS IN THE REPEAT INTERVAL. SPHALERITE DECREASES									
R	96.00	104.55		DRAMATICALLY GOING DOWNSECTION.									
Z	104.55	106.01	1.46	4 SILT SF	Py S16 LM LC 1 2 6 4	R	LM	70 L2		L=			
L				6A	SN+ FU								
R	104.55	106.01		THESE REPEAT INTERVALS ARE HIGHLY SILICIOUS AND PYRITIC. A									
R	104.55	106.01		CYCLIC REPETITION OF QUARTZ, PYRITE AND SILTSTONE LAYERS IS									
R	104.55	106.01		PRESENT.									

G E O L O G F O I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PR-7N-AR-8A SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :81-DH082
TOTAL DEPTH/LENGTH : 520.29
CORE/HOLE DIAMETER : NQHLCOLLAR ELEVATION: 1363.11
NORTHING (= IF S): 7004715.00
EASTING (= IF N): 432979.12AZIMUTH(DEG) : 30.00
VERTICAL ANGLE : -75.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : WJJ +
DATE (YY/MM/DD): 810929
PROJECT NUMBER : JASON

SEN. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	173.74	39.00	-73.50
2	185.93	39.50	-74.00
3	198.12	39.00	-73.50
4	210.31	41.00	-73.50
5	222.50	44.00	-73.25
6	234.70	46.00	-73.00
7	246.89	44.00	-72.50
8	259.08	44.00	-72.00
9	271.27	45.00	-71.50
10	283.46	43.00	-71.00
11	295.66	44.00	-70.75
12	307.85	44.00	-71.00
13	320.04	44.00	-70.50
14	332.23	46.00	-70.00
15	365.76	46.50	-70.50
16	396.24	48.00	-70.00
17	426.72	46.50	-70.00
18	460.55	49.00	-69.00
19	476.10	49.00	-69.00
20	487.68	46.50	-70.00
21	518.16	44.00	-69.66

F = INTERVAL = CORE I = Z TYPE= OAL TEX= GRAIN PGT STRUCTUR=1 ALTERATION MINS ORE-TYPE MINS SUMMARY
 K L (UNITS = . DEC. PLACE) RECHV- M M ROCK FLYING MIN TURES CHARACS H H H H H ANY H H H ANY ALT ORE
 E A (METRIC FT=FOOTRIC) ERY G T TM TR MAT TX TX F C % M ARG /RI T ID STK DIP A A A A A MIN A A A MIN - - - -
 Y G F R D H - T O - I N T (.) D X TYPE 1 2 QM1 1 2 F F C A 1 AZM RT QZ FL CY CA BA XX PY CP GL YY A 1 A 2

 K F ROCK FR RT TM QM2 TX 1X S C O O CHT T ID STK DIP MG MU CL SD QS HA PR MT SL HA
 E L QUAL AGE FR- D LC- 3 3 4 0 / 2 AZM RT H H H H H H H H H H 1 1
 Y G DESIG VIR COL R C STRUCTUR-2 A A A A A A A A A A A A 2 2

R SVY 173.74 332.23 REPRESENTS MULTI-SHOT DATA.
 R SVY 365.76 520.29 REPRESENTS SINGLE-SHOT DATA.

/ 0.00 3.66 5.66
 L

OVER

P

/ 3.66 16.50 12.84
 L
 R 3.66 16.50

ANSI

SI= LM FS A F * H
3A SN+

P

1 LM 55
FS 55

L-

HIGHLY FS NEAR TOP OF HOLE.

/ 16.50 19.51 3.01
 L

ARSD

SI1 SS (L A F 2 H
4A SN3

P

3 LM U32

B-

K	F	F	R	O	M	-	T	O	-	I	N	T	RECUM	MD	%	ROCK	TM	TM	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Y	G												R	O	D	AGE	EV	RD	LC	TM	QMP	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	NS	HA	PR	MT	SL	HA							

[illegible]

K	F	F	R	D	P	-	T	O	-	I	D	T	RECOV	MD	%	ROCK	TM	IN	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
F	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G												R	Q	D	AGE	EV	RO	LC	TM	QMI	TX	TX	S	C	U	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R 140.57 140.79 CORE BROKEN UP. POSSIBLE FAULT ZONE.

Z	143.20	317.72	174.52		ARSI		SI2 LM SS		P	2 LM	65		B*
L					3A		SN1						

Z	VEN	143.20	143.55	0.35	3 VEIN		SD1 PX	A A A	R				D-
L													D-

R 143.20 317.72 INCREASE IN SI SN CONTENT. LIGHT SHEARING MAY BE SS PARALLEL BD

Z	VEN	145.45	145.95	0.50	X VEIN		MX	A A A	R			<X
L												

R 145.45 145.95 REDUCED TO NO CORE SIZE AT 147.22M

Z		150.32	153.58	3.36	X ARSN		SN4 BD SS A F 6 F		R	4 BD	70		D-
L					5A		SI2					V=	

Z	VEN	155.30	156.83	0.53	6 VEIN		MX	A A A	R				D*
L												>X	

Z	VEN	165.90	166.57	0.67	4 VEIN		MX	A A A	R				D*	D.
L												>8		

Z		204.22	205.10	0.88	X ARSN		SN5 BD SS A F 7 G		R	4 BD	72 V+		D.
L					5A		SI2						

R 204.22 205.10 SD CONTAINS FINE SI LAMS.

Z		269.53	270.53	1.00	X ARSN		SN5 BD SS A F 4 G		R	4 BD	55 >1		D(D.
L					4A		SI1					D*	

R 269.53 270.53 SN BEDS CONTAIN FINE SI LAMS.

Z		273.24	273.76	0.52	X ARSN		SN6 BD SS A F 8 G		R	5 BD	70		D.
L					5A		SI2					D*	

R 273.24 273.76 SN BEDS CONTAIN FINE SI LAMS.

Z		278.41	281.22	2.81	X ARSN		SI1 BD SS A F 5 G		R	2 BD	60		D.
L					4A		SN4						

R 278.41 281.22 SN BEDS CONTAIN FINE SI LAMS.

X FLT 312.90 312.90 0.00

Z	FLT	312.90	314.25	1.35	X FAUL		GG9		R			
L												

Z		317.72	322.60	4.88	ARSN		SI1 BD SS A F 6 G		P	2 BD	60 <.		D(
L					5A		SN5						

X FLT 320.82 320.82 0.00

Z	FLT	320.82	320.85	0.03	4 FAUL		GG4		R	F/	60	
L												

Z		322.60	324.53	1.93	ARSI		SI+ LM BD		P	1 LM	65 <-		6(
L					4A		SN2 SS						

[illegible]

[illegible]

G E O L O G

[illegible]

R	418.14	419.70	ARGL OCCURS AS SHEARED DISRUPTED BEDS. SL IS MAINLY ASSOCIATED
R	418.14	419.70	WITH LZ <.

/	419.70	430.25	10.56	AKS1	SI+ RD	SS	A	F	2	G	P	BD	60	D*
L				4A	SM2	CG								

R	419.70	430.25	SH OR SS HAS DISRUPTED RD AND LM, PRODUCING A STRETCHED PEBBLE
R	419.70	430.25	CONGLOMERATE TEXTURE. PY OCCURS MAINLY IN THE SN SI BEDS.

420.42	421.02	0.60	X SA(0)	SI1 SX	C F 9 G	R	D.
			50	509			

VEN	425.50	426.35	0.85	6 VEIN AR	J26	AA3	R		D= B. B.
					SM3			>6	B=

R	425.50	426.35	SL, GL, CP OCCUR In 32.
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7	430.25	431.47	1.21	SAND	AR	S12	MX	A	F	7	G	P	V)	<*
1					BA	SOL								

R	430.28	431.47	ARGL OCCURS AS DISRUPTED LAMS.
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431.47	433.14	1.67	ARGL	SI + Mx BD A F = G	P 3	D*
			3A	SS + SS		V)

REF	431.47	433.14	SI SH EFDS DISPUTED BY SS SH.
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1	433.14	435.30	2.16	SAND	ARE	MX	LM	P	1	LM	90	0*
				SA	SIP							

R	453.14	455.30	LAMS FOLDS AND DISRUPTED DUE TO SS SH OBSCURING ORIGINAL SED
R	453.14	455.30	FEATURES. LM ATTITUDE VARIES FROM 90 TO 60 DEGREES.
R	455.30	458.40	BEDDED WITH SL SN BEDS UP TO .60M THICK IMODE 3

[illegible]

R	440.60	442.57	LAMINATED WITH SI SM.	TMODE 1.
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/	443.96	450.70	6.74	ARSEN	SI= LM	RD A F 4 G	P 2 LM	60	D*
L				4A	SN3 SS				

R	443.96	450.70	CLOSELY LAMINATED WITH LAMS .2CM TO 2CM APART. FAINT ARGL LAMS
R	443.96	450.70	OCCUR IN THICKER (3CM) SIL SN BEDS.

/	450.70	453.54	2.84	ARSI	ST+ MX LM A F 1 G	P 1 LM	75	D-
L				3A	SN1 SS			B.

R	450.70	453.54	SL OCCURS IN QS <.
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/	451.26	451.67	0.41	X SAND	SII	EX LST D F 9 G	R	C1	80	D*
L				SA	SII				<*	

R	451.26	451.67	SL OCCURS IN QS <. FAINT DISTORTED ANGL LAMS.
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/	VEIN	453.00	453.50	0.50	X	VEIN		ARJ	MX	VG	A	A	A	R
L								SD=						

/	453.54	458.05	14.51	ARSO	S11 LM BD A F 4 G	P 2 LM	68	D-
L				4A	S13 SS			<*

[illegible]

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-7N-AG-BA STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 41-DH083
TOTAL DEPTH/LENGTH : 332.23
CORE/HOLE DIAMETER : HQCOLLAR ELEVATION: 1188.12
NORTHING (= IF S): 7002421.00
EASTING (= IF W): 436918.44AZIMUTH(DEG) : 355.00
VERTICAL ANGLE : -77.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : BHO +
DATE (YY/MM/DD): 810926
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	41.76	357.00	-76.00
2	62.29	358.00	-76.25
3	75.90	2.00	-75.50
4	91.44	4.50	-75.00
5	106.37	4.00	-75.00
6	127.41	8.00	-74.00
7	151.79	15.00	-73.00
8	167.34	18.00	-72.00
9	185.01	20.00	-72.00
10	201.17	21.50	-71.50
11	217.02	23.00	-71.25
12	231.65	23.00	-71.00
13	246.89	23.00	-70.00
14	276.76	26.50	-69.00
15	294.74	28.00	-67.33
16	313.03	29.00	-67.25
17	328.27	30.00	-66.75

F	I	R	E	R	V	A	L	-	CORE	T	%	TYP	QUAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L	(UNITS =	DEC. PLACE)	RECDV	M	H	ROCK	TYING	MIN	TURES	CHARACS											
E	A	(1=METRIC	FI=FEET)	ERY	D	I	TR	TM	MAI	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A
Y	G	F	X	Q	D	-	I	D	-	I	N	(.)	D	X	TYPE	1	2	Q	1	2

K	F						ROCK	FM	RT	TM	Q	2	1	TX	S	C	O	D	CHT	T	ID	STK
E	L						QUAL	AGE	FM	N	LC	3	3	4	0	/	2	AZM	RT	H	H	
Y	G						DESIG	MIR	COL						R	C		STRUCTUR-2	A	A	A	

/ OVR 0.00 13.60 13.60

OVER

P

/ 13.60 16.52 2.92

BRHM CR
3AMP8 P
C JK*

D+

/ 13.60 16.52

PYRITE IS ALSO SEEN AS A REPLACEMENT OF THE CHART <1%.

/ 16.52 31.15 10.63

BRHT CR *C)
3AF* MR+ P
SS 3 C LN2

R+

/ 16.52 31.15

PYRITE OCCURS AS REPLACEMENT OF THE CHART. THESE ARE ALSO

/ 16.52 31.15

PYRITE OR BEDDING SURFACES WITHIN SOME OF THE FRAGMENTS.

/ 16.52 31.15

LARGE ARGL DO HAVE SILT LAYERING.

/ SHR 30.23 31.15 0.92

X BRHT GR CR GG=

F* MR+ R

FO U80 7)

<)

/	81.00	82.20	0.40	X	REH4	GR	PY	S11	SS	SC	NRB	R	L+
---	-------	-------	------	---	------	----	----	-----	----	----	-----	---	----

R	125.00	151.70	SAND CONTENT INCREASES TOWARDS THE BOTTOM OF THE INTERVAL.
R	125.00	151.70	SPHALERITE APPEARS TO BE A REPLACEMENT FEATURE OF THE CHART.
R	125.00	151.70	129.33 M. IT ALSO SEEM TO BE ASSOCIATED WITH FRACTURE AND

G E O L O G

[illegible]

R	185.25	216.99	ADD SHOT GRADING. PYRITE OCCURS AS A REPLACEMENT FEATURE 0.03%.
R	185.25	216.99	APPROX 20% IS ARSN FRAGMENTS.

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/      185.45   185.58    0.13          * VEIN SD SF *C= SS SC           MT7     R              >1                D-
|

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R	185.45	185.58	THIS INTERVAL CONTAINS TWO LARGE VEINS AND THE AREAS BETWEEN AND NEAR THEM CONTAIN NUMEROUS MICRO-VEINS. IT IS HIGHLY FRACTURED. THE VEINS CONTAIN ARGL AND CHERT FRAGMENTS.
R	185.45	185.58	
R	185.45	185.58	

1	188.11	188.72	0.61	X 384T GR CR 6G3	R	<1	<1	R)
---	--------	--------	------	------------------	---	----	----	----

/	216.99	220.20	3.21	BRPM	SF	SX3	F*	0	4	2	P	LP4	P	U	V)	D)
1					SA	*C=	R*	FU	4	=		K04				V=

R	216.99	220.20	THE SAND CONTENT APPEARS TO INCREASE TOWARDS THE TOP THAT
R	216.99	220.20	THE FRAGMENTS DECREASE IN SIZE TOWARDS THE TOP.
R	216.99	220.20	QUARTZ VEINING APPEARS TO PRE DAD POST DATE BRECCIATION.

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/      220.20   228.69   8.69      0010 SF      S11 SS SC 0 4 1 0 NU8      P      <)      L)
L      3A      SN= F* R*      )      KO+      <.      **

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R	220.20	228.89	SPHALERITE IS CONCENTRATED AT 225.74 M AND APPEARS TO BE A
R	220.20	228.89	RESULT OF BRECCIA FILLING. THE ARGL FRAGMENTS ARE LARGE AND
R	220.20	228.89	ARE COMPOSED MAINLY OF ANSI. PYRITE ALSO OCCURS AS A
R	220.20	228.89	REPLACEMENT FEATURE.

228.49	233.53	4.60	RRPM SF	SI4 SS F* 0	5 1 R MR3	P	V-	P)
			44	SM1 R*	3 + KP1			

/	233.53	235.10	1.57	4850	SF	SIN4	SS	SC	0	5	4	M	P	BD	80	7-	0)
1				44	SIP				6								>

R	233.53	235.10	THIS INTERVAL COULD POSSIBLY BE A FRAGMENT. CONTACT IS RATHER
R	235.53	235.10	SHARP AND THE BEDDING CHANGES BY APPROX 10%. THE BEDDING
R	233.53	235.10	IS DISRUPTED DUE TO SLUMPING.

/	235.10	236.86	1.73	ARGL	SF	LM	P	BD	90	<-	DD
L				PA		MX					

X	235.10	236.85	THE UNIT IS PASSIVE, BUT FINALLY LAMINATED.
X	236.83	239.88	THE UNIT IS COMPETENT, BUT THE SHEARING IS TAKING PLACE ON THE
X	236.43	239.88	BEDDING SURFACES. BARITE IS COATING THESE SHEARS. THE BEDDING
X	236.43	239.86	ANGLE CHANGES SLIGHTLY NEAR THE BASE.

1	236.85	241.78	4.95	AKSH SF	SN4	SS	SC	0	4	4	N	P		V)	C-	D) #. #.
1				4A CR S11				5					BD	90		V.

1	SHR	256.83	239.88	3.05	X	ARSH	GR	CR	SN4	SS	SC	0	4	4	N	R			V)		C-	D)	#.	#.
1							4A	CR	SI1			5					80	90		V.				

/ FLT	240.03	240.20	0.17	X ANGL CR	GGX	R
L				1A		
R	240.03	240.20	THE CORE BELOW THIS INTERVAL IS BROKEN UP FOR APPROX 3 M.			

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/      241.73   245.54   3.76          ARG1    CR SI= SS BD          P  2 BD          65 <)          L)
/      2A SE

```

/	245.54	248.87	3.33	BRHT SF	SN1 SS SC	NS6	P	>+		D)	
L				3A	*S1	(F	1 C KN+		<.		
R	245.54	248.87		SANDSTONE FRAGMENT AT 247.09 M CONTAINS FLUTE CAST.							
R	245.54	248.87		THE INTERVAL BETWEEN 245.67-246.89 M IS MODERATLY FRACTURED							
R	245.54	248.87		AND CONTAINS QUARTZ - SIDERITE VEINS.							
/	248.87	253.00	4.13	BRHT SF CR	*C1 F*	R*	LP5	P	>)	R+	
L				4A GR SN=	SS		+ C LP3				
/	252.50	253.00	0.50	X BRHT CR GR GG5				R			
L											
R	252.50	253.00		THIS INTERVAL IS HIGHLY BROKEN UP AND ON BOTH SIDES IT IS							
R	252.50	253.00		MODERATLY BROKEN UP.							
/	253.00	264.57	11.57	ARGL CR	SN= SS LM		P	BD	50 V=	L)	
L				3A GR SI+							
R	253.00	264.57		THE CORE BETWEEN 262.13-264.57 M IS BROKEN UP. THIS APPEARS							
R	253.00	264.57		TO BE A RESULT OF SHEARING. PYRITE APPEARS TO BE CONCENTRATED							
R	253.00	264.57		IN SAND LAYERS, POSSIBLE REPLACEMENT.							
/	264.57	277.26	12.69	ARGL	SN+ SS		P	2 BD	70 <=	C. L)	
L				3A SF SI+					<.		
R	264.57	277.26		THE CORE HAS BEEN BROKEN UP AND ARRANGED IN THE WRONG ORDER.							
R	264.57	277.26		CONTACTS BETWEEN REPEATS INTERVALS ARE NOT CLEAR. PYRITE IS							
R	264.57	277.26		LAMINATED AND APPEARS TO BE A REPLACEMENT OF THE SAND UNITS.							
/	265.57	266.12	0.55	X BRPM SF	SN1 SS	0 2 1 P LP5	R				
L				3A CR SI2		3	0 212			R)	
R	265.57	266.12		CONTACT NOT SEEN BUT APPEARS TO BE A DEPOSITIONAL FEATURE							
R	265.57	266.12		RATHER THAN A FRAGMENT.							
/	273.79	274.49	0.70	X BRHT SF	*C= R* R*	NP6	R			R)	
L				4A	SN1 SS	KM2					
/	277.26	281.33	4.07	BRPM SF	SN4 SS R* 1 5 3 P LP4	P	1 BD	070 <=	C. D)		
L					SI1 DB FU	0 KM1			<.		
R	277.26	281.33		THE AMOUNT OF SAND INCREASES TOWARDS THE TOP AND BEDDING IS							
R	277.26	281.33		WELL DEFINED. AT THE BASE THE FRAGMENTS ARE COARSER AND BEDDING							
R	277.26	281.33		IS UNDEFINED. CHERT CONTENT DECREASES TOWARDS THE TOP.							
R	277.26	281.33		AGAIN CONTACTS ARE NOT WELL DEFINED.							
/	281.33	287.12	5.79	ARGL	CR SN+ SS SC		P	1 BD	65	C. D)	
L				3A SF SI+							
/	281.33	287.12	5.79	X ARGL CR GR GG= SS SC			R	1 BD	65	C. D)	
L				3A SF SI+							
R	281.33	287.12		CORE IS BROKEN UP DUE TO SHEARS.							
R	281.33	287.12		THE WHOLE INTERVAL IS SHEARED. SOME PARTS WORSE THAN OTHERS.							
R	281.33	287.12		THERE IS ALSO A SMALL SANDSTONE UNIT AT 284.38 M.							
/	287.12	295.66	8.54	BRPM SF	SN5 SS DR 1 4 4 P KP3	P				C) R)	
L				4A	SI1	5	0 KM=				

K	F	F	R	O	D	-	T	O	-	T	N	T	RECDV	RD	%	ROCK	TM	TM	Q1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
F	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G												R	Q	D	AGE	EV	RD	LC	TM	Q2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	OS	HA	PR	MT	SL	HA								

R 287.12 295.66 BARITE OCCURS ON MOST SHEAR SURFACES. MOST OF THE INTERVAL IS
 R 287.12 295.66 BROKEN UP DUE TO SHEARING AND FAULTING. BOTH THE UPPER & LOWER
 R 287.12 295.66 CONTACTS ARE UNDEFINED.

/ FLT 295.62 294.02 0.40 X BRPM CR GR GGB R D)

L
 / 295.66 307.23 11.57 ARSN SF CR SN3 SS SC 1 4 3 M P 1 BD 70 <- C+ D)
 L 3A SI1 6

/ 295.66 296.36 1.20 X ARSN SF CR SN3 SS SC 1 4 3 M R 1 BD 80 <- C+ D)
 L 3A SI1 6

R 295.66 307.24 THE BEDDING ANGLES CHANGE FROM TOP TO BOTTOM. IT IS 80' NEAR
 R 295.66 307.23 TOP, THEN 70', 60' AND BACK TO 80' NEAR BASE. BARITE OCCURS
 R 295.66 307.23 MAINLY ON FRACTURE SURFACES BUT ALSO OCCURS AS SMALL VEINS.
 R 295.66 307.23 MOST OF THE INTERVAL IS SHEARED.

/ 296.86 299.01 2.15 X ARSN SF CR SN3 SS SC 1 4 3 M R 1 BD 70 <- C+ D)
 L

/ 299.01 302.86 3.85 X ARSN SF CR SN3 SS SC 1 4 3 M R 1 BD 60 <- C+ D)
 L

/ 302.86 307.23 4.37 X ARSN SF CR SN3 SS SC 1 4 3 M R 1 BD 80 <- C+ D)
 L

/ 306.43 306.63 0.20 X ARSN CR GR GGB R D) D)

K UM1 307.23 307.23 0.00

/ LSX 307.23 308.63 1.40 LMSX PY SF SI= LM LC 0 1 + J P 1 80 C- L2 L4 C. L+
 L 5A CH3 L) L+

R 307.23 308.63 CORE IS BROKEN UP CARBONATE CRYSTALS OCCURS ON FRACTURE SURFACES
 R 307.23 308.63 PURPLE, BLUE STAINING DUE TO COPPER. SPHALERITE AND GALENA
 R 307.23 308.63 OCCURS MAINLY WITH THE LAMINATED CHERT.

/ FSX 308.63 309.08 0.45 FGSX SF BA RR M03 P *) *2 #3 **
 L 1A PY **1

R 308.63 309.08 THE ARGL. FRAGMENTS COMPOSE 30% OF THE INTERVAL AND ARE SILIFIED
 R 308.63 309.08 THESE FRAGMENTS ALSO CONTAIN INTERSTITIAL BARITE. THE SULPHIDE
 R 308.63 309.08 FRAGMENTS ARE LAMINATED. THE INTERVAL IS HIGHLY FRAGMENTED AND
 R 308.63 309.08 BRECCIATED. BOTH THE SPHALERITE AND GALENA ARE FINED GRAINED.

/ LSX 309.08 309.53 0.45 LMSX SF PY SI2 LM LC 0 1 1 N P 2 BD 60 L5 82 C. L)
 L Y= BA SC L=

R 309.08 309.53 SPHALERITE IS FINE GRAIN AND VARIES IN COLOUR FROM A YELLOW TO
 R 309.08 309.53 PINKY-RED. IN PLACES THE BEDDING IS DISLOCATED. NEAR THE END
 R 309.08 309.53 OF THE INTERVAL, THE ROCK IS CRUSHED, THEREFORE THE LENGTH OF
 R 309.08 309.53 THE INTERVAL IS ESTIMATED. BARITE IS WEATHERED THEREFORE LOW
 R 309.08 309.53 S.G.

G E O L O G

[illegible]

/	LSX	309.53	310.47	0.94	LSX	SF	PY	SI	LI	LC	P	1	BD	80	L4	L3	L+
						BA	BA			SS							L1

R	309.53	310.47	THE YY MINERAL IS WITHERITE WHICH IS YELLISH-RED IN COLOUR.
R	309.53	310.47	THERE IS APPROX. 5% LAMINATED, CHERT AND 10% SILICIFIED SILT. THE
R	309.53	310.47	WITHERITE OCCURS IN BANDS AND REPRESENTS 1% OF THE UNIT. PYRITE
R	309.53	310.47	MARCASITE IS ASSOCIATED WITH FRACTURE FILLING.

Z	LSX	310.47	310.35	0.38	LSX	SP	PY	SS	SC	P	0	LM	70	L4	L2	L+ WI
						SA	BA	TA	LM							L= L-

R	310.47	310.85	THIS INTERVAL CONTAINS APPROX 30% ARSI AND HAS INTERSTITIAL BARITE
R	310.47	310.85	RANGING UP TO 40% OF THE TOTAL COMPOSITION. THE SPHALERITE AND
R	310.47	310.85	GALENA IS FINE GRAINED AND IS THINLY LAMINATED. THERE IS ALSO A
R	310.47	310.85	MINOR SHEAR ZONE WITHIN THIS UNIT.

/ LSX	310.85	311.74	0.89	LSX BA PY	LM LC	P	L5	L4	L+
				5A					L=

L			
R	310.45	311.74	THE LENGTH OF THIS INTERVAL IS ESTIMATED DUE TO LOST AND
R	310.85	311.74	GRINDING OF CORE. PERCENTAGES DIFFICULT TO ESTIMATE. THE
R	310.85	311.74	BARITE IS HIGHLY WEATHERED AND HAS A LOW S.G.I+ ALSO HAS A
R	310.85	311.74	SUGARY TEXTURE.

/	LSX	511.74	512.08	0.34	LSX	SF	PY	LM	LC	P	2	RD	70	L3	L3	L)
						SA	SA	SS	SC							L+

[illegible]

LSX	312.08	314.15	2.07	LSX SF 3A	LM LC	P 2 BD	70	L4	L3	L+
				LSX SF	SS SC					L1

[illegible]

/	LSX	314.15	315.53	1.38	LMSX	SF	PY	LM	LS	P	1	LM	80	L2	L4	L)
							BA		SS							L+

R	314.15	315.53	TIS UNIT CONTAINS 35% SILIFIED ARSI. THERE IS A SHEAR ZONE
R	314.15	315.53	WITHIN THE INTERVAL. THESE SHEARING SURFACES ARE GRAPHIC. NEAR
R	314.15	315.53	THE END OF THE INTERVAL, PYRITE INCREASES TO 60% OF THE ROCK.
R	314.15	315.53	THE ARSI IS LAMINATED.

/	315.55	320.77	5.24		ARSI	SF	PY	SI2	LM	CC	1	2	= M		P	1 LM	70	C=	L+	<
						3A	HA	SN=	SS			7								<

315.55	320.77	THERE HAS BEEN MOVEMENT ALONG BEDDING PLANES. ALONG THESE
315.53	320.77	SHEARED SURFACES, BARITE AND MINOR GRAPHITE HAS FORMED.
315.55	320.77	SPHALERITE AND GALENA OCCURS WITH BARITE IN MICROVEINS. THE
315.53	320.77	LAST 3 METERS IN THIS INTERVAL IS HIGHLY FRAGMENTED.

7	LSX	320.77	321.81	1.04	LSX PY BA	LM LC	P 3 BD	80 <-	L1	L7	L+
						NY					L1

THIS UNIT IS COMPOSED OF MAINLY BEDDED PYRITE. THERE IS ALSO

G E O L O G

K F F R U M - T O - I R T RECDV RD % ROCK TM IN QM1 TX TX F C % M ARG RI 1 ID AZM DIP QZ FL CY CA BA XX PY CP GL YY A 1 A 2
E -L- -----
Y G R D D AGE EV RD LC TM QM2 TX TX S C O O CHT 2 ID AZM DIP MG MU CL SD QS HA PR MT SL HA

R 320.77 321.61 APPROX. 2% ARG1 WHICH INCREASES TOWARDS THE BASE.

K LM1 321.81 321.81 0.00

/ 321.81 330.71 8.90 SILT SF PY SM1 LM SS 0 2 1 K P 1 LM 80 <) <) L) <.

L 3A CR SC 7 C. <.

R 321.81 330.71 THE WHOLE INTERVAL IS HIGHLY SHEARED. BARITE OCCURS AS MICRO
R 321.81 330.71 VEIN AND OR SHEAR SURFACES. SPHALERITE OCCURS WITH THE QUARTZ
R 321.81 330.71 VEINS.

/ FLT 327.54 327.86 0.32 X SILT GR GR GG9 R D) D+

L

/ 330.71 332.23 1.52 BRPM SF PY *C2 R* F* 1 4 3 P MP4 P >) C- D+

L LA SN3 2 0 KM2

R 330.71 332.23 THIS UNIT IS MODERATELY FRAGMENTED DUE TO FAULTING AND SHEARING
R 330.71 332.23 WITHIN THE ZONE. T.D. AT 332.23%.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-7R-AG-4A STE DEPOSIT, Y.T.

FORMAT VERSION : 6R02

DRILLHOLE/TRVERSE :81-DH084

COLLAR ELEVATION: 1233.15

AZIMUTH(DEG) : 172.00

GEOLOGGED BY : BHO +

TOTAL DEPTH/LENGTH : 621.49

NORTHING(- IF S): 7002328.00

VERTICAL ANGLE : -85.25

DATE (YY/MM/DD): 810000

CORE/HOLE DIAMETER :

EASTING (- IF W): 436584.62

CO-ORD SYSTEM :

PROJECT NUMBER : JASON

SER. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	12.00	171.30	-85.25
2	24.00	169.70	-85.25
3	37.00	167.60	-85.38
4	49.00	163.60	-85.38
5	61.00	158.60	-85.52
6	73.00	154.70	-85.42
7	85.00	151.90	-85.42
8	98.00	146.10	-85.50
9	110.00	138.90	-84.97
10	122.00	134.30	-82.83
11	134.00	132.50	-82.47
12	146.00	132.80	-81.75
13	159.00	131.00	-80.97
14	171.00	130.30	-80.05
15	183.00	130.40	-79.42
16	195.00	132.10	-78.83
17	207.00	131.30	-78.58
18	219.00	131.50	-78.38
19	232.00	121.40	-79.30
20	244.00	119.50	-79.03
21	256.00	117.70	-78.33
22	268.00	117.70	-77.42
23	280.00	113.90	-76.83
24	293.00	110.80	-75.17
25	305.00	109.80	-74.03
26	317.00	110.70	-71.75
27	329.00	111.50	-68.78
28	341.00	112.50	-68.38
29	354.00	111.50	-68.17
30	366.00	108.20	-67.03
31	378.00	107.20	-67.03
32	390.00	105.10	-67.17

33	402.00	104.10	-66.80
34	415.00	103.00	-66.42
35	427.00	102.00	-66.17
36	439.00	106.20	-65.33
37	451.00	104.10	-64.50
38	463.00	104.30	-63.88
39	475.00	103.20	-63.53
40	488.00	102.00	-63.00
41	500.00	100.90	-62.67
42	512.00	101.90	-62.55
43	524.00	101.70	-62.03
44	536.00	101.20	-60.50
45	549.00	102.40	-58.27
46	561.00	102.00	-57.17
47	573.00	102.80	-56.42
48	585.00	102.60	-56.00
49	597.00	101.40	-56.00
50	610.00	100.20	-56.08
51	616.00	101.30	-56.05

F - I N T E R V A L -										CORE T- %		TYPI- DAL		TEX- GRAIN		PGI		STRUCTUR-1		ALTERATION MINS		ORE-TYPE MINS		SUMMARY	
K L (UNITS = . DEC.PLACE) RECOV-										M M ROCK		FYING MIN		TURES CHARACS						H H H H H ANY H H H ANY		ALT ORE			
E A (MT=METRIC FT=FOOTRIC) ERY										O I		TM TM MAT		TX TX F C % M ARG		/RI		T ID STK DIP		A A A A A MIN A A A MIN		- - - -			
Y G F R D M - I D - I N T (.)										O X TYPE		1 2 OM1		1 2 F F C A				1		AZM RT QZ FL CY CA BA XX PY CP GL YY		A 1 A 2			
-----										-----		-----		-----		-----		-----		-----		-----		-----	
K F										ROCK FM		RT		TM OM2 TX TX S C O O CHT				T ID STK DIP		MG MU CL SD QS HA PR MT SL HA					
E L										QUAL AGE EN- O LC- 3		3 4 O		/				2		AZM RT H H H H H H H H H		1 1			
Y G										DESIG		VIR COL		R C				STRUCTUR-2		A A A A A A A A A		2 2			

R SVY 0.00 0.00 DATA FROM GYROSCOPIC DIRECTIONAL SURVEY. THE DATA REPRESENTED
R SVY 0.00 0.00 IN S000-S051 SHOULD BE USED FOR PLOTTING PURPOSES.

/ OVB 0.00 28.75 28.75 OVER P
L

/ WET 28.75 45.11 16.36 BRHM CR SI+ R* B* MS9 P D*
L 1A *C. LO+
R 28.75 45.11 MATRIX OF BRHM.

/ FLT 32.80 45.11 12.31 X BRHM CR SI+ R* B* MS9 R D*
L GG3

/ FAL 37.49 38.00 0.51 X FAUL CR GG9 R D*
L R

/ FLT 45.11 51.30 6.19 BRHT CR SI+ R* F* NR7 P B*
L 1A *C) H* NP3

R 45.11 51.30 ROCK HIGHLY FRACTURED, BUT VERY LITTLE GOUGE.

/ 51.30 58.80 7.50 BRHT CR GR SI= NP9 P R)
L 1A MD1

R 51.30 58.80 PYRITE REPLACES SILT IN ARSI CLASTS, AND CHERT FRAGMENTS.

/ FLT 52.00 52.43 0.43 X BRHT CR GR SI= NP9 R R)
L GG3 LN

/ FLT 56.50 57.00 0.50 X BRHT CR GR SI= NP9 R R)
L GG3 LN=

/ FLT 57.00 58.80 1.80 X BRHM SI= SS SC R <+ <) 7+
L 1A GG4 LN+

Z	L	R	58.80	60.45	1.65	BRHT CR SF *C+ R* F*	NP6	P	#2		7+
			58.80	60.45		OTHER CLASTS ARE SAND.	1 L03				
Z	FAL	L	60.45	73.50	13.05	BRHT CR GR GG6	MQ9	P	<)	<*	R+
			60.45	73.50		ARG AND CRT CLASTS ALIKE REDUCED TO GOUGE.	LO=				
Z	L	R	73.50	77.46	3.96	BRHT CR GR *C= SC F*	NR4	P	>+		R+
			73.50	77.46		NATRIX DE BRPM. NZ ALSO AS MICROVEINS. MATRIX MOSTLY MUD.	3A B* R* . . O MP4				
Z	L	R	77.46	81.50	4.04	BRHT	P4 C 5	P		HE R.	
Z	L	R	81.50	84.30	2.80	BRHT	1 G;	NP5	P	U	
			81.50	84.30		MATRIX OF BRPM. COARSE GRADING OF CLASTS UPHOLE. CR CLASTS.	O L03				
			81.50	84.30		GR IN SHEARS.					
			82.60	82.50		REDUCE TO NW IN AN ATTEMPT TO FLATTEN HOLE.					
Z	L	R	84.30	85.45	1.15	BRHT CR GR *C1 F*	NP5	P	V*		R+
						2A SF R* R* . . C MQ5					
Z	L	R	85.45	90.50	5.05	BRHT CR GR *C2 B* F*	KD3	P	<+		R+
			85.45	90.50		MUCH LESS MUD IN MATRIX- GRIT TO GRANULE SIZE COMMON.	QA R* C KP7				
Z	L	R	90.50	95.40	4.90	BRHT CR GR	MQ6	P	V1		R+
						3A C LP4					
Z	FAL	L	95.00	95.40	0.40	X BRHT CR GR	MQ6	R	V1		R+
						3A GG6 C LP4					
Z	FLT	L	95.40	100.50	5.10	BRPM CR GR SN1 VG SC 1 4	5 DR8	P	<)	WI R)	
			95.40	100.50		1A GG2 4 O LN+				<*	
			95.40	100.50		LARGE ARGL CLASTS WITH PEBBLY SAND TO SANDY MUD AS MATRIX.					
						ARGL CLASTS ALSO INCLUDE ARSI AND ARSN. SAND IS VUGGY.					
Z	L	R	98.45	98.95	0.50	X SAND	IM G; 3 4 4 5	R	IM	U30	
			98.45	98.95		COARSE SAND TO GRIT PARTICLES ALL ARG.	3A 6				
Z	L	R	100.50	105.77	5.27	BRHM CR GR SN=	3 4 4 NR9	P	<)	<*	WI 8+
						1A) C KN+			<.	<*	<.
Z	FLT	L	105.77	106.98	1.21	BRHT	SN2 VG 3 4 5 NP6	P	<*		WI R+
						2A GG2 O KN3					<*
Z	FLT	L	106.98	119.43	12.50	BRHT CR GR SN1 SC 3 4 5	NQ9	P	<)	<*	WI R+
						1A GG2) LN=			C.	<*	<*

[illegible]

R	194.16	258.35	PYRITE AS REPLACEMENT, AND VEIN WITH Q7. GRAPHITIC IN SHEARS.
R	194.16	271.27	POSSIBLY A CONTINUOUS BRHM UNIT WITH THE ARSI PGI ABOVE BEING A

R	194.15	271.27	LARGE CLAST.										
/ FAL L	197.00	197.50	0.50	X BRHM CR 2A	*C= H* R* GG2 DR	LN1 KM3	R					C.	R+
/ L	199.50	199.95	0.45	X BRHM CR GR	*S+ RR R* d	DR9	R			V)			8+
/ L	199.95	202.08	2.13	X BRHM CR GR	*S+ RR R* 6	DR9	R			V)			8+
/ L	202.98	202.25	0.17	X SAND GR 2A	SS MX 3 4 4 5 7		R					C.	R=
/ L	202.25	203.91	1.66	X BRHM	7		R						
/ L	208.80	209.30	0.50	X BRHM CR GR	*S+ RR R* 7	DR9	R			V)			8+
/ L	212.30	217.32	5.02	X BRHM CR GR	*S+ RR R* 8	DR9	R			V)			8+
/ FAL L R	223.90	224.30	0.40	X BRHM GR	*C= R*	KN2 KN2	R			<*		C.	R=
/ FAL L	223.90	224.30		GR IN SHEARS.									
/ FAL L	227.60	227.70	0.10	X SAND CR 2A	SS MX 3 4 4 5 7		R						R)
/ FAL L R R R	227.70	227.90	0.20	X CGCP SF 3A	R* H* F*	KN1 K09	R						R+
	227.70	227.90		POOR RECOVERY MAKES DETERMINATION DIFFICULT. ONLY 10CM WERE									
	227.70	227.90		RECOVERED, OF WHICH 7CM IS A SINGLE CHERT CLAST. MODERATELY									
	227.70	227.90		ROUND.									
/ FLT L R	238.35	246.60	8.25	ARSI CR 1A	SI1 // SS 0 1 2 GG4	P 2 BD 1 LM	70 70					C*	R)
/ L	238.35	246.60		SI LAMINATIONS IN ARGL BEDS. POSSIBLE FRG.									
/ L	239.60	242.93	3.13	X ARSI CR	SI1 // SS 0 1 2 1	R 2 BD	70						R)
/ FLT L R	246.60	271.27	24.67	BRHM CR GR 1A	*S+ GG1	DU9 JM*	P			<)		C.	R+
/ L	246.60	271.27		CLASTS MAINLY ARSI.									
/ L	260.10	260.30	0.20	X SAND 3A	//	3 4 3 4 R	R 3 BD	30		<=			R)
/ L	262.77	268.40	5.63	X BRHM CR GR	*S+	DU9	R			<=			R+

/ FAL	268.40	268.84	0.43	X BRHM CR SF *S+ 8		OU9	R	<*)		R+
L										
/ FLT	271.27	302.06	30.79	ARSI CR	SQ3 SS //	0 1 4 2	P 2 BD	70 <*		HE R)
L				1A	SC	6	CV	70	C.	R*
R	271.27	302.06		HE REPLACEMENT OF SILT/SAND. SILT/SAND 2 TO 15MM THICK.						
R	284.38	284.38		REDUCED TO BQ.						
/ FAL	302.06	304.00	1.94	ARSI CR	SQ2 SS //	0 1 4 2	P 2 BD	90 >+		HE R)
L					GG3			90		
/ FAL	304.00	308.50	4.50	ARSI CR	SQ1 SS //	0 1 4 2	P 2 BD	70 >+		HE R)
L					GG3					
/ SHR	308.50	309.90	1.40	ARSI	SI/ BR SS	0 2 2	P 2 BD			HE 7)
L				1A	SC //	7			C.	R(
R	308.50	309.90		UNIT IS BORDERLINE GRM. EXTREME DEFORMATION. PY REPLACEMENT						
R	308.50	309.90		AND AS MICROVEINS.						
/	309.90	311.51	1.61	ARSI CR	SI2 //	SS 0 2 2	P 2 BD	30 <)		HE D)
L				1A	SC				C.	R(
/	311.51	316.20	4.69	BRHM CR	SI1		NQ8 P			HE R)
L				1A					C.	R(
R	311.51	316.20		CLASTS ARE ARSI IN MOD MATRIX. HIGHLY DEFORMED ARSI.						
/ SHR	316.20	325.73	9.53	ARSI CR	SI1 //	SS 0 2 2	P 2 BD	75 <*		HE R)
L				1A	SC BR				C.	R=
/ FAL	323.39	324.31	0.92	X ARSI CR	SI1 //	SS 0 2 2	R 2 BD	75 <*		HE R)
L				1A	GG5 SC BR				C.	R=
/	325.53	325.73	0.20	X ARSI CR SF	SI1 //	SS 0 2 2	R 2 BD	75 <*		HE R) <. <.
L				1A	SC BR				C.	R=
/	325.73	332.90	7.17	ARSI CR	SI1 BR SS	0 2 2	P 2 BD	85 <*		HE R)
L				1A	SC //		CV	85	C.	R=
R	325.73	332.90		LOCALLY INTENSE DEFORMATION.						
/	332.90	335.58	2.68	ARSI CR	SI1 SS BR	0 2 2	P 2 BD	60 <*		HE R)
L					SC //					
/ FAL	335.00	335.58	0.58	X ARSI CR	SI1 //	SS 0 2 2	R 2 BD	75 <*		HE R)
L					GG4					
/ FLT	335.58	394.72	59.14	ARSI CR	SI1 BR SS	0 2 2	P 2 BD	V+		HE R+ B. B.
L				1A	GG= SC //				C.	R.
R	335.58	394.72		STRONGLY DEFORMED. BEDDING FROM 60 TO 90 DEGREES. TRACES OF CP						
R	335.58	394.72		AND GL IN GZ-VEINS. MILDLY CR.						
/ FAL	353.30	353.87	0.57	X ARSI CR	SI1 BR SS	0 2 2	R 2 BD	V+		HE R+ B. B.
L					8					

[illegible]

K E Y	F R O M - T O - -L- G	I N T R E C D V ---	R D % R O C K T M R D D A G E E V R D L C T M	Q M 1 T X Q M 2 T X	T X F C % M A R G T X S C U O C H T	RI 1 ID AZM DIP QZ FL CY CA BA XX PY CP GL YY A 1 A 2 2 ID AZM DIP MG MU CL SD QS HA PR MT SL HA
/ L	469.55	469.65	0.10	X VEIN		R >9 B*
/ L	FLT 470.50	474.50	4.20	BRPM 3A	SN3 *C= + LO3 LO2	P <+ 7+ C(
/ L	470.30	470.92	0.62	X SAND 3A	// SS SC 2 4 3 5 6	R 2 RD 75 <* D* C.
/ L	471.85	474.50	2.67	X BRPM 3A	SN3 *C= + LO3 LO2	R >1 7+ C(
/ L	474.00	474.50	0.50	X VEIN		R >9 B+ Q1
/ L	SHR 474.50	475.70	1.20	CGBR 2A	*S+ IB DB *C1 LO6 KM3	P IB 65 8) C.
/ L	SHR 475.70	476.30	0.60	CGPS	SUB BR SS DB CU 2 4 4 5 6	P V(8) C.
/ L	SHR 476.30	477.30	1.00	BRPM 2A	SN6 BR *S+ + LN1 LN2	P <) 8) C.
/ L	SHR 477.30	479.20	1.90	SAND 3A	SS SC G; 2 4 4 6 5	P 2 RD 75 <* 8*
/ L	SHR 479.20	483.20	4.00	BRPM 2A	SN6 BR MP2 KL1	P #1 6) C.
R	479.20	483.20		PY AS REPLACEMENT BLEBS, MICROVEINS. SOME QZ MACROVEINING		
/ L	482.15	483.20	1.05	X BRPM SF 3A	SN4 BR *S+ KN4	R <) 8) Q(<)
R	482.15	483.20		FRAGMENTS OF QZ-SO VEINS. INTERVAL POSSIBLY FRG.		
/ L	FLT 483.20	494.00	10.80	BRHT CR SF 2A	SN1 F* R* *S=) MS7 KN2	P C- B. 6+
R	483.20	494.00		ARSI MAKES UP ARG. FRAGMENTS FILLED BY HIGH CHERT MATRIX.		
R	483.20	494.00		RAKE ARGL/CR CLASTS WITH SO BLEBS.		
/ L	489.20	489.30	0.10	X VEIN	HR	R >9 HE <+ B+ R.
/ L	FRG 489.80	490.15	0.35	X SAND 3A	MX CU G; 3 4 4 5	R 8(C.
/ L	FRG 493.00	493.30	0.30	X BRPM SF 3A	SN4 F* R* *S+ LN3	R <) 8) Q(<)
R	493.00	493.30		IDENTICAL TO BRPM FRG. 482.15-483.20M. ANGULAR TO SUBROUNDED		
R	493.00	493.30		FRG.		

553.00	553.30	SIDERITIC MATRIX.
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[illegible]

Interval	Start (m)	End (m)	Thickness (m)	Stratigraphic Unit	Lithology	Notes	Core ID	Depth (m)	Remarks
553.52 - 557.00	553.52	557.00	3.48	BRHM	*S+ R* H*	MO2 P	V)	8+	
553.52 - 557.00	553.52	557.00		SD REPLACED CLASTS.	SN2 F* DB	LP3	R*		
557.00 - 590.00	557.00	590.00	33.00	BRHM CR SF *C) R*	OS9 P	V)	6+		
557.00 - 590.00	557.00	590.00		1A *S+ =	LP+				
557.00 - 590.00	557.00	590.00		ARGL FRAGS VARIABLY CR, AND SF.	MATRIX MUDDY WITH CHERT AND				
557.00 - 590.00	557.00	590.00		ARGL FRAGMENTS.	PY VEINING, REPLACEMENT.				
577.05 - 577.20	577.05	577.20	0.15	X BRHM CR SF *C) R* BR	OS9 R	#6	6+		
579.25 - 590.00	579.25	590.00	10.75	X BRHM CR SF *C) R*	OS9 R	V)	6+		
590.00 - 601.50	590.00	601.50	11.50	CGBR SF	DB F*	LN3 P	V)	8(
590.00 - 601.50	590.00	601.50		3A	R*	LO7			
590.00 - 601.50	590.00	601.50		LITTLE CHERT REPLACEMENT BY PY.					
601.50 - 602.59	601.50	602.59	1.09	BRHT	SN1	LO9 P	<=	7+	
601.50 - 602.59	601.50	602.59		1A *C=	C KL=				
601.50 - 602.59	601.50	602.59		LARGE, ROUNDED ARGL CLASTS WITH CHERT IN MUDDY MATRIX.					
602.59 - 603.70	602.59	603.70	1.11	CGXX	*C3 F*	KL2 P	<+	6=	
602.59 - 603.70	602.59	603.70		3A	C LN7				
602.59 - 603.70	602.59	603.70		POOR SORTING SHEAR BY MUDDY MATRIX.					
603.70 - 606.55	603.70	606.55	2.85	VEIN CR	BR	0 1 2 P	#9	#=	
603.70 - 606.55	603.70	606.55		ROCK TYPE UNIDENTIFIABLE: ONLY ARGL CAN BE SEEN IN THE RUBBLE.					
606.55 - 608.99	606.55	608.99	2.44	FAUL CR GR GG9	P	<=	<+		
606.55 - 608.99	606.55	608.99		ROCK TYPE UNIDENTIFIABLE. PROBABLY BRHM.					
608.99 - 621.49	608.99	621.49	12.50	BRHM CR GR SN=	NQ9 P	V)	7+		
608.99 - 621.49	608.99	621.49		N SF	KM)				
608.99 - 621.49	608.99	621.49		PY-REPLACES SAND/SILT BEDS IN ARSI, AND AS VEINING. VARIABLY					
608.99 - 621.49	608.99	621.49		SF.					
620.40 - 620.75	620.40	620.75	0.35	X BRHM CR GR SN= BR	NQ9 R	#1	#6		

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PR-ZN-AG-BASIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE :41-DH085

COLLAR ELEVATION: 1244.36

AZIMUTH(DEG) : 0.00

GEOLOGGED BY : JWP +

TOTAL DEPTH/LENGTH : 324.31

NORTHING(- IF S): 7002370.00

VERTICAL ANGLE : -90.00

DATE (YY/MM/DD): 811012

CORE/HOLE DIAMETER : 4000

EASTING (- IF N): 436553.06

CO-ORD SYSTEM : UTM

PROJECT NUMBER : J-S

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	12.00	49.80	-87.80
2	24.00	49.90	-87.58
3	37.00	67.80	-86.50
4	49.00	79.60	-86.92
5	61.00	92.50	-86.67
6	73.00	111.40	-86.50
7	85.00	103.30	-87.00
8	98.00	97.20	-86.17
9	110.00	99.10	-86.03
10	122.00	119.10	-86.25
11	134.00	118.00	-86.17
12	146.00	119.00	-85.75
13	159.00	113.00	-86.67
14	171.00	114.00	-86.83
15	183.00	108.00	-87.47
16	195.00	135.00	-85.50
17	207.00	146.00	-85.10
18	219.00	143.10	-84.92
19	232.00	155.10	-84.53
20	244.00	156.10	-84.25
21	256.00	166.30	-84.17
22	268.00	164.40	-84.05
23	280.00	159.50	-82.00
24	289.86	160.00	-83.25
25	302.06	156.00	-82.00
26	316.38	153.00	-81.00
27	323.29	148.00	-80.50

F	I	I	E	R	V	A	L	-	CORE	T	-	%	TYPI	QUAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY														
K	L	(UNITS =	DEC.PLACE)	RECOV	M	M	ROCK	FYING	MIN	TURES	CHARACS																										
E	A	(METRIC)	FT=FOOTRIC)	ERY	0	I		TM	TM	MAT	TX	TX	F	C	%	M	ARG	/PI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-	
Y	G	F	R	O	N	-	T	O	-	T	R	T	(.)	0	X	TYPE	1	2	QM1	1	2	F	F	C	A										
K	F						ROCK	FM	RT	TM	QM2	TX	TX	S	C	O	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L						QUAL	AGE	EN	-	0	LC	-	3						2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G						DESIG	VIR	COL												STRUCTUR-2	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 0.00 THIS DATA IS ASSUMED TO BE MORE ACCURATE AND SHOULD BE USED
 R SVY 0.00 0.00 FOR PLOTTING THE SECTION.
 R SVY 0.00 0.00 THE LAST PART OF THIS HOLE WAS NOT GYRO LOGGED SO SPERRY SUN
 R SVY 0.00 0.00 SINGLE-SHOT DATA WILL BE USED TO COMPLETE THE PLOT.

/ 0.00 21.95 21.95

OVER

P

L

[illegible]

/	71.63	83.76	12.13	ARSI	SV= 77	A 1 1 J	P	2 80	68	D. D= HE D*
L				3A	SI+ DR SS					D= D(
R	71.63	83.76		SOME PY IS SEEN AS REPLACEMENT CLASTS.						
/	74.41	76.80	2.39	X ARSI	SN= BR DR		R			D= D. HE D)
L				3A	SI= SS					D(
R	74.41	76.80		THE PY IS FOUND DISS. IN THE SANDY BEDS BUT ALSO AS CLASTS.						
/	81.99	83.76	1.77	X WEDG			R			
L										
R	81.99	87.73		HALL AND ROWE STEEL WEDGE, FULL STEEPING. STARTED CORING AT						
R	81.99	87.73		81.99 BOTTOM AT 87.78. THE CORE IS REPEATED FROM 84.43 TO						
R	81.99	87.73		87.78M.						
/	83.76	115.68	31.92	BRHM	*S2 DR R*	LR8	P	CL	90 <)	D= <) HE D)
L					SS	2 0			D.	C= **
/	83.76	87.78	4.02	X WEDG			R			
L										
R	83.76	115.53		THE SN CLASTS ARE ARSI. THIS HAS CHAOTIC BEDDING AND SLUMPING						
R	83.76	115.53		FEATURES. THIS HAS NOT MOVED FAR FROM ITS SOURCE AND IS VERY						
R	83.76	115.53		SIMILAR TO THE UNIT ABOVE IT.						
R	106.50	109.60		BEDDING SHOWN BY SMALL SAND BEDS IS SEEN DIP IS 90 DEGREES.						
/	115.68	126.49	10.81	BRPM GR CR	*S= SS R*	KN3	P			D. HE *(
L					*C+	=	LO=			D(D.
R	115.68	126.49		THE FIRST CHERT CLASTS ARE FOUND HERE. BEDDING IS CHAOTIC DUE						
R	115.68	126.49		TO THE RESULT OF DERRIS FLOWS. SOME OF THE PY IS FOUND						
R	115.68	126.49		REPLACING THE CHERT PEBBLES. THE MATRIX IS MUDDY AND SANDY						
R	115.68	126.49		WHICH MAKES GREATER THAN 50% OF THE ROCK.						
R	117.04	121.31		THE CORE HAS BEEN DUPLICATED FOR THIS INTERVAL.						
/	119.18	121.31	2.13	X WEDG			R			
L										
R	119.18	121.31		HALL AND ROWE STEEL WEDGE, HALF AZM RIGHT HALF STEEPENING.						
/	126.49	139.18	12.69	BRPM GR	*S2 *R SS	MT4	P		<=	<= C(HE D)
L						2 LN)				D= D=
R	126.49	139.18		LARGER AND MORE CHERT PEBBLES ARE FOUND. THE SANDY-MUDDY MATRIX						
R	126.49	139.18		IS LESS A LOT OF THE ARGL CLASTS ARE ACTUALL ARSI CLASTS.						
R	137.46	137.46		CHANGED FROM HQ TO HQ CORE, BECAUSE NO HQ WEDGES LEFT.						
/	139.18	149.08	9.90	BRHT GR CR	*R SS	MP6	P		<(<= C. R) D.
L					H* G:	K01				C= D=
/	140.51	141.52	1.01	X WEDG			R			
L										
R	140.51	141.52		CLAPPISON WEDGE, FULL STEEPENING.						
/	143.17	143.41	0.24	X ARSR	SN3 LC	A F 3 G	R	1 80	40	L*
L				4A	SI= SS					

/	L	146.90	147.40	0.50	X ARSI 3A	S11 LM LC A E 1 F SN= SS	R 1 BD	70		HE D- D.
/	L	148.26	149.08	0.82	X SAND	G: F I 5 D	R	<(HE D*
/	L	149.08	154.68	5.60	BRHT GR 7A	*S1 SS R* *C4 P*	M02 P	<(<-	D)
R		149.08	154.68		PY IS FOUND IN THE MATRIX BUT ALSO IT IS SEEN STARTING TO					
R		149.08	150.68		REPLACE CHERT CLASTS.					
/	L	154.15	154.68	0.53	X BRHT GR GGX	*S1 SS R* GGX	M02 R	<(<-	D)
/	L	154.68	160.94	6.26	ARSI GR CB SI= SA SN)	SS A F 1 G 7	P 2 BD CV	20 <- 90		D)
R		154.68	160.94		MICROFAULTS ARE SEEN DISRUPTING THE BEDS.					
/	L	156.36	157.88	1.52	X WEDG		R			
R		156.36	157.38		CLAPPISON WEDGE FULL STEEPENING					
/	L	160.65	160.80	0.15	X SAND 8A	E F 5 G 8	R	<+		D(
/	L	160.94	174.03	13.09	BRPM GR SA	*S= SS R* JN+	JP4 P		C. <*	D(
R		160.94	174.03		TRANSPORTATION OF THIS DEBRIS FLOW WAS IN A MUD, SHOWN BY THE					
R		160.94	174.03		MATRIX. THE CLASTS ARE CHAOTICALLY DISTRIBUTED AND THE MUP					
R		160.94	174.03		FLOWS AROUND THE CLASTS.					
/ FRG	L	174.03	183.84	9.81	BRHT GR 7A	R* F* R*	L01 P JU7		C. <)	D) D.
R		174.03	183.84		PY IS SEEN DISS. BUT ALSO AS REPLACEMENT CLASTS. GR IS FOUND					
R		174.03	183.84		ALONG SHEARS AND AT THE EDGE OF CLASTS.					
/	L	174.65	176.17	1.52	X WEDG		R			
R		174.65	176.17		CLAPPISON WEDGE FULL STEEPENING.					
/	L	185.64	186.73	2.89	ARSI 2A	S11 LM SM+ SS	A E 1 F 8	P 2 BD CV	55 90	D)
/	L	186.73	195.56	8.83	BRHT GR 4A	SN= H* R* =	LT6 P JU1		C-	D+
R		186.73	195.56		LARGE CLASTS ARE PRESENT, ONE SUCH CLAST AT 192.55 TO 192.94M,					
R		186.73	195.56		SHOULD BE NOTED. IT IS A CONGLOMERATE WITH A SANDY-PEBBLY					
R		186.73	195.56		MATRIX.					
/	L	192.94	194.46	1.52	X WEDG		R			

[illegible]

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 314MH06P
TOTAL DEPTH/LENGTH : 869.93
CORE/HOLE DIAMETER : 4000COLLAR ELEVATION: 1275.94
NORTHING(- IF S): 7002472.00
EASTING (- IF W): 436496.25AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : BHO +
DATE (YY/MM/DD): 810000
PROJECT NUMBER : J-S1

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	146.90	-89.47
2	61.00	169.10	-87.40
3	91.00	151.30	-85.47
4	122.00	131.50	-86.75
5	152.00	124.20	-86.42
6	183.00	121.80	-86.10
7	213.00	117.80	-86.00
8	244.00	117.20	-85.38
9	274.00	120.10	-84.13
10	305.00	132.80	-84.92
11	335.00	151.50	-84.20
12	366.00	164.00	-80.53
13	396.00	164.50	-77.00
14	427.00	157.50	-74.20
15	457.00	154.20	-69.00
16	488.00	154.30	-64.80
17	518.00	154.80	-58.13
18	549.00	158.60	-49.80
19	579.00	162.80	-46.00
20	610.00	166.30	-43.00
21	640.00	165.90	-40.50
22	671.00	166.60	-39.00
23	701.00	167.90	-37.33
24	724.00	167.30	-37.00
25	735.79	166.50	-37.50
26	747.98	165.00	-36.50
27	760.17	166.50	-36.50
28	772.36	167.00	-36.67
29	784.56	166.00	-36.50
30	796.75	165.00	-36.00
31	808.94	164.00	-36.00
32	821.13	166.00	-36.00

33	833.32	165.00	-35.00
34	845.52	166.50	-34.00
35	851.61	166.00	-33.75

R HED

NO CORE

F - INTERVAL - CORE T- %		TYPE- DUAL TEX- GRAIN		PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY	
K L (UNITS = DEC. PLACE) RECOV- M N ROCK FLYING MIN TURES CHARACS	E A (MT=METRIC FT=FOOTRIC) ERY 0 1	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A
Y G F R D K - T D - I N T (.)	D X TYPE	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A	1 2 0M1 1 2 F F C A
K F	ROCK FM RT	1M 0M2 TX TX S C O O CHT	T ID STK DIP	MG MU CL SD QS HA PR MT SL HA	
F L	DUAL AGE EN- J LC- 3	3 4 0 /	2 AZM RT H H H H H H H H	1 1	
Y G	DESIG VIR CIL	K C	STRUCTUR-2 A A A A A A A A	2 2	

R SVY 0.00 0.00 SURVEY DATA DONE BY GYROSCOPIC DIIRECTIONAL SURVEY

R SVY 0.00 0.00 SPERRY SUN OF CANADA.

R SVY 0.00 0.00 GYROSCOPIC DATA ENDS AT 724.00 M. FROM 735.79 M TO 869.93 M

R SVY 0.00 0.00 WAS DONE BY SPERRY SUN MULTI-SHOT SURVEY.

R SVY 869.93 869.93 END OF WEDGED HOLE A.

R SVY 0.00 0.00 THE GYROSCOPIC DIRECTIONAL SURVEY IS CONSIDERED MORE ACCURATE

R SVY 0.00 0.00 THAN SPERRY SUN SINGLE AND MULTI-SHOT DATA. THEREFORE THE

R SVY 0.00 0.00 SURVEY INFORMATION IN S000-S035 SHOULD BE USED FOR PLOTTING

R SVY 0.00 0.00 PURPOSES.

R SVY 735.79 851.61 10 DEGREES WAS ADDED TO ORIGINAL MULTI-SHOT DATA TO NULLIFY

R SVY 735.79 851.61 THE MAGNETIC DISCREPANCIES. ORIGINAL DATA MAY BE OBTAINED BY

R SVY 735.79 851.61 SUBTRACTING 10 DEGREES FROM THE AZIMUTH.

/ 0.00 348.69 348.69 MISS P

/ 348.69 357.16 8.47 BRPM N08 P

L 5A *S- 2 1) LN=

/ 354.50 357.16 2.66 X ARSI GR SN= RD 0 3 = 3 R 2

L 2A

R 354.50 357.16 FRAG CUT BY NS VNS WITH MNR PYR. PYR ALSO DISSEM IN

R 354.50 357.16 SAND LAYERS.

/ 357.16 364.40 7.24 BRHT NP6 P

L 6A *S) 2) LP3

/ 364.40 367.75 3.35 BRHT KG4 P

L 6A 5 IM6

R 364.40 367.75 SANDY INTERVAL (SANDY MIX).

/ 367.75 379.30 11.55 BRHT DS7 P

L 4A *S+ 2) + M02

/ 379.30 391.00 11.70 BRHM CH GR RS9 P

L 5A *S) 2) LN)

R 379.30 391.00 SOME ARGL FRAGS ARE CARB (BLK)

R 379.30 391.00 A COUPLE OF NARROW (UP TO 5 CM) SAND ZONES ARE PYRITIZED.

/ 379.60 383.15 3.55 X FAUL GR GG1 R

L 379.60 383.15 APPROX 60% OF INTV RUBBLY CORE-PROBABLE FAUL-LOCALLY GR (ALONG

R 379.60 383.15 SLIPS).

/ 391.00 399.90 8.90 BRPM TT8 P

L 4A 3 JN1

/ 399.90 404.90 5.00 X FAUL GR GG1 R

L 4A 3 JN1

/ 404.90 409.90 5.00 X FAUL GR GG1 R

L 4A 3 JN1

G E O L O G

K	F	F	R	U	M	-	T	O	-	I	R	T	RECOV	MD	%	RUCK	TM	TM	QNT	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																																																	

R 606.35 619.02 CGCP-UNCLEAR WHETHER CGCP IS ORIGINAL SEDIMENT OR FRAGS.
R 606.35 619.02 -PROBABLY FRAG.

/ FRG 609.50 615.54 6.04 X CGCP R
L

R 609.50 615.54 INTERVAL DOMINATED BY CGCP PROBABLE FRAG. POSSIBLY
R 609.50 615.54 SEVERAL FRAGS.

/ 619.02 636.82 17.80 BRHM DU9 P >+ D)
L 5A 3 + + LO=
R 619.02 636.82 BRECCIATED INTV 626.67-627.79 INFILLED WITH QUARTZ.

/ 636.82 641.82 5.00 BRHT SD S*(MQ4 P D.
L *C) H* (KN6 R* D-

/ FGT 639.57 640.47 0.90 X ARSI R
L

/ 641.12 641.82 0.70 X VEIN QZ R V/ 84 D- D-

R 636.82 641.82 BRECCIA MIX MATERIAL DOMINANTLY CONSISTS OF ANGULAR SAND TO
R 636.82 641.82 GRIT SIZE CHERT FGTS ALTERATION RIMS COMMON SOME SIDERITIZED
R 636.82 641.82 ANGULAR FGTS IN MIX TRACE SL AND GL IN MIX

/ 641.82 656.40 14.58 SAND SD *CI MX G; H K 4 O 3 P U >+ D. D.
L 6A B* F* 4 7 D+ D-
R 641.82 656.40 THIS SEQUENCE MAY REPRESENT 2 BOUMA AB CYCLES. NOTABLE FEATURES
R 641.82 656.40 OF SAND UNITS INCLUDE 20% ANGULAR BLEACHED CH FRAGS.
R 641.82 656.40 ARGILLITE FRAGS & MIX PREFERENTIALLY SIDERITIZED.

R 641.82 656.40 MGR SL DISSEM LOCALLY IN MIX.
R 641.82 656.40 MGR SL, GL & PY IN QTZ VNS.

/ 643.30 644.92 1.62 X CGXX SD MQ3 R
L 6A 8 C MN7 D=
R 643.30 644.92 SIDERITE OCCURS AS DISSEM & ALSO AS VEINLETS CROSS-CUTTING FRAGS

/ 646.00 646.90 0.90 X CGXX LN3 R D. D.
L 6A 6 C LN7 D-

/ 655.15 656.40 1.25 X CGXX LQ2 R D+ D+
L 6A 5 C LQ6

/ 656.40 664.76 8.36 BRHT *S= QS6 P D* D+
L 5A 2 = IN2
R 656.40 664.76 FINE MIX CONSISTS OF GRIT SIZE ANGULAR FGTS-BLEACHED RIMS COMMON
R 656.40 664.76 . PY SELECTIVELY COATS OR REPLACES PEBBLE SIZE CHT FRAGS.

/ 664.76 669.06 4.30 BRHM CR QS9 P
L JK)

/ 669.06 678.70 9.64 BRHT QS7 P <= #1 #)
L LQ3 #)

[illegible]

[illegible][illegible]

R	800.40	802.73	LOCAL BRECCIATION AND MINOR FOLDING. UPPER 0.7 M BRECCIATED
R	800.40	802.73	AND INFILLED WITH PY AND GREY METALLIC MIN-POSSIBLY STIBNITE.
R	800.40	802.73	INTV COMPRISES ALTERNATING CHT & SULFIDE-RICH BANDS(PYR, SL,
R	800.40	802.73	CHT, CALCITE).

[illegible]

G F D L O G

A UMM	RQD	SP.GR.
A TYP	CM	SG
A AMH	B-B	WEIGH
A LAB	FLD	FLD

R ASY 0.00 0.00 RQD=RECOVERY(C17-20) IS MEASURED IN CM BLOCK TO BLOCK(B-B)

R ASY 0.00 0.00 RQD=ROCK QUALITY DESIGNATOR(C27-32) MEASURED IN CM BLOCK TO BLOCK

R ASY 0.00 0.00 RQD IS THE TOTAL LENGTH (BETWEEN BLOCKS) OF PIECES OF CORE

R ASY 0.00 0.00 AT LEAST 2-1/2 TIMES DIAMETER OF CORE TO NEAREST CM, DIVIDED

R ASY 0.00 0.00 BY LENGTH OF INTERVAL = BLOCK(TO) MINUS BLOCK(FROM) TIMES 100

R ASY 0.00 0.00 CM INDICATES THAT MEASUREMENTS ARE IN CM'S WHICH ARE TO BE RIGHT

R ASY 0.00 0.00 JUSTIFIED AGAINST THE DOUBLE VERTICAL LINE AT RIGHT MARGIN

R ASY 0.00 0.00 OF EACH FIELD.

R ASY 0.00 0.00 B-B=BLOCK-TO-BLOCK (DRILLERS BLOCKS). ENTER METRAGE OF ONE BLOCK

R ASY 0.00 0.00 AS THE TO OF ANY INTERVAL AND THE METRAGE OF THE NEXT BLOCK.

R ASY 0.00 0.00 ADDITIONAL POINTS (FROM-TO'S) CAN BE ESTABLISHED BETWEEN

R ASY 0.00 0.00 BLOCKS TO BRACKET SPECIFIC INTERVALS OF LOCALIZED POOR

R ASY 0.00 0.00 RECOVERY. B-B IS ENTERED RIGHT JUSTIFIED IN EACH FIELD IN

R ASY 0.00 0.00 THE AMH HEADER.

R ASY 0.00 0.00 THE FIRST INTERVAL, THROUGH THE OVERBURDEN, WITH ZERO RECOVERY,

R ASY 0.00 0.00 SHOULD BE ENTERED FIRST -- SEE BELOW.

A 100 348.69 350.22 153 156

A 100 350.22 351.74 152 143

A 100 351.74 355.09 271 166

A 100 355.09 358.14 252 72

A 100 358.14 361.49 298 228

A 100 361.49 364.85 278 113

A 100 364.85 366.37 00 00

A 100 366.37 368.20 134 78

A 100 368.20 369.72 102 13

A 100 369.72 372.77 267 110

A 100 372.77 375.82 189 99

A 100 375.82 378.56 240 97

A 100 378.56 379.78 82 12

A 100 379.78 381.30 121 27

A 100 381.30 383.15 130 00

A 100 383.15 385.57 183 51

A 100 385.57 387.10 00 00

A 100 387.10 388.32 69 00

A UMM	ROD	SP.GR.
A TYP	CM	SG
A MTH	H-B	WEIGH
A LAB	FLD	FLD

A 100	388.32	389.84	68	00
A 100	389.84	392.28	192	105
A 100	392.28	395.34	262	57
A 100	395.33	396.85	119	31
A 100	396.85	397.76	78	19
A 100	397.76	399.90	172	42
A 100	399.90	402.95	263	145
A 100	402.95	405.99	282	147
A 100	405.99	407.52	153	117
A 100	407.52	408.74	00	00
R ASY	407.52	408.74	WEDGE	
A 100	408.74	409.65	53	26
A 100	409.65	411.18	132	64
A 100	411.18	413.61	192	70
A 100	413.61	416.66	295	192
A 100	416.66	418.95	218	92
A 100	418.95	419.71	48	00
A 100	419.71	420.32	7	00
A 100	420.32	421.34	149	66
A 100	421.34	423.76	184	98
A 100	423.76	425.81	172	58
A 100	425.81	426.42	50	17
A 100	426.42	428.85	210	91
A 100	428.85	431.90	305	198
A 100	431.90	432.51	35	00
A 100	432.51	434.22	171	140
A 100	434.22	434.40	18	00
A 100	434.40	436.73	234	78
A 100	436.73	439.83	298	207
A 100	439.83	441.05	118	100
A 100	441.05	441.96	00	00
A 100	441.96	442.87	75	15
A 100	442.87	444.40	143	106
A 100	444.40	447.90	303	210
A 100	447.90	451.10	305	170
A 100	451.10	453.24	182	117
A 100	453.24	456.29	305	116
A 100	456.29	459.33	304	179
A 100	459.33	462.17	250	126
A 100	462.17	465.28	311	207
A 100	465.28	468.48	302	80
A 100	468.48	470.31	181	69
A 100	470.31	472.74	231	96
A 100	472.74	473.35	48	00
A 100	473.35	473.66	22	00
A 100	473.66	474.57	44	00
A 100	474.57	475.18	46	00
A 100	475.18	477.01	181	27
A 100	477.01	477.47	46	25
A 100	477.47	480.36	289	198
A 100	480.36	483.41	292	192

A UMM				ROD	SP. GR.
A TYP				CM	SG
A MTH				d-B	WEIGH
A LAB				FLO	FLO
A 100	483.41	485.55	210	59	
A 100	485.55	486.77	119	00	
A 100	486.77	487.98	98	13	
A 100	487.98	489.20	110	33	
A 100	489.20	489.81	53	32	
A 100	489.81	492.25	224	61	
A 100	492.25	493.17	85	00	
A 100	493.17	494.08	68	00	
A 100	494.08	495.91	162	65	
A 100	495.91	498.95	295	159	
A 100	498.95	502.01	296	179	
A 100	502.01	505.05	291	114	
A 100	505.05	508.10	283	141	
A 100	508.10	510.24	191	89	
A 100	510.24	513.28	297	215	
A 100	513.28	516.33	300	146	
A 100	516.33	518.15	183	138	
A 100	518.15	519.63	124	43	
A 100	519.63	522.12	202	72	
A 100	522.12	523.95	159	57	
A 100	523.95	526.39	244	164	
A 100	526.39	529.44	305	221	
A 100	529.44	531.83	244	107	
A 100	531.83	534.01	196	105	
A 100	534.01	537.06	289	120	
A 100	537.06	540.11	305	178	
A 100	540.11	543.15	301	139	
A 100	543.15	545.59	221	65	
A 100	545.59	548.64	273	140	
A 100	548.64	550.77	205	94	
A 100	550.77	553.21	214	89	
A 100	553.21	553.82	61	39	
A 100	553.82	554.43	59	59	
A 100	554.43	556.87	241	207	
A 100	556.87	559.92	294	240	
A 100	559.92	562.97	295	260	
A 100	562.97	566.01	291	242	
A 100	566.01	569.06	290	216	
A 100	569.06	572.11	295	266	
A 100	572.11	575.16	294	257	
A 100	575.16	578.21	291	229	
A 100	578.21	581.25	286	188	
A 100	581.25	583.39	176	224	
A 100	583.39	584.30	78	28	
A 100	584.30	584.91	40	21	
A 100	584.91	585.52	49	00	
A 100	585.52	586.13	28	00	
A 100	586.13	586.44	31	13	
A 100	586.44	587.55	91	38	
A 100	587.55	588.87	137	132	
A 100	588.87	590.40	133	121	

A UMM	GRD	SP.GR.
A TYP	CM	SG
A MTH	FT	WEIGH
A LAB	FLD	FLD

A 100	590.40	593.14	239	164
A 100	593.14	596.19	297	263
A 100	596.19	599.24	303	218
A 100	599.24	602.28	303	176
A 100	602.28	604.42	214	150
A 100	604.42	606.86	224	96
A 100	606.86	609.90	302	184
A 100	609.90	613.26	298	243
A 100	613.26	614.78	136	68
A 100	614.78	615.39	61	15
A 100	615.39	616.31	92	59
A 100	616.31	617.52	87	39
A 100	617.52	619.05	132	67
A 100	619.05	620.57	126	57
A 100	620.57	622.10	148	57
A 100	622.10	623.62	136	81
A 100	623.62	625.14	102	14
A 100	625.14	626.67	153	133
A 100	626.67	627.89	96	15
A 100	627.89	628.80	60	00
A 100	628.80	630.33	147	51
A 100	630.33	631.85	151	37
A 100	631.85	633.37	149	136
A 100	633.37	634.90	153	36
A 100	634.90	636.12	97	34
A 100	636.12	637.95	167	78
A 100	637.95	639.47	152	109
A 100	639.47	640.84	116	62
A 100	640.84	642.44	147	119
A 100	642.44	644.35	153	115
A 100	644.35	645.87	141	69
A 100	645.87	647.40	145	79
A 100	647.40	648.92	143	41
A 100	648.92	650.44	144	81
A 100	650.44	651.97	150	134
A 100	651.97	653.49	152	108
A 100	653.49	655.02	153	78
A 100	655.02	656.54	152	78
A 100	656.54	658.06	130	00
A 100	658.06	659.59	143	56
A 100	659.59	660.81	112	24
A 100	660.81	662.33	152	124
A 100	662.33	663.85	152	120
A 100	663.85	665.38	148	78
A 100	665.38	666.90	142	29
A 100	666.90	667.51	43	00
A 100	667.51	668.43	74	00
A 100	668.43	669.95	144	80
A 100	669.95	671.47	129	97
A 100	671.47	672.69	122	101
A 100	672.69	674.22	125	97

A UMM
A TYP
A MTH
A LABRND
CM
N-B
FLDSP.GR.
SG
WEIGH
FLD

A 100	674.22	675.74	152	116
A 100	675.74	677.27	142	62
A 100	677.27	678.79	142	74
A 100	678.79	680.31	152	129
A 100	680.31	680.62	24	24
A 100	680.62	682.14	152	148
A 100	682.14	683.67	152	123
A 100	683.67	685.19	148	118
A 100	685.19	686.41	122	97
A 100	686.41	687.93	146	111
A 100	687.93	689.46	146	155
A 100	689.46	690.98	149	119
A 100	690.98	691.59	61	36
A 100	691.59	693.12	153	81
A 100	693.12	694.64	152	120
A 100	694.64	696.16	145	99
A 100	696.16	697.69	156	101
A 100	697.69	699.21	151	71
A 100	699.21	700.74	141	31
A 100	700.74	702.26	144	95
A 100	702.26	703.78	148	65
A 100	703.78	705.31	153	113
A 100	705.31	706.98	143	96
A 100	706.98	708.66	145	107
A 100	708.66	710.18	122	70
A 100	710.18	711.71	153	118
A 100	711.71	713.23	146	142
A 100	713.23	714.76	151	109
A 100	714.76	716.28	142	108
A 100	716.28	718.41	213	193
A 100	718.41	721.46	305	242
A 100	721.46	724.51	286	162
A 100	724.51	727.56	303	149
A 100	727.56	730.61	305	166
A 100	730.61	733.65	301	213
A 100	733.65	736.70	294	223
A 100	736.70	739.75	300	256
A 100	739.75	741.58	175	126
A 100	741.58	743.10	146	91
A 100	743.10	744.93	172	40
A 100	744.93	745.24	30	00
A 100	745.24	747.37	188	114
A 100	747.37	748.89	132	00
A 100	748.89	751.94	289	141
A 100	751.94	754.99	294	265
A 100	754.99	758.04	297	244
A 100	758.04	761.09	286	137
A 100	761.09	764.13	304	247
A 100	764.13	767.18	300	279
A 100	767.18	770.23	281	260
A 100	770.23	773.28	305	269

A DMM	RED	SP.GR.
A TYP	CM	SG
A MTH	B-B	WEIGH
A LAB	FLD	FLD

A 100	775.26	776.33	305	238
A 100	776.33	779.37	304	269
A 100	779.37	782.42	280	159
A 100	782.42	785.47	305	249
A 100	785.47	788.52	305	227
A 100	788.52	791.57	296	280
A 100	791.57	794.61	304	279
A 100	794.61	797.66	301	255
A 100	797.66	800.40	272	198
A 100	800.40	803.45	305	251
A 100	803.45	806.50	292	184
A 100	806.50	809.55	283	143
A 100	809.55	812.60	288	167
A 100	812.60	815.95	313	186
A 100	815.95	819.00	305	251
A 100	819.00	821.44	207	78
A 100	821.44	824.48	304	95
A 100	824.48	827.53	305	202
A 100	827.53	828.45	92	84
A 100	828.45	831.19	239	157
A 100	831.19	834.24	299	216
A 100	834.24	836.98	267	229
A 100	836.98	838.20	122	111
A 100	838.20	840.33	203	101
A 100	840.33	843.38	305	270
A 100	843.38	846.43	301	193
A 100	846.43	849.48	295	195
A 100	849.48	852.53	285	201
A 100	852.53	853.74	121	69
A 100	853.74	855.57	160	118
A 100	855.57	858.62	305	233
A 100	858.62	861.71	302	157
A 100	861.71	862.93	120	83

R SUM TARGET: SOUTH ZONE. APPROX 615M BENCH LEVEL, 64M WEST OF DDH 568

R SUM . IMPRESSIONS ON MINERALIZED ZONES.

R SUM (1) BANDED SL GENERALLY TENDS TO BE YW AND LIGHT BROWN. A LATE

R SUM PHASE OF SL OCCURS IN LATE VEINS WITH QTZ AND CALCITE AND IS

R SUM M-DK BN IN COLOR. THIS LATE SL (REMobilized) IS MINOR).

R SUM (2) GALENA OCCURS IN 3 PRINCIPLE MODES

R SUM A. LAMINAE

R SUM B. LATE VEINS WITH QTZ AND CALCITE-MINOR.

R SUM C. BRECCIA FILLING ASSOCIATED WITH BRECCIATED CHT BANDS.

R SUM

-THIS MAY SUGGEST THAT GL IS REMOBILIZED.

R SUM

(3) PYR OCCURS AS LAMINAE (CLUSTERS OF XLS PARALLEL TO BANDING)

R SUM

AND AS DISSEM GRAINS THROUGHOUT MINERALIZED ZONES.

R SUM

(4) STYLOLITES OCCUR OCCASIONALLY, PARTICULARLY IN CHT BANDS. PY

R SUM

, GL, AND SL COMMONLY OCCUR ALONG STYLOLITES (REMOBILIZED).

R SUM

(5) AN UNIDENTIFIED GREY MINERAL OCCURS TOWARDS THE BASE OF THE

R SUM

SECOND DRE ZONE. MINERAL IS STEEL GY, PRISMATIC XLS, WITH

R SUM

VESTICAL STRIATIONS, HARDNESS APPROX 4, STREAK GY, OCCURS WITH

R SUM

PYRITE AS FILLING IN BRECCIATED CHT ZONE, AND ALSO IN LATE VEINS

R SUM

WITH QTZ AND CALCITE. XLS MAY FORM RADIATING AGGREGATES.

R SUM

POSSIBLY STIBITE. LESSER POSSIBILITY IS RUBY SILVER.

R SUM

(6) CHT BANDS UNDERGO BRITTLE DEFORMATION ARE OCCASIONALLY

R SUM

BRECCIATED. TENSION FRACTURES ARE COMMON AND ARE GENERALLY

R SUM

FILLED WITH QTZ VEINS WITH MINOR CALCITE. FRACTURES ARE GENERALLY

R SUM

PERPENDICULAR TO BDG.

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-7N-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81ANB070
TOTAL DEPTH/LENGTH : 910.00
CORE/HOLE DIAMETER : NNCOLLAR ELEVATION: 1296.71
NORTHING(- IF S): 7002575.00
EASTING (- IF W): 436528.81AZIMUTH(DEG) : 171.20
VERTICAL ANGLE : -80.10
CO-ORD SYSTEM : UTMGEOLOGGED BY : PCH + JWP
DATE (YY/MM/DD): 810827
PROJECT NUMBER : J-S3

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	165.90	-80.53
2	61.00	168.40	-80.30
3	91.00	172.90	-79.73
4	122.00	168.50	-78.50
5	152.00	166.30	-77.10
6	183.00	165.90	-75.65
7	213.00	160.60	-75.50
8	244.00	158.80	-74.77
9	274.00	156.00	-74.02
10	305.00	152.20	-73.43
11	335.00	150.50	-72.18
12	366.00	149.30	-70.37
13	396.00	149.20	-68.42
14	427.00	150.30	-67.95
15	440.44	148.80	-67.75
16	455.98	147.00	-66.50
17	460.25	149.00	-66.50
18	482.50	151.00	-65.50
19	491.34	148.00	-64.75
20	501.70	149.00	-64.25
21	517.25	148.00	-64.50
22	531.88	148.50	-63.50
23	549.86	145.00	-63.75
24	561.44	144.00	-63.50
25	579.12	145.00	-63.50
26	591.31	142.00	-63.50
27	620.88	152.00	-59.50
28	639.17	155.00	-55.75
29	643.43	157.00	-54.50
30	666.29	157.50	-52.25
31	693.42	152.00	-50.50
32	710.79	148.00	-50.00

33	732.43	152.00	-47.00
34	748.59	152.00	-45.25
35	760.48	150.00	-44.00
36	795.09	142.00	-39.00
37	798.88	146.00	-39.00
38	804.67	146.00	-38.50
39	819.91	146.00	-38.00
40	835.15	146.00	-37.00
41	850.39	143.50	-36.00
42	865.63	145.00	-36.00
43	880.87	148.00	-35.00
44	896.11	143.00	-35.00

F - I N T E R V A L - C O R E										1 - %	T Y P I - Q U A L T E X - G R A I N				PGI	S T R U C T U R - 1				A L T E R A T I O N				M I N S		O R E - T Y P E				M I N S		S U M M A R Y										
K	L (U N I T S = . D E C . P L A C E) R E C D V -					M	M	R O C K		F	Y I N G	M I N	T U R E S	C H A R A C S																												
E	A (M T = M E T R I C F T = F O O T R I C) E R Y					U	I				I N	I N	M A T	T X	T X	F	C	%	M	A R G	/ R I	T	I D	S T K	D I P	A	A	A	A	A	M I N	A	A	A	A	M I N	-	-	-	-		
Y	G	F R O M - T O - I N T (.)					D	X	T Y P E		1	2	Q M 1	1	2	F	F	C	A				1		A Z M	R T	D Z	F L	C Y	C A	B A	X X	P Y	C P	G L	Y Y	A	1	A	2		
-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
K	F							R O C K	F M	R T	T M	Q M 2	T X	T X	S	C	O	O	C H T				T	I D	S T K	D I P	M G	M U	C L	S D	Q S	H A	P R	M T	S L	H A						
E	L							Q U A L	A G E	E N -	O	L C -	3	3	4	0	/						2		A Z M	R T	H	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G							D E S I G		V I R	C O L								C																					2	2	

R SVY 0.00 0.00 DATA FROM GYROSCOPIC DIRECTIONAL SURVEY
 R SVY 0.00 0.00 THIS DATA IS CORRECT AND WILL BE USED FOR PLOTTING THE SECTION
 R SVY 440.44 910.44 ONLY SPERRY SUN SINGLE-SHOT. DATA IS AVAILABLE FOR BRANCH HOLE
 R SVY 440.44 910.44 70A AND THIS WILL BE USED TO COMPLETE THE SURVEY FILE.
 R SVY 440.44 440.44 BEGINNING OF WEDGED HOLE A.
 R SVY 440.44 440.44 HALL AND ROWE STEEL WEDGE, FULL AZM LEFT.
 R SVY 910.44 910.44 END OF WEDGED HOLE A.

/ 0.00 440.44 440.44 MISS P

/ 440.44 445.70 5.26 SAND CH2 G; J L 1 M P
 L 5A 7 C

/ 440.44 442.40 1.96 X SAND CH2 G; J L 1 M R V=
 L 5A 7 C V)

/ 445.70 453.26 7.56 BRHT NS8 P
 L 2 = C MN1

/ 453.26 457.39 4.13 BRHT S9 P
 L 3A C JL=

/ 457.39 459.33 1.94 ARSI SI1 LM P 1
 L 3A

/ 459.33 460.18 0.85 ARSN SN4 // F J 2 J P
 L 5A C

/ CON 460.18 461.58 1.40 BRHT SH= NP8 P CN 66
 L 2 = C KN1

/ 461.58 472.84 11.26 BRHT CR 2 OTX P
 L 2A C JM) C* V*
 R 461.58 472.84 SL VEINLET (REDDISH BROWN COLOUR) WITH SILICIFIED ENVELOPE
 R 461.58 472.84 AT 466.8 M.

/ 465.60 465.12 1.52 X WEDG R

/ 465.60 465.12 1.52 X WEDG R

/	L	595.00	611.50	16.50	X ARSN	SI3 LR SC SN+	R	2 LM 4 BD	U52
/	L	604.72	605.94	1.22	X WEDG		R		
/	L	620.40	628.92	8.52	X BRHM		NQX KKC	P	
/	L	628.92	629.72	0.80	X SAND	// F H 8 H 9 C	R	BD	40
/	L	629.72	661.70	31.98	ARSI	SI2 LM	P	2 BD	
/	L	639.17	639.17	0.00	X ARSI	SI2 LM	R	2 BD	40
/	L	644.35	644.35	0.00	X ARSI	SI2 LM	R	2 BD	45
/	L	646.18	647.70	1.52	X WEDG		R		
/	L	654.10	654.10	0.00	X ARSI	SI2 LM	R	2 BD	47
/	L	656.95	661.70	4.75	X BRHM	*B+ +	DT9 JN+	R	
/	L	661.70	663.15	1.45	CGPS	*C2 B* F* H L 3 N R* 3 O	P		
/	L	663.15	664.85	1.70	MISS		P		
R	EDT	663.15	664.85		MISSING INTERVAL.				
/	L	664.85	667.70	2.85	CGPS	B* F* H L 3 O R* 3 O	P		
R		664.85	667.70		BOTH CGPS UNITS APPEAR TO REPRESENT SEPARATE DEPOSITIONAL GRAVITY FLOW EVENTS OF SIMILAR CHARACTER - MAY HAVE INCORPORATED ANGULAR ARGL CLASTS.				
R		664.85	667.70						
R		664.85	667.70						
/	L	667.70	671.64	3.94	BRHM 5A	*S2 2	PS9 KM+	P	
/	L	671.64	672.96	1.32	BRHT		OP6 LN2	P	B-
/	L	672.96	674.89	1.93	CGXX 7A	D M 4 N 4 C	P		
R		672.96	674.89		CHARACTERIZED BY BLACK WELL ROUNDED MED SIZE PEBBLES (DEPOSITIONAL CONTACTS).				
R		672.96	674.89						

[illegible]

[illegible][illegible]

G E O L O G

R SUM SOUTH ZONE 1 BA 32.85%

R SUM PB 3.49%

R SUM ZN 7.55%

R SUM

R SUM SOUTH ZONE 2 BA 21.86%

R SUM PB 10.89%

R SUM ZN 12.22%

R SUM

R SUM CORE RECOVERY WAS EXCELLENT THROUGHOUT BOTH ORE ZONES.

R SUM IT WAS APPROXIMATELY 98% IN BOTH ZONES.

R SUM

R SUM

R SUM SPECIAL REMARKS

R SUM

R SUM DRILLING

R SUM THIS HOLE, 70A WAS WEDGED OFF OF HOLE 70 AT 440.44 M.

R SUM A TOTAL OF 10 WEDGES WERE UTILIZED IN THE DRILLING AND COMPLETION

R SUM OF THIS HOLE. AT 754.08M THE HOLE WAS REDUCED FROM NQ TO BQ

R SUM SIZE TO REDUCE TORQUE ON THE DRILL RODS.

R SUM

R SUM MINERALIZATION

R SUM MINERALIZATION WAS MAINLY BARITIZATION A LARGE DEGREE OF

R SUM SILIFICATION. SOME MINOR FOLDS WERE SEEN, BUT MAINLY THE BEDS

R SUM AND LAMINATIONS WERE CONVOLUTED. IN S-1 THE BEDDING DIP VARIED

R SUM GREATLY BUT IN S-2 THE BEDDING DIPS WERE MORE CONSISTANT.

R SUM

R SUM CONCLUSIONS

R SUM THIS HOLE WAS SUCCESSFUL IN HITTING THE ORE ZONE AND PROVING UP

R SUM THE ORE.

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.
JASOB PB-ZN-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 81ANH97R
TOTAL DEPTH/LENGTH : 181.79
CORE/HOLE DIAMETER : 60

COLLAR ELEVATION:	1296.37
NORTHING (- IF S):	7002568.00
EASTING (- IF W):	436555.31

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AZIMUTH( DEG ) : 355.00
VERTICAL ANGLE : -83.00
CO-ORD SYSTEM : UTM

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GEOLOGGED BY : JDK + JWP
DATE (YY/MM/DD): 810922
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
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1	27.43	0.00	-81.50
2	88.39	5.00	-81.25
3	118.26	6.00	-81.25
4	134.42	10.50	-80.30
5	143.26	13.00	-79.00
6	158.50	14.00	-79.00
7	173.43	14.00	-78.50
8	180.14	14.00	-78.50

R HED

HOLE ABANDONED DUE TO WEDGE PROBLEMS AT 182.27M.

F - I N T E R V A L -

CORE I- 2

TYPE - DAL

TEX- GRAIN

GRAIN

PGI

STRUCTUR-1

TERATION MINS

ORE-TYPE MINS

SUMMARY

[illegible]

R SVY	134.42	134.42	BEGINNING OF WEDGED HOLE A.
R SVY	134.42	134.42	HALL AND ROWE STEEL WEDGE, FLATTENING.
R SVY	182.27	182.27	CLAP RETRIEVABLE WEDGE LOST IN HOLE.
R SVY	181.79	181.79	END OF WEDGED HOLE A.

1	0.00	131.76	131.76
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MISS

P

1	131.76	132.61	0.85
---	--------	--------	------

RRHM PY GR *S1 F* R*
1A

NQ7 P
KM2

8+

1	132.61	137.77	5.16
---	--------	--------	------

SAND PY GR
4A

P 2 BD U72

82

/	132.61	137.77	5.16
---	--------	--------	------

2 BRHT PY
3A

NP5 R 3 BD
MN5

8+

1	133.29	133.59	0.30
---	--------	--------	------

X BRHT PY
3A

NPS	R
MNS	

84

/	155.46	155.94	0.48
---	--------	--------	------

X SAND PY GR
2A

R 2 BD U70

8.

Q	135.46	135.94	CORE IS BADLY BROKEN.
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G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PR-ZN-AG-BR SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 41A V H 085
TOTAL DEPTH/LENGTH : 620.27
CORE/HOLE DIAMETER : HJNCCOLLAR ELEVATION: 1244.36
NORTHING (- IF S): 7002370.00
EASTING (- IF E): 436553.06AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : JWP +
DATE (YY/MM/DD): 811101
PROJECT NUMBER : J-S1

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	12.00	49.80	-87.80
2	24.00	49.90	-87.58
3	37.00	67.80	-86.50
4	49.00	79.60	-86.92
5	61.00	92.50	-86.67
6	73.00	111.40	-86.50
7	85.00	103.30	-87.00
8	98.00	97.20	-86.17
9	110.00	99.10	-86.03
10	122.00	119.10	-86.25
11	134.00	118.00	-86.17
12	146.00	119.00	-85.75
13	159.00	113.00	-86.67
14	171.00	114.00	-86.83
15	183.00	108.00	-87.47
16	195.00	135.00	-85.50
17	207.00	146.00	-85.10
18	219.00	143.10	-84.92
19	232.00	155.10	-84.53
20	244.00	156.10	-84.25
21	256.00	166.30	-84.17
22	268.00	164.40	-84.05
23	280.00	159.50	-82.00
24	293.00	160.50	-81.08
25	305.00	164.50	-80.08
26	317.00	171.50	-79.42
27	329.00	171.50	-78.58
28	341.00	168.70	-79.00
29	354.00	170.70	-79.33
30	366.00	171.00	-79.08
31	378.00	170.10	-79.00
32	390.00	168.10	-78.75

33	402.00	164.20	-78.07
34	415.00	168.20	-77.78
35	427.00	162.30	-77.00
36	439.00	158.40	-76.03
37	451.00	157.50	-75.83
38	463.00	156.50	-75.33
39	475.00	154.60	-75.05
40	488.00	154.60	-74.75
41	500.00	152.60	-74.50
42	512.00	151.70	-73.42
43	524.00	149.80	-71.50
44	536.00	149.80	-70.47
45	549.00	147.00	-69.83
46	561.00	146.20	-68.58
47	573.00	147.10	-68.38
48	585.00	147.20	-68.17
49	597.00	148.20	-68.63
50	610.00	145.50	-68.47
51	616.00	145.50	-68.43

F - I N T E R V A L -		CORE	T- %	TYP1- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
K	L	(UNITS = . DEC.PLACE)RECOV-	M M ROCK	FLYING MIN	TURES CHARACS			H H H H H ANY	H H H ANY	ALT	ORE	
F	A	(MT=METRIC FT=FOOTRIC)	ERY	0 1	TM TM MAT TX TX F C % M ARG	/RI	T ID STK DIP	A A A A A	A MIN A A A MIN	- - -	-	
Y	G	F R O M - T O - I N T (.)	0 X TYPE	1 2 QAL	1 2 F F C A		1 AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2				

K	F	ROCK	FM	RT	TM QM2 TX TX S C O O CHT		T ID STK DIP	MG MU CL SD QS HA PR MT SL HA				
E	L	QAL	AGE	EN- N LC- 3	3 4 0 /		2 AZM RT H H H H H H H H	1 1				
Y	G	DESIG	VIR	COL	R C		STRUCTUR-2	A A A A A A A A A A	2 2			

R SVY	0.00	0.00	DATA FROM GYROSCOPIC DIRECTIONAL SURVEY.
R SVY	0.00	0.00	THIS DATA IS ASSUMED TO BE MORE ACCURATE AND SHOULD BE USED.
R SVY	282.55	282.55	THIS IS THE POINT WHERE THE BRANCH WEDGE FOR DDH 81-85A IS.
R 201	27.74	45.72	40.00-87.50 7298.50
R 202	45.72	52.12	74.00-85.33 9772.67
R 203	52.12	64.31	79.00-85.25 11636.75
R SVY	52.43	52.42	HALL AND ROWE STEEL WEDGE FULL STEEPENING.
R 204	64.31	71.02	89.00-86.50 13535.50
R 205	71.02	85.34	94.00-85.75 15644.25
R SVY	71.63	71.63	HALL AND ROWE STEEL WEDGE FULL STEEPENING.
R 206	85.34	106.98	108.00-85.50 19254.50
R SVY	87.78	87.78	HALL AND ROWE STEEL WEDGE FULL STEEPENING.
R 207	106.98	134.11	104.00-85.80 24127.20
R SVY	121.31	121.31	HALL AND ROWE STEEL WEDGE HALF AZM RIGHT, HALF STEEPENING.
R 208	134.11	137.16	118.00-86.00 27159.00
R 209	137.16	148.44	118.00-86.25 28591.75
R SVY	137.16	137.16	REDUCE FROM HQ TO MQ.
R SVY	140.51	140.51	CLAPPISON RETRIEVABLE WEDGE HALF AZM RIGHT, HALF STEEPENING.
R 210	148.44	169.47	123.00-85.50 31828.50
R SVY	156.36	156.36	CLAPPISON RETRIEVABLE WEDGE FULL STEEPENING.
R 211	169.47	185.91	137.00-86.25 35498.75
R SVY	174.65	174.65	CLAPPISON RETRIEVABLE WEDGE FULL STEEPENING.
R 212	185.01	192.63	102.00-87.25 37778.75
R 213	192.63	202.69	114.50-87.25 39559.25
R SVY	192.94	192.94	CLAPPISON RETRIEVABLE WEDGE FULL AZM RIGHT.
R 214	202.69	210.31	138.00-85.33 41352.67
R SVY	207.87	207.87	HALL AND ROWE STEEL WEDGE FULL AZM RIGHT.
R 215	210.31	219.76	125.00-85.50 43046.50
R 216	219.76	225.86	146.00-84.75 44623.25
R 217	225.86	234.79	141.00-85.00 46112.00
R 218	234.79	245.36	147.00-85.00 48068.00
R SVY	235.61	235.61	CLAPPISON RETRIEVABLE WEDGE FULL AZM RIGHT.

K	F	F	R	O	M	-	T	D	-	I	D	T	RECOV	SD	%	ROCK	TM	IM	QMI	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2		
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G																																														

R 295.38 313.26 A LOT OF VARYING CLASTS ARE PRESENT PRESENT IN THIS CHAOTIC
R 295.48 313.26 BRECCIA.

/ 301.14 302.67 1.53 X WEDG R
L

R 301.14 302.67 CLAPPISON WEDGE, HALF AZM RIGHT, HALF FLATTENING.

/ 309.30 310.19 0.89 9 VEIN QZ R V/ 85 Q* D(Q-
L

/ 313.26 315.73 2.47 ARSN GR SM1 // A I 3 J P 2 BD 65 B*
L 3A SI2 7 CV 90 C- <-

R 313.26 316.90 APPEARS TO BE DEPOSITIONAL SEQUENCE WITH DEPOSITIONAL
R 313.26 316.90 CONTACTS BETWEEN THE UNITS.

/ 315.73 315.77 0.04 ARGL A A A P
L 2A

/ 315.77 316.90 1.13 CGBR F* B* J H 4 D LO2 P <C <- Q.
L 7A 4 KN3

/ 316.90 318.29 1.39 BRXX GR *S) IM R* KO2 P 2 BD 52 R*
L 3A (L //)) KN1

R 316.90 318.29 THIS BRXX IS A DERRIS FLOW. BEDDING CAN BE SEEN, THE CLASTS
R 316.90 318.29 OF SAND AND CONG ARE IN VARIOUS BEDS. THE TRANSPORTING MEDIUM
R 316.90 318.29 WAS PROBABLY MUD FLOW.

/ 318.29 319.35 1.06 CGBR GR F* B* K M 4 D KN3 P <- <- B.
L 6A 4 KO4 C-

/ 319.35 321.56 2.21 BRHT GR *S) R* F* LP6 P Q(
L 4A SS 1) KO2 C-

/ 320.04 321.56 1.52 X WEDG R
L

R 320.04 321.56 CLAPPISON WEDGE, FULL AZM RIGHT.

/ 321.56 376.42 54.86 ARSI GR SI= (F // A F = G P 1 BD 68 <C B*
L 3A GG+ C- <C R.

R 321.56 376.42 THIS IS IN A DISTAL ENVIRONMENT, WHERE IT WAS RELATIVELY QUIET
R 321.56 376.42 TO GET NICKLY FORMED BEDS.

/ 341.99 346.10 4.11 X ARSI GR SI= (F // A F = G R 1 BD 90 <C B*
L

/ 346.10 347.47 1.37 X ARSI GR SI= (F // A F = G R 1 BD 68 <C B*
L GGX

/ 350.96 351.43 0.47 X BRPM GR IM JN4 R BD 70 Q*
L 3A

/ 351.43 352.96 1.53 X WEDG R
L

G E O L O G F O T T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASOP PR-ZE-AG-84 STF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 813NH068
TOTAL DEPTH/LENGTH : 806.81
CORE/HOLE DIAMETER : 40MMCOLLAR ELEVATION: 1275.94
NORTHING (= IF S): 7002472.00
EASTING (= IF W): 436496.25AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : DWB +
DATE (YY/MM/DD): 810000
PROJECT NUMBER : J-S2

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	146.90	-89.47
2	61.00	169.10	-87.40
3	91.00	151.30	-85.47
4	122.00	131.50	-86.75
5	152.00	124.20	-86.42
6	183.00	121.80	-86.10
7	213.00	117.80	-86.00
8	244.00	117.20	-85.38
9	274.00	120.10	-84.13
10	305.00	132.80	-84.92
11	335.00	151.50	-84.20
12	366.00	164.00	-80.53
13	396.00	164.50	-77.00
14	427.00	157.50	-74.20
15	457.00	154.20	-69.00
16	488.00	154.30	-64.80
17	518.00	154.80	-58.13
18	549.00	158.60	-49.80
19	579.00	162.80	-46.00
20	610.00	166.30	-43.00
21	640.00	165.90	-49.50
22	671.00	166.60	-39.00
23	681.84	165.80	-38.25
24	685.80	165.50	-37.00
25	697.99	166.00	-37.00
26	710.18	166.00	-36.50
27	722.57	166.00	-36.25
28	734.57	166.00	-36.00
29	746.76	166.50	-35.00
30	758.95	166.50	-35.00
31	771.84	166.50	-35.00
32	783.44	166.50	-35.00

F - INTERVAL -		CORE 1-2	TYPICAL	TEXT	GRAIN	PGI	STRUCTURE-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY																					
K	L (UNITS = DEC. PLACE)	RECOV =	MIN ROCK	FLYING	MIN TURES	CHARACS		H	H	H	H	ANY	H	H	H	ANY	ALT	ORE															
E	A (METRIC FEET)	ERY	01	TM	TM	MAI	TX	TX	F	C	%	M	ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-	
Y	G	F	R	O	M	-	T	O	-	I	N	T	(.)	D	X	T	Y	P	E	C	A										
K	F	ROCK	FM	RI	TM	Q	M2	TX	TX	S	C	O	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L	QUAL	AGE	EN	D	LC	-	3		3	4	0	/		2	AZM	RT	H	H	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G	DESIG	VIR	COL						R	C					STRUCTURE-2	A	A	A	A	A	A	A	A	A	A	A	A	A	2	2		

R SVY 0.00 681.84 DATA FOR UPPER PART OF HOLE OBTAINED FROM GYROCOMPASS SURVEY OF
R SVY 0.00 681.84 DDH 81-68A. REMAINDER OF HOLE FROM SPERRY SUN MULTI-SHOT.
R SVY 0.00 681.84 THE GYROCOMPASS DATA IS CONSIDERED MORE ACCURATE, AND SHOULD BE
R SVY 0.00 681.84 USED FOR PLOTTING PURPOSES. NO SPERRY SUN READINGS EXIST FOR
R SVY 0.00 681.84 DDH 81-68A ABOVE ITS BRANCH POINT: 681.84 M. SPERRY SUN DATA

R SVY 0.00 681.84 FOR PILOT HOLE CAN BE FOUND IN LOG FOR DDH 81-68.
R SVY 681.84 681.84 BEGINNING OF WEDGED HOLE B.
R SVY 681.84 681.84 HALL AND ROWE STEEL WEDGE - FULL FLATTENING.
R SVY 681.84 806.81 REMAINDER OF SURVEYS FROM SPERRY SUN.
R SVY 685.80 783.34 THESE AZIMUTH VALUES REPRESENT 10 DEGREES ADDED TO THE ORIGINAL
R SVY 685.80 783.34 MULTI-SHOT DATA TO COMPENSATE FOR MAGNETIC INTERFERENCE.
R SVY 685.80 783.34 TO OBTAIN ORIGINAL SURVEY DATA SUBTRACT 10 DEGREES FROM THE
R SVY 685.80 783.34 AZIMUTH.

/ 0.00 680.01 680.01 MISS P
/ 680.01 681.85 1.84 BRHM SF ST PS9 P V= #) R=
L 5A 3 JO) R=
R 680.01 681.85 HIGHLY SILICIFIED. MINOR DK BN SL RTZ OR AT 680.65M. SL, GL AND
R 680.01 681.85 PY ALL OCCUR AS REPLACEMENTS WITHIN CHERT FRAGMENTS AND TO A
R 680.01 681.85 LESSER EXTENT DISSEM IN BRECCIA MTX.

/ 681.85 683.88 2.03 ARSI SF LM ST P 2 BD T45 V+ L*
L 5A B45
R 681.85 683.88 PROBABLY DEPOSITIONAL AS CORE: BDG ANGLE PARALLELS THAT OF
R 681.85 683.88 UNDERLYING LMSX. BOTTOM CONTACT IS SLIGHTLY DISRUPTED HOWEVER.
K US1 683.88 683.88 0.00

/ 683.88 685.52 1.64 BNSX SL GL CH8 BN LM P 2 BD T45 <(< D* L+
L CB B40 L1
R 683.88 685.52 VERY SILICEOUS ZONE-SULFIDES ARE INTIMATELY INTGWN WITH LT GY
R 683.88 685.52 CHT. OCCASIONAL THICK BANDS OF DK GY CHT. SULFIDE-RICH BANDS
R 683.88 685.52 ARE CALCAREOUS.

/ 685.52 686.66 1.14 BRXK GL SL CH2 MX P <(< M2 M3
L CB M2
R 685.52 686.66 MASSIVE. LOCALLY CRINOID BEDDED WITH IRREGULAR CONVOLUTE AND
R 685.52 686.66 DISCONTINUOUS BDG. INTV DOMINATED BY IRREGULAR SL, GL & PY-RICH
R 685.52 686.66 PATCHES. CONTAINS OCCASIONAL SULFIDE AND CHT FRAGS. INTV IS
R 685.52 686.66 PROBABLY THE RESULT OF SOFT SED SLUMPING OF BNSX.

/ 686.66 689.28 2.62 BNSX GL SL CH8 LM BN P 2 BD T70 <*< L) L* L=
L CB LC T40 L2
R 686.66 689.28 VERY SILICEOUS ZONE. ALTERNATING SULFIDE-RICH BANDS AND CHT
R 686.66 689.28 BANDS. SULFIDES ARE INTIMATELY INTGWN WITH CHT AND MAY BE
R 686.66 689.28 LAMINATED IN PART. SULFIDE-RICH BANDS ARE CALCAREOUS. BEDDING
R 686.66 689.28 LOCALLY EXHIBITS SLUMP FOLDING.

/ 689.28 691.90 2.62 BNSX SL GL CH9 LM BN P 2 BD T60 <*< L* L)
L B40 L1

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-7N-AG-RA SIF DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 81B9H078
TOTAL DEPTH/LENGTH : 376.85
CORE/HOLE DIAMETER : HQ80COLLAR ELEVATION: 1296.37
NORTHING (- IF S): 7002568.00
EASTING (- IF W): 436555.31AZIMUTH(DEG) : 355.00
VERTICAL ANGLE : -83.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : JER + JOK
DATE (YY/MM/DD): 810926
PROJECT NUMBER : J-MAIN

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
---------------------------	---------------------------------------	--------------------	------------------------

1	27.43	0.00	-81.25
2	88.39	5.00	-81.25
3	118.26	6.00	-81.25
4	134.42	10.50	-80.34
5	143.25	13.00	-79.00
6	158.50	14.00	-79.00
7	170.99	16.30	-79.30
8	185.93	19.00	-79.75
9	200.56	19.00	-79.75
10	220.06	25.00	-80.10
11	231.65	21.50	-78.30
12	246.58	21.00	-78.00
13	259.99	23.50	-77.80
14	270.66	22.00	-78.00
15	285.90	22.00	-78.25
16	301.14	20.50	-77.66
17	313.64	25.00	-78.50
18	328.57	25.00	-78.66
19	344.78	26.00	-78.25
20	359.05	27.00	-78.30

F	- I N T E R V A L -	CORE	T- %	TYPI- GAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K	L (UNITS = . DEC.PLACE) RECOV-	M M ROCK	FYING MIN	TURES	CHARACS			H H H H H ANY H H H ANY	ALT ORE	
E	A (MT=METRIC FT=FOOTRIC) FRY	O I	IN IN MAT	TX TX	F C % M ARG	/RI T	ID STK DIP	A A A A A MIN A A A MIN	- - - -	
Y	G F R D M - T O - I N T (.)	D X TYPE	1 2 NM1	1 2 F F C A		1	AZM RT QZ FL CY CA BA XX PY CP GL YY	A 1 A 2		
K	F	ROCK	FM	RT	IN DM2 TX TX S C O O CHT	T	ID STK DIP MG MU CL SD QS HA PR MT SL HA			
F	L	QUAL	AGE EN- N LC- 3	3 4 0	/	2	AZM RT H H H H H H H H H	1 1		
Y	G	DESIG	VIR	COL	R C		STRUCTUR-2 A A A A A A A A A	2 2		

R SVY	134.42	134.42	BEGINNING OF WEDGED HOLE A.		
R SVY	134.42	134.42	HALL AND ROWE STEEL WEDGE FLATTENING.		
R SVY	170.99	170.99	BEGINNING OF WEDGED HOLE B.		
R SVY	170.99	170.99	HALL AND ROWE STEEL WEDGE.		
R SVY	202.08	282.08	CLAP RETRIEVABLE WEDGE, FLATTENING		
R SVY	233.78	233.78	CLAP RETRIEVABLE WEDGE. WEDGE WAS BROKEN, NO EFFECT.		
R SVY	376.85	376.85	END OF WEDGED HOLE B.		

/ 0.00 173.71 173.71

MISS

P

/ 173.71 174.74 1.03

BRHT PY GR

F* H*

NP2

P

6*

L

3A

H* 2

C N08

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PACIFIC OCEAN OIL LTD.

JASON PR-76-AG-RA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 31844085

COLLAR ELEVATION: 1244.36

AZIMUTH(DEG) : 0.00

GEOLOGGED BY : DWB + JER

TOTAL DEPTH/LENGTH : 469.04

NORTHING(- IF S): 7002370.00

VERTICAL ANGLE : -90.00

DATE (YY/MM/DD): 810000

CORE/HOLE DIAMETER : NO

EASTING (- IF W): 436553.06

CO-ORD SYSTEM :

PROJECT NUMBER : J-S2

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	12.00	49.80	-87.80
2	24.00	49.90	-87.58
3	37.00	67.80	-86.50
4	49.00	79.60	-86.92
5	61.00	92.50	-86.67
6	73.00	111.40	-86.50
7	85.00	103.30	-87.00
8	98.00	97.20	-86.17
9	110.00	99.10	-86.03
10	122.00	119.10	-86.25
11	134.00	118.00	-86.17
12	146.00	119.00	-85.75
13	159.00	113.00	-86.67
14	171.00	114.00	-86.83
15	183.00	108.00	-87.47
16	195.00	135.00	-85.50
17	207.00	146.00	-85.10
18	219.00	143.10	-84.92
19	232.00	155.10	-84.53
20	244.00	156.10	-84.25
21	256.00	166.30	-84.17
22	268.00	164.40	-84.05
23	280.00	159.50	-82.00
24	293.00	160.50	-81.08
25	305.00	164.50	-80.08
26	317.00	171.50	-79.42
27	329.00	171.50	-78.58
28	341.00	168.70	-79.00
29	354.00	170.70	-79.33
30	366.00	171.00	-79.08
31	378.00	170.10	-79.00
32	390.00	168.10	-78.75

33	402.00	164.20	-78.07
34	415.00	168.20	-77.78
35	427.00	162.30	-77.00
36	439.00	158.40	-76.03
37	451.00	157.50	-75.83
38	463.00	156.50	-75.33
39	475.00	154.60	-75.05
40	488.00	154.60	-74.75
41	500.00	152.60	-74.50
42	512.00	151.70	-73.42
43	524.00	149.80	-71.50
44	536.00	149.80	-70.47
45	549.00	147.00	-69.83
46	561.00	146.20	-68.58
47	573.00	147.10	-68.38
48	585.00	147.20	-68.17
49	594.66	145.40	-68.00
50	657.45	134.00	-68.00
51	666.60	135.00	-68.00

F	- I N T E R V A L -	CORE	T- %	TYPI- DAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY	
K	L (UNITS = . DEC. PLACE)	RECDV-	M R ROCK	FYING	MIN TURES	CHARACS		H H H H H H	ANY	H H H H H H	ANY	ALT ORE	
E	A (METRIC FT=FOOTRIC)	ERY	D I	TM TM	MAT TX TX	F C % M ARG	/RI	T ID	STK	DIP	A A A A A	MIN A A A MIN	- - -
Y	G F R O M - T O - I N T (.)	D X	TYPE	1 2	QM1 1 2	F F C A		1	AZM	RT QZ	FL CY CA BA	XX PY CP GL YY	A 1 A 2
K	F	ROCK	FM	RT	TM	Q42 TX TX	S C D O CHT	T	ID	STK	DIP	MG MU CL SD QS	HA PR MT SL HA
E	L	DUAL	AGE	FN- D	LC- 3	3 4 D	/	2	AZM	RT H	H H H H H H	H H H H H	1 1
Y	G	DESIG	VIR	COL		R C			STRUCTUR-2	A A A A A A	A A A A A	A A A A A	2 2

R SVY 0.00 585.00 DATA FROM GYROSCOPIC DIRECTIONAL SURVEY. THIS DATA IS ASSUMED
 R SVY 0.00 585.00 TO BE CORRECT AND MOST ACCURATE SO IT WILL BE USED TO PLOT
 R SVY 0.00 585.00 DRILL SECTION.
 R SVY 594.66 594.66 BEGINNING OF WEDGED HOLE B.
 R SVY 0.00 0.00 HALL AND RUDE STEEL WEDGE, PUT IN BLIND. THE PURPOSE OF THI
 R SVY 0.00 0.00 WEDGE WAS TO GO THROUGH THE ORE ZONE A SECOND TIME AND TRY A
 R SVY 0.00 0.00 GET BETTER RECOVERY.
 R SVY 594.66 669.04 SPERRY SUN SINGLE-SHOT DATA WILL BE USED TO COMPLETE THE SURVEY
 R SVY 594.66 669.04 DATA FOR PLOTTING PURPOSES SINCE THE BOTTOM PART OF THE HOLE
 R SVY 594.66 669.04 WAS NOT GYRO LOGGED.

/ 0.00 594.66 594.66 MISS P
 L
 / 594.66 597.41 2.75 LOST P
 L
 R 594.66 597.41 REAMED FOR HALL AND RUDE STEEL WEDGE.
 / 597.41 598.70 1.29 ARSN SF SN3 RD RD L C 0 4 34 P 1 RD 85 LC
 L 4A LM
 R 597.41 598.70 UNIT CONTAINS A LARGE AMOUNT OF SAND WHICH DOESN'T GENERALLY
 R 597.41 598.70 OCCUR IN DISCRETE BEDS TYPICAL OF ARSN IE. UNIT IS ESSENTIALLY
 R 597.41 598.70 A SANDY ARGILLITE. BEDDING IS SOMEWHAT IRREGULAR + COMMONLY
 R 597.41 598.70 COMPRISES ELONGATE DISCONTINUOUS + LENTICULAR MASSES OF SANDY
 R 597.41 598.70 ARGILLITE SEPARATED BY CLAY. THESE SANDY LENSES TEND TO BE
 R 597.41 598.70 CLOSELY PACKED. TEXTURE APPEARS TO SUGGEST INCIPIENT SLUMPING
 R 597.41 598.70 OF SANDY ARGILLITE UNIT. CORE: BDG ANGLE AS MEASURED FROM LONG
 R 597.41 598.70 AXES OF SAND-RICH LENSES, PARALLELS THAT MEASURED FROM
 R 597.41 598.70 ESSENTIALLY UNDISTURBED BEDS. INTV IS MODERATELY TO HIGHLY
 R 597.41 598.70 SILICIFIED.

/ 598.70 602.72 4.02 BRHM SF CB *C. R* N07 P <- L+ L) L+
 L

7	509.69	611.12	1.52	LOST	P
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[illegible]

G E O L O G

K	F	F	R	D	D	-	I	N	T	RECOV	MD	%	POCK	IN	TH	Q	M	TX	TX	F	C	%	M	ARG	RT	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2			
E	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G									R	D	D	AGE	EV	RU	LC	TH	Q	M	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA						

R 626.97 627.58 POOR RECOVERY (7%). VERY RUBBLY CORE. ALTERNATING BANDS OF
R 626.97 627.58 SALMON-COLOURED (SL-RICH) AND LT GY CHT.

/ 627.58 629.10 1.52 RMSX BA GL CH7 LC RD P 3 L1 L* L=
L 7A SF SS L)

R 627.58 629.10 PREL ALTERNATING BANDS OF CHT, ARG CHT AND POSSIBLY HIGHLY
R 627.58 629.10 SILICIFIED ARG. BEDS ARE CONVOLUTE AND LOCALLY BRECCIATED.
R 627.58 629.10 GL OCCURS LOCALLY IN BRECCIA INTERSTICES (REMOBILIZED?). BASAL
R 627.58 629.10 PART OF INTV APPEARS TO BE PARTICULARLY ARGILLACEOUS AND IS
R 627.58 629.10 PROBABLY GRADATIONAL WITH UNDERLYING ARG.

/ 629.10 631.76 2.66 ARG. SF ST= 0 3 = 3 P 1 BD 70 V= <+ L= D.
L 5A CH)
R 629.10 631.76 VERY HIGHLY SILICIFIED. BOTTOM 0.2M CONTAINS THIN CHT-PYR BANDS
R 629.10 631.76 AND IS GRADATIONAL INTO UNDERLYING UNIT.
R 631.76 631.76 EXCELLENT CORE RECOVERY CORE GENERALLY VERY COMPETENT.

/ 631.76 634.64 2.88 RMSX BA GL CH1 LM LC P 1 BD T70 L7 L= L1
L CH BD 865 L1
R 631.76 634.64 MODERATELY CALCAREOUS. HDG MODERATELY CONVOLUTE BECAUSE OF
R 631.76 634.64 SLUMPING. HENCE CAR VARIES. GL TENDS TO OCCUR IN BEDS UP TO
R 631.76 634.64 3CMS (RELATIVELY MASSIVE). SL+PYR TEND TO OCCUR IN LESS MASSIVE
R 631.76 634.64 FORM, DISSEM WITHIN BARITE BANDS.

/ 633.90 633.98 0.08 X RMSX BA GL CH1 LM LC R 1 BD T32 L7 L= L1
L
/ 634.64 637.69 3.05 RMSX GL SL CH7 LC SS P 2 BD T75 L1 D= L=
L CH LM 885 L1

R 634.64 637.69 SLIGHTLY CALCAREOUS. ALTERNATING YW AND LT-M GY CHT BANDS.
R 634.64 637.69 BANDS ARE CONVOLUTE, DISCONTINUOUS AND LOCALLY BRECCIATED,
R 634.64 637.69 PROBABLY DUE TO SLUMPING. GL COMMONLY OCCURS IN BRECCIA
R 634.64 637.69 INTERSTICES (REMOBILIZED).

/ 637.69 638.69 1.00 RMSX SL GL CH9 BD P 2 BD 80 <+ L= L= L)
L 5A L+
R 637.69 638.69 ESSENTIALLY CHT WITH LOCAL BARITE-SULFIDE LAM. LOCALLY
R 637.69 638.69 BRECCIATED. INTERSTICES INFILLED WITH SL+PYR. QTZ-FILLED
R 637.69 638.69 TENSION GASHES ARE COMMON.

/ 638.69 640.14 1.45 RMSX GL SL CH8 BD LM P 3 BD T45 L= L+ L=
L CB LC SS 860 L1

R 638.69 640.14 BANDS & LAM TEND TO BE WAVY, CONVOLUTE & DISCONTINUOUS; HENCE
R 638.69 640.14 CAR VARIES. LOCALLY BRECCIATED. SULFIDES TEND TO BE INTIMATELY
R 638.69 640.14 INTERGROWN WITH CHT. GL OCCURS LOCALLY AS LAM & AS BLEBS WITHIN
R 638.69 640.14 CHT. PYR & SL OCCUR LOCALLY IN BRECCIA INTERSTICES. AT 639.30M
R 638.69 640.14 IS A BAND OF DISSEM OK GRAINS APPROX 2MM IN DIAMETER. THESE ARE
R 638.69 640.14 ANGULAR, SILICIOUS AND EXHIBIT RHOMBIC AND HEXAGONAL FORMS. THE
R 638.69 640.14 VARIETY OF SHAPES APPEARS TO BE DUE TO CROSS-CUTTING RANDOMLY
R 638.69 640.14 ORIENTED QTZ XLS. THE FACT THAT QTZ HAS HAD THE FREEDOM TO FORM
R 638.69 640.14 FIBROUS XLS MAY HOLD GENETIC IMPLICATIONS WHICH CAN BE

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.

PAN OCEAN OIL LTD.

JASON PB-ZS-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRVERSE : 310MH068
TOTAL DEPTH/LENGTH : 726.34
CORE/HOLE DIAMETER : 40MMCOLLAR ELEVATION : 1275.94
NORTHING (- IF S) : 7002472.00
EASTING (- IF E) : 436496.25AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : DWR +
DATE (YY/MM/DD) : 810000
PROJECT NUMBER : J-S3

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	146.90	-89.47
2	61.00	169.10	-87.40
3	91.00	151.30	-85.47
4	122.00	131.50	-86.75
5	152.00	124.20	-86.42
6	183.00	121.80	-86.10
7	214.24	124.90	-85.70
8	231.34	126.00	-85.50
9	251.46	141.00	-85.50
10	287.12	160.00	-84.25
11	304.80	168.00	-82.75
12	326.14	170.00	-80.50
13	346.86	170.00	-77.75
14	382.83	168.00	-73.25
15	395.63	169.00	-72.67
16	408.12	168.00	-72.25
17	435.56	164.50	-70.25
18	454.15	164.00	-67.67
19	466.34	163.50	-67.34
20	481.58	162.00	-64.50
21	494.69	162.00	-64.00
22	508.71	162.00	-62.50
23	523.95	161.50	-61.25
24	538.89	161.50	-60.00
25	557.78	161.50	-59.00
26	575.77	160.00	-59.00
27	581.86	161.00	-58.75
28	593.45	160.00	-58.25
29	594.66	160.00	-58.50
30	606.25	160.00	-58.50
31	618.44	160.00	-58.00
32	630.63	160.00	-59.00

33	642.82	161.00	-57.50
34	655.02	161.50	-57.25
35	667.21	162.00	-57.00
36	679.40	162.00	-57.00
37	691.50	163.00	-56.75
38	703.78	163.00	-56.75
39	715.98	163.00	-56.34
40	725.12	163.50	-55.50

F - I N T E R V A L -				CORE	T- %	TYPI- QAL	TEX- GRAIN	PGI	STRUCTUR-1	ALTERATION MINS	ORE-TYPE MINS	SUMMARY
K L (UNITS = . DEC.PLACE) RECHV- M H ROCK FYTIG MIN TURES CHARACS												
E A (MT=METRIC FT=FOOTRIC) FRY D I												
Y G F R D M - T D - I N T (.) D X TYPE 1 2 QH1 1 2 F F C A												

K F				ROCK	FM	RT	TH QM2 TX TX S C D O CHT		T ID STK DIP	MG MU CL SD QS HA PR MT SL HA		
E L				QUAL	AGE EN- J LC- 3		3 4 D /		2 AZM RT H H H H H H H H H H			1 1
Y G				DESIG	VIR	COL	P C		STRUCTUR-2	A A A A A A A A A A		2 2
R SVY	0.00	218.24		READINGS FOR UPPER PART OF HOLE FROM GYROCOMPASS SURVEY OF								
R SVY	0.00	218.24		DDH 81-68A. REMAINDER FROM SPERRY SUN MULTI-SHOT.								
R SVY	0.00	218.24		THESE SURVEY DATA (S000-S040) SHOULD BE USED FOR PLOTTING								
R SVY	0.00	218.24		PURPOSES.								
R SVY	218.24	218.24		BEGINNING OF WEDGED HOLE C.								
R SVY	218.24	218.24		HALL AND ROWE STEEL WEDGE - FULL AZIMUTH RIGHT.								
R SVY	99.97	99.97		HALL AND ROWE STEEL WEDGE - FULL STEEPENING.								
R SVY	218.24	726.34		SURVEY DATA FROM SPERRY SUN MULTI-SHOT.								
R SVY	235.31	235.31		CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO RIGHT.								
R SVY	255.12	255.12		CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO RIGHT.								
R SVY	270.56	270.56		CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO RIGHT.								
R SVY	288.65	288.65		CLAP RETRIEVABLE WEDGE - HALF AZIMUTH TO RIGHT								
R SVY	288.65	288.65		AND HALF FLATTENING.								
R SVY	305.71	305.71		CLAP RETRIEVABLE WEDGE - FULL FLATTENING.								
R SVY	328.83	328.83		CLAP RETRIEVABLE WEDGE - DIP 1.50 TO FLATTEN.								
R SVY	413.92	413.92		CLAP RETRIEVABLE WEDGE - DIP 1.50 TO FLATTEN.								
R SVY	437.99	437.99		CLAP RETRIEVABLE WEDGE - DIP 1.50 TO FLATTEN.								
R SVY	467.56	467.56		CLAP RETRIEVABLE WEDGE - DIP 1.50 TO FLATTEN.								
R SVY	726.34	726.34		END OF WEDGED HOLE C.								
R SVY	351.13	351.13		CLAP RETRIEVABLE WEDGE - DIP 1.50 TO FLATTEN.								
/	0.00	217.32	217.32		MISS			P				
/	217.32	220.55	3.23		ARST		SN1 BD SS 0 3 1 3	P 2 BD	T55 <.		D.	
L					3A				B50			
R	217.32	220.55		BDG OCCASIONALLY SLIGHTLY DISRUPTED BY SOFT SED SLUMP.								
/	220.55	235.75	15.20		BRHT		*C= B* F*	OT6	P			
L					5A		*S+	2 +	MO4			
/	235.75	256.95	21.20		BRPM		*C* F* H*	OT4	P		R.	
L					4A		*S-	4 - - O	LO2			
R	235.75	256.95		BRM PYR ASSOCIATED WITH CH1 CLASTS.								
/	252.38	252.60	0.22		X SAND		G: BD 3 J 5 K	R 2 BD	U45			
L					7A		6					
R	252.38	252.60		NARROW SAND ZONE-IN PLACE-GRADES UPWARD INTO OVERLYING								
R	252.38	252.60		CLAY-RICH BRPM MIX.								
/	256.95	262.43	5.48		BRPM		*S+	PS8	P		D.	
L					4A		5 +	LL)				
/	262.43	273.30	10.87		BRPM			QT7	P		D.	
L					4A		1S-	4 - - O	LO1			

[illegible]

L 5A

R	621.12	621.67		THE CRACKLED TEXTURE REPRESENTS A SYNDEPOSITIONAL EVENT.									
/	621.67	623.01	1.34	RMSX SF 3A	LM BN	P	1 LM	U60		L7	81	L1	
L				3A GL	SS KR		2 BD	U60	D=			D.	
R	621.67	623.01		INTERBEDDED CHERT CONTENT IS 10 % OF THIS PGI.									
/	623.01	630.44	7.43	RMSX PY 3A	LM BN	P	1 LM	U65		L5	62	L2	
L				3A GL	SS		2 RN	U65	L1			D.	
R	623.01	630.44		INTERBEDDED CHERT CONTENT IS 5 % IN THIS INTERVAL.									
R	623.01	630.44		LAMINATED GALENA CONCENTRATION AT CONTACT WITH CHERT.									
R	623.01	630.44		CARBONATE PRESENT IN BLEDERS AND STRINGERS.									
/	624.75	625.15	0.40	X CHER PY	PY4 BN SS	R				61	64	L)	
L				TR									
/	630.44	631.24	0.80	CHER PY 3A	CH5 L4 DB	P	1 LM	U65	<=	L3	62	6=	
L				3A GL	SS								
/	631.24	633.43	2.19	CHAR SF PY	DB SS	P			<1		61	D.	
L				2A									
R	631.24	633.43		EXTENSIVE MICROVEINING OF QUARTZ IN THIS INTERVAL.									
/	631.24	633.43	2.19	2 ARSN SF PY	SI2 DB SS 2 4 4 4	R			<1		61		
L				3A	SN4								
R	631.24	633.43		INTERBEDDED SAND.									
R	633.43	633.43		END SAMPLE INTERVALS FOR SOUTH ZONE 1.									
K LS1	633.43	633.43	0.00										
/	633.43	634.43	1.00	CHAR SF PY	DB SS	P			<1		61		
L				2A									
R	633.43	634.43		EXTENSIVE QZ MICROVEINING.									
/	633.43	634.43	1.00	2 ARSN SF PY	SI2 DB SS 2 4 4 4	R			<1		61		
L				3A	SN4								
R	633.43	634.43		INTERBEDDED SAND.									
/	634.43	637.44	3.01	ARSN SF PY	SI2 LM SS 2 4 4 4	P			<1		61		
L				5A	SN4 DB RM								
R	634.43	637.44		FROM 634.39 - 634.89 LAMINATIONS DISPLAY INTENSE DEFORMATION.									
/	635.84	636.14	0.30	X ARGL 3A SF	RA1 DB	R			<=	81	D*		
L				2A									
R	635.84	636.14		BLERBY BARITE HORIZON.									
/	636.14	640.81	4.67	RRHM SF	F* R*	PQ9	P		<+		8)		
L				3A	R*	JJ+							
R	636.14	640.81		CHERT CONTENT HARD TO ESTIMATE DUE TO SILICIFICATION.									
/	640.81	641.01	0.20	SAND PY SF	BS G;	258	P				8+		
L				5A	R* F*	122							

R	640.81	641.01	THIS REPRESENT A COMPLETE ROOMA SEQUENCE JUST ABOVE A BLEBBY																
R	640.81	641.01	BARITE HORIZON.																
/	641.01	641.41	0.40	ARSN	BA	SF	BA4	2	3	3	3	P		B4	D*				
L				SA			SA3												
R	641.01	641.41	BLEBBY BARITE HORIZON.																
/	641.41	642.47	1.06	ARGL	SF	PY	//					P	3	BD	U75 <)	D*			
L				SA															
/	642.47	655.93	13.46	BRHT	SF	PY					QS7	P			<)	8=			
L				SA				1		3	C				<=				
R	655.93	655.93	REGIO ASSAY INTERVAL FOR SZ-S.																
/	655.93	657.93	2.00	BRXX	SF	PY	SI6	2	4	4	4	P			<*	D=			
L				SA			SA4												
R	655.93	657.93	BRECCIA IS COMPOSED OF SANDSTONE FRAGMENTS.																
/	657.93	658.69	0.76	ARSN	SF	PY	SI5 //	2	4	3	4	P	1	LM	U56 <+	<* <*	D=		
L				SA	CB		SA3												
/	658.69	661.30	2.61	ARSN	SF	PZ	SI5 //	DB	2	4	3	4	P	1	LM	U56 <1	<= <)	8+ B.	
L				SA			SA3												
R	658.69	661.30	INTERSE QUARTZ-CARBONATE-BARITE MICROVEINING, 20% OF PGI.																
R	658.69	661.30	GALENA BLENDS OCCUR WITHIN QUARTZ-CARBONATE-BARITE VEINS.																
K US2	661.30	661.30	0.00																
/	661.30	661.66	0.36	BNSX	SF	CH	CH5 //	DB				P	1	LM	U65 <)	L3	81	6*	
L				SA			SS						2	BD	U65	L*		L.	
R	661.30	661.66	GALENA CONCENTRATION OCCURS WITHIN A BRECCIATED CHERT-QUARTZ																
R	661.30	661.66	VEIN.																
/	661.66	666.57	4.91	LMSX	BA	CB	CH5 //	SS				P	1	LM	U85	81	L5	81	B)
L				SA	GL		DB BN						2	BD	U85	8)	<=		L.
R	661.66	666.57	CHERT OCCURS AS BEDS (BANDS) UP TO 3 CM WIDE.																
/	666.57	673.42	6.85	BNSX	BA	SF	CH2 DB BR					P	1	LM	U85		65	81	6=
L				SA	CB		SS LM									8)			6.
R	666.57	673.42	LAGINA AND BANDS OF BARITE HAVE BEEN TECTONICALLY BRECCIATED AND																
R	666.57	673.42	PYRITE IS ACTING AS A MATRIX LOCALLY. BRECCIATION IS LOCALIZED																
R	666.57	673.42	THROUGHOUT THIS INTERSECTION.																
/	673.42	678.48	5.06	BNSX	BA	SF	CH6					P	1	LM	U65	D.	L2	L1	L1
L				SA	CB								3	BD	U65		L.		
R	673.42	678.48	CHERT BANDS RANGE UP TO 4 CM IN WIDTH. CHERT BANDS ARE SEPARATED																
R	673.42	678.48	BY 3 CM BANDS OF LAMINATED SULPHIDES. GALENA LAMINATIONS ARE																
R	673.42	678.48	CONCENTRATED AT THE CONTACT WITH THE CHERT BANDS.																
/	678.48	682.51	4.03	BRXX	SF	CB	CH6 BR DB					P			<)		6=	6=	6=
L				SA							NPR					6)			D.

[illegible]

K	F	F	R	O	D	-	T	D	-	T	R	T	RECOV	MD	%	ROCK	TR	TR	QM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
F	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G																																																	

/		706.11	709.30	3.19																																													
L																																																	

K	US5	709.30	709.30	0.00																																													
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/		709.30	712.17	2.87																																													
L																																																	

K	LS5	712.17	712.17	0.00																																													
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/		712.17	718.85	6.68																																													
L																																																	

R		712.17	718.85																																														
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CARBONATE OCCURS IN LAMINA. CROSS CUTTING QUARTZ VEINS.

/		718.85	726.34	7.49																																													
L																																																	

ARGL	SF	SI+	2	2	+	2
2A						

P	3	BD	U60	<	61
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G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PR-ZN-AG-BR STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : B10AH068
TOTAL DEPTH/LENGTH : 750.31
CORE/HOLE DIAMETER : 80MMCOLLAR ELEVATION: 1275.94
NORTHING (- IF S): 7002472.00
EASTING (- IF E): 436496.25AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM :GEOLOGGED BY : DWB +
DATE (YY/MM/DD): 810000
PROJECT NUMBER : J-S2

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	146.90	-89.47
2	58.52	145.20	-89.34
3	78.94	144.00	-85.33
4	100.58	164.00	-83.00
5	118.87	130.00	-82.00
6	137.16	119.00	-80.00
7	152.40	114.00	-78.00
8	167.64	137.00	-76.67
9	176.48	114.00	-76.00
10	198.12	121.00	-75.00
11	222.20	122.00	-74.00
12	246.27	129.00	-71.67
13	265.17	132.00	-70.00
14	274.01	133.00	-69.25
15	295.65	137.00	-67.25
16	310.59	139.00	-66.00
17	327.35	143.00	-64.00
18	344.11	146.00	-63.00
19	359.35	150.00	-61.50
20	374.90	150.00	-60.50
21	392.58	151.00	-59.00
22	411.48	151.50	-58.00
23	432.51	152.00	-56.00
24	455.37	154.00	-55.00
25	475.18	153.50	-53.50
26	503.22	154.50	-50.00
27	521.20	152.00	-48.00
28	532.48	150.50	-47.00
29	551.69	152.00	-44.50
30	581.86	153.00	-41.00
31	609.60	156.00	-37.50
32	641.91	156.50	-33.50

33	643.74	156.50	-32.50
34	655.93	156.50	-31.00
35	660.50	156.50	-30.75
36	668.12	156.50	-30.50
37	680.31	155.70	-30.50
38	692.51	155.20	-30.50
39	704.70	154.60	-30.00
40	708.05	154.50	-30.00
41	716.89	155.80	-28.50
42	729.08	157.50	-28.00
43	741.27	157.50	-27.50
44	747.37	157.50	-27.00
45	748.89	157.50	-27.00

F - INTERVAL -		CORE	1 - %	TYP	QUAL	TEX	GRAIN	PGI	STRUCTUR-1	ALTERATION	MINS	ORE-TYPE	MINS	SUMMARY
L (UNITS = . DEC. PLACE)		RECOV	REC	ROCK	FLYING	MIN	TURES	CHARACS						
E A (METRIC FT=FOOTRIC)		ERY	DI	TM	TM	MAT	TX	TX	F	C	%	M	ARG	/RT
Y G F R D A - I D - I N T (.)		D X	TYPE	1	2	QM1	1	2	F	F	C	A		1
K F		ROCK	FM	RT	TM	DM2	TX	TX	S	C	O	O	CHT	T
E L		DUAL	AGE	EA	O	LC	3	3	4	O	/			2
Y G		DESIG	VIN	CUL					R	C				STRUCTUR-2
														A A A A A A A A A A
														2 2

R SVY	0.00	0.00	ALL READINGS BY SPERRY SUN SINGLE-SHOT AND MULTI-SHOT, EXCEPT											
R SVY	0.00	0.00	FOR S001 WHICH WAS DONE BY GYROSCOPIC DIRECTIONAL SURVEY.											
R SVY	58.52	58.52	BEGINNING OF WEDGED HOLE D.											
R SVY	58.52	58.52	HALL AND ROWE STEEL WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	181.66	181.66	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	200.25	200.25	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	230.43	230.43	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	249.63	249.63	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	276.45	276.45	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	376.43	376.43	CLAP RETRIEVABLE WEDGE-FULL AZIMUTH TO THE RIGHT.											
R SVY	750.31	750.31	END OF WEDGED HOLE D.											

/	0.00	60.66	60.66	MISS					P					
/	60.66	63.20	2.54	BRHT CR					M04	P				R+
L				3A				3	JM2					
/	62.03	62.60	0.57	7 SAND CR		SN5 G; MX	1 3 5 6		R					D+
L				3A		SI3	7							
R	62.03	62.60		THE HETEROLITHIC BRECCIA GRADES INTO A SILTY-SANDSTONE.										
/	62.95	63.20	0.25	X BRHT CR		BR			M04	R		V4		B+
L						SK								
/	63.20	83.43	20.23	BRHT CR		SS			MP9	P			<*	
L				3A		3			KN)					
R	63.20	83.43		BARITE AND A DULL RED MINERAL ARE ASSOCIATED IN VEINS AT THE TOP										
R	63.20	83.43		OF THE INTERVAL. CHERT FRAGMENTS OCCUR I.										
/	83.43	94.20	10.77	BRHT CR	*S+	G;			LTS	P		<*		D)
L				4A	*C+ F*	R* 2	+		K03					
R	83.43	94.20		PYRITE OCCURS AS DISSEMINATIONS IN THE ARGILLITE MATRIX, AS										
R	83.43	94.20		SMALL NODULES WITH QUARTZ ENVELOPES AND AS A REPLACEMENT MINERAL										
R	83.43	94.20		IN CHERT CLASTS. THE INTERVAL'S FRAMEWORK SUPPORTED. CHERT										
R	83.43	94.20		CLASTS APPEAR TO GRADE NORMALLY, INDICATING THAT TOPS ARE IN A										
R	83.43	94.20		UPHOLE DIRECTION. TWO LARGE SANDSTONE CLASTS OCCUR BETWEEN 86										
R	83.43	94.20		AND 88.75 METRES.										

K	F	F	R	O	I	-	T	O	-	T	N	T	RECPV	MD	%	ROCK	TM	TM	TM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-	L	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G												R	O	D	AGE	FV	RO	LC	TM	TM2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA								

R 94.20 105.97 LARGE SILTY ARGILLITE CLASTS ARE RAFTED IN A PERBLY MUDSTONE
R 94.20 105.97 MATRIX.

/ 105.97 205.20 99.23 BRHM SN1 LV9 P <) D)
L 4A 2

R 105.97 205.20 ESSENTIALLY A DISRUPTED ARSI UNIT.

/ FLT 125.90 142.21 15.31 5 BRHM GR GG1 LV9 R <+ <)
L

R 125.90 142.21 THIS INTERVAL IS VERY GRAPHITIC AND MILDLY SHEARED DUE TO
R 125.90 142.21 FAULTING. QUARTZ AND PYRITE VEINING IS ALSO PREVALENT.

/ SHR 161.95 165.02 3.07 X BRHM GG1 LV9 R <) D)
L

/ SHR 172.52 181.66 9.14 X BRHM GG= LV9 R <+ <)
L

/ 181.66 183.18 1.52 X VEDGE R

R 181.66 183.18 VEDGE.

/ 183.18 187.76 4.58 X BRHM SN1 LV9 R <+ D)
L

/ 194.45 195.20 0.75 X BRHM SN1 LV9 R <) #.
L

R 194.45 195.20 INTV IS BRECCIATED + INFILLED WITH QTZ-CARB (SID?).

/ 205.20 207.87 2.67 BRHT *S) F* NO6 P 0=
L 5A *C) 2) NO2

/ 207.87 217.30 9.43 BRPA *C(N; H* I L 5 R KR2 P >2 D.
L 6A 5 C KN5

R 207.87 217.30 INTV IS FAIRLY COMPLEX - ESSENTIALLY A SAND ZONE-EXHIBITS

R 207.87 217.30 WELL-DEFINED NORMAL GRADING FROM PERBLE SIZE (LESS THAN 1CM)

R 207.87 217.30 ARGL+CHT CLASTS AT BASE TO MED. SAND AT TOP. BOTTOM 3.33M

R 207.87 217.30 (213.97 - 217.30M) COMPRISES. A SAND/PERBLE MTX, WITH FRAGS OF

R 207.87 217.30 ARGL AS MUCH AS 3CMS LONG (IE ESSENTIALLY A BRHT). UPPER 6.1M

R 207.87 217.30 (207.87 - 213.97M) IS ESSENTIALLY A SANDSTONE COMPRISES ARGL +

R 207.87 217.30 CHT GRAINS, WITH NO LARGE CHT FRAGS. UPPER 4M IS CUT BY TWO

R 207.87 217.30 LARGE QTZ VN SYSTEMS WITH MNR CARB (SID?)

/ 208.45 210.92 2.07 9 VEIN ST MX R >9 D.
L 8A

/ 211.50 212.00 0.50 5 BRPA *C(N; H* I L 5 R KR2 P >5 D.
L 7A

R 211.50 212.00 SANDSTONE AS ABOVE, CUT BY PROMINENT QTZ STOCKWORK.

/ 213.97 217.30 3.33 X BRPA *C(H* M; LR5 R D.
L 6A 3 KN4

Z		217.30	246.40	29.10	BRHT	*S)	RV7	P	D=
L					SA	*C+ F*	2)	MO2	
R		217.30	246.40		UPPER PART OF INTV APPEARS TO BE CONTINUOUS WITH OVERLYING UNIT.				
Z FRG		222.40	228.45	6.05	X ARST	SN2 LF	0 3 2 3	R 1 BD	87 L*
L					4A				
Z SHR		243.15	244.75	1.60	X FAUL	GG1		R	
L					4A				
R		243.15	244.75		RUBBLY INTV; LOCAL GOUGE.				
Z		246.40	252.68	6.28	BRHM	*S+	PR8	P	
L					4A		3 + KM+		
R		246.40	252.68		LOCALLY BECOMES BRPM.				
Z		252.68	259.60	6.92	BRPM	*S) F*	QQ3	P	D.
L					SA	*C-	2) 0 NP2		
R		252.68	259.60		LOCALLY BECOMES BRHT				
Z		259.60	267.70	8.10	BRHM	*S*	PQ7	P	D.
L					4A		* KN+		
R		259.60	267.70		LOCALLY BRPM.				
Z		267.70	295.00	27.30	BRHT	*S) F* B*	QT4	P	<(D.
L					SA	*C) H*) NO5		
K UDF		295.00	295.00	0.00					
R UDF		295.00	295.00		POSSIBLE TOP OF THICK SEQUENCE OF DEBRIS FLOWS CHARACTERIZED				
K UDF		295.00	295.00	0.00					
R UDF		295.00	295.00		BY CGCP CLASTS.				
Z		295.00	305.50	10.50	CGRH	*S+	RT5	P	<(D. D.
L					SA		3 + LO=		
R		295.00	305.50		INTV MAY REPRESENT TOP OF BRCG UNIT AS NOTED ABOVE. ALTHOUGH				
R		295.00	305.50		CGCP FRAGS ARE QUITE ABNT IN THIS INTV HOWEVER, THEY ARE				
R		295.00	305.50		RELATIVELY RARE BENEATH THIS ZONE IF CGRH UNIT IS NOT AS WELL				
R		295.00	305.50		DEVELOPED IN DDH 68D AS IN 68, 68A AND 68C. IN A COUPLE OF				
R		295.00	305.50		INSTANCES, IT IS UNCLEAR WHETHER CGCP INTERVALS ARE FRAGMENTS OR				
R		295.00	305.50		REPRESENT A DEPOSITIONAL EVENT.				
Z SHR		297.70	298.40	0.70	X CGHR GR	*S+	RT5	R	<(D. D.
L					4A				
R		297.70	298.40		RUBBLY INTV (SHR), GRAPHITIC.				
Z FRG		298.90	300.45	1.55	X CGSN SF	MX	I L 3 0	R	B. D- D.
L					6A		4 0		
R		298.90	300.45		UNCLEAR WHETHER THIS IS A FRAGMENT OR IS DEPOSITIONAL-PROBABLE				
R		298.90	300.45		FRAGMENT.				
Z		305.50	327.80	22.30	BRHM	*S+	RT9	P	D.
L					4A		+ (N)		

K	F	F	R	D	M	-	I	D	-	I	M	T	REC'D	DD	%	POCK	IN	IN	DM1	TX	TX	F	C	%	M	ARG	RT	1	ID	AZM	DIP	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2					
E	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G													R	Q	D	AGE	EV	RU	IC	IN	DM2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

R 305.50 327.80 LOCALLY BRHM. INTV CONSISTS PREDOMINANTLY OF ARSI FRAGMENTS
R 305.50 327.80 CONTAINING 15-20% SAND LAM.

/ SHR 326.30 327.80 1.50 X BRHM *S+ RT9 R D.

R 326.30 327.80 RUBBLY INTV.
R 327.80 328.75 PROBABLY DEPOSITIONAL 2 GRADED CYCLES FROM PEBBLES AT BASE TO
R 327.80 328.75 FINE SAND AT TOP. 15CM ZONE FROM 327.85M TO 328.0M COMPRISES
R 327.80 328.75 ARGL AT BASE (CONFORMABLE WITH UNDERLYING SAND, AND BRHT AT TOP.

/ 327.80 330.00 2.20 BRHM LR3 P < <

L 6A KP6

/ 327.80 328.75 0.95 X SAND G; I K 2 L R V=

L 7A 6

/ 329.90 330.00 0.10 X SAND I K 2 N R 2 BD 40 <+

L 7A 5

R 329.90 330.00 TURBIDITE; ALTERNATING RELATIVELY FINE + RELATIVELY COARSE SAND
R 329.90 330.00 BEDS. UPPER HALF CONTAINS APPROX 20% SHALE FRAGS UP TO 1CM.

/ 330.00 365.20 35.20 BRHM *C. B* 5V9 P D.

L 5A *S(3 1 (LU* D-

R 330.00 365.20 INTV HAS A VERY LOW CHT CONTENT AND IS EFFECTIVELY A BRHM EXCEPT
R 330.00 365.20 FOR THE PRESENCE OF SEVERAL PEBBLY SANDSTONE ZONES RANGING FROM
R 330.00 365.20 10CMS TO 1.7CMS. THE MAJOR PEBBLY SAND ZONES ARE 331.7 - 331.94
R 330.00 365.20 (FRAG), 337.7 - 337.9 (PROBABLE FRAG), 358.28 - 358.75 (FRAG)
R 330.00 365.20 AND 365.2 - 366.98M (PROBABLE FRAG). INTV IS LOCALLY RUBBLY. A
R 330.00 365.20 PATCH OF SIDERITIZED ARGL APPROX. 10CMS LONG OCCURS AT 358.80M.
R 330.00 365.20 THIS IS A POSSIBLE FRAGMENT.

/ FLT 334.15 337.41 3.26 X FAUL R

L 5A

R 334.15 337.41 RUBBLY INTV.

/ 358.30 358.75 0.45 X CGSN *C+ F* B* J L 3 N + R

L 7A 3 0 9

R 358.30 358.75 PROBABLY FRAGMENT, BUT DIFFICULT TO BE SURE.

/ FLT 361.26 365.20 3.94 X FAUL GG1 B* 5V9 R D.

L 5A

R 361.26 365.20 RUBBLY INTV WITH LOCAL FAUL GOUGE.

K UDF 365.20 365.20 0.00

R UDF 365.20 365.20 PROBABLY FRAG, BUT DIFFICULT TO BE SURE.

/ 365.20 366.98 1.78 CGSN *C= B* H* J L 4 0 1 P D.

L 7A F* 3 C 9

/ 366.98 381.61 14.63 BRHT OT9 P < D.

L 4A 3) LM=

[illegible][illegible]

Z	FRG	470.45	470.79	0.36	X	CGS4	J	L	4	M	R	D.
L						hA	3			C		

Z	FRG	472.83	473.75	0.93	X CGSN		J L 3 0	R			R-
L					6A		4 0				
Z	FRG	477.20	478.58	1.68	X CGSN		J L 3 N	R	V)		D.
L					6A		4 0				
Z	SHR	477.20	478.88	1.68	X FAUL GR	GG= F*	PS5	R	<		R(
L					8A						
R		477.20	478.88								
R		483.63	488.09								
R	EDT	483.63	488.09								
R		483.63	488.09								
Z		483.63	490.02	6.39	BRHM		OS6	P	<-		R)
L					4A		5 LP)				
Z	SHR	483.63	488.09	4.46	X FAUL GR	GG4	OS6	R	>+		R)
L					3A		5 LP)				
R		483.63	490.02								
R											
Z		490.02	506.70	16.68	BRHT	*S=	US5	P			R-
L					4A	*C= F*	2 1 = MP2				
R		490.02	506.70								
R		490.02	506.70								
R		490.02	506.70								
Z	FRG	494.67	495.72	1.05	X CGSN	*C= F* H*	J R 4 P LO+	R			D.
L					6A		4 0				
R		494.67	495.72								
R											
Z	FRG	495.91	496.51	0.60	X CGSN SD	*C= F* R*	J M 4 N	R			D.
L					6A		3 0				
R		495.91	496.51								
R		495.91	496.51								
Z	FRG	505.60	506.00	0.40	X CGSN	*S(R* H*	J M 3 N LM*	R			D.
L					6A		3 (0				
R		505.60	506.00								
R											
Z		506.70	513.80	7.10	BRPM	*S1 F* H*	OS5	P			R.
L					5A	*C.	2 (= M03				
R		506.70	513.80								
R		506.70	513.80								
Z	FRG	508.10	508.54	0.24	X CGCP PY	*C= F* H*	J N 3 0	R			D-
L					6A	*S=	3 - C				
R		508.10	508.54								
R											
Z		512.11	512.57	0.26	X SAND PY		BD G; I J 2 M	R 2	U40		D.
L					6A		7				

[illegible]

[illegible]

R	541.83	545.93		INTERVAL CONTAINS AT LEAST ONE LARGE CG FRAG.										
/	545.93	561.83	15.90	BRHM PY	SN3	NS1	P						0.	
L				4A		2	3	0	N06					
R	545.93	561.83		INTERVAL IS MODERATELY SANDY WITH A SANDY MATRIX AND SAND BANDS										
R	545.93	561.83		UP TO .2M ALSO ARG FRAGS UP TO .8M ARE PRESENT AND ARE REPEATED										
R	545.93	561.83		CORE IS LOCALLY RUBBLY.										
/	FRG	556.05	556.83	0.78	X ARGL	SN) LM	A F + F	R						
L					3A	SI)	8							
/	FRG	557.52	557.72	0.20	X ARGL SF		A A A	R					<(
L					6A		9							
R	557.52	557.72		FRAG IS STRONGLY SILICIFIED AND HAS A FEW Q17 VEINLETS										
/		561.83	566.22	4.39	BRHM	SN=	QT9	P						
L					4A		3	= C	KM)					
R	561.83	566.22		INTERVAL CONSIST OF SEVERAL LARGE LAM ARGL CLASTS WITH MINOR										
R	561.83	566.22		CHERT AT TOP OF INTERVAL.										
/		566.22	575.51	9.29	BRHT	SN+	NR3	P						
L					5A		2 + +	LOS						
R	566.22	575.51		INTERVAL IS LOCALLY SANDY.										
/		575.51	588.97	13.46	BRHM	SN=	QT9	P						
L					4A		5	= C	0				C.	
R	575.51	588.97		FRAGS ARE LARGE WITH ONLY A FEW SMALLER FRAGS.										
/		588.97	601.20	12.23	BRHT PY	SN= F* R*	QS4	P					0.	
L						*C)	2 + =	M04						
R	588.97	601.20		INTERVAL IS LOCALLY SANDY-ALSO SOME SAND CLASTS PRESENT										
K	LDF	601.20	601.20	0.00										
/		601.20	613.32	12.12	ARSI PY GR	SI1 // LM	P	1	LM	U58	<.		8+	
L					2A	SI2 SS IR								
/		602.33	602.91	0.58	X BRHT PY	IR F*	N09	R	5				6=	
L					3A		LM1							
/		604.97	605.11	0.14	X SAND PY	SI2 IR BD		R	2	BD	U50		81	
L					5A	SI2 //								
/		609.55	609.72	0.17	X SAND PY	SI3 IR BD		R	2	BD	U50		81	
L					5A	SI3 //								
/		610.60	611.62	1.02	X BRHT PY	SN1 IR F*	N05	R					6+	
L					5A	DB	1	K04						
R	610.60	611.62		SANDSTONE FRAGMENTS MAKE UP 10% OF THIS REPEAT UNIT.										
/		613.32	626.15	12.83	BRHM PY	F* R*	PT7	P					8)	
L					2A		7	LN1						

R	613.32	625.15	COMPOSED OF 70% ARSN FRAGMENTS.									
/	615.04	615.61	0.57	X ARSN PY	SI3	2 3 5 3	R				L+	
L				3A	SN5							
R	615.04	615.61	PROBABLE LARGE FRAGMENT.									
/	622.35	626.15	5.80	X ARGL PY			R	2 BD	U83		D*	
L				1A								
R	622.35	626.15	PROBABLE LARGE FRAGMENT.									
/	626.15	649.37	23.22	BRHT PY		QS9	P				8+	
L				2A		JJ+						
/	629.96	630.41	0.05	X SAND PY	SI2	2 4 8 4	R				D)	
L				4A	SN8	2						
R	629.96	630.41	PROBABLE FRAGMENT.									
/	631.86	632.41	0.55	X ARSI PY	SI2 LM	// 1 2 1 2	R	1 LM	U53		L=	
L				3A	SN1 SS							
R	631.86	632.41	PROBABLE FRAGMENT.									
/	644.35	645.10	0.75	X BRHT PY	F*	LP8	R				D+	
L				3A		JL2				<)		
R	644.35	645.10	PROBABLE FRAGMENT.									
/	647.40	648.45	1.05	X ARGL PY	MX		R		< (D+	
L				1A								
R	647.40	648.45	PROBABLE FRAGMENT.									
/	649.37	650.44	1.07	BRHT PY	F* H*	NP4	P				8+	
L				4A		3 LN3						
R	649.37	650.44	ARSN FRAGMENTS MAKE UP 30% OF THIS INTERVAL.									
/	650.44	652.54	2.10	SAND PY GR	SI2 BS IN	2 4 7 5	P				8=	
L				5A	SN7	5						
R	650.44	652.54	AN UPPER SEQUENCE OF A BOUMA SEQUENCE INCLUDES LOCAL LARGE									
R	650.44	652.54	ARGILLITE FRAGMENTS, 5% OF PGI. IMBRICATED AT 50% UP HOLE.									
/	652.54	656.86	4.32	BRHT PY GR	BS	NP4	P				8+	
L				5A		2 JM4						
R	652.54	656.86	LOWER PORTION OF BOUMA SEQUENCE, THAT EXTENDS FROM 650.44 TO									
R	652.54	656.86	656.86. ARSN FRAGMENTS MAKE UP 20% OF THIS PGI.									
/	656.86	665.00	8.14	BRHT PY	F* H*	PR6	P		<)		6=	
L				3A	H*	3 MN1			C/			
/	656.86	665.00	8.14	3 BRXX PY	SI2	2 3 4 3	R				6=	
L				4A	SN4							
R	656.86	665.00	FAIRLY ARSN FRAGMENTS.									
/	665.00	665.40	0.40	CGCP PY			P				6+ 6*	
L				5A								

K	F	F	R	D	A	-	T	D	-	I	N	T	RECOV	RD	%	ROCK	TM	TM	DM1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
F	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Y	G												R	D	D	AGE	EV	RD	LC	TM	DM2	TX	TX	S	C	D	D	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA							

Y	G	665.40	666.60	1.20	RRH4 PY GL 3A	F* R* H*	MO9 JK1	P	C.	62	6+
K	US1	666.60	666.60	0.00							
/	MSX	666.60	666.88	0.28	MSX PY GL A8 SL	BR MX		P		B*	63 6+
L											
R		666.60	666.88		START OF FIRST ORE ZONE. LOCALLY SILICEOUS.						
/	MSX	666.88	667.30	0.42	MSX PY GL TS SL	BR MX		P	B1	B*	64 6=
L											
R		666.88	667.30		SLIGHTLY CALCAREOUS ALONG FRACTURES.						
/	MSX	667.30	667.90	0.60	MSX PY GL TS SL	BR MX		P	<1	B) D(B* 64 61
L											
R		667.30	667.90		CARBONATE OCCURS LOCALLY IN BLENDS AND VUG FILL. SPHALERITE CONCENTRATIONS OCCUR AS NAVEY BANDS.						
/	BSX	667.90	668.25	0.35	BSX PY GL 3A SL	BR		P	81	L3 D*	62 6=
L											
R		667.90	668.25		BARITE APPEAR TO BE SILICIFIED.						
/	BSX	668.25	668.48	0.23	BSX PY SL 6A GL	BR		P	6=	6= D* B*	61 63
L											
R		668.25	668.48		CARBONATE AND QTZ OCCUR TOGETHER AS PRIMARY CRYSTALS AS WELL AS LAMINATIONS WITH MINOR BARITE.						
/	BSX	668.48	668.92	0.44	BSX PY GL *C=	BR F*		P	B=	R1	62 62
L											
/	MSX	668.92	669.47	0.55	MSX GL SL TS PY	MX LM RR		P	81	B+ D.	61 64
L											
R		668.92	669.47		LAMINATIONS ARE VISABLE WITHIN THE MASSIVE SPHALERITE ZONES.						
/	BSX	669.47	670.85	1.38	BSX PY GL 6A CR	MX BR VG LM		P	82	62 L+	63 6+
L											
R		669.47	670.85		SOME LOCALIZED PODS OF PYRITE, MAY REPRESENT FRACTURE FILL.						
/		670.85	673.65	2.80	BSX GL PY 7A CR	BR		P	<1	61 61	63 82 < 62 D.
L											
/		673.65	674.62	0.97	BSX PY GL 5A CR	BR		P	<+	61 D+	65 61 62 6*
L											
/		674.62	675.29	0.67	BSX PY GL 5A CR	BR		P	<+	62 61	64 61 62 D*
L											
/		675.29	676.35	1.06	BSX PY CR 5A GL	BR		P		61 8*	64 61 <1 61 6. 62 8)
L											
R		675.29	676.35		QUARTZ-SIDERITE VEINS CONTAIN THE MAJORITY OF THE SPHALERITE.						

[illegible]

Z	734.96	736.00	1.04	3	ARGL	PY	IB	//	R	1	LM	U80		D.	
L						7A		LM	SS						
R	734.96	736.00			FIDOR SIDERITE INTERBEDDED										
Z	736.00	736.44	0.44		MSSD	SD	PR	SD6	IB	LM	P	1	LM	U88	D+
L						TS	PY		//	SS		3	BD	U88	65 L) 8*
Z	736.00	736.44	0.44	4	CHER				IB	LM	R	1	LM	U88	
L						7A			//	SS		3	BD	U88	
Z	736.44	738.84	2.40		ARGL	PY	IB	LM	P	1	LM	U78		D.	
L						2A		//	SS		3	BD	U78	L1 L(D.	
Z	736.44	738.84	2.40	4	CHER		IB	LM	R	1	LM	U78			
L						7A		//	SS		3	BD	U78		
Z	737.74	738.04	0.30	6	MSSD	SD	PR	SD6	IB	LM	R	3	BD	U65	L(
L						TS		//	SS					L6 L+ D(
Z	737.74	738.04	0.30	4	CHER		IB	LM	R	3	BD	U65			
L						7A		//	SS						
K US2	737.00	737.00	0.00												
Z	738.84	739.34	0.50		MSSD	SD	PR	SD6	IB	LM	P			<2	<*
L						TS								66 6)	
Z	738.84	739.34	0.50	2	CHER				DB		R				
L						7A									
Z	739.34	739.65	0.31		ARSI	PY	GR	SI1	LB	BD	P	1	LM	U82	<+
L						4A		SN2	SS			2	BD	U82	61
Z	739.65	739.85	0.20		ARSI	PY	GR	SI1	DB	BR	P			<=	C*
L						4A		SN2	LM	SS					62
R	739.65	739.85			MAY REPRESENT A SHEAR ZONE, DUE TO THE BRECCIATED NATURE OF THE										
R	739.65	739.85			INTERVAL.										
Z	739.85	740.14	0.29		MSSD	SD	PR	SD5	IB	LM	P	1	LM	U35	6= D*
L						TS	PY			SS		3	BD	U35	65 8=
Z	739.85	740.14	0.29	4	ARGL	PY	IB	LM	R	1	LM	U35			
L						4A		SS		2	BD	U35			
R	739.85	740.14			PYRITE LAMINATIONS AT SIDERITE-ARGL CONTACT.										
K LS2	740.14	740.14	0.00												
Z	740.14	740.54	0.40		CHER	PY			LM	//	P	1	LM	U65	<*
L						7A				SS					8+ 8)
Z	740.54	741.21	0.67		ARGL	PY			LM	SS	P	1	LM	U57	6=
L						5A				DB					

G E O L O G E D I T L I S T I N G

SYSTEMS ENGINEERING BY
INTERNATIONAL GEOSYSTEMS CORP.PAN OCEAN OIL LTD.
JASON PB-70-AG-BA STE DEPOSIT, Y.T.

FORMAT VERSION : 6802

DRILLHOLE/TRAVERSE : 81ENH068
TOTAL DEPTH/LENGTH : 980.54
CORE/HOLE DIAMETER : HQ66COLLAR ELEVATION: 1275.94
NORTHING (= IF S): 7002472.00
EASTING (= IF E): 436496.25AZIMUTH(DEG) : 0.00
VERTICAL ANGLE : -90.00
CO-ORD SYSTEM : UTMGEOLOGGED BY : JDK +
DATE (YY/MM/DD): 811009
PROJECT NUMBER : JASON

SEQ. NO OF SURVEY DATA	LENGTH FROM COLLAR TO SURVEY POINT	AZIMUTH (DEG)	VERT. ANGLE (DEG)
1	30.00	146.90	-89.47
2	58.52	145.00	-87.25
3	78.94	144.00	-85.33
4	100.58	164.00	-83.00
5	118.87	130.00	-82.00
6	137.16	119.00	-80.00
7	152.40	114.00	-78.00
8	167.64	137.00	-76.67
9	176.48	114.00	-76.00
10	198.12	121.00	-75.00
11	222.20	122.00	-74.00
12	246.27	129.00	-71.67
13	260.27	129.00	-71.67
14	280.72	128.00	-69.67
15	306.02	125.00	-68.75
16	327.96	127.00	-68.25
17	350.82	127.00	-67.67
18	369.72	124.00	-66.50
19	383.13	128.00	-66.00
20	389.84	130.00	-60.50
21	403.86	132.00	-65.50
22	420.93	132.00	-65.25
23	424.89	132.00	-64.75
24	434.34	134.25	-64.25
25	445.31	136.00	-63.00
26	466.95	133.00	-61.00
27	489.51	136.00	-56.67
28	503.53	134.00	-55.50
29	528.32	137.00	-53.66
30	544.07	137.00	-53.33
31	559.00	137.00	-53.25
32	573.63	139.00	-52.00

33	587.65	137.00	-51.50
34	602.59	139.00	-50.50
35	618.74	136.00	-50.33
36	632.76	136.00	-50.33
37	646.78	137.00	-51.00
38	665.99	137.50	-50.00
39	689.76	133.00	-47.00
40	696.16	133.00	-46.75
41	711.10	133.00	-45.00
42	726.34	131.00	-47.50
43	744.32	134.00	-44.75
44	748.28	133.00	-44.25
45	760.47	129.00	-44.50
46	772.67	129.00	-44.50
47	784.86	129.00	-44.50
48	797.05	128.50	-44.00
49	809.24	128.50	-43.50
50	821.43	128.00	-42.75
51	833.63	127.50	-42.50
52	845.82	127.00	-42.33
53	858.01	127.50	-42.00
54	870.20	127.50	-42.00
55	882.40	127.00	-41.00
56	894.59	127.00	-40.50
57	906.78	126.50	-39.00
58	918.97	126.50	-38.75
59	931.16	126.50	-38.00
60	943.36	126.50	-37.25
61	955.55	126.50	-37.00
62	967.74	126.50	-36.75
63	979.93	126.50	-36.75

F - I N T E R V A L - CORE T- % TYPE QUAL TEX GRAIN PGI STRUCTUR-1 ALTERATION MINS ORE-TYPE MINS SUMMARY																																	
K	L	(UNITS = . DEC. PLACE)	RECOV-	M F	ROCK	FLYING	MIX	TURES	CHARACS		ARG	/RI	T	ID	STK	DIP	A	A	A	A	A	MIN	A	A	A	MIN	-	-	-	-			
Y	G	F R O M - T O - I N T (.)	D	X	TYPE	1	2	0-1	1	2	F	F	C	A		1	AZM	RT	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2	

K	F		ROCK	FM	RT	TM	QA2	TX	TX	S	C	O	O	CHT		T	ID	STK	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA				
E	L		QUAL	AGE	FM	U	LC	3		3	4	O		/		2		AZM	RT	H	H	H	H	H	H	H	H	H	H	1	1		
Y	G		DESIG		VIR	COL				R		C						STRUCTUR-2		A	A	A	A	A	A	A	A	A	2	2			

R SVY	0.00	0.00	READING BY SPERRY SUN SINGLE SHOT AND MULTI-SHOT, EXCEPT FOR
R SVY	0.00	0.00	S001 WITH WAS DONE BY GYROSCOPIC DIRECTIONAL SURVEY.
R SVY	58.52	58.52	BEGINNING OF WEDGED HOLE D.
R SVY	58.52	58.52	HALL AND ROWE STEEL WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	181.65	181.65	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	200.25	200.25	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	230.43	230.43	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	249.63	249.63	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	260.27	260.27	END OF WEDGED HOLE D.
R SVY	260.27	260.27	BEGINNING OF WEDGED HOLE E.
R SVY	260.27	260.27	HALL AND ROWE STEEL WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	383.13	389.84	AZIMUTH FOR S019 HAS NOT BEEN USED DUE TO MAGNETICS.
R SVY	389.84	420.93	SURVEY S020 AND S021 ALSO HAVE BEEN AFFECTED BY MAGNETICS,
R SVY	389.84	420.93	AND THERE AZIMUTH HAS BEEN EXTRAPOLATED.
R SVY	470.00	470.00	1/2+1/2 WEDGE TO THE RIGHT.
R SVY	503.53	503.53	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	673.91	673.91	CLAP RETRIEVABLE WEDGE - FULL AZIMUTH TO THE RIGHT.
R SVY	0.00	0.00	THE FIRST AND THIRD READINGS BELOW ARE FROM SINGLE SHOT
R SVY	0.00	0.00	SURVEYS AND ARE LESS ACCURATE THAN THE GYROSCOPIC SURVEY.
R SVY	0.00	0.00	THEREFORE THEY SHOULD NOT BE USED IN PLOTTING THE HOLE.

Z	332.23	339.25	7.02	BRHT	PY GR	F*	PR5	P				D)
L				3A			3 C JN1			C.		
Z	335.12	335.75	0.63	X BRHM	PY		JK2	R				D)
L				4A			JK3					
Z	339.25	349.97	10.72	BRHM	PY		QP9	P				D)
L				2A			LN*			C.		
Z	349.97	391.36	41.39	ARSI	PY	SI= // BD		P	1 LM	U55 <(8+
L				2A		SN= LM SS			2 BD	U55	C.	
Z	363.93	363.96	0.03	X ARSI	PY	SI= // BD		R	1 LM	U60 <(8+
L				2A		SN= LM SS			2 BD	U60	C.	
Z	371.50	371.60	0.10	X ARSI	PY	SI= // BD		R	1 LM	U82 <(8+
L				2A		SN= LM SS			2 BD	U82	C.	
Z	379.63	379.73	0.10	X ARSI	PY	SI= // BD		P	1 LM	U80 <(8+
L				2A		SN= LM SS			2 BD	U80	C.	
Z	385.27	385.37	0.10	X ARSI	PY	SI= // BD		R	1 LM	U81 <(8+
L				2A		SN= LM SS			2 BD	U81	C.	
Z	389.20	389.30	0.10	X ARSI	PY	SI= // BD		R	1 LM	U80 <(8+
L				2A		SN= LM SS			2 BD	U80	C.	
Z	391.36	392.62	1.26	BRHM	PY	*C* F* R*	NQ8	P				D.
L				1A			KN=			C.		
Z	392.62	398.60	6.18	SAND	PY	SN7 R* F* 3 J 3 N		P		<(D*
L				6A		5 C						
Z	398.80	423.78	24.98	BRHT	PY	F*	PR7	P				D.
L				3A			2 C J01			C.		
Z	401.01	402.21	1.20	X SAND	PY	SI4 LC G; 2 4 6 5		R	3 BD	D43		D.
L				5A		SN6 FU //						
R	401.01	402.21	SEVERAL FU CYCLES / TOPS DOWN HOLE-SLUMPED TURBIDITE SEQUENCE.									
R	401.01	402.21	THESE CYCLES FORM PART OF COARSENING UPWARD MEGASEQUENCE									
R	401.01	402.21	INDICATED BY INCREASING THICKNESS OF COARSE CLAST INTERVALS									
Z	423.78	430.99	7.21	ARSI	PY	SI1 // SS 2 3 1 3		P	1 LM	U70		D*
L				3A		SN1 LM PH			2 BD	U7	C.	
Z	430.99	430.63	3.64	BRHM	PY	*S4 F* R*	PQ5	P				D)
L				3A			4 C JL=			C.		
R	430.99	430.63	40% OF THIS INTERVAL IS REPRESENTED BY SANDSTONE AND ARSN									
R	430.99	430.63	FRAGMENTS.									
Z	434.63	436.64	2.01	ARSI	PY	GP SI1 PH // 2 3 3		P	1 LM	U85		D*
L				2A		SS LM			2 BD	U85	C.	

	Interval	Depth (m)	Interval (m)	Lithology	Grade	Notes	Remarks	Other	Comments	
/L	436.54 - 437.39	0.75		BRHM PY SA	*S4	OP6 0	P		D*	
/L	437.39 - 442.67	5.28		ARSI PY GR 4A	S11 LM BD 2 4 1 4 SM SS PH		P 1 LM 2 BD	U50 U50	C. D)	
/L	442.67 - 445.92	3.25		BRHM PY SA		OQ8 2 0	P		D*	
R	442.67 - 445.92			20% OF THIS INTERVAL IS REPRESENTED BY SANDSTONE AND ARSN FRAGMENTS.						C.
/L	445.92 - 449.28	3.36		ARSH PY 4A	S11 LM BD 2 4 1 4 S42 // SS		P 1 LM 2 BD	U55 U55	C. D*	
/L	449.28 - 453.50	4.22		BRHM PY PA	*S=	PR9 JK=	P		D)	
/L	453.50 - 474.50	21.00		BRPM PY 4A	S42 F* R* H* B* +	NS4 O LM3	P	<*	8) C. <(D) 8.	
R	453.50 - 474.50			SPHALERITE OCCURS WITHIN FRACTURED CHERT PEBBLES BEING CONTROLLED BY QUARTZ VEINING.						
R	453.50 - 474.50			SIMILAR SPHALERITE ASSOCIATIONS WERE SEEN IN 81-68C, WELL ABOVE THE DRF ZONE. INCREASING SAND CONTACT BASE (DOWNHOLE).						
/L	474.50 - 484.68	10.18		BRHM PY AA	S43 M; R* H* R*	OQ3 MO4	P		D*	
R	474.50 - 484.68			BASE OF SEQUENCE GRADES TO BRPM LOCALLY.						
/L	484.68 - 491.57	6.89		BRHM PY PA	DB	RS9	P		8)	
/L	491.57 - 497.18	5.61		BRHM PY SA	*S= F* R* H*	OR8 KM=	P		D)	
/L	497.18 - 533.29	36.11		ARSI PY SA	S12 LM BD 2 3 1 4 S41 SS DB		P 1 LM 2 BD	U40 U40	C. < <* D* D. D. D.	
R	497.18 - 533.29			TOWARDS THE TOP OF THIS INTERVAL BEDS ARE DISTURBED AND SLIGHTLY FRAGMENTED; FRAGMENTS ARE NOT ROTATED.						
R	497.18 - 533.29			STIBNITE ALSO OCCURS WITHIN QUARTZ-SIDERITE.						
R	497.18 - 533.29			THE INTERVAL IS ALSO PHYLLITIC LOCALLY.						
/L	500.00 - 500.01	0.01		X ARSI PY	S12 LM BD 2 3 1 4		R 2 BD	U90	<. D* D. D.	
/L	502.00 - 503.53	1.53		X WEDG			R	U72 U72		
/L	505.05 - 505.06	0.01		X ARSI PY	S12 LM BD 2 3 1 4		R 2 BD	U80	<. D* D. D.	

/	509.63	509.64	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U64	<	D* D. D.
L							2 BD	U64		
/	514.50	514.51	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U54	<	D* D. D.
L							2 BD	U54		
/	519.99	520.00	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U61	<	D* D. D.
L							2 BD	U61		
/	525.17	525.18	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U66	<	D* D. D.
L							2 BD	U66		
/	525.50	525.55	0.05	X GAUG	GG*	R				
L				PA						
/	527.00	527.01	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U68	<	D* D. D.
L							2 BD	U68		
/	529.00	529.01	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U40	<	D* D. D.
L							2 BD	U40		
/	530.00	530.01	0.01	X ARSI PY	SI2 LM BD 2 3 1 4	R	1 LM	U40	<	D* D. D.
L							2 BD			
/	533.29	535.17	1.88	ARGL	ST1 MX 0 3 1 3	P				D.
L				PA					C.	
/	535.17	551.69	16.52	ARSI DS	LM DB 0 4 = 4	P	1 BD	T50		D.
L				3A	SS BD		3 BD	B20	C.	> C.
R	535.17	551.69		BEDS ARE LOCALLY DISTURBED, POSSIBLY DUE TO DEWATERING.						
R	535.17	551.69		THERE IS A CHANGE IN CORE TO BEDDING ANGLES FROM TOP TO BOTTOM						
R	535.17	551.69		OF INTERVAL -ALSO THERE ARE LOCAL FRAGMENTS- HOWEVER,						
R	535.17	551.69		DEFORMATION APPEARS TO BE LOCAL SLUMPING AND IS NOT WIDESPREAD						
R	535.17	551.69		ENOUGH TO BE A PRHM.						
/	548.62	549.25	0.63	3 VEIN DS		R	V/	90 >3		D-
L										
R	548.62	549.25		VEIN IS PARALLEL TO CORE AXIS - IT COMPRISES 30% OF INTERVAL						
R	548.62	549.25		WITH OTHER 70% BEING ARSI.						
/	549.25	549.25	0.00	X ARSI DS	LM DB 0 4 = 4	R	2 BD	T55		D.
/	550.44	551.19	0.75	2 VEIN DS		R	V/	90 >2		D-
L										
R	550.44	551.19		VEIN IS PARALLEL TO CORE AXIS - IT COMPRISES 20% OF INTERVAL						
R	550.44	551.19		WITH OTHER 80% BEING ARSI.						
/	551.40	551.40	0.00	X ARSI DS	LM DB 0 4 = 4	R	1 BD	T60		D.
/	551.69	564.56	12.87	ARSI PY	SH= SS 0 2 2 2	P				D-
L				4A	SI2 2				C.	V-

/	591.43	602.24	10.81	X GRIT	*S-	NT7	R	V-	V.
L				4A		2 (-	MU2		
R	591.43	619.70		INTERVAL IS DISTINCTIVE IN THAT THE MATRIX IS SANDY;					
R	591.43	619.70		ONE LARGE ARG1 FRAG IS REPEATED. INTERVAL CONTAINS AT LEAST					

R	677.28	680.52	APPEARS TO BE A LARGE FRAG.						
/	684.46	686.94	2.48	X	ARGL	0 3 1 3	R	<	D.
L					4A			C	

K	F	F	R	D	N	-	T	O	-	I	D	T	RECOV	ED	%	ROCK	IN	IN	NO1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	OZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2				
F	-	L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Y	G																																																

R 684.46 686.94 APPEARS TO BE A LARGE FRAG.

/ 686.54 723.59 35.05 ARG L GR 662 LM P 1 LM 90 < D-

L 3A C.

R 688.54 723.59 HARDLY BROKEN CORE. DRILLING PARALLEL TO STRONG BEDDING

R 688.54 723.59 FOLIATION.

/ FLT 689.39 693.42 4.12 X FAUL 649 R

L

/ SHR 720.24 722.58 2.14 7 VEIN GR 649 R >7 D)

L 6A

R 720.24 722.58 INTERVAL IS COMPLETELY BROKEN AND IS HARD TO DESCRIBE,

R 720.24 722.58 IT IS A LARGE QUARTZ VEIN INTRODUCED INTO ARG L.

/ FLT 722.58 723.59 1.21 X FAUL GR 66X R

L 2A

R 722.58 723.59 INTERVAL IS CARBONACEOUS GUDGE, IT APPEARS TO HAVE BEEN A ARG L.

/ 723.59 726.15 2.56 CHRT PY 584 F* 6R2 P < <

L 5A *C2 H* 3 M08 C.

R 723.59 726.15 INTERVAL IS LARGELY CHRT FRAGS WITH SOME ARG L FRAGS IN A MATRIX

R 723.59 726.15 OF ANGULAR CHRT GRIT.

/ 726.15 735.11 8.96 BRHT *S- F* R* 6R4 P < R.

L 4A *C. H* 2 + - M04 C. C.

R 726.15 735.11 INTERVAL IS A HETEROGENEOUS BRECCIA WITH CHRT, ARG L, LARGE CONG

R 726.15 735.11 ADD SAND FRAGS. SEVERAL ARG L FRAGS EXHIBIT SILIFICATION PRIOR

R 726.15 735.11 TO DEPOSITION. SOME PY REPLACEMENT OF CHRT IS EVIDENT.

/ 735.11 747.90 12.79 ARG L GR MX 0 3 = 3 P < <

L 2A C- C.

R 735.11 747.90 INTERVAL IS A MASSIVE BLACK ARG L. THERE IS EXTENSIVE QUARTZ

R 735.11 747.90 MICROFRACTURING. AFTER THE VEINS ARE PYRITIC, AS WELL LOCALLY THE

R 735.11 747.90 VEINLETS HAVE BRECCIATED THE ARG L. AT 739.75 M, 10 CM OF BRHT

R 735.11 747.90 IS PRESENT, HOWEVER THE ENDS OF THE FRAG DO NOT APPEAR TO MATCH

R 735.11 747.90 THE ADJOINING CORE.

/ 747.90 751.00 3.10 BRHT GR SS 009 P < R.

L 3A 2 . JM- C. C.

R 747.90 751.00 INTERVAL IS LOCALLY BROKEN. CONSEQUENTLY IT IS SOMETIMES

R 747.90 751.00 DIFFICULT TO OBSERVE THE NATURE OF THE CORE. AT TOP OF INTERVAL

R 747.90 751.00 THERE ARE SOME CHRT AND CONGLOMERATE FRAGS, THE REST OF

R 747.90 751.00 INTERVAL IS ARG L BRECCIA (BRHT).

/ 751.00 757.20 6.20 BRHT PY GR 581 F* R* PS6 P < R(

L 3A R* 2 L03 C.

R 751.00 757.20 MOST OF THE CHRT OCCURS IN FRAGMENTS OF SAND.

/ 757.20 763.00 5.80 BRHT RS9 P D(

L 2A

/	833.72	843.80	9.88	EGSX	CR	HA	CR*	SS	BR	P	<+	C*	#=	D*
L					AA	PY			LB					#+

G E O L O G

K	F	F	R	O	M	-	T	O	-	I	N	T	REC'DV	MD	%	ROCK	IN	TM	Q1	TX	TX	F	C	%	M	ARG	RI	1	ID	AZM	DIP	QZ	FL	CY	CA	BA	XX	PY	CP	GL	YY	A	1	A	2			
E	-L-	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
Y	G												R	N	D	AGE	EV	R	L	C	IN	Q2	TX	TX	S	C	O	O	CHT	2	ID	AZM	DIP	MG	MU	CL	SD	QS	HA	PR	MT	SL	HA					

R	833.72	843.60	UNIT IS DOMINANTLY ARGILLITE WITH LOCAL LAM SULPHIDES.
R	833.72	843.60	UNIT HAS SUBSEQUENTLY UNDERGONE SOFT SEDIMENT DEFORMATION
R	833.72	843.60	RESULTING IN SLUMP TEXTURES AND BRECCIATION.
R	833.72	843.60	SULPHIDE MUD HAS BEEN REWORKED INTO BRECCIA INTERSTICES - STRONG
R	833.72	843.60	OVERPRINTING HAS RESULTED IN BRECCIATION AND IN FILLING BY QZ/BA
R	833.72	843.60	VEINING WITH MINOR SL, GL AND PY. HIGH APPARENT S.G OF ARGL AND
R	833.72	843.60	PRESENCE OF BARITE SLIPS SUGGEST A HIGH BARIUM CONTENT IN THE
R	833.72	843.60	ARGILLITE ALTHOUGH THIS IS NOT EVIDENT MEGASCOPICALLY.
R	833.72	843.60	NO DISCRET BARITE BANDS ARE PRESENT. DISRUPTED CHERT BANDS
R	833.72	843.60	OCCUR LOCALLY.

7	841.33	841.65	6.32	X ANGL CR	ST1 AX	R
---	--------	--------	------	-----------	--------	---

Z	841.65	842.50	0.89	X LMSX	PY1 SS RR	R	L1
L							L=
R	841.65	842.54	THIS INTERVAL EXHIBITS STRONG LAMINATED CHARACTER.				

R	841.65	842.54	EXCELLENT PRIMARY TEXTURES SHOW DISTURBED BEDDING FEATURES.
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K	LS1	845.60	843.60	0.00
---	-----	--------	--------	------

/	843.50	853.50	9.90	BRNM PY	US9	P	<.	C.	D*
L				4A				C.	

R	843.50	853.50	THE ARGILLITE IS AN ARSL WITH 10% SILT AND SAND.
---	--------	--------	--------------------------------------------------

✓ SHR 852.27 853.50 1.23 X FAUL 6.2 R
L 2A

/	853.50	859.84	6.34	BRIM PY	*53	PQ6	P	<*	<. C.	D)
1				4A		1				

R 853.50 659.84 10% OF THIS INTERVAL IS INTERBEDDED CHERT.

/	SHR	859.74	859.84	0.10	X FAUL	R
1					2A	

7	859.84	865.24	6.40	ARSI PY CR	LM RD	P 1 LM	U50 <(6*
1				4A	SS	2 RD	U50	

R	859.84	866.24	UNIT IS SLIGHTLY CARBONACEOUS. AN UNKNOWN BLACK MINERAL OCCURS
R	859.84	866.24	IN SOME OF THE QUARTZ VEINS. PYRITE ALSO OCCURS WITHIN THE
R	859.84	866.24	CENTRAL PART OF THE QUARTZ VEINS.

1	866.24	670.72	4.48	SAND PY	MX BD	P 2 BD	U55	D)
				7A				

/	866.24	866.34	0.10	X BRHT PY	R* R* 3 4 5 4 LN5	R	D+
L				6A	F* LM5		

/	868.00	868.00	0.00	X SAND PY	MX BD	R 2 BD	U60	00
---	--------	--------	------	-----------	-------	--------	-----	----

/	570.00	570.00	0.00	X SAND PY	EX BD	R 2 BD	U60	00
---	--------	--------	------	-----------	-------	--------	-----	----

870.72	879.79	9.07	BRHM PY	*SS	QR5	P	<	0+
			4A					

	Interval	Start	End	Width	Description	Core	Depth	Notes	Grade	Comments
/	879.79 - 899.11	879.79	899.11	19.32	BRHM PY 3A	QR9	P	D= C.	D)	
L	879.79 - 899.11	879.79	899.11		10% OF THIS INTERVAL IS REPRESENTED BY SANDSTONE FRAGMENTS					
R	899.11 - 899.61	899.11	899.61	0.50	ARSN PY 6A	SIG LM SS 5 2 RD 6	3 4 2 4 6	P 1 LM 2 RD	U55 U55	D*
/	899.61 - 900.29	899.61	900.29	0.68	ARS1 PY 2A	LM // SS		P 1 LM	U50 <=	D)
L	900.29 - 900.29	900.29	900.29	0.00						
R	900.29 - 900.77	900.29	900.77	0.48	BRHT SL PY 7A GL GL+ H* R*	MN5 KM2	H* F* H* R*	P	<. 62	6+ 61 62
/	900.29 - 900.77	900.29	900.77		UNIT IS SLIGHTLY CALCAREOUS.					
L	900.77 - 901.01	900.77	901.01	0.24	BRHT CH SL 7A GL	*S2 H* R*	B* F* H* R*	P3 M3	<. D=	D) D. 6+ 6= 62
/	901.01 - 901.62	901.01	901.62	0.61	BRHT CH SL 7A GL		B* F* H* R*	OP6 MO3	P	D. D.) 8(6)
L	901.62 - 901.92	901.62	901.92	0.30	FGSX SL GL TS PY			P	D. D.)	D= 6- PU 63 6.
R	901.62 - 901.92	901.62	901.92		THIS UNIT HAS BEEN SATURATED BY SPHALERITE, MAY INDICATE THE CLOSE PROXIMITY OF THE ORE ZONE. SL & GL OCCUR AS BRECCIA MATRIX FILLING; FRAGS IN BRECCIA ARE SIMILAR TO UNITS ABOVE.					
R	901.62 - 901.92	901.62	901.92							
K	901.92 - 901.92	901.92	901.92	0.00						
/	901.92 - 902.38	901.92	902.38	0.46	BRHM PY 2A	*S=		OP9	P	D=
L	901.92 - 902.38	901.92	902.38						C.	
/	902.38 - 902.59	902.38	902.59	0.21	BRPM 6A	F* B* H* R*		P	<. D.	D. 0. 0.
L	902.59 - 921.41	902.59	921.41	18.82	BRHM PY 5A			PD9	P	<* C. C= D(<) D) 6. 6.
R	902.59 - 921.41	902.59	921.41		THIS UNIT IS A BRECCIATED ARSI, WITH 10% OF IT BEING REPRESENTED BY THE SAND CONTENT. THE MAJORITY OF THE CORE IS BADLY BROKEN.					
R	902.59 - 921.41	902.59	921.41		SPHALERITE AND GALENA OCCUR WITHIN QUARTZ-SIDERITE VENTS AND IN SANDSTONE UNITS.					
R	902.59 - 921.41	902.59	921.41							
/	904.71 - 905.13	904.71	905.13	0.42	X SAND PY SL 7A GL	3 4 6 4 6		R	<=	D= D* D)
L	904.71 - 905.13	904.71	905.13		FRAGMENT CONTAINING DISSEMINATED SPHALERITE.					
R	906.48 - 906.73	906.48	906.73	0.25	X FAUL QZ 7A			R	<5	D*
L	906.48 - 906.73	906.48	906.73		QUARTZ FILLED SHEAR ZONE.					

[illegible]

Z	909.14	909.31	0.17	X FAUL	024	R	<S		D*	D.
L				7A						D.
R	909.14	909.31		QUARTZ FILLED SHEAR ZONE.						
Z	916.84	917.75	0.91	X FAUL		R	<*		D=	D=
L								C*	<=	D=
R	916.84	917.75		SPHALERITE AND GALENA OCCUR WITHIN QUARTZ-SIDERITE VEINS.						
Z	921.41	932.27	10.86	ARSN PY	IR SS 3 4 7 4	P	1 LN	U65	<=	D*
L				6A	LC 6		3 RD	U65	<*	
R	921.41	932.27		LOCALIZED AREAS BRECCIATED BY QUARTZ-SIDERITE VEINS.						
Z	932.27	939.54	7.27	ARSN PY	IR SS 3 4 2 4	P	1 LN	U45	<C	D=
L				5A	6		5 B D	U45	C .	<C
Z	936.34	938.57	0.23	X CHER	IR	R	4 RD	U40		
L				7A						
Z	936.97	939.00	0.03	X CHER	IR	R	3 RD	U40		
L				7A						
R	938.97	939.00		SIMILAR CHART BANDS OCCUR IN DRILL P1-68 BETWEEN 876.91 AND						
R	938.97	939.00		878.00 M. STILL UNABLE TO DETERMINE EXACT STRATIGRAPHIC						
R	938.97	939.00		LOCATION OF 68E IN RELATION TO OTHER SOUTH ZONE HOLES WITH						
R	938.97	939.00		REFERENCE TO ORE ZONE LOCATIONS AND WHETHER OR NOT WE ARE BELOW						
R	938.97	939.00		THE THIRD ORE ZONE.						
Z	939.54	943.00	3.46	BRHM PY		PQ8	P		<=	6)
L				4A	2				C.	<=
R	939.54	943.00		20% OF THIS UNIT IS REPRESENTED BY SANDSTONE AND ARSN FRAGS.						
Z	943.00	947.01	4.01	CGPS PY	*S1	OP2	P			D.
L				7A		LN7			C.	
Z	947.01	956.16	9.15	BRHM PY	*S1 F* H*	PQ5	P		<.	D)
L				6A	R* B* 3 1 1 0	JM=			C=	<=
R	947.01	956.16		INTERVAL IS MAINLY ARSN & CGCP CLASTS.						
Z	956.16	968.04	11.88	CGCP PY		MO3	P		<=	6)
L				6A	2	MO7			6=	
R	956.16	968.04		SIMILAR ARGILLITE FRAGMENTS THAT HAVE BEEN PYRITE REPLACED AS						
R	956.16	968.04		FOUND IN P1-68 FROM 873.86 - 879.96 M. BIMODAL SORTING IS						
R	956.16	968.04		APPARENT THROUGHOUT THIS INTERVAL.						
Z	968.04	972.10	4.06	CGHR GR	SH	MO5	P			
L										
R	968.04	972.10		GRADATIONAL WITH ABOVE CGCP, CONTAINS HIGHER CONTENT OF						
R	968.04	972.10		ARGILLITE FRAGS.						
Z	972.10	980.54	8.44	BRHM PY	F* B*	PQ6	P		<.	6)
L				4A	B*	3 LN)			C.	D.

R	972.10	980.54	SPHALERITE FOUND AS A REPLACEMENT MINERAL WITHIN SOME CHERT
R	972.10	980.54	CLASTS. THIS UNIT ALSO CONTAINS 30% SAND IN SANDSTONE FRAGMENTS
R	972.10	980.54	AND IR ARSE FRAGMENTS. CHERT IS BROKEN OVER THE ENTIRE INTERVAL.
R ASY	58.52	78.94	CHECK AZIMUTH VALUE.



CORDILLERAN ENGINEERING

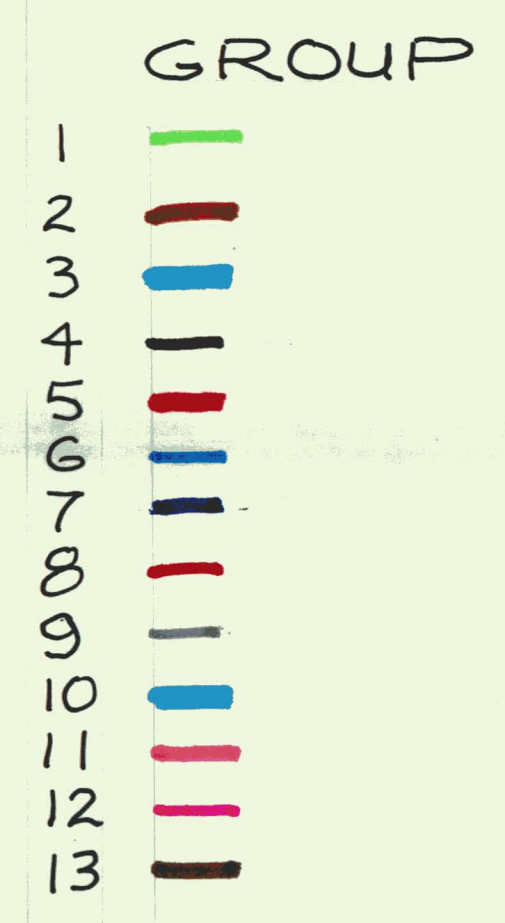
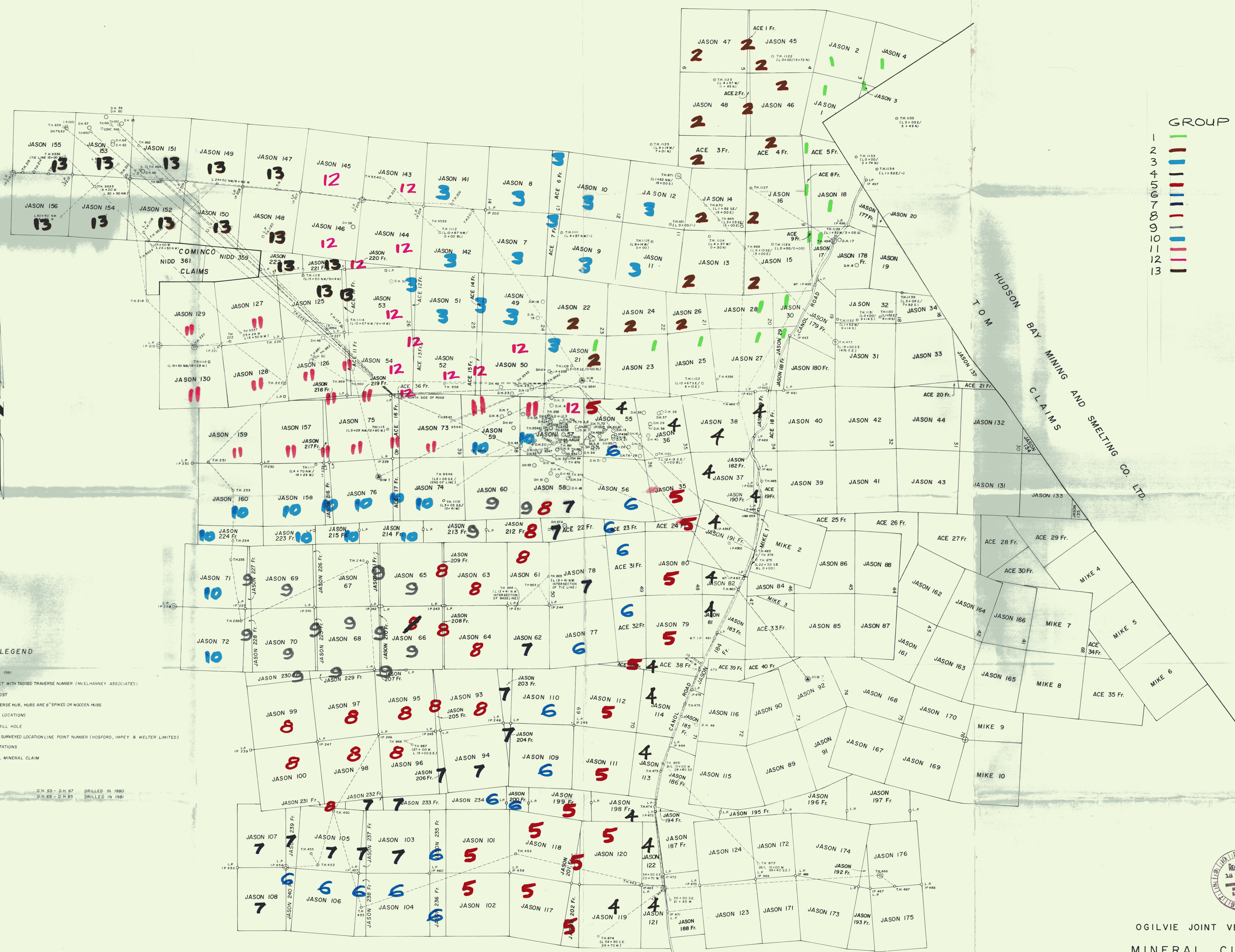
1 9 8 1 DIAMOND DRILL SUMMARY RECORD

PROPERTY: JASON

N.S. - Not Surveyed

HOLE No.	NORTHING	EASTING	ELEV'N	SECTION	INCLINATION	AZIMUTH	CASING	CLAIM	% REC'Y	DATE START	DATE FINISH	REMARKS	HOLE LENGTH	TOTAL
81-68	700 2472.41	436 496.30	1275.94		-90°		12.19	Jason 57		May 17D	June 30N	HQ 228.30 NQ 743.09	971.39	971.39
81-69	700 2950.93	436 447.97	1347.38		-80°	180°	17.37	Jason 21		May 20D	Aug 13D	HQ 170.08 NQ 431.29 BQ 441.96	1043.33	2014.72
81-70	700 2575.52	436 528.84	1296.71		-80°	177°	5.49	Jason 57		June 7D	Aug 12D	HQ 54.25 NQ 793.40	847.65	2862.37
81-71	700 2550.10	436 733.96	1253.00		-50°	020°	15.24	Jason 55	76.7	June 8D	June 15N	HQ 108.20	108.20	2970.57
81-72	700 2550.10	436 733.96	1253.00		-75°	020°	8.84	Jason 55	87.2	June 16D	June 23N	HQ 203.00	203.00	3173.57
81-73	700 2474.33	436 718.67	1236.10		-70°	020°	3.66	Jason 55		June 25D	June 26D	HQ 24.99	24.99	3198.56
81-74	700 2473.89	436 718.43	1236.10		-80°	020°	3.66	Jason 55	77.7	June 26D	July 11D	HQ 274.93	274.93	3473.49
81-68A					BRANCH		---	Jason 57		July 6D	Aug 9N	NQ 345.95w to 862.89	516.94	3990.43
81-75	700 2472.54	436 719.52	1235.54		-82°	018°	4.27	Jason 55		July 11N	Aug 19D	HQ 486.77 NQ 67.05	553.82	4544.25
81-76	700 2568.49	436 555.34	1296.37		-59°	005°	3.05	Jason 57		Aug 14N	Aug 25N	HQ 168.25	168.25	4712.50
81-70A					BRANCH		---			Aug 17D	Sept 30N	NQ 437.69w to 910.44	472.75	5185.25
81-68B					BRANCH		---			Aug 14D	Aug 19D	NQ 677.57w to 806.80	129.23	5314.48
81-77	700 2472.73	436 719.94	1235.53		-76°	018°	4.24	Jason 55		Aug 21N	Sept 6N	HQ 121.01 NQ 177.08	298.09	5612.57
81-78	700 2568.19	436 555.34	1296.37		-83°	355°	5.79	Jason 57		Aug 26N	Sept 17N	HQ 338.94 NQ 89.61	428.55	6041.12
Caron 81-79	700 4716.64	432 979.60	1362.88		-60°	210°	3.28	Jason 155		Sept 4D	Sept 16D	HQ 137.27 NQ 266.59	403.86	6444.98
81-68C					BRANCH		---			Aug 20N	Sept 10D	NQ 214.58w to 726.34	511.76	6956.74
81-80	700 2524.25	436 837.19	1219.65		-83.5°	015°	16.99	Jason 55		Sept 7N	Sept 15D	HQ 249.02	249.02	7205.76
81-68D					BRANCH		---			Sept 11D	Oct 2N	HQ 58.52w to 67.67 = 9.15 NQ 681.22	690.37	7896.13
81-81	700 2524.55	436 837.19	1219.65		-65°	025°	15.76	Jason 55		Sept 16D	Sept 23N	HQ 109.73	109.73	8005.86

NS



LEGEND

○ LOCATION TARGETED 1981
□ IP 230 DENOTES IRON POST SET WITH TAGGED TRAVERSE NUMBER (MCELHANNAY ASSOCIATES)
□ L.P. DENOTES LOCATION POST
□ T.H. 233 DENOTES TAGGED TRAVERSE HUB, HUBS ARE 6" SPIKES OR WOODEN HUBS
(60SK/15NW) DENOTES GRID LINE LOCATIONS
○ D.H. 34 DENOTES DIAMOND DRILL HOLE
48 DENOTES PREVIOUSLY SURVEYED LOCATION LINE POINT NUMBER (HOSFORD, IMPEY & WELTER LIMITED)
● HW 1, HW 6 DENOTES CONTROL STATIONS
Fr. DENOTES FRACTIONAL MINERAL CLAIM
B/L DENOTES BASELINE
WT. DENOTES WITNESS

D.H. 1 - D.H. 7 DRILLED IN 1975
D.H. 8 - D.H. 20 DRILLED IN 1976
D.H. 21 - D.H. 26 DRILLED IN 1977
D.H. 27 - D.H. 43 DRILLED IN 1978
D.H. 44 - D.H. 52 DRILLED IN 1979

EXPIRY YEAR

1982
1983
1984
1985
1986
1987
1988
1989
1992
1995-1997
2000-2005

NOTE: ALL CLAIMS HAVE COMMON EXPIRY DATE OF DEC. 31.

Ogilvie Joint Venture
MINERAL CLAIMS
JASON PROPERTY
MACMILLAN PASS AREA (N.T.S. 1050-1)
MAYO AND WATSON LAKE MINING DISTRICTS, YUKON TERRITORY

SCALE IN METERS

BY
CORDILLERAN ENGINEERING
1418 - 305 BURNARD STREET
VANCOUVER, B.C. V6C 2B8

DECEMBER 1981

PLATE 1